

SOIL AND MATERIAL CONSULTANTS, INC.

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> September 1, 2020 File No. 24919 UPDATED

Mr. Duane O'Laughlin, P.E. Ciorba Group 8725 W. Higgins Road, Suite 600 Chicago, IL 60631

> Re: Phase II Roadway Geotechnical Report Clavey Road Reconstruction US 41 to Green Bay Road FAU Route 1265 Section No. 15-00125-00-PV Highland Park, Illinois

Dear Mr. O'Laughlin:

This is an updated report to reflect changes to the project limits and incorporate IDOT review comments. The following is our report for the pavement investigation and soil survey completed along approximately 5,745 feet of Clavey Road between US 41 and Green Bay Road in the City of Highland Park, located within Cook County, Illinois.

The investigation was requested to determine current subsurface soil and water conditions at all boring locations. Additionally, a core was performed to determine the pavement section at a location on Green Bay Road. The findings of the field investigation and the results of laboratory testing are intended to assist in the planning, design and construction of proposed roadway improvements. We understand it is proposed to reconstruct Clavey Road from Sta. 25+90 to Sta. 32+00.

SCOPE OF THE INVESTIGATION

Our investigation included a total of 18 soil borings and 1 pavement core at various locations shown on the attached sketches. Additionally, Geocon Professional Services obtained 6 borings in April of 2017 east and west of the Clavey Road Bridge over the Skokie River which are included for reference in this report. The borings were auger drilled and sampled to a depth of 10.0 feet. Soil samples were obtained using a split barrel sampler advanced utilizing an automatic SPT hammer.

All pavement materials and soil samples obtained during the field investigation were returned to our laboratory for testing. The soil samples were group classified and soil moisture contents determined. Additional testing included determination of dry unit weight, unconfined compressive strength (by a calibrated RIMAC compression tester), organic content, grain-size distribution, Atterberg limits, Illinois Bearing Ratio, and related testing. The results of all field and laboratory testing are included in summary with this report.

8 W. COLLEGE DR. • SUITE C • ARLINGTON HEIGHTS, IL 60004

SITE GEOLOGY/USDA SOIL TYPING

Enclosed is a map indicating the pedological characteristics of the site as determined by the USDA Soil Conservation Service. The soils indicated are a generalization of soil types and conditions anticipated to exist at or near existing surface elevations. Typically, these maps were developed without benefit of a direct on-site soil investigation. The soil typing map is presented for general information only.

<u>Symbol</u>	<u>Soil Types</u>
153A	Pella Silty Clay Loam – 0 to 2 percent slopes
153A+	Pella Silt Loam – 0 to 2 percent slopes, overwash
192A	Del Ray Silt Loam – 0 to 2 percent slopes
320A	Frankfort Silt Loam – 0 to 2 percent slopes
330A	Peotone Silt Clay Loam – 0 to 2 percent slopes
530B	Ozaukee Silt Loam – 2 to 4 percent slopes
530D	Ozaukee Silt Loam – 6 to 12 percent slopes
802B	Orthents, loamy, undulating
805B	Orthents, clayey, undulating
1330A	Peotone Silty Clay Loam – undrained, 0 to 2 percent slopes

CLIMATIC CONDITIONS

Climatic conditions for the period prior to obtaining site soil borings include the following information recorded at O'Hare International Airport in Chicago, Illinois:

Month		Total <u>Precipitation</u>	Departure From Normal	Average <u>Temperature</u>	Departure From Normal
October	2019	6.76 in.	+3.61 in.	50.9° F.	-1.6° F.
November	2019	1.87 in.	-1.28 in.	34.8° F.	-5.5° F.
December	2019	1.55 in.	-0.70 in.	34.0° F.	+6.3° F.
January	2020	2.80 in.	+1.07 in.	30.1 ° F.	+6.3° F.

The above information has been considered in our analysis of the site soil conditions.

EXISTING CONDITIONS

The existing pavement on Clavey Road is composed of 2 lanes with concrete curb and gutter. Adjacent land uses consist of both commercial and residential properties. Visual inspection of the existing pavement surface show areas of distress including meandering cracking, cold joint cracking, alligatoring, potholes, and previously patched areas. The pavement core was performed on Green Bay Road just north of Clavey Road to determine the existing pavement section. The summary table below indicates pavement materials and thicknesses encountered at the core location. Please refer to the individual core log for more detailed information.

	HMA	Portland Cement	Total
Core	Surface (in.)	Concrete (in.)	Pavement (in.)
C-201	4.5	8.75	13.25

BOLD indicates a failure in that layer of material

We performed a total of 18 borings along Clavey Road from Sta. 113+05 to Sta. 170+50. The pavement section from B-101 to B-117 consisted of 5.0 inches to 9.0 inches of concrete over 3.5 inches to 20.0 inches of granular base. The pavement section at B-118 consisted of 3.0 inches of bituminous concrete over 6.0 inches of concrete. The granular base for the pavement section at B-118 was 4.0 inches thick. The total pavement sections ranged from 9.5 inches to 30.0 inches.

Fill soil conditions were encountered underlying the pavement materials at borings B-102 to B-107. Composition of the fill includes the presence of silt/clay, clay/silt and silt/clay/sand mixtures extending to depths of 3.5 feet to 5.0 feet at these boring locations. The limits of fill placement were not determined within the scope of this investigation.

Underlying natural soil conditions include the presence of cohesive soils. These are classified as stiff to very hard clay/silt mixtures with lesser portions of sand and gravel. Non-cohesive soils were also encountered as indicated. These include very loose to medium dense silt/clay/sand, silt/sand, silt/clay, silt, and sand mixtures often found in a damp to very damp condition. Cobbles and boulders may be present within the site soils at any elevation, although none were encountered while drilling.

An organic silt deposit was encountered at borings B-102 to B-107. The deposit was present within 3.5 feet to 5.0 feet of the surface and ranged in thickness from 1.0 feet to 2.5 feet. These soils have extremely high moisture contents and low strengths.

SUBGRADE PREPARATION

Generally, normal subgrade preparation is anticipated for the reconstruction of Clavey Road. This would include the complete removal of the existing pavement section along with unsuitable surface conditions including vegetation, topsoil, unsuitable fill soils and other deleterious conditions which may be encountered. Any unsuitable soils should be removed to a distance of at least 1.0 foot behind the proposed new curb. Additional over-digging equal to the depth of fill required below the curb should be considered. An increased width of soil removal may be necessary when subgrade supported improvements such as sidewalks, drives or paved shoulders are planned. The soils in cut areas should be excavated to establish design subgrade elevations. After removal has been completed the soils should be compacted to a minimum of 95% compaction based on the standard proctor, AASHTO T-99 or ASTM D-698, within 1.0 foot of the surface. The exposed subgrade soils should then be proof-rolled or observed by the Soil Engineer if the width is too narrow for a proof-roll. If proof-rolling reveals unstable soil conditions due to high moisture contents, these soils should be aerated or removed. Discing and aeration of the soil can be effective to depths of up to 1.0 foot depending upon the equipment used. If the high moisture content condition extends to depths greater than the effective depth of discing, removal of the unstable soils will be necessary.

Based on the condition of the existing roadway we do not believe full depth removal of the organic silt is necessary. The soils should be evaluated in the field to determine if an undercut is necessary. If the exposed subgrade soils appear to have high moisture contents, they should be disked and dried, then reevaluated prior to performing an undercut.

We recommend including a plan quantity of Aggregate Subgrade Improvement (CY) equal to at least 25% of the planned full depth pavement area, assuming a thickness of 12 inches. This material should be used to replace any unsuitable soils encountered below the bottom of the improved subgrade layer that are encountered in the field during construction. The actual need for removal and replacement with Aggregate Subgrade Improvement should be determined in the field at the time of construction by the Geotechnical Engineer or soils inspector. All potentially unstable soils should be tested with a cone penetrometer and treated in accordance with Article 301.04 of the Standard Specifications for Road and Bridge Construction and the undercut guidelines in the IDOT Subgrade Stability Manual. Any material not needed for undercut replacement at the time of construction should be deleted from the contract with no extra compensation to the contractor.

Based on the above recommendation, there will be a need for two separate Aggregate Subgrade Improvement line items in the Schedule of Quantities (SOQ) included in the design plans:

• Aggregate Subgrade Improvement 12" (SQ YD) – This will be used for the 12 inch aggregate subgrade improvement below new pavement sections and widening pavement sections.

• Aggregate Subgrade Improvement (CU YD) – This will be used in locations where there are undercuts (below the 12 inch improved subgrade layer) where poor soils were removed.

Both of these line items reference back to the District One Aggregate Subgrade Improvement Special Provision.

We also recommend including a plan quantity of Geotechnical Fabric for Ground Stabilization (SQ YD) equal to at least 25% of the planned pavement area. We recommend placing geotextile fabric at the base of undercut areas where low strength subgrade soils are encountered. The 12 inches of improved subgrade is not considered an undercut, and we do not recommend placing the fabric at the base of the proposed 12 inch improved subgrade layer unless it is determined to be necessary to achieve stability by the Geotechnical Engineer or soils inspector at the time of construction. Fabric should meet the requirements of Article 210, Fabric for Ground Stabilization, of the SSRBC. Any material not needed at time of construction should be deleted from the contract with no extra compensation to the contractor.

Based on the project scope of work borings were not performed outside of the existing roadway. If work is planned outside of the existing pavement, we would estimate a 12" topsoil thickness. The actual need for topsoil removal should be decided in the field. We also recommend that the removed topsoil should be stockpiled, sorted, and reused for the proposed landscaping improvements.

Areas where fill is required to establish the design subgrade elevation should be prepared as indicated above. Properly prepared areas can then be filled using suitable onsite soils or an approved offsite source. Fill soil should be placed in lifts not to exceed 8.0 inches when uncompacted. Each lift should exceed the minimum compaction requirement prior to placement of the next lift. If high soil moisture content prevents achieving minimum compaction requirements then it will be necessary to disc and aerate the soil prior to final compaction. Compaction requirements also apply to backfill placement around structures and within trench excavations located beneath pavement areas.

The new pavement section should include the 12 inches of the District One Aggregate Subgrade Improvement Special Provision (April 1, 2016) in the design. For further reference, IDOT specifications for subgrade preparation are given in Section 301 of the Standard Specifications

FILL SOURCES

Material to be used as fill should meet the requirements of the District One Embankment I Special Provision. The onsite non-organic soils are generally suitable for use as backfill in undercuts where the use of select borrow is indicated. Offsite sources may also be used provided they are approved by the Soil Engineer. For road improvements constructed under the provisions of the Illinois Department of Transportation, soils are deemed unsuitable if the organic content is greater than 10.0% when tested in accordance with AASHTO T-194 and when the maximum density is less than 90 lbs./cu.ft. based on the standard proctor test, AASHTO T-99 or ASTM D-698. Aeration by discing or other mechanical means may be necessary to reduce the moisture content of the soil prior to compaction. This will most likely be necessary when the soil is borrowed from near the surface where seasonal fluctuations in soil moisture content as determined by the standard proctor test in order for the soils to meet or exceed minimum compaction requirements. We would recommend a shrinkage factor of 15% be used for earthwork calculations.

UNDERDRAINS

The presence of saturated conditions within the frost zone may deteriorate supporting soils. This results in inadequate support of the pavement section. To provide drainage for the proposed pavement areas, we recommend installing transverse pipe underdrains below the pavement in areas where the road will be completely reconstructed. Underdrains should be installed per Section 601 in the SSRBC and consist of Type 2 underdrains. Areas where there will be full width reconstruction should have longitudinal underdrains as well as transverse underdrains. The spacing of the transverse underdrains should be 300 feet and at all low points,

including pavement areas. In areas where the existing roadway section will be widened, longitudinal underdrains should be used. The underdrains should tie into the proposed stormwater drainage system.

PAVEMENT DESIGN

A representative subgrade soil sample from B-1 was obtained to determine an Illinois Bearing Ratio. The soil was classified as clay, A-4(13), and the IBR value was determined to be 3.0. If the Mechanistic Pavement Design will be used for these improvements, based on the test results a Subgrade Support Rating (SSR) of POOR is representative of the average condition.

SUBSURFACE WATER

Excavations may require dewatering due to subsurface water seepage and/or surface precipitation. This water can likely be removed to depths of several feet by standard sump and pump operations. If the soils exposed at undercut elevations are permitted to become saturated, loss of bearing strength and instability may occur, requiring additional soil excavation.

It should be noted that fill soils, organic soils, non-cohesive soils, and others can be quite unstable when saturated. These soils tend to cave or run when submerged or disturbed. Also, slope stability is minimal to non-existent as confining soil pressures are removed. Proper drainage within excavations is necessary particularly when excavations extend below anticipated water levels and below saturated soils.

The contractor should be made responsible for designing and constructing stable temporary excavations. Also, the contractor should shore, slope, bench or restrain the sides of the excavations as required to maintain stability of both the excavation sides and bottom. In no case, should the slope, slope heights, or excavation depth exceed those in the local, state, and federal safety regulations.

CONCLUSION

This report has been prepared to assist in initial determination of anticipated soil support conditions and needed subgrade treatments. Variations in existing pavement sections, soil conditions and ground water conditions may be present between these test locations.

An inspection by a Soil Engineer is recommended during subgrade soil preparation, particularly in the noted problem areas. A period of dry weather prior to the beginning of the earthwork may result in improved soil moisture content conditions near the surface and decreased subgrade soil preparation costs. A period of wet weather may create the need for increased discing and drying efforts. Problem soil conditions should be reviewed at the time of subgrade preparation to verify that planned treatments will be effective for the actual soil conditions encountered.

File No. 24919 - UPDATED Re: Clavey Road Reconstruction US 41 to Green Bay Road Highland Park, Illinois

Any questions concerning this report should be directed to our office.

Very truly yours,

SOIL AND MATERIAL CONSULTANTS, INC.

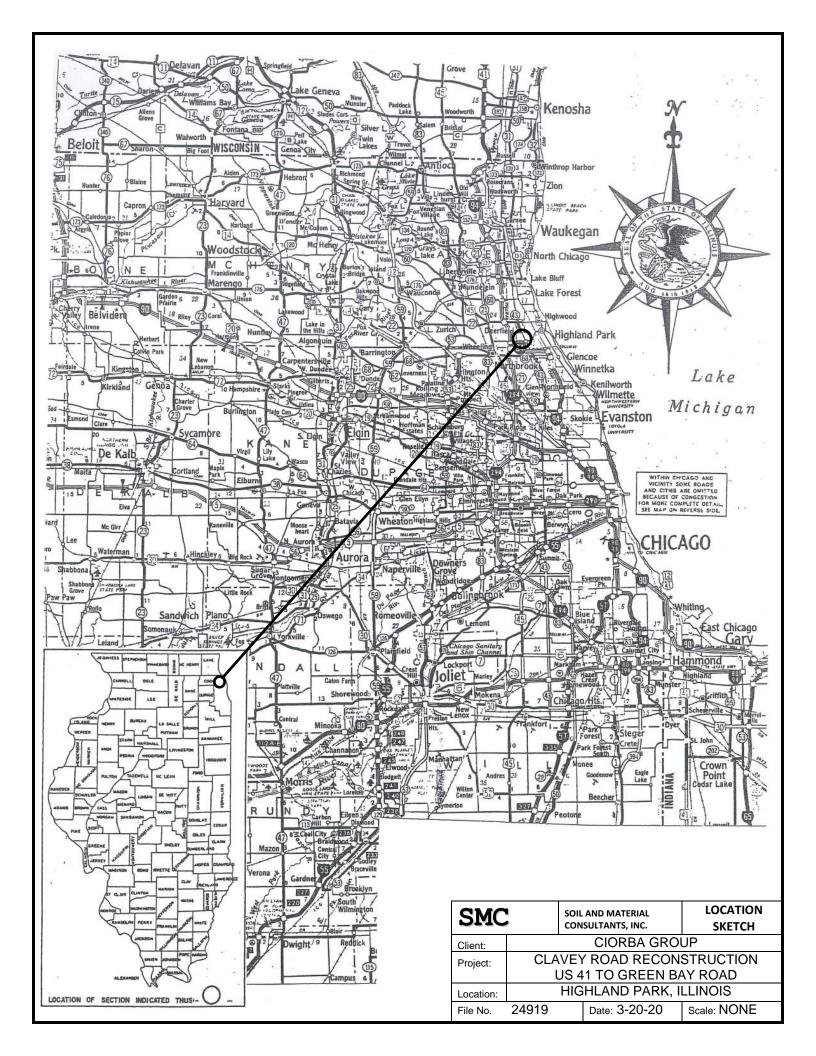
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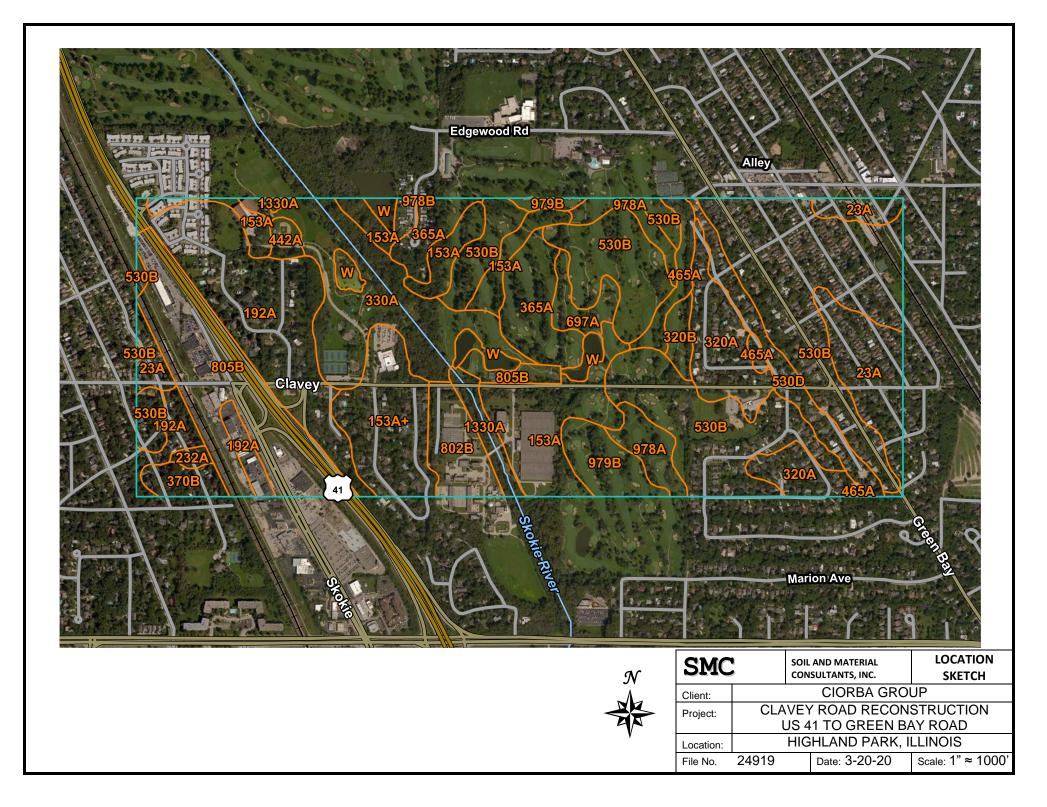
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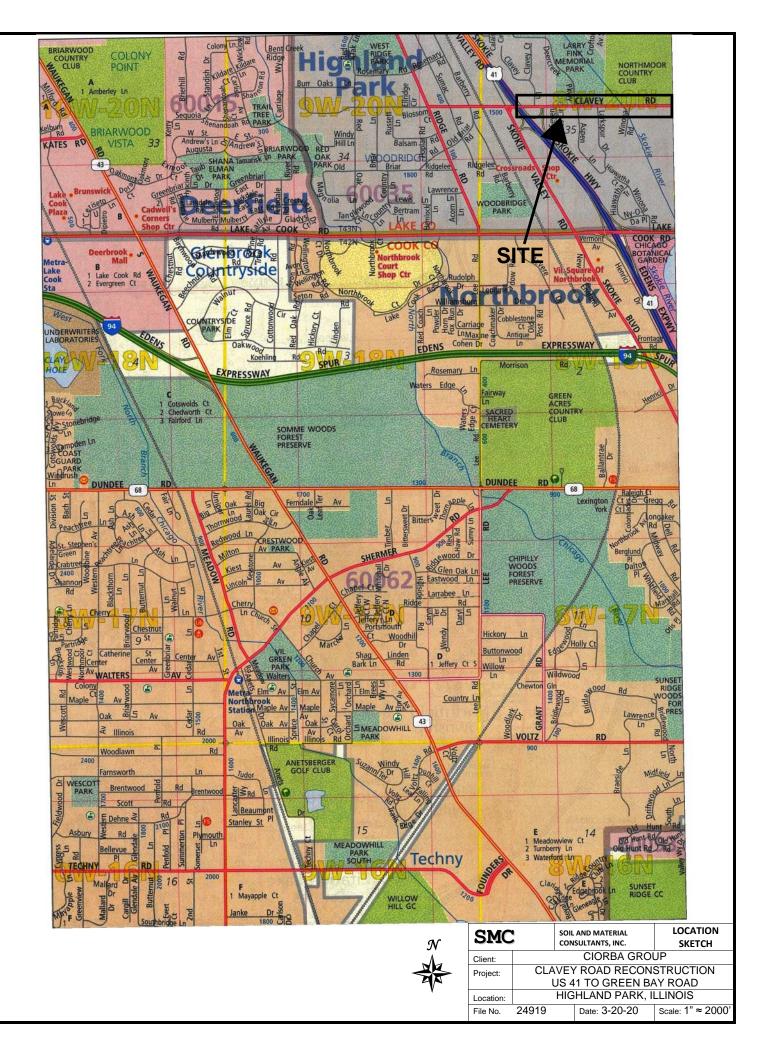
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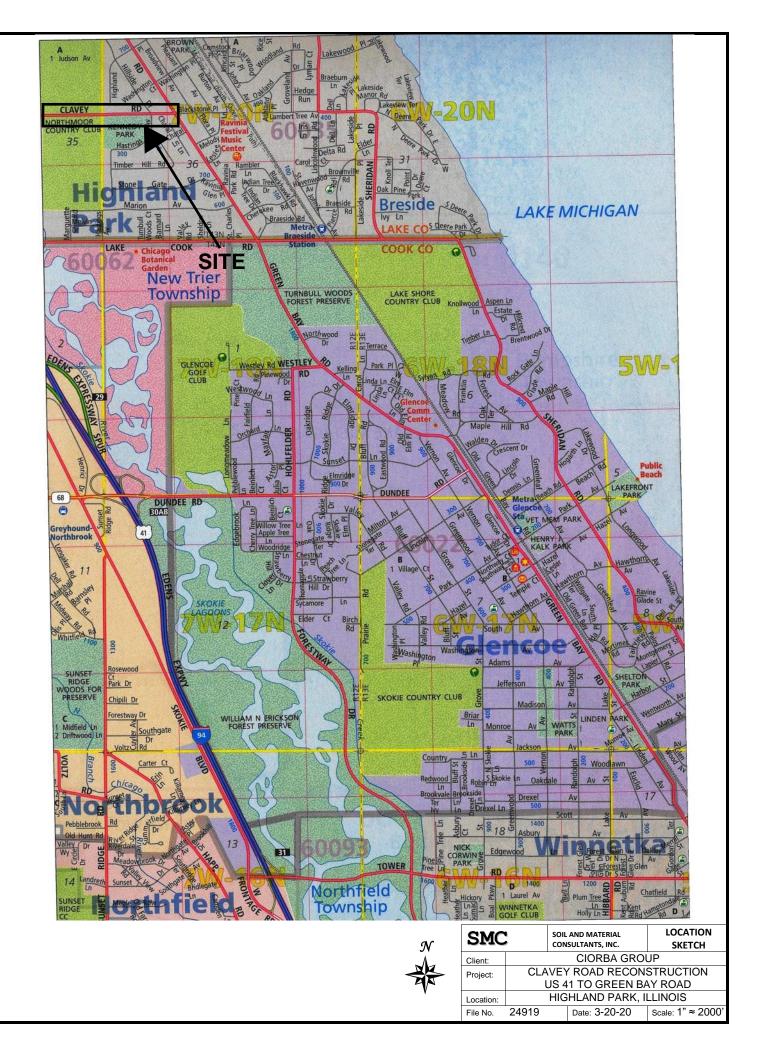
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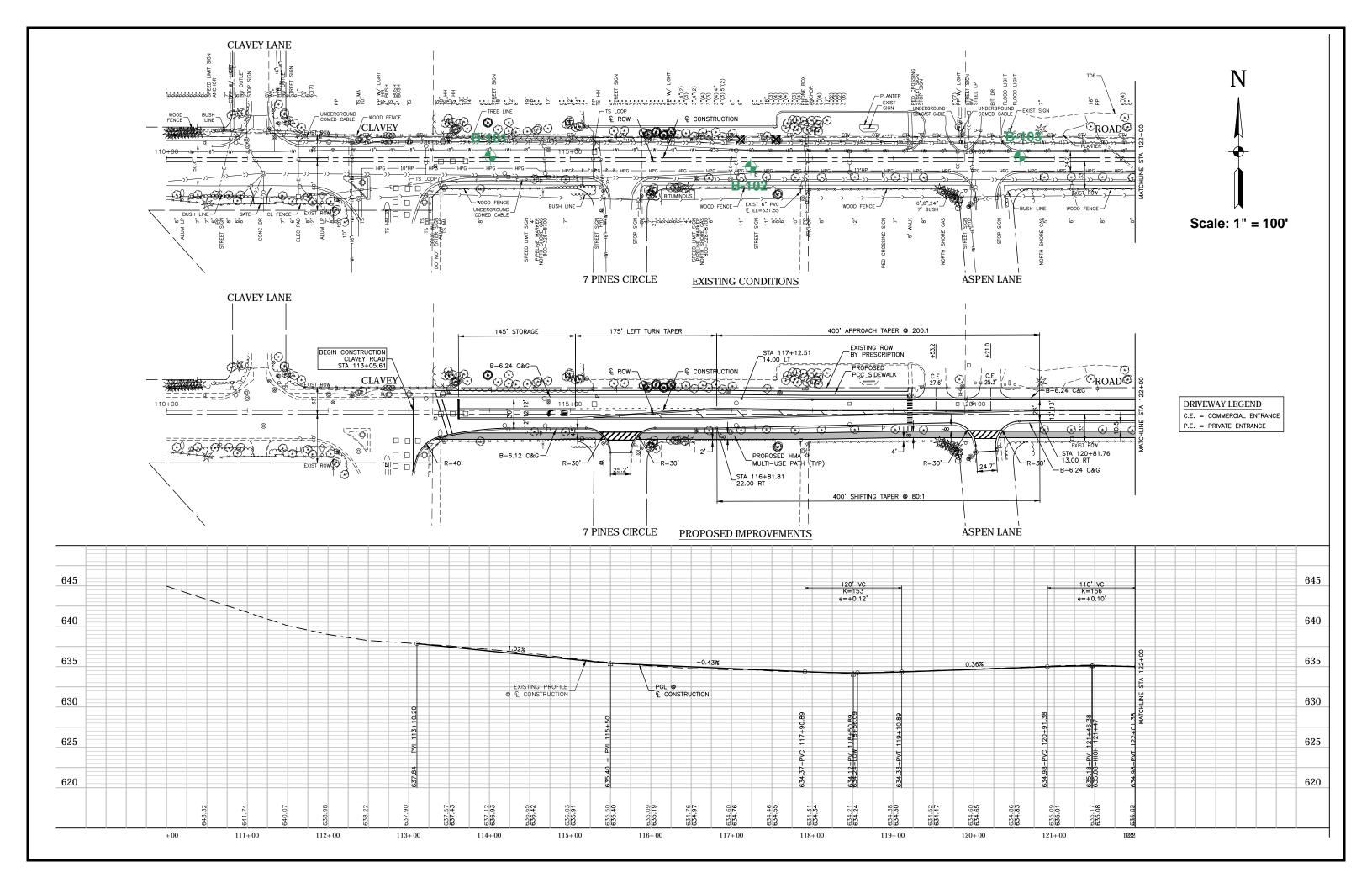
Thomas P. Johnson, P.E. President

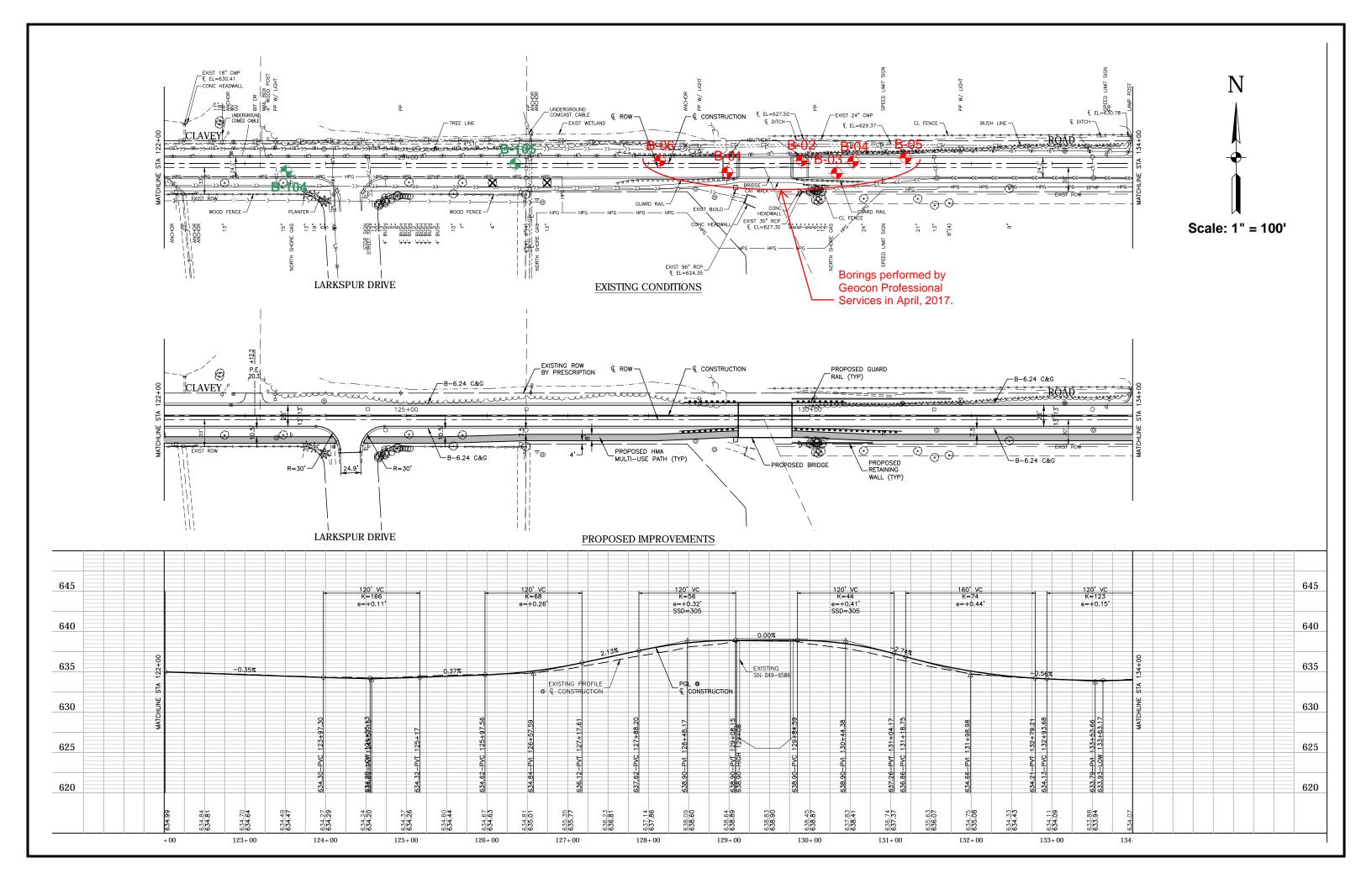


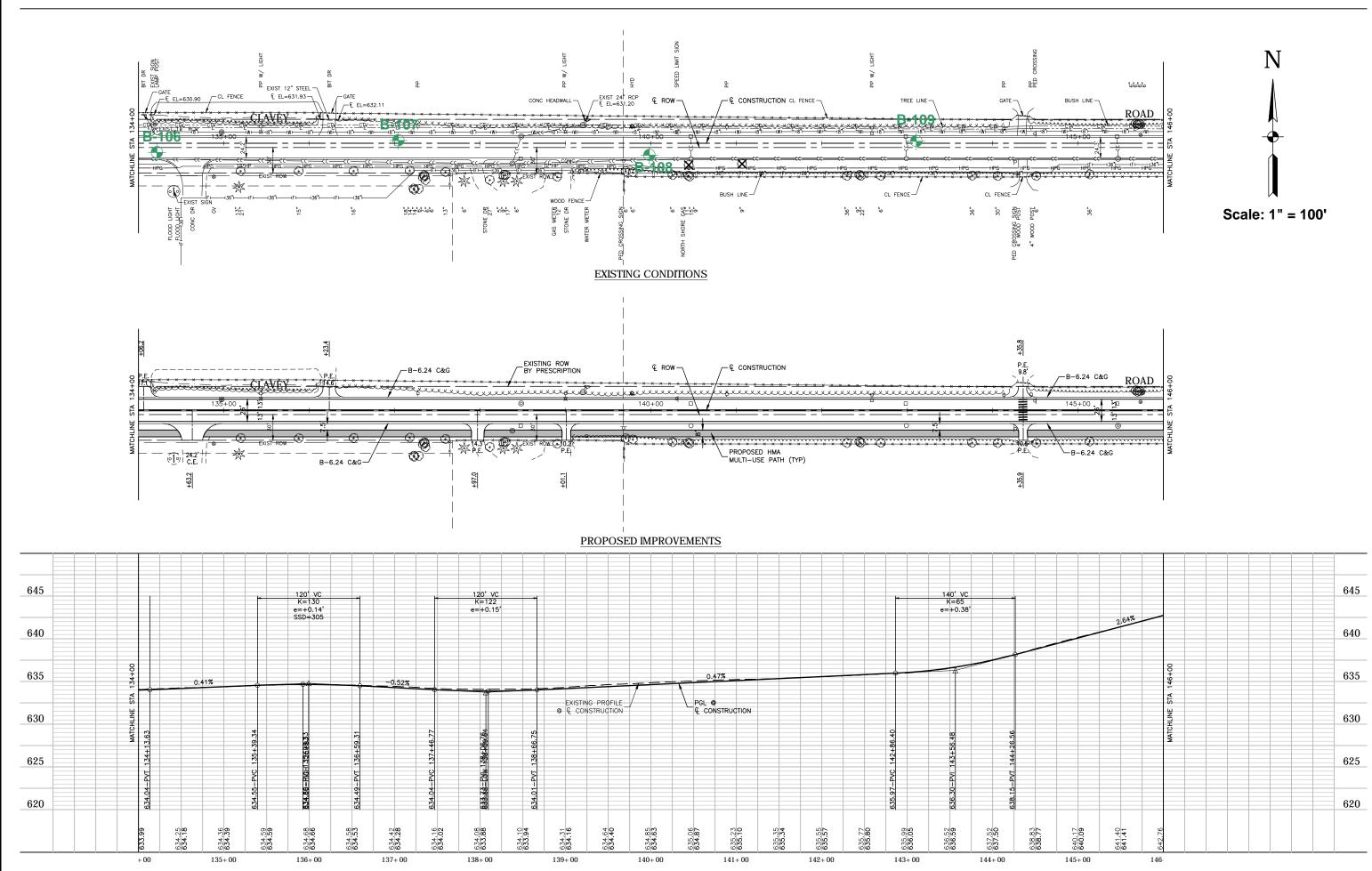


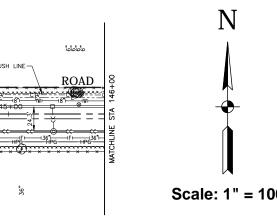


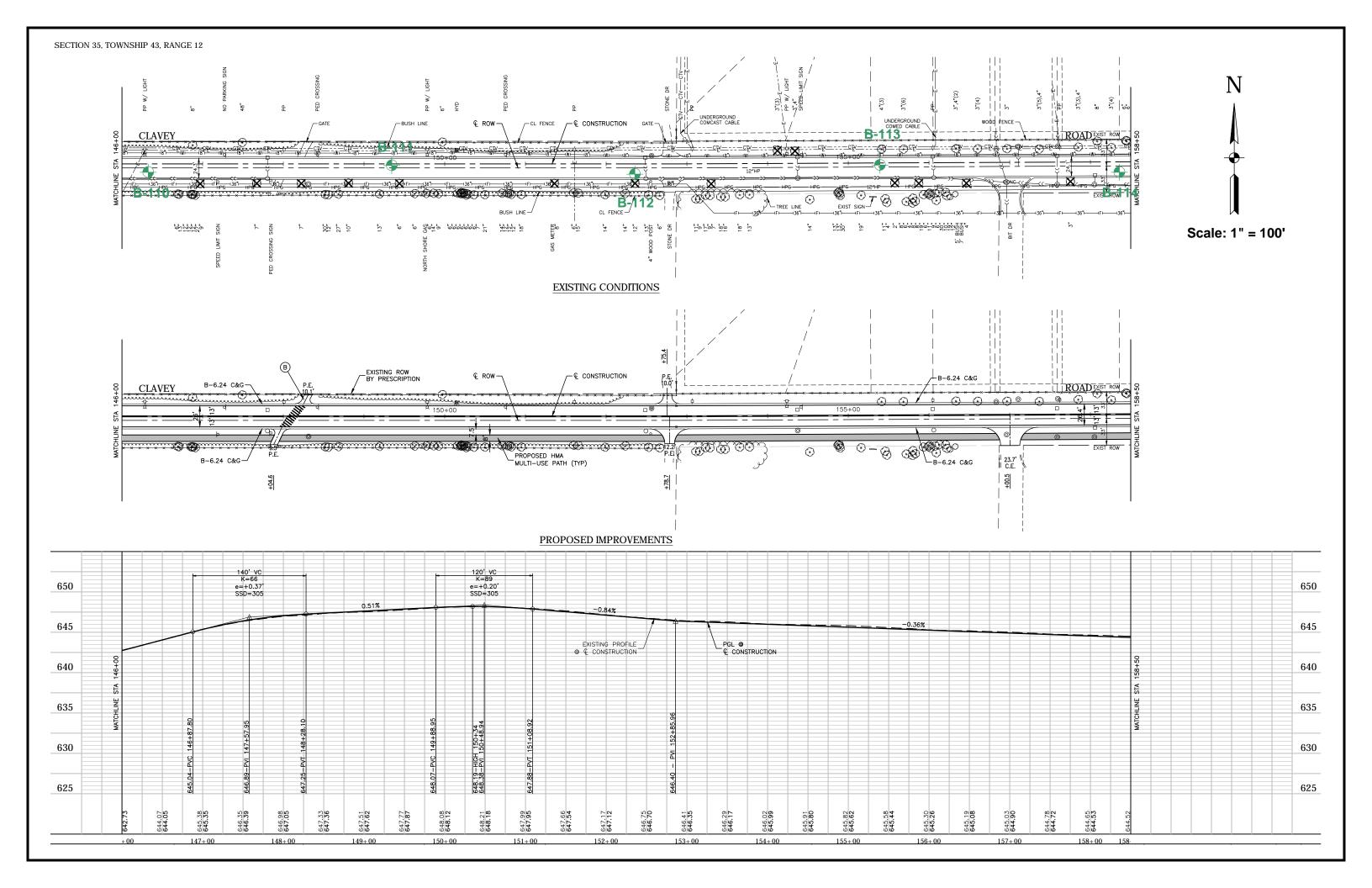


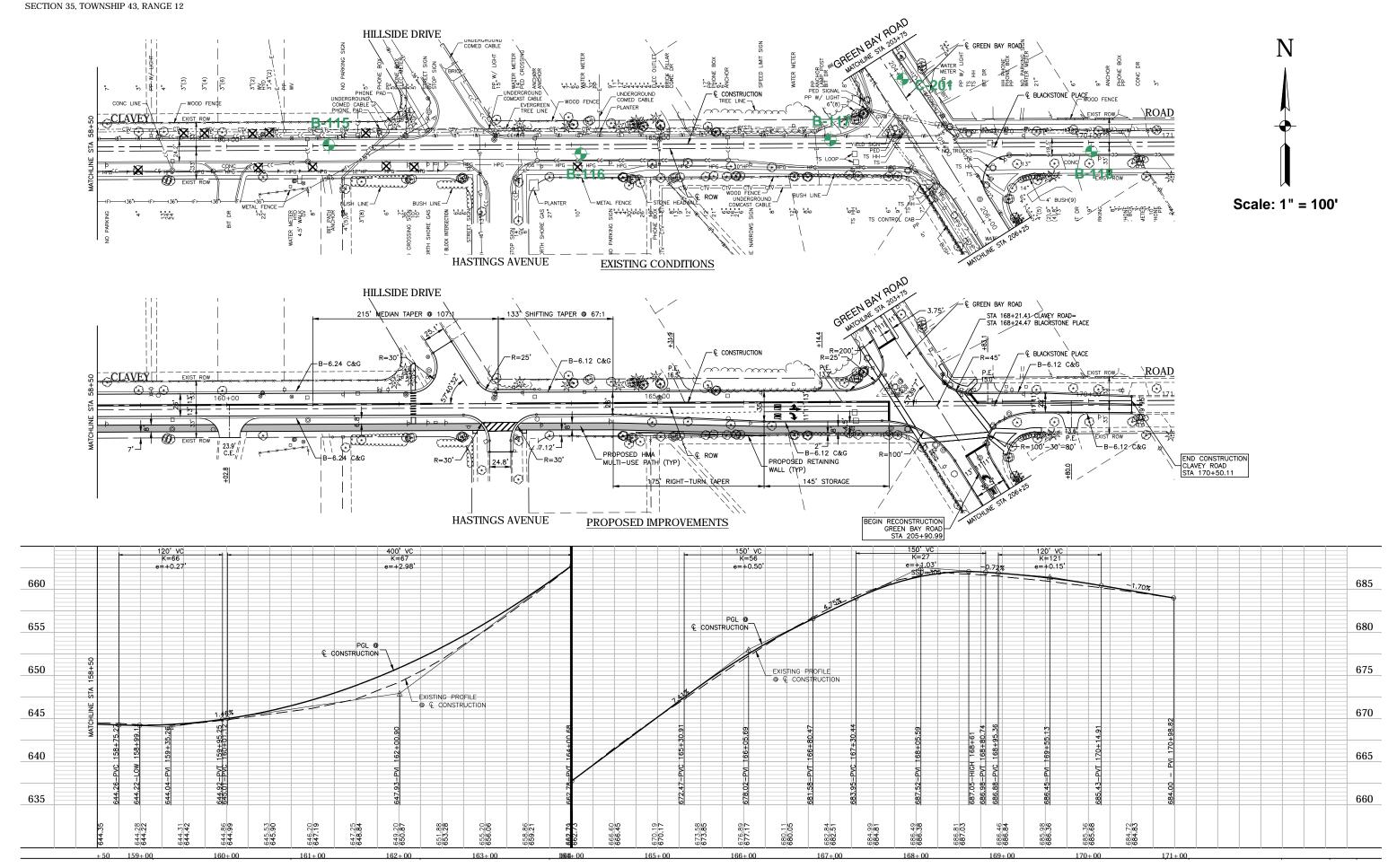


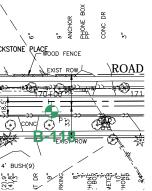


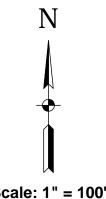












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-F-111b-1

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Qu - unconfined compressive strength, tons/sq. ft.

Comments Station 137 + 00	Project	τ			1		ructio Road	on	Date 2/2	18/2
	Locatio						nouu		d By	
	Equipn	nen	t 🖾 C	ME 4	5В 🗆	H.A. C]Other	Logge	ed By —	CS
Elev., ft. 634.5' Description Depth, ft.	0	S	Т	R	В	N	Pen.	W	Uw	Q
633.8'Concrete - 8.0"					2					1
633.0' Sand & gravel, damp, medium dense	()				13		1 . J.S			8
Brown-gray clay & silt,trace sand	_	1 2	SS	10"	5	10		6.2 18.5		
- & gravel,damp,stiff - Fill						1	Ţ	1		
631.0'	1		16		2	18				-
Black-dark brown organic silt,damp very loose 629.5'	?				1					
	5	3	SS	18"	2	3		143.1		2.10
Dark gray to gray silt, some clay, trace fine sand & organic matter,	9	, 8			- 1					
very damp, very loose				1.1		1.1				
승규는 것 같은 것 같은 것 같아. 것이 많은 것 같아.		,		1.011	1		2	28.3	e	
		4	SS	18"	<u>⊥</u>	<u>_</u>		20.3		-
	_						10		1.1.1.1	
625.5' Brown-gray clay, some silt, trace fi	ine			e	<u>1</u> 2					
624.5'sand,damp,stiff	10	5	SS	18"	3	5	1.0	28.1	102.9	1.
End of Boring	_							1		
						1				
				E	3		×.		12	1.1
_						-				
					1				· · · · ·	Ľ.
							_		5	
_	15	2				- ¹	1.0		 ? 	
									2	
							1		1.1	
-	_	2	à.		1		57 [°] ° .	-	:	
			7				(1 a -			
						1	1			
-	~		- 1					2		
			- 00	1		4	а 1911 г. – 1	а. Г.	· . · .	<u> </u>
	20				-			X		

Comments <u>Station 140 + 00</u>	Proje Locat	1	JS 4	1 to	Green	n Bay	Road		Date $\frac{2/1}{2}$	
	Equip	omen	t⊠C	ME 4	5B 🗆 I	H.A. C	Other	Logge	d By	SS
Elev., ft. 634.5' Description Depth,	ft. 0	S	Т	R	В	N	Pen.	W	Uw	Qı
633.9'Concrete - 7.0" 633.5'Brown sand & gravel,damp-5.0"					-			10		
Brown-gray silt, some clay, trace	_				6				1.1	4
632.0'sand & gravel, damp, medium dense		1	SS	18"	5 6	11		16.3		
Brown-gray to brown clay, some si	— 1 +									
- trace sand & gravel, damp, hard					5					
	_				7	1	-			
	5	2	SS	18"	9	16	4.5+	15.5	117.3	7.
- Martinese									5	
<u>-</u> 1	_				6				1.1.2	
		3	SS	18"	12	21	4.5+	17.0	113.3	7.
<u> </u>	_				6				1.1.1	
624.5'		,		10	8	17		15 7	115 0	F
End of Boring	10	4	SS	18	9	17	4.5+	15.7	115.8	5.
	_									
	-									
								-		÷
	15									
_										
	_							8		
	·			6.5						
	<u></u>				, , , , , , , , , , , , , , , , , , ,					
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SOLE AND MATERIAL CONSOLIANTS, INC.	File N Client			ba Gi	COUD				OG_1	
						econs	tructio	n	Sheet 1	
	Projec	ct	US 4	l to	Green	n Bay	Road		Date 2/	
	Locat	ion <u>1</u>	High	land	Park	, IL		Drille	ed By	AC
and and a second s	Equip	men	it ⊠C	ME 4	5B 🗆 I	H.A. C	Other	Logge	ed By —	CS
Elev., ft. 636.0' Description Depth, ft.	0	S	Т	R	В	N	Pen.	W	Uw	Qu
35.4' Concrete - 7.0" 34.9' Brown sand & gravel,damp-6.0"					-	1	1.1			3
 Brown-gray to brown clay, some silt trace sand & gravel, damp, hard 	,	1	SS	12"	5 5 5	10	4.0	17.7	102.0	5.4
	_				<u></u>			<		
	_		-		5					
	5	2	SS	18"	7	17	4.5+	17.0	117.3	4.8
	_				10					
29.5'				1	7		+	1		
Gray clay, some silt, trace sand & gravel, damp, hard	_	3	SS	18"	7 8 10	18	3.5	14.3	121.1	4.6
Gray silt, some clay, trace sand & gravel, damp, medium dense					7					
26.0'	10	4	SS	18"	8	16		12.2		
- End of Boring								- 1 - 1		
	-								1 G B	
	_									
				-				. 1	1	
	-						-			
	15	_	_						911	
	-		24							
	_				-		· .			
	_				Υ	-				
	-				2					
							-			
	20							-		
ater Level — depth,ft. elev., ft. B - while drilling: dry _ N	- SPT, I	lard P blows	enetra /foot to	tion Tes drive 2	st(SPT),	blows/ 6 plit-spoc		with 140 lb.	R - recovery W - water co hammer fal veight of soi	ontent, % ling 30"

	Client			ba Gr					Sheet	_of _		
nments Station 146 + 30	Proied	ct (Clav	ey Ro	ad Re	econst	ructio	n	Date _2/	/18/2		
		US 41 to Green Bay Road AC Location Highland Park, IL Drilled By										
	Equip	men	nt⊠C	ME 4	5в 🗆	H.A. C	Other	Logge	ed By —	CS		
ev., ft. 643.5' Description Depth, f	t. 0	S	Т	R	В	N	Pen.	W	Uw	Qu		
2.9'Concrete - 7.0"	_	14		1.1.1		-						
¥ (a) see below				1	4				VINCE	Set.		
Brown-gray to brown clay, some sil	.t,		1		4					126		
trace sand & gravel,damp,hard		.1	SS	14"	4	8	4.5+	18.6	108.7	4.8		
	-			33			1 1		1.1	36		
				1.5	5		1.1.1			210		
	_	2	SS	18"	7	1 1 7		20 /	100 6	-		
	5	2	22	10	10	17	4.5+	20.4	109.6	5.2		
				1.18			3.13					
	-			1	5				- 1			
5.0'	-	3	SS	18"	6 10	16	4.0	16.8	114.4	4.3		
Gray clay, some silt, trace sand &	-				10	10		10.0	114.4	4.5		
gravel, damp, very stiff	_					1						
		4			6		2.5	19.5	108.6	3.1		
5.' (b) see below	10		SS	18"	7	13	2.5	8.2	420.4			
End of Boring	-			1.1								
-	-									1.1		
<pre>(a) Brown sand & gravel,damp-very _ damp=7.0"</pre>						150						
(b) Gray silt, some sand & clay,												
trace gravel,damp,medium dens	e —			100			1911 - 19		(† 13) 19	1.72		
	_			1.1		19			1.00	1		
	15						1.1					
	-15									1.2.1		
							1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -			N.F.		
	-			3			š.		1. 3%			
									- T			
	-				2		1 ×		1.2.4			
				-					1.1	1.		
	20											

SOIL AND MATERIAL CONSULTANTS, INC.	Client		Ciorl	ba Gr	oup			s	heet <u>1</u>	_of
omments Station 149 + 40	Proje	ct C	Clave	ey Ro	ad Re	const	ructio		Date _2/	
Sama and Sama and Sama and Sama		ι	JS 41 Highl	l to land	Greer Park,	n Bay IL	Road		ed By	
· · · · · · · · · · · · · · · · · · ·	Equip	men	t ⊡C	ME 4	5B 🗆 I	H.A. D	Other	Logge	ed By —	CS
Elev., ft. 648.0' Description Depth, ft.	0	S	Т	R	В	N	Pen.	W	Uw	Qu
F7.4'Concrete - 2.5" Brown sand & gravel,damp-very damp			-			-				
Brown-gray silt, some clay, trace sa		1	SS	18"	5 4 5	9		13.0		
- Brown-gray to brown clay & silt,	_									
<pre>- trace sand & gravel,damp,hard</pre>	_			1.011	4					
ter and the state of the state of the	5	2	SS	18"	9	15	3.75	17.9	117.2	4.4
- Brown-gray to brown clay & silt,					3					
40.5, trace sand & gravel, damp, very stif	f	3	SS	18"	5	9	2.25	18.9	111.0	3.1
Brown to gray fine sand & silt, saturated,loose	10	4	SS	12"	6 5 4	9		19.3		
- End of Boring	_		-							
	_									
	_							() () () ()		
	15									
슬 때 그는 말에 가지 않는 것	_						6 × 5	· · · ·		
	_						$\mathbb{P}(t^{2^m})$	· * .	-13	
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	_									
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	20	_	1			<u> </u>				

TI'S X SUIL AND MATERIAL CONSULIANTS, INC.	File N Client					10		NG L		
	Client					econst	ructio	n	heet 1	
	Proje	ct	JS 41	L to	Greer	n Bay	Road		Date <u>2/</u>	
	Locat		iigni		Park,	<u>, IL</u>			d By	
	Equip	men	t ⊠C	ME 4	5B 🗆 I	H.A. C	Other	Logge	d By —	CS
Elev., ft. 647.0' Description Depth, ft.	0	S	Т	R	В	N	Pen.	W	Uw	Qu
Brown sand & gravel,damp - 11.0"					6					
Brown-gray to brown clay, some silt trace sand & gravel, damp, very stif to hard		1	SS	14"	3	7	3.25	23.8	99.8	3.3
	_									-
	5	2	SS	18"	4 5 6	11	3.5	18.3	110.5	4.5
41.5' <u> </u>	ay									1 =
Brown fine sand, saturated, very	_	3		5	3 1 1	2		18.6 33.0		
- loose 		4			1	2		35.0	1. B.	
	_				1					
37.0'	_10	5	SS	12"	1	1		29.0		
End of Boring	_					7.			-13	
	_							22	1.45	
	15									
	-						2			
토 - 이미 및 여행성이 생							/			
	_		1							
	20					-				
ter Level — depth,ft. elev., ft. B - while drilling: <u>6.0</u> <u>641.0</u> ' N	- SPT,	dard P blows	enetra /foot to	tion Tes drive 2	st(SPT),	blows/ 6 plit-spoo		with 140 lb.	R - recovery N - water co hammer fall reight of soil	ontent, ling 30

Soil and material consultants, inc.	File N	lo	249	919	_	E	BORI	NG L	OG _1	13
	Client		Ciorl	ba Gi	coup			5	Sheet 1	_of <u>1</u>
omments <u>Station 155 + 40</u>	Proje	ct C	Clave	ey Ro	ad Re	econst	ructio	n	Date	/19/2
		U					Road			AC
	Equip	men	t ⊠C	ME 4	5B 🗆 I	H.A. D]Other	Logge	ed By —	CS
Elev., ft. 645.5' Description Depth, ft.	0	S	Т	R	в	N	Pen.	W	Uw	Qu
44.6' (a & b) see below	-		100	1.6						
Brown-gray silt, some clay, trace		1	÷ .		4		- ⁻	14.1		
Brown-gray clay, some silt, trace		2		12"	5		2.0		_	
- sand & gravel, damp, very stiff		2	55	12"	6	11	3.0	18.2		-
42.0'		ŝ.				1				
- Brown-gray silt, some clay, trace	-				5					
<pre>sand & gravel,damp,medium dense</pre>	5	3	\$S	18"	8	14		19.4		
40.0'				1						
Brown-gray to gray clay, some silt,	_				5					
trace sand & gravel,damp,hard (small saturated fine sand seam		4	55	18"	7	16	4.5+	19.6	112.0	4.9
- ⊻ between 7.5'-8.0')			00	10	9	10	4.57	19.0	112.0	4.5
37.0'										
Brown-gray to gray clay, some silt,	-				4				- 1	
	10	5	SS	18"	6	11	3.25	19.8	113.7	2.0
_ End of Boring	-								18 13	
(a) Concrete - 7.5"							2			
(b) Brown sand & gravel-2,5"										
	-									
	15									
	-							-		
								SANCEAN MARKANING A CANCER		
	-				_					
_	-									
	20									

SOIL AND MATERIAL CONSULTANTS, INC.	File N	lo	249	919		E	BORI	NG L	OG _1	.14
	Client		lior	ba Gi	coup			5	Sheet 1	_of _
omments Station 158 + 40	Draia	, C	lave	ey Ro	ad Re	econst	tructio		Date _2/	
	Projec	U					Road			AC
	Locat	ion <u>H</u>	lighl	and	Park,	, IL		Drille	ed By	AU
	Equip	men	t⊠C	ME 4	5B 🗆	H.A. C	Other	Logge	ed By —	CS
Elev., ft. 644.5' Description Depth, ft.	0	S	Т	R	В	N	Pen.	W	Uw	Qu
3.7' (a & b) see below	_									
Brown clay.some silt.trace sand &				14	2					
gravel, damp, very stiff		1			4		3.0	21.9	104.3	3.8
Brown-gray to gray-brown silt, some	-	2	SS	18"	5.	9	Section of	19.5		
clay, trace sand & gravel, damp, medium dense	-					1				
40.5'		3			5	1	11.0	15.1		
- Brown gray to brown clay, some silt	, _	4	SS	18"	7	16	4.5+	19.7	110.9	7.3
— trace sand & gravel, damp, hard	5	а —			9		4.51	17.1	110.9	1.5
		2				1				
-	_				5	-				
	-	5	SS	18"	<u>8</u> 12	20	4.5+	19.0	110.8	6.5
$\overline{\nabla}$	_									
- 7	_				9					
					9 11	•				
34.5'	10	6	SS	18"	12	23	4.5+	18.0	111.3	7.0
End of Boring										
(a) Concrete - 5.5"						-				
(a) concrete = 5.5 (b) Brown sand & gravel, very damp-		Ρ.				1				
saturated - 4.0"	-									
			1							
-	_	9								
-	-									
	15									
-	_									
	_									
	-									
-	20									
ater Level depth,ft. elev., ft. B - while drilling: 8.0 636.5' N - after drilling: dry Pen.	- samp - Stanc - SPT, - pocke	lard P blows et pen	enetra /foot to etrome	tion Te drive 2 ter rea	st(SPT),	blows/ 6 split-spoo is/sq. ft.	Uw	with 140 lb.	R - recovery W - water c hammer fal weight of soi	onten Iling 3

Comments Station 161 + 20	Client Proje	·		ey Ro	70	econs	tructio	n	Sheet <u>1</u> Date <u>2/</u>	
		U					Road			AC
	Equip	men	t 🖾 C	ME 4	5В 🗆	H.A. C	Other	Logge	ed By —	CS
Elev., ft. 646.5' Description Depth, ft	t. O	S	Т	R	В	N	Pen.	W	Uw	C
645.6' ^(a & b) see below							*			
Brown-gray to brown clay,some sil trace sand & gravel,damp,hard to very hard	t,	1	SS	12"	3 5 6	11	4.0	20.2	108.3	4
	-				7 10					
	5	2	SS	12"	14	24	4.5+	20.1	109.0	8
	-		4	-	5					
	_	3	SS	18"	12	21	4.5+	17.4	117.8	8
638.0' Brown-gray to brown clay,some sil 636.5' ^{trace} sand & gravel,damp,hard	t,10	4	SS	18"	7 9 12	21	4.5+	23.1	103.6	6
End of Boring (a) Concrete - 7.5" (b) Brown sand & gravel,damp - 3.5"						-			- 10	
								η.		
	 								4	
	_									

Comments Station 164 + 10	Client	-	lave	ey Ro	ad Re	const	tructio		Sheet $\frac{1}{2/2}$			
		US 41 to Green Bay Road AC										
	Locat	ion <u>H</u>	ligh.	and	Park,	IL		Drille	ed By	CS		
	Equip	ment	t⊠C	ME 4	5B 🗆 I	H.A. D	Other	Logge	ed By —			
Elev., ft. 663.5' Description Depth, ft.	0	S	Т	R	В	N	Pen.	W	Uw	Qu		
_ Concrete - 8.5"				-	-							
62.8' Brown sand & gravel, damp -7.5"					7				1.1			
Brown silt, some clay, trace sand &		1		15"	5	11		1/ 0				
_ gravel,damp,medium dense			55	13	6	11		14.8				
50.0'												
Brown-gray clay & silt,trace sand					4	÷.,			1.1.1			
& gravel,damp,hard	5	2	SS	18"	8	14	4.5+	16.7	116.8	5.3		
57.5'						1						
					4			÷				
 Brown-gray clay & silt,trace sand & gravel,damp,very stiff to hard 					7							
		3	SS	18"	9	16	3.25	16.7	112.6	3.7		
		8-11					·					
그는 영상에서 가지 않는 것이 없다.				103	6				2			
53.5'	10	4	SS	18"	8 10	18	3.75	16.8	116.0	4.5		
_ End of Boring	_				0			and the second second second				
<u>-</u>												
<u> </u>					100							
-												
	-	•	1					<u> </u>				
-	15				-							
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-	-						-					
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<u> </u>				×			2					
_	20			1	_							
	20					8X						

Qu - unconfined compressive strength, tons/sq. ft.

F-111b-1

hrs. after drilling:

	Clien	τ			oup		ruction		Sheet	
Comments Station 167 + 00	Proje	ct	S 41	Date						
	Locat	tion <u>H</u>	igh1	and	Park,	IL	Road	Drille	ed By	A C
	Equip	omen	t 🖬 C	ME 4	5B 🗆	H.A. [Other	Logge	ed By —	0
Elev., ft. 683.0' Description Depth, f	t. O	S	T.	R	В	N	Pen.	W	Uw	I
Concrete - 8.0"										10
Brown sand,gravel & crushed limestone			ę s		- 7	-	S			
680.5'		1	SS	18"	7	16		8.7		
Brown-gray to brown clay & silt,										
trace sand & gravel,damp,hard			11		5			100		
	5	2	SS	18"	7	13	4.25	15.4	120.1	
en la segura de la calendaria de la composición de la compo	_				7					
	_	3	SS	18"	10	18	3.75	15.1	121.0	
675.0' \	_		-							100
Gray clay, some silt, trace sand & gravel, damp, stiff					3			11		19.00
673.0'	10	4	SS	18"	6	10	1.5	15.7	122.0	
End of Boring						1		1		
-	_			÷.,	<u> </u>	1				
						 				_
	_									
	-									
	15						-			-
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	-									
_		-100-007								-
	_					1			1.1-3	
	20					1				

	Client								Sheet 1	_of _
omments <u>Station 170 + 00</u>	Projec	ct _C	lave	ey Ro	ad Re	econst	ructio	n	Date 2/	/19/2
		U	IS 41	. to	Green	n Bay , IL	Road		ed By	
	Equip	men	t 🖬 C	ME 4	5B 🗆	H.A. C	Other	Logge	ed By —	OS
Elev., ft. 685.5' Description Depth, ft.	0	S	Т	R	В	N	Pen.	W	Uw	Qu
34.8'(a & b) see below	_	100	1	1					1.1.1.1	18 1.
34.4'Brown sand & gravel,damp - 4.0"				1	3				Nilla S	
- Brown-gray silt,some clay,trace	-				6					3.09
sand & gravel, damp, medium dense	1	1	SS	15"	8	14		14.4		
		1.1	-	1						
51.5'	-			2	6	1			2 N	in the second
	-				9				1.1	
Brown-gray to brown clay & silt,	5	2	SS	18"	11	20	4.0	15.1	124.2	6.6
trace sand & gravel,damp,hard	_						1.1		1.0	1
		1			6					
					10	1	S			
	-	3	SS	18"	13	23	4.5+	16.0	119.2	6.7
7.5'					-			S. 1. 1.	-	
 Gray clay, some silt, trace sand & gravel, damp, very stiff 		13		1	5		ia - 3			1
	-				6					
5.5'	10	4	SS	18"	7	13	2.0	15.4	120.8	2.9
End of Boring	-	-			2.3	0	6.5.1		2.1	120
(a) Bituminous concrete - 3.0"	_			1.00						
(b) Concrete - 6.0"	-	-		1	1	2 C				
	-	-				-				
				12		1.5	1.1		1114	
		1	2.7		2					10
	15	1				1.1			1.	
_	15			-						
<u></u>										<u></u>
	-				- 20	1.1	1. I		1.1.1	
		1		-		1.0	21		1.24	
		(Carlotter) and			12					
이 가지 않는 것이 가지 않는 것이 않는	-				- 4					
동네는 것이 아이지 않는 것이 많이							- <			13
	20									
S	- samp	ie T	- type	: J(Jar)	, SS(spl	it-spoon)	, ST(shelby	(tube)	R - recovery	y length



General Notes

SAMPLE CLASSIFICATION

Soil sample classification is based on the Unified Soil Classification System, the Standard Practice for Description and Identification of Soils (Visual-Manual Procedure), ASTM D-2488, the Standard Test Method for Classification of Soils for Engineering Purposes, ASTM D-2487(when applicable), and the modifiers noted below.

CONSISTENC	Y OF COHESIVE	SOILS	RELATIVE DENSITY OF GRANULAR SOILS					
Term	Qu -tons/sq. ft.	N (unreliable)	Term	N - blows/foot				
Very Soft	0.00 - 0.25	0 - 2	Very Loose	0-4				
Soft	0.26 - 0.49	3 - 4	Loose	5-9				
Medium Stiff	0.50 - 0.99	5 - 8	Medium Dense	10 - 29				
Stiff	1.00 - 1.99	9 - 15	Dense	30 - 49				
Very Stiff	2.00 - 3.99	16 - 30	Very Dense	50 +				
Hard	4.00 - 7.99	30 +	,					
Very Hard	8.00 +							
IDENTIFICATIO	ON AND TERMINO	DLOGY	DRILLING, SAMPL	ING & SOIL PROPERTY SYMBOLS				
Term	Siz	e Range	CF - Continuous F	Flight Auger				
			HS - Hollow Stem	Auger				
Boulder	01	ver 8 in.	HA - Hand Auger					
Cobble	3 in.	to 8 in.	RD - Rotary Drillin					
Gravel -coars		to 3 in.	AX - Rock Core, 1					
-medi		to 1 in.	BX - Rock Core, 1					
-fine		to 3/8 in.	NX - Rock Core, 2					
Sand -coars		to #4 sieve	S - Sample Num					
-medi		to #10 sieve	T - Type of Sam	ple .				
-fine		to #40 sieve	J - Jar					
Silt		to #200 sieve	AS - Auger Sampl					
Clay	smaller that	an 0.002 mm		2 in. O.D. with 1-3/8 in. I.D.)				
				(2 in. O.D. with 1-7/8 in. I.D.)				
Modifying Term	Percent	by Weight	-R - Recovery Ler					
				nterval, Standard Penetration Test (SPT)				
Trace		- 10		drive 2 in. O.D. split-spoon sampler				
Little		- 20		nammer falling 30 in., (STP)				
Some		- 35		rometer reading, tons/ sq. ft.				
And	36	- 50	W - Water Conter					
				ght of soil, lbs./ cu. ft.				
MO	bisture Condition		Str - % Strain at Q	compressive Strength, tons/ sq. ft.				
	Det		WL - Water Level	u.				
	Dry		WD - While Drilling					
	Damp.		-					
	Very Damp		AD - After Drilling DCI - Dry Cave-in					
	Saturated		WCI - Wet Cave-in					
				4				
			LL - Liquid Limit, 9 PL - Plastic limit, 9					
			PL - Plasticity Inde					
			LI - Liquidity Index					
· ·			Liquidity Inde					

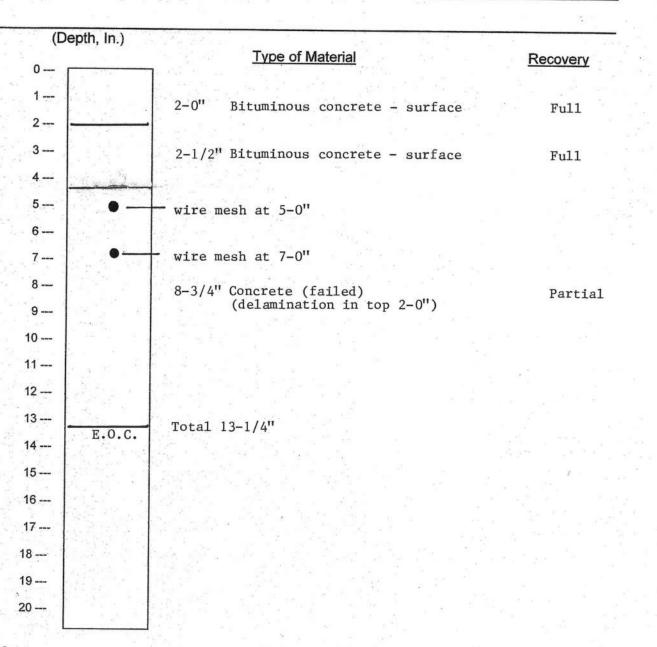


Date:	2/19/20	
File No.:	24919	
		-

8 W. COLLEGE DR. • SUITE C • ARLINGTON HEIGHTS, IL 60004

an an a			CORE LOG		
Client:	Ciorba Group	x	Reference	Clavey Road Reconstruction US 41 to Green Bay Road	
Core No	201	Work Done By:_	AC & CS	Highland Park, IL	
Location	of Core:	Green Bay Roa	d Station	204 + 10, 7' left of CL	

Comments:



G-333



SOIL AND MATERIAL CONSULTANTS, INC.

File No. 24919

8 WEST COLLEGE DRIVE OFFICE: (847) 870-0544 ARLINGTON HEIGHTS, IL 60004 FAX: (847) 870-0661

SOIL TEST DATA

CLIENT: Ciorba Group Inc.

PROJECT: Clavey Road Reconstruction, US 41 to Green Bay Road, Highland Park, Illinois

BORING NO.			B-101	B-105	B-106
SAMPLE NO.			S-2	S-2	S-4
DEPTH			3.5' – 5.0'	2.0' – 2.5'	6.0' – 7.5'
ELEVATION			633.5' –	628.0' –	627.5' –
ELEVATION			632.0'	626.5'	626.0'
USDA SOIL C	LASSIFICATION		Clay	Silty Clay Loam	Clay Loam
AASHTO CLA	SSIFICATION		A-4(13)	A-4(5)	A-6(8)
GRADATION-	PASSING 1" SIEVE	%	100	100	100
"	3/4" "	%	100	100	100
"	1/2" "	%	100	1000	100
"	3/8" "	%	100	100	100
"	No. 4 "	%	100	99	100
"	No. 10 "	%	98	97	99
"	No. 40 "	%	96	94	97
"	No. 100"	%	91	87	82
"	No. 200"	%	89	82	65
GRAVEL		%	0	1	0
SAND		%	10	17	35
SILT		%	50	54	42
CLAY		%	40	28	23
LIQUID LIMIT		%	34	26	34
PLASTICITY I	NDEX	%	15	8	15

REMARKS:

SOIL AND MATERIAL CONSULTANTS, INC.

File No. 24919

8 WEST COLLEGE DRIVE OFFICE: (847) 870-0544 ARLINGTON HEIGHTS, IL 60004 FAX: (847) 870-0661

SOIL TEST DATA

CLIENT: Ciorba Group Inc.

PROJECT: Clavey Road Reconstruction, US 41 to Green Bay Road, Highland Park, Illinois

BORING NO.			B-108	B-112	B-113
SAMPLE NO.			S-1	S-3	S-3
DEPTH			1.0' – 2.5'	6.0' – 6.5'	3.5' – 5.0'
ELEVATION			633.5' –	641.0' –	642.0' –
ELEVATION			632.0'	640.5'	640.5'
USDA SOIL C	LASSIFICATION		Silty Clay Loam	Clay Loam	Silty Clay Loam
AASHTO CLA	SSIFICATION		A-4(5)	A-4(3)	A-4(3)
GRADATION-I	PASSING 1" SIEVE	%	100	100	100
"	3/4" "	%	100	100	100
"	1/2" "	%	100	1000	100
"	3/8" "	%	100	100	100
"	No. 4 "	%	100	100	100
"	No. 10 "	%	99	99	100
"	No. 40 "	%	98	98	100
"	No. 100"	%	89	73	100
"	No. 200"	%	79	67	95
GRAVEL		%	0	0	0
SAND		%	21	34	5
SILT		%	51	44	69
CLAY		%	28	22	26
LIQUID LIMIT		%	24	23	21
PLASTICITY II	NDEX	%	9	8	6

REMARKS:

Ciorba Group	March 20, 2020
Re: Clavey Road Reconstruction US 41 to Green Bay Rd.,	File No. 24919
Highland Park, Illinois	

ORGANIC CONTENT

BORING NO.	SAMPLE NO.	<u>DEPTH, FT</u> .	% ORGANIC CONTENT
102	4	5.5' to 6.0'	13.1
103	4	4.5' to 5.0'	41.3
104	2	3.5' to 5.0'	29.8
105	3	4.0' to 5.0'	29.6
106	3	3.5' to 5.0'	66.4
107	3	3.5' to 5.0'	27.3

Illinois Department of Transportation

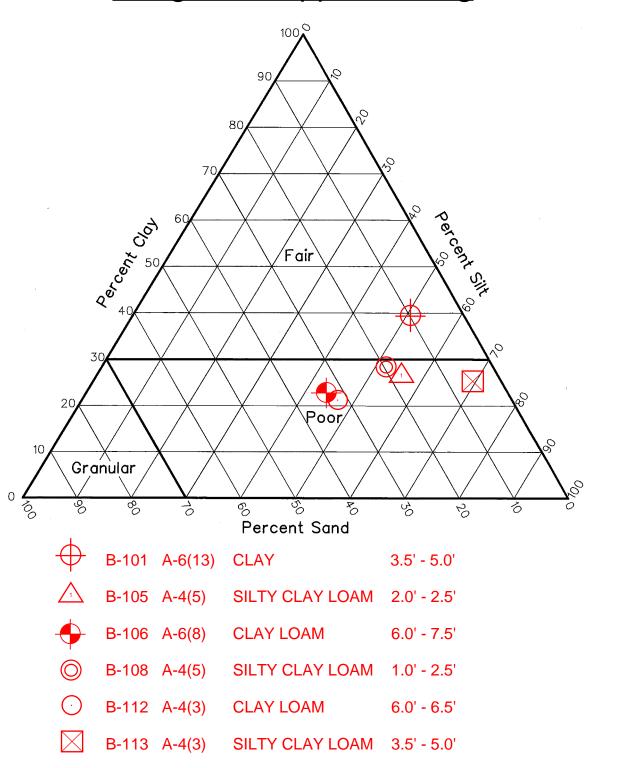
Summary Report on Pavement, Base and Subbase Design

State Job Number:	C-91-117-17 Project	ct: 025R(982)	Route: FAU	1265
Section: <u>15-00125-0</u>	00-PV City c	or County: City of Highla	and Park Date:	03/19/2020
ADT: <u>11,000</u> Ye	ear: <u>2040</u> Design Pe	eriod: 20	Class Highway:	Major Collector
Passenger Cars Per	Day: <u>10,670</u> Truck	s S.U. Per Day: <u>165</u>	Trucks M.U. P	Per Day: <u>165</u>
Pavement Structure:	HMA			
Type Surface Courses	HMA SURFACE COU	RSE, MIX "D", N70	Thickness:	2"
Type Base Course:	HMA BINDER COURSE	:	Thickness:	6"
Type Subbase Materi	al: Subgrade Aggrega	te Improvement	Thickness:	12"
Sta. to Sta.	112+50 to 115+60	124+90 to 127+20	138+50 to 141+50	153+90 to 156+90
*Sta. of Test	114+00	126+30	140+00	155+40
*Drainage Class	Fair	Poor	Poor	Poor
*Ave. Frost Penetration	42"	42"	42"	42"
Illinois Textural Classification	Clay	Silty Clay Loam	Silty Clay Loam	Silty Clay Loam
Classification and Group Index (AASHTO M 145)	A-4(13)	A-4(5)	A-4(5)	A-4(3)
*Percent Silt (AASHTO T 88)	50%	54%	51%	69%
*Illinois Bearing Ratio (%)	3.0			
Std. Dry Density (IL Mod. AASHTO T 99)	118.7			
Optimum Moisture (IL Mod AASHTO T 99)	13.1%			

* Indicates worst condition within the above station limits.

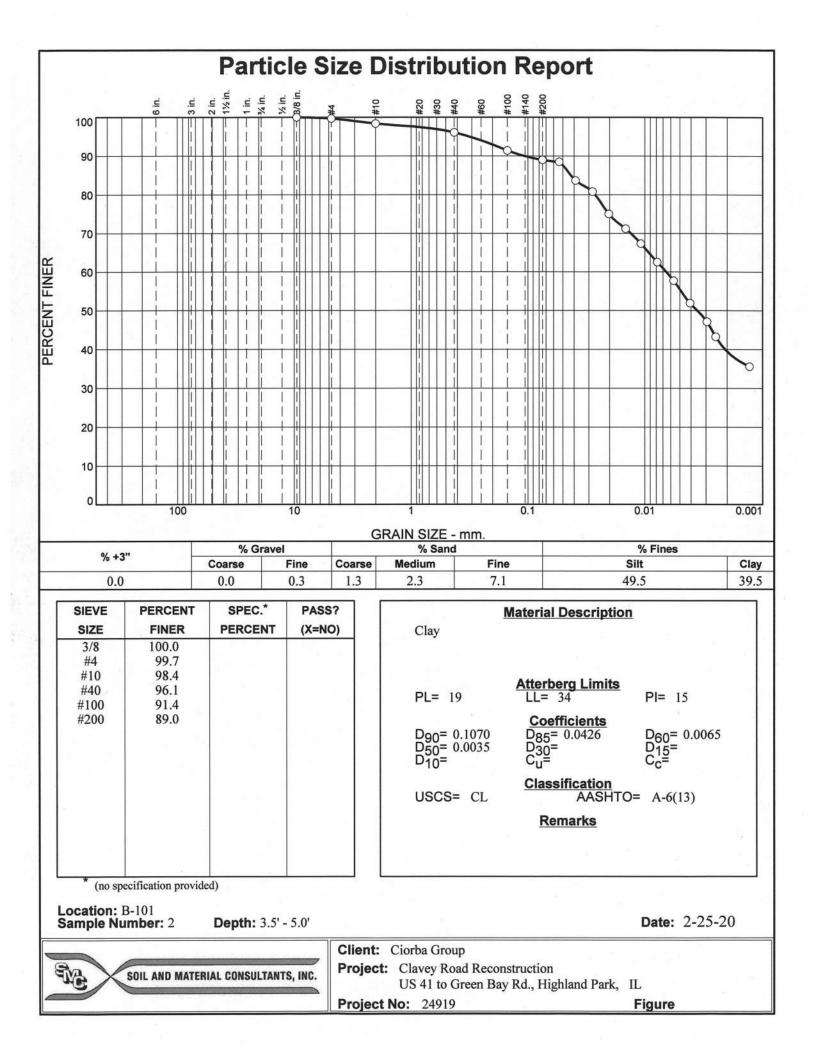
Remarks:

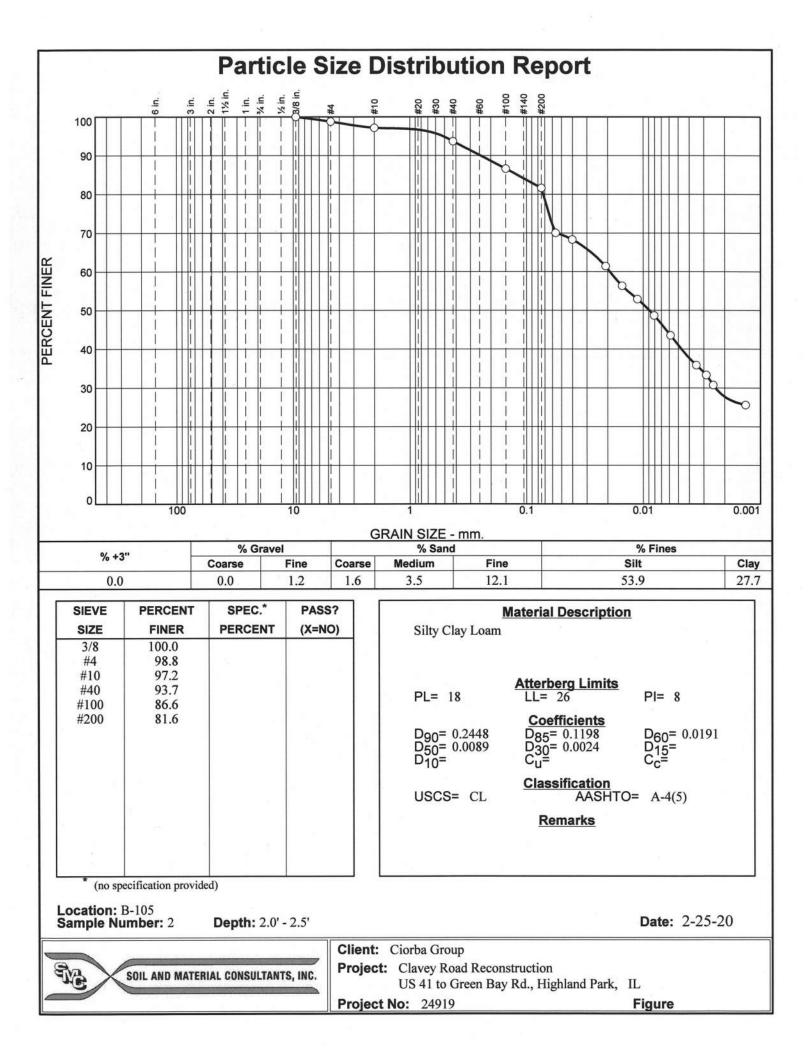
Subgrade Support Rating

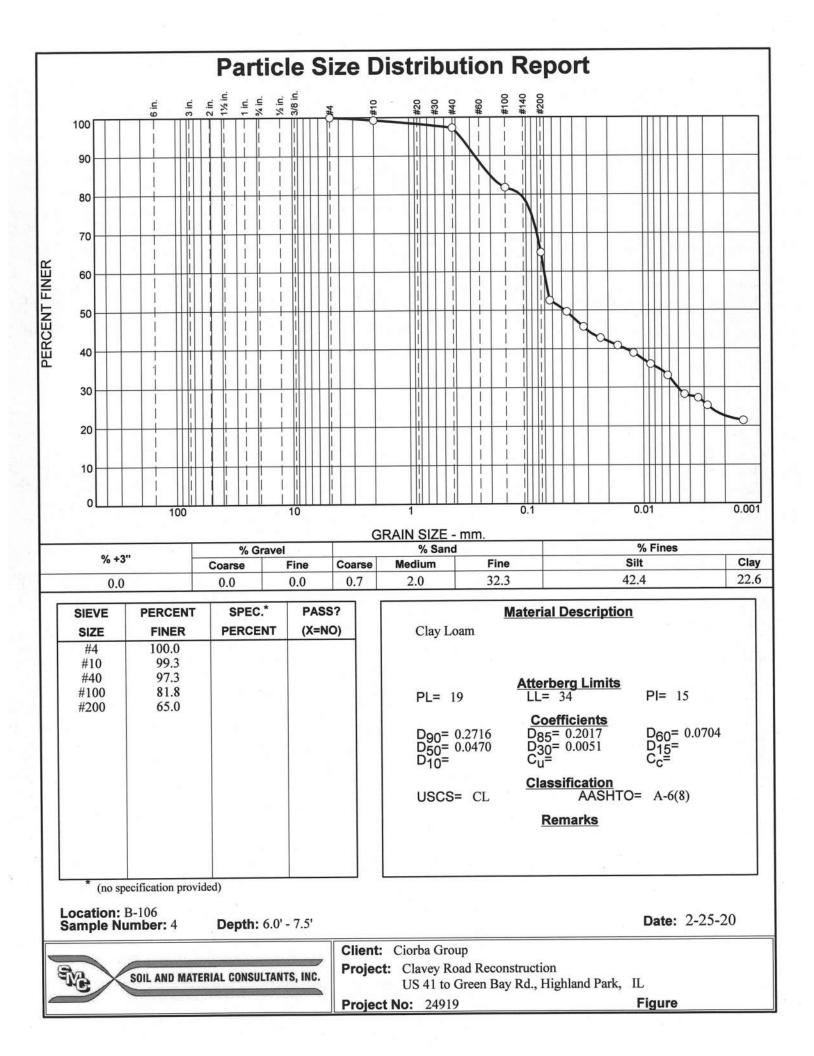


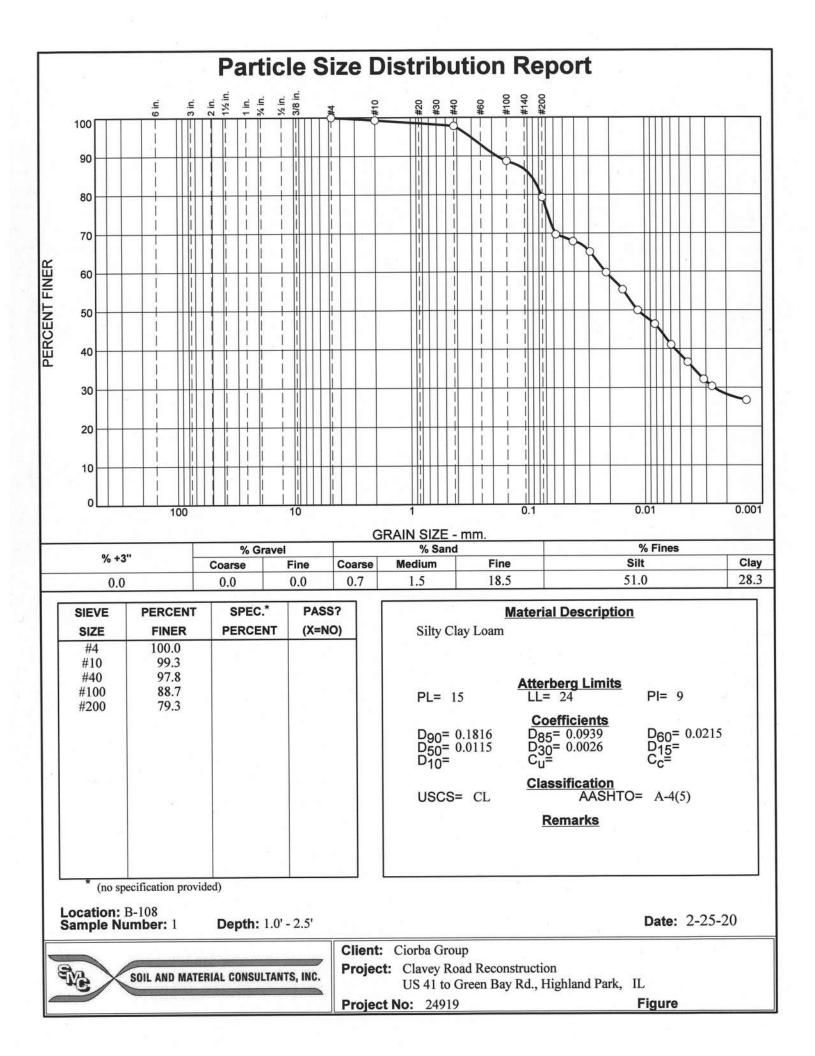
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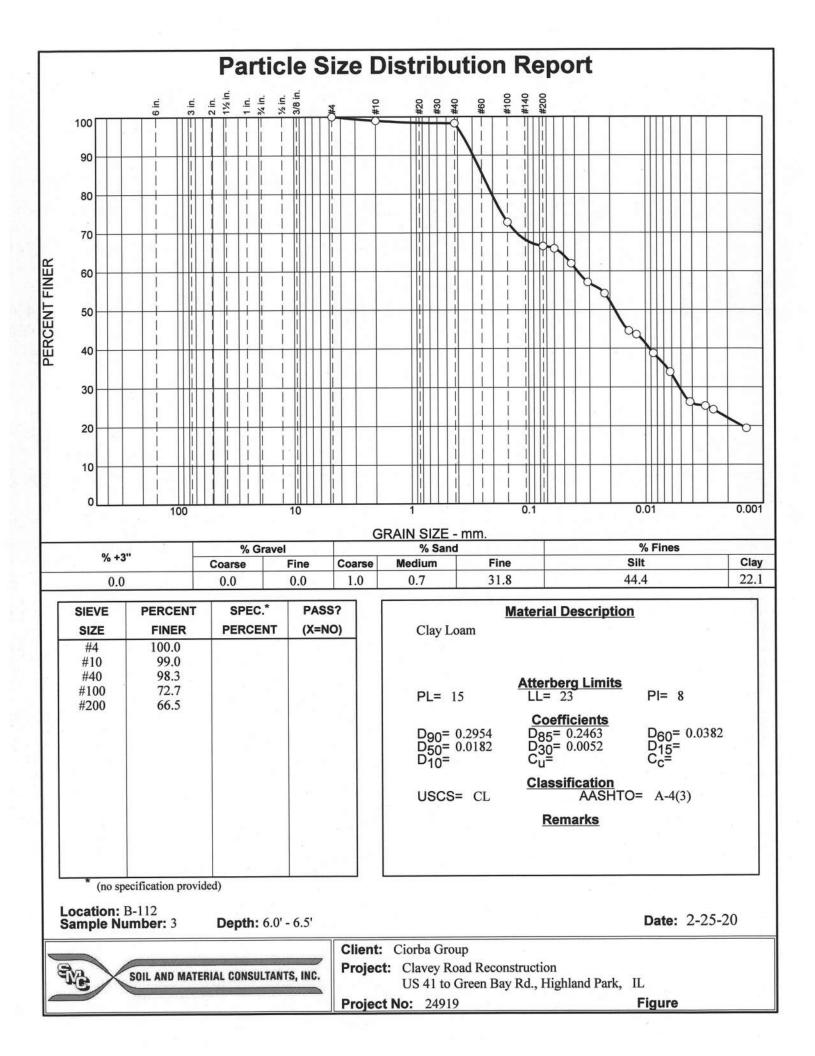
SMC		AND MATERIAL SULTANTS, INC.	LOCATION SKETCH
Client:		CIORBA GRO	JP
Project:	CLAVE	(ROAD RECON	STRUCTION
,	US 4	1 TO GREEN BA	AY ROAD
Location:	HIG	HLAND PARK, I	LLINOIS
File No.	24919	Date: 3-20-20	Scale: NONE

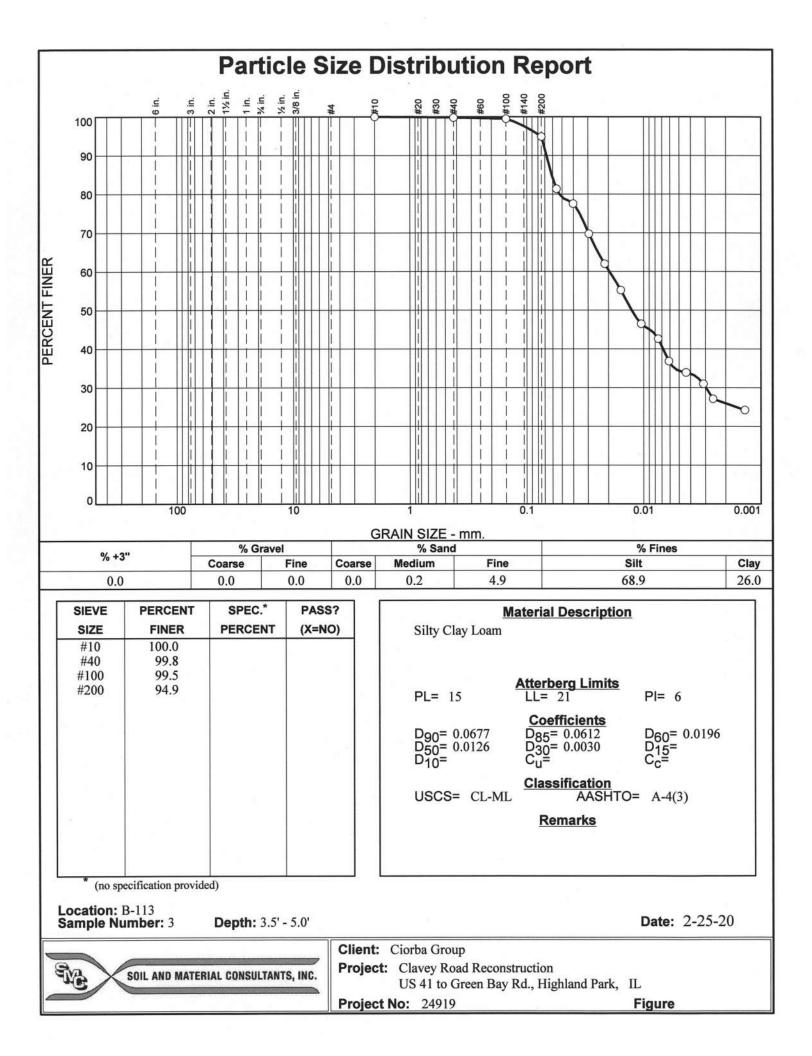


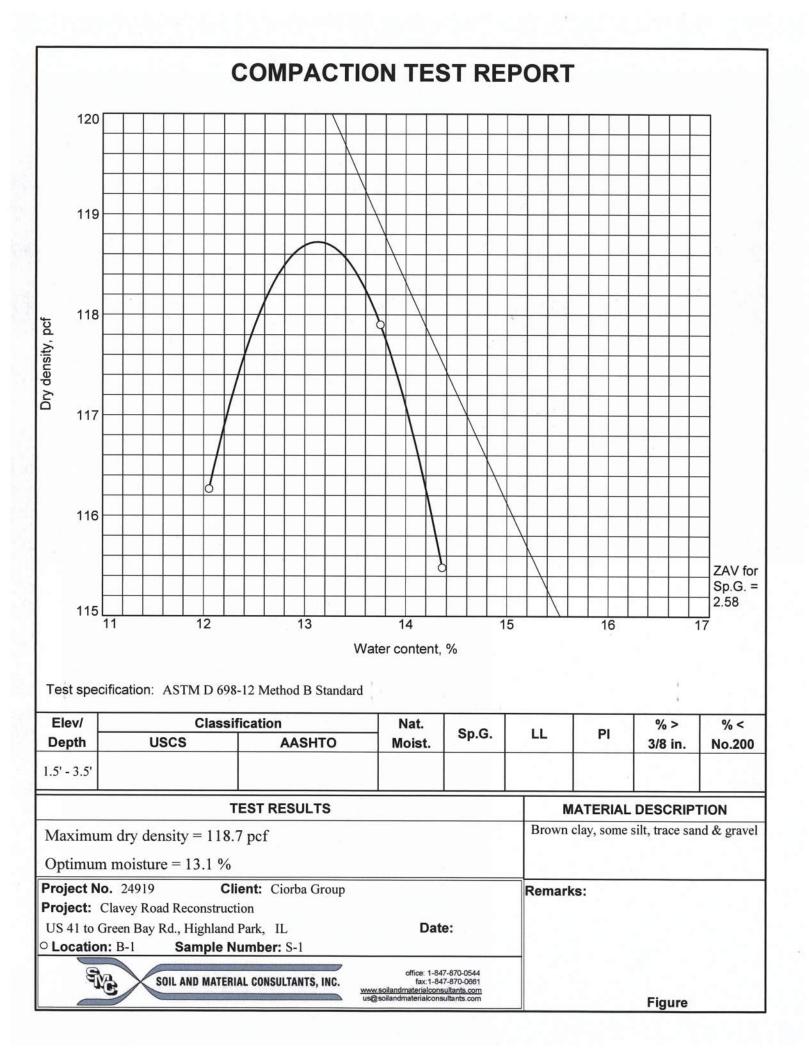


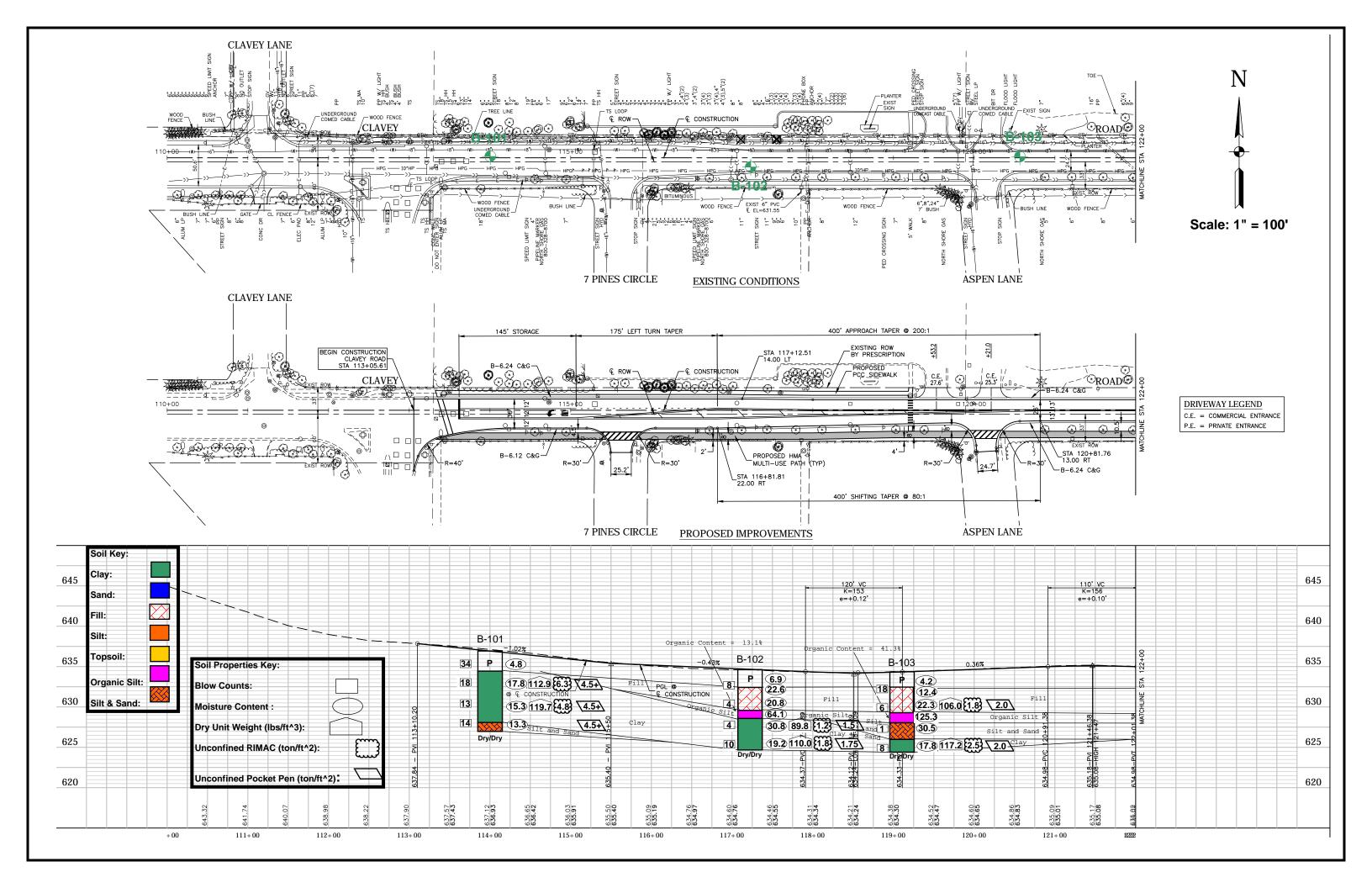


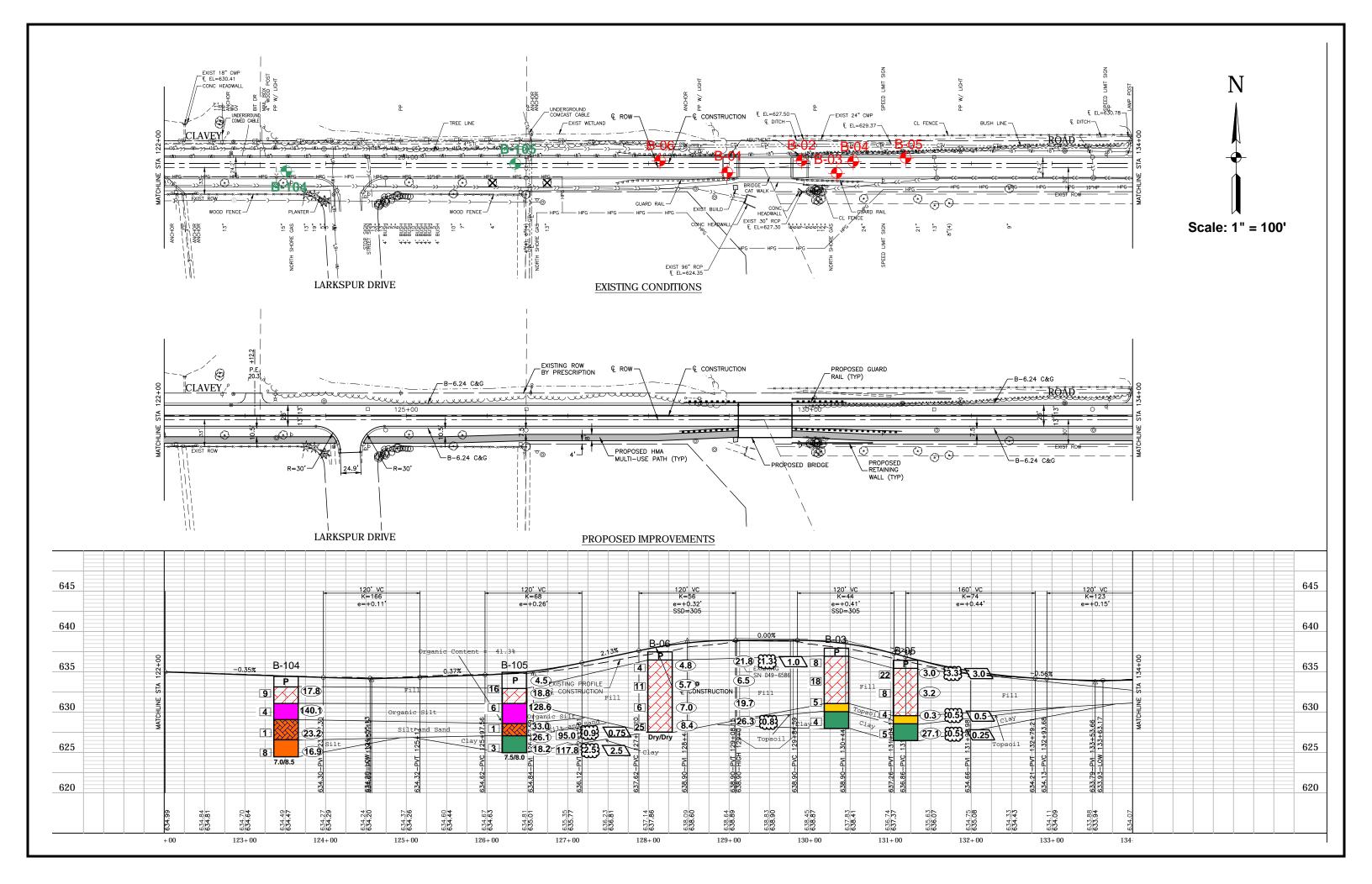


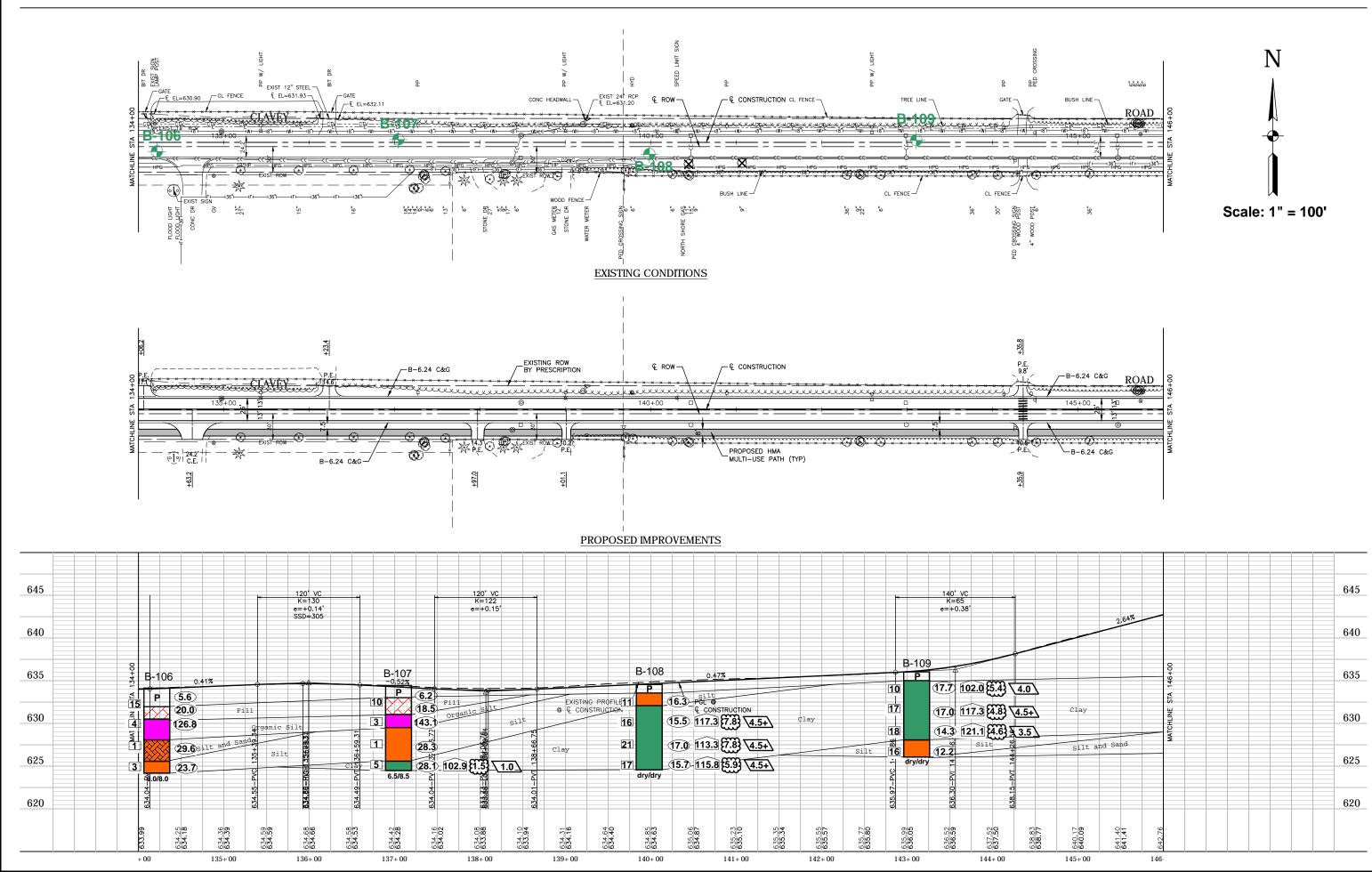


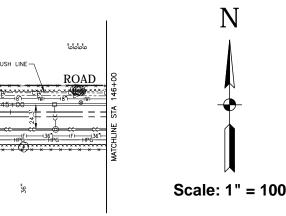


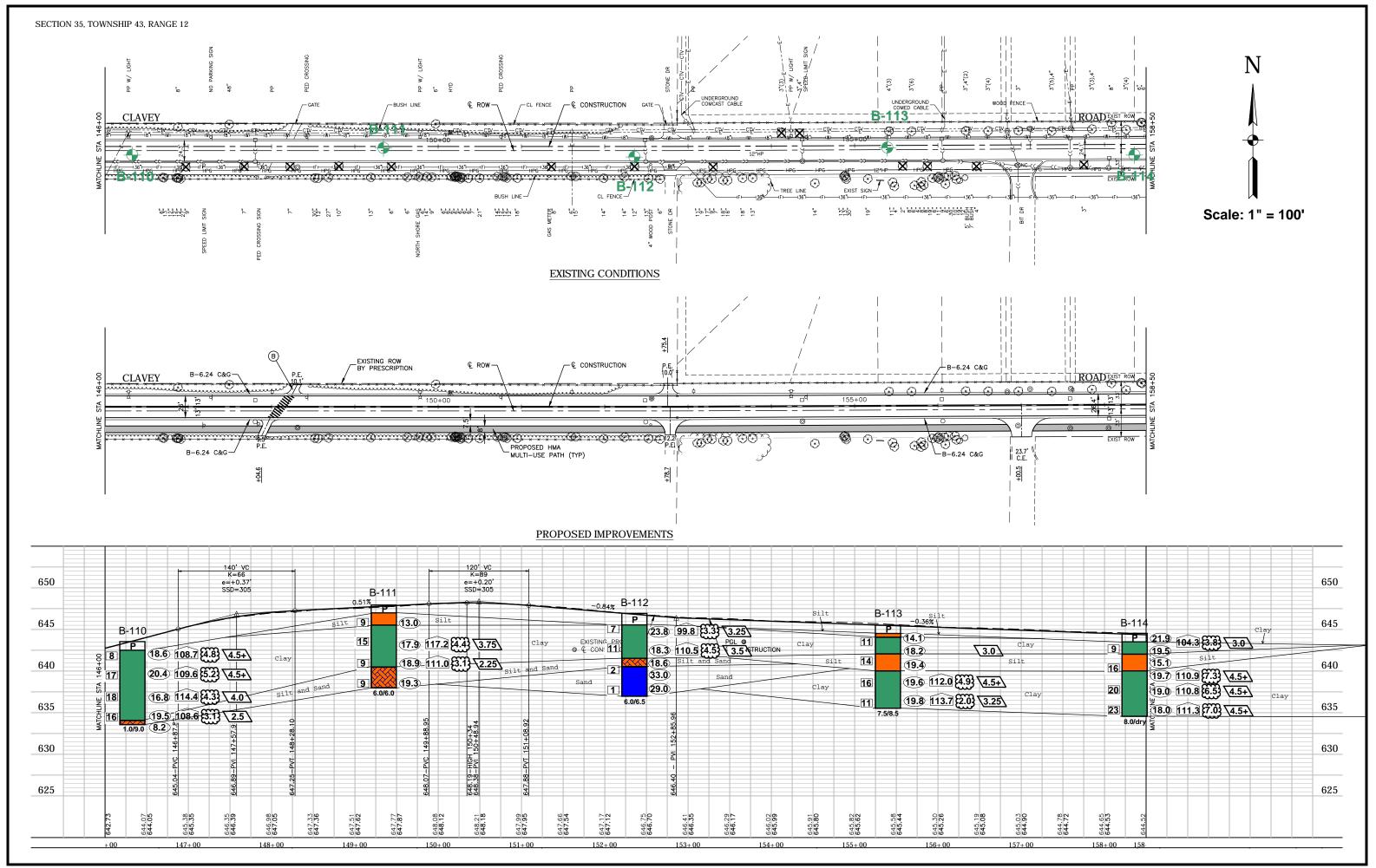


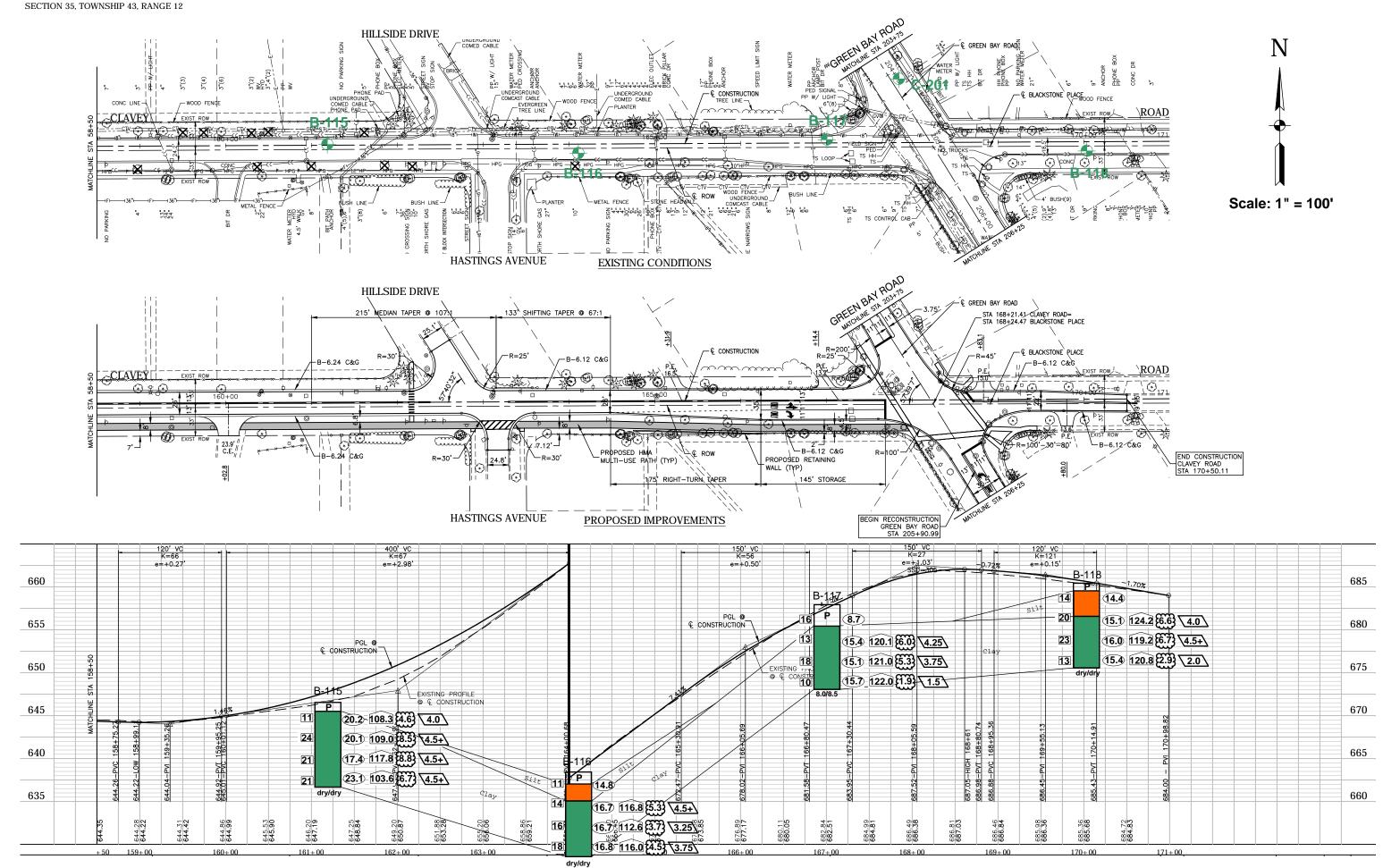




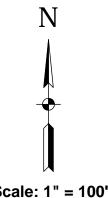












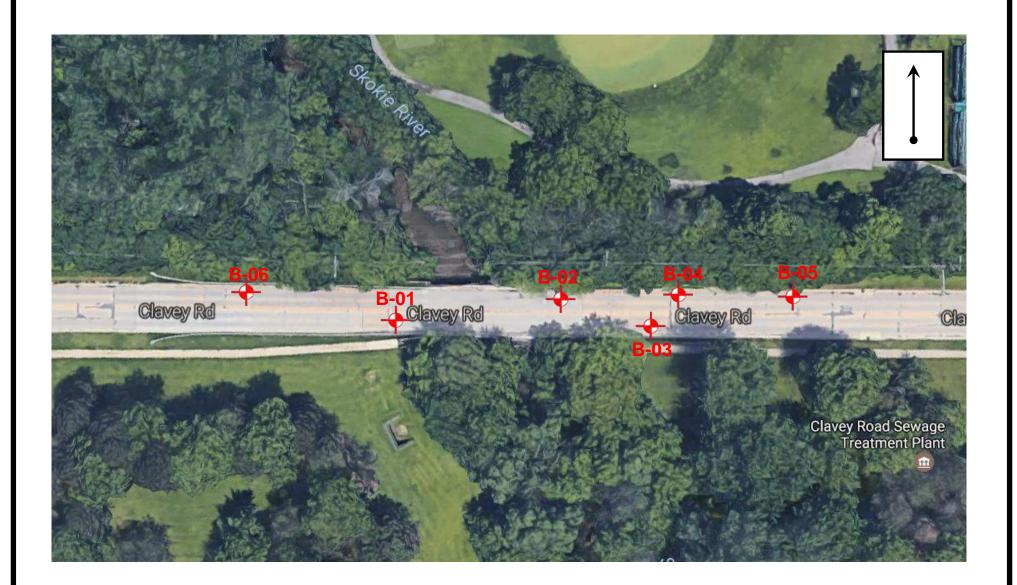
APPENDIX





9370 Laraway Road, Suite D Frankfort, IL 60423 P.815.806.9986 F. 815.464.8691 FIGURE 1 SITE VICINITY MAP Clavey Road Bridge over Skokie River Highland Park, Illinois PROJECT NUMBER: 17-G0411

DATE: June 2017





9370 Laraway Road, Suite D Frankfort, IL 60423 P.815.806.9986 F. 815.464.8691

FIGURE 2

BORING LOCATION DIAGRAM Clavey Road Bridge over Skokie River Highland Park, Illinois PROJECT NUMBER: 17-G0411

DATE: April 2017



			Engineering, Ltd. _17-G0411			ME <u>Clave</u>					r			
DATE		ETED	4/17/17 LOGGED BY NJ/GL	DRILLI	NG ME	THOD _3.2	25 in. I	.D. HS	SA					
							др)	(Qu)					LIMITS	
C DEPTH O DEPTH (ft)	ELEVATION (ft.)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT. (pcf)	ORGANIC CONTENT (%)	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX
I KIVI	636.9 636.4		0-5" CONCRETE PAVEMENT 5-11" AGGREGATE BASE	-										
			mottled blue and gray CLAY FILL with gravel very stiff, moist	ss 1	56	5-3-7 (10)	2.0	-	17.3					
	-			ss 2	44	9-5-6 (11)	3.5	3.6	14.7					
=CIS/1/-G0411 CL	629.4			SS 3	56	6-4-5 (9)	2.5	2.6	19.2					
	627.4		black BURIED TOPSOIL (A-8) medium stiff, moist	SS 4	44	1-2-4 (6)			56.3		7.4	-		
	-		mottled brown and gray CLAY (A-6) soft, moist	ST 5	25		0.5	0.43	26.8	102.0				
======================================	622.4			SS 6	56	2-1-2 (3)	0.5	-	28.1			28	14	14
	-		gray SILTY LOAM (A-4) stiff, moist	ss 7	67	6-7-6 (13)	2.0	2.0	16.2					
	e depth Jnd Wat At time	ft Fer Le Of Di Of Dr	RILLING None RILLING Dry upon completion	N(DTES									
			ation represent an approximate boundary between s and the transition may be gradual. Dashed lines are in 9370 W. Laraway Road, Suite D Frankfort, IL	dicative of	potent	ially erratic o	or unkn	iown cł	nanges			and b	etween	



BORING NO. B-01 PAGE 2 OF 5

PROJ		MBER	ngineering, Ltd. 17-G0411 4/17/17 LOGGED BY NJ/GL		CT LO	ME <u>Clave</u> CATION <u>H</u> THOD <u>3.2</u>	lighla	nd Par	k, Illin					
							2	(n						
DEPTH (ft)	ELEVATION (ft.)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT. (pcf)	ORGANIC CONTENT (%)	LIQUID	PLASTIC LIMIT	
			gray CLAY (A-6) very stiff, moist	SS 8	78	4-8-12 (20)	3.5	3.2	13.2	-				
				ss 9	78	5-10-16 (26)	2.5	2.4	17.6	-				
				ST 10	44		2.0	0.33	18.4	118.4				
25	<u>612.4</u> 611.4		gray SILTY LOAM (A-4) with gravel ── dense, moist	- SS 11	44	9-10-8 (18)			13.9					
· -			brown CLAY (A-6) stiff, moist	SS 12	67	5-6-6 (12)	1.5	2.0	18.1	-				
30				SS 13	89	6-6-7 (13)	1.5	1.7	16.7	-				
				ST 14	92		2.0	-	15.4	-				
35				SS 15	78	6-6-8 (14)	2.0	1.8	19.0	-				
 				√ ss	78	6-7-7	1.75	1.7	21.4	-				
			tion represent an approximate boundary between and the transition may be gradual. Dashed lines are in		Variati		cur be	etween	sampl		ervals	and b	etween	
	0	, -	9370 W. Laraway Road, Suite D Frankfort, IL		•				•		1			



BORING NO. B-01 PAGE 3 OF 5

TE COMI (ft) (ft) (ft) (ft)		4/17/17 LOGGED BY NJ/GL					_PROJECT LOCATION Highland Park, Illinois _ DRILLING METHOD _3.25 in. I.D. HSA											
(ff) (ft) ELEVATION (ft.)	읃										ATT	ERBE	R					
	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT. (pcf)	ORGANIC CONTENT (%)	LIQUID	PLASTIC LIMIT	PI ASTICITY					
-		brown CLAY (A-6) stiff, moist <i>(continued)</i>																
<u>593</u> - 4 <u>5</u> -	.9	brown CLAY (A-6) very stiff, moist	SS 17	78	6-8-9 (17)	2.5	2.0	19.9										
- - 50			SS 18	89	5-10-14 (24)	3.0	3.3	19.8										
			SS 19	78	6-10-15 (25)	3.0	3.1	21.4										
- - - <u>578</u> -	.9	gray CLAY (A-6) very stiff, moist	SS 20	89	4-5-5 (10)	1.5	1.6	24.7										
_	f Democra	tion represent an approximate boundary betwe		Variati			twoor		ing int	envelo	and h							



PAGE 4 OF 5

			17-G0411 4/17/17 LOGGED BY NJ/GL		CT LO	ME <u>Clave</u> CATION <u></u>	lighlar	nd Par		ois				
						<u>. 1600 _3.2</u>	5 m. i					AT	ERBE	ERC
DEPTH (ft)	ELEVATION (ft.)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT. (pcf)	ORGANIC CONTENT (%)			
- - 65 -			gray CLAY (A-6) very stiff, moist <i>(continued)</i>	SS 21	89	3-6-6 (12)	1.5	1.2	13.2					
- - 70 -	567.4		gray CLAY (A-6) very stiff to hard	SS 22	78	4-5-6 (11)	1.5	1.7	19.7					
75					100	9-50/2"	2.0		14.2					
- - 80 -				SS 24	56	10-14-16 (30)	2.5		14.0					
- - 85				SS 25	67	16-25-19 (44)	4.5	4.5	13.9					



PAGE 5 OF 5

PROJI		BER	ngineering, l 17-G0411			PROJE		ME <u>Clave</u> CATION <u></u>	Highla	nd Par	k, Illin		er			
DATE	COMPLI		4/17/17	LOGGED BY NJ/GL		DRILLI	IG ME	THOD <u>3.2</u>	25 in. I	.D. HS	SA	1				
						111	,		Qp)	(Qu)					FERBE	
(ff) 82	ELEVATION (ft.)	GRAPHIC LOG		IATERIAL DESCRIPTION	J	SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT. (pcf)	ORGANIC CONTENT (%)	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY
			gray CL/ very stiff	AY (A-6) to hard <i>(continued)</i>												
-																
90						SS 26	67	14-19-17 (36)	4.5	4.0	11.7					
-						√ ss	56	15-19-31	4.5	4.5	13.2	_				
95						27	50	(50)	4.5	4.5	13.2	_				
							67	17-25-38 (63)	4.5	-	12.7	_				
100	537.4		Во	ottom of borehole at 100.0	feet.	/ \										
L	ines of D oring loca	emarca	tion represer	nt an approximate boundary	y between so d lines are ind	il types.	Variati	ons may or ally erratic of	ccur be	etween nown ch	samp	ling int	ervals	and b	etweer	1
b	oring loca	ations, a	and the transit	ion may be gradual. Dashed araway Road, Suite D Fra	d lines are ind	icative of	potenti	ally erratic o	or unkr	nown ch	nanges	3.				



CLI	ENT Robi		Ingineering, Ltd.	PROJE	CT NA	ME Clave	ey Road	d over	Skoki	e Rive	r			
PRC	DJECT NU	MBER	17-G0411	PROJE	CT LO		Highlar	nd Par	k, Illin	ois				
DAT	E COMPL	ETED	4/18/17 LOGGED BY NJ/GL	DRILLI	NG ME	THOD <u>3.2</u>	25 in. I	.D. HS	SA					
				ц	%		(Qp)	H (Qu)	()	<u>г</u> .	()	AT1		ERG
DEPTH DEPTH (#)	ELEVATION (ft.)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	RECOVERY (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT. (pcf)	ORGANIC CONTENT (%)	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX
	638.1 637.7	P 4 4												
H H	- 037.7		5-10" AGGREGATE BASE				-			-				
JE OVER SKC	635.6		with gravel stiff, moist	SS 1	44	4-5-6 (11)	-		72.0	-				
	_		brown GRAVEL FILL dense, moist	ss 2	56	9-19-13 (32)			14.7	-				
11 CLAVEY F	632.6					(32)	-			-				
CIS/1/-G04	-		brown CLAY FILL stiff, moist	SS 3	67 (6)	3-3-4 (7)	1.5	1.3	21.9					
	<u>630.6</u> 		black BURIED TOPSOIL (A-8) stiff, moist	ST 4	58		1.0		56.0					
	626.6		brown CLAY LOAM (A-6) soft, moist	ss	78	1-1-2 (3)			43.6	-				
10:30 - C:\USEI	625.6		gray CLAY (A-6) very soft, moist	ss 6	67	1-1-2 (3)	0.25	0.2	29.6	-				
15	622.6		gray CLAY (A-6)							-				
I EMIRTATE.c	-		very stiff, moist	ST 7	63		2.0		15.9					
	IPLETION	DEPT	H 80 ft GROUND ELEVATION 638.56	S ft N	DTES	1		1		1			1	
	/E DEPTH	ft	BACKFILL Soil Cuttings		-									
GRC	ound wa	TER LE	VELS:											
- 90	AT TIME	OF D	RILLING None											
EULECH L	AT END		RILLING Dry upon completion NG											
			ation represent an approximate boundary betwee and the transition may be gradual. Dashed lines ar								ervals	and be	etween	
0			9370 W. Laraway Road, Suite D Frankfort,	IL 60423	Phone	815-806-9	986	Fax 8	315-46	4-869´	1			



BORING NO. B-02 PAGE 2 OF 4

DATE COMPLETED 4/18/17 LOGGED BY NJ/GL DRILLING METHOD 3.25 in. I.D. HSA T (i) (i)<				Engineering, Ltd. _17-G0411			ME <u>Clave</u>					er			
Human Material Description Material Desc															
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $									(n						
		ELEVATION (ft.)	GRAPHIC LOG		SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT. (pcf)	ORGANIC CONTENT (%)			
						78		3.25	3.4	15.9	-		27	14	13
						78		4.0	4.0	14.9					
						78		3.25	3.4	15.1	-				
						78		3.0	3.1	16.6	-				
	 _ <u>30</u>					96		3.0	2.42	17.4	116.1		28	15	13
35 35 36 14 89 4-7-7 (14) 2.25 2.1 14 89 4-7-7 (14) 19.5						89		2.25	2.3	16.8	-				
	 _ <u>35</u>					89		2.25	2.1	19.5	-				
40 SS 100 4-8-9 (17) 2.5 2.5 14.6						100		2.5	2.5	14.6					
Lines of Demarcation represent an approximate boundary between soil types. Variations may occur between sampling intervals and between boring locations, and the transition may be gradual. Dashed lines are indicative of potentially erratic or unknown changes. 9370 W. Laraway Road, Suite D Frankfort, IL 60423 Phone 815-806-9986 Fax 815-464-8691				and the transition may be gradual. Dashed line	s are indicative of	potent	ally erratic o	or unkn	own cł	nanges	5.		and b	etweer	<u></u>



BORING NO. B-02 PAGE 3 OF 4

	COMPLE		17-G0411 \$/18/17 LOGGED BY <u>NJ/GL</u>			CATION _ THOD _3.2								
	_	_	<u> </u>										TERBE	
(ff)	ELEVATION (ft.)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT. (pcf)	ORGANIC CONTENT (%)	LIQUID LIMIT	PLASTIC LIMIT	
_			gray CLAY (A-6) very stiff, moist <i>(continued)</i>											
_ _ 45				SS 16	78	5-8-8 (16)	2.5	2.9	20.9	-				
-														
- 50				SS 17	78	6-9-11 (20)	2.25	2.2	22.1	-				
- 55	583.6			SS 18	78	5-9-10 (19)	2.25	2.6	20.5	_				
-			gray CLAY (A-6) very stiff, moist											
- 60				SS 19	78	6-9-11 (20)	2.0	2.0	13.4	-				
-	nes of D	emarcat	on represent an approximate boundary b	etween soil types	Variati	ons may or			samp	ing int	ervale	and b	etweer	
b	oring loca	ations, ar	Id the transition may be gradual. Dashed lin	etween son types. les are indicative c	f potenti	ally erratic o	or unkr	nown cl	hanges		o vals		CINNEEL	'



PAGE 4 OF 4

	18/17 LOGGED BY NJ/GL	DRILLI		-	lighlar							
<u>u</u>			NG ME	THOD <u>3.2</u>	25 in. I.		SA 				ERBE	
GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT. (pcf)	ORGANIC CONTENT (%)			
	gray CLAY (A-6) very stiff, moist <i>(continued)</i>	SS 20	78	5-10-11 (21)	2.25	2.0	14.7	-				
		SS 21	67	10-16-20 (36)	2.5	2.2	14.2	-				
		SS 22	67	13-18-19 (37)	3.5	2.9	14.8	-				
.6		SS 23	67	13-20-26 (46)	3.5	2.9	14.3	-				
		6	gray CLAY (A-6) very stiff, moist (continued)	gray CLAY (A-6) very stiff, moist (continued) Image: style="text-align: center;">Image: style="text-align: center;">SS 78 Image: style="text-align: center;">Image: style="text-align: center;">SS 20 78 Image: style="text-align: center;">Image: style="text-align: center;">SS 20 78 Image: style="text-align: center;">Image: style="text-align: center;">SS 20 78 Image: style="text-align: center;">Image: style="text-align: center;">SS 67 Image: style="text-align: center;">SS 67 Image: style="text-align: center;">SS 67 Image: style="text-align: center;">SS 67	gray CLAY (A-6) very stiff, moist (continued) Image: stiflet in the stiflet in t	gray CLAY (A-6) very stiff, moist (continued) Image: Continued of the second secon	gray CLAY (A-6) very stiff, moist (continued) Image: Continued (Continued) Image: Continued (Continued) Image: Continue (Continued) Image: Continue (Continued) Image: Continue (Continued) Image: Continue (Continue (Continut	gray CLAY (A-6) very stiff, moist (continued) Image: Continued of the second secon	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	gray CLAV (A-6) very stiff, moist (continued) Image: Signature of the second secon	$\begin{array}{ c c c c c c c } \hline & & & & & & & & & & & & & & & & & & $	$\begin{array}{ c c c c c c } \hline & & & & & & & & & & & & & & & & & & $



			ngineering, Ltd. 17-G0411			ME <u>Clave</u> CATION H					r			
			4/19/17 LOGGED BY NJ/GL			THOD 3.2								
							Zp)	(Qu)					LIMIT:	
o DEPTH (ft)	ELEVATION (ft.)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT (pcf)	ORGANIC CONTENT (%)	LIMIT	PLASTIC LIMIT	PLASTICITY INDEX
-	<u>638.1</u> 637.7		0-6" CONCRETE PAVEMENT											
			blue CLAY FILL with gravel stiff, moist	ss 1	44	3-3-5 (8)	1.0	1.3	21.8	-				
	634.6		brown CLAY FILL with gravel very stiff, moist		44	9-11-7 (18)			6.5	-				
	631.6		black BURIED TOPSOIL (A-8)		44	3-2-3 (5)	-		19.7	-				
 _ <u>10</u>	630.6		soft, moist mottled brown and gray CLAY (A-6) medium stiff, moist		56	2-2-2 (4)	-	0.8	26.3	-				
	625.6		∇	SS 5	78	2-3-4 (7)	-	0.6	23.8	-		30	14	16
 <u>15</u>	020.0		brown SILTY LOAM (A-4) medium stiff, moist		56	3-3-3 (6)	0.5	-	16.8	-				
	622.6		gray CLAY (A-6) very stiff, moist	ss 7	78	7-8-9 (17)	3.0	3.5	16.1	-				
					78	10-12-13 (25)	4.0	3.0	13.4	-				
CAVE GROU ⊈	DEPTH IND WAT	<u>10 ft</u> Fer Le Of Di Of Dr	EVELS: RILLING13.00 ft / Elev 625.57 ft RILLING10.00 ft / Elev 628.57 ft	57 ft N	OTES									
			ation represent an approximate boundary betwee and the transition may be gradual. Dashed lines a 9370 W. Laraway Road, Suite D Frankford	are indicative o	of potent	ially erratic o	or unkn	nown cł	nanges	5.		and b	etweer	1



BORING NO. B-03 PAGE 2 OF 2

			ngineering, Ltd. 17-G0411			ME <u>Clave</u>	-				r			
	COMPLE	_				THOD <u>3.2</u>				015				
													LIMITS	
DEPTH (ft)	ELEVATION (ft.)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT. (pcf)	ORGANIC CONTENT (%)	LIQUID	PLASTIC	PLASTICITY
			gray CLAY (A-6) very stiff, moist <i>(continued)</i>			8-9-11 (20)	3.25	3.9	14.2					
						6-7-10 (17)	3.5	4.0	15.3			27	14	13
· _					³ 67	6-7-9 (16)	2.5	2.6	16.4					
<u> </u>					2 78	6-6-10 (16)	3.0	3.8	10.9					
35					3 78	6-9-12 (21)	3.25	3.9	14.4					
 40	598.6		Bottom of borehole at 40.0 fe		3 78	5-10-14 (24)	3.0	3.2	16.2					
L	ines of Do	emarca tions, a	tion represent an approximate boundary nd the transition may be gradual. Dashed li	between soil types nes are indicative	. Variat	ions may oo ially erratic o	ccur be or unkr	etween nown ch	sampl	ing int	ervals	and b	etweer	1
	0	, -	, , , , , , , , , , , , , , , , , , , ,			,			5-5					



DATE C	CT NUN		17-G0411 4/18/17 LOGGED BY NJ/GL	PRO	JECT										
	COMPLE	ETED	4/18/17 I OGGED BY NJ/GI					lighlar	nd Par	k, Illino	ois				
TH (_ DRIL	LING	S ME	THOD _ 3.2	25 in. I.	.D. HS	A					
Ħ_								(d	Qu)						
O DEPTH (ft)	ELEVATION (ft.)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE		RECUVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT. (pcf)	ORGANIC CONTENT (%)	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX
_	637.2	P 4 4	0-6" CONCRETE PAVEMENT												
	<u>636.9</u> 634.7		6-10" AGGREGATE BASE		SS 1	56	5-6-9 (15)	2.0	1.4	17.9					
			brown SAND FILL with gravel medium dense, moist		SS 2	33	6-6-5 (11)	0.5		23.0					
· _	631.7	<u>x¹ 1₂ x¹ 1₂</u>	black BURIED TOPSOIL (A-8) soft, moist		SS 3	33	5-2-3 (5)	-		11.9		5.7			
10	629.7		mottled brown and gray CLAY LOAM (A-6) very soft to medium stiff, moist	1 X 1	3S 4 1	100		0.75	0.49	31.4	91.5				
				s	SS - 5	78	2-2-1 (3)			23.2					
· _					6	63		0.5	0.16	36.1	94.2				
15	622.7				SS - 7	78	1-2-1 (3)	0.75	0.5	28.4					
· -			gray CLAY (A-6) very stiff, moist												
20					8 8	78	6-8-9 (17)	2.75	3.5	15.8					
CAVE [GROUN A A	DEPTH ND WAT AT TIME	ft Er Le Of Di Of Dr	RILLING None		NOTI	ËS		<u> </u>							
			ation represent an approximate boundary between s and the transition may be gradual. Dashed lines are ir									ervals	and be	etweer	



BORING NO. B-04 PAGE 2 OF 2

			ngineering, Ltd.					ME Clave					r			
		-	<u>17-G0411</u>									ois				
DATE	COMPLE		<u>4/18/17</u> LC	DIGGED BY NJ/GL	DR	ILLIN		THOD <u>3.2</u>	25 in. i	.D. н5 Т	A				ERBE	
									(d	Qu)						
DEPTH (ft)	ELEVATION (ft.)	GRAPHIC LOG		RIAL DESCRIPTION	SAMPLE TYPE	NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT. (pcf)	ORGANIC CONTENT (%)	LIQUID	PLASTIC LIMIT	PI ASTICITY
			gray CLAY (A- very stiff, mois	6) t (continued)	X	SS 9	78	7-10-16 (26)	3.5	3.0	14.9					
25					X	SS 10	78	6-9-12 (21)	3.5	3.2	15.8					
-						SS 11	78	5-7-9 (16)	2.5	2.8	17.2					
30					X	SS 12	67	6-9-10 (19)	2.5	2.0	14.4					
35					X	SS 13	78	5-7-8 (15)	2.25	2.2	17.5					
	597.7				Μ	SS 14	78	4-6-8 (14)	2.25	2.4	18.8					
			Bottom	of borehole at 40.0 feet.												
L	ines of D	emarca itions, a	tion represent an a nd the transition ma	pproximate boundary be y be gradual. Dashed line	tween soil types are indicativ	oes. ve of	Variati potenti	ons may oo ally erratic o	ccur be or unkn	etween nown ch	sampl	ing inte	ervals	and be	etweer	1
			9370 W araway	Road, Suite D Frankf		<u> </u>		915 906 0		F -14	45 40	4 000				



			ingineering, Ltd.	_		ME <u>Clave</u>					r			
				-		CATION <u> </u> THOD <u>3.2</u>				ois				
													LIMITS	
o DEPTH (ft)	ELEVATION (ft.)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT. (pcf)	ORGANIC CONTENT (%)	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX
	636.9 636.6		0-6" CONCRETE PAVEMENT											
	635.4		mixed black and brown CLAY FILL with gravel very stiff, moist	ss ss	56	12-6-16 (22)	3.0	3.3	3.0					
			brown GRAVEL FILL medium dense, moist				_							
5	632.4			ss 2	56	3-4-4 (8)			3.2					
			mixed brown and gray CLAY FILL with sand soft, moist	√ ss		2-2-2				-				
	630.4 629.4		black BURIED TOPSOIL (A-8) soft, moist	3	44	(4)	0.5	0.5	0.3					
	627.4		mottled brown and gray CLAY (A-6) soft, moist ▼	ss 4	67	2-2-3 (5)	0.25	0.5	27.1					
			gray SILT LOAM (A-4) stiff to very stiff, wet	ss	67	3-4-3 (7)	-		21.2					
 15			∇	ST 6	88		2.5	3.24	19.2	251.1				
0 	619.4			ss 7	78	8-10-12 (22)	2.0	1.2	14.7					
 <u>20</u>	013.4		gray CLAY (A-6) very stiff to hard, moist		78	7-9-12 (21)	4.25	4.4	13.8					
COMP	DEPTH	13 ft		N	OTES								<u> </u>	<u> </u>
GRUU		of di of dr	ILLING 15.00 ft / Elev 622.40 ft ILLING 10.00 ft / Elev 627.40 ft											
L	ines of D	emarca	ation represent an approximate boundary between so and the transition may be gradual. Dashed lines are ind								ervals	and be	etween	1
		,	9370 W. Laraway Road, Suite D Frankfort, IL 6		•				0		1			



BORING NO. B-05 PAGE 2 OF 2

CLIEN	IT <u>Robi</u>	nson E	Engineering, Ltd.	PROJE	CT NA	ME <u>Clave</u>	ey Roa	d over	Skoki	e Rive	er			
PROJ	ECT NUN	IBER	17-G0411	PROJE	CT LO	CATION _	Highlar	nd Par	k, Illin	ois				
DATE	COMPLI	ETED			NG ME	THOD _ 3.2	25 in. I	.D. HS	A					
							(d	Qu)				AT		ERG
DEPTH (ft)	ELEVATION (ft.)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT. (pcf)	ORGANIC CONTENT (%)	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY INDEX
			gray CLAY (A-6) very stiff to hard, moist <i>(continued)</i>	ST 9	46		3.75	2.33	13.9	120.2				
				SS 10	78	9-13-17 (30)	2.5	2.3	14.5	-				
				SS 11	89	5-6-12 (18)	2.0	4.0	16.2	-				
 <u>30</u>				SS 12	78	6-8-11 (19)	3.0	4.0	16.0	-		27	12	15
	603.4		gray CLAY (A-6)	ss	67	5-10-13	_	1.0	13.5	-		25	14	11
	599.4		stiff, moist	13		(23)	_			-				
 40	599.4		gray CLAY (A-6) hard, moist	SS 14	78	4-12-12 (24)	4.0	4.1	14.7	-				
			Bottom of borehole at 40.0 feet.											
b			ation represent an approximate boundary betw and the transition may be gradual. Dashed lines	are indicative of	potenti	ially erratic o	or unkn	own cł	nanges			and b	etweer	
			9370 W. Laraway Road, Suite D Frankfor	t, IL 60423 I	Phone	815-806-9	986	Fax 8	15-46	4 - 869´	1			



PAGE 1 OF 1

DATE	COMPL	Inson Engineering, Ltd. PROJECT NAME Clavey Road over Skokie River MBER 17-G0411 PROJECT LOCATION Highland Park, Illinois ETED 4/19/17 LOGGED BY NJ/GL DRILLING METHOD 3.25 in. I.D. HSA												
		ETED _	4/19/17 LOGGED BY NJ/GL	DRILLI		THOD <u>3.2</u>	25 in. I.	.D. HS	SA					
ļ							(dC	(Qu)					FERBE LIMITS	
DEPTH (ft)	ELEVATION (ft.)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT (pcf)	ORGANIC CONTENT (%)	LIQUID	PLASTIC LIMIT	PLASTICITY
0.0			0-9" CONCRETE PAVEMENT											-
	636.2		9-13" AGGREGATE BASE											
_	635.8		brown SAND FILL with gravel loose to dense, moist	SS 1	56	2-2-2 (4)			4.8					
2.5				V N										
				SS 2	56	5-5-6 (11)			5.7					
-														
7.5				SS 3	67	4-3-3 (6)			7.0					
_														
- 10.0	626.9			SS 4	33	5-12-13 (25)			8.4					
			Bottom of borehole at 10.0 feet.								-			
COMF	LETION		I _10 ft GROUND ELEVATION _636.9	1 ft N	DTES									
CAVE	DEPTH	9 ft	BACKFILL Soil Cuttings											
	IND WA		-											
			ILLING None											
			LLING Dry upon completion IG											
			tion represent an approximate boundary between the transition may be gradual. Dashed lines a								ervals	and be	etweer	 1
	3.20	, u	9370 W. Laraway Road, Suite D Frankfort		•				0					



BORING NO. Composite PAGE 1 OF 1

PROJECT MILL	IRFR 17 /	(-()411						<u>d over</u> nd Par						
PROJECT NUN DATE COMPLE		LOGGED B	3Y			_	ligiliai	iu r ai	<u>, IIII I</u>	015				
								<u> </u>					TERBE	
O DEPTH (ft) ELEVATION (ft.)	GRAPHIC LOG	MATERIAL DES	SCRIPTION	SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT. (pcf)	ORGANIC CONTENT (%)	LIQUID		
-				S ss										
CAVE DEPTH	ft ER LEVEL	<u>ft</u> GROUND EL BACKFILL _ S: NG	Soil Cuttings		DTES									
CAVE DEPTH GROUND WAT AT TIME AT END	ft ER LEVEL: OF DRILLI OF DRILLI	BACKFILL _ S: NG NG	Soil Cuttings		DTES									
CAVE DEPTH GROUND WAT AT TIME AT END AFTER D	ft ER LEVEL: OF DRILLI OF DRILLIN DRILLING _	BACKFILL _ S: NG NG	Soil Cuttings											
CAVE DEPTH GROUND WAT AT TIME AT END AFTER D Lines of D	ft ER LEVEL: OF DRILLI OF DRILLING _ emarcation	BACKFILL _ S: NG NG	Soil Cuttings	en soil types.	Variatio	ons may oc ally erratic o	ccur be	etween iown ch	sampl	ling int	ervals	and b	etween	

REPORT OF GEOTECHNICAL INVESTIGATION

Clavey Road Bridge over Skokie River

Existing Structure # 049-6585

Highland Park, Illinois

Prepared by:

Soil and Material Consultants, Inc. 8 West College Drive, Suite C Arlington Heights, Illinois 60004

Prepared for:

Ciorba Group, Inc. 5507 North Cumberland Ave. Suite 402 Chicago, Illinois 60656



SOIL AND MATERIAL CONSULTANTS, INC.

Office: 847-870-0544 Fax: 847-870-0661 us@soilandmaterialconsultants.com www.soilandmaterialconsultants.com

> September 3, 2020 File No. 24919 UPDATED

Brett Sauter, P.E., S.E. Ciorba Group 5507 North Cumberland Avenue Chicago, IL 60656

> Re: Structural Geotechnical Report Clavey Road Bridge over Skokie River Structure No. 049-6585 Highland Park, Illinois

Dear Mr. Sauter:

This in an updated report to reflect changes to the project limits and incorporate IDOT review comments. The following is our structural geotechnical report, using the information provided by Geocon Professional Services report number 17-G0411 completed on April 17, 2017, for the Clavey Road Bridge over Skokie River in the Village of Highland Park, Illinois. This report is intended to assist in the planning, design, and construction of proposed site improvements.

We understand it is proposed to remove the existing bridge and replace it with a new bridge supported on a driven pile or drilled pier foundation. Specific plans for the bridge type and location have not been finalized at the time of this report. We understand the project limits in the design plans extend from Station 25+90 to Station 32+00.

SCOPE OF THE INVESTIGATION

The field investigation performed by Geocon Professional Services included 2 borings at the locations indicated on the enclosed location sketch.

The 2 structure borings were auger drilled to depths of 100.0 feet and 80.0 feet below existing surface elevations. Soil samples were obtained at a 2.5-foot interval until a depth of 35.0 feet in which soil samples were taken at a 5.0 foot interval to the end of the borings. Additional testing included determination of dry unit weight, unconfined compressive strength, grain-size distribution, Atterberg limits, and related testing.

SITE GEOLOGY/USDA SOIL TYPING

Enclosed is a map indicating the pedological characteristics of the site as determined by the USDA Soil Conservation Service. The soils indicated are a generalization of soil types and conditions anticipated to exist at or near existing surface elevations. Typically, these maps were developed without benefit of a direct on-site soil investigation. The soil typing map is presented for general information only.

8 W. COLLEGE DR. • SUITE C • ARLINGTON HEIGHTS, IL 60004

File No. 24919

Re: Clavey Road Bridge over Skokie River Structure No. 049-6585 Highland Park

<u>Symbol</u>	<u>Soil Types</u>
153A	Pella Silty Clay Loam, 0 to 2 percent slopes
330A	Peotone Silty Clay Loam, 0 to 2 percent slopes
802B	Orthents, loamy, undulating
805B	Orthents, clayey, undulating
1330A	Peotone Silty Clay Loam, undrained, 0 to 2 percent slopes

CLIMATIC CONDITIONS

Climatic conditions for the period prior to obtaining site soil borings include the following information recorded at O'Hare International Airport in Chicago, Illinois:

Month	Total	Departure	Average	Departure
	<u>Precipitation</u>	From Normal	Temperature	From Normal
Dec 2016	1.77 in.	-0.48 in.	25.0° F.	-2.7° F.
Jan 2017	2.87 in.	1.14 in.	28.8° F.	5.0° F.
Feb 2017	1.52 in.	-0.27 in.	38.1° F.	10.4° F.
Mar 2017	4.01 in.	1.51 in.	39.5° F.	1.6° F.

The above information has been considered in our analysis of the site soil conditions.

RESULTS OF THE INVESTIGATION - BRIDGE

Enclosed are boring logs indicating soil conditions encountered at each location. Borings B-1 and B-2 were performed in the area of the proposed abutments. Site surface conditions include the existing structure, pavement materials, and fill soil conditions.

Fill soil conditions were encountered at each boring location. Composition of the fill includes the presence of clay/silt, and gravel mixtures extending to a depth of 8.0 feet below existing surface elevations. The limits of fill placement were not determined within the scope of this investigation. Beneath the fill soils, buried topsoil was encountered which extended to depths of 10.0 feet to 12.0 feet below surface elevations. Larger debris may also be present within the fill but was not encountered during the investigation.

Underlying natural soil conditions include the presence of cohesive soils. These are classified as stiff to very hard clay/silt mixtures with lesser portions of sand and gravel. Cobbles and boulders may be present within the site soils at any elevation, although none were encountered while drilling.

File No. 24919 Re: Clavey Road Bridge over Skokie River Structure No. 049-6585 Highland Park

The following table summarizes depth ranges below existing grade, the magnitude of soil strength within these ranges and other information:

<u>Boring</u>	Surface Elevation <u>(feet)</u>	Depth Range Below Existing Surface <u>(feet)</u>	Net Allowable Bearing Capacity <u>(Ibs./sq.ft.)</u>	Recorded Water Levels, W.D./A.D. <u>(feet)</u>
1	637.4	0.0 to 4.0 4.0 to 15.0 15.0 to 19.0 19.0 to 25.0 25.0 to 44.0 44.0 to 54.0 54.0 to 74.0 74.0 to 79.0 79.0 to 84.5 84.5 to 97.0	*2,000 *500 4,000 *500 3,000 5,000 3,000 4,000 5,000 8,000	Dry / Dry
2	638.6	1.5 to 17.0 17.0 to 19.0 19.0 to 24.0 24.0 to 74.0 74.0 to 77.0	*500 4,000 6,000 4,000 5,000	Dry / Dry

SHALLOW FOUNDATIONS

We understand shallow depth approach footings will be used beneath the approach pavements. These footings can be supported on suitable fill soils. Weak soil conditions may be discovered locally at design footing elevations and may require extending the foundation to a deeper elevation. Alternately, removal of the weak soil followed by replacement with properly compacted crushed granular fill may be feasible. When removal is approved by the Soil Engineer, the removal of the weak soil should also extend beyond the face of footings to a distance at least equal to the depth of fill that will be present beneath the footings. A capping layer of finer crushed granular fill (CA06) can be utilized to establish a working surface.

Sliding Resistance Factors for geotechnical resistance of shallow foundations at the strength limit state are 0.85 and 0.80 for the for cast-in-place concrete on clay and sand respectively. These values were obtained from Table 10.5.5.2.2-1-1 of the AASHTO LRFD Bridge Design Specifications.

DRILLED PIER FOUNDATIONS

A drilled pier foundation system is currently under consideration for support of the new bridge foundations. The drilled pier foundation system, designed by a licensed structural engineer, can be utilized to support the structure utilizing skin friction and end bearing of soils at deeper elevations. Drilled piers should extend about 3.0 feet or deeper into soils possessing the design bearing strength. The bottom of the shafts could possibly be belled to increase the load

carrying capacity of each caisson. Belling would require extending the drilled shaft further into the cohesive soils as needed to assure non-caving soil conditions in the sidewall of the bell.

Temporary or permanent casing extending above the ground surface is needed to prevent caving of the soil around the top of the drilled shaft. Further, temporary or permanent casing will be needed when drilling through caving soils. The casing will also reduce the volume of water seeping into the drilled shaft.

Downdrag and liquefaction are not expected to affect the design of the new bridge foundations. A scour elevation of 604.90 feet was provided by Ciorba Group, Inc. and used in estimating the drilled pier depths. If a drilled pier foundation is chosen, Ciorba has estimated 6 drilled piers will be used to support each bridge abutment with an approximate non-factored vertical load of 173 kips per drilled pier.

The following table shows estimated drilled pier lengths for a 3.0 ft. diameter shaft with a 4.5 ft. diameter bell. The estimates are based upon the Geocon boring logs and formulas by Reese and O'Neill (1989) for estimation of the ultimate and allowable bearing capacity of drilled shafts.

Location	Depth (feet)	Strength Limit State (kips)	Service Limit State (kips)
West Abutment (B-1)	44.0	125	295
	61.0	150	345
	70.0	175	403
East Abutment (B-2)	46.0	125	276
	53.0	150	336
	60.0	175	395

Please note the strength limit state was calculated using a safety factor of 3 while the service limit state does not contain a safety factor.

DRIVEN PILE FOUNDATIONS

A driven pile foundation system could also be considered for support of the new bridge. The pile foundation system, designed by a licensed structural engineer, can be utilized to transmit loads into suitable soil conditions present at the deeper elevations. The selection of a pile foundation system should include consideration of the negative impact of vibration on adjacent structures.

The following table shows estimated pile lengths for metal shell and H-Piles based upon the Modified IDOT Static Method of Estimating Pile Length using a geotechnical resistance factor (Φ_G) of 0.55, modified September, 2017. Downdrag and liquefaction are not expected to affect the design of the new bridge foundations. A scour elevation of 604.90 feet was provided by Ciorba Group, Inc. and used for estimating the driven pile lengths.

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Table of Estimated Lengths for Metal Shell 14" w/ .312" Walls						
Location West Side (B-1)	<u>R_n (kips) ⁽¹⁾</u> 280 332 390	<u>R_f (kips) ⁽²⁾</u> 80 100 120	Length (ft.) ⁽³⁾ 46 52 58			
East Side (B-2)	330 380 415	80 100 120	44 50 54			
Table of Estim	nated Lengths for I	Metal Shell 16" w/ .3	312" Walls			
Location West Side (B-1)	<u>R_n (kips) ⁽¹⁾</u> 385 440 482	<u>R_f (kips) ⁽²⁾</u> 125 150 175	Length (ft.) ⁽³⁾ 53 62 67			
East Side (B-2)	435 485 535	125 150 175	50 57 63			
Table o	f Estimated Lengt	<u>hs for HP 12 x 53 P</u>	iles			
Location West Side (B-1)	<u>R_n (kips) ⁽¹⁾</u> 226 250 275	<u>R_f (kips) ⁽²⁾</u> 70 85 100	Length (ft.) ⁽³⁾ 47 57 63			

East Side (B-2) 240 70 46 270 85 53 300 100 58

⁽¹⁾ R_n: Nominal Required Bearing

⁽²⁾ R_f: Factored Resistance Available

⁽³⁾ Pile Lengths were estimated assuming the piles would be driven from a surface elevation of 633.4 feet and the piles would be cut-off at elevation 634.4 feet.

If pile foundations are chosen to support the structure, we recommend that one test pile be performed at each substructure location. The piles should be driven until the required driving resistance is developed as determined using the appropriate pile driving formula. The test piles should be driven to not less than 110% of the Nominal Required Bearing. We would also recommend that the WSDOT formula be used in the field as the construction verification. The designer should also consider the use of metal shell pile shoes as the piles may encounter cobbles, boulders and thin dense layers of material during driving.

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We would recommend foundations extend at least 60.0 inches below exposed surface elevations to provide adequate protection against uplift due to freezing of the supporting soils. Adequate reinforcing steel in foundations and wing walls should be used to minimize the effects of long-term differential settlement.

DESIGN VALUES

Where applicable, the following average values can be utilized for design:

Clay Fill Soils

Unit Weight (lbs./cu.ft.)	=	120.0
Angle of Internal Friction (drained)	=	22°
Angle of Internal Friction (undrained)	=	0°
Cohesion, Cu (psf)	=	500
Active Stress Coefficient, Ka	=	0.45
Passive Stress Coefficient, K _p	=	2.20
At-Rest Stress Coefficient, K _o	=	0.63
Soil Modulus, K (pci)	=	100
Soil Strain, E50	=	0.01

Granular Fill Soils

Unit Weight (lbs./cu.ft.)	=	110.0
Angle of Internal Friction	=	38°
Active Stress Coefficient, Ka	=	.24
Passive Stress Coefficient, K _p	=	4.20
At-Rest Stress Coefficient, K _o	=	0.38

Topsoil

Unit Weight (lbs./cu.ft.)	=	85.0
Angle of Internal Friction	=	10°
Active Stress Coefficient, Ka	=	.70
Passive Stress Coefficient, K _p	=	1.42
At-Rest Stress Coefficient, K _o	=	0.83

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Cohesive Soils (soft to stiff)

Unit Weight (lbs./cu.ft.)	=	110.0
Angle of Internal Friction (drained)	=	23°
Angle of Internal Friction (undrained)	=	0°
Cohesion, Cu (psf)	=	1500
Active Stress Coefficient, Ka	=	.29
Passive Stress Coefficient, K _p	=	3.39
At-Rest Stress Coefficient, K _o	=	.46
Soil Modulus, K (pci)	=	200
Soil Strain, E50	=	0.007
Cohesive Soils (very stiff to hard)		
Unit Weight (lbs./cu.ft.)	=	132.0
Angle of Internal Friction (drained)	=	30°
Angle of Internal Friction (undrained)	=	0°
Cohesion, Cu (psf)	=	3000
Active Stress Coefficient, Ka	=	.33
Passive Stress Coefficient, K _p	=	3.00
At-Rest Stress Coefficient, K _o	=	.50
Soil Modulus, k (pci)	=	400
Soil Strain, E50	=	0.005
Granular Backfill (CA06, crushed gravel)		
Unit Weight (lbs./cu.ft.)	=	142.0
Angle of Internal Friction	=	32°
Active Stress Coefficient, K _a	=	.31
Passive Stress Coefficient, K _p	=	3.25
At-Rest Stress Coefficient, K _o	=	.47
Granular Backfill (CA07, crushed gravel)		

Unit Weight (lbs./cu.ft.)	=	105.0
Angle of Internal Friction	=	32°
Active Stress Coefficient, Ka	=	.31
Passive Stress Coefficient, K _p	=	3.25
At-Rest Stress Coefficient, Ko	=	.47

File No. 24919 Re: Clavey Road Bridge over Skokie River Structure No. 049-6585 Highland Park

Factors of Safety are not applied to the above values. All backfill materials placed behind walls are presumed to be drained. Passive pressures within 4.0 feet of the surface should be omitted due to seasonal weather conditions.

The boring logs indicate subsurface water was not encountered in the bore holes at the time of the drilling operations and during the period of these readings. It is expected that fluctuations from the water levels recorded will occur over a period of time due to variations in rainfall, temperature, subsurface soil conditions, soil permeability and other factors not evident at the time of the water level measurements.

SEISMIC CONSIDERATIONS

Seismic Site Class is based on the average properties of subsurface materials to a depth of 100 feet below the ground surface. Based on the soil conditions encountered in Geocon's report and using the LRFD Seismic Soil Site Class Definition, a Site Class C was determined by Geocon.

The proposed new bridge is located in Seismic Performance Zone (SPZ) 1 with a risk category of II. The design spectral acceleration at 1.0 sec (S_{D1}) = 0.066 g and the design spectral acceleration at 0.2 sec (S_{Ds}) = 0.098 g.

<u>SETTLEMENT</u>

The existing soils are expected to undergo some small degree of long-term settlement as the soils consolidate under loading. A preliminary estimate based upon initial design information suggests that post-construction total and differential settlement of bridge abutments could be in the range of 0.75 inches and 0.50 inches respectively. Variations in supporting soil strength will likely increase the magnitude of total and differential settlement. Minimal settlement is expected for any new embankments constructed provided they are constructed in accordance with the IDOT Standard Specifications.

DEWATERING

Excavations may require dewatering due to subsurface water seepage and/or surface precipitation. This water can likely be removed to depths of several feet by standard sump and pump operations. Soils exposed at foundation, slab or undercut elevations should not be permitted to become saturated. Loss of bearing strength and stability may occur, requiring additional soil excavation.

Cohesive soils, non-cohesive soils and others can be unstable when saturated. These soils tend to cave or run when submerged or disturbed. The stability of exposed embankments is minimal to non-existent as confining soil pressures are removed. Proper drainage within excavations is necessary at all times, particularly when excavations extend below anticipated water levels and below saturated soils.

The contractor should be made responsible for designing and constructing stable temporary excavations. Also, the contractor should shore, slope, bench or restrain the sides of the

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excavations as required to maintain stability of both the excavation sides and bottom. In no case, should the slope, slope heights, or excavation depth exceed those in the local, state, and federal safety regulations.

CONCLUSION

The information within this report is intended to provide initial information concerning subsurface soil and water conditions on the site. Variations in subsurface conditions are expected to be present between boring locations due to naturally changing and filled soil conditions. Our understanding of the proposed improvements is based on information available to us at the writing of this report.

If you have any questions concerning the findings or recommendations presented in this report, please let us know.

Very truly yours,

SOIL AND MATERIAL CONSULTANTS, INC.

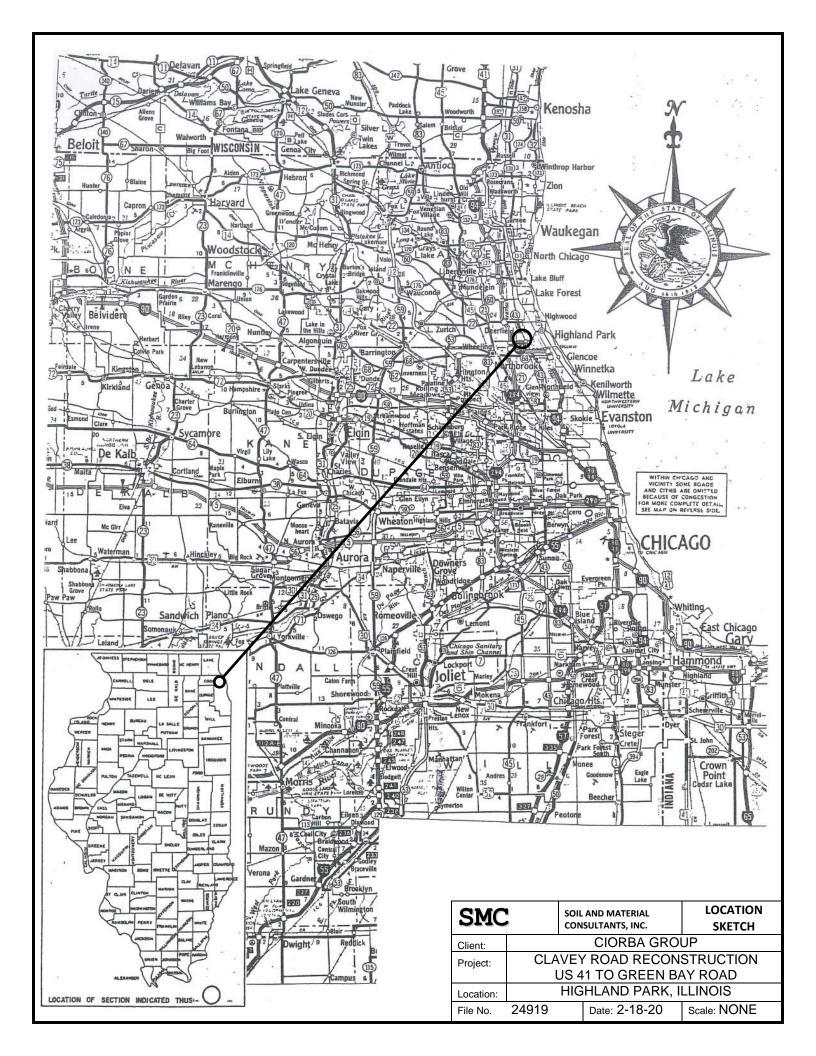
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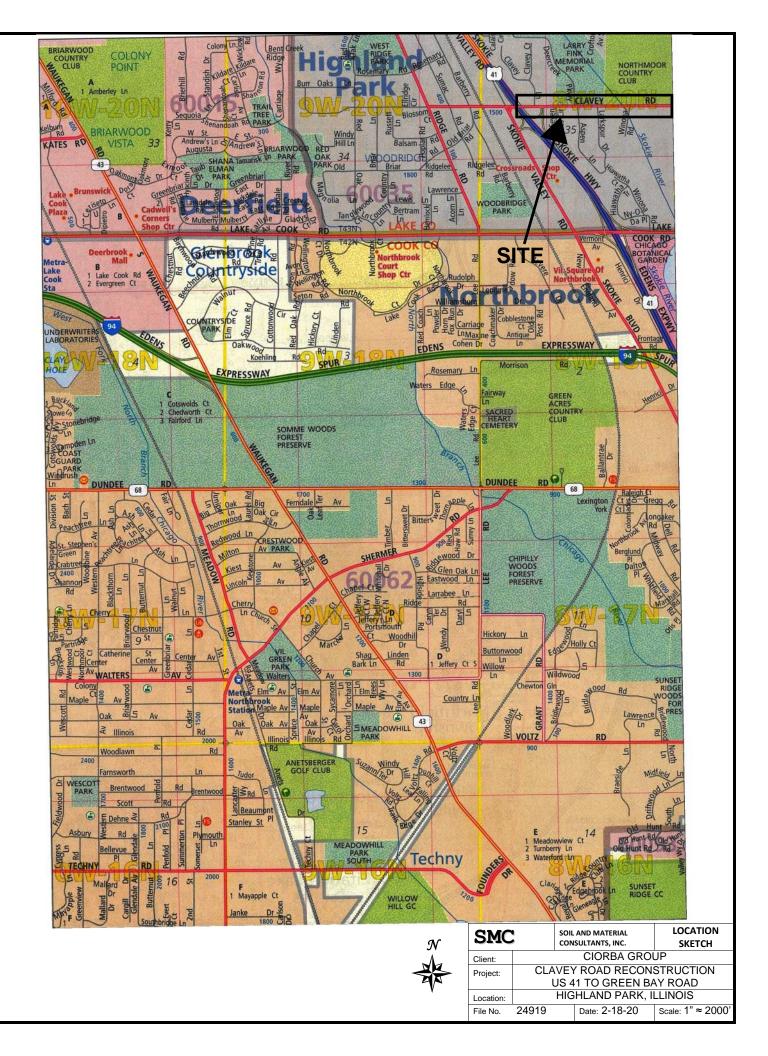
Reid T. Steinbach, P.E. Project Engineer

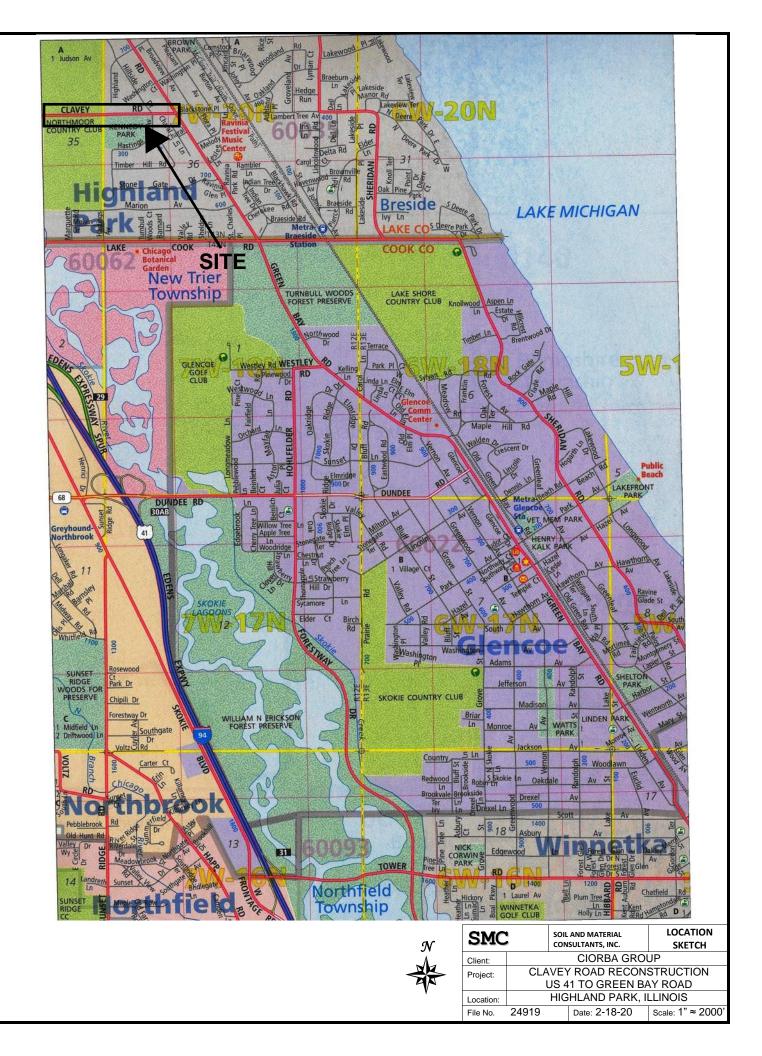
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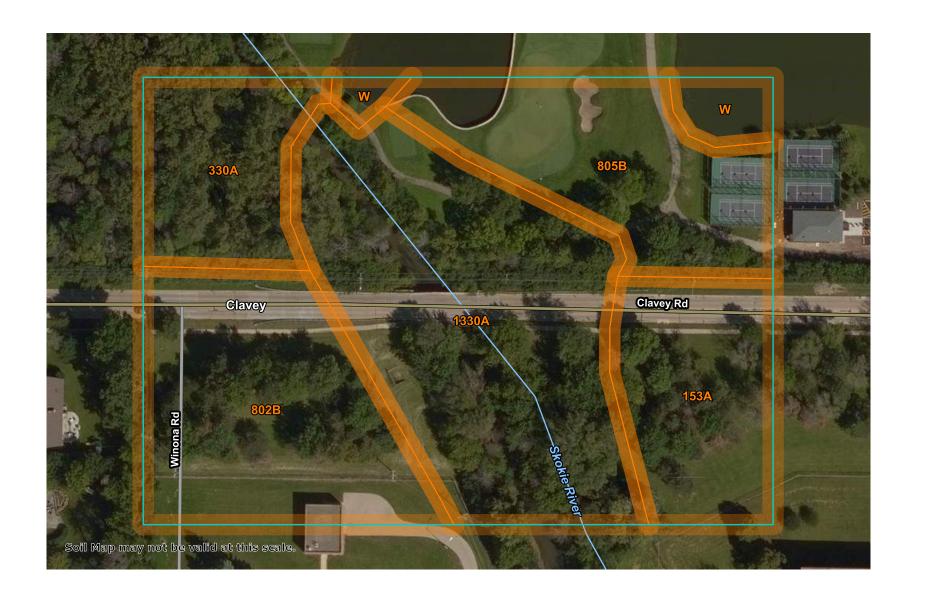
Thomas P. Johnson, P.E. President

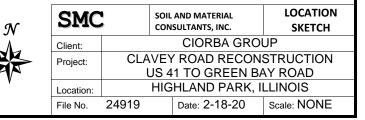
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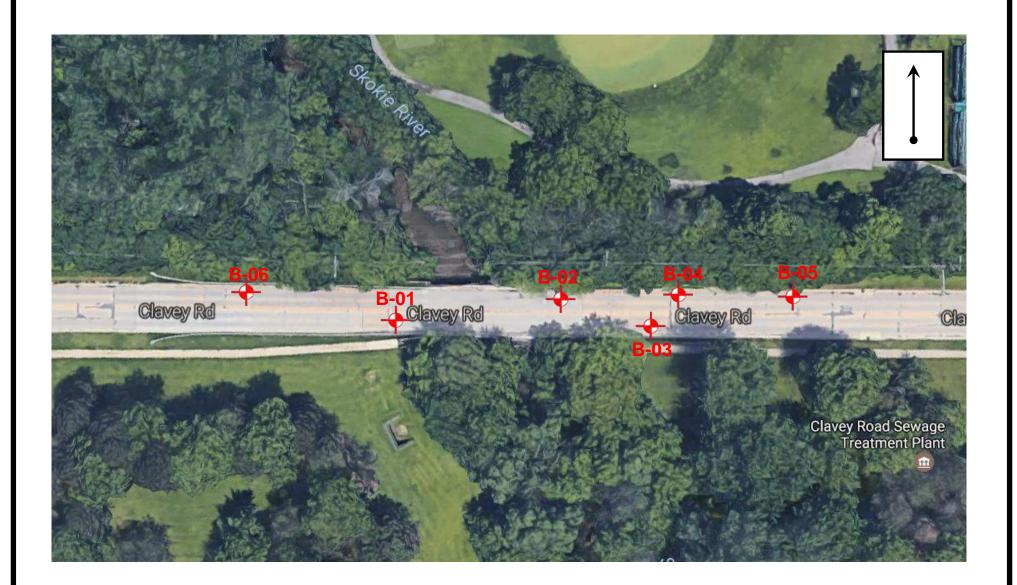






9370 Laraway Road, Suite D Frankfort, IL 60423 P.815.806.9986 F. 815.464.8691 FIGURE 1 SITE VICINITY MAP Clavey Road Bridge over Skokie River Highland Park, Illinois PROJECT NUMBER: 17-G0411

DATE: June 2017





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FIGURE 2

BORING LOCATION DIAGRAM Clavey Road Bridge over Skokie River Highland Park, Illinois PROJECT NUMBER: 17-G0411

DATE: April 2017



PAGE 1 OF 5

			Engineering, Ltd. _17-G0411			ME <u>Clave</u>					r			
DATE		ETED	4/17/17 LOGGED BY NJ/GL	DRILLI	NG ME	THOD _3.2	25 in. I	.D. HS	SA					
							др)	(Qu)					LIMITS	
C DEPTH O DEPTH (ft)	ELEVATION (ft.)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT. (pcf)	ORGANIC CONTENT (%)	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX
I KIVI	636.9 636.4		0-5" CONCRETE PAVEMENT 5-11" AGGREGATE BASE	-										
			mottled blue and gray CLAY FILL with gravel very stiff, moist	ss 1	56	5-3-7 (10)	2.0	-	17.3					
	-			ss 2	44	9-5-6 (11)	3.5	3.6	14.7					
=CIS/1/-G0411 CL	629.4			SS 3	56	6-4-5 (9)	2.5	2.6	19.2					
	627.4		black BURIED TOPSOIL (A-8) medium stiff, moist	SS 4	44	1-2-4 (6)			56.3		7.4	-		
	-		mottled brown and gray CLAY (A-6) soft, moist	ST 5	25		0.5	0.43	26.8	102.0				
======================================	622.4			SS 6	56	2-1-2 (3)	0.5	-	28.1			28	14	14
	-		gray SILTY LOAM (A-4) stiff, moist	ss 7	67	6-7-6 (13)	2.0	2.0	16.2					
	e depth Jnd Wat At Time	ft Fer Le Of Di Of Dr	RILLING None RILLING Dry upon completion	N(DTES									
			ation represent an approximate boundary between s and the transition may be gradual. Dashed lines are in 9370 W. Laraway Road, Suite D Frankfort, IL	dicative of	potent	ially erratic o	or unkn	iown cł	nanges			and b	etween	



BORING NO. B-01 PAGE 2 OF 5

PROJ		MBER	ngineering, Ltd. 17-G0411 4/17/17 LOGGED BY NJ/GL		CT LO	ME <u>Clave</u> CATION <u>H</u> THOD <u>3.2</u>	lighla	nd Par	k, Illin					
							2	(nt						
DEPTH (ft)	ELEVATION (ft.)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT. (pcf)	ORGANIC CONTENT (%)	LIQUID	PLASTIC LIMIT	
			gray CLAY (A-6) very stiff, moist	SS 8	78	4-8-12 (20)	3.5	3.2	13.2	-				
				ss 9	78	5-10-16 (26)	2.5	2.4	17.6	-				
				ST 10	44		2.0	0.33	18.4	118.4				
25	612.4 611.4		gray SILTY LOAM (A-4) with gravel ── dense, moist	- SS 11	44	9-10-8 (18)			13.9					
· -			brown CLAY (A-6) stiff, moist	SS 12	67	5-6-6 (12)	1.5	2.0	18.1	-				
30				SS 13	89	6-6-7 (13)	1.5	1.7	16.7	-				
				ST 14	92		2.0	-	15.4	-				
35				SS 15	78	6-6-8 (14)	2.0	1.8	19.0	-				
 				√ ss	78	6-7-7	1.75	1.7	21.4	-				
			tion represent an approximate boundary between and the transition may be gradual. Dashed lines are in		Variati		cur be	etween	sampl		ervals	and b	etween	
	0	, -	9370 W. Laraway Road, Suite D Frankfort, IL		•				•		1			



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TE COMI (ft) (ft) (ft) (ft)		4/17/17 LOGGED BY NJ/GL			THOD <u>3.2</u>								
(ff) (ft) ELEVATION (ft.)	읃										ATT	ERBE	R
	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT. (pcf)	ORGANIC CONTENT (%)	LIQUID	PLASTIC LIMIT	PI ASTICITY
-		brown CLAY (A-6) stiff, moist <i>(continued)</i>											
<u>593</u> - 4 <u>5</u> -	.9	brown CLAY (A-6) very stiff, moist	SS 17	78	6-8-9 (17)	2.5	2.0	19.9					
- - 50			SS 18	89	5-10-14 (24)	3.0	3.3	19.8					
			SS 19	78	6-10-15 (25)	3.0	3.1	21.4					
- - - <u>578</u> -	.9	gray CLAY (A-6) very stiff, moist	SS 20	89	4-5-5 (10)	1.5	1.6	24.7					
_	f Democra	tion represent an approximate boundary betwe		Variati			twoor		ing int	envelo	and h		



PAGE 4 OF 5

			17-G0411 4/17/17 LOGGED BY NJ/GL		CT LO	ME <u>Clave</u> CATION <u></u>	lighlar	nd Par		ois				
						<u>. 1600 _3.2</u>	5 m. i					AT	ERBE	ERC
DEPTH (ft)	ELEVATION (ft.)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT. (pcf)	ORGANIC CONTENT (%)			
- - 65 -			gray CLAY (A-6) very stiff, moist <i>(continued)</i>	SS 21	89	3-6-6 (12)	1.5	1.2	13.2					
- - 70 -	567.4		gray CLAY (A-6) very stiff to hard	SS 22	78	4-5-6 (11)	1.5	1.7	19.7					
75					100	9-50/2"	2.0		14.2					
- - 80 -				SS 24	56	10-14-16 (30)	2.5		14.0					
- - 85				SS 25	67	16-25-19 (44)	4.5	4.5	13.9					



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PROJI		BER	ngineering, l 17-G0411			PROJE		ME <u>Clave</u> CATION <u></u>	Highla	nd Par	k, Illin		er			
DATE	COMPLI		4/17/17	LOGGED BY NJ/GL		DRILLI	IG ME	THOD <u>3.2</u>	25 in. I	.D. HS	SA	1				
						111	,		Qp)	(Qu)					FERBE	
(ff) 82	ELEVATION (ft.)	GRAPHIC LOG		IATERIAL DESCRIPTION	J	SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT. (pcf)	ORGANIC CONTENT (%)	LIQUID LIMIT	PLASTIC LIMIT	PLASTICITY
			gray CL/ very stiff	AY (A-6) to hard <i>(continued)</i>												
-																
90						SS 26	67	14-19-17 (36)	4.5	4.0	11.7					
-						√ ss	56	15-19-31	4.5	4.5	13.2	_				
95						27	50	(50)	4.5	4.5	13.2	_				
							67	17-25-38 (63)	4.5	-	12.7	_				
100	537.4		Во	ottom of borehole at 100.0	feet.	/ \										
L	ines of D oring loca	emarca	tion represer	nt an approximate boundary	y between so d lines are ind	il types.	Variati	ons may or ally erratic of	ccur be	etween nown ch	samp	ling int	ervals	and b	etweer	1
b	oring loca	ations, a	and the transit	ion may be gradual. Dashed araway Road, Suite D Fra	d lines are ind	icative of	potenti	ally erratic o	or unkr	nown ch	nanges	3.				



PAGE 1 OF 4

CLI	ENT Robi		Ingineering, Ltd.	PROJE	CT NA	ME Clave	ey Road	d over	Skoki	e Rive	r			
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				ц	%		(Qp)	H (Qu)	()	<u>ц</u>	()	AT1		ERG
DEPTH DEPTH (#)	ELEVATION (ft.)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	RECOVERY (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT. (pcf)	ORGANIC CONTENT (%)	LIQUID	PLASTIC LIMIT	PLASTICITY INDEX
	638.1 637.7	P 4 4												
H H	- 037.7		5-10" AGGREGATE BASE				-			-				
JE OVER SKC	635.6		with gravel stiff, moist	SS 1	44	4-5-6 (11)			72.0	-				
	_		brown GRAVEL FILL dense, moist	ss 2	56	9-19-13 (32)			14.7	-				
11 CLAVEY F	632.6					(32)	-			-				
CIS/1/-G04	-		brown CLAY FILL stiff, moist	SS 3	67 (6)	3-3-4 (7)	1.5	1.3	21.9					
	<u>630.6</u> 		black BURIED TOPSOIL (A-8) stiff, moist	ST 4	58		1.0		56.0					
	626.6		brown CLAY LOAM (A-6) soft, moist	ss	78	1-1-2 (3)			43.6	-				
10:30 - C:\USEI	625.6		gray CLAY (A-6) very soft, moist	ss 6	67	1-1-2 (3)	0.25	0.2	29.6	-				
15	622.6		gray CLAY (A-6)							-				
I EMIRCATE.c	-		very stiff, moist	ST 7	63		2.0		15.9					
	IPLETION	DEPT	H 80 ft GROUND ELEVATION 638.56	S ft N	DTES	1		1	ı	1			1	
	/E DEPTH	ft	BACKFILL Soil Cuttings		-									
GRC	ound wa	TER LE	VELS:											
- 90	AT TIME	OF D	RILLING None											
EULECH L	AT END		RILLING Dry upon completion NG											
			ation represent an approximate boundary betwee and the transition may be gradual. Dashed lines ar								ervals	and be	etween	
0			9370 W. Laraway Road, Suite D Frankfort,	IL 60423	Phone	815-806-9	986	Fax 8	315-46	4-869´	1			



BORING NO. B-02 PAGE 2 OF 4

DEPTH (ff) (ff) (ff) (ff) (ff) CAPHIC LOG CLOG CLOG CLOG CLOG CLOG CLOG CLOG	PLASTIC LIMIT LIMIT PLASTICITY
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SS 13 89 6-10-10 2.25 2.3 16.8	15 13
SS 14 89 4-7-7 (14) 2.25 2.1 19.5	
35 35 40 Lines of Demarcation represent an approximate boundary between soil types. Variations may occur between sampling intervals and b boring locations, and the transition may be gradual. Dashed lines are indicative of potentially erratic or unknown changes. 9370 W. Laraway Road, Suite D Frankfort, IL 60423 Phone 815-806-9986 Fax 815-464-8691	
40 SS 100 4-8-9 (17) 2.5 2.5 14.6	
Lines of Demarcation represent an approximate boundary between soil types. Variations may occur between sampling intervals and b boring locations, and the transition may be gradual. Dashed lines are indicative of potentially erratic or unknown changes. 9370 W. Laraway Road, Suite D Frankfort, IL 60423 Phone 815-806-9986 Fax 815-464-8691	etween



BORING NO. B-02 PAGE 3 OF 4

	COMPLI		17-G0411 \$/18/17 LOGGED BY <u>NJ/GL</u>			CATION _ THOD _3.2								
	-	_	<u> </u>		-								TERBE	
(ff)	ELEVATION (ft.)	GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT. (pcf)	ORGANIC CONTENT (%)	LIQUID LIMIT	PLASTIC LIMIT	
_			gray CLAY (A-6) very stiff, moist <i>(continued)</i>											
- - 45				SS 16	78	5-8-8 (16)	2.5	2.9	20.9	-				
_														
- - 50				SS 17	78	6-9-11 (20)	2.25	2.2	22.1					
-														
-	583.6			SS 18	78	5-9-10 (19)	2.25	2.6	20.5	-				
			gray CLAY (A-6) very stiff, moist											
- 60				SS 19	78	6-9-11 (20)	2.0	2.0	13.4	-				
-	ines of D	emarcat	on represent an approximate boundary b	etween soil types	Variati				samn		ervals	and b	etweer	
b	oring loca	ations, ar	In the transition may be gradual. Dashed lin	es are indicative c	f potenti	ially erratic	or unkr	nown cl	hanges				CINVEEI	'



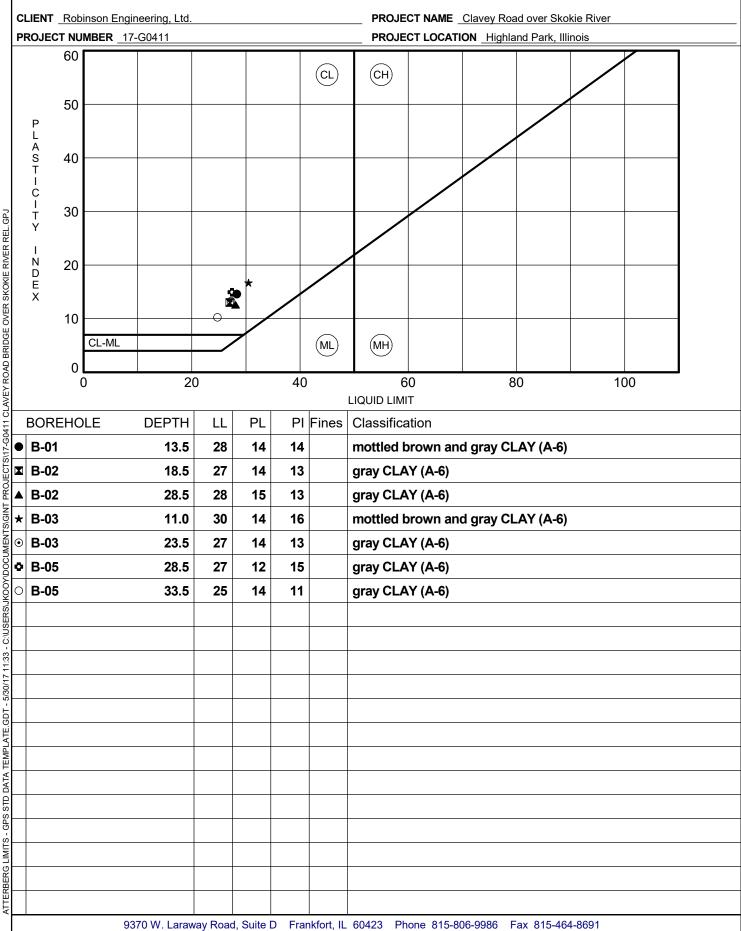
PAGE 4 OF 4

PLETED <u>4/1</u> 으	18/17 LOGGED BY NJ/GL	DRILLI		-			<u>k, Illin</u>					
<u>ں</u>			NG ME	THOD <u>3.2</u>	25 in. I.		SA 				ERBE	
GRAPHIC LOG	MATERIAL DESCRIPTION	SAMPLE TYPE NUMBER	RECOVERY % (RQD)	BLOW COUNTS (N VALUE)	POCKET PEN. (Qp) (tsf)	UNC. STRENGTH (Qu) (tsf)	MOISTURE CONTENT (%)	DRY UNIT WT. (pcf)	ORGANIC CONTENT (%)			PLASTICITY 0
	gray CLAY (A-6) very stiff, moist <i>(continued)</i>	SS 20	78	5-10-11 (21)	2.25	2.0	14.7	-				
		SS 21	67	10-16-20 (36)	2.5	2.2	14.2					
		SS 22	67	13-18-19 (37)	3.5	2.9	14.8	-				
.6		SS 23	67	13-20-26 (46)	3.5	2.9	14.3	-				
		6	gray CLAY (A-6) very stiff, moist (continued)	gray CLAY (A-6) very stiff, moist (continued) Image: style="text-align: center;">Image: style="text-align: style="text-align: center;">Image: sty	gray CLAY (A-6) very stiff, moist (continued) Image: stiflet in the stiflet in t	gray CLAY (A-6) very stiff, moist (continued) Image: Continued of the second secon	gray CLAY (A-6) very stiff, moist (continued) Image: Continued (Continued) Image: Continued (Continued) Image: Continue (Continued) Image: Continue (Continued) Image: Continue (Continued) Image: Continue (Continue (Continut	gray CLAY (A-6) very stiff, moist (continued) SS 78 5-10-11 2.25 2.0 14.7 SS 20 78 5-10-11 2.25 2.0 14.7 SS 21 67 10-16-20 2.5 2.2 14.2 SS 21 67 10-16-20 2.5 2.2 14.2 SS 22 67 13-18-19 3.5 2.9 14.8 SS 26 7 13-20-26 3.5 2.9 14.3	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	gray CLAV (A-6) very stiff, moist (continued) Image: Signature of the second secon	$\begin{array}{ c c c c c c c } \hline & & & & & & & & & & & & & & & & & & $	$\begin{array}{ c c c c c c } \hline & & & & & & & & & & & & & & & & & & $



ATTERBERG LIMITS RESULTS

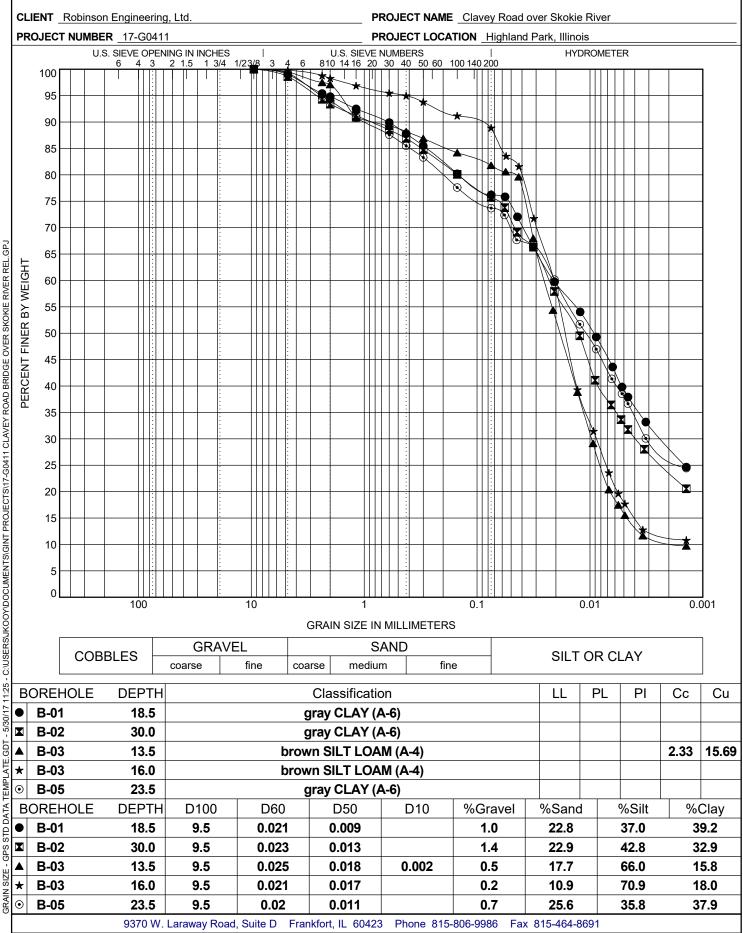
PRINT DATE _5/30/2017





GRAIN SIZE DISTRIBUTION

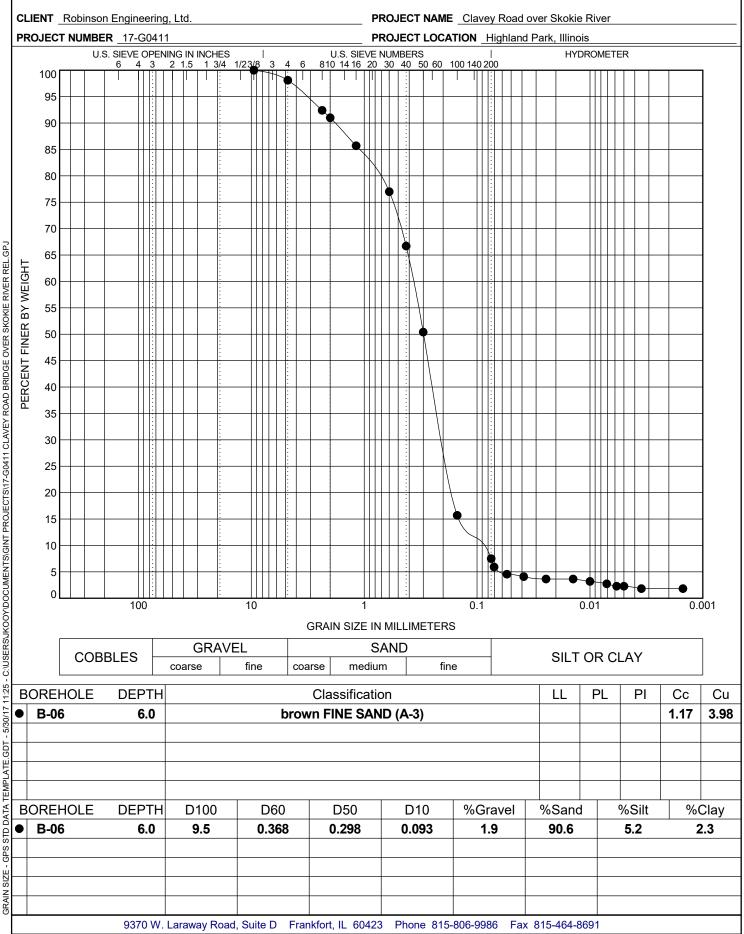
PRINT DATE _ 5/30/2017





GRAIN SIZE DISTRIBUTION

PRINT DATE _ 5/30/2017



UNCONFINED COMPRESSION TEST

PRINT DATE 5/30/2017



CLIENT _Robinson Engineering, Ltd. PROJECT NAME _Clavey Road over Skokie River PROJECT NUMBER 17-G0411 PROJECT LOCATION Highland Park, Illinois 6,500 6,000 5,500 5,000 4,500 4,000 STRESS, psf 3,500 3,000 2,500 2,000 ø 1,500 1,000 XX 500 4 8 12 16 20

STRAIN, %

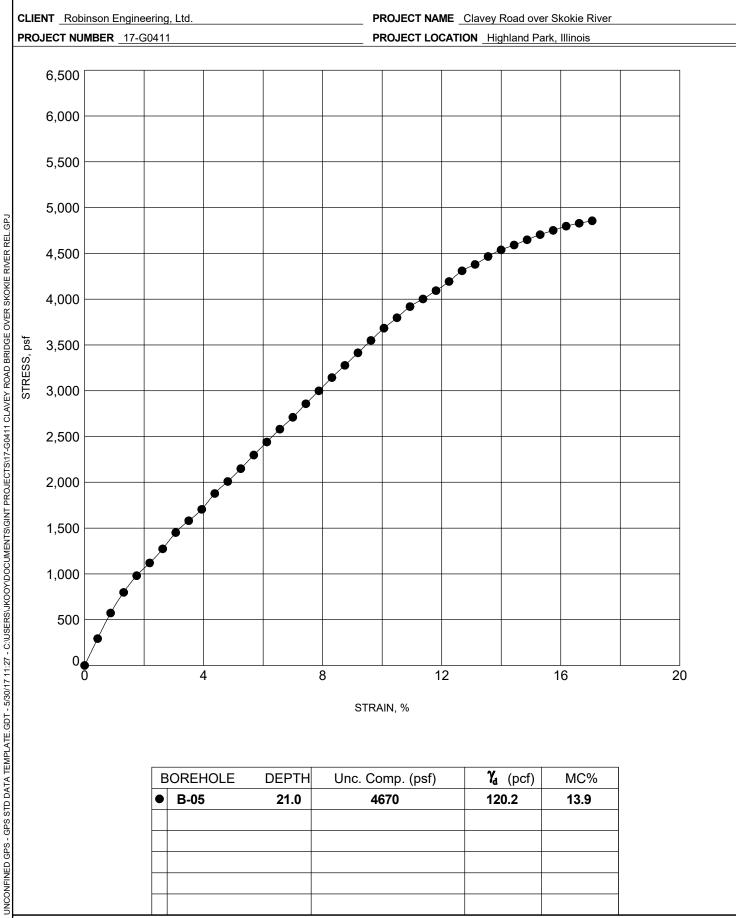
E	OREHOLE	DEPTH	Unc. Comp. (psf)	γ _d (pcf)	MC%
ullet	B-01	11.0	860	102.0	26.8
	B-01	23.0	670	118.4	18.4
	B-02	28.0	4830	116.1	17.4
*	B-04	8.0	970	91.5	31.4
۲	B-04	11.5	310	94.2	36.1
٥	B-05	13.0	6480	251.1	19.2
70 W	Laraway Road S	uite D Frankf	fort II 60423 Phone 815-80	6-9986 Fax 81	5-464-8691

UNCONFINED GPS - GPS STD DATA TEMPLATE.GDT - 5/30/17 11:27 - C:/USERS/JKOOY/DOCUMENTS/GINT PROJECTS/17-60411 CLAVEY ROAD BRIDGE OVER SKOKIE RIVER REL.GPJ

9370

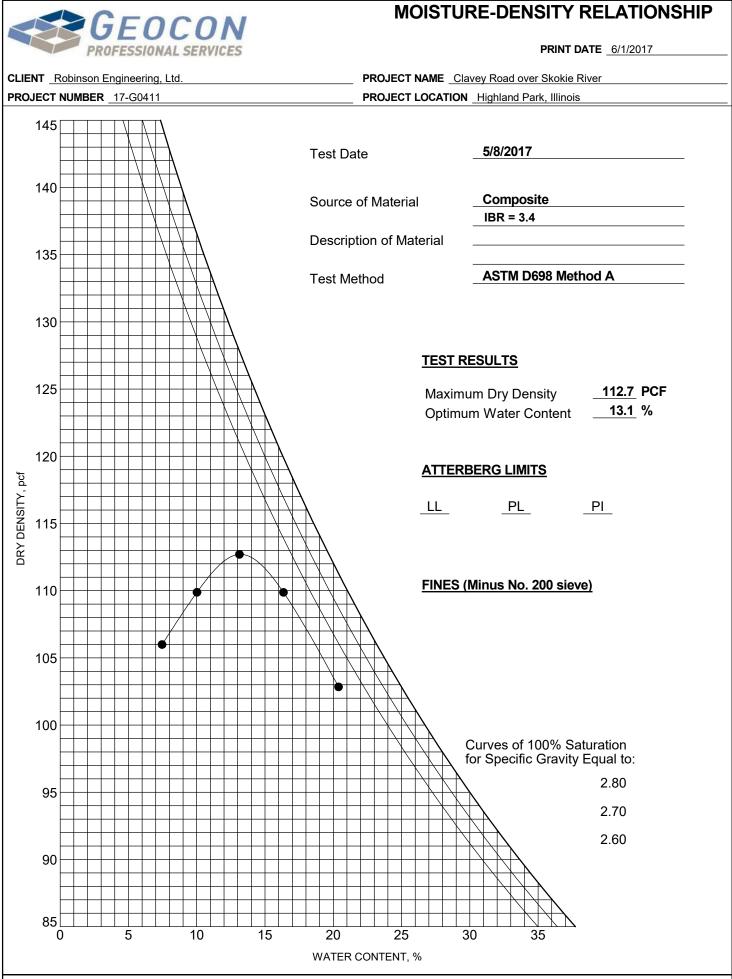
UNCONFINED COMPRESSION TEST

PRINT DATE 5/30/2017



GEOCON PROFESSIONAL SERVICES

9370 W. Laraway Road, Suite D Frankfort, IL 60423 Phone 815-806-9986 Fax 815-464-8691





PROJECT TITLE==== 17-G0411 Clavey Road Bridge over Skokie River Substructure 4 Substructure 1 Substructure 2 Substructure 3 Base of Substruct. Elev. (or ground surf for bents 622 ft Base of Substruct. Elev. (or ground surf for bents 622 ft. Base of Substruct. Elev. (or ground surf for bents) Base of Substruct. Elev. (or ground surf for bents Pile or Shaft Dia. 14 inches Pile or Shaft Dia. 14 inches Pile or Shaft Dia. inches Pile or Shaft Dia. inches Boring Number Boring Number Boring Number Boring Number Top of Boring Elev 637.4 ft Top of Boring Elev Top of Boring Elev Top of Boring Elev Approximate Fixity Elev. Approximate Fixity Elev. Approximate Fixity Elev. Approximate Fixity Elev. 615 ft. 615 ft. ft. ft Individual Site Class Definition: Individual Site Class Definition: Individual Site Class Definition: Individual Site Class Definition: N (bar): N (bar): 23 (Blows/ft.) Soil Site Class D N_{ch} (bar): NA (Blows/ft.) NA N (bar): 22 (Blows/ft.) Soil Site Class D (Blows/ft.) NA (Blows/ft.) NA N (bar): N (bar): N_{ch} (bar): (Blows/ft.) NA N_{ch} (bar): (Blows/ft.) NA N_{ch} (bar): (Blows/ft.) NA s_u (bar): 2.53 (ksf) Soil Site Class C <----Controls s_u (bar): 2.54 (ksf) Soil Site Class C <----Controls s_u (bar): (ksf) NA s_u (bar): (ksf) NA Seismic Bot. Of Layer Seismic Bot. Of Layer Seismic Bot. Of Layer Seismic Bot. Of Layer Soil Column Sample Description Soil Column Sample Sample Description Soil Column Sample Sample Description Soil Column Sample Sample Description Sample Depth Elevation Thick. N Qu Boundary (ft.) (tsf) (ft) (ft.) (tsf) (ft) (ft.) (tsf) (ft.) (tsf) (ft) (ft) 634. 3.0 632.4 2.5 35 632. 3.0 в 629.4 3.0 630. В 26 R 627.4 2.0 В 626. 4.00 В 624. 2.50 625. 1.00 В 622 622 2.5 3.0 B B 619.4 3.0 620. 2.5 B 616.9 2.5 617. 2.5 614.4 615. 40 0.0 24 2.00 2.50 3.40 2.6 0.3 В 612 612. 2 3.6 611.4 1.0 в 4. 610. 2.50 3.1 6.1 608. 2.50 12 7. 607 2.50 2.4 9.9 9.1 605. 3.00 605 12 17 23 12.1 14.9 602. 3.0 600. 5.0 15.1 599. 19. 595. 3.0 5.0 5.0 5.0 20. 594 17 24.9 590. 20 25.1 5.0 29.9 585. 589 5.0 17 30. 584. 5.0 34. 580 5.00 2 35. 39.9 579. 5.0 575. 5.00 40.1 574.9 44.9 570 5.0 5.0 45.1 569. 49.9 565. 5.0 50. 564. 54.9 560 5.0 45 10 55. 559. 20 100.0 515 20 5.00 60. 554. 65. 549. 5.00 44 4.5 70.1 544. 5.00 4.0 75.1 539. 5.0 100.0 515.0 24.9

Global Site Class Definition: Substructures 1 through 2

 N (bar):
 23 (Blows/ft.)
 Soil Site Class D

 N_{ch} (bar):
 (Blows/ft.)
 NA, H < 0.1*H (Total)</td>

 s_u (bar):
 2.54 (ksf)
 Soil Site Class C <---Controls</td>

Pile Design Table for West Abutement utilizing Boring #1

		le loi west								_	
ſ	Nominal	Factored	Estimated		Nominal	Factored	Estimated		Nominal	Factored	Estimated
	Required	Resistance	Pile		Required	Resistance	Pile		Required	Resistance	Pile
	Bearing	Available	Length		Bearing	Available	Length		Bearing	Available	Length
	(Kips)	(Kips)	(Ft.)		(Kips)	(Kips)	(Ft.)		(Kips)	(Kips)	(Ft.)
Metal S		w/.25" walls		Steel	HP 10 X 42	(<u></u>	Steel I	IP 12 X 84	(0.17
inclui O	178	31	37	01001	156	42	42		161	34	37
	218	53	42		182	56	47		204	58	42
	256	74	47		193	62	52		235	75	47
	282	88	52		206	70	57		245	80	52
	303	100	57		224	80	62		259	88	57
	328	113	62		244	91	67		283	102	62
	356	129	67		268	104	72		309	116	67
	389	147	72		321	133	82		341	133	72
Metal S		w/.25" walls		Steel	HP 10 X 57				413	173	82
notal o	211	38	37		160	43	42		449	192	87
	260	65	42		186	58	47		487	214	92
										214	92
	304	89	47		197	64	52	Steel	HP 14 X 73		
	332	104	52		210	71	57		189	42	37
	356	118	57		229	81	62		242	71	42
	385	134	62		250	93	67		276	90	47
	419	152	67		274	106	72	1	284	94	52
	458	174	72	1	328	136	82		300	103	57
Metal S		w/.312" wal		1	354	150	87		329	119	62
	211	38	37	1	382	165	92		360	135	67
	260	65	42	Stool	HP 12 X 53	100	52		397	156	72
			~~ =>.	Steel			07				
	304	89	47		155	33	37		485	204	82
	332	104	52		196	55	42		530	229	87
	356	118	57		226	71	47	Steel I	HP 14 X 89		
	385	134	62		236	77	52		192	42	37
	419	152	67		250	85	57		245	72	42
	458	174	72		273	98	62		280	91	47
Metal S	hell 16"Φ	w/.312" wal	ls		298	112	67		288	95	52
	245	46	37		328	128	72		304	104	57
	303	77	42		397	166	82		333	120	62
				Stool	HP 12 X 63	100	02				
	354	105	47	Steel					364	137	67
	382	121	52		156	33	37	1	401	158	72
	409	136	57		198	56	42	1	491	207	82
	443	155	62		228	72	47	1	538	233	87
	482	176	67		238	78	52	1	587	260	92
	528	201	72		253	86	57	Steel I	HP 14 X 10	2	
Metal S	hell 16"Φ	w/.375" wal	ls		276	99	62	1	194	43	37
	245	46	37		301	113	67	1	248	73	42
	303	77	42		331	129	72	1	284	92	47
	354	105	42		401	168	82		204	96	52
									307		
	382	121	52		435	186	87	1		105	57
	409	136	57		472	207	92	1	337	122	62
	443	155	62	Steel	HP 12 X 74			1	368	139	67
	482	176	67		159	34	37	1	406	160	72
	528	201	72		201	57	42	1	497	210	82
Steel H	P 8 X 36				231	73	47		545	236	87
	144	43	47		241	79	52		595	264	92
	155	50	52		256	87	57	Steel I	HP 14 X 11		
	166	56	57		280	100	62		197	44	37
			62		305	114	67	1	252	74	42
	181	64									
	197	72	67		336	131	72		287	94	47
	216	83	72		407	170	82	1	294	98	52
	255	105	77		442	189	87	1	311	107	57
	255	105	82		480	210	92		341	123	62
	273	114	87						372	140	67
									411	162	72
									504	213	82
								1	552	239	87
				1				-	603	267	92
								Preca	226 st 14"x 14"	25	32

Pile Design Table for East Abutment utilizing Boring #2

					у Болид #4						
	Nominal	Factored	Estimated		Nominal	Factored	Estimated		Nominal	Factored	Estimate
	Required	Resistance	Pile		Required	Resistance	Pile		Required	Resistance	Pile
	Bearing	Available	Length		Bearing	Available	Length		Bearing	Available	Length
	(Kips)	(Kips)	(Ft.)	-	(Kips)	(Kips)	(Ft.)		(Kips)	(Kips)	(Ft.)
Metal S	Shell 12"Ф	w/.25" walls		Steel I	HP 10 X 42			Steel H	IP 12 X 84		
	238	43	37	1	175	45	42	1	204	48	37
	269	60	42		200	58	47		224	59	42
	303	79	47	1	217	68	52	1	256	77	47
	332	95	52	1	236	78	57	1	275	87	52
	360	110	57	1	257	90	62	1	299	100	57
	391	127	62	1	284	105	67	1	326	115	62
Metal S		w/.25" walls			309	118	72		361	135	67
	239	29	32	Steel I	HP 10 X 57			1	392	152	72
	283	53	37		179	46	42	Steel H	IP 14 X 73		
	317	72	42		204	60	47		202	37	32
	358	94	47		221	69	52	1	241	59	37
	390	112	52		241	80	57		263	71	42
	424	131	57		263	92	62		200	91	42
Motal		w/.312" wal			290	107	67		320	103	52
metal	239	29	32		315	107	72	1	320	103	52 57
	239	29 53	32	Stool	HP 12 X 53	121	12				
				Steern		40	07		379	135	62
	317	72	42		196	46	37		421	158	67
	358	94	47	1	216	57	42		457	178	72
	390	112	52		246	73	47	Steel	IP 14 X 89		
	424	131	57		265	84	52		204	38	32
	459	150	62		288	97	57		244	60	37
	503	174	67		314	111	62	1	266	72	42
	546	198	72		348	130	67	1	303	92	47
Metal S		w/.312" wal			378	146	72	1	324	104	52
	278	36	32	Steel I	HP 12 X 63			1	352	119	57
	329	64	37		198	46	37		383	137	62
	367	85	42		218	57	42		427	160	67
	414	111	47		248	74	47	1	462	180	72
	450	130	52		268	85	52	Steel H	IP 14 X 102	2	
	488	151	57		291	98	57	1	207	39	32
	529	174	62		317	112	62		247	61	37
	580	202	67		352	131	67		269	73	42
	629	229	72		381	147	72	1	307	94	47
Metal S	Shell 16"Φ	w/.375" wal	s	Steel I	HP 12 X 74				328	105	52
	278	36	32		201	47	37	1	356	121	57
	329	64	37		221	58	42		388	138	62
	367	85	42		252	75	47		432	162	67
	414	111	47		271	86	52	1	467	182	72
	450	130	52		295	99	57	Steel H	IP 14 X 117		•=
	488	151	57		321	113	62		210	40	32
	529	174	62		357	133	67	1	251	62	37
	580	202	67		387	149	72		272	74	42
	629	229	72		007	140	12	1	311	95	47
Stool L	IP 8 X 36	223	12					1	332	95 107	52
oleer r	159	46	47					1	360	107	52
								1			
	174	54	52 57					1	392	140	62
	190	62	57					1	437	164	67
	207	72	62						473	184	72
	228	83	67					Precas	st 14"x 14"		
	248	94	72	1			I	1	257	19	27