

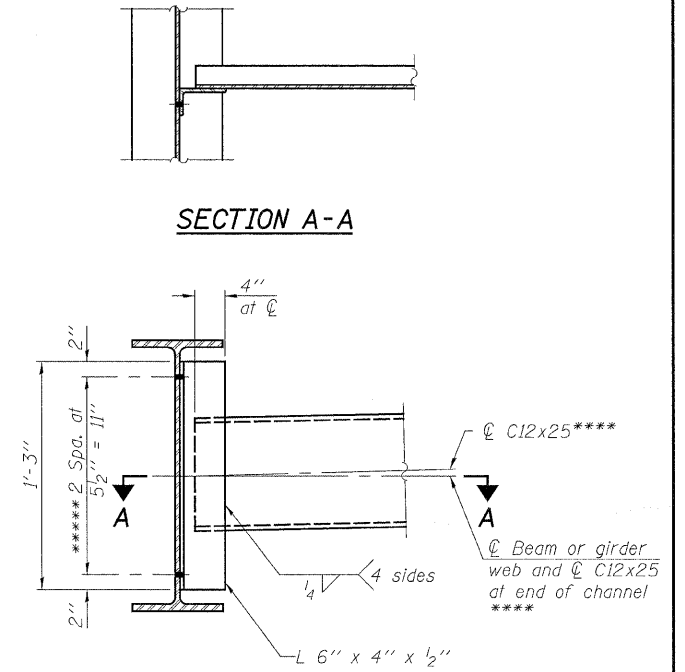
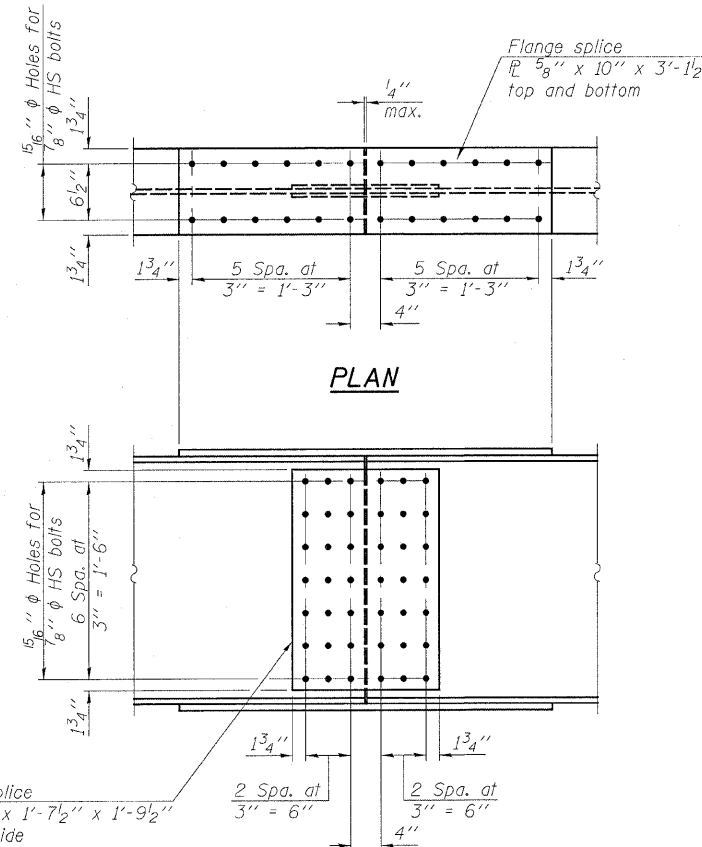
STATE OF ILLINOIS
DEPARTMENT OF TRANSPORTATION

ROUTE NO. 328	SECTION (8BR-2) B-1	COUNTY WAYNE	TOTAL SHEETS 140	SHEET NO. 37	SHEET NO. 15 25 SHEETS
F.A.P.		ILLINOIS		FED. AID PROJECT	

Contract #74040

	0.4 Sp. 1 or 0.6 Sp. 3	Pier 1 or Pier 2	0.5 Sp. 2
I_s	3620	3620	3620
$I_c(n)$	10361	-	10361
$I_c(3n)$	7792	-	7792
S_s	267	267	267
$S_c(n)$	400	-	400
$S_c(3n)$	365	-	365
Z	305	305	305
ρ	0.807	0.807	0.807
$M\phi$	128.0	245.3	130.4
$s\phi$	0.483	0.483	0.483
$M_s\phi$	86.3	122.6	102.2
$M\phi$	343.9	196.4	393.6
M_{Imp}	99.7	55.0	106.3
$s_3 [M\phi + M_{Imp}]$	739.3	419.0	833.2
M_o	1239.7	1023.0	1385.5
M_u	1609.7	-	1609.7
$f_s \rho_{non-comp}$	5.8	11.0	5.9
$f_s \rho_{comp}$	2.8	5.5	3.4
$f_s s_3 [M\phi + M_{Imp}]$	22.2	18.8	25.0
$f_s (Overload)$	30.8	35.3	34.3
$f_s (Total)$	-	45.9	-
VR	38.5	-	41.9

- I_s, S_s : Non-composite moment of inertia and section modulus of the steel section used for computing f_s (Total and Overload) due to non-composite dead loads (in.⁴ and in.³).
- $I_c(n), S_c(n)$: Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing f_s (Total and Overload) due to short-term composite live loads (in.⁴ and in.³).
- $I_c(3n), S_c(3n)$: Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing f_s (Total and Overload) due to long-term composite (superimposed) dead loads (in.⁴ and in.³).
- Z : Plastic Section Modulus of the steel section in non-composite areas (in.³).
- ρ : Un-factored non-composite dead load (kips/ft.).
- $M\phi$: Un-factored moment due to non-composite dead load (kip-ft.).
- $s\phi$: Un-factored long-term composite (superimposed) dead load (kips/ft.).
- $M_s\phi$: Un-factored moment due to long-term composite (superimposed) dead load (kip-ft.).
- $M\phi$: Un-factored live load moment (kip-ft.).
- M_{Imp} : Un-factored moment due to impact (kip-ft.).
- M_o : Factored design moment (kip-ft.).
 $1.3 [M\phi + M_s\phi + \frac{2}{3} (M\phi + M_{Imp})]$
- M_u : Compact composite moment capacity according to AASHTO LFD 10.50.1.1 or compact non-composite moment capacity according to AASHTO LFD 10.48.1 (kip-ft.).
- $f_s (Overload)$: Sum of stresses as computed from the moments below (ksi).
 $M\phi + M_s\phi + \frac{2}{3} (M\phi + M_{Imp})$
- $f_s (Total)$: Sum of stresses as computed from the moments below on non-compact section (ksi).
 $1.3 [M\phi + M_s\phi + \frac{2}{3} (M\phi + M_{Imp})]$
- VR: Maximum $L +$ impact horizontal shear range within the composite portion of the span for stud shear connector design (kips).



	Abut.	Pier
$R\phi$	23.6	78.2
$R\phi$	42.7	48.7
Imp.	12.4	13.6
R_{Total}	78.7	140.5

* Compact section
** Braced non-compact and partially braced section

ELEVATION
SPLICE DETAIL
(12 Required)

Note:
All bolts shall have the threads excluded from the shear plane.

INTERIOR DIAPHRAGM
Note:
Two hardened washers required for each set of oversized holes.

**** Alternate channels are permitted to facilitate material acquisition. Calculated weight of structural steel is based on the lighter section.
***** 7/8" ϕ HS bolts, 1/16" ϕ holes

The angle and channel of the interior diaphragm shall be AASHTO M 270 Grade 36.

***** TOP OF BEAM ELEVATIONS**

Location	ϕ Brg. S. Abut.	ϕ Brg. Pier 1	ϕ Splice 1	ϕ Brg. Pier 2	ϕ Splice 2	ϕ Brg. N. Abut.
Beam 1	427.40	427.48	427.50	427.45	427.44	427.36
Beam 2	427.54	427.63	427.65	427.61	427.60	427.51
Beam 3	427.65	427.74	427.76	427.73	427.72	427.64
Beam 4	427.64	427.74	427.76	427.73	427.72	427.65
Beam 5	427.51	427.62	427.64	427.61	427.61	427.54
Beam 6	427.36	427.47	427.49	427.46	427.46	427.40

*** For fabrication only

DESIGNED	SJB
CHECKED	EML
DRAWN	KLH
CHECKED	EML

HORNER & SHIFRIN, INC.
ENGINEERS

STRUCTURAL STEEL DETAILS
F.A.P. ROUTE 328 - SECTION (8BR-2)B-1
WAYNE COUNTY
STATION 888+60.00
STRUCTURE NO. 096-0067