

# **Abbreviated Structure Geotechnical Report**

Original Report Date: 12/1/2023 Pro	ed SN: 057-0258	Route:	FAP 317
<b>Revised Date:</b> 01/09/2024 <b>Ex</b>	g SN: 057-0070	Section:	28BR-1
Geotechnical Engineer: Doris D. Gonzale	County:	McLean	
Structural Engineer: BBS		Contract:	70571

**Indicate the proposed structure type, substructure types, and foundation locations (attach plan and elevation drawing):** The proposed structure is a simple span bridge with PPC IL beams and integral abutments supported by piles. This structure will replace an existing three-span reinforced concrete slab bridge supported by precast concrete piles. The Project Planning Unit estimated a factored load of 883 kips at each abutment. A location map is included in the Attachments.

**Discuss the existing boring data, existing plans foundation information, new subsurface exploration and need for any additional exploration to be provided with SGR Technical Memo (attach all data and subsurface profile plot):** Two borings designated boring 1 WB and 2 EB were each advanced approximately 65 ft from the location of the proposed abutments. The soil profile consists of interbedded layers of clays and sands over stiff clay till. The boring logs, as well as a TSL with their location is included in the Attachments.

Provide the location and maximum height of any new soil fill or magnitude of footing bearing pressure. Estimate the amount and time of the expected settlement. Indicate if further testing, analysis, and/or ground improvement/treatment is necessary: Per the provided Plan and Profile, the grade will be maintained, and no new fills are expected. Settlement is neglegible and no further testing or analyses are necessary.

Identify any new cuts or fill slope angles and heights. Estimate the factor of safety against slope failure. Indicate if further testing, analysis or ground improvement/treatment is necessary: Per the provided Plan and Profile, the grade will be maintained, and no new fills or significant cuts are expected. The static slope stability analyses reflected a Factor of Safety greater than 1.5 for both end slopes.

Indicate at each substructure, the 100-year and 200-year total scour depths in the Hydraulics report, the nongranular scour depth reduction, the proposed ground surface, and the recommended foundation design scour elevations: The Design Scour Elevation Table is shown below. The design and check scour elevations for integral abutments should be taken as the corresponding bottom of abutment cap elevations.

Event/L imit	Design Scour	ltem		
State	W. Abut.	E. Abut.	113	
Q100	707.82	707.54		
Q200	707.82	707.54	0	
Design	707.82	707.54	Ö	
Check	707.82	707.54		

**Determining the seismic soil site class, the seismic performance zone, the 0.2 and 1.0 second design spectral accelerations and indicate if that the soils are liquefiable:** The project is located in Seismic Performance Zone 1, has a global Site Class equal to class C, and the corresponding spectral accelerations are as

follows: Site Adjusted

Site Adjusted PGA ( $A_s$ ) = 0.059g SDS = 0.138g SD1 = 0.080g

Since the proposed structure is located in SPZ 1, the risk of liquefaction is minimal; therefore, a liquefaction analysis is not necessary.

Confirm feasibility of the proposed foundation or wall type and provide design parameters. Attach a pile design table indicating feasible pile types, various nominal required bearings, factored resistances available and corresponding estimated lengths at locations where piles will be used. Provide factored bearing resistance and unit sliding resistance at various elevations and confirm no ground improvement/treatment is necessary where spread footings are proposed. Estimated top of rock elevations as well as preliminary factored unit side and tip resistance values shall be indicated when drilled shafts are proposed: The proposed integral abutments are feasible and pile design tables have been included in the Attachments section. FGU recommends utilizing Metal Shell piles with pile shoes to support the proposed abutments. One test pile per abutment is recommended.

The piles will be analyzed for lateral loads during final design.

Calculate the estimated water surface elevation and determine the need for cofferdams (type 1 or 2), and seal coat: The provided estimated water surface elevation (EWSE) is equal to 698.3 ft. Since the EWSE is located below the bottom of both abutments, there is no need for cofferdams.

Assess the need for sheeting or soil retention or temporary construction slope and provide recommendation for other construction concerns: Traffic will be maintained utilizing stage construction. Temporary Sheet Piling is feasible at both abutments.

Attachments



Figure 1: Location Map

Input Data and Para	meter Calculations	Output Calculations and Ground Moti	ion Maps
Select <u>G</u> eogr	aphic Region	2007 AASHTO Bridge Design Guidelines	1
Conterminous 48 States	•	AASHTO Spectrum for 7% PE in 75 years Latitude = 40.741114 Longitude = -088.754926 Site Clase B	
Guideline	s <u>E</u> dition	Data are based on a 0.05 deg grid spacing.	
2007 AASHTO Bridge Design Gu	uidelines	Period Sa (sec) (g) 0.0 0.049 PGA - Site Class B	
Specify Site Location by Lati Latitude-Longitude : <u>R</u> ecor	tude-Longitude or Zip Code nmended <u>Zip Code</u>	0.2 0.115 Ss - Site Class B 1.0 0.047 S1 - Site Class B	
40.74111444 La <u>t</u> itude (50.0 to 24.6)	-88.75492603 Lo <u>ng</u> itude (-125.0 to -65.0)	Conterminous 48 States 2007 AASHTO Bridge Design Guidelines Spectral Response Accelerations SDs and SD1 Latitude = 40.741114	(
Calculate Basic De	sign Parameters	As = FpgaPGA, SDs = FaSs, and SD1 = FvS1	
Probability of Exceedance	7% PE in 75 years	Site Class C - Fpga = 1.20, Fa = 1.20, Fv = 1. Data are based on a 0.05 deg grid spacing.	.70
Calculate PGA, Ss, and S1	C <u>a</u> lculate As, SDs, and SD1	Period Sa (sec) (g) 0.0 0.059 As - Site Class C 0.2 0.138 SDs - Site Class C	
Calculate <u>R</u> esp	oonse Spectra	1.0 0.000 301 - 310 0123 0	
Map Spectrum	Design Spectrum	1	

Figure 2: Seismic Data

# Pile Design Table for 057-0258 utilizing Boring #1 WB

	Nominal	Factored	Estimated
	Required	Resistance	Pile
	Bearing	Available	Length
	(Kips)	(Kips)	(Ft.)
Metal She	ell 12"Φ w/	.25" walls	
	97	53	22
	127	70	23
	131	72	25
	136	75	27
	140	77	29
	392	216	31
Metal She	ell 14"Φ w/	.25'' walls	
	115	63	22
	155	85	23
	160	88	25
	165	91	27
	170	94	29
	459	252	31
Metal She	ell 14"Φ w/	.312" walls	
	115	63	22
	155	85	23
	160	88	25
	170	91	27
	570	94	29
Motal Sha	טיט /ש <b>16"ה ש</b>	312" walle	51
	104 44 VI 101	.512 walls	10
	135	74	22
	184	101	23
	190	105	25
	196	108	27
	202	111	29
	654	360	31
Metal She	ell 16"Φ w/	.375" walls	
	121	66	19
	135	74	22
	184	101	23
	190	105	25
	196	108	27
	202	111	29
	782	430	31

# Pile Design Table for 057-0258 utilizing Boring #2 EB

	Nominal	Factored	Estimated
	Required	Resistance	Pile
	Bearing	Available	Length
	(Kips)	(Kips)	(Ft.)
Metal She	ell 12"Φ w/	.25" walls	
	119	65	22
	142	78	25
	178	98	30
	202	111	33
	342	188	35
	392	216	39
Metal She	ell 14"Φ w/	.25'' walls	
	143	79	22
	170	94	25
	213	117	30
	241	132	33
	428	235	35
	459	252	39
Metal She	ell 14''Φ w/	.312" walls	
	143	79	22
	189	104	28
	428	235	35
	449	247	38
	491	270	40
Motol Cha	232 /بیر <b>م</b> ریم ا	293	44
metal She	160 160		00
	100	93	22
	201	10	20
	221	122	20
	522	287	35
	597	328	40
	645	355	44
Metal She	ell 16'' <b>0</b> w/	.375" walls	
	168	93	22
	221	122	28
	250	137	30
	522	287	35
	546	301	38
	597	328	40
	645	355	44

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	Division of Highways IL DEPARTMENT OF TRANS	PI LALI		1		JU			G		Date	4/1	4/22
F	ROUTE FAP_317 (US 24)	DES	SCR		۱	US 24		NT STREAM	L0	oggi	ED BY	D	DB
ę	SECTION28BR-1			LOCA	ATION	<u>0.9 r</u>	ni W of I-55, <b>SEC.</b> 3, <b>T</b>	<b>WP.</b> T26N, <b>R</b>	<b>NG</b> . R41	E, 3 <sup>rd</sup>	PM., 0	GPS:	
(	COUNTY MCLEAN D	RILLING	ME	THOD			HSA	HAMMER	TYPE		AUTC	ΜΑΤΙ	С
ę	STRUCT. NO. 057-0070	ſ	D	s	U	м	Surface Water Elev.		ft	D	S	U	м
	Station 1494+00		E P	Р Т	C S	0 	Stream Bed Elev.		ft	E P	Р   Т	C S	0
E	SORING NO.         1 WB           Station         1495+00		Т Н	N	Qu	S T	Groundwater Elev.: First Encounter	694.0	ft ▼	T H	N	Qu	S T
	Offset 6.00ft LT Ground Surface Fley. 715.00	ft	(ft)	(/12")	(tsf)	(%)	Upon Completion After Hrs.		_ ft _ ftft	(ft)	(/12")	(tsf)	(%)
4		714.67_					GRAY SILTY CLAY	(continued)					
		713.84 -		-			MOIST GRAY SAND	Y CLAY	694.00	<b>_</b>	3		
3			_								7	0.5 D	20.2
Å	AGGREGATE	-					GRAY COARSE SAN	ND	692.50			1	
5	STIFF BLACK CLAYEY	711.50		11			NO SAMPLE (WASH	HED	691.50		7		
E	EMBANKMENT	-		6	2.5	16.7	BORING)				8		
		-	5	8	P		MOIST GRAY COAF	RSE SANDY	690.00	-25	8		
		-		2					689.00		Q		
				2	1.5	28.6	GRAT STIFF SAND	I CLAT			11	1.5	16.2
		-		5	P						10	Р	
		-											
		-		4	17	32.4					3	15	15.2
		-	-10	4	B	02.1			685.00	-30	7	P	10.2
-	TAN VARVED SILTY CLAY	704.50	_				GRAY COARSE SAN (WASHED BORING)	ND )					
122		-	_	2									
T 4/26		-		3	1.7 B	24.0							
OT.GD		-		-									
		701.00		1							3		
DA.GP.	TAN MOIST COARSE CLAYEY SAND			2	1.0 P	23.8					3		
CHENC		699.50	-15	4						35	4		
N OF	MOIST GRAY SILTY CLAY	-		2									
- 1 M		698.00		3	0.5	19.0							
0200-2	GRAY SILTY CLAY			3	В				677.00	_			
IG 057		-					VERY STIFF GRAY	CLAY TILL	077.00		_		
BORIN		-		2	1.7	24.8					8 33		6.8
SOIL			-20	7	В	_				-40	69		_

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The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer) The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

(P)	Illinois De	partme	ent		s			Page <u>2</u> of <u>2</u>
	Division of Highways							Date
ROUTE		DESCI		J	115 2/			
				•	0024			
SECTION	28BR-1			ATION	<u>    0.9   </u>	ni W of I-55, <b>SEC.</b> 3, 1	TWP. T26N, RNG. R4	<u>1E, 3<sup>rd</sup> PM., GPS:</u>
COUNTY	MCLEAN D	RILLING M	ETHOD			HSA	HAMMER TYPE	AUTOMATIC
STRUCT. NO Station	0. <u>057-0070</u> 1494+00	D E P	S P T	U C S	M O I	Surface Water Elev. Stream Bed Elev.	ft ft	
BORING NO. Station Offset	1 WB 1495+00 6.00ft LT	H	N	Qu	S T	Groundwater Elev.: First Encounter Upon Completion	694.0ft ⊻ft	-
Ground Su	face Elev. 715.00	) ft (ft	) (/12")	(tsf)	(%)	After Hrs.	ft	
(continued)	GRAY CLAY TILL	-	_					
			_					
		-	32					
			50		6.7			
		4	<sub>5</sub> 50-4"					
		-	_					
			_					
		-	22					
			52	10.0	7.7			
End of Boring	9	665.00 -5	000					
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The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer) The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

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	Division of Highways IL DEPARTMENT OF TRAN	SPORTATION		I							Date	4/2	1/22
	<b>ROUTE</b> FAP 317 (US 24)	DES	SCR	PTION	I	US 24	OVER INTERMITTANT	STREAM	LC	GGI	ED BY	D	DB
	SECTION28BR-1			LOCA	ATION	<u>0.9 r</u>	ni W of I-55, <b>SEC.</b> 3, <b>TW</b>	/P. T26N, RN	<b>G.</b> R4E	, 3 <sup>rd</sup>	PM., C	GPS:	
	COUNTY MCLEAN	ORILLING	ME	THOD			HSA	HAMMER T	YPE _		AUTO	MATIO	С
	STRUCT. NO.         057-0070           Station         1494+00           BORING NO         2 FB		D E P T	S P T	U C S	M 0 I %	Surface Water Elev Stream Bed Elev		ft ft	DEPT	S P T	U C S	M 0 I ⊗
	Station         1493+00           Offset         6.00ft RT		н	N	Qu	Т	First Encounter	694.0	ft ⊻ ft	н	N	Qu	т
	Ground Surface Elev. 715.0	0 <b>ft</b>	(ft)	(/12")	(tsf)	(%)	After Hrs		ft	(ft)	(/12")	(tsf)	(%)
	ASPHALT CONCRETE	714.67_					MOIST SOFT GRAY S (continued)	SILTY CLAY					
	AGGREGATE STIEF VARVED CLAY	713.84 713.59							-	¥ 			
							GRAY COARSE SAND	) C	692.00				
	BURIED PCC PAVEMENT -	711.00			4.0	21.2	(WASHED BORING)				6 6		
	NOT POSSIBLE	710.00	-5		P					-25	7		
	SOFT BLACK TOPSOIL			2									
				3	0.7	20.9							
			_	3	В								
								(	686.50	_	_		
				4 5	4.1	23.4	CLAY	SANDY			7 10	2.5	8.8
			-10	4	S					-30	11	Р	
	SOFT VARVED CLAY	704.50						(	684.00				
6/22		·		3	10	30.4	MOIST GRAY COARS	SE SAND		_			
DT 4/2				2	B	00.4	GRAY CLAY TILL		083.00	_			
DOT.G	STIFF GRAY SILTY CLAY	702.00											
ין ור				2					-		7		10.1
IOA.GF		700.00	-15	4	2.5 P	22.7				-35	8 8	2.5 P	12.1
CHEN	SOFT VARVED CLAY	100.00							679.50				
I W OF	STIFF GRAY SILTY CLAY	699.00		3			STIFF VARVED CLAY	6	678.50				
0 - 1 M			_	4	1.5 P	21.2	STIFF GRAY CLAY TI	LL					
57-007				+					-				
ING 0		606.00	_	3					-	_	4		
L BOR	MOIST SOFT GRAY SILTY CLA	Y		6	1.5	18.3			-		4	3.2	10.2
SOI			-20	7	S					-40	8	В	

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer) The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

( ) Illinois Depart	tment	SC			Page <u>2</u> of <u>2</u>
Division of Highways IL DEPARTMENT OF TRANSPORTAT					Date <u>4/21/22</u>
ROUTE FAP 317 (US 24) I	DESCRIPTION	US 24	OVER INTERMITTAN	IT STREAM LOG	GED BY DDB
SECTION 28BR-1		ATION 0.9	mi W of I-55, <b>SEC.</b> 3, <b>T</b>	WP. T26N, RNG. R4E, 3	B <sup>rd</sup> <b>PM., GPS:</b>
COUNTY MCLEAN DRILLI	NG METHOD		HSA	HAMMER TYPE	AUTOMATIC
STRUCT. NO.         057-0070           Station         1494+00	D S E P P T	U M C O S I	Surface Water Elev. Stream Bed Elev.	ft ft	
BORING NO.         2 EB           Station         1493+00           Offset         6.00ft RT	T H N	Qu T	Groundwater Elev.: First Encounter Upon Completion	694.0ft ⊻ft	
Ground Surface Elev. 715.00 f	t (ft) (/12")	(tsf) (%)	After Hrs.	ft	
(continued)					
	9				
	17 _45 23	8.5 10.1 S			
	_				
	17	3.4 10.4	-		
	<u>-50</u> 27	В	-		
8	13				
4/30/2 ⊢	50 17 28	7.5 8.6 B			
AUGER REFUSAL			-		
0070	_				

#### Benchmark: Northeast wingwall of SN 057-0070 at Sta. 1494+46.57 - 18.45' Lt., Elevation 715.13.

Existing Structure: SN 057-0070 was originally built in 1959 under Section 28-BR at Station 1494+00. The structure is a 3-span RC slab bridge measureing 86'-10" between back of abutments carrying F.A.P. 317 (US 24) over an unnamed tributary of Rooks Creek 0.9 miles West of F.A.I. 55 by Chenoa. The structure was repaired in 1996 under Section ((28,29,30)R)S-1&28BR with deck patching, integral abutment conversion, new approach slabs, scarification with microsilica overlay and steel bridge rails. Deck patching was performed in 2021.





/.P.T. Sta. 1494+81.00 Elev. 714.56

#### **PROFILE GRADE** (Along @ U.S. 24)

-0.36%

The profile grade shows the final elevations after grinding.



2020 AASHTO LRFD Bridge Design Specifications, 9th Edition

### LOADING HL-93

Allow 50#/sq. ft. for future wearing surface.

### DESIGN STRESSES FIELD UNITS

f'c = 3,500 psi f 'c = 4,000 psi (Superstructure) fy = 60,000 psi (Reinforcement)

PRECAST PRESTRESSED UNITS

f'c = 8,500 psi f 'c = 6,500 psi fpu = 270,000 psi (0.6" Dia. low lax. Strands) fpbt = 202,300 psi (0.6" Dia. low lax. Strands)

## SEISMIC DATA

Seismic  $\overline{Performance Zone}$  (SPZ) = 1 Design Spectral Acceleration at 1.0 sec. (SD1) = 0.080g Design Spectral Acceleration at 0.2 sec. (SDS) = 0.138g Soil Site Class = C

## HIGHWAY CLASSIFICATION

F.A.P. Rte. 317 - U.S. 24 Functional Class: Other Principal Arterial ADT: 3300 (2021); 3650 (2041) ADTT: 726 (2021); 803 (2041) DHV: 260 Design Speed: 60 m.p.h. Posted Speed: 55 m.p.h. Two-Way Traffic Directional Distribution: 55/45

GENERAL PLAN & ELEVATION U.S. RTE. 24 OVER UN-NAMED TRIBUTARY TO ROOKS CREEK F.A.P. RTE. 317 - SEC. 28BR-1 MCLEAN COUNTY STATION 1494+00.00 STRUCTURE NO. 057-0258

	F A P RTE	SEC	TION		COUNTY	TOTAL SHEETS	SHEET NO.
	317	28BR-1		McLean	2	1	
					CONTRA	CT NO.	70571
TS			ILLINOIS	FED. A	D PROJECT		



8.1	18 mi. <sup>2</sup> Existing Low Grade Elev. 714.40 @ Sta. 1496+00 Proposed Low Grade Elev. 714.40 @ Sta. 1496+00									
	Freq.	Q	Openi	ing Ft <sup>2</sup>	Nat.	Head	1 - Ft.	Headwater El.		
	Yr.	C.F.S.	Exist.	Prop.	H.W.E.	Exist.	Prop.	Exist.	Prop.	
	10	1150	237	247	706.6	0.3	0.2	706.9	706.8	
	50	1850	305	321	708.1	0.7	0.6	708.8	708.7	
	100	2160	325	342	708.5	1.0	0.8	709.5	709.3	
ĸ	200	2487	340	358	708.8	1.2	1.0	710.0	709.8	
	500	2920	361	381	709.2	1.5	1.3	710.7	710.5	

			-
nt / Limit	Design Scour	Item	
State	W. Abut.	E. Abut.	113
Q100	707.82	707.54	
Q200	707.82	707.54	
esign	707.82	707.54	0
Check	707.82	707.54	



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	<u>1496</u>	  		  1497 
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	FREEBO	ARD = 5.7 f		
ADWATER ELEVATION = 7	08.7 👽			
L4 14 195+50	04 1496+00	F.A. RTE.	1496+5 <u>0</u> SECTION	 1497+00 TOTAL SHEET SHEETS NO. TNO

720			3.296							
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		> ₩ ₩ ₩			Material Name	Color Unit Weight (lbs/ft3)	Cohesion (psf)	Phi (deg)		
- - - - - - - - - - - - - - - - - - -					New Fill Clay Sandy Clay 1 Sand	120 120 120 120 117	1000 1700 500	0 0 0 32		
				ľ	Sandy Clay 2 Clay Till	120 130	1500 5000	0		
- - - - - - - - - - - - - - - -		· · · · · · · · · · · · · · · · · · ·				· · · · · · · · · · · · · · · · · · ·	· · · · · .	1 1 1	·····	
	0 20	406080100120140160ProjectSlide2 - An Interactive Slope Stability Program								
	rocscience	Group Drawn By	Group Group 1			Scenario Master Scenario				
SLIDEINTERPRE	EINTERPRET 9.024 Date 11/3/2023, 9:47:58 AM			File Name West Embankment.slmd						

740		3.164								
- <u>- 1</u> - <u>- 200</u> 					Material Name New Fill Clay Silty Clay 1 Sand Sandy Clay 2 Clay Till	Color Color	Unit Weight (lbs/ft3) 120 120 120 120 117 1 1 130	Cohesion (psf) 1000 1000 1500 2500 5000	Phi (deg) 0 0 32 0 0	
		40 Project						120		140
Γ.	roccionco	Group 1 Slide2 - An Interactive Slope Stability Program								
	IUCSCIENCE	Drawn By Date	11/3/2023 9·47·58 ΔΜ		Company File Name	Fact	Fmhankm	ent slmd		
SLIDEINTERPRET	9.024		11, 5/ 2025, 51 17 150 AP			Lust	Linbunkin	chilonnu		