

Original Report Date: 3/2/2018 Proposed SN: 050-0261 Route: CH 9
 Revised Date: 4/2/2019 Existing SN: 050-0081 Section: (50-3)HBR-3
 Geotechnical Engineer: Adam Bohnhoff, Civil Design Inc. County: LaSalle
 Structural Engineer: Jim Clinard, Chamlin & Associates Inc. Contract: 66C59

Indicate the proposed structure type, substructure types, and foundation locations (attach plan and elevation drawing): The proposed two span structure carries CH 9 over I-80 and will be a reinforced concrete deck on steel plate girders with integral abutments. The abutments will be support by steel H pile driven to refusal. The pier will be supported by a spread footing. A preliminary TSL drawing is attached.

Discuss the existing boring data, existing plans foundation information, new subsurface exploration and need for any additional exploration to be provided with SGR Technical Memo (attach all data and subsurface profile plot): The existing plans indicate abutments are supported on concrete piles and the 3 piers are supported on creosote pile supported spread footings. The original 1961 logs included soil borings at both abutments and all 3 piers. In 2011, a soil boring was taken near each abutment. In 2016, a soil boring was taken at the proposed pier location. Copies of these logs are attached.

Provide the location and maximum height of any new soil fill or magnitude of footing bearing pressure. Estimate the amount and time of the expected settlement. Indicate if further testing, analysis, and/or ground improvement/treatment is necessary: The profile of CH 9 will be increased by approximately 4 feet. The soils within the existing embankments have strengths exceeding 3 tsf and moisture contents around 25% or less. Minimal settlement is anticipated under the existing embankments. No additional testing or treatment for settlement is necessary.

Identify any new cuts or fill slope angles and heights. Estimate the factor of safety against slope failure. Indicate if further testing, analysis or ground improvement/treatment is necessary: The proposed CH 9 alignment is shifted to the east. The existing embankment will be widened to accommodate. Side and end slopes will be 2:1. Due to the cohesive soil strengths in the existing embankment and below, long term drained conditions control over short term undrained conditions. The SF against slope failure is 1.5 at the abutment cross sections and 1.7 for the end slopes using the Bishop Method with long term drained conditions. Note the toe of the slope at the existing building on the southwest side of the bridge is not considered critical for slope stability. No additional analysis or treatment is required.

Indicate at each substructure, the 100-year and 200-year total scour depths in the Hydraulics report, the non-granular scour depth reduction, the proposed ground surface, and the recommended foundation design scour elevations: Scour is not applicable because this is a grade separation structure.

Determining the seismic soil site class, the seismic performance zone, the 0.2 and 1.0 second design spectral accelerations and indicate if that the soils are liquefiable: The seismic data is as follows: Seismic Soil Site Class = C; Seismic Performance Zone = SPZ 1; Design Spectral Acceleration at 0.2 sec. (SDS) = 0.124; Design Spectral Acceleration at 1.0 sec. (SD1) = 0.070. Liquefaction is not applicable because the SPZ = 1.

Confirm feasibility of the proposed foundation or wall type and provide design parameters. Attach a pile design table indicating feasible pile types, various nominal required bearings, factored resistances available and corresponding estimated lengths at locations where piles will be used. Provide factored bearing resistance and unit sliding resistance at various elevations and confirm no ground improvement/treatment is necessary where spread footings are proposed. Estimated top of rock elevations as well as preliminary factored unit side and tip resistance values shall be indicated when drilled shafts are proposed: See the attached supplemental information.

Calculate the estimated water surface elevation and determine the need for cofferdams (type 1 or 2), and seal coat: Water surface elevations and cofferdams/seal coat are not applicable because this is a grade separation structure.

Assess the need for sheeting or soil retention or temporary construction slope and provide recommendation for other construction concerns: Temporary sheet piling will not be needed to construct the abutments because the structure will closed to all traffic during construction. Constructing the footing at the pier is feasible within the median without requiring braced excavation.

Bench Mark: "0" - Chiseled square on S.E. concrete curb of bridge S.N. 050-0081. Elev. 653.755

Existing Structure: SN 050-0081 (Sec 50-3HB-1) was constructed in 1961 as a four-span continuous steel I-beam structure with concrete piers on pile supported spread footings. The structure measures 224'-6" back to back of abutments and 29'-8" out to out of deck with 24'-0" clear width between the curbs. The deck was constructed as a 6 1/2" concrete deck. Structure to be removed and replaced. No salvage. Traffic is to be detoured.

Bridge Omission (Sta. 13+80.83 to Sta. 16+04.16)

DESIGN SPECIFICATIONS

2017 AASHTO LRFD Bridge Design Specifications

HIGHWAY CLASSIFICATION

F.A.I. Rte. 80 - I-80.	C.H. 9 - County Highway 9
Functional Class: Interstate	Functional Class: Major Collector
ADT: 33,384 (2020); 39,804 (2040)	ADT: 468 (2020); 558 (2040)
ADTT: 14,767 (2040)	ADTT: 25(2040)
DHV: 3980	DHV: 56
Design Speed: 70 m.p.h.	Design Speed: 55 m.p.h.
Posted Speed: 70 m.p.h.	Posted Speed: 55 m.p.h.

LOADING HL-93

Allow 50#/sq. ft. for future wearing surface.

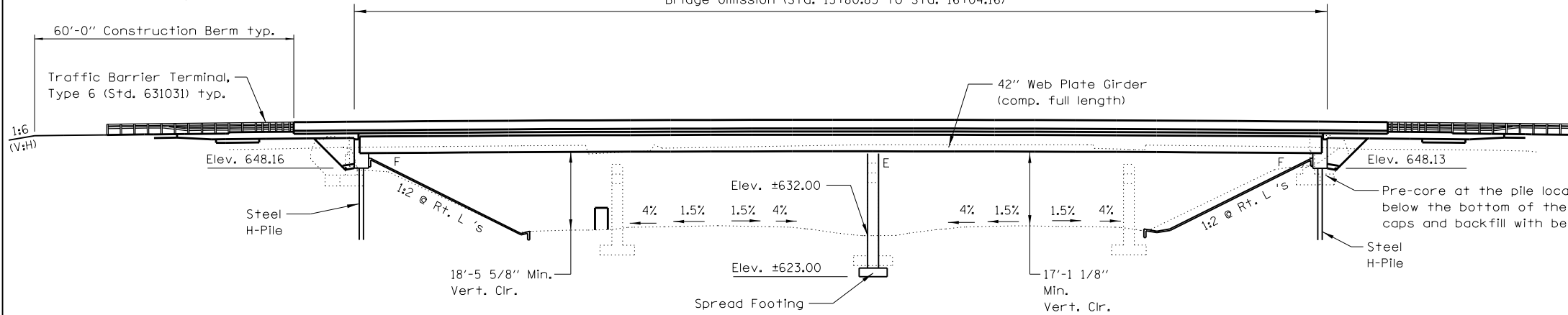
SEISMIC DATA

Seismic Performance Zone (SPZ) = 1
 Design Spectral Acceleration at 1.0 sec. (SD1) = 0.070
 Design Spectral Acceleration at 0.2 sec. (SDS) = 0.124
 Soil Site Class = C

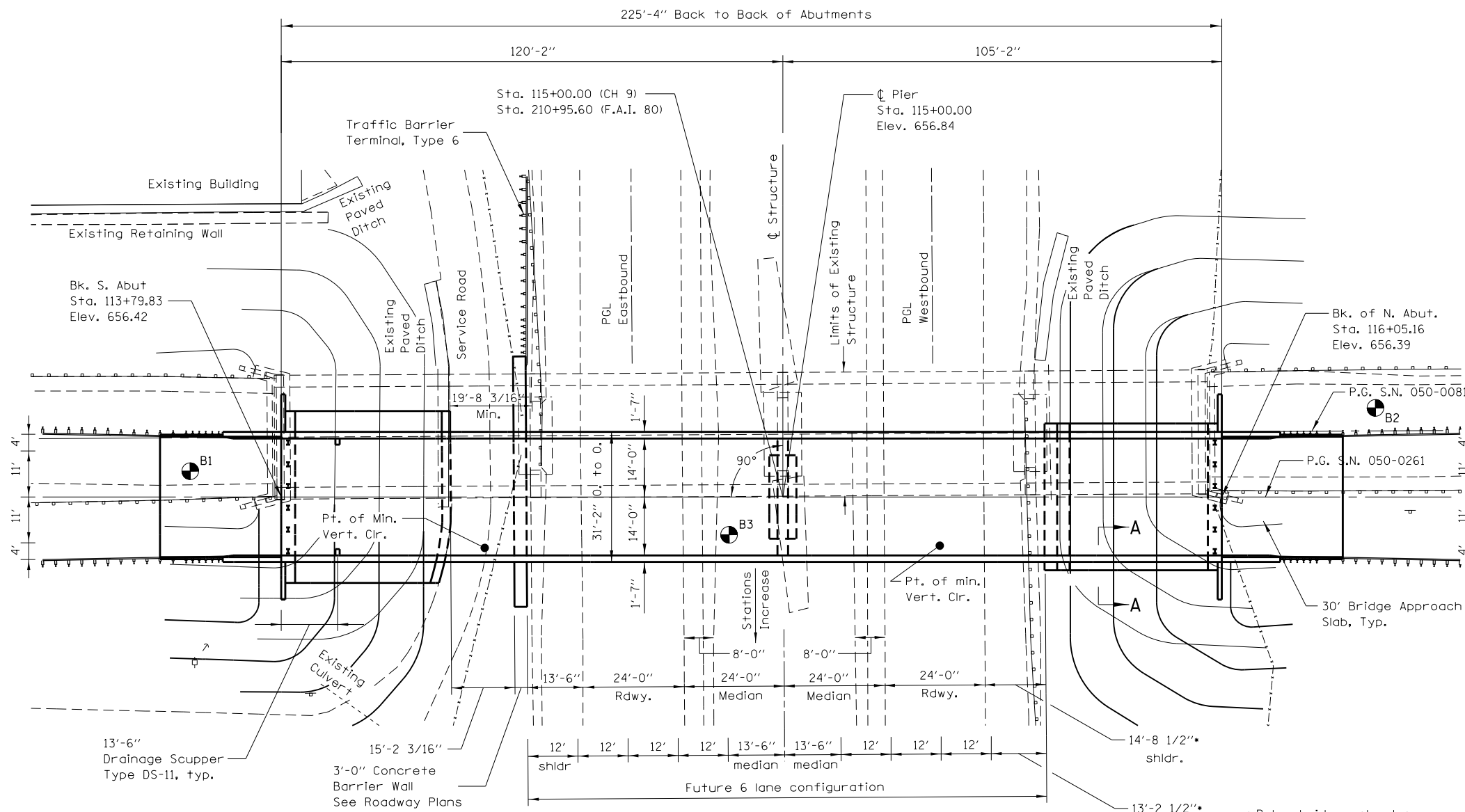
DESIGN STRESSES

FIELD UNITS

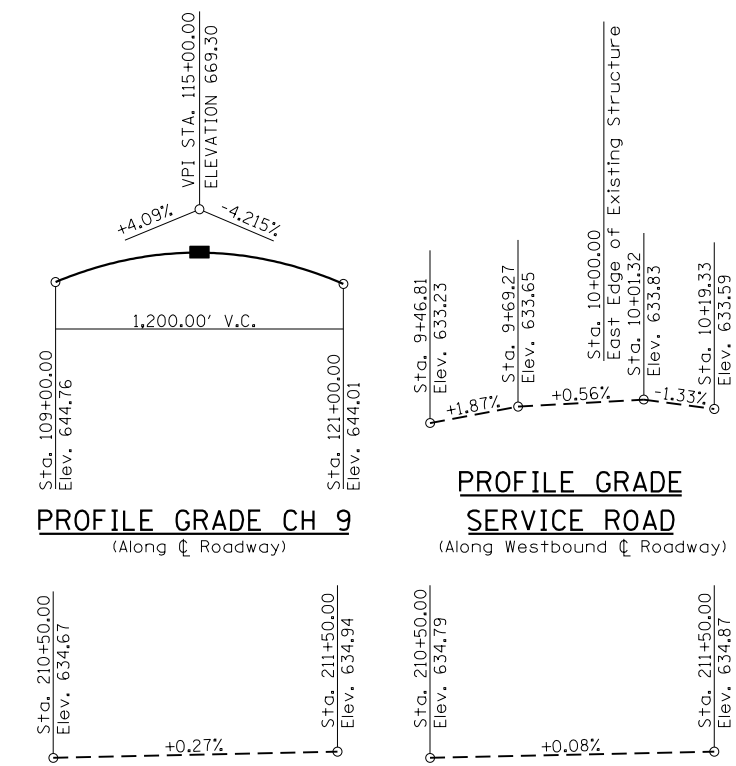
f'c = 3,500 psi
 f'c = 4,000 psi (Superstructure Concrete)
 fy = 60,000 psi (Reinforcement)
 fy = 50,000 psi (M270 Grade 50)



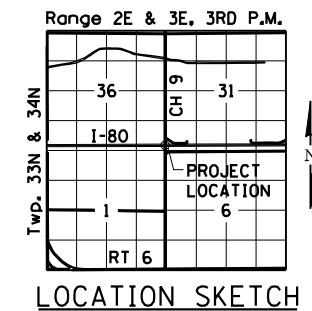
ELEVATION



PLAN



PROFILE GRADE CH 9 (Along Centerline Roadway)
 PROFILE GRADE SERVICE ROAD (Along Westbound Centerline Roadway)
 PROFILE GRADE I-80 (Along Eastbound Centerline Roadway)
 PROFILE GRADE I-80 (Along Westbound Centerline Roadway)



LOCATION SKETCH

GENERAL PLAN & ELEVATION
CH 9 OVER I-80
F.A.I. RTE. 80 (I-80)
SECTION (50-3) HBR-3
LASALLE COUNTY
STATION 115+00
SN 050-0261 (PROP.)

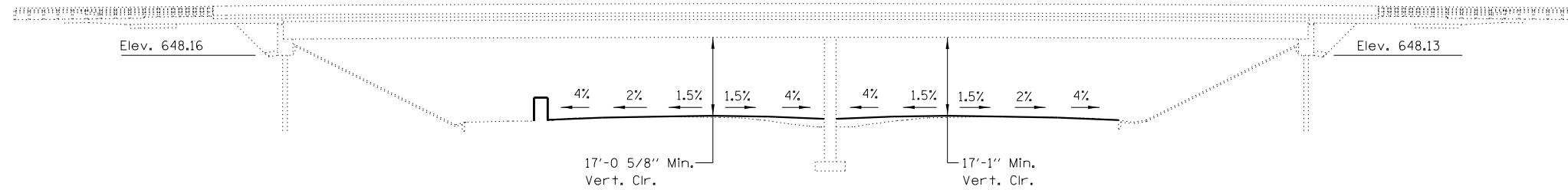
FILE NAME =
 USER NAME = --
 PLOT SCALE = 1"=32'
 PLOT DATE = 01/16/2019

DESIGNED - JKC	REVISD -
CHECKED - JKC	REVISD -
DRAWN - ARR / LAG	REVISD -
CHECKED - JKC	REVISD -

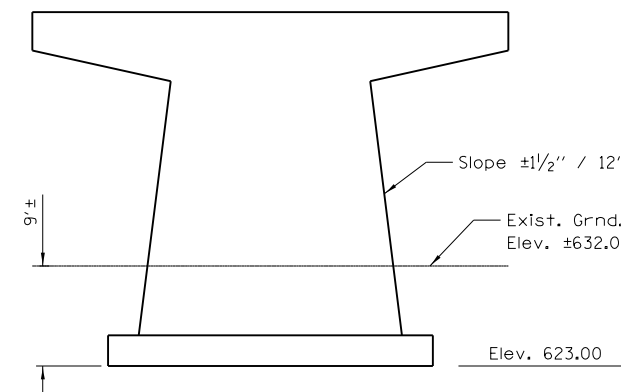
STATE OF ILLINOIS
 DEPARTMENT OF TRANSPORTATION

SHEET NO. OF SHEETS

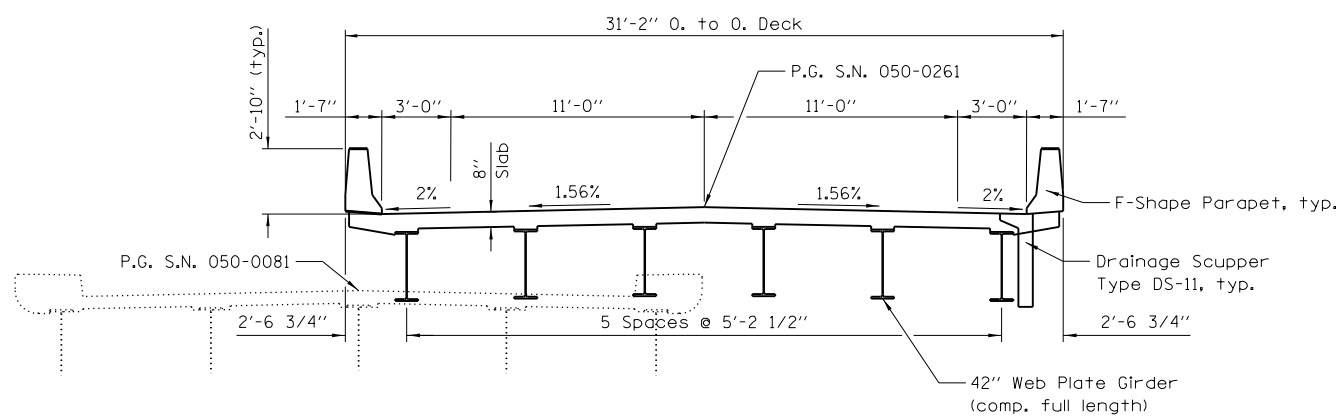
F.A. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
			2	1
CONTRACT NO. 66C59				
ILLINOIS FED. AID PROJECT				



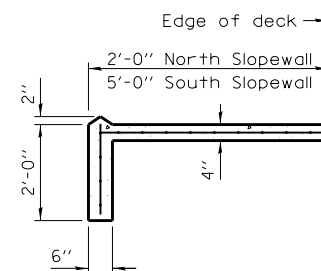
FUTURE ELEVATION
(Assumed PG Elev. 635.00)



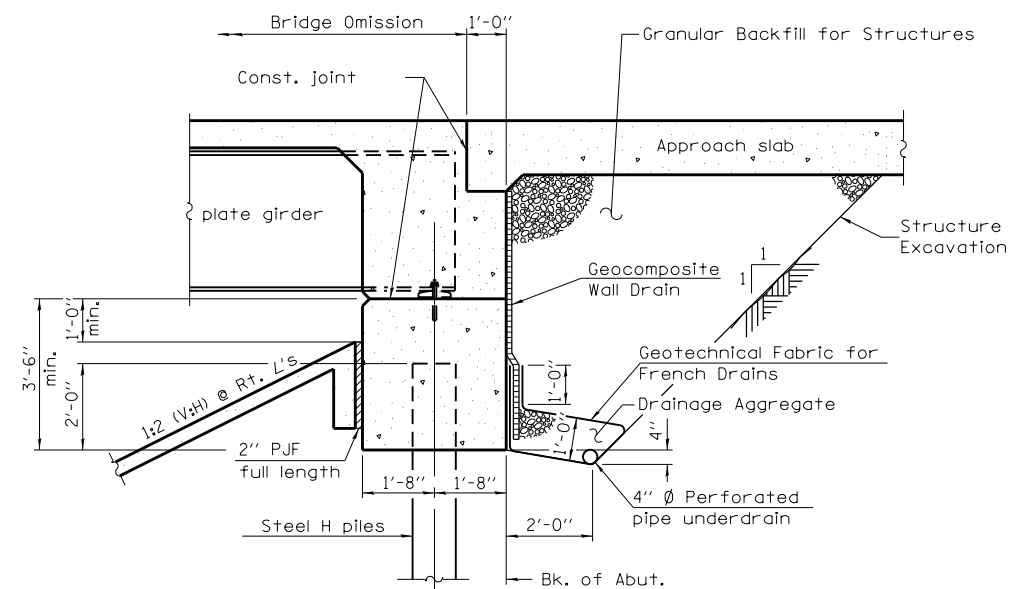
PIER SKETCH



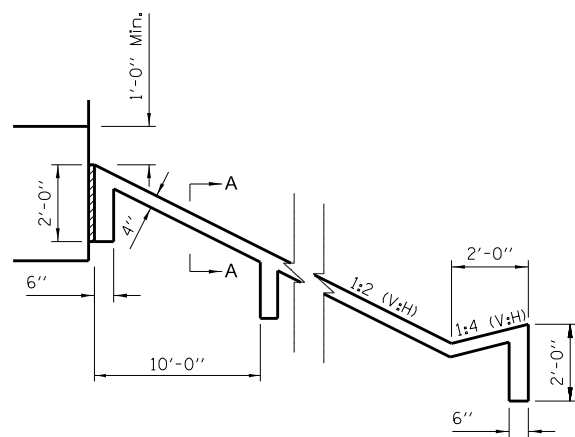
CROSS SECTION
Looking North



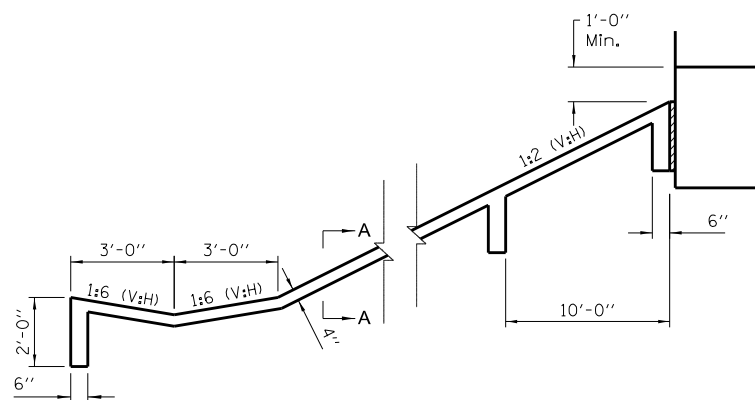
SECTION A-A



SECTION THRU INTEGRAL ABUTMENT
(Horiz. dim. @ Rt. L's)



SLOPE WALL ADJACENT TO SERVICE ROAD
(South)



SLOPE WALL ADJACENT TO I-80
(North)

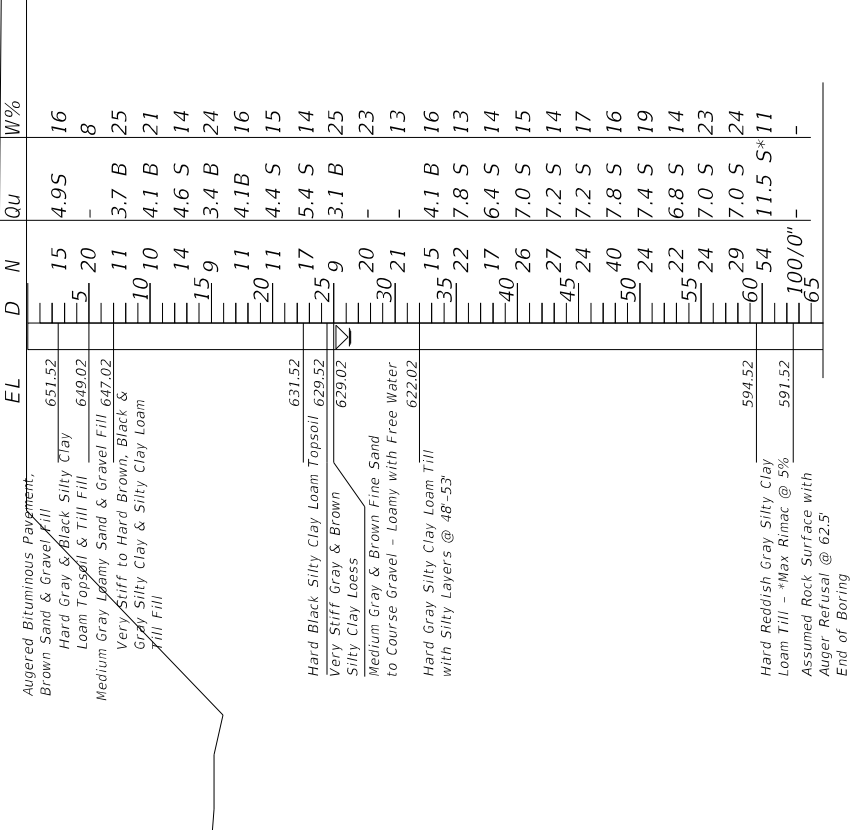
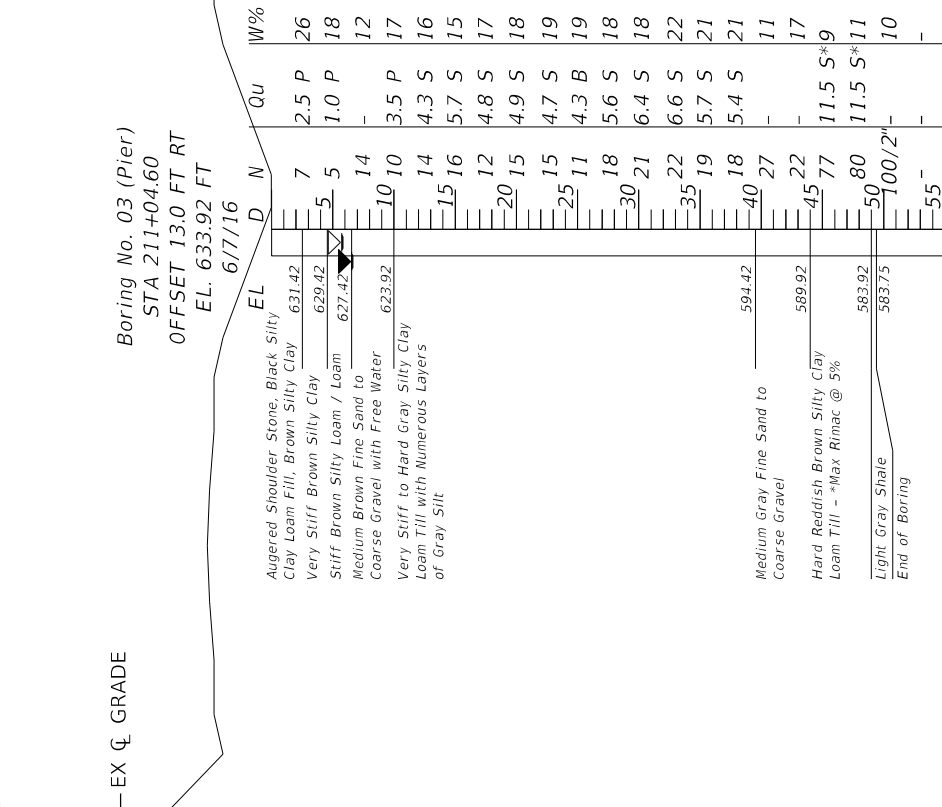
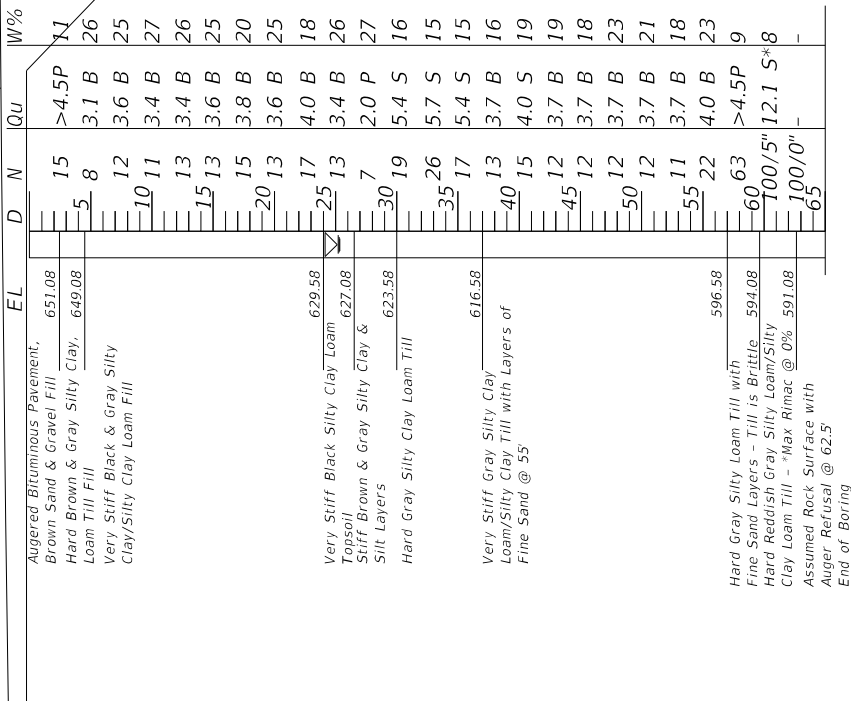
GENERAL PLAN & ELEVATION
CH 9 OVER I-80
F.A.I. RTE. 80 (I-80)
SECTION (50-3) HBR-3
LASALLE COUNTY
STATION 115+00
SN 050-0261 (PROP.)

FILE NAME = 	USER NAME = --	DESIGNED - JKC	REVISED -	STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION	F.A. RTE. SECTION COUNTY TOTAL SHEETS SHEET NO. 2 2 CONTRACT NO. 66C59 ILLINOIS FED. AID PROJECT
	PLOT SCALE = 1"=32'	CHECKED - JKC	REVISED -		
	PLOT DATE = 01/16/2019	DRAWN - ARR / LAG	REVISED -		
		CHECKED - JKC	REVISED -		
SHEET NO. OF SHEETS					

Note: Boring Stationing and Offsets shown in reference to I-80 profile.

Boring No. 01 (S. Abut.)
 STA 210+88.60
 OFFSET 142.0 FT RT
 EL 653.58 FT
 6/3/11

Boring No. 02 (N. Abut.)
 STA 210+75.10
 OFFSET 142.0 FT LT
 EL 654.02 FT
 6/7/11



LEGEND

- EL = Elevation (FT)
 - D = Depth Below Existing Ground Surface (FT)
 - N = SPT N-VALUE (AASHTO T206)
 - Qu = Unconfined Compressive Strength in tons per sq. ft. (tsf)
 Failure Mode (B=bulge, S=shear, P=penetrometer)
 - W% = Moisture Content Percentage
 - ▶ = Groundwater Level First Encountered
 - ◀ = Groundwater Upon Completion
 - ▽ = Groundwater After 24 to 72 hours
- Soil profile is or illustrative purposes only. Actual conditions will vary.

SUBSURFACE DATA PROFILE
 CH 9 OVER I-80
 F.A.I. RTE. 80 (I-80)
 SECTION (50-3) HBR-3
 LASALLE COUNTY
 STATION 115+00
 SN 050-0261 (PROP.)



SOIL BORING LOG

ROUTE I-80 (FAI 80) DESCRIPTION County Highway 9-D over FAI 80 (Sta 210+80.6) LOGGED BY Gehler

SECTION 50-3HB-1 LOCATION SW 1/4, SEC. 31, TWP. 34N, RNG. 3E, 3rd PM,
Latitude , Longitude

COUNTY LaSalle DRILLING METHOD Hollow Stem Auger HAMMER TYPE _____

STRUCT. NO.	Station	DEPTH (ft)	BLOW S (1/6")	UCS (tsf)	MOIST (%)	Surface Water Elev. (ft)	Stream Bed Elev. (ft)	GROUNDWATER ELEV. (ft)	DEPTH (ft)	BLOW S (1/6")	UCS (tsf)	MOIST (%)	
050-0081	210+80.6												
BORING NO. 1 (Pier #2)	Station 15+00												
Offset 15.0 ft Lt.													
Ground Surface Elev. 632.97													
Very Stiff Brownish Black Silty Clay													
			15	2.9 S						16	4.4 B	18	
	629.47												
Stiff Yellowish Brown Silty Clay													
	627.97	-5	7	1.7 S					-25	16	4.1 B	19	
Loose Yellowish Brown Sandy Loam													
	626.97												
Medium Yellowish Brown Coarse Rounded Sand to Coarse Rounded Gravel													
	624.47		14							27	5.5 B	18	
Hard Brown Clay (Till)													
	621.97	-10	14	4.3 B					602.97	-30	37	6.2 B	17
Hard Gray Clay (Till)													
			24	6.2 S					600.97		24	3.9 S	18
									599.47				
		-15	22	8.3 B						-35	28	3.1 S	24
			21	5.4 S							27	4.3 B	21
									594.47				
		-20	18	4.3					592.97	-40	54	6.3	9

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



SOIL BORING LOG

ROUTE I-80 (FAI 80) DESCRIPTION County Highway 9-D over FAI 80 (Sta 210+80.6) LOGGED BY Gehler

SECTION 50-3HB-1 LOCATION SW 1/4, SEC. 31, TWP. 34N, RNG. 3E, 3rd PM,
 Latitude , Longitude

COUNTY LaSalle DRILLING METHOD Hollow Stem Auger HAMMER TYPE _____

STRUCT. NO. <u>050-0081</u>	D E P T H H	B L O W S	U C S Qu	M O I S T	Surface Water Elev. _____ ft
Station <u>210+80.6</u>					Stream Bed Elev. _____ ft
BORING NO. <u>1 (Pier #2)</u>	ft (ft)	(/6")	(tsf)	(%)	Groundwater Elev.: _____
Station <u>15+00</u>					First Encounter _____ ft
Offset <u>15.0 ft Lt.</u>					Upon Completion <u>625.0</u> ft ▽
Ground Surface Elev. <u>632.97</u> ft					After <u>24</u> Hrs. <u>625.5</u> ft ▽

Soil Description	Depth (ft)	Blow Count (/6")	UCS (tsf)	Moisture (%)	Notes
Hard Gray Clay (Till)	591.97		B		
Hard Gray Clay Loam (Till)	589.97	175	9.7	9	
End of Boring					
	-45				
	-50				
	-55				
	-60				

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
 The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



SOIL BORING LOG

ROUTE I-80 (FAI 80) DESCRIPTION FAS 174 (CH 9) over I-80, 4 miles East of IL 178 LOGGED BY Larry Myers

SECTION 50-3HB-1 LOCATION SE 1/4, SEC. 36, TWP. 34N, RNG. 2E, 3rd PM,
Latitude , Longitude

COUNTY LaSalle DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME Automatic

STRUCT. NO.	Station	BORING NO.	Station	Offset	Ground Surface Elev.	D E P T H ft	B L O W S (ft)	U C S (/6")	M O I S T (tsf)	M O I S T (%)	Surface Water Elev.	Stream Bed Elev.	Groundwater Elev.:	First Encounter	Upon Completion	After	Hrs.	D E P T H ft	B L O W S (ft)	U C S (/6")	M O I S T (tsf)	M O I S T (%)	
050-0081 (Exist.)	210+80.6	02 (N. Abut.)	210+75.1	142.0 ft Lt.	654.02										628.0								
Augered Bituminous Pavement, Brown Sand & Gravel Fill						651.52																	
Hard Gray & Black Silty Clay Loam Topsoil & Till Fill							7																
Medium Gray Loamy Sand & Gravel Fill							10																
Very Stiff to Hard Brown, Black & Gray Silty Clay & Silty Clay Loam Till Fill							4																
							5	3.7	25														
							6	B															
						-10	4																
							3	4.1	21														
							7	B															
							3																
							6	4.6	14														
							8	S															
						-15	3																
							4	3.4	24														
							5	B															
							4																
							5	4.1	16														
							6	B															
						-20																	

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



SOIL BORING LOG

ROUTE I-80 (FAI 80) DESCRIPTION FAS 174 (CH 9) over I-80, 4 miles East of IL 178 LOGGED BY Larry Myers

SECTION 50-3HB-1 LOCATION SW 1/4, SEC. 31, TWP. 34N, RNG. 3E, 3rd PM,
Latitude 41.368118, Longitude -88.933246

COUNTY LaSalle DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME Automatic

STRUCT. NO. 050-0081 (Exist.)
Station 210+80.6

BORING NO. 03 (Pier)
Station 211+04.6
Offset 13.0 ft Rt.
Ground Surface Elev. 633.92 ft

DEPTH H S	B L O W S	U C S Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

Surface Water Elev. _____ ft
Stream Bed Elev. _____ ft

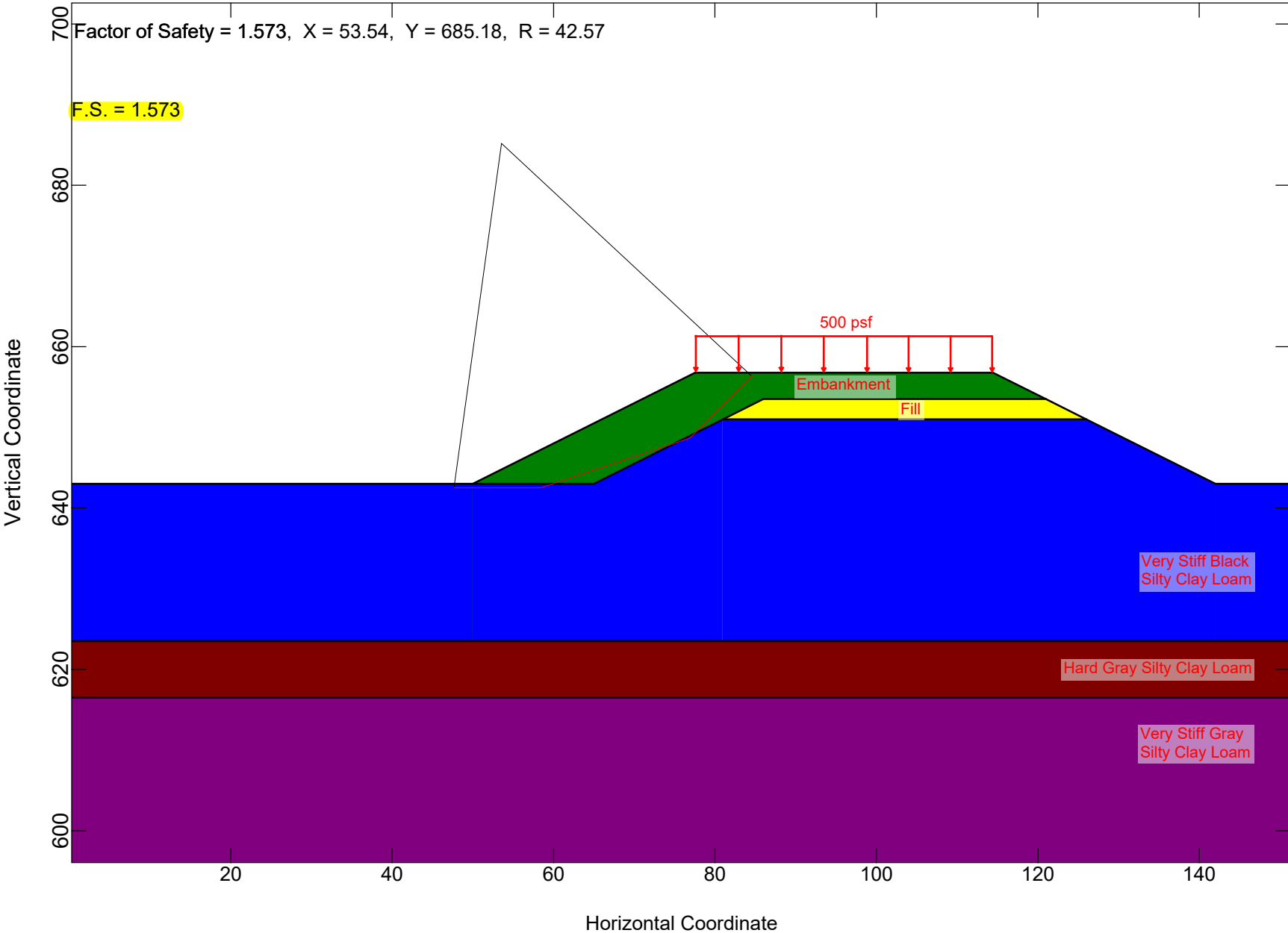
Groundwater Elev.:
First Encounter 627.4 ft ▼
Upon Completion 627.9 ft ▼
After _____ Hrs. _____ ft

Medium Gray Fine Sand to Coarse Gravel (<i>continued</i>)	7		
	12		11
	15		
589.92	8		
	10		17
	12		
Hard Reddish Brown Silty Clay Loam Till * Max Rimac @ 5%	-45		
	27		
	36	11.5	9
	41	S*	
583.92	25		
	35	11.5	11
	45	S*	
583.75	-50		
Light Gray Shale	100/2"		10
End of Boring			
	-55		
	-60		

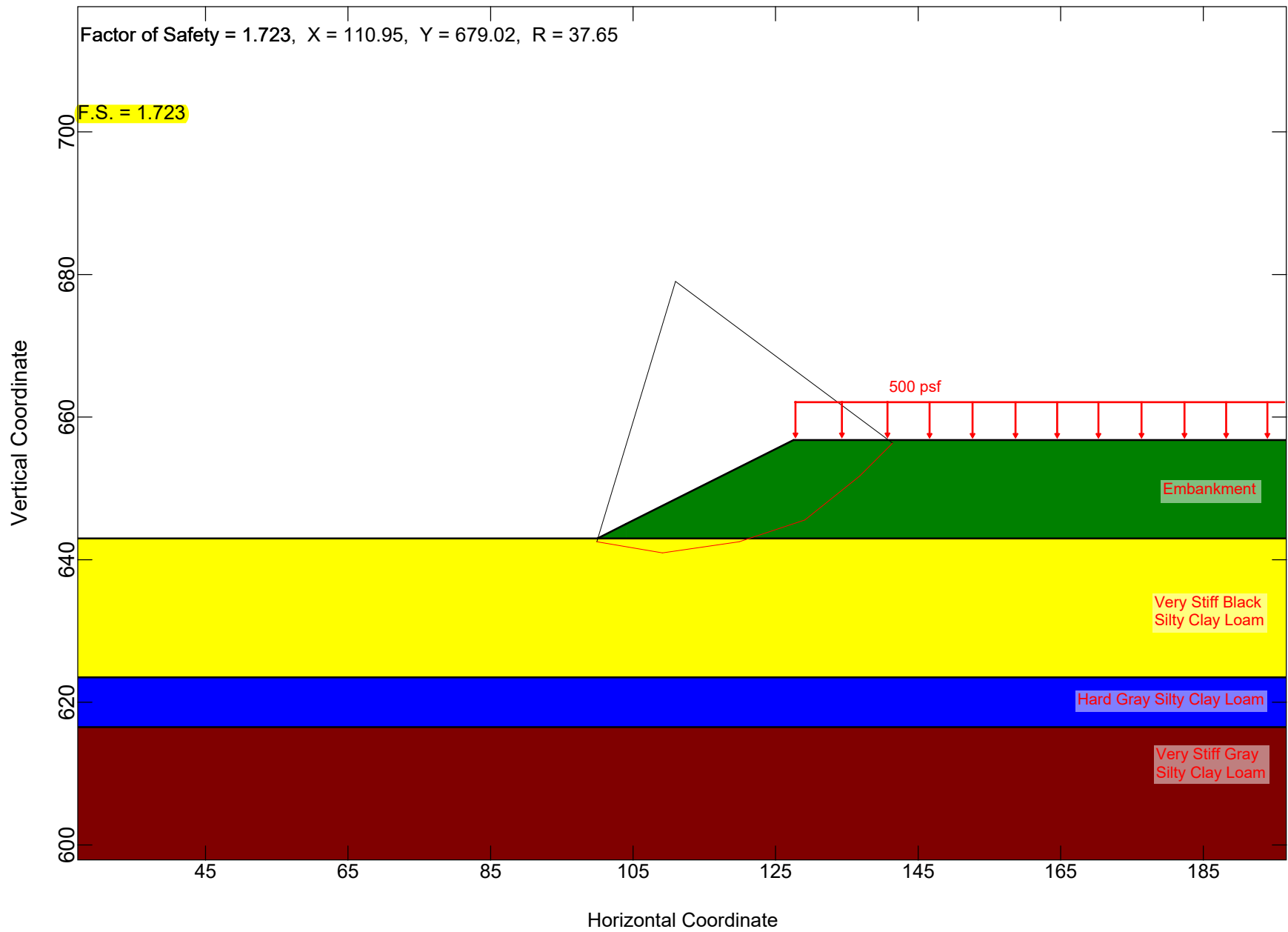
SOIL BORING 050-0081.GPJ IL_DOT.GDT 6/15/16

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

Slope Stability - CH 9 over I-80, Abutment Cross Section, Long Term Conditions



Slope Stability - CH 9 over I-80, Abutment End Slope, Long Term Conditions



Abbreviated Structure Geotechnical Report – Supplemental Information

Proposed SN 050-0261

Existing SN 050-0081

Integral Abutment Feasibility

Integral abutments are the preferred end bent type due to elimination of the joints in the bridge decks, decreasing maintenance costs and increasing service life. The proposed structure length typically fits in the range of applicability for integral abutments; however, the soil at a critical depth of 10 feet below the abutment is very stiff (Unconfined compressive strength, Q_u : 3.4 tsf – 3.9 tsf). According to the IDOT ABD Memo 12.3, the integral abutment study only pertains to soils with Q_u less than 3.0 tsf. See the attached IDOT BBS 145 spreadsheet for In Situ Integral Abutment Feasibility.

Investigating further, the IDOT Geotechnical Manual discusses pre-coring pile locations to 10 feet below the abutment and backfilling with bentonite pellets, which reduces the soil pressures on the pile during expansion. To simulate the effects of bentonite, assume $Q_u = 1.5$ tsf over the critical depth.

Also, note the proposed bridge is shifted to the east of the original alignment. Approximately half of the piles will be located over a new embankment cone. Piles embedded into existing soil 10 feet below the abutment will require pre-coring and backfilling, whereas piles embedded into new embankment will not. Per ABD Memo 12.3, an abutment constructed on new embankment shall assume $Q_u = 1.5$ tsf.

Using $Q_u=1.5$ tsf for both bentonite and embankment conditions, the results show integral abutments are applicable for all piles sizes. See attached Bentonite/Embankment Integral Abutment Feasibility spreadsheet.

Abutment Pile Discussion

Metal shell piles and HP piles are both considered for integral abutment applications. While the pile could develop sufficient capacity before reaching rock, it is likely to be less expensive to drive the piles to rock and eliminate the cost of the test pile at each abutment. For piles driven to rock surface, test piles are not needed provided the designer adds two extra feet to the estimated length of each pile as indicated in the table below. This will accommodate any changes in the driven length of the pile without requiring splices. HP piles are most effective in point bearing applications; therefore, HP piles are recommended over metal shell piles. Pile shoes are not recommended. The proposed pile locations need to be checked for conflict with the existing piling.

Substructure Unit	Pile Length	Pile Length plus Addl. 2 ft.
South Abutment	66 ft.	68 ft.
North Abutment	66 ft.	68 ft.

South Abutment - H-Pile Capacity at 66 ft Pile Length

Pile Size	Maximum Nominal Required Bearing (k)	Factored Resistance Available (k)
HP 12x74	589	324
HP 12x84	664	365
HP 14x89	705	388
HP 14x102	810	446
HP 14x117	929	511

North Abutment - H-Pile Capacity at 66 ft Pile Length

Pile Size	Maximum Nominal Required Bearing (k)	Factored Resistance Available (k)
HP 12x74	589	324
HP 12x84	664	365
HP 14x89	705	388
HP 14x102	810	446
HP 14x117	929	511

Pier Foundation Discussion

A shallow foundation (spread footing) and deep foundation (pile supported spread footing) were investigated for the proposed pier foundation type. The existing piers are founded on creosote timber pile supported spread footings; however, approximately 8 feet beneath the ground line at the proposed pier location is very stiff silty clay loam till, which is conducive to using a spread footing.

Based on a 30 foot long by 10 foot wide spread footing with bottom of footing elevation at 623.0, the factored bearing resistance is 10.1 ksf and the factored sliding resistance is 3.0 ksf. Evaluating the factored loads and factored bearing resistance, a spread footing is determined feasible. Spread footings are the preferred foundation over pile supported spread footings due to potential issues with proposed deep foundation piles avoiding the existing pier piles. Also, using a spread footing simplifies construction and eliminates the need for large pile driving equipment in the interstate median.

Due to the alignment of the bridge being shifted to the east, the proposed spread footing will be resting partially over the existing timbers piles and partially over virgin soil, causing potential differential settlement. To minimize differential settlement concerns, the limits of the excavation shall be the minimum necessary to remove each existing timber pile 2 ft below the proposed footing elevation. The excavation shall be backfilled with uncompacted FA-1 or FA-2 sand.

No ground improvement/treatment of the virgin soil is necessary at the spread footing.

GENERAL DATA

STRUCTURE NUMBER=====050-0261
 STRUCTURE TYPE =====MULTI-SPAN
 STRUCTURE SKEW=====0 DEGREES
 SUPER. DATA IN REFERENCE TO SUB. DATA ===== ABUT 1

TOTAL STRUCTURE LENGTH=====220.00 FT
 NUMBER OF SPANS =====2
 END SPAN LENGTH =====119.00 FT
 ADJACENT INTERIOR SPAN LENGTH =====0.01 FT

SUPERSTRUCTURE POSITIVE MOMENT REGION DATA (END OR MAIN SPAN)		
BEAM TYPE =====	PLATE GIRDER	
TOP FLANGE WIDTH =====	12.00	IN
TOP FLANGE THICKNESS =====	0.75	IN
WEB DEPTH =====	48.00	IN
WEB THICKNESS =====	0.44	IN
BOTTOM FLANGE WIDTH =====	12.00	IN
BOTTOM FLANGE THICKNESS =====	0.75	IN
BEAM SPACING PERP. TO CL =====	5.20	FT
SLAB THICKNESS =====	8.00	IN
SLAB F'C =====	4.00	KSI

SUPERSTRUCTURE POSITIVE MOMENT REGION DATA (ADJACENT SPAN)		
TOP FLANGE WIDTH =====	12.00	IN
TOP FLANGE THICKNESS =====	0.75	IN
WEB DEPTH =====	48.00	IN
WEB THICKNESS =====	0.44	IN
BOTTOM FLANGE WIDTH =====	12.00	IN
BOTTOM FLANGE THICKNESS =====	0.75	IN
BEAM SPACING PERP. TO CL =====	5.20	FT
SLAB THICKNESS =====	8.00	IN
SLAB F'C =====	4.00	KSI

ABUTMENT #1 DATA		
ABUTMENT NAME =====	South	
ABUTMENT REFERENCE BORING =====	B-1	
BOTTOM OF ABUTMENT ELEVATION =====	648	FT
ESTIMATED NUMBER OF PILES AT ABUT. =====	6	
PILE SPACING PERP. TO CL =====	5.2	FT

ABUTMENT #2 DATA		
ABUTMENT NAME =====	North	
ABUTMENT REFERENCE BORING=====	B-2	
BOTTOM OF ABUTMENT ELEVATION=====	648	FT
ESTIMATED NUMBER OF PILES AT ABUT.=====	6	
PILE SPACING PERP. TO CL =====	5.2	FT

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #1				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
645.50	2.50	3.1		
643.00	2.50	3.6		
640.50	2.50	3.4		
638.00	2.50	3.4		

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #2				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
646.00	2.00		20	2.9
643.50	2.50	3.7		
641.00	2.50	4.1		
638.50	2.50	4.60		
636.00	2.50	3.40		

10.00 FT = TOTAL DEPTH ENTERED

12.00 FT = TOTAL DEPTH ENTERED

WEIGHTED AVERAGE Qu FOR ABUTMENT #1=====: 3.38 TSF

ENTER 10 FT OF SOIL DATA

WEIGHTED AVERAGE Qu FOR ABUTMENT #2=====: 3.78 TSF

PILE STIFFNESS MODIFIER FOR ABUTMENT #1
 = 1/(1.45-[0.3*3.38])===== 2.29

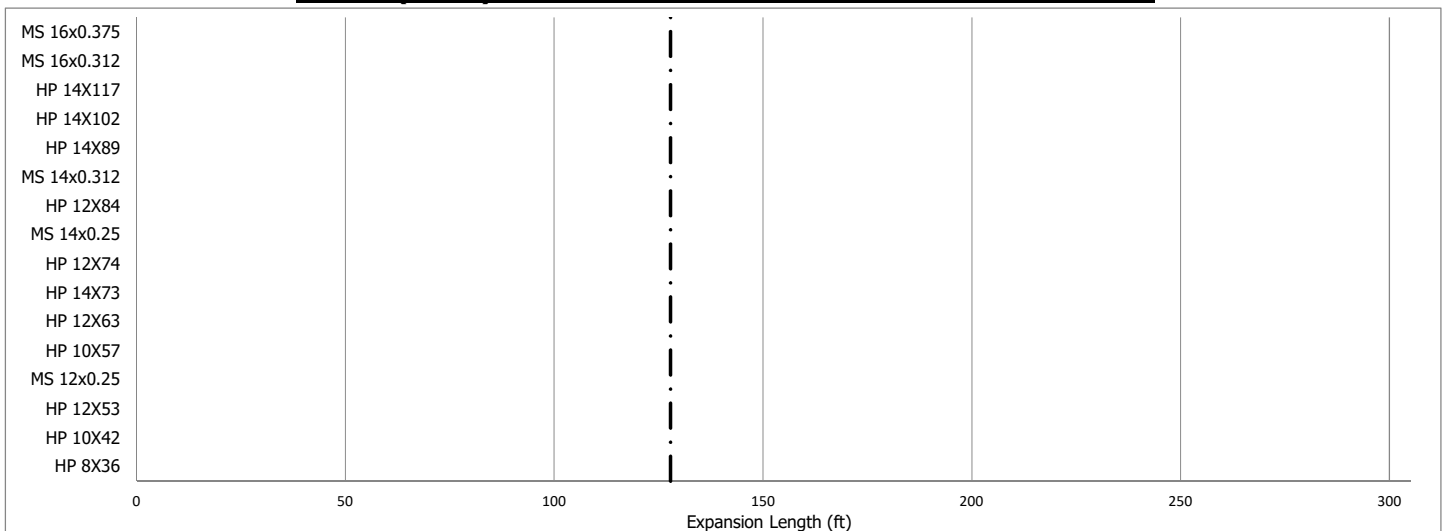
PILE STIFFNESS MODIFIER FOR ABUTMENT #2
 = 1/(1.45-[0.3*3.78])===== 3.17

WEIGHTED AVG. Qu > 3.0 TSF WITH TRIB. LENGTH > 20%, INTEGRAL ABUTMENT STRUCTURE NOT ALLOWED

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #1 = [2.29*6*0+3.17*6*220]/[2.29*6+3.17*6]===== 127.88 FT

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #2 = [3.17*6*0+2.29*6*220]/[3.17*6+2.29*6]===== 92.12 FT

ABUT 1 (South) - EXPANSION LENGTH LIMIT CHART - 0 DEG. SKEW



----- = Estimated expansion length for the indicated abutment. Piles with an expansion length greater than this are suitable for consideration.
 (Note: The same size pile should be used at both abutments.)

GENERAL DATA

STRUCTURE NUMBER=====	050-0261 w/ Bentonite/Embankment	TOTAL STRUCTURE LENGTH=====	220.00	FT
STRUCTURE TYPE =====	MULTI-SPAN	NUMBER OF SPANS =====	2	
STRUCTURE SKEW=====	0	END SPAN LENGTH =====	119.00	FT
SUPER. DATA IN REFERENCE TO SUB. DATA =====	ABUT 1	ADJACENT INTERIOR SPAN LENGTH =====	0.01	FT

SUPERSTRUCTURE POSITIVE MOMENT REGION DATA (END OR MAIN SPAN)		
BEAM TYPE =====	PLATE GIRDER	
TOP FLANGE WIDTH =====	12.00	IN
TOP FLANGE THICKNESS =====	0.75	IN
WEB DEPTH =====	48.00	IN
WEB THICKNESS =====	0.44	IN
BOTTOM FLANGE WIDTH =====	12.00	IN
BOTTOM FLANGE THICKNESS =====	0.75	IN
BEAM SPACING PERP. TO CL =====	5.20	FT
SLAB THICKNESS =====	8.00	IN
SLAB F'C =====	4.00	KSI

SUPERSTRUCTURE POSITIVE MOMENT REGION DATA (ADJACENT SPAN)		
TOP FLANGE WIDTH =====	12.00	IN
TOP FLANGE THICKNESS =====	0.75	IN
WEB DEPTH =====	48.00	IN
WEB THICKNESS =====	0.44	IN
BOTTOM FLANGE WIDTH =====	12.00	IN
BOTTOM FLANGE THICKNESS =====	0.75	IN
BEAM SPACING PERP. TO CL =====	5.20	FT
SLAB THICKNESS =====	8.00	IN
SLAB F'C =====	4.00	KSI

ABUTMENT #1 DATA		
ABUTMENT NAME =====	South	
ABUTMENT REFERENCE BORING =====	B-1	
BOTTOM OF ABUTMENT ELEVATION =====	648	FT
ESTIMATED NUMBER OF PILES AT ABUT. =====	6	
PILE SPACING PERP. TO CL =====	5.2	FT

ABUTMENT #2 DATA		
ABUTMENT NAME =====	North	
ABUTMENT REFERENCE BORING =====	B-2	
BOTTOM OF ABUTMENT ELEVATION =====	648	FT
ESTIMATED NUMBER OF PILES AT ABUT. =====	6	
PILE SPACING PERP. TO CL =====	5.2	FT

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #1				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
645.50	2.50	1.5		
643.00	2.50	1.5		
640.50	2.50	1.5		
638.00	2.50	1.5		

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #2				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
645.50	2.50	1.5		
643.00	2.50	1.5		
640.50	2.50	1.5		
638.00	2.50	1.50		

10.00 FT = TOTAL DEPTH ENTERED

10.00 FT = TOTAL DEPTH ENTERED

WEIGHTED AVERAGE Qu FOR ABUTMENT #1=====: 1.50 TSF

WEIGHTED AVERAGE Qu FOR ABUTMENT #2=====: 1.50 TSF

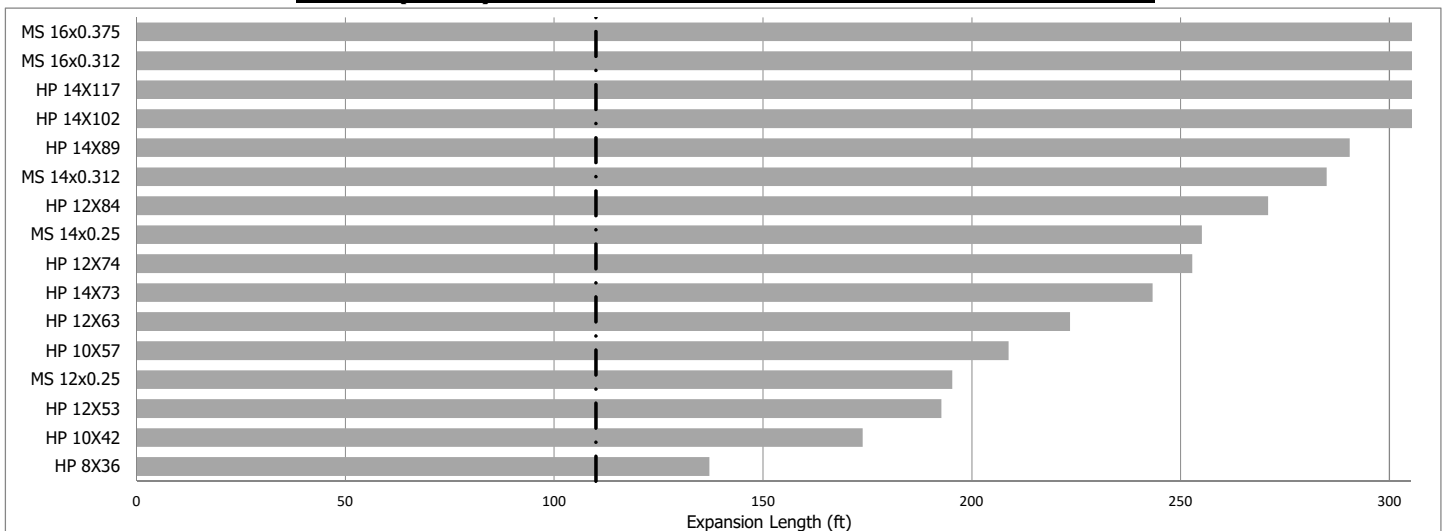
PILE STIFFNESS MODIFIER FOR ABUTMENT #1
= 1/(1.45-[0.3*1.5])===== 1.00

PILE STIFFNESS MODIFIER FOR ABUTMENT #2
= 1/(1.45-[0.3*1.5])===== 1.00

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #1 = [1*6*0+1*6*220]/[1*6+1*6]===== 110.00 FT

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #2 = [1*6*0+1*6*220]/[1*6+1*6]===== 110.00 FT

ABUT 1 (South) - EXPANSION LENGTH LIMIT CHART - 0 DEG. SKEW



--- = Estimated expansion length for the indicated abutment. Piles with an expansion length greater than this are suitable for consideration.
(Note: The same size pile should be used at both abutments.)

Substructure Loading

	Service			Load Factor	Factored (Str. 1)		
	S. Abut.	Pier	N. Abut.		S. Abut.	Pier	N. Abut.
Non-composite (DC1)	30.8	103.3	23.1	1.25	38.5	129.1	28.9
Composite (DC2)	6.7	21.3	5	1.25	8.4	26.6	6.3
Wearing Surface (DW)	10.3	33.2	7.7	1.5	15.5	49.8	11.6
One Beam Total	47.8	157.8	35.8		62.3	205.6	46.7
Six Beam Total	286.8	946.8	214.8		374.0	1233.3	280.1
Appr. Slab (DC)	106.9		106.9	1.25	133.6		133.6
Appr. Slab Wearing Surface (DW)	18.3		18.3	1.5	27.5		27.5
Two Lane Reaction (w/ Impact)	235.4		225.8	1.75	411.95		395.15
Two Lane Reaction (w/o Impact)		380.6		1.75		666.05	
Substructure Dead Load (DC)	148.9	248	148.9	1.25	186.1	310.0	186.1
Soil Above Spread Footing (EV)		105.1		1.35		141.9	
Total Substructure Load	796.3	1680.5	714.7		1133.1	2351.2	1022.4

Note: Load units = kips