

# STRUCTURE GEOTECHNICAL REPORT

**Proposed SN 083-7102**  
**Existing SN 083-7067**

**US Route 45 over Unnamed Stream**  
**FAP Route 881**  
**Section 32B-2**  
**Saline County**



*2-28-2020*

**PTB 157 - Item 46**  
**Contract No. 78501**  
**Job No. D-99-061-15**

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## **Project Description and Scope**

This project involves the complete replacement of an existing structure near the intersection of US Route 45 and TR 184 (Feazel Road) carrying traffic over an unnamed stream, located in Saline County. The project site is located in Section 28, Range 6E, Township 9S, in the 3<sup>rd</sup> Principal Meridian, about 1.5 miles southwest of the US 45 and IL 34 Junction. A *Location Map* is presented in Exhibit A.

The existing culvert on US Route 45, SN 083-7067, was constructed in 1921. It is a double barrel 8' span x 5' rise concrete box culvert with parallel wing walls. The culvert measures 31'-4" long, with no skew. In 2013 the north headwall was stabilized using steel piles.

Per the preliminary Type, Size & Location Plan (TSL), the proposed structure on US Route 45, SN 083-7102, is a double barrel concrete box culvert with horizontal cantilever wing walls. The proposed structure will be 45'-6" long out to out headwalls, with no skew. The maximum fill height will be approximately 3.1 feet above the proposed culvert.

The structure is adjacent to the intersection of US 45 and Feazel Road. Both roads are on a horizontal tangent alignment and on a vertically tangent section of roadway. Guardrail will be provided at each end the culvert. It is anticipated that the adjacent proposed culvert carrying Feazel Road over Pankey Branch, SN 083-2018, will be constructed as part of the same contract. The southeast wing wall of SN 083-7102 will intersect with the northwest wing wall of SN 083-2018. Traffic on US 45 will be maintained utilizing stage construction, while Feazel Road will be closed during construction of SN 083-2018. The new structure is to be designed following LRFD Bridge Design Specifications.

See *Preliminary TSL* attached in Exhibit B for further information about the proposed structures.

## **Field Exploration**

### **Subsurface Exploration and Testing**

The site is located in a rural area on the south edge of Harrisburg, IL with a wooded area located at the northwest quadrant, farm fields located to the south, and commercial buildings with gravel parking lots located to the north. Drainage from an unnamed stream flows from north to south beneath US Route 45 where it intersects Pankey Branch, and then flows west to east beneath Feazel Road. Overhead power lines cross US Route 45 at this location, running parallel to and just west of Feazel Road.

The subsurface investigation consisted of two borings (1-S and 2-S) drilled by IDOT District 9 personnel in October 2019. 1-S was west of the proposed culvert and within the north lane of US 45; 2-S was drilled just east of the proposed culvert within the south lane of US 45. Boring locations can be found in Exhibit B.

Beginning at the ground surface, standard penetration tests (SPT) were conducted every 2.5 feet according to AASHTO T 206, using a Hollow Stem Auger. Borings 1-S and 2-S were terminated in stiff clay at depths of approximately 30 feet.

## **Subsurface Conditions**

While drilling, groundwater was encountered at an elevation of 344.8 with surface water elevation at 366.4.

Layers of silty clay loam, silty loam and clay are present down to elevation 344.3 where the borings were terminated. These cohesive layers have  $Q_u$  values ranging from 0.1 tsf to 2.7 tsf.

Further descriptions of the soil conditions encountered in the borings are presented in the *Soil Borings* attached in Exhibit D and the *Subsurface Data Profile* in Exhibit C.

## **Geotechnical Evaluations**

### **Settlement**

No significant roadway profile change is expected at this structure. The proposed culvert on US 45 (SN 083-7102) will be extended outside the limits of the existing culvert, which will increase pressure at the culvert ends due to the new culvert and fill weight.

The amount of differential settlement expected on the currently unloaded soils ranges from 1.08 inches to 0.85 inches (Boring 2-S and 1-S respectively), assuming the soil will be removed down to an elevation of 362 and replaced with Rock Fill – Foundation in order to allow for the desired removal and replacement of unsuitable material. Refer to Ground Improvement recommendations within the Construction Considerations section of this report.

### **Slope Stability**

Preliminary stability analyses using Bishop's method were performed for both structures. According to AASHTO LRFD 11.6.2.3, the required resistance factor for slope stability is 0.65 which is equivalent to factor of safety of 1.54. SN 083-7102 used a 10.7' high 1:1 temporary excavation end slope model which rendered factor of safety of 2.79. Slope stability analyses are presented in Exhibit F. No slope stability problems are expected.

### **Seismic Considerations**

Per the IDOT Culvert Manual and Article 3.10.1 of the AASHTO LRFD Bridge Design Specifications, buried structures are not designed for seismic effects. The wing walls are considered part of the buried structures and therefore are not designed for seismic loading either.

### **Scour**

Per IDOT All Bridge Designer Memorandum 14.2, the Design Scour Elevation table is not required for closed bottom box culverts.

### **Mining Activity**

A review of the Illinois State Geological Survey (ISGS) "Directory of Coal Mines in Illinois" for Saline County indicates that mining activity has been present near the project

location. The nearest coal mine point is approximately 0.3 miles southwest of the structure location.

### **Foundation Recommendations**

#### **Culvert Barrels**

A 3-sided structure is not desired at this location due to the the estimated differential settlement.

A cast in place culvert appears to be the most appropriate construction option for the given site conditions and due to the need for cast in place wing walls and head walls. The precast option is not recommended due to the staging requirements of SN 083-7102 and the amount of anticipated differential settlement.

With the large foundation footprint of the box culvert, along with the Rock Fill – Foundation material being placed beneath the culvert, the allowable bearing capacity at the base of foundation was found to be more than adequate for resisting estimated pressures.

#### **Wing Walls**

Per the 2017 IDOT Culvert Manual, horizontal cantilever wing walls are the most economical and preferred wall type for most cast in place concrete box culverts, with a proposed wall length limited to 16 feet. The Preliminary TSL plans indicate all wall lengths are under 16 feet.

#### **Hydraulics**

Class A4 Stone Riprap shall be provided at each end of the culvert as a scour countermeasure. The Estimated Water Surface Elevation (EWSE) during construction is 366.5.

### **Construction Considerations**

#### **Cofferdams**

Considering the EWSE of 366.5, the structure can be constructed using conventional methods of water diversion determined by the Contractor.

#### **Stage Construction**

In order to maintain traffic along US 45, stage construction shall be utilized on SN 083-7102. Temporary Sheet Piling is proposed to retain existing soil along the stage line adjacent to the existing and proposed culverts. A 1:1 slope will be provided between the existing roadway and stage removal line. A geotextile retaining wall will retain the proposed roadway during construction.

#### **Temporary Soil Retention**

Temporary sheet piling appears to be a suitable option to retain excavation and backfill areas during construction along US 45. Using a retained height of 11 feet, it's estimated that a minimum section modulus of 8.05 in<sup>3</sup>/ft be used with a minimum embedment of 8.25 ft.

### **Excavation**

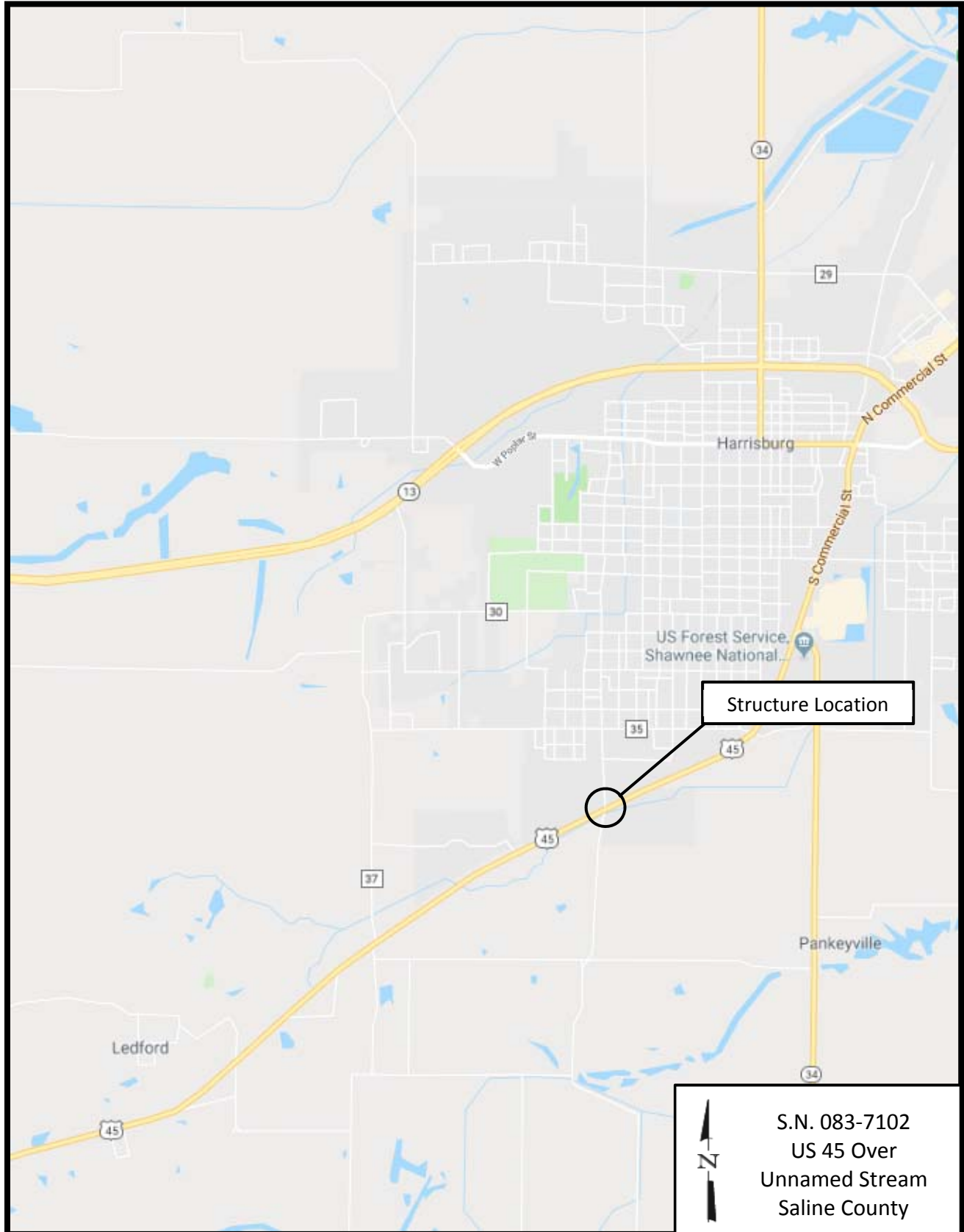
A 1:1.5 temporary excavation slope for construction clearance has an adequate factor of safety. The factor of safety is limited to 1:1.5 slopes and any steeper slopes are not recommended.

### **Ground Improvement**

Since SN 083-7102 will primarily be supported on pre-loaded soil with only the culvert ends on currently unloaded soil, the bottom slab is considered rigid enough to not cause major structural issues due to differential settlement. To mitigate the potential differential settlement, it's recommended to provide 3 feet of removal of unsuitable material and replacement with Rock Fill – Foundation beneath the proposed slab.

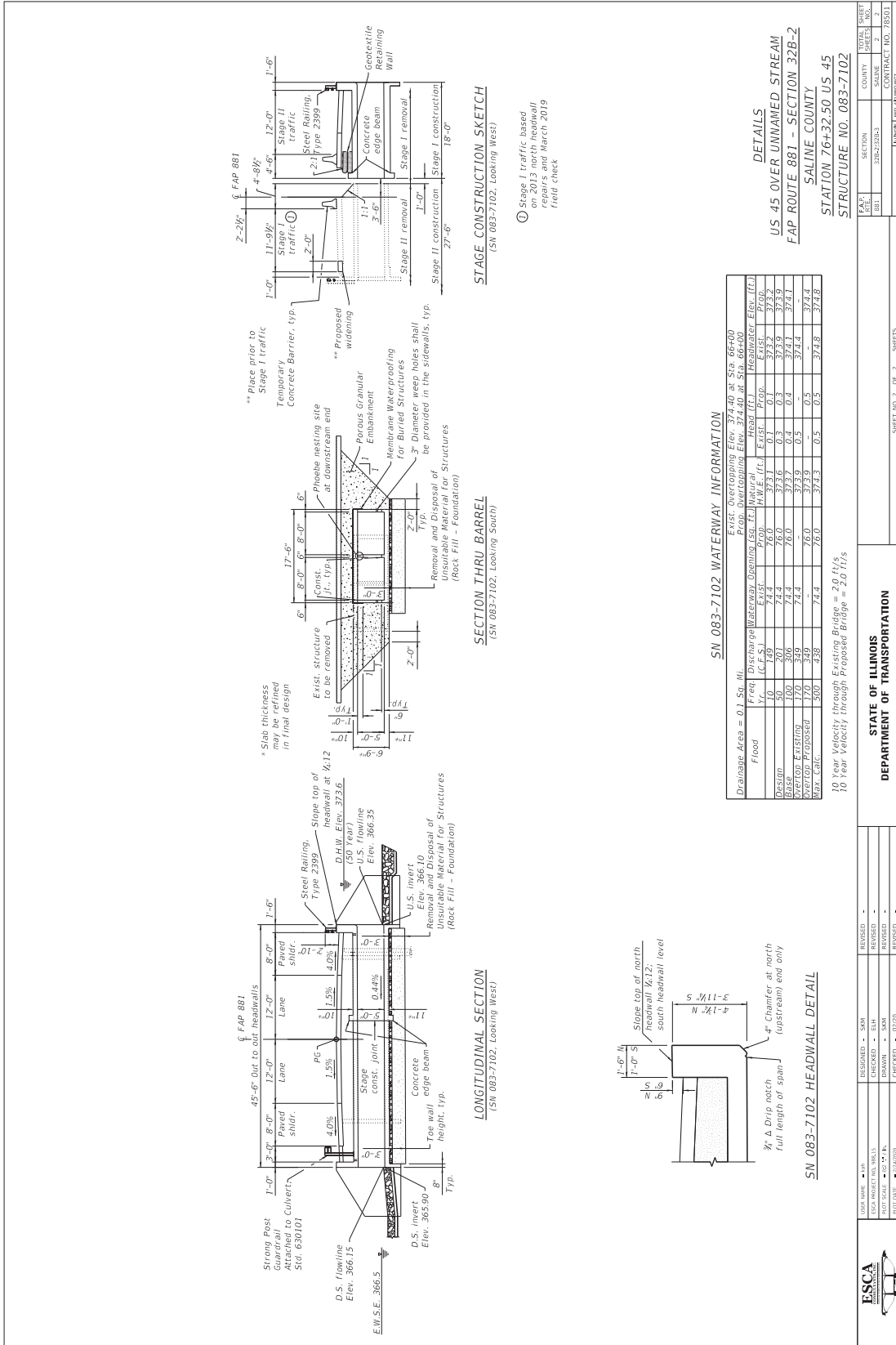
### **Limitations**

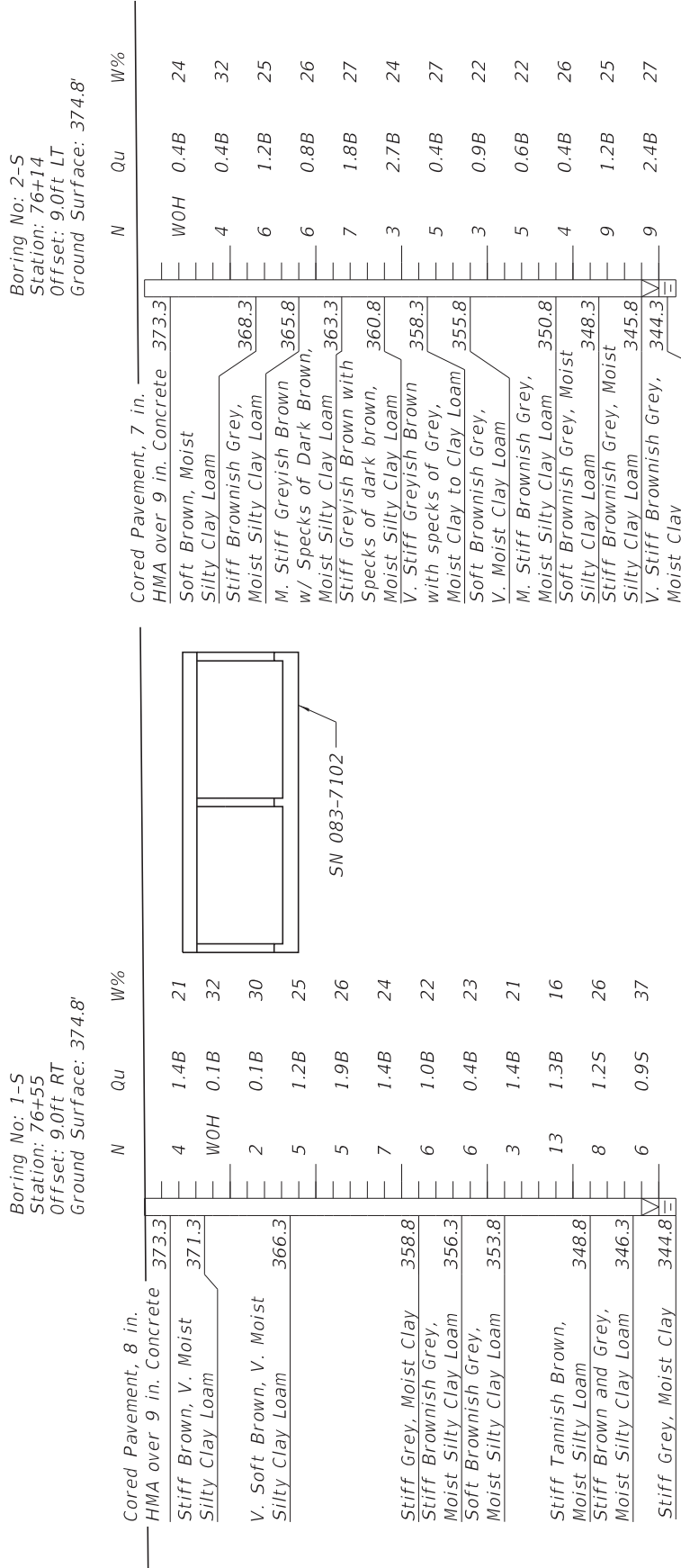
The recommendations provided herein are for the exclusive use of IDOT and ESCA Consultants, Inc. They are specific only to the project described, and are based on subsurface information obtained at boring locations within the bridge area, our understanding of the project as described herein, and geotechnical engineering practice consistent with the standard of care. No other warranty is expressed or implied. Lin Engineering, Ltd. should be contacted if conditions encountered during construction are not consistent with those described.











Legend

▽ Ground Water at Completion





**Illinois Department of Transportation**  
Division of Highways  
District 9

# SOIL BORING LOG

Page 1 of 1

Date 10/1/19

ROUTE US 45 DESCRIPTION Double barrel 8'x5' box culvert/stream LOGGED BY L. Estel

SECTION 32B-3;32B-2 LOCATION Near Feazel St S of Harrisburg, SEC. 28, TWP. 9S, RNG. 6E, PM

COUNTY Saline DRILLING METHOD Hollow stem auger (8" O.D., 3.25" I.D.) HAMMER TYPE Auto SPT 140 lbs

STRUCT. NO. 083-7067 DEPTH (ft) BLOW S (tsf) M O I S  
Station 70+32  
BORING NO. 2-S DEPTH (ft) BLOW S (tsf) M O I S  
Station 76+14  
Offset 9.0ft LT  
Ground Surface Elev. 374.8 ft

Surface Water Elev. N/A ft  
Stream Bed Elev. 366.4 ft  
Groundwater Elev.:  
▽ First Encounter 344.8 ft  
▽ Upon Completion 344.8 ft  
▽ After      Hrs.      ft

DEPTH (ft)	BLOW S (tsf)	M O I S (%)	DESCRIPTION	DEPTH (ft)	BLOW S (tsf)	M O I S (%)	DESCRIPTION
373.30			Cored Pavement, 7 in. HMA over 9 in. CONCRETE		2	B	M. Stiff Brownish Grey, Moist SILTY CLAY LOAM (continued)
					1		
			Soft Brown, Moist SILTY CLAY LOAM		2	0.6	22
					3	B	
				350.80			
					1		Soft Brownish Grey, Moist SILTY CLAY LOAM
					1	0.4	26
					3	B	
368.30			Stiff Brownish Grey, Moist SILTY CLAY LOAM	348.30			Stiff Brownish Grey, Moist SILTY CLAY LOAM
					1		
					4	1.2	25
					5	B	
365.80			M. Stiff Greyish Brown with specks of dark Brown, Moist SILTY CLAY LOAM	345.80			V. Stiff Brownish Grey, Moist CLAY
					1		
					4	2.4	27
					5	B	
363.30			Stiff Greyish Brown with specks of dark Brown, Moist SILTY CLAY LOAM				Bottom of hole @ 30.5 ft
							Ground surface elevation calculated from Contract 78501 plan sheets
							To convert "N" values to "N60", multiply by 1.5
360.80			V. Stiff Greyish Brown with specks of Grey, Moist CLAY TO CLAY LOAM				
					1	2.7	24
					2	B	
358.30			Soft Brownish Grey, V. Moist CLAY LOAM				
					1		
					2	0.4	27
					3	B	
355.80			M. Stiff Brownish Grey, Moist SILTY CLAY LOAM				
					1	0.9	22

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer, E-Estimated) Abbreviations W.O.H - Sampler Advanced By Weight of Hammer, W.O.P - Advanced by Weight of Pipe, B.S. - Before Seating The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206) BBS, from 137 (Rev. 8-99)

File Name S:\MATERIALS GEOTECHNICAL UNIT\BORING LOGS USING GINT\STATE STRUCTURES\SALINE\083-7067.GPJ Data Template D6\TEMPLATE.GDT Date Printed 10/23/19 Latitude Longitude Datum NAD83 Job Number



**COHESIVE SOIL SETTLEMENT ESTIMATE**

LOCATION AND BORING USED ===== Boring 1-S  
 TYPE OF SURCHARGE ===== 2 (1=2:1 bridge cone, 2=continuous embank., 3=rectangular surch.)  
 DEPTH TO WATER TABLE (below top of existing embankment) == 8.4 FT

NEW EMBANKMENT:  
 NEW EMBANKMENT FILL UNIT WEIGHT ===== 75.6 PCF  
 NEW EMBANKMENT FILL HEIGHT ===== 9.9 FT  
 PROPOSED WIDTH AT TOP ===== 45.5 FT  
 PROPOSED WIDTH AT BOTTOM ===== 45.5 FT (which is a 0.0:1 slope)

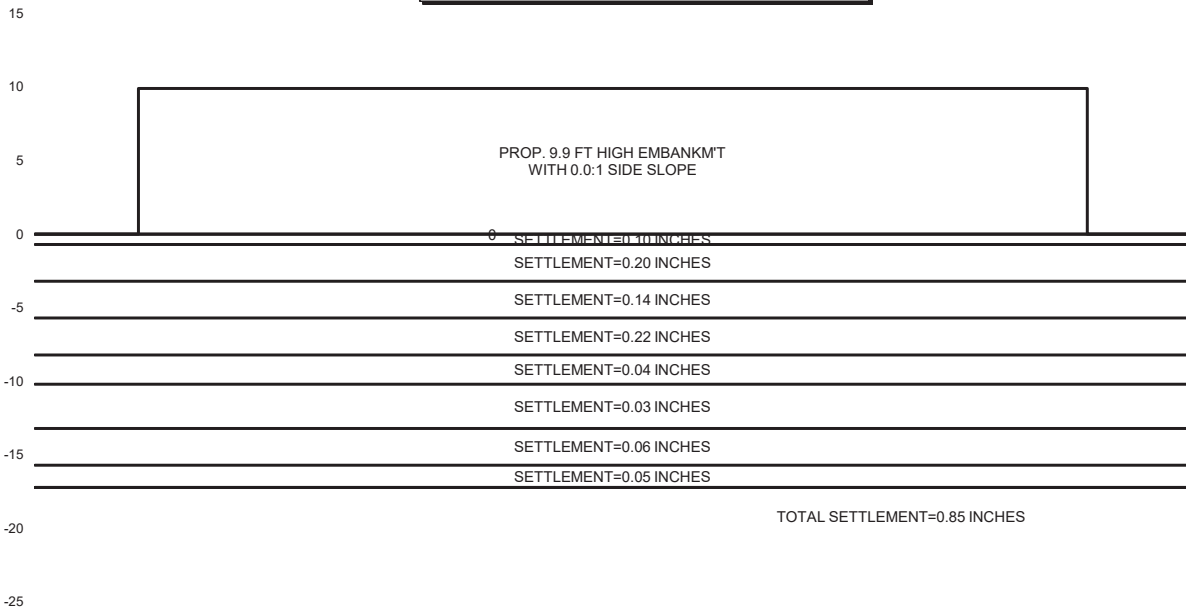
**ASSUMPTIONS:**  
 Soil Deposit is Normally Consolidated  
 Cohesive Layers are Saturated  
 Soils have a Low Sensitivity  
 Liquid Limit (LL)=Moist. Content (MC%)  
 Initial Void Ratio (Eo)=2.7\*(MC%)/100  
 Comp. Index (Cc)=0.009\*(LL-10)  
 Neglecting Granular & Secondary Settlement

EXISTING EMBANKMENT (IF ANY):  
 EXISTING EMBANKMENT UNIT WEIGHT ===== 0 PCF  
 EXISTING EMBANKMENT HEIGHT ===== 0 FT  
 EXISTING WIDTH AT TOP ===== 0 FT  
 EXISTING WIDTH AT BASE ===== 0 FT (which is a 0.0:1 slope)

LAYER THICK (FT)	TOTAL UNIT WT. (PCF)	UNCONF. STRENGTH (TSF)	COMP. (Qu)	MOIST. CONTENT (%)	EXISTING PRESSURE (KSF)	PRESSURE INCREASE (KSF)	INITIAL VOID RATIO	COMPRESSION INDEX (Cc)	Qu CORRECTION FACTOR	LAYER SETTLEMENT (IN.)
0.7	129.1	1.90	26	26	0.045	0.741	0.702	0.144	0.116	0.10
2.5	125.4	1.40	24	24	0.247	0.708	0.648	0.126	0.150	0.20
2.5	121.5	1.00	22	22	0.556	0.656	0.594	0.108	0.200	0.14
2.5	111.4	0.40	23	23	0.847	0.607	0.621	0.117	0.436	0.22
2.0	125.4	1.40	21	21	1.062	0.565	0.567	0.099	0.150	0.04
3.0	124.6	1.30	16	16	1.218	0.522	0.432	0.054	0.160	0.03
2.5	123.6	1.20	26	26	1.388	0.479	0.702	0.144	0.171	0.06
1.5	120.3	0.90	37	37	1.508	0.450	0.999	0.243	0.219	0.05

TOTAL SETTLEMENT UNDER CENTER OF CONTINUOUS EMBANKMENT = 0.85 IN.

EMBANKMENT AND SOIL PROFILE





**COHESIVE SOIL SETTLEMENT ESTIMATE**

LOCATION AND BORING USED ===== Boring 2-S  
 TYPE OF SURCHARGE ===== 2 (1=2:1 bridge cone, 2=continuous embank., 3=rectangular surch.)  
 DEPTH TO WATER TABLE (below top of existing embankment) == 8.4 FT

NEW EMBANKMENT:  
 NEW EMBANKMENT FILL UNIT WEIGHT ===== 75.6 PCF  
 NEW EMBANKMENT FILL HEIGHT ===== 9.9 FT  
 PROPOSED WIDTH AT TOP ===== 45.5 FT  
 PROPOSED WIDTH AT BOTTOM ===== 45.5 FT (which is a 0.0:1 slope)

**ASSUMPTIONS:**  
 Soil Deposit is Normally Consolidated  
 Cohesive Layers are Saturated  
 Soils have a Low Sensitivity  
 Liquid Limit (LL)=Moist. Content (MC%)  
 Initial Void Ratio (Eo)=2.7\*(MC%)/100  
 Comp. Index (Cc)=0.009\*(LL-10)  
 Neglecting Granular & Secondary Settlement

EXISTING EMBANKMENT (IF ANY):  
 EXISTING EMBANKMENT UNIT WEIGHT ===== 0 PCF  
 EXISTING EMBANKMENT HEIGHT ===== 0 FT  
 EXISTING WIDTH AT TOP ===== 0 FT  
 EXISTING WIDTH AT BASE ===== 0 FT (which is a 0.0:1 slope)

LAYER THICK (FT)	TOTAL UNIT WT. (PCF)	UNCONF. STRENGTH (TSF)	COMP. (TSF)	MOIST. CONTENT (%)	EXISTING PRESSURE (KSF)	PRESSURE INCREASE (KSF)	INITIAL VOID RATIO	COMPRESSION INDEX (Cc)	Qu CORRECTION FACTOR	LAYER SETTLEMENT (IN.)
1.2	128.5	1.80	27	27	0.077	0.736	0.729	0.153	0.121	0.16
2.5	133.5	2.70	24	24	0.321	0.697	0.648	0.126	0.100	0.11
2.5	111.4	0.40	27	27	0.627	0.646	0.729	0.153	0.436	0.36
2.0	120.3	0.90	22	22	0.887	0.602	0.594	0.108	0.219	0.08
3.0	115.7	0.60	22	22	1.099	0.556	0.594	0.108	0.309	0.13
2.5	111.4	0.40	26	26	1.241	0.510	0.702	0.144	0.436	0.17
2.5	123.6	1.20	25	25	1.378	0.471	0.675	0.135	0.171	0.05
1.5	132	2.40	27	27	1.507	0.443	0.729	0.153	0.100	0.02

TOTAL SETTLEMENT UNDER CENTER OF CONTINUOUS EMBANKMENT = 1.08 IN.

EMBANKMENT AND SOIL PROFILE

