

<b>Original Report Date:</b> 1/13/2017	<b>Proposed SN:</b> 027-0104	<b>Route:</b> FAS 1522 (US 45)
<b>Revised Date:</b> 4/10/2017	<b>Existing SN:</b> 027-0012	<b>Section:</b> 31-X-BR
<b>Geotechnical Engineer:</b> Michael Short, IDOT District 3		<b>County:</b> Ford
<b>Structural Engineer:</b> Lori Sommer, Milhouse Engineering & Const.		<b>Contract:</b> 66C84

**Indicate the proposed structure type, substructure types, and foundation locations (attach plan and elevation drawing):** The proposed structure is a three span bridge with a reinforced concrete deck. Integral abutments are preferred. The preliminary TS&L is attached. The proposed structure will be shifted approximately 8 feet north compared to the existing structure to improve the alignment with the channel.

**Discuss the existing boring data, existing plans foundation information, new subsurface exploration and need for any additional exploration to be provided with SGR Technical Memo (attach all data and subsurface profile plot):** Soil borings from June 2014 are attached. The existing structure is founded on 18" square precast concrete piles at the abutments and spread footings at the piers.

**Provide the location and maximum height of any new soil fill or magnitude of footing bearing pressure. Estimate the amount and time of the expected settlement. Indicate if further testing, analysis, and/or ground improvement/treatment is necessary:** The proposed profile of the roadway is not expected to change and a site visit found no signs of settlement at the existing structure. Therefore, the soil is not anticipated to experience any additional loading that would result in settlement. No further analysis for settlement is warranted.

**Identify any new cuts or fill slope angles and heights. Estimate the factor of safety against slope failure. Indicate if further testing, analysis or ground improvement/treatment is necessary:** Because the proposed side slopes are less than 15 feet high and are a maximum of 1:3 (V:H) and because the existing slopes exhibit no slope stability issues, a side slope analysis was not performed. However, an end slope stability analysis was performed. The IDOT Geotechnical Manual requires a Factor of Safety of 1.5 because the analysis is based on Rimac samples. Based on the analysis of a 1:2 (V:H) end slope, the factor of safety against slope failure is 4.6. A printout of the slope configuration used in the analysis is attached. No further analysis for slope stability is warranted.

**Indicate at each substructure, the 100-year and 200-year total scour depths in the Hydraulics report, the non-granular scour depth reduction, the proposed ground surface, and the recommended foundation design scour elevations:** The scour results from the hydraulic report indicate 6.0 feet of scour for the 100 year event and 10.7 feet of scour for the 200 year event. The soil borings indicate cohesive soils with unconfined compressive strength greater than 4.0 tsf. Therefore, a 50% scour reduction will be used. Based on this reduction, the scour elevation table will be as follows:

Design Scour Elevations (ft.)					Item 113
Event/Limit State	South Abutment	Pier 1	Pier 2	North Abutment	
Q100	731.50	709.40	709.40	730.50	8
Q200	731.50	707.05	707.05	730.50	
Design	731.50	709.40	709.40	730.50	
Check	731.50	707.05	707.05	730.50	

**Determining the seismic soil site class, the seismic performance zone, the 0.2 and 1.0 second design spectral accelerations and indicate if that the soils are liquefiable:** The seismic soil site class is D. The seismic performance zone is 1. The 0.2 second design spectral acceleration is 0.204 g. The 1.0 second design spectral acceleration is 0.123 g. Liquefaction is not a concern at this location.

**Confirm feasibility of the proposed foundation or wall type and provide design parameters. Attach a pile design table indicating feasible pile types, various nominal required bearings, factored resistances available and corresponding estimated lengths at locations where piles will be used. Provide factored bearing resistance and unit sliding resistance at various elevations and confirm no ground improvement/treatment is necessary where spread footings are proposed. Estimated top of rock elevations as well as preliminary factored unit side and tip resistance values shall be indicated when drilled shafts are proposed:**

Preliminary substructure loadings are attached.

The BB&S "Integral Abutment Feasibility Analysis" spreadsheet was used to determine the pile sizes available for use at the abutments, based on the current BB&S policy. The current policy would allow for the use of following piling sizes and shapes: HP10X42, HP12X53, HP10X57, HP12X74, HP14X73, HP12X84, HP14X89, HP14X102, and HP14X117. A draft version of the proposed revisions to the BB&S integral abutment policy was also used. The proposed draft policy expands this list by including MS12X0.179, MS12X0.25, MS14X0.25, MS14X0.312, MS 16X0.312 and MS 16X0.375. A copy of the results is attached. It is recommended to use the draft policy as it is expected that the policy will be adopted in the near future.

One test pile is recommended at each of the substructure units. The District prefers that the same pile type and size be used throughout the structure. Pile design tables were created using the BB&S "Pile Capacity and Length Estimates" spreadsheet. These tables are attached. At Pier 1, the tables were created assuming a 12 inch diameter pre core to elevation 696.0 prior to driving metal shell piles. This is necessary to prevent damage to metal shell piles during driving through the dense granular soils. By using a 12 inch diameter pre core with a 14 or 16 inch diameter metal shell pile, the risk of damage to the pile is minimized while still developing skin friction. This is necessary to ensure a minimum length of pile is installed prior to reaching the bearing capacity of the pile or damaging the pile.

Metal shell piles are preferred by the District because their estimated lengths are shorter than H piles. Additionally, the estimated lengths of metal shell piles are expected to be more predictable than the estimated length of H piles because the H piles will not encounter bedrock.

If metal shell piles are used, pile shoes are recommended to penetrate the dense granular soils. If H piles are used, pile shoes are not needed.

No underground Coal mines were identified near the project site according to the Illinois State Geological Survey website.

**Calculate the estimated water surface elevation and determine the need for cofferdams (type 1 or 2), and seal coat:** The estimated water surface elevation (EWSE) is 715.9. A Type 1 cofferdam is necessary at each pier. A seal coat is not necessary.

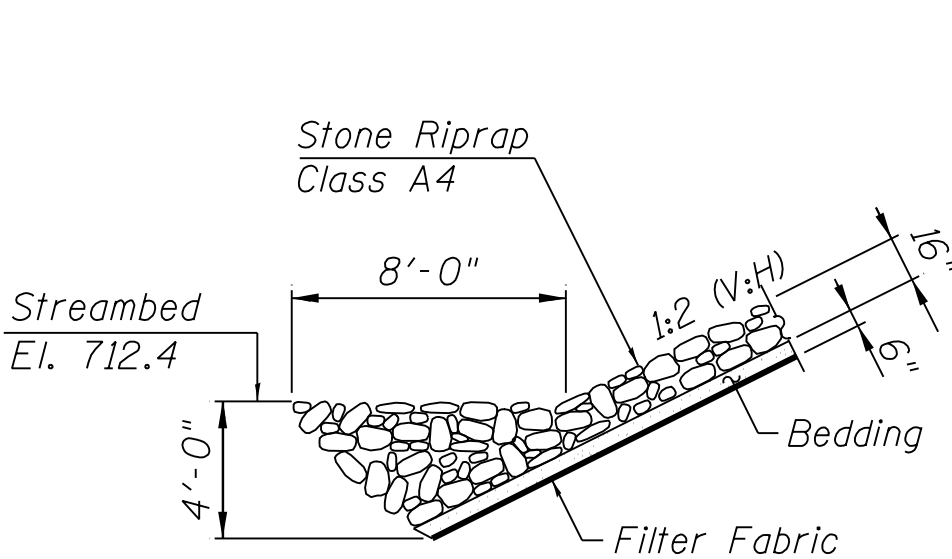
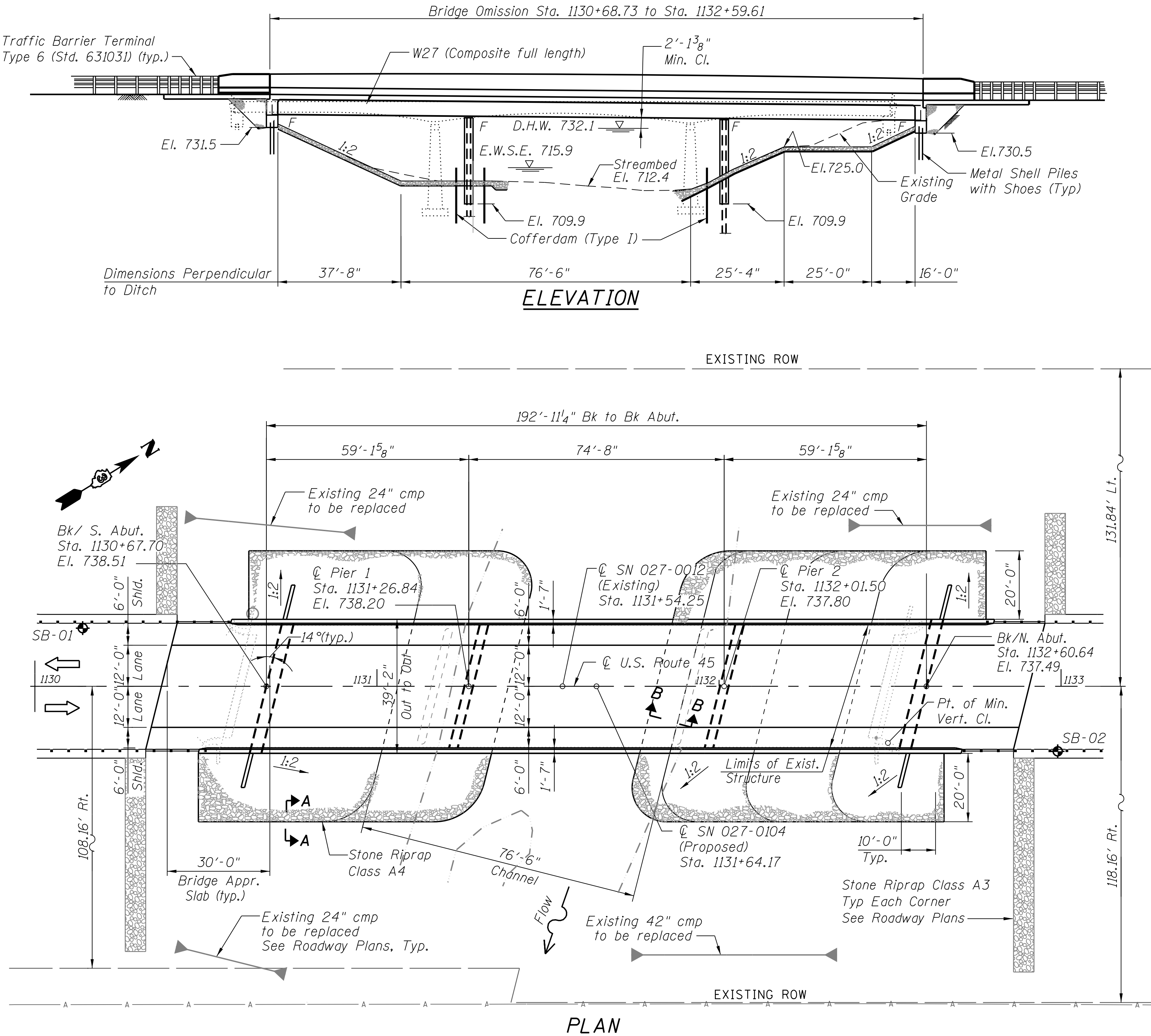
**Assess the need for sheeting or soil retention or temporary construction slope and provide recommendation for other construction concerns:** Sheet piling, soil retention, or temporary construction slopes will not be necessary for this structure because the structure is expected to be constructed using a detour. If stage construction becomes necessary, temporary sheet piling is feasible because soils with strengths exceeding 4.5 tsf are below the required embedment depth.

Benchmark: Bm # 41A U.S.G.S. Benchmark disc on top of SW wingwall SN 027-0012.  
Sta. 1130+63.65. 21.22 Lt. Elev. 738.97

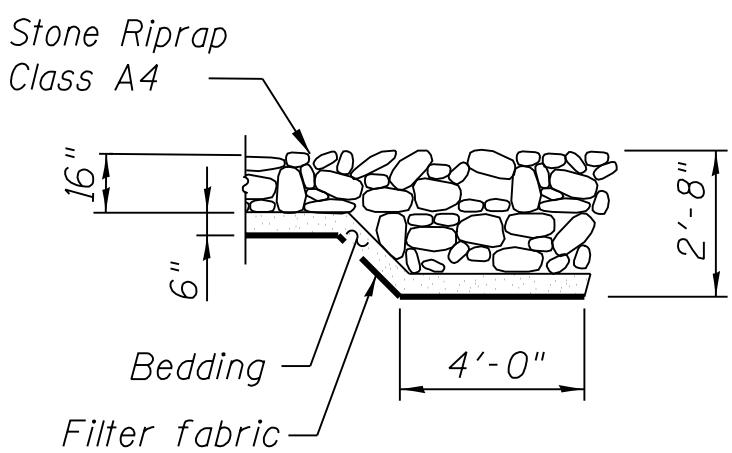
Existing Structure: SN 027-0012 was originally constructed in 1953 as SBI Rt 25, Section 31-X-B. The existing structure was patched and the deck expansion devices replaced in 1994 as Section 31 I & 32W & RS-1. The bridge was retrofitted with a curb mounted steel guardrail. The existing superstructure is a three span bridge (57'-5", 74'-8", 57'-5") constructed of reinforced T-beams and a 7" deck plus a 1 1/2" bituminous overlay. The bridge is 193'-10" back to back of abutments and is 35'-8" wide out to out of deck. It is skewed 14°left forward . The abutments are stub abutments supported on piles. The piers are solid shafts supported on spread footings

Traffic shall be detoured during construction.

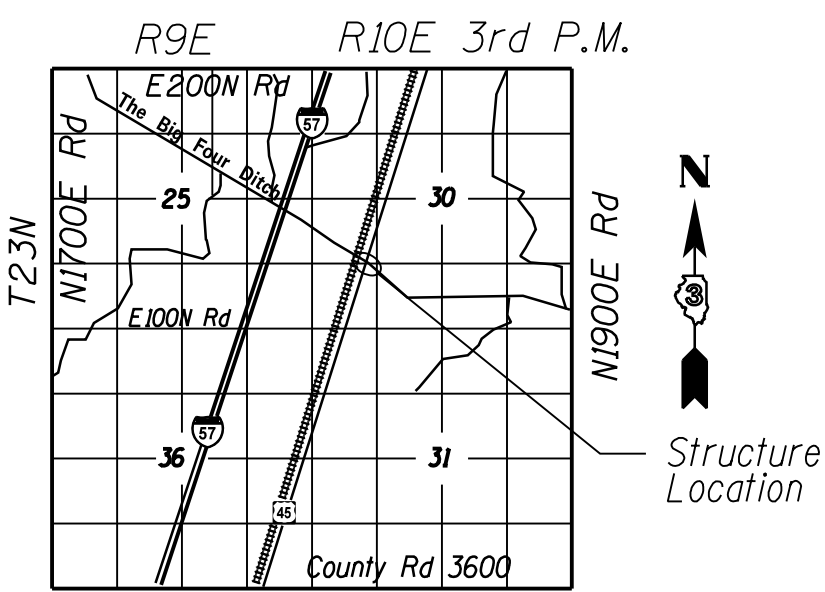
No Salvage



SECTION B-B



SECTION A-A



**LOADING HL-93**  
Allow 50#/sq. ft. for future wearing surface

**HIGHWAY CLASSIFICATION**

Route: FAS 1522 (US Route 45)  
Functional Class: Major Collector  
ADT: 3450 (2015), 4284 (2039)  
DHV = 1000  
ADTT = 110 (2015), 137 (2039)  
Design Speed: 55 mph  
Posted Speed: 55 mph  
Directional Distribution: 50/50  
Two Way Traffic

**SEISMIC DATA**

Seismic Performance Zone (SPZ) = 1  
Design Spectral Acceleration @ 1.0 sec (SD1) = .123g  
Design Spectral Acceleration @ 0.2 sec (SDS) = .204g  
Soil Site Class = D

**DESIGN SPECIFICATIONS**

AASHTO LRFD Bridge Design  
Specifications with 2015 & 2016 Interims

**DESIGN STRESSES**

**FIELD UNITS**

$f'_c$  = 3,500 psi  
 $f'_c$  = 4,000 psi (Superstructure Concrete)  
 $f_y$  = 60,000 psi (Reinforcement)  
 $F_y$  = 50,000 psi (M270 Grade 50W)

**GENERAL PLAN**  
**U.S. ROUTE 45 OVER BIG FOUR DITCH**  
**FAS 1522 (US RTE 45)**  
**SECTION 31-X-BR**  
**FORD COUNTY**  
**STA. 1131+64.17**  
**STRUCTURE NO. 027-0104**



USER NAME = talegde	DESIGNED - LAS	REVISED -
PLOT SCALE = 19.1667' / in.	CHECKED - DAZ	REVISED -
PLOT DATE = 4/7/2017	DRAWN - TCS	REVISED -
	CHECKED - LAS	REVISED -

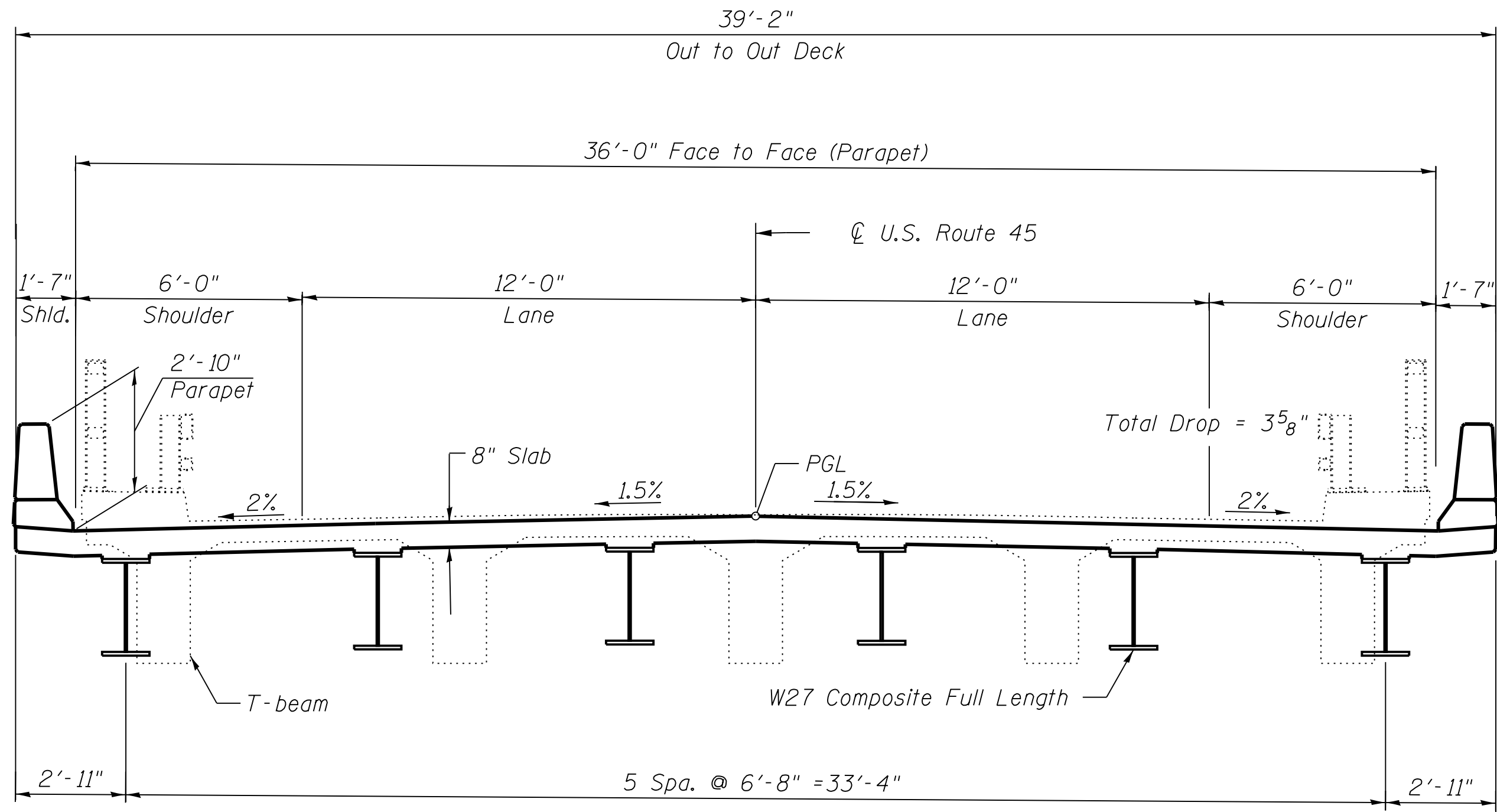
STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION

GENERAL PLAN  
STRUCTURE NO. 027-0104

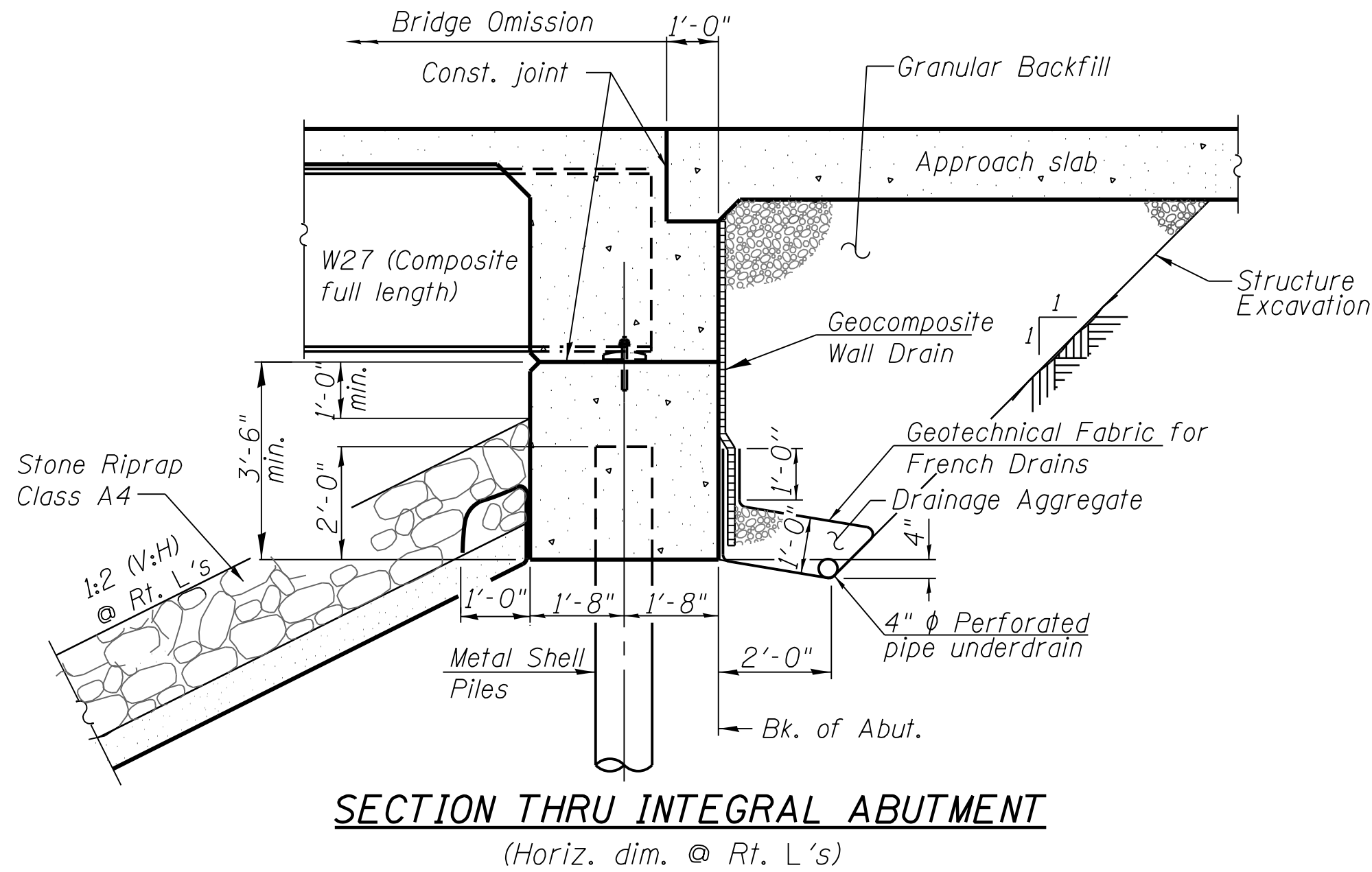
SHEET NO. 1 OF 2 SHEETS

F.A.S. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
1522	31-X-BR	FORD		
CONTRACT NO. 66C84				
ILLINOIS FED. AID PROJECT				

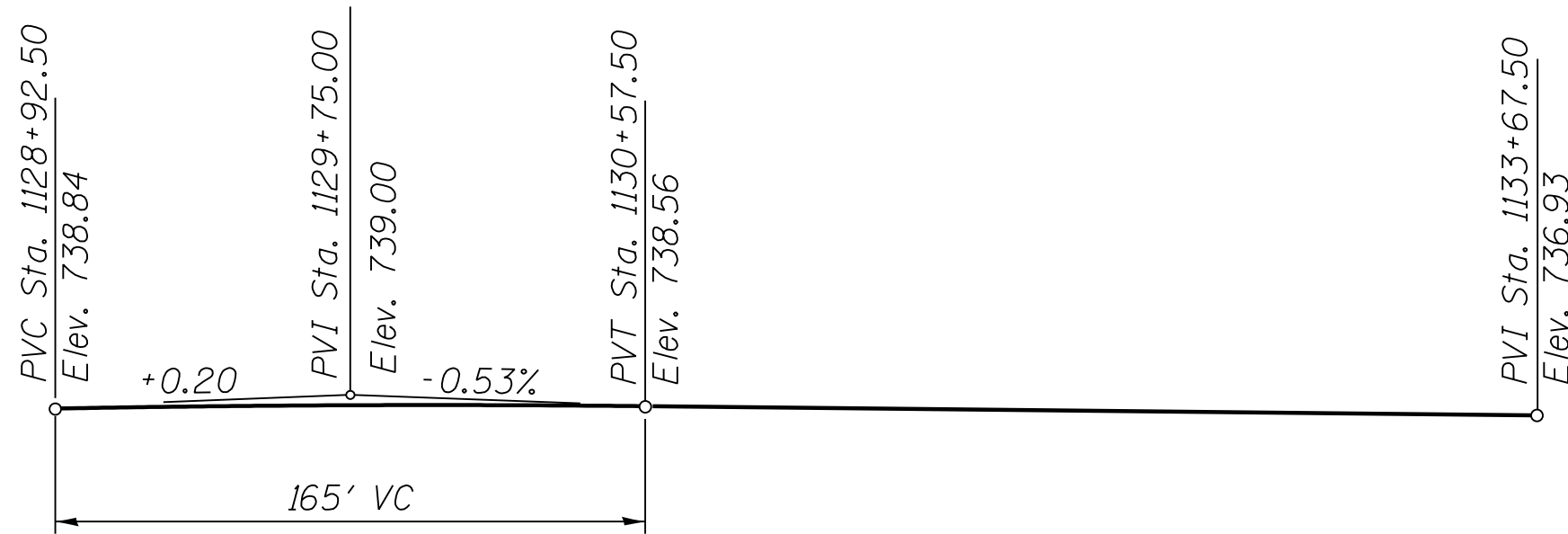
FILE NAME = P:\2015\0566-1001-D3 Various Phase II (PTB 145-18) WD12.13 & 14\0566-05 (TSI US45 over Four Big Ditch)\04-CADD\04-Sheet Files\TSSA Drawings\Gen Data & X-Section.dgn



**CROSS SECTION**  
(Looking North)



**SECTION THRU INTEGRAL ABUTMENT**  
(Horiz. dim. @ Rt. L's)



**PROFILE GRADE**  
(along  $\varnothing$  US Route 45)

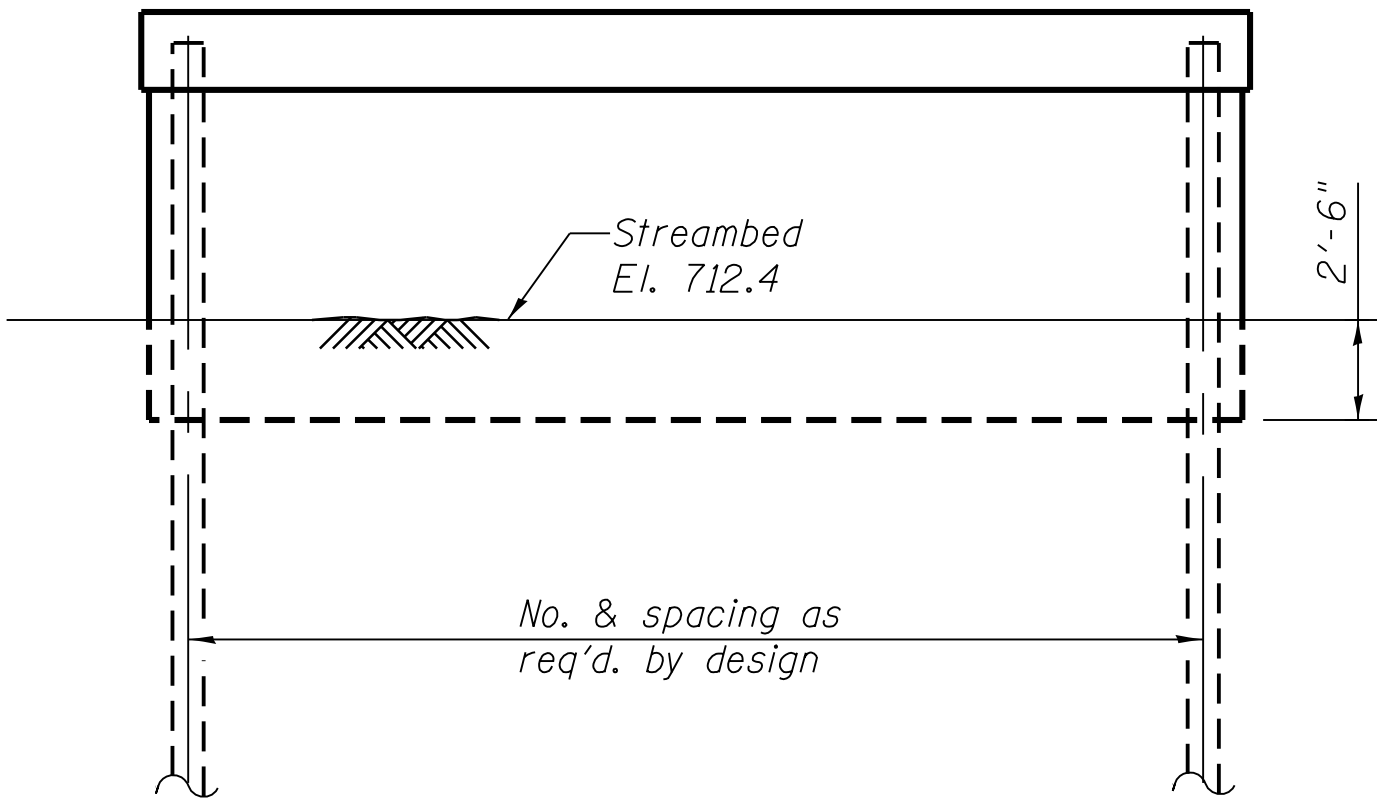
**DESIGN SCOUR ELEVATION TABLE**

Event / Limit State	Design Scour Elevations (ft.)				
	S. Abut.	Pier 1	Pier 2	N. Abut.	Item 113
Q100	731.5	709.4	709.4	730.5	8
Q200	731.5	707.1	707.1	730.5	
Design	731.5	709.4	709.4	730.5	
Check	731.5	707.1	707.1	730.5	

**WATERWAY INFORMATION**

Drainage Area = -		159 sq. mi		Exist. Low Grade Elev. = 736.41 @ Sta. 1134+00 Prop. Low Grade Elev. = 736.41 @ Sta. 1134+00					
Flood	Freq. Yr.	Q C.F.S.	Opening Sq. Ft.		Nat. H.W.E.	Head - Ft.		Exist.	Prop.
			Exist.	Prop.		Exist.	Prop.		
Hydraulic Design	10	5460	1826	1935	730.5	0.1	0.1	730.6	730.6
Base	50	8340	2074	2204	732.1	0.1	0.1	732.2	732.2
Scour Design	100	9560	2188	2326	732.8	0.2	0.2	733.0	732.9
Max. Calc.	200	10846	2257	2398	733.2	0.2	0.2	733.4	733.4
Overtopping	500	12500	2371	2515	733.9	0.3	0.3	734.2	734.1
	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A

10-Year Velocity through Existing Bridge = 3.0 fps  
10-Year Velocity through Proposed Bridge = 2.8 fps



**PIER SKETCH**

**SECTIONS**  
**U.S. ROUTE 45 OVER BIG FOUR DITCH**  
**FAS 1522 (US RTE 45)**  
**SECTION 31-X-BR**  
**FORD COUNTY**  
**STA. 1131+64.17**  
**STRUCTURE NO. 027-0104**



USER NAME = taledge  
PLOT SCALE = 12,0038 " / in.  
PLOT DATE = 4/7/2017

DESIGNED - LAS  
CHECKED - DAZ  
DRAWN - TCS  
CHECKED - LAS

REVISED -  
REVISED -  
REVISED -  
REVISED -

**STATE OF ILLINOIS**  
**DEPARTMENT OF TRANSPORTATION**

**SECTIONS**  
**STRUCTURE NO. 027-0104**

SHEET NO. 2 OF 2 SHEETS

F.A.S. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
1522	31-X-BR	FORD		
CONTRACT NO. 66C84				
ILLINOIS FED. AID PROJECT				

Page 1 of 2Date 6/19/14

US 45 over Big Four Ditch, 3.04 miles South of IL  
9

<b>ROUTE</b>	US 45 (SBI-25)	<b>DESCRIPTION</b>	9	<b>LOGGED BY</b>	Larry Myers
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<b>SECTION</b>	31-X-B	<b>LOCATION</b>	SW 1/4, <b>SEC. 30, TWP. 23N, RNG. 10E, 3<sup>rd</sup> PM,</b> <b>Latitude 40.418174, Longitude -88.113446</b>
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**COUNTY** Ford **DRILLING METHOD** Hollow Stem Auger **HAMMER TYPE** CME Automatic

**STRUCT. NO.** 027-0012 (Exist.)  
**Station** 1131+54.25

<b>BORING NO.</b>	01 (S.W. Quad.)
<b>Station</b>	1130+14
<b>Offset</b>	17.0 ft Lt.
<b>Ground Surface Elev.</b>	738.59

DEPTH	BLOW COUNTS	U C S  Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

Surface Water Elev.	715.09	ft
Stream Bed Elev.	713.09	ft
Groundwater Elev.:		
First Encounter	716.1	ft ▼
Upon Completion	698.6	ft ▼
After Hrs.		ft

D E P T H	B L O W S	U C S  Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

SOIL BORING 027-0012.GPJ IL DOT.GDT 10/14/14

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, form 137 (Rev. 8-99)

Page 2 of 2Date 6/19/14

<b>ROUTE</b>	US 45 (SBI-25)	<b>DESCRIPTION</b>	9	<b>LOGGED BY</b>	Larry Myers
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**COUNTY** Ford **DRILLING METHOD** Hollow Stem Auger **HAMMER TYPE** CME Automatic

D E P T H	B L O W S	U C S  Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

Very Dense Gray Fine Sand with no free water, Grading to Medium & Coarse Sand at 40' (continued)		24			677.09	5		
		33		2		6	3.5	27
		40				7	P	
696.59					End of Boring			
Very Stiff to Hard Gray Sandy Clay Loam Till with Coarse Sand Layers		6						
		8	3.7	11				
		10	B					
	-45	6			-65			
		10	4.1	12				
		12	B					
		8						
	689.59	11	6.3	10				
	16	S						
Hard Black / Dark Brown Silty Clay Loam / Silty Clay - Paleosoil?	-50	5			-70			
		11	>4.5	29				
		16	P					
683.59	-55	10			-75			
Hard to Very Stiff Dark Brown to Black Silty Clay Loam / Silty Loam with Layers of Loam, Silt & Sand - Lake / Swamp Deposits		14	5.5	17				
		18	S					
	-60				-80			

SOIL BORING 027-0012.GPJ IL DOT.GDT 10/14/14

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, form 137 (Rev. 8-99)

Page 1 of 2

**Date** 6/20/14

<b>ROUTE</b>	US 45 (SBI-25)	<b>DESCRIPTION</b>	9	<b>LOGGED BY</b>	Larry Myers
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<b>SECTION</b>	<u>31-X-B</u>	<b>LOCATION</b>	<u>SW 1/4, SEC. 30, TWP. 23N, RNG. 10E, 3<sup>rd</sup> PM,</u> <b>Latitude 40.418898, Longitude -88.113004</b>
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**COUNTY** Ford **DRILLING METHOD** Hollow Stem Auger **HAMMER TYPE** CME Automatic

SOIL BORING 027-0012.GPJ IL DOT.GDT 10/14/14

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, form 137 (Rev. 8-99)



# SOIL BORING LOG

ROUTE US 45 (SBI-25) DESCRIPTION US 45 over Big Four Ditch, 3.04 miles South of IL 9 LOGGED BY Larry Myers

SECTION 31-X-B LOCATION SW 1/4, SEC. 30, TWP. 23N, RNG. 10E, 3<sup>rd</sup> PM,  
Latitude 40.418898, Longitude -88.113004

COUNTY Ford DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME Automatic

STRUCT. NO. 027-0012 (Exist.)  
Station 1131+54.25

BORING NO. 02 (N.E. Quad.)  
Station 1132+99  
Offset 19.0 ft Rt.  
Ground Surface Elev. 736.91 ft

D E P T H  (ft)	B L O W S  (/6")	U C S  (tsf)	M O I S T  (%)
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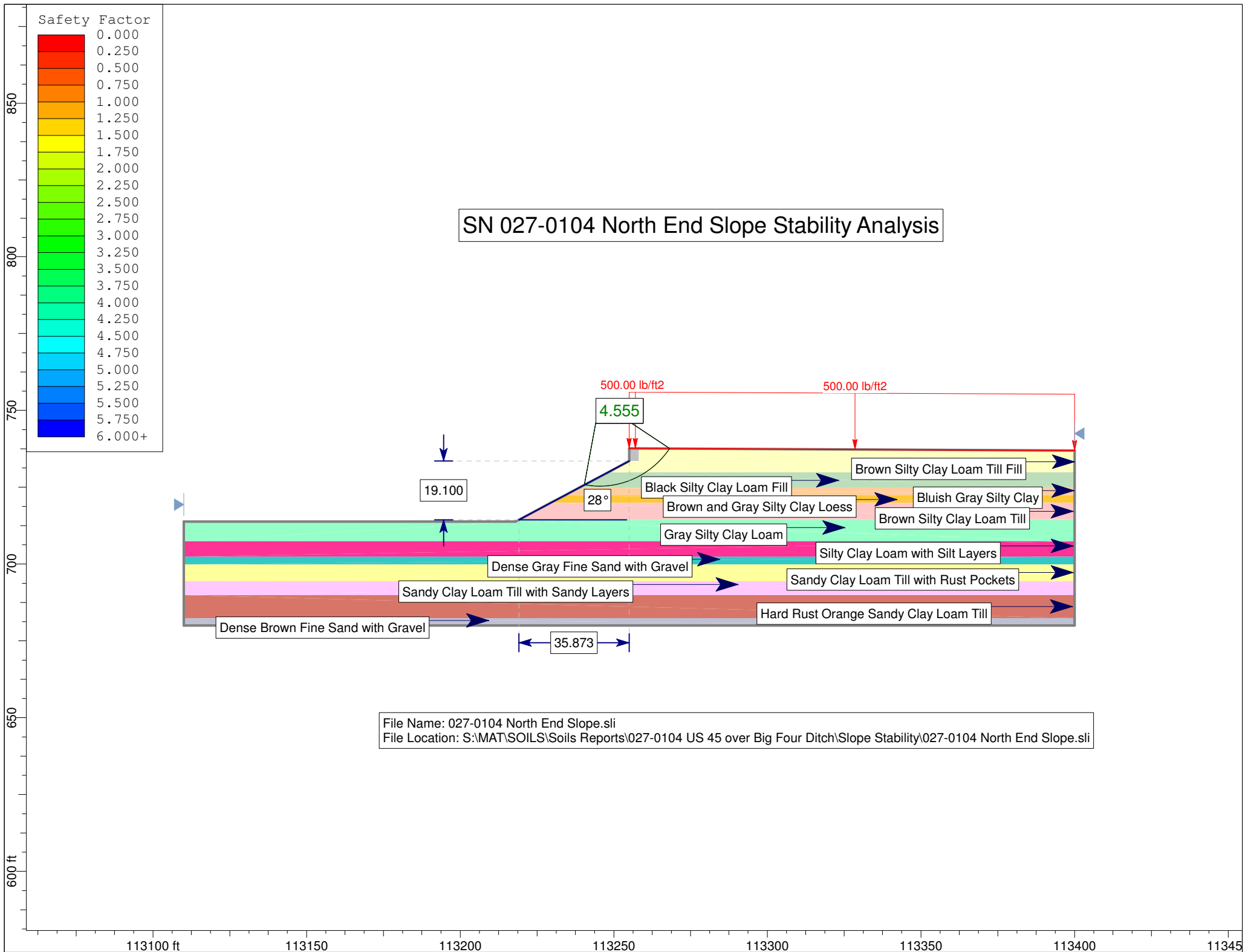
Surface Water Elev.	715.09	ft
Stream Bed Elev.	713.09	ft
Groundwater Elev.:		
First Encounter	714.9	ft ▼
Upon Completion	696.9	ft ▼
After _____ Hrs.		ft

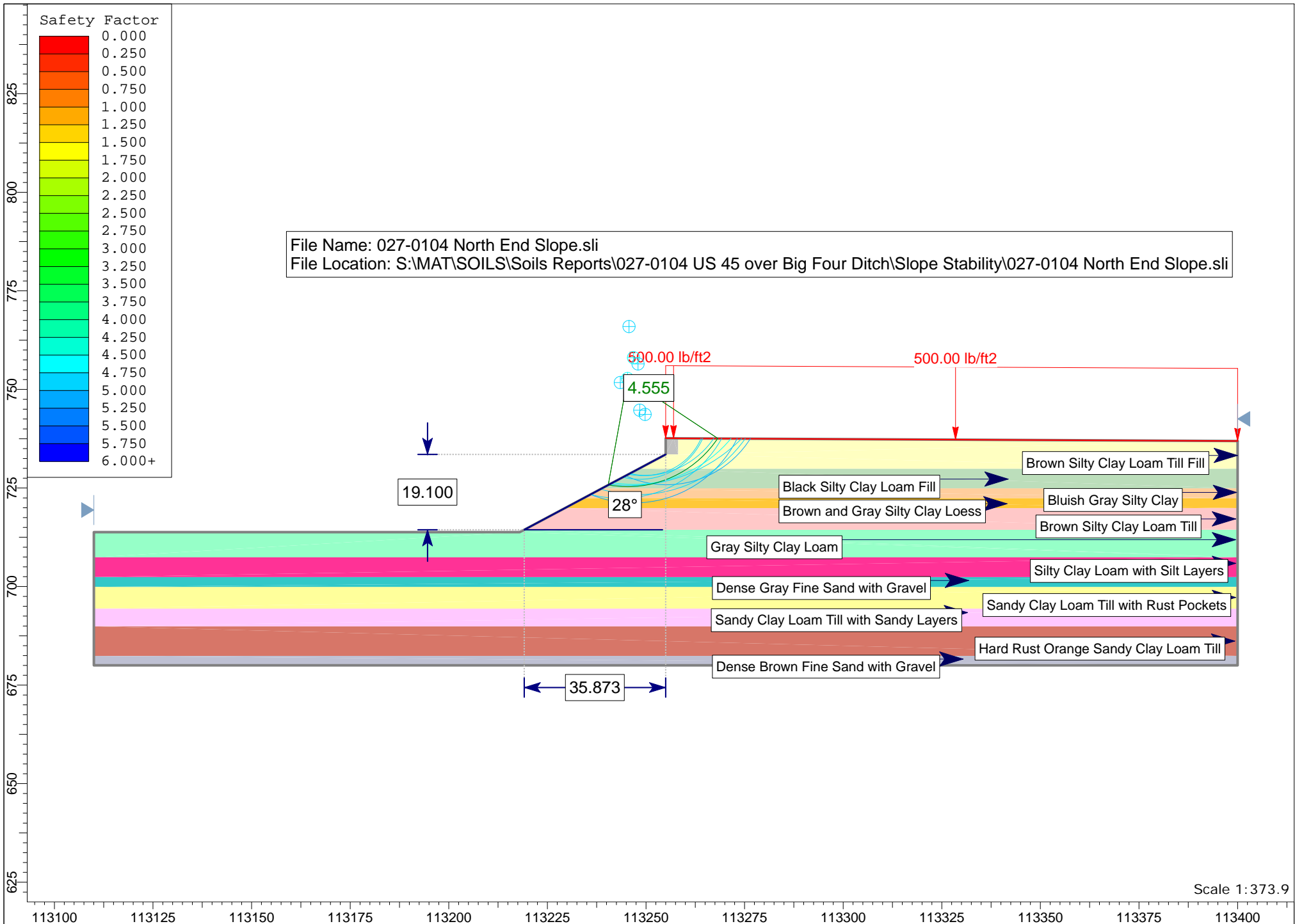
D E P T H  (ft)	B L O W S  (/6")	U C S  (tsf)	M O I S T  (%)
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Hard Gray Sandy Clay Loam Till with Sand Layers ( <i>continued</i> )	7			Dense Brown Fine Sand to Coarse Gravel with free water ( <i>continued</i> )	10		
	10	6.1	9		19		16
	14	S			30		
694.41				675.41			
Hard Brown & Gray Sandy Clay Loam Till with Heavy Rust Pockets	8			End of Boring			
	10	6.1	13				
	15	S					
-45					-65		
Hard Rust Orange Sandy Clay Loam Till	10						
	11	6.1	18				
	14	S					
689.91							
Hard Rust Orange Sandy Clay Loam Till	7						
	9	5.4	15				
	12	S					
-50					-70		
Dense Brown Fine Sand to Coarse Gravel with free water	7						
	7	5.3	14				
	8	S					
Dense Brown Fine Sand to Coarse Gravel with free water	7						
	9	5.1	16				
	10	S					
682.41					-75		
Dense Brown Fine Sand to Coarse Gravel with free water	9						
	16		17				
	21						
Dense Brown Fine Sand to Coarse Gravel with free water	12						
	18		16				
	21						
-60					-80		

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)









# SEISMIC SITE CLASS DETERMINATION

PROJECT TITLE=====SN 027-0104

Substructure 1 South Abutment					
Base of Substruct. Elev. (or ground surf for bents) 731.6 ft.					
Pile or Shaft Dia. 12 inches					
Boring Number 1					
Top of Boring Elev. 738.6 ft.					
Approximate Fixity Elev. 725.6 ft.					
Individual Site Class Definition:					
N (bar): 13 (Blows/ft.) Soil Site Class E					
N <sub>60</sub> (bar): NA (Blows/ft.) NA					
s <sub>u</sub> (bar): 3.84 (ksf) Soil Site Class C <----Controls					
Seismic Soil Column	Bot. Of Sample	Layer			
Depth	Elevation	Thick.	N	Qu	Description
(ft)	(ft)	(ft)	(tsf)		Boundary
	736.1	2.50	2	1.00	B
	733.6	2.50	6	2.50	
	731.1	2.50	5	2.50	
	728.6	2.50	9	3.50	
	726.1	2.50	9	2.70	B
1.5	724.1	2.00	2	2.00	B
4.0	721.6	2.50	6	2.50	B
6.5	719.1	2.50	2	1.50	
9.0	716.6	2.50	2	1.00	B
11.5	714.1	2.50	19		B
14.0	711.6	2.50	22	6.60	
16.5	709.1	2.50	19	6.80	
19.0	706.6	2.50	18	6.20	
21.5	704.1	2.50	19	6.00	B
24.5	701.1	3.00	16	5.00	B
27.0	698.6	2.50	88		
29.0	696.6	2.00	73		B
31.5	694.1	2.50	18	3.70	
34.0	691.6	2.50	22	4.10	
36.0	689.6	2.00	27	6.30	B
39.0	686.6	3.00	27	4.50	
42.0	683.6	3.00	27	4.50	B
44.5	681.1	2.50	32	5.50	
47.0	678.6	2.50	32	5.50	B
48.5	677.1	1.50	13	3.50	B
51.5	674.1	3.00	24	4.50	
54.5	671.1	3.00	24	4.50	
57.5	668.1	3.00	24	4.50	
60.5	665.1	3.00	24	4.50	
63.5	662.1	3.00	24	4.50	
66.5	659.1	3.00	24	4.50	
69.5	656.1	3.00	24	4.50	
72.5	653.1	3.00	24	4.50	
75.5	650.1	3.00	24	4.50	
79.0	646.6	3.50	24	4.50	
82.5	643.1	3.50	24	4.50	
86.0	639.6	3.50	24	4.50	
89.5	636.1	3.50	24	4.50	
93.0	632.6	3.50	24	4.50	
96.5	629.1	3.50	24	4.50	
100.0	625.6	3.50	24	4.50	B

Substructure 2 Pier 1					
Base of Substruct. Elev. (or ground surf for bents) 709.9 ft.					
Pile or Shaft Dia. 12 inches					
Boring Number 1					
Top of Boring Elev. 738.6 ft.					
Approximate Fixity Elev. 703.9 ft.					
Individual Site Class Definition:					
N (bar): 24 (Blows/ft.) Soil Site Class D					
N <sub>60</sub> (bar): NA (Blows/ft.) NA					
s <sub>u</sub> (bar): 4.5 (ksf) Soil Site Class C <----Controls					
Seismic Soil Column	Bot. Of Sample	Layer			
Depth	Elevation	Thick.	N	Qu	Description
(ft)	(ft)	(ft)	(tsf)		Boundary
	736.1	2.50	2	1.00	B
	733.6	2.50	6	2.50	
	731.1	2.50	5	2.50	
	728.6	2.50	9	3.50	
	726.1	2.50	9	2.70	B
	724.1	2.00	2	2.00	B
	721.6	2.50	6	2.50	B
	719.1	2.50	2	1.50	
	716.6	2.50	2	1.00	B
	714.1	2.50	19		B
	711.6	2.50	22	6.60	
	709.1	2.50	19	6.80	
	706.6	2.50	18	6.20	
	704.1	2.50	19	6.00	B
2.8	701.1	3.00	16	5.00	B
5.3	698.6	2.50	88		
7.3	696.6	2.00	73		B
9.8	694.1	2.50	18	3.70	
12.3	691.6	2.50	22	4.10	
14.3	689.6	2.00	27	6.30	B
17.3	686.6	3.00	27	4.50	
20.3	683.6	3.00	27	4.50	B
22.8	681.1	2.50	32	5.50	
25.3	678.6	2.50	32	5.50	B
26.8	677.1	1.50	13	3.50	B
31.3	672.6	4.50	24	4.50	
35.8	668.1	4.50	24	4.50	
40.3	663.6	4.50	24	4.50	
44.8	659.1	4.50	24	4.50	
49.3	654.6	4.50	24	4.50	
53.8	650.1	4.50	24	4.50	
58.3	645.6	4.50	24	4.50	
62.8	641.1	4.50	24	4.50	
67.3	636.6	4.50	24	4.50	
71.8	632.1	4.50	24	4.50	
76.3	627.6	4.50	24	4.50	
80.8	623.1	4.50	24	4.50	
85.3	618.6	4.50	24	4.50	
90.0	613.9	4.70	24	4.50	
95.0	608.9	5.00	24	4.50	
100.0	603.9	5.00	24	4.50	B

Substructure 3 Pier 2					
Base of Substruct. Elev. (or ground surf for bents) 709.9 ft.					
Pile or Shaft Dia. 12 inches					
Boring Number 2					
Top of Boring Elev. 736.9 ft.					
Approximate Fixity Elev. 703.9 ft.					
Individual Site Class Definition:					
N (bar): 35 (Blows/ft.) Soil Site Class D					
N <sub>60</sub> (bar): 42 (Blows/ft.) Soil Site Class D <----Controls					
s <sub>u</sub> (bar): 4.8 (ksf) Soil Site Class C					
Seismic Soil Column	Bot. Of Sample	Layer			
Depth	Elevation	Thick.	N	Qu	Description
(ft)	(ft)	(ft)	(tsf)		Boundary
	734.4	2.50	2	1.00	B
	731.9	2.50	5	2.00	
	729.9	2.00	4	1.50	B
	727.4	2.50	4	1.50	
	724.9	2.50	5	2.00	B
	722.4	2.50	7	2.00	B
	719.9	2.50	8	2.50	B
	717.4	2.50	20	5.90	
	714.4	3.00	27	8.40	B
	711.9	2.50	32	10.90	
	709.4	2.50	24	8.00	
	707.4	2.00	20	5.30	B
	704.9	2.50	19	4.60	
1.5	702.4	2.50	19	4.10	B
4.0	699.9	2.50	56		B
6.5	697.4	2.50	20	4.20	
9.5	694.4	3.00	24	6.10	B
12.0	691.9	2.50	25	6.10	
14.0	689.9	2.00	25	6.10	B
16.5	687.4	2.50	21	5.40	
19.0	684.9	2.50	15	5.30	
21.5	682.4	2.50	19	5.10	B
24.0	679.9	2.50	37		
26.5	677.4	2.50	39		
28.5	675.4	2.00	49		B
32.5	671.4	4.00	42		
37.0	666.9	4.50	42		
41.5	662.4	4.50	42		
46.0	657.9	4.50	42		
50.5	653.4	4.50	42		
55.0	648.9	4.50	42		
59.5	644.4	4.50	42		
64.0	639.9	4.50	42		
68.5	635.4	4.50	42		
73.0	630.9	4.50	42		
77.5	626.4	4.50	42		
82.0	621.9	4.50	42		
86.5	617.4	4.50	42		
91.0	612.9	4.50	42		
95.5	608.4	4.50	42		
100.0	603.9	4.50	42		B

Substructure 4 North Abutment					
Base of Substruct. Elev. (or ground surf for bents) 730.9 ft.					
Pile or Shaft Dia. 12 inches					
Boring Number 2					
Top of Boring Elev. 736.9 ft.					
Approximate Fixity Elev. 724.5 ft.					
Individual Site Class Definition:					
N (bar): 27 (Blows/ft.) Soil Site Class D					
N <sub>60</sub> (bar): 42 (Blows/ft.) Soil Site Class D <----Controls					
s <sub>u</sub> (bar): 4.26 (ksf) Soil Site Class C					
Seismic Soil Column	Bot. Of Sample	Layer			
Depth	Elevation	Thick.	N	Qu	Description
(ft)	(ft)	(ft)	(tsf)		Boundary
	734.4	2.50	2	1.00	B
	731.9	2.50	5	2.00	
	729.9	2.00	4	1.50	B
	727.4	2.50	4	1.50	
	724.9	2.50	5	2.00	B
2.1	722.4	2.50	7	2.00	B
4.6	719.9	2.50	8	2.50	B
7.1	717.4	2.50	20	5.90	
10.1	714.4	3.00	27	8.40	B
12.6	711.9	2.50	32	10.90	
15.1	709.4	2.50	24	8.00	
17.1	707.4	2.00	20	5.30	B
19.6	704.9	2.50	19	4.60	
22.1	702.4	2.50	19	4.10	B
24.6	699.9	2.50	56		B
27.1	697.4	2.50	20	4.20	
30.1	694.4	3.00	24	6.10	B
32.6	691.9	2.50	25	6.10	
34.6	689.9	2.00	25	6.10	B
37.1	687.4	2.50	21	5.40	
39.6	684.9	2.50	15	5.30	
42.1	682.4	2.50	19	5.10	B
44.6	679.9	2.50	37		
47.1	677.4	2.50	39		
49.6	674.9	2.50	49		B
52.6	671.9	3.00	42		
55.6	668.9	3.00	42		
58.6	665.9	3.00	42		
61.6	662.9	3.00	42		
64.6	659.9	3.00	42		
67.6	656.9	3.00	42		
70.6	653.9	3.00	42		
73.6	650.9	3.00	42		
76.6	647.9	3.00	42		
79.6	644.9	3.00	42		
82.6	641.9	3.00	42		
85.6	638.9	3.00	42		
89.1	635.4	3.50	42		
92.6	631.9	3.50	42		
96.1	628.4	3.50	42		
100.0	624.5	3.90	42		B

## Global Site Class Definition: Substructures 1 through 4

N (bar): 25 (Blows/ft.) Soil Site Class D  
N<sub>60</sub> (bar): 43 (Blows/ft.) Soil Site Class D <----Controls  
s<sub>u</sub> (bar): 4.24 (ksf) Soil Site Class C



PROJECT TITLE=====

Printed 1/4/2017

# Design Maps Summary Report

## User-Specified Input

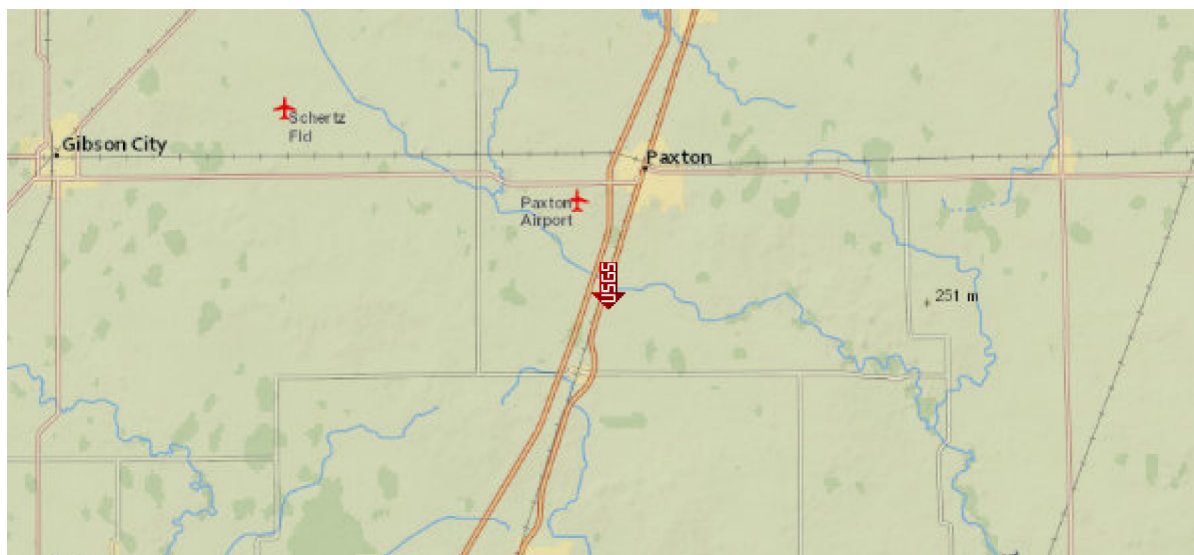
**Report Title** SN 027-0104

Wed January 4, 2017 19:07:00 UTC

**Building Code Reference Document** 2009 AASHTO Guide Specifications for LRFD Seismic Bridge Design  
(which utilizes USGS hazard data available in 2002)

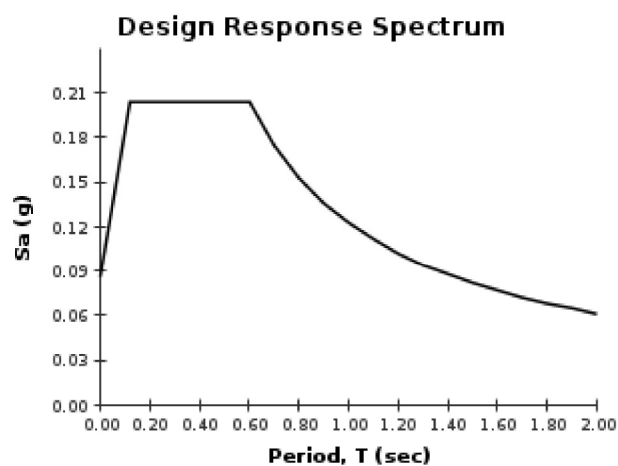
**Site Coordinates** 40.41817°N, 88.11345°W

**Site Soil Classification** Site Class D – “Stiff Soil”



## USGS-Provided Output

<b>PGA</b> = 0.054 g	<b>A<sub>s</sub></b> = 0.086 g
<b>S<sub>s</sub></b> = 0.128 g	<b>S<sub>DS</sub></b> = 0.204 g
<b>S<sub>1</sub></b> = 0.051 g	<b>S<sub>D1</sub></b> = 0.123 g



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[External] US 45 over Big Four Ditch

Hide

**From:** Lori Sommer

**Sent:** 12/19/2016 2:24 PM

**To:** Short, Michael A; Ferguson, Steven P

**Cc:** Deborah Zroka

 Message  PTSL US 45 over Big Four Ditch.pdf (1.9 MB)

Mike,

I have attached the preliminary TSL for the bridge carrying US 45 over the Big Four Ditch.

These are the preliminary substructure loads:

- Abutments
  - Service Dead Load=305k
  - Service Live Load plus Impact =255k
  - Total Service Load= 560k
  - Factored Dead Load=390k
  - Factored Live Load plus Impact= 440k
  - Total Factored Load = 830k
- Piers
  - Service Dead Load=975k
  - Service Live Load =305k
  - Total Service Load= 1280k
  - Factored Dead Load=1250k
  - Factored Live Load = 535k
  - Total Factored Load = 1785k

Please let me know if you need any other information.

**Lori Sommer SE, PE** | Senior Structural Engineer

**Milhouse Engineering & Construction, Inc.**

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D: 847.968.4312 | O: 312.987.0061 | F: 312.987.0071

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STRUCTURE NUMBER===== SN 027-0104  
STRUCTURE TYPE ===== MULTI-SPAN  
STRUCTURE SKEW===== 14 DEGREES  
TOTAL STRUCTURE LENGTH===== 192.94 FT  
LONGEST END SPAN LENGTH ===== 59.14 FT

**ABUTMENT #1 DATA**

ABUTMENT NAME ===== South Abutment  
ABUTMENT REFERENCE BORING===== Boring 01  
BOTTOM OF ABUTMENT ELEVATION===== 731.6 FT  
ESTIMATED NUMBER OF PILES AT ABUT.===== 8

**ABUTMENT #2 DATA**

ABUTMENT NAME ===== North Abutment  
ABUTMENT REFERENCE BORING===== Boring 02  
BOTTOM OF ABUTMENT ELEVATION===== 730.5 FT  
ESTIMATED NUMBER OF PILES AT ABUT.===== 8

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #1				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
729.10	2.50	3.5		
726.60	2.50	2.7		
724.10	2.50	2.0		
721.60	2.50	2.5		

10.00 FT = TOTAL DEPTH ENTERED

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #2				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
729.90	0.60	1.5		
727.40	2.50	1.5		
724.90	2.50	2.0		
722.40	2.50	2.00		
720.50	1.90	2.50		

10.00 FT = TOTAL DEPTH ENTERED

WEIGHTED AVERAGE Qu FOR ABUTMENT #1===== 2.68 TSF

WEIGHTED AVERAGE Qu FOR ABUTMENT #2===== 1.94 TSF

PILE STIFFNESS MODIFIER FOR ABUTMENT #1  
= 1/(1.45-[0.3\*2.68])===== 1.54

PILE STIFFNESS MODIFIER FOR ABUTMENT #2  
= 1/(1.45-[0.3\*1.94])===== 1.15

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #1 = [1.54\*8\*0+1.15\*8\*192.94]/[1.54\*8+1.15\*8]===== 82.43 FT

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #2 = [1.15\*8\*0+1.54\*8\*192.94]/[1.15\*8+1.54\*8]===== 110.51 FT

**EFFECTIVE EXPANSION LENGTH (EEL) CALCULATION**

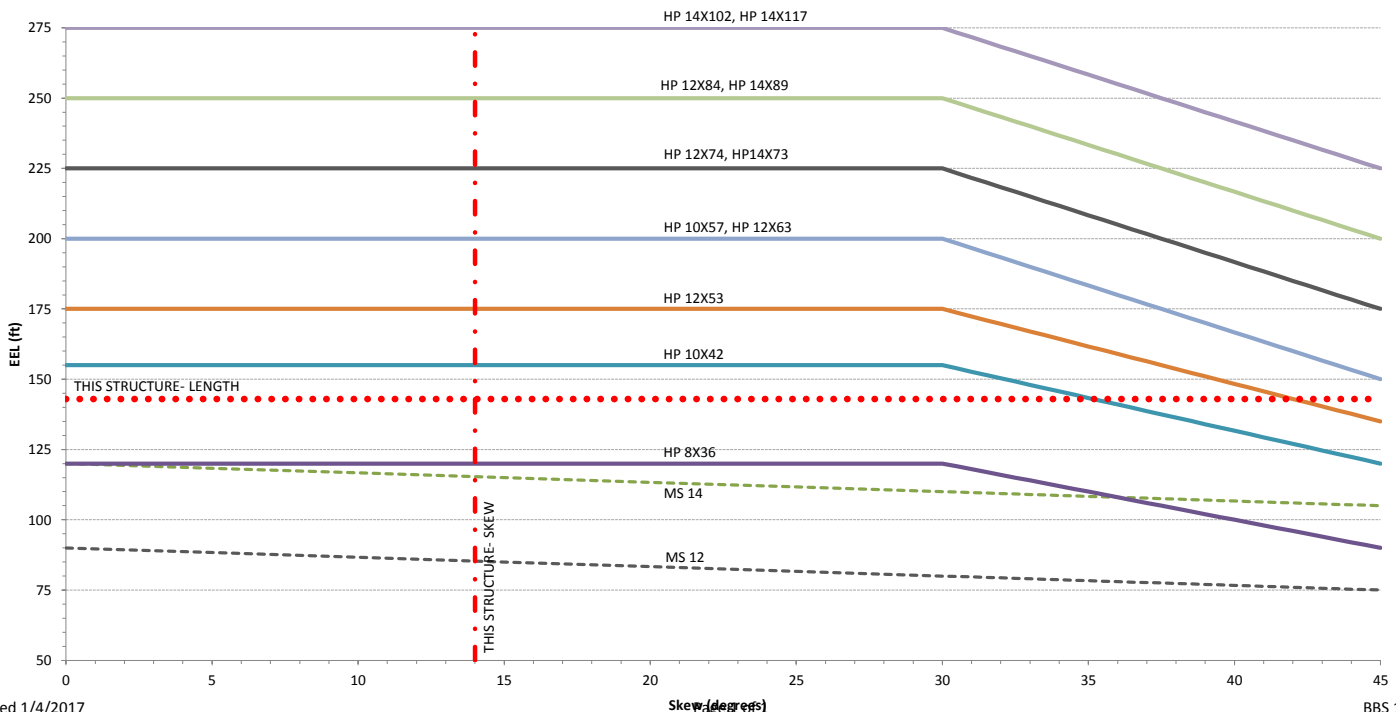
CONTROLLING ABUTMENT===== ABUT. #2 North Abutment  
CONTROLLING EXPANSION LENGTH (DISTANCE TO CENTROID OF STIFFNESS FROM CONTROLLING ABUTMENT) ===== 110.51 FT  
WEIGHTED AVE. Qu FOR CONTROLLING ABUTMENT ===== 1.94 TSF  
Qu CORRECTION FACTOR ===== 1.94/1.5 ===== 1.29  
EFFECTIVE EXPANSION LENGTH (EEL) ===== EEL = 110.51\*1.29 ===== 142.92 FT

**FEASIBLE PILE TYPES PER CHART IN ABD MEMO 12.3 BASED ON SKEW AND EEL OR MODIFIED EEL:**

PILE SIZES AT OR ABOVE THE LENGTH LINE AT THE INTERSECTION WITH THE SKEW LINE ARE ALLOWED FOR USE WITH THIS INTEGRAL ABUTMENT STRUCTURE

**AVAILABLE PILE SIZES:**

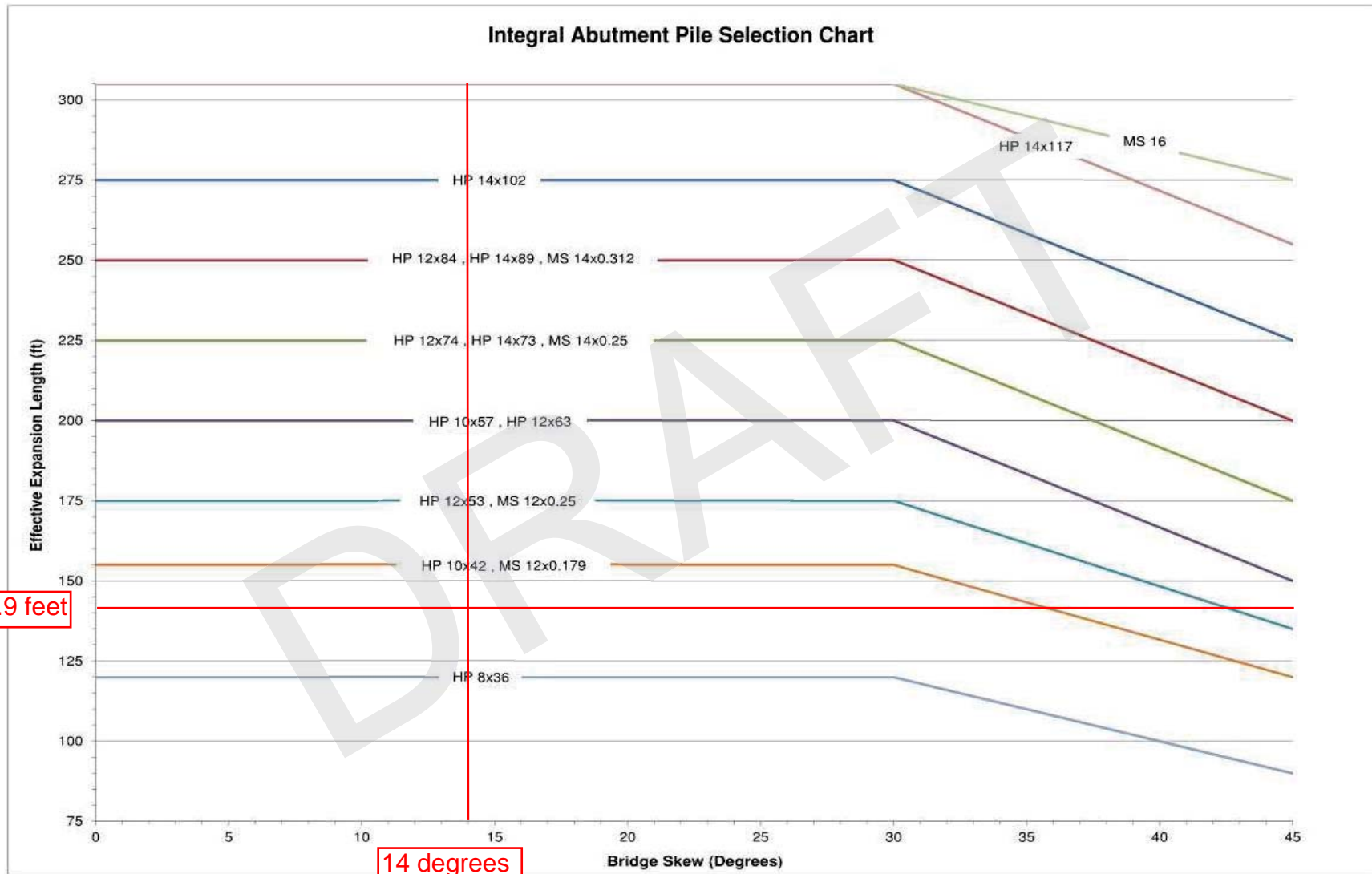
HP 10X42, HP 12X53, HP 10X57, HP 12X63, HP 12X74, HP 14X73, HP 12X84, HP 14X89, HP 14X102, HP 14X117



# SN 027-0104 Proposed Integral Abutment Policy Pile Selection Chart

Structure Skew = 14 degrees

Effective Expansion Length = 142.9 feet



Allowable pile sizes:

MS 12X0.179, MS 12X0.25, MS 14X0.25, MS 14X0.312, MS 16  
HP 10X42, HP 10X57, HP 12X53, HP 12X63, HP 12X74, HP 12X84  
HP 14X73, HP 14X89, HP 14X102, HP 14X117



SUBSTRUCTURE===== **South Abutment**  
 REFERENCE BORING ===== **1**  
 LRFD or ASD or SEISMIC ===== **LRFD**  
 PILE CUTOFF ELEV. ===== **733.60** ft  
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = **731.60** ft  
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== **None**  
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft  
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

**MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses**

Maximum Nominal Req'd Bearing of <u>Pile</u>	Maximum Nominal Req'd Bearing of <u>Boring</u>	Maximum Factored Resistance Available in <u>Boring</u>	Maximum Pile Driveable Length in <u>Boring</u>
<b>588</b> KIPS	<b>377</b> KIPS	<b>207</b> KIPS	<b>31</b> FT.

TOTAL FACTORED SUBSTRUCTURE LOAD ===== **830** kips  
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== **37.10** ft  
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== **1**  
 Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 178.98 KIPS  
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 67.12 KIPS

PILE TYPE AND SIZE ===== **Metal Shell 16"Φ w/.312" walls**

Pile Perimeter===== 4.189 FT.  
 Pile End Bearing Area===== 1.396 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL						NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)								
729.10	2.50	3.50	9	Sandy Gravel	28.1		69.4				69	0	0	38	5
726.60	2.50	2.70	9		23.3	41.4	82.0				82	0	0	45	7
724.10	2.50	2.00	4		19.1	30.6	108.7				109	0	0	60	10
721.60	2.50	2.50	6		22.1	38.3	115.5				115	0	0	64	12
719.10	2.50	1.50	2		15.8	23.0	123.6				124	0	0	68	15
716.60	2.50	1.00	2		11.6	15.3	286.9				287	0	0	158	17
714.10	2.50		19		23.5	167.0	244.5				245	0	0	134	20
711.60	2.50	6.60	22		34.1	101.1	281.6				282	0	0	155	22
709.10	2.50	6.80	19		34.1	104.1	306.5				307	0	0	169	25
706.60	2.50	6.20	18		34.1	95.0	337.5				338	0	0	186	27
704.10	2.50	6.00	19	Fine Sand Medium Sand	34.1	91.9	356.3				356	0	0	196	30
702.60	1.50	5.00	16		20.4	76.6	376.8				377	0	0	207	31
701.10	1.50	5.00	16		20.4	76.6	1094.1				4094	0	0	602	33
698.60	2.50		88		156.9	773.5	1119.2				4119	0	0	616	35
696.60	2.00		73		111.3	641.6	645.5				646	0	0	355	37
694.10	2.50	3.70	18		29.3	56.7	680.9				681	0	0	375	40
691.60	2.50	4.10	22		31.7	62.8	746.3				746	0	0	440	42
689.60	2.00	6.30	27		27.3	96.5	746.0				746	0	0	440	44
687.10	2.50	4.50	27		34.1	68.9	780.1				780	0	0	429	47
684.60	2.50	4.50	27		34.1	68.9	814.2				814	0	0	448	49
683.60	1.00	4.50	27	Hard Till Hard Till	13.6	68.9	956.6				957	0	0	526	50
681.10	2.50		30		17.2	197.8	973.8				974	0	0	536	53
678.60	2.50		30		17.2	197.8	846.9				847	0	0	466	55
677.10	1.50	3.50	13			53.6									

**Pile Design Table for South Abutment utilizing Boring #1**

Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)
<b>Metal Shell 16"Φ w/.312" walls</b>			<b>Steel HP 10 X 57</b>			<b>Steel HP 14 X 73</b>		
115	64	12	106	58	20	97	53	15
124	68	15	131	72	22	135	74	17
245	134	20	156	86	25	149	82	20
282	155	22	177	97	27	186	102	22
307	169	25	185	102	30	221	121	25
338	186	27	195	107	31	257	141	27
356	196	30	236	130	37	286	157	30
377	207	31	255	140	40	300	165	31
<b>Metal Shell 16"Φ w/.375" walls</b>			289	159	44	349	192	37
115	64	12	306	168	47	378	208	40
124	68	15	324	178	49	428	235	44
245	134	20	326	179	50	452	249	47
282	155	22	326	179	55	475	261	55
307	169	25	<b>Steel HP 12 X 53</b>			<b>Steel HP 14 X 89</b>		
338	186	27	111	61	17	98	54	15
356	196	30	122	67	20	137	75	17
377	207	31	153	84	22	153	84	20
<b>Metal Shell 14"Φ w/.25" walls</b>			182	100	25	190	105	22
106	59	15	212	117	27	225	124	25
203	112	20	228	126	30	261	144	27
235	129	22	241	132	31	290	159	30
258	142	25	285	157	37	304	167	31
285	157	27	309	170	40	354	195	37
303	167	30	350	192	44	383	211	40
321	177	31	370	204	47	433	238	44
<b>Metal Shell 14"Φ w/.312" walls</b>			391	215	49	458	252	47
106	59	15	392	216	55	481	264	55
203	112	20	<b>Steel HP 12 X 63</b>			<b>Steel HP 14 X 102</b>		
235	129	22	114	63	17	99	55	15
258	142	25	126	69	20	139	76	17
285	157	27	157	86	22	156	86	20
303	167	30	186	103	25	193	106	22
321	177	31	217	119	27	228	126	25
<b>Steel HP 8 X 36</b>			231	127	30	264	145	27
120	66	25	243	134	31	294	162	30
132	73	27	288	159	37	309	170	31
140	77	30	312	171	40	358	197	37
149	82	31	353	194	44	388	213	40
183	101	37	374	206	47	439	241	44
197	109	40	395	217	49	464	255	47
224	123	44	396	218	55	486	268	55
238	131	47	<b>Steel HP 12 X 74</b>			<b>Steel HP 14 X 117</b>		
252	139	49	115	63	17	101	55	15
255	140	50	129	71	20	141	78	17
256	141	55	160	88	22	160	88	20
<b>Steel HP 10 X 42</b>			189	104	25	198	109	22
102	56	20	219	121	27	233	128	25
128	70	22	235	129	30	269	148	27
152	84	25	247	136	31	298	164	30
173	95	27	292	161	37	313	172	31
180	99	30	316	174	40	363	200	37
191	105	31	358	197	44	393	216	40
230	127	37	380	209	47	445	244	44
249	137	40	401	220	49	470	258	47
282	155	44	401	221	55	492	271	55
299	165	47	<b>Steel HP 12 X 84</b>			<b>Precast 14"x 14"</b>		
317	174	49	117	64	17	116	64	10
319	175	50	131	72	20	125	69	12
319	176	55	162	89	22	136	75	15
			192	106	25	<b>Timber Pile</b>		
			222	122	27	111	61	15
			238	131	30	152	84	17
			251	138	31			
			297	163	37			
			321	177	40			
			364	200	44			
			385	212	47			
			406	223	49			
			407	224	55			

SUBSTRUCTURE===== **Pier 1**

REFERENCE BORING ===== **1**

LRFD or ASD or SEISMIC ===== **LRFD**

PILE CUTOFF ELEV. ===== **733.60** ft

GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = **709.90** ft

GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== **Scour**

BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== **709.40** ft

TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

TOTAL FACTORED SUBSTRUCTURE LOAD ===== **1785** kips

TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== **37.10** ft

NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== **1**

Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 384.91 KIPS

Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 144.34 KIPS

**MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses**

Maximum Nominal Req'd Bearing of <u>Pile</u>	Maximum Nominal Req'd Bearing of <u>Boring</u>	Maximum Factored Resistance Available in <u>Boring</u>	Maximum Pile Driveable Length in <u>Boring</u>
<b>588</b> KIPS	<b>579</b> KIPS	<b>319</b> KIPS	<b>47</b> FT.

PILE TYPE AND SIZE ===== **Metal Shell 16"Φ w/.312" walls**

Pile Perimeter===== 4.189 FT.

Pile End Bearing Area===== 1.396 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL						NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)								
707.00	2.90	6.20	18		39.5		39.5				40	0	0	22	27
704.10	2.90	6.00	19		39.5		79.1				79	0	0	43	30
703.35	0.75	5.00	16		10.2		89.3				89	0	0	49	30
702.60	0.75	5.00	16		10.2		99.5				100	0	0	55	31
701.85	0.75	5.00	16		10.2		109.7				110	0	0	60	32
701.60	0.25	5.00	16		3.4		113.1				113	0	0	62	32
701.35	0.25	5.00	16		3.4		116.5				117	0	0	64	32
701.10	0.25	5.00	16		3.4		120.0				120	0	0	66	33
700.85	0.25		88	Fine Sand	15.7		135.6				136	0	0	75	33
700.60	0.25		88	Fine Sand	15.7		151.3				151	0	0	83	33
700.10	0.50		88	Fine Sand	31.4		182.7				183	0	0	100	34
698.60	1.50		88	Fine Sand	94.2		276.9				277	0	0	152	35
697.60	1.00		73	Medium Sand	55.7		332.5				333	0	0	183	36
697.10	0.50		73	Medium Sand	27.8		360.4				360	0	0	198	37
696.60	0.50		73	Medium Sand	27.8		444.9				445	0	0	245	37
694.10	2.50	3.70	18		29.3	56.7	480.3				480	0	0	264	40
691.60	2.50	4.10	22		31.7	62.8	545.6				546	0	0	300	42
689.60	2.00	6.30	27		27.3	96.5	545.3				545	0	0	300	44
687.10	2.50	4.50	27		34.1	68.9	579.4				579	0	0	319	47
684.60	2.50	4.50	27		34.1	68.9	613.5				613	0	0	337	49
683.60	1.00	4.50	27		13.6	68.9	756.0				756	0	0	416	50
681.10	2.50		30	Hard Till	17.2	197.8	773.2				773	0	0	426	53
678.60	2.50		30	Hard Till	17.2	197.8	646.2				646	0	0	355	55
677.10	1.50	3.50	13		16.8	53.6	663.1				663	0	0	365	57
674.60	2.50	3.50	13		28.1	53.6	691.1				691	0	0	380	59
672.10	2.50	3.50	13		28.1	53.6	719.2				719	0	0	396	62
669.60	2.50	3.50	13			53.6									

**Pile Design Table for Pier 1 utilizing Boring #1**

Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)
<b>Metal Shell 16"Φ w/.312" walls</b>			<b>Steel HP 10 X 57</b>			<b>Steel HP 14 X 73</b>		
183	100	34	255	140	59	246	135	40
277	152	35	269	148	62	294	162	42
333	183	36	<b>Steel HP 12 X 53</b>			296	163	44
360	198	37	259	142	47	320	176	47
445	245	37	279	154	49	343	188	55
480	264	40	280	154	55	355	195	57
545	300	44	291	160	57	375	206	59
579	319	47	308	169	59	395	217	62
<b>Metal Shell 16"Φ w/.375" walls</b>			325	178	62	<b>Steel HP 14 X 89</b>		
183	100	34	<b>Steel HP 12 X 63</b>			249	137	40
277	152	35	262	144	47	299	165	42
333	183	36	282	155	49	300	165	44
360	198	37	283	156	55	325	178	47
445	245	37	293	161	57	347	191	55
480	264	40	311	171	59	359	198	57
545	300	44	328	180	62	380	209	59
579	319	47	<b>Steel HP 12 X 74</b>			400	220	62
613	337	49	245	135	44	<b>Steel HP 14 X 102</b>		
<b>Metal Shell 14"Φ w/.25" walls</b>			266	146	47	253	139	40
242	133	35	287	158	49	303	166	42
291	160	36	287	158	55	304	167	44
315	173	37	298	164	57	329	181	47
383	211	37	315	173	59	351	193	55
<b>Metal Shell 14"Φ w/.312" walls</b>			332	183	62	364	200	57
242	133	35	<b>Steel HP 12 X 84</b>			384	211	59
291	160	36	248	137	44	405	223	62
315	173	37	270	148	47	<b>Steel HP 14 X 117</b>		
383	211	37	291	160	49	256	141	40
413	227	40	291	160	55	308	169	42
467	257	42	302	166	57	308	169	44
470	258	44	320	176	59	333	183	47
499	275	47	337	185	62	356	196	55
<b>Steel HP 8 X 36</b>						368	203	57
210	115	62				389	214	59
<b>Steel HP 10 X 42</b>						410	225	62
249	137	59				<b>Precast 14"x 14"</b>		
263	145	62				204	112	34
						<b>Timber Pile</b>		
						151	83	33

SUBSTRUCTURE===== Pier 2  
REFERENCE BORING ===== 2  
LRFD or ASD or SEISMIC ===== LRFD  
PILE CUTOFF ELEV. ===== 732.50 ft  
GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 709.90 ft  
GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== Scour  
BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== 709.40 ft  
TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft  
  
TOTAL FACTORED SUBSTRUCTURE LOAD ===== 1785 kips  
TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 37.10 ft  
NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 1  
Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 384.91 KIPS  
Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 144.34 KIPS

**MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses**

Maximum Nominal Req'd Bearing of <u>Pile</u>	Maximum Nominal Req'd Bearing of <u>Boring</u>	Maximum Factored Resistance Available in <u>Boring</u>	Maximum Pile Driveable Length in <u>Boring</u>
<b>704</b> KIPS	<b>561</b> KIPS	<b>309</b> KIPS	<b>50</b> FT.

PILE TYPE AND SIZE ===== Metal Shell 16"Φ w/.375" walls  
Pile Perimeter===== 4.189 FT.  
Pile End Bearing Area===== 1.396 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL						NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)								
707.40	2.50	5.30	17		34.1		104.5				105	0	0	57	25
704.90	2.50	4.60	14		34.1	70.5	130.9				131	0	0	72	28
702.40	2.50	4.10	21		31.7	62.8	469.0				469	0	0	258	30
699.90	2.50		56	Sandy Gravel	153.3	369.2	317.4				317	0	0	175	33
697.40	2.50	4.20	13		32.3	64.3	378.8				379	0	0	208	35
694.90	2.50	6.10	9		34.1	93.4	412.9				413	0	0	227	38
692.40	2.50	6.10	13		34.1	93.4	447.0				447	0	0	246	40
689.90	2.50	6.10	18		34.1	93.4	470.3				470	0	0	259	43
687.40	2.50	5.40	15		34.1	82.7	502.9				503	0	0	277	45
684.90	2.50	5.30	14		34.1	81.2	533.9				534	0	0	294	48
683.90	1.00	5.10	16		13.6	78.1	547.5				548	0	0	301	49
683.40	0.50	5.10	16		6.8	78.1	554.3				554	0	0	305	49
682.90	0.50	5.10	16		6.8	78.1	561.1				561	0	0	309	50
682.40	0.50	5.10	16		6.8	78.1	815.1				815	0	0	448	50
679.90	2.50		37	Sandy Gravel	63.2	325.2	895.8				896	0	0	493	53
677.90	2.00		39	Sandy Gravel	56.3	342.8	1040.1				1040	0	0	572	55
675.40	2.50		49	Sandy Gravel		430.7									

**Pile Design Table for Pier 2 utilizing Boring #2**

Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)
<b>Metal Shell 16"Φ w/.312" walls</b>			<b>Steel HP 10 X 57</b>			<b>Steel HP 14 X 73</b>		
131	72	28	262	144	50	240	132	38
317	175	33	276	152	53	276	152	40
379	208	35	302	166	55	306	168	43
413	227	38	<b>Steel HP 12 X 53</b>			329	181	45
447	246	40	245	135	43	349	192	48
470	259	43	264	145	45	359	198	49
503	277	45	282	155	48	364	200	49
534	294	48	290	160	49	369	203	50
548	301	49	294	162	49	402	221	50
554	305	49	298	164	50	423	233	53
561	309	50	323	178	50	466	256	55
<b>Metal Shell 16"Φ w/.375" walls</b>			340	187	53	<b>Steel HP 14 X 89</b>		
131	72	28	375	206	55	245	135	38
317	175	33	<b>Steel HP 12 X 63</b>			281	155	40
379	208	35	248	136	43	311	171	43
413	227	38	267	147	45	333	183	45
447	246	40	285	157	48	354	195	48
470	259	43	293	161	49	364	200	49
503	277	45	297	164	49	369	203	49
534	294	48	302	166	50	374	206	50
548	301	49	326	180	50	408	224	50
554	305	49	343	189	53	429	236	53
561	309	50	379	208	55	474	261	55
<b>Metal Shell 14"Φ w/.25" walls</b>			<b>Steel HP 12 X 74</b>			<b>Steel HP 14 X 102</b>		
108	59	28	252	138	43	248	136	38
271	149	33	271	149	45	284	156	40
321	177	35	289	159	48	315	173	43
351	193	38	298	164	49	338	186	45
381	209	40	302	166	49	359	197	48
402	221	43	306	168	50	369	203	49
<b>Metal Shell 14"Φ w/.312" walls</b>			332	182	50	374	206	49
108	59	28	349	192	53	379	208	50
271	149	33	385	212	55	414	228	50
321	177	35	<b>Steel HP 12 X 84</b>			435	239	53
351	193	38	256	141	43	479	263	55
381	209	40	276	152	45	<b>Steel HP 14 X 117</b>		
402	221	43	294	162	48	252	139	38
431	237	45	302	166	49	289	159	40
459	252	48	307	169	49	320	176	43
471	259	49	311	171	50	343	189	45
476	262	49	337	185	50	364	200	48
482	265	50	354	195	53	374	206	49
<b>Steel HP 8 X 36</b>			392	215	55	379	208	49
228	126	55				384	211	50
<b>Steel HP 10 X 42</b>						420	231	50
256	141	50				441	243	53
269	148	53				486	267	55
295	162	55				<b>Precast 14"x 14"</b>		
						137	75	28
						<b>Timber Pile</b>		
						80	44	28

SUBSTRUCTURE===== **North Abutment**  
 REFERENCE BORING ===== **2**  
 LRFD or ASD or SEISMIC ===== **LRFD**  
 PILE CUTOFF ELEV. ===== **732.50** ft  
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = **730.50** ft  
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== **None**  
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft  
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

**MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses**

Maximum Nominal Req'd Bearing of <u>Pile</u>	Maximum Nominal Req'd Bearing of <u>Boring</u>	Maximum Factored Resistance Available in <u>Boring</u>	Maximum Pile Driveable Length in <u>Boring</u>
<b>588</b> KIPS	<b>331</b> KIPS	<b>182</b> KIPS	<b>28</b> FT.

TOTAL FACTORED SUBSTRUCTURE LOAD ===== **830** kips  
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== **37.10** ft  
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== **1**  
 Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 178.98 KIPS  
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 67.12 KIPS

PILE TYPE AND SIZE ===== **Metal Shell 16"Φ w/.312" walls**

Pile Perimeter===== 4.189 FT.  
 Pile End Bearing Area===== 1.396 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL						NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)								
729.90	0.60	1.50	4	Hard Till	3.8		26.8				27	0	0	15	3
727.40	2.50	1.50	4		15.8	23.0	50.2				50	0	0	28	5
724.90	2.50	2.00	5		19.1	30.6	69.3				69	0	0	38	8
722.40	2.50	2.00	7		19.1	30.6	96.0				96	0	0	53	10
719.90	2.50	2.50	8		22.1	38.3	170.2				170	0	0	94	13
717.40	2.50	5.90	20		34.1	90.4	242.5				243	0	0	133	15
714.40	3.00	8.40	27		40.9	128.6	365.7				366	0	0	201	18
711.90	2.50		32		18.4	211.0	295.7				296	0	0	163	21
709.40	2.50	8.00	24		34.1	122.5	288.5				288	0	0	159	23
707.40	2.00	5.30	20		27.3	81.2	305.0				305	0	0	168	25
704.90	2.50	4.60	19	Sandy Gravel	34.1	70.5	331.4				331	0	0	182	28
702.40	2.50	4.10	19		31.7	62.8	792.5				793	0	0	436	30
699.90	2.50		56		153.3	492.2	517.9				518	0	0	285	33
697.40	2.50	4.20	20		32.3	64.3	579.3				579	0	0	319	35
694.90	2.50	6.10	24		34.1	93.4	613.4				613	0	0	337	38
692.40	2.50	6.10	25		34.1	93.4	647.4				647	0	0	356	40
689.90	2.50	6.10	25		34.1	93.4	670.8				671	0	0	369	43
687.40	2.50	5.40	21		34.1	82.7	703.3				703	0	0	387	45
684.90	2.50	5.30	15		34.1	81.2	734.4				734	0	0	404	48
682.40	2.50	5.10	19		34.1	78.1	1015.5				1016	0	0	550	50
679.90	2.50		37	Sandy Gravel	63.2	325.2	1096.3				1096	0	0	603	53
677.40	2.50		39	Sandy Gravel	70.4	342.8	1254.6				1255	0	0	690	55
675.40	2.00		49	Sandy Gravel		430.7									

**Pile Design Table for North Abutment utilizing Boring #2**

Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)
<b>Metal Shell 16"Φ w/.312" walls</b>			<b>Steel HP 10 X 57</b>			<b>Steel HP 14 X 73</b>		
96	53	10	122	67	18	97	53	13
170	94	13	133	73	21	139	76	15
243	133	15	152	84	23	174	95	18
288	159	23	159	88	25	187	103	21
305	168	25	172	95	28	218	120	23
331	182	28	214	117	33	246	135	25
<b>Metal Shell 16"Φ w/.375" walls</b>			249	137	35	263	144	28
96	53	10	266	147	38	321	177	33
170	94	13	284	156	40	381	210	35
243	133	15	295	162	43	406	223	38
288	159	23	311	171	45	430	237	40
305	168	25	327	180	48	441	243	43
331	182	28	359	197	50	463	255	45
<b>Metal Shell 14"Φ w/.25" walls</b>			372	205	53	484	266	48
80	44	10	401	221	55	537	295	50
139	76	13	<b>Steel HP 12 X 53</b>			558	307	53
198	109	15	113	62	15	<b>Steel HP 14 X 89</b>		
244	134	23	143	79	18	101	55	13
259	143	25	154	85	21	143	79	15
283	156	28	180	99	23	177	97	18
<b>Metal Shell 14"Φ w/.312" walls</b>			198	109	25	192	106	21
80	44	10	211	116	28	222	122	23
139	76	13	261	143	33	250	137	25
198	109	15	306	168	35	266	146	28
244	134	23	327	180	38	326	179	33
259	143	25	348	191	40	387	213	35
283	156	28	358	197	43	411	226	38
<b>Steel HP 8 X 36</b>			378	208	45	436	240	40
120	66	25	396	218	48	447	246	43
131	72	28	<b>Steel HP 12 X 63</b>			469	258	45
164	90	33	117	64	15	490	270	48
190	104	35	147	81	18	544	299	50
204	112	38	158	87	21	565	311	53
218	120	40	184	101	23	616	339	55
227	125	43	200	110	25	<b>Steel HP 14 X 102</b>		
241	132	45	214	117	28	103	57	13
253	139	48	263	145	33	147	81	15
277	152	50	310	170	35	179	98	18
<b>Steel HP 10 X 42</b>			330	182	38	196	108	21
119	65	18	351	193	40	225	124	23
129	71	21	362	199	43	252	139	25
148	82	23	381	210	45	270	148	28
155	86	25	399	220	48	330	181	33
168	92	28	441	243	50	392	216	35
209	115	33	458	252	53	417	229	38
243	134	35	496	273	55	442	243	40
260	143	38	<b>Steel HP 12 X 74</b>			453	249	43
277	153	40	120	66	15	476	262	45
288	158	43	149	82	18	496	273	48
304	167	45	162	89	21	551	303	50
319	176	48	187	103	23	573	315	53
			203	112	25	625	343	55
			217	119	28	<b>Steel HP 14 X 117</b>		
			267	147	33	106	58	13
			315	173	35	152	83	15
			336	185	38	182	100	18
			357	196	40	201	111	21
			368	202	43	229	126	23
			387	213	45	256	141	25
			405	223	48	274	151	28
			448	246	50	334	184	33
			465	256	53	397	219	35
			504	277	55	423	232	38
			<b>Steel HP 12 X 84</b>			448	246	40
			86	48	13	459	252	43
			123	68	15	482	265	45
			150	83	18	503	277	48
			165	91	21	558	307	50
			189	104	23	580	319	53
			206	114	25	633	348	55
			220	121	28	<b>Precast 14"x 14"</b>		
			271	149	33	102	56	10
			319	176	35	177	97	13
			341	187	38	252	139	15
			362	199	40	<b>Timber Pile</b>		
			373	205	43	97	53	13
			393	216	45	138	76	15
			411	226	48			
			454	250	50			
			472	260	53			
			512	281	55			