## STRUCTURE GEOTECHNICAL REPORT CULVERT AT STATION 598+48.00 ILLINOIS 47 OVER KISHWAUKEE RIVER TRIBUTARY EX SN 056-0247, PR SN 056-0309 MCHENRY COUNTY, ILLINOIS

For Strand Associates, Inc. 1170 South Houbolt Road Joliet, IL 60432

Submitted by
Wang Engineering, Inc.
1145 North Main Street
Lombard, IL 60148

Original Report: August 24, 2018

**Revised Report: NA** 

#### **Technical Report Documentation Page**

1. Title and Subtitle Structure Geotechnical Report, Culvert at Sta. 598+48.00 Illinois Route 47 over Kishwaukee River Tributary  4. Route / Section / County FAI 326 (IL 47)/ 105-N-2(15) / McHenry		2. Original Date: August 24, 2018 Revised Date: NA  3. Report Type SGR RGR Draft Final Revised  5. Contract D-91-011-14				
				<b>6. PSB / Item No.</b> 14-3/003	7. Existing Structure Number(s) SN 056-0247	8. Proposed Structure Number(s) SN 056-0309
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#### TABLE OF CONTENTS

1.0	INTRODUCTION	I
1.1	Proposed Structure	1
1.2	EXISTING STRUCTURE AND LAND USE	1
2.0	GEOLOGICAL SETTING	2
2.1	Physiography	2
2.2	SUFICIAL COVER	2
2.3	Bedrock	3
3.0	METHODS OF INVESTIGATION	3
3.1	FIELD INVESTIGATION	4
3.2	LABORATORY TESTING	4
4.0	INVESTIGATION RESULTS	5
4.1	LITHOLOGICAL PROFILE	5
4.2	GROUNDWATER CONDITIONS	6
5.0	FOUNDATION ANALYSIS AND RECOMMENDATIONS	6
5.1	SCOUR CONSIDERATIONS	6
5.2	GROUND IMPROVEMENT	7
5.3	BEARING CAPACITY	7
5.4	Settlement	8
5.5	GLOBAL STABILITY	8
5.6	CAST-IN-PLACE OR PRECAST CULVERT CONSIDERATIONS	8
5.7	STAGED CONSTRUCTION CONSIDERATIONS	9
6.0	CONSTRUCTION CONSIDERATIONS	9
6.1	SITE PREPARATION	9
6.2	EXCAVATION, DEWATERING, AND UTILITIES	9
6.3	FILLING AND BACKFILLING	10
6.4	EARTHWORK OPERATIONS	10
7.0	QUALIFICATIONS	11



REFERENCES	12
EXHIBITS	
1. SITE LOCATION MAP	
2. Site and Regional Geology	
3. BORING LOCATION PLAN	
4. Soil Profile	
5. Removal and Replacement Sketch	
APPENDIX A	
BORING LOGS	
APPENDIX B	
LABORATORY TEST RESULTS	
APPENDIX C	
GLOBAL STABILITY ANALYSIS	
APPENDIX D	
PRELIMINARY GENERAL PLAN AND ELEVATION SHEETS	
LIST OF TABLES	
Table 1: Summary of Consolidation Testing.	5
Table 2 : Design Secur Florestions	7



# STRUCTURE GEOTECHNICAL REPORT CULVERT AT STATION 598+48.00 ILLINOIS 47 OVER KISHWAUKEE RIVER TRIBUTARY EX SN 056-0247, PR SN 056-0309 MCHENRY COUNTY, ILLINOIS FOR STRAND ASSOCIATES, INC.

#### 1.0 INTRODUCTION

This report presents the results of our subsurface investigation, laboratory testing, and geotechnical evaluations to support the removal and replacement of a culvert on Illinois Route 47 (IL 47) at Station 598+48 that is about 400 feet north of the intersection between Pleasant Valley Road and IL 47. The proposed structure replacement is part of the widening and reconstruction of 1.65-mile long of IL 47 between Station 565+80 and Station 660+92 in McHenry County, Illinois. A *Site Location Map* is presented as Exhibit 1.

#### 1.1 Proposed Structure

Based on the information provided by Strand Associates, Inc. (Strand) and Christopher B. Burke Engineering, Ltd. (CBBEL) on February 14, 2018, and the *Preliminary General Plan and Elevation* (GPE) received in May, 2018, Wang Engineering, Inc. (Wang) understands the existing 6-foot wide by 5-foot tall culvert will be removed and replaced with a 8-foot wide by 6-foot tall culvert. The proposed culvert will be 164-foot long, which is about 66 feet longer than the existing one. The proposed culvert will have the upstream invert elevation at 898.76 feet and the downstream invert elevation at 898.53 feet; with flow directed from southwest to northeast. The proposed culvert will have bottom elevation slightly lower than the existing. Apron with vertical wingwalls are proposed to support the widened roadway embankment at both the upstream and downstream ends. The roadway profile grade elevation will be slightly raised by 0.5 feet at the centerline of the road.

#### 1.2 Existing Structure and Land Use

The existing 6-foot by 5-foot concrete box culvert was originally constructed in 1936 and has a total length of 60 feet then widened in 1971 by about 38 feet at the west end with concrete drainage ditch. The existing culvert has a horizontal wingwalls at both ends.



The purpose of this investigation was to characterize the site soil and groundwater conditions, perform geotechnical analyses, and provide recommendations for the design and construction of the proposed culvert replacement and wingwalls.

#### 2.0 GEOLOGICAL SETTING

The project area is located along IL 47 in Dorr Townships, in McHenry County, Illinois. On the USGS *Huntley 7.5 Minute Series Quadrangle map*, the project is located in SW ¼ of Section 33, Tier 44 N, Range 7 E of the Third Principal Meridian.

The following review of published geologic data, with emphasis on factors that might influence the design and construction of the proposed engineering works, is meant to place the project area within a geological framework and confirm the dependability and consistency of the subsurface investigation results. For the study of the regional geologic framework, Wang considered northeastern Illinois in general and McHenry County in particular. Exhibit 2 illustrates the *Site and Regional Geology*.

#### 2.1 Physiography

The IL 47 at the culvert location runs through rural setting, surrounded by agricultural fields. The surface topography is generally flat with elevation of about 905 feet. At culvert location the elevation along IL 47 roadway is about 908 feet and at the drainage ditch bottom is about 900 feet. The water along the drainage ditch flows from southwest to northeast through a 6-foot wide concrete box culvert.

#### 2.2 Surficial Cover

The project area was shaped during the Wisconsin-age glaciation and about 200-foot thick overburden covers the bedrock. The glacigenic deposits were emplaced during pulsating advances and retreats of an icesheet lobe responsible for the formation of end moraines and associated low-relief till and lake plains (Hansel and Johnson 1996). The surficial cover within the project area consists of organic silt and clay of the Grayslake Peat found discontinuously throughout the project area. The Grayslake Peat overlies either the clay and silt of the Equality Formation, or the silty clayey diamicton of the Yorkville Member of the Lemont Formation. The clayey diamicton overlies the loamy diamicton of the Tiskilwa Formation or gravelly sand outwash of the Henry Formation. The outwash of the Henry Formation interfingers with the two diamictons.



The Grayslake Peat, less than 10-foot thick, consists of black to brown peat interbedded with gray organic reach sand and silty clay and white to light gray marl (Curry and Thomason 2012). The Equality Formation, less than 15-foot thick, consists of brown to gray bedded fine sand, silt, and clay lacustrine deposits (Curry and Thomason 2012). The Henry Formation consists of stratified sand and gravel outwash with thicknesses of about 5 to 10 feet, within the project limits (Curry and Thomason 2012). The Yorkville Member of the Lemont Formation, up to 15-foot thick, consists of yellowish brown to gray silty clay to silty clay loam diamicton that contains lenses of gravel, sand, silt, and clay (Hansel and Johnson 1996, Curry and Thomason 2012). The Tiskilwa Formation, about 65 feet thick, consists of calcareous reddish brown to gray clay loam, loam to sandy loam diamicton that contains lenses of gravel, sand, silt, and clay (Wickham et al. 1988, Curry and Thomason 2012). The Tiskilwa Formation diamicton rests over the Illinoian-age drift, which in turn unconformably rests over the Silurian-age dolostone (Curry and Thomason 2012). The diamicton account for about 75% of the subsurface soil.

From a geotechnical viewpoint, the Yorkville Member characterized by low plasticity to moderate, high strength, and low to moderate moisture content and the Tiskilwa Formation characterized by low plasticity, medium to high strength, low moisture content, moderately to highly pebbly (Wickham et al. 1988, Bauer et al. 1991).

#### 2.3 Bedrock

In McHenry County, the surficial cover rests unconformably on top of Silurian-age and Ordovician-age bedrock. The top of the bedrock lies about 160 to 200 feet below the ground surface (bgs). Structurally, the site is located on the eastern flank of the Wisconsin Arch (Willman 1971). No active faults or underground mines are known in the area.

Our subsurface investigation results fit into the local geologic context. The borings drilled in the project area encountered native sediments consisting of organic reach silt and clay of the Grayslake Peat, gravel and sand outwash of the Henry Formation interbedded with silty clay diamicton of the Yorkville Member of the Lemont Formation and loamy diamicton of the Tiskilwa Formation. None of the borings were deep enough to encounter bedrock.

#### 3.0 METHODS OF INVESTIGATION

The following sections outline the subsurface and laboratory investigations performed by Wang.



#### 3.1 Field Investigation

The subsurface investigation consisted of three structure borings, designated as CUL-01 through CUL-03, and two Shelby tube borings, designated as CUL-02ST and CUL-03ST. In addition, two peat delineation borings drilled south of the culvert, designated PT6-03 and PT7-06, were included in the report. The borings were drilled by Wang on October and December 2017 and were advanced to depths of 6 to 35 feet bgs. The as-drilled northings and eastings were acquired with a mapping-grade GPS unit; boring elevations were surveyed with a level. Stations and offsets were determined from drawings provided by Strand. Boring location data are presented in the *Boring Logs* (Appendix A). The as-drilled boring locations are shown in the *Boring Location Plan* (Exhibit 2).

An ATV- mounted drilling rig, equipped with hollow stem augers, was used to advance and maintain open boreholes. Soil sampling was performed according to AASHTO T 206, "*Penetration Test and Split Barrel Sampling of Soils*." The soil was sampled at 2.5-foot intervals to 30 feet below ground surface (bgs) and at 5-foot intervals, thereafter. Peat delineation borings were sampled continuously. Soil samples collected from each sampling interval were placed in sealed jars and transported to the laboratory for further examination and laboratory testing. Shelby tube samples were obtained from Borings CUL-02ST and CUL-03ST where soft to medium stiff organic clay to silty clay was encountered.

Field boring logs, prepared and maintained by Wang geologists, include lithological descriptions, visual-manual soil classifications (IDH Textural), results of Rimac and pocket penetrometer unconfined compressive strength testing on cohesive soils, and results of Standard Penetration Tests (SPT) recorded as blows per 6 inches of penetration.

Groundwater observations were made during and at the end of drilling operations. Due to safety considerations, boreholes were backfilled immediately upon completion with soil cuttings and/or chips. The pavement surface was restored to its original condition.

#### 3.2 Laboratory Testing

The soil samples were tested in the laboratory for moisture content (AASHTO T265). Atterberg limits (AASHTO T89/T90) and particle size (AASHTO T88) analyses were performed on selected samples. A one-dimensional consolidation test (AASHTO T216) was performed on a shelby tube sample. Field visual descriptions of the soil samples were verified in the laboratory and index tested samples were classified according to the IDH Soil Classification System. Laboratory test results are shown in the *Boring Logs* (Appendix A) and in the *Laboratory Test Results* (Appendix B).



#### 4.0 INVESTIGATION RESULTS

Detailed descriptions of the soil conditions encountered during the subsurface investigation are presented in the attached *Boring Logs* (Appendix A) and in the *Soil Profile* (Exhibit 4). Please note that strata contact lines represent approximate boundaries between soil types. The actual transition between soil types in the field may be gradual in horizontal and vertical directions.

#### 4.1 Lithological Profile

The borings encountered 3 to 22 inches of silty clay loam topsoil at the surface. In descending order, the general lithologic succession encountered beneath the surface includes: 1) man-made ground (fill); 2) soft to medium stiff organic silty clay to silty clay loam; and 3) stiff to hard silty clay to silty clay loam and clay loam to loam.

#### 1) Man-made ground (fill)

Beneath the topsoil, Borings CUL-02 and PT6-03 revealed 2 to 7 feet of fill material. The fill material is cohesive, consisting of medium stiff to stiff, dark brown silty clay loam. The unconfined compressive strength  $(Q_u)$  values of 0.9 and 1.5 tsf and the moisture content values of 16 to 19%. Below the fill, Boring CUL-02 encountered 6 inches of buried clay loam topsoil.

#### 2) Soft to medium stiff organic silty clay to silty clay loam

Beneath the fill and topsoil, at elevations of 898 to 900 feet, the borings encountered 3 to 8 feet of soft to medium stiff, brown to gray organic silty clay to silty clay loam. The unit has  $Q_u$  values of 0.41 to 1.00 tsf. The moisture content values range from 17 to 57%. Laboratory index testing on samples from this layer shows liquid limit ( $L_L$ ) values of 26 to 38% and plastic limit ( $P_L$ ) values of 13 to 19%. The consolidation properties of this soft to medium stiff silty clay layer were obtained. The resulting soil parameters are summarized in Table 1 and the laboratory test results are attached in Appendix B.

Table 1: Summary of Consolidation Testing

	Test	Test					Moisture
Boring ID	Depth	Elevation	$C_{\rm C}$	$C_S$	$e_{O}$	OCR/P'c	Content
	(feet)	(feet)				(psf)	(%)
CUL-02ST	9 to 11	895	0.491	0.112	1.157	1.31/1835	44

C<sub>C</sub>: Compression index; C<sub>S</sub>: Swelling index ; e<sub>O</sub>: Initial void ratio; OCR: Over consolidation ratio; and

P'c: Preconsolidation pressure.



#### 3) Stiff to hard silty clay to silty clay loam and clay loam to loam

At elevations of 892 to 903 feet, the borings encountered gray, stiff to hard silty clay to silty clay loam and clay loam to loam with wet to saturated sandy gravel to gravelly sand interbeds. The unit has  $Q_u$  values of 1.3 to 4.6 tsf and moisture content values of 9 to 15%. The sandy gravel to gravelly sand interbeds have N values of 12 to 27 blows per foot and moisture content values of 11 to 19%.

#### 4.2 Groundwater Conditions

Groundwater was encountered while drilling at elevations of 885 to 889 (11 to 20 feet bgs). At the completion of drilling, the groundwater was observed at elevations of 874 to 900 feet (0 to 31 feet bgs).

#### 5.0 FOUNDATION ANALYSIS AND RECOMMENDATIONS

Geotechnical evaluations and recommendations for the culvert and wingwalls are included in the following sections. The proposed culvert replacement will have upstream and downstream invert elevations of 898.76 and 898.53 feet, respectively. The base of the culvert barrel will be installed slightly deeper than the existing. Apron with wingwalls will be used to support the roadway embankment widening at both ends.

Wang has performed bearing capacity, settlement, and global stability analyses for the proposed culvert barrel and wingwalls.

#### 5.1 Scour Considerations

The design scour elevation should be taken at the bottom of the cutoff wall (IDOT 2012). At the horizontal cantilever wingwalls, the cutoff walls are established 3.0 feet below the culvert invert elevations; whereas for T-type wingwalls, the cutoff walls are established 4.0 feet below the invert elevations. The design scour elevations with cutoff walls established at 4.0 feet below the invert elevations, as shown in the GPE drawing, are summarized in Table 2. To prevent local erosion, we recommend placing stone riprap or a concrete apron at the ends of the culvert; this will be particularly important if precast sections are used. This will also prevent sediments from entering and accumulating in the culvert, minimize long term maintenance, and provide protection to the stream bed at the interface.



Table 2 : Design Scour Elevations

	Upstream	Downstream
Design Scour Elevations (feet)	894.76	894.53

#### 5.2 Ground Improvement

The subsurface investigation indicates the soils along the culvert base are primarily soft to medium stiff organic silty clay, clay to silty clay, and silty clay loam. To mitigate settlement issues and to provide stable working platforms, Wang recommends removal and replacement of soft to medium stiff soil along the proposed culvert barrel and wingwalls. The recommended removal limit and depth are:

- From the downstream end of the culvert going 65 feet upstream, for a depth of 5.5 feet below the proposed bottom of the culvert or to elevation 892 feet; and
- From 65 feet of downstream to upstream end, for a depth of 1.0 foot below the proposed bottom of the culvert or to elevation 897 feet.

A sketch of the proposed removal is shown in Exhibit 5. The replacement material should extend a minimum of two feet beyond each side of the box (IDOT 2016). In addition, the following note should be shown in the plans.

"The limits and quantities of removal and replacement shown are based on the boring data may be modified by the District Geotechnical and Field Engineers for variable subsurface conditions encountered in the field"

#### **5.3** Bearing Capacity

After the proposed removal and replacement, the walls should be designed based on a maximum factored bearing resistance of 4,000 psf, determined with a bearing resistance factor ( $\phi_b$ ) of 0.45 (AASHTO 2016). The wingwalls should be sized and designed based on the information and typical sections shown in IDOT *Culvert Manual*, Sections 4.3 and 4.4 (IDOT 2017).

The culvert wingwalls could also be constructed as horizontal cantilever walls if they are less than 16 feet in length and the wingwall location can be adequately dewatered (IDOT 2017). Horizontal cantilever walls should be designed based on the structural guidelines provided in Section 4.2 of the



IDOT (2017). These wingwalls should be founded at a minimum depth of 3.0 feet below the culvert invert elevations.

The wingwalls types suitable for precast concrete culvert include apron, driven sheet pile and cast-in-place T-type wingwalls. For the cast-in-place culvert, the horizontal cantilever, L-type or T-type wingwalls are typically considered. The apron wingwalls should be designed and constructed based on IDOT Specifications and IDOT Base Sheet dated 2/17/2017 "SCB-GPE."

#### 5.4 Settlement

As discussed in Section 5.2, soft to medium stiff soil will be encountered below the base of proposed culvert. Without removal and replacement, we estimate up to 3 inches of settlement under the new culvert and fill loads. After the proposed removal and replacement, we estimate the foundation soils will experience total long-term settlements of about 0.2 to 0.6 inches, with differential settlement of 0.5 inches over 65 feet. We estimate the settlements are suitable for the construction of the proposed culvert and wingwalls.

#### 5.5 Global Stability

The global stability of the wingwalls was analyzed based on the generalized soil profile described in Section 4.1. The maximum total fill height behind the wingwalls will be about 9 feet with a backfill slope of 1:3 (V:H). We have performed global stability analyses for the wingwalls at the downstream section with the weaker soil conditions under both undrained (short-term) and drained (long-term) conditions. The analyses were performed with *Slide v6.0* and the results of the evaluations are provided in Appendix C. We estimate a factor of safety (FOS) of 3.3 for undrained soil condition and a FOS of 1.6 for a drained soil condition. The FOSs meet the minimum FOS requirement of 1.5 (IDOT 2015).

#### **5.6** Cast-In-Place or Precast Culvert Considerations

After the recommended removal of unsuitable soil, the results of the analyses indicate that both the cast-in-place and precast culvert options are appropriate and feasible at the site. The differential settlement will be about 0.5 inches over 65 feet, which will not cause excessive separation of the precast sections. For precast end sections, we recommend considering either a concrete apron or riprap armoring at the downstream invert to protect against scour and erosion that could undermine the precast end section assuming a hydraulic analysis does not indicate a low-scour condition.



#### **5.7** Stage Construction Considerations

Based on the information provided by Strand, Wang understands a temporary sheet piling system will be utilized to accommodate stage construction. The sheet piling should be designed based on IDOT Design Guide 3.13.1. Assuming an exposed height of about 16.5 feet (from elevation 908.5 to 892.0 feet) located at the stage construction line, our evaluations indicate the temporary steel sheet piling is feasible.

#### 6.0 CONSTRUCTION CONSIDERATIONS

#### **6.1** Site Preparation

The existing culvert will be removed and any vegetation, surface topsoil, and debris should be cleared and stripped where the new culvert and wingwalls will be placed. If unstable or unsuitable materials are exposed during excavation, they should be removed and replaced with compacted fill material as described in Section 6.3. The embankment fill behind the proposed wall will be placed against existing sloped embankment. These existing embankments should be deeply plowed or benched in accordance with IDOT Section 205.03 (IDOT 2016) prior to the placement of fill materials. We recommend that all embankment construction be performed in accordance with the District One Embankment I Special Provision.

#### 6.2 Excavation, Dewatering, and Utilities

Excavations should be performed in accordance with local, state, and federal regulations. The potential effect of ground movements upon nearby utilities should be considered during construction. Excavations for the placement of the culvert barrel should be steeped at no steeper than 1:2 (V:H). Any slopes that cannot be graded at 1:2 (V: H) should be properly shored with temporary sheeting or soil retention systems. Excavated material should not be stockpiled immediately adjacent to the top of slopes, nor should equipment be allowed to operate too closely to open excavations.

During the subsurface investigation, groundwater was encountered at elevation ranging from 885 to 900 feet. The proposed barrel and wingwalls will be established between 894.5 and 898.8 feet elevation, which is below the encountered groundwater elevations. Therefore, the groundwater may be encountered and temporary steel piling or cofferdam will be required for dewatering of foundation excavation. Contractor should be prepared for dewatering measures. Any water that accumulates in open excavations by seepage or runoff should be immediately removed by sump-pump. Depending upon prevailing climate conditions and the time of the year when culvert construction takes place, control runoff and maintenance of existing flows may require temporary water diversion and control.



#### 6.3 Filling and Backfilling

Fill material used to attain the final design elevations should be IDOT Standard Specifications. Coarse aggregate of IDOT gradation CA-6 or pre-approved, compacted, cohesive or granular soils conforming to Section 204 would be acceptable as fill material (IDOT, 2016). The fill material should be free of organic matter and debris and should be placed in lifts and compacted according to IDOT Section 205, *Embankment* (IDOT, 2016).

Groundwater may exist beneath the culvert. As mentioned in IDOT (2017), in cases such as replacement below box culvert where dewatering and compaction may not be possible, the pay item "Rockfill" is commonly used. In this case, the following note should be added.

"The Rockfill shall be capped with 6 in. of CA7 and satisfy the Standard Specifications unless otherwise indicated in the Special Provisons. The cost of the capping material shall be included in the pay item for Rockfill."

#### **6.4 Earthwork Operations**

The required earthwork can be accomplished with conventional construction equipment. Moisture and traffic will cause deterioration of exposed subgrade soils. Precautions should be taken by the Contractor to prevent water erosion of the exposed subgrade. A compacted subgrade will minimize water runoff erosion.

Earth moving operations should be scheduled to not coincide with excessive cold or wet weather (early spring, late fall or winter). Any soil allowed to freeze or soften due to the standing water should be removed. Wet weather can cause problems with subgrade compaction.

It is recommended that an experienced geotechnical engineer be retained to inspect the exposed subgrade, monitor earthwork operations, and provide material inspection services during the construction phase of this project.



#### 7.0 QUALIFICATIONS

The analysis and recommendations submitted in this report are based upon the data obtained from the borings drilled at the locations shown on the boring logs and in Exhibit 3. This report does not reflect any variations that may occur between the borings or elsewhere on the site, variations whose nature and extent may not become evident until the course of construction. In the event that any changes in the design and/or location of the structure are planned, we should be timely informed so that our recommendations can be adjusted accordingly.

It has been a pleasure to assist Strand Associates, Inc. and the Illinois Department of Transportation on this project. Please call if there are any questions, or if we can be of further service.

Respectfully Submitted,

#### WANG ENGINEERING, INC.

Andri A. Kurina, P. E. Senior Geotechnical Engineer Corina T. Farez, P.E, P.G. QA/QC Reviewer

Nesam S. Balakumaran, P.Eng. Project Geotechnical Engineer

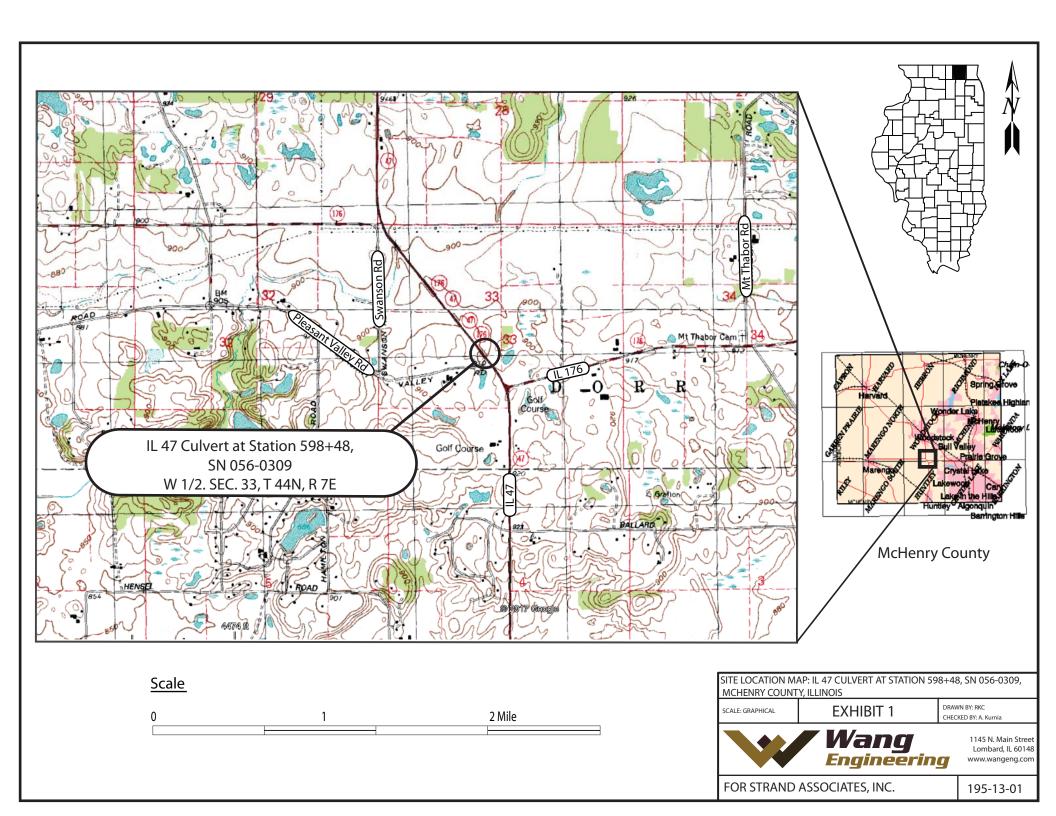


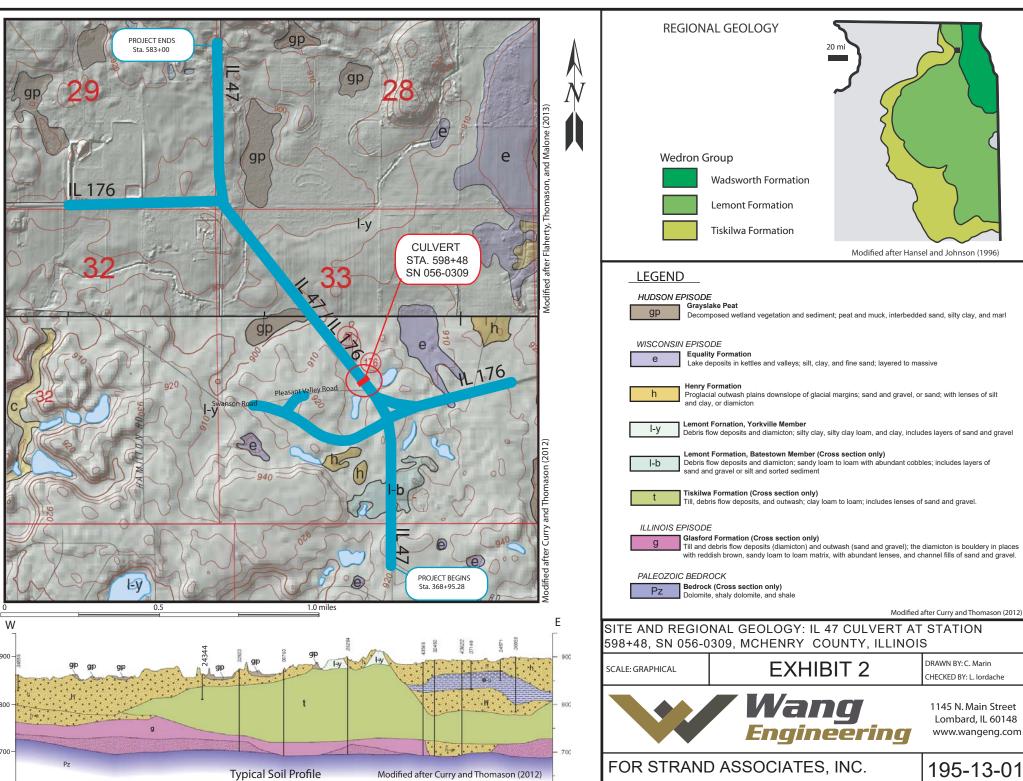
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#### **EXHIBITS**





195-13-01



Legend

Soil Borings

Scale

200 400 Feet BORING LOCATION PLAN: IL 47 CULVERT AT STATION 598+48, SN 056-0309, MCHENRY COUNTY, ILLINOIS

SCALE: GRAPHICAL

EXHIBIT 3-1

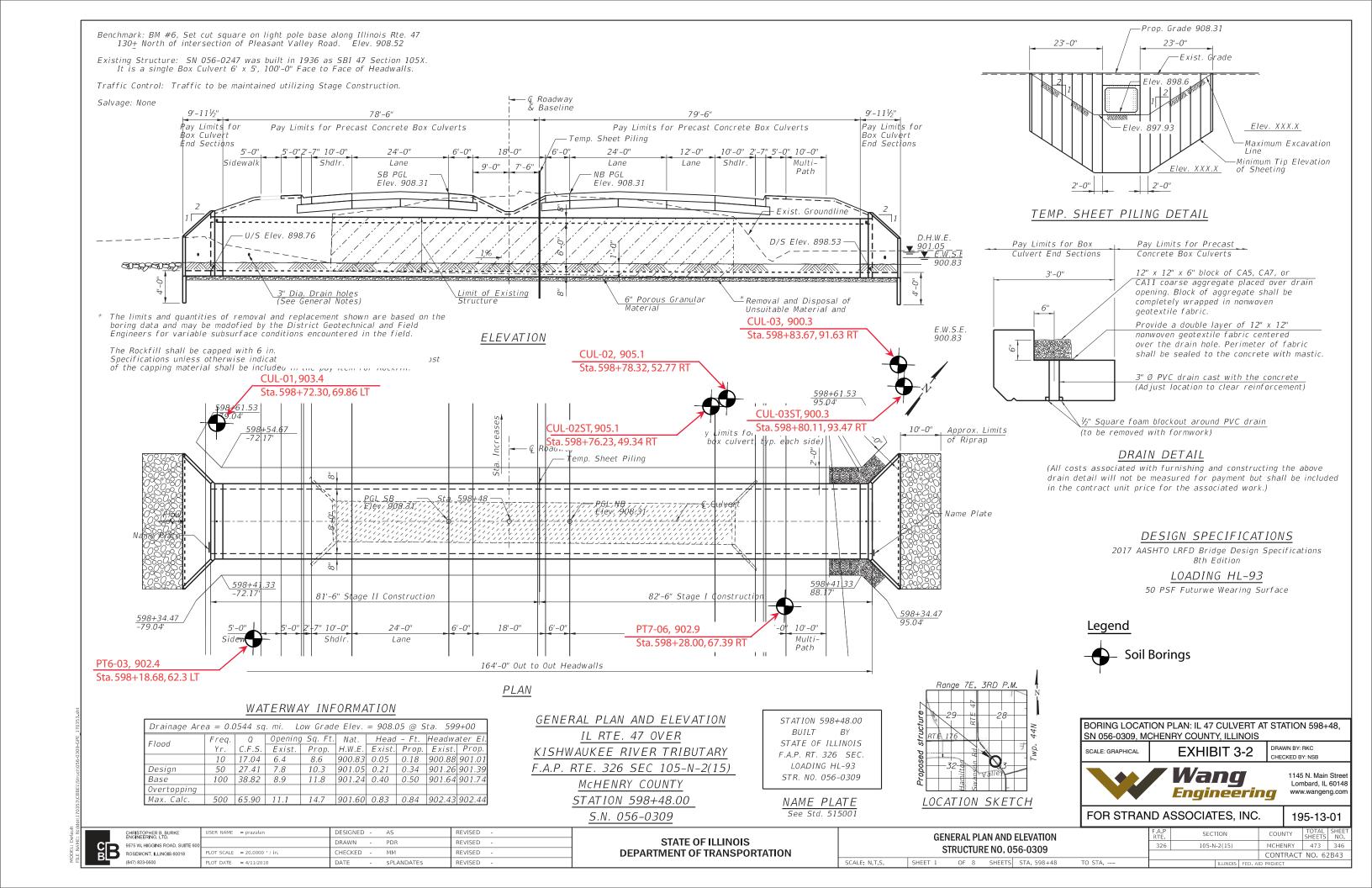
DRAWN BY: RKC CHECKED BY: A. Kurnia

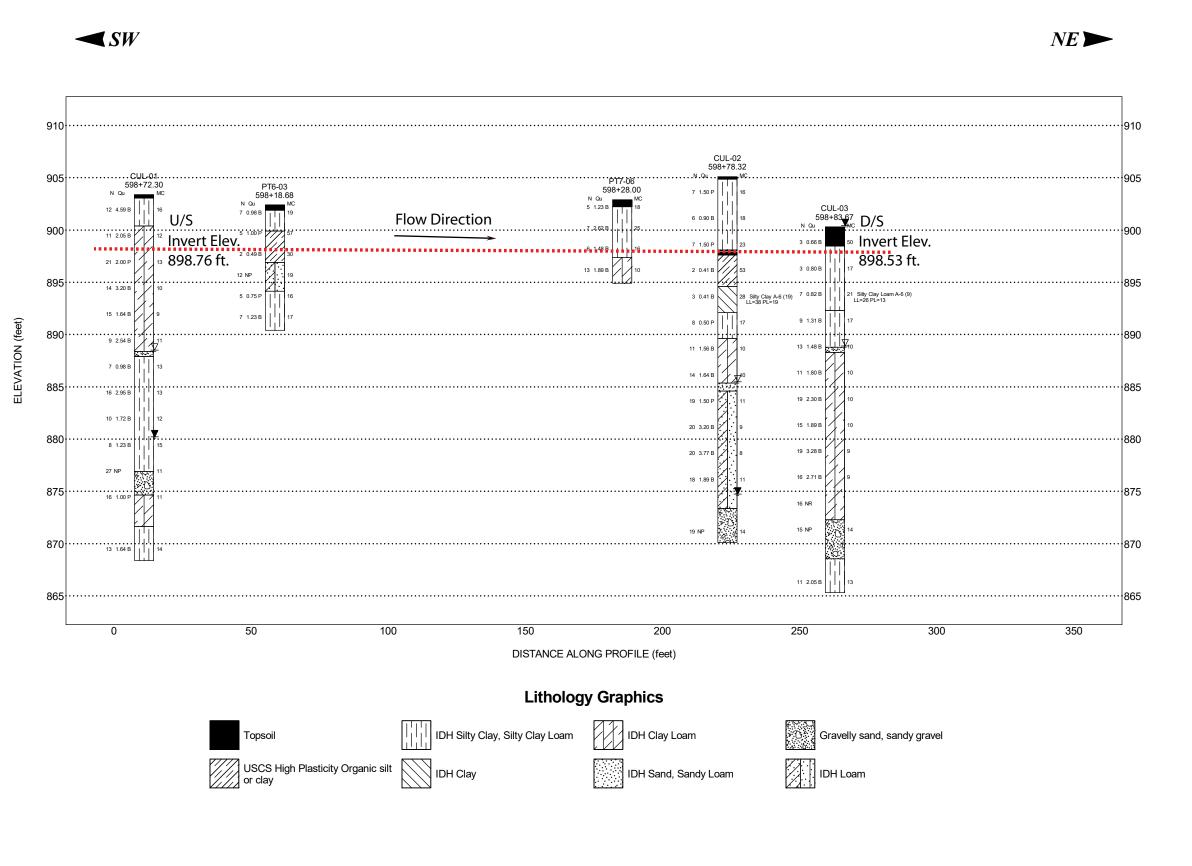


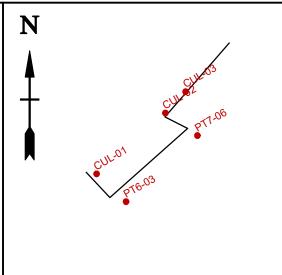
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195-13-01

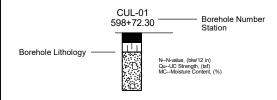






Site Map Scale 1 inch equals 130 feet

#### **Explanation:**



Water Level Reading at time of drilling.
Water Level Reading 24-hr after drilling or at end of drilling



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Vertical Exaggeration: 4x

#### Wang Engineering, Inc.

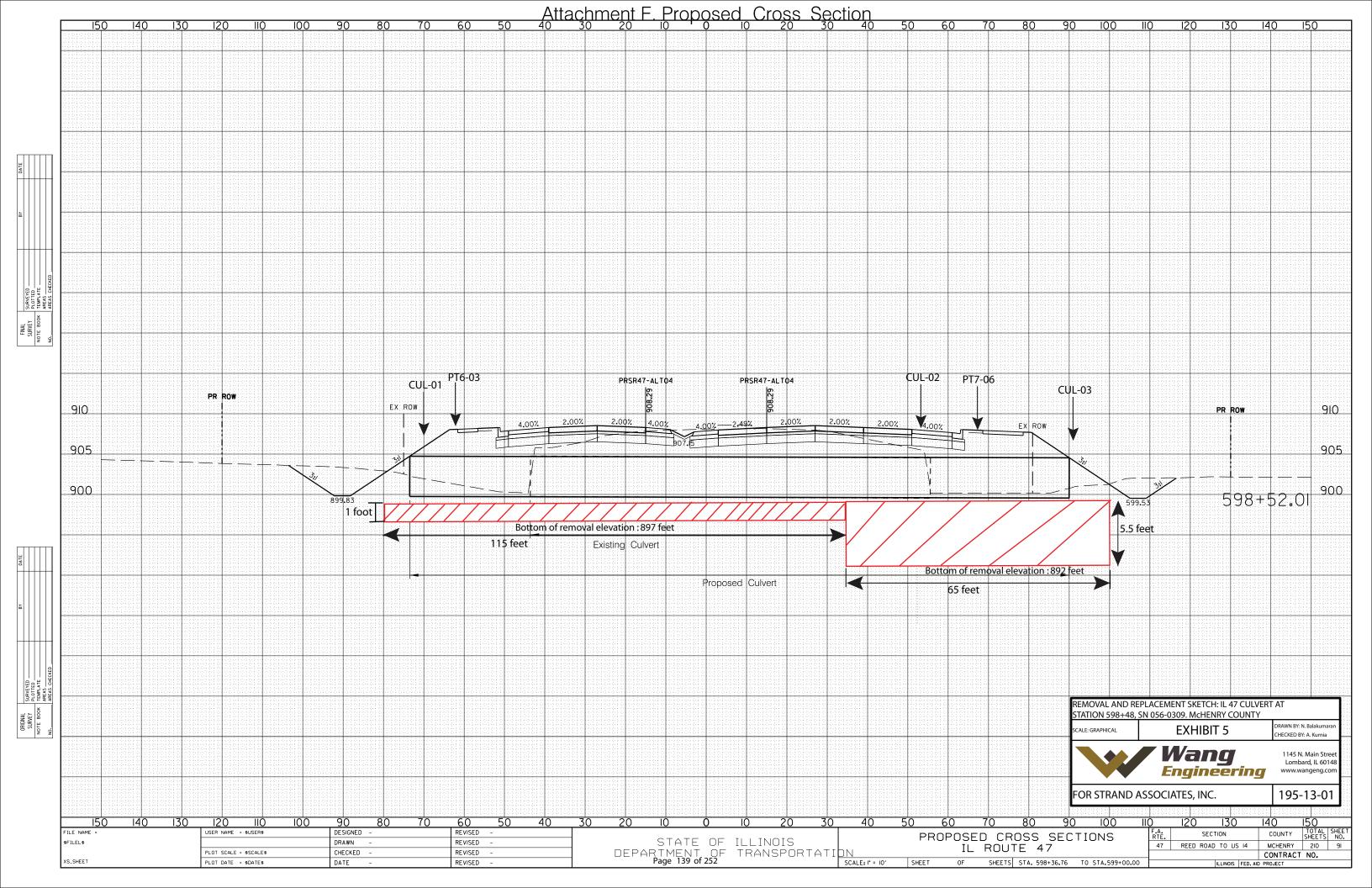
1145 North Main Street Lombard, IL 60148

#### Subsruface Data Profile Culvert at Station 598+48, SN 056-0309



IL 47 between US 14 and S of IL 176 McHenry County, Illinois

JOB NUMBER	PLATE NUMBER
195-13-01	EXHIBIT 4





#### APPENDIX A



#### LEGEND FOR BORING LOG

Relative Density of Non- Cohesive Soils		
N-Blows/ Relative Density 12 inches Term		
0-3	Very Loose	
4-9	Loose	
10-29	Medium Dense	
30-49	Dense	
50-80+	Very Dense	

Consistency of Cohesive Soils		
Unconfined Compressive Strength Qu, tsf  Consistency Term		
<0.25	Very Soft	
0.25-0.49	Soft	
0.50-0.99	Medium Stiff	
1.00-1.99	Stiff	
2.00-3.99 Very Stiff		
>4.00 Hard		

Rock Quality Designation (RQD)		
0-25%	Very Poor	
25-50%	Poor	
50-75% Fair		
75-90%	75-90% Good	
90-100% Excelent		

Geoprobe

SS	= Split Spoon
ST	= Shelby Tube
SPT	= Standard Penetration Test
$Q_{\mathrm{u}}$	= Unconfined Compressive
	Strength
	NP = Non Plastic
	P = Pocket Penetrometer
	S = Shear failure of sample,
	Rimac test
	B = Bulge failure of sample,
	Rimac test
SSA	= Solid Stem Augers,
HSA	= Hollow Stem Augers,

Proportional Terms			
Trace	1-9	Pe	
Little	10-19	Percent Dry Weigh	
Some	20-34	de de la	
And	35-50	of t	
Gradation Terminology			
Boulders	>200	)mm	
Cobbles	200mm to 75mm		
Gravel	75mm to 2mm		
Sand	2-0mm to 0.074mm		
Silt	0.074mm to 0.002mm		
Clay	<0.002mm		

**Relative Drilling Resistance (RDR)** 

Some Chatter - Moderate Advancement

No Chatter - Very Easy Drilling No Chatter - Easy Drilling

Relative Moisture Conditions			
Term	Description		
Dry	Dusty, No visible moisture		
Damp	Cohesives hard to mold; Granulars do not flow easily		
Moist	Cohesives can be molded; Granulars start to stick together		
Wet	Cohesives can be very easily molded and sticky; Granulars stick together easily		
Saturated	Only granular soils; Water drains freely from sample		

# Sample Type Symbols Split Spoon Rock Core In-situ Vane Shear Test Shelby Tube Spr = Standard Penetration Test No Recovery Shelby Tube Spr = Standard Penetration Test No Value is the sum of the second and the third numbers

(Rev. 05/23/2018)

**Auger Cuttings** 



#### **BORING LOG CUL-01**

WEI Job No.: 195-13-01

Client Strand Associates, Inc.

Project IL 47 between US 14 and S of IL 176

Location McHenry County, Illinois

Datum: NAVD 88 Elevation: 903.40 ft North: 2032766.30 ft East: 959415.12 ft Station: 598+72.30 Offset: 69.86 LT

Profile	SOIL AND R DESCRIPT	0) 3	Sample Type	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AN DESCR		Depth (#)	Sample Type	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	903.14-inch thick, black SIL \LOAM \ Hard, brown SILTY C gravel; damp	-TOPSOIL/	-	1	5 6 6	4.59 B	16					- - -		9	3 5 5	1.72 B	12
	Stiff to very stiff, brow SILTY CLAY LOAM to LOAM, trace gravel; o	CLAY		2	3 6 5	2.05 B	12					- - 25_		10	4 4 4	1.23 B	15
				3	7 10 11	2.00 P	13			um dense, g VEL; satura	ated	DR 3		11	27 16 11	NP	11
		cobbles 10_		4	5 6 8	3.20 B	10			gray CLAY el; damp		ce - DR 230_		12	6 4 12	1.00 P	11
				5	4 7 8	1.64 B	9			gray SILTY gravel; dan	np	- 	-				
	888.4 887.9GRAVEL; saturated	15\		6	3 5 4	2.54 B	11		868.4 Borin	ng terminate	d at 35.00	- - 35 ft		13	7 8 5	1.64 B	14
8/10/18	Medium stiff to very st SILTY CLAY LOAM, t damp to moist			7	2 2 5	0.98 B	13					- - - -	-				
MANGENGINC 1951301.GPJ WANGENG.GDT 88 ind		20_		8	3 5 11	2.95 B	13					- - 40					
2. 2. 2.		ENERAL N					4.07	. 00	47	\A(I 'I \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		R LEVE					
ENGINC 19513 ind Dri	ller <b>K&amp;N</b> L	17 Co Testing Serv ogger T. Ro ISA; 140 lb a	thscl	[	Drill Rig	D.ecked	by	ΓV [ C. N	[88%] Marin	While Drilling At Completion Time After Dr Depth to Wat	n of Drilling	Ÿ Ÿ NA.			00 ft 30 ft		
WANG	upon completion						_			The stratificati between soil to	on lines repre	sent the app	roxim may b	ate b e gra	oundary idual.	/	



#### **BORING LOG CUL-02**

WEI Job No.: 195-13-01

Client Strand Associates, Inc.

Project IL 47 between US 14 and S of IL 176

Location McHenry County, Illinois

Datum: NAVD 88 Elevation: 905.10 ft North: 2032847.66 ft East: 959507.08 ft Station: 598+78.32 Offset: 52.77 RT

Profile	BESOKII HON	(ft) Sample Type	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)		CRIF	PTION		Depth (ff)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	
	904.93-inch thick, black to dark brown SILTY CLAY LOAM TOPSOIL/  Medium stiff to stiff, dark brown SILTY CLAY LOAM; trace gravelFILLRDR 2		1	2 2 5	1.50 P	16		Stiff	ay SAND urated f to very : AY LOAN vel; dam	stiff, pir	F nkish gr DAM, litt		-/ <del> </del>		9	7 8 11	1.50 P	11	
		5	2	4 3 3	0.90 B	18							25_/		10	7 8 12	3.20 B	9	
	898.1 897.6Black CLAY LOAM BURIED TOPSOIL		3	3 4 3	1.50 P	23									11	6 8 12	3.77 B	8	
	Soft, dark gray ORGANIC SILTY CLAY to CLAY with organic matter; moistRDR 1organic content= 7.0%1	0_	4	1 1 1	0.41 B	53							30		12	5 7 11	1.89 B	11	
	Soft, light gray CLAY to SILTY CLAY; wetRDR 1L <sub>L</sub> (%)=38, P <sub>L</sub> (%)=19%Gravel=0.1		5	1 1 2	0.41 B	28			dium der AVEL; s		ed		- - - - -						
	892.1%Sand=3.9%Silt=57.2%Clay=38.8A-6 (19)sand seams; moist Medium stiff, gray SILTY CLAY,  889.6trace gravel; moist	5	6	3 4 4	0.50 P	17		870.1 Bor	ring termi	inated		RDR 2	35		13	3 9 10	NP	14	
	Stiff, pinkish gray CLAY LOAM to LOAM; trace to little gravel; damp		7	3 4 7	1.56 B	10							- - -						
Beç Drill Drill Drill			8	3 5 9	1.64 B	10							40_						
5	GENERAL							]			WATE		VEL						
Beg Dril Dril	lling Contractor <b>Wang Testing Se</b> ller <b>K&amp;N</b> Logger <b>T. R</b>	othsc	[	Orill Rig	D.ecked	by	ΓV [ C. M	88%] /larin	Time Af	pletion o		Ş ¥ N.	Α			75 ft 50 ft		,	
PAN DUI	Drilling Method 2.25 IDA HSA; 140 Ib autohammer; Boring backfilled The stratification between soil by the stratification												Y NA es represent the approximate boundary he actual transition may be gradual.						



#### **BORING LOG CUL-02ST**

WEI Job No.: 195-13-01

Client Strand Associates, Inc.

Project IL 47 between US 14 and S of IL 176

Location McHenry County, Illinois

Datum: NAVD 88 Elevation: 905.10 ft North: 2032843.89 ft East: 959505.71 ft Station: 598+76.23 Offset: 49.34 RT

Profile	SOIL AND ROCK DESCRIPTION	Depth (ft) Sample Type	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND		Depth	Sample Type	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	Blind drilled to 9 feet		+									(0)				
		-														
		-														
		-														
		-														
		5														
		_														
		-														
		-														
		4														
	Gray SILTY CLAY; moist	100														
	C <sub>c</sub> =0.491, OCR=	=1.3 <sub>10</sub> _	1	P   U		44										
				S		44										
4	894.1 Boring terminated at 11.00 ft			Н												
	Borning terminated at 11.00 h	· -														
		_														
		-														
		-														
		15														
		-														
		-														
		_														
		-														
		-														
		20														
	GENE	RAL NOT	ES					Į.	,	WATER	R LEVE	L D	AT	Α		
_	gin Drilling 10-24-2017	Complete		-		0-24			While Drilling		<u> </u>			RY		
Drill Drill	lling Contractor Wang Testir ller K&N Logger															
	ller K&N Logger lling Method 3,25 IDA HSA; 1															
		TY.IV.GULUI	JOH			IIIU D	uun	····cu	- Dopur to water							



#### **BORING LOG CUL-03**

WEI Job No.: 195-13-01

Client Strand Associates, Inc.

Project IL 47 between US 14 and S of IL 176

Location McHenry County, Illinois

Datum: NAVD 88 Elevation: 900.30 ft North: 2032876.10 ft East: 959534.10 ft Station: 598+83.67 Offset: 91.63 RT

Profile	SOIL AND ROCK DESCRIPTION	Sample Type	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROO DESCRIPTION	0)	Sample Type	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	22-inch thick, medium stiff, black SILTY CLAY LOAM, some organic matterTOPSOIL Medium stiff, brown to gray SILTY CLAY LOAM, some fine sand and clay interbeds; wet	1	1 1 2	0.66 B	50				- - - -		9	5 8 11	3.28 B	9
	RDR 1  5_	2	2 2 1	0.80 B	17				- - - 25_		10	6 8 8	2.71 B	9
	L <sub>L</sub> (%)=26, P <sub>L</sub> (%)=13 %Gravel=4.2 %Sand=11.4 %Silt=61.3 %Clay=23.1 892.3A-6 (9)	3	2 3 4	0.82 B	21		872.3		- - - -		11	5 5 11	NR	
	Stiff, gray SILTY CLAY, trace gravel; dampRDR 2	4	3 4 5	1.31 B	17			dium dense, gray GR DARSE SAND; wet -	AVELLY - -RDR 2 - 30_ -		12	2 5 10	NP	14
	888.8 B888.3 Basa.3Gray SANDY GRAVEL; wet Stiff to very stiff, pinkish gray CLAY LOAM to SILTY LOAM, trace gravel; damp	5	9 7 6	1.48 B	10			ry stiff, gray SILTY CL AM; trace gravel	AY - -RDR 2					
	RDR 2  15_	6	4 5 6	1.80 B	10		865.3 <b>Bo</b> l	ring terminated at 35.0	- - 35 00 ft		13	6 5 6	2.05 B	13
8/10/18	- - -	7	10 10 9	2.30 B	10				- - - -	-				
MANGENGINC 1951301.6PJ WANGENG.GDI 8710718  Did	20_	8	8	1.89 B	10				- - - 40_	-				
	GENERAL N	IOTES	3					WAT	ER LEVE					
Be		mplete D	-		0-24			While Drilling	<u> </u>			50 ft		
P Dri	illing Contractor Wang Testing Serv							At Completion of Drillin			0.0	0 ft		
E Dri	iller K&N Logger F. E							Time After Drilling	NA V NA	••••				
S Dr	illing Method 3.25 IDA HSA; 140 Ib a upon completion				_		ınea	Depth to Water  The stratification lines re between soil types; the a	NA present the app	roxima	ate b	oundar	y	
≳I	upon compienon	. <b></b> .						between soil types: the a	ctual transition	mav be	e ara	idual.		



#### **BORING LOG CUL-03ST**

WEI Job No.: 195-13-01

Client Strand Associates, Inc.

Project IL 47 between US 14 and S of IL 176

Location McHenry County, Illinois

Datum: NAVD 88 Elevation: 900.30 ft North: 2032874.72 ft East: 959536.58 ft Station: 598+80.11 Offset: 93.47 RT

Profile	SOIL AND ROCK DESCRIPTION	Depth (ft) Sample Type	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL DES		ROCK TION	<b>C</b> Depth	Sample Type	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
1;1;	Drilled to 4 feet without sampling  896.3  Medium stiff, brown to gray	- - - - - - - -		Р													
<u> </u>	SILTY CLAY LOAM  894.3  Boring terminated at 6.00 ft	5	1	U % H	0.75 P												
		15															
Po	GENERAL NOTES  Begin Drilling 10-23-2017 Complete Drilling 10-23-2017								While D		VATE						
Dri Dri	Drilling Contractor Wang Testing Services Drill Rig D50 ATV [88%]  Driller K&N Logger F. Bozga Checked by CLM  Drilling Method 3.25 IDA HSA; 140 Ib autohammer; Boring backfilled upon completion								Time After Drilling NA								



#### **BORING LOG PT6-03**

WEI Job No.: 195-13-01

Client Strand Associates, Inc.

Project IL 47 between US 14 and S of IL 176

Location McHenry County, Illinois

Datum: NAVD 88 Elevation: 902.40 ft North: 2032729.17 ft East: 959454.53 ft Station: 598+18.68 Offset: 62.3 LT

Profile	SOIL AND ROCK deed DESCRIPTION	Sample Type	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND RO		Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	901.96-inch thick, black SILTY CLAY  LOAM TOPSOIL  Medium stiff, brown and black  SILTY CLAY; damp		1	1 3 4 4	0.98 B	19									
	Soft to stiff, black and gray SILTY CLAY, little to some organic matter; moist		2	2 2 3 4	1.00 P	57									
	RDR 2 5_ 896.9 Medium dense, gray LOAM;	-	3	1 1 1 2	0.49 B	30									
	moist to wetRDR 2		4	1 3 9 6	NP	19									
	Medium stiff to stiff, gray SILTY CLAY LOAM, trace gravel; dampRDR 2		5	3 2 3 6	0.75 P	16									
	890.4														
	Boring terminated at 12.00 ft														
	15_	- - - -													
8															
WANGENGINC 1951301.GPJ WANGENG.GDT 8/10/18															
NAW .	20_	1													
01.GF	GENERAL N					0.40	00	17		TER LEVE					
19513 D	egin Drilling 12-19-2017 Co rilling Contractor Wang Testing Serv	mplete vices		-		2-19 50 A			While Drilling  At Completion of Dril	<u>♀.</u> ling <u>¥.</u>			RY RY		
ONS Di	riller N&J Logger T. Ro								Time After Drilling	NA NA		ا بــــــــــــــــــــــــــــــــــــ	. 7. 1	• • • • • • •	•••••
D GEN	rilling Method 2.25 IDA HSA; 140 Ib a								Depth to Water	Ţ NA					
X X	upon completion		The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.												



#### **BORING LOG PT7-06**

WEI Job No.: 195-13-01

Client Strand Associates, Inc.

Project IL 47 between US 14 and S of IL 176

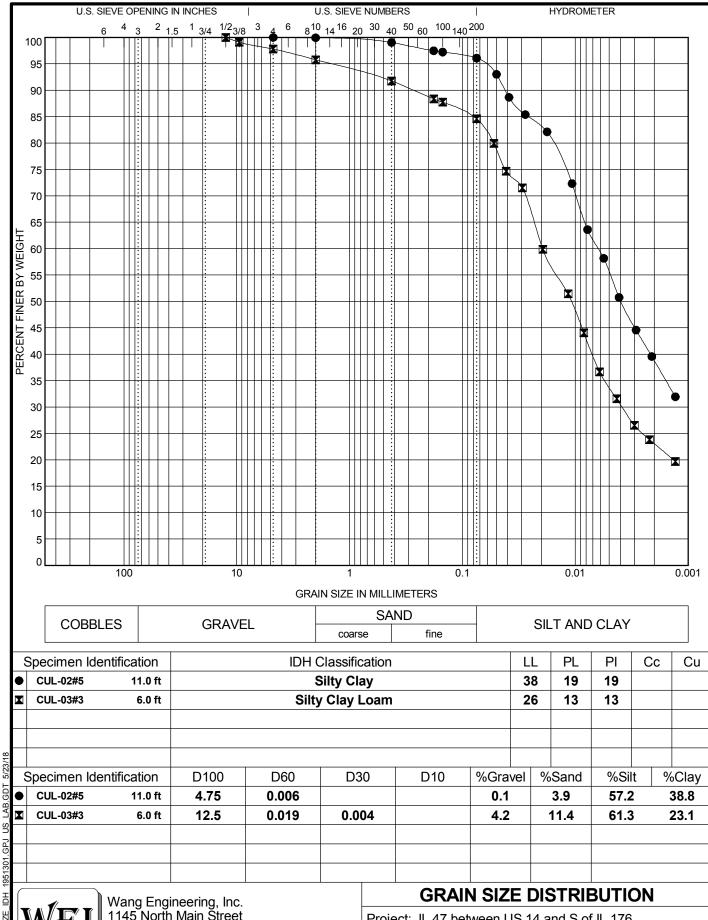
Location McHenry County, Illinois

Datum: NAVD 88 Elevation: 902.90 ft North: 2032817.50 ft East: 959549.94 ft Station: 598+28.00 Offset: 67.39 RT

Profile	SOIL AND ROCK DESCRIPTION	Depth (ft) Sample Type	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROC DESCRIPTION		Sample Type	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	8-inch thick, black SILTY CLAY  902.2LOAM, trace gravelTOPSOIL Stiff to very stiff, black, brown and gray SILTY CLAY, trace gravel;	-/  di	1	1 2 3 4	1.23 B	18									
	damp		2	3 3 4 4	2.62 B	25									
	897.4 Stiff, brown CLAY LOAM, trace gravel; damp	5	3	2 3 3 5	1.48 B	16									
	894.9		4	5 6 7 6	1.89 B	10									
	Boring terminated at 8.00 ft	-													
		10													
		-													
		1													
		-													
		-													
		15													
		-													
		-													
		-													
		-													
		-													
		20													
	GENERAL							4.7		R LEVE	L D				
Beg	Begin Drilling 12-07-2017 Complete Drilling 12-07-2017  Drilling Contractor Wang Testing Services Drill Rig D50 ATV [88%]								While Drilling  At Completion of Drilling	<u>Ş.</u>			RY RY		•••••
Dril									Time After Drilling	NA	•••••	ابر	! }.!	• • • • • • •	•••••
l	ling Method 2.25 IDA HSA; 140 I								Depth to Water	NA					
	upon completion					_			The stratification lines representation between soil types; the act		roxima may b	ate b e gra	oundarı ıdual.	/	



#### APPENDIX B



SINCE 1982

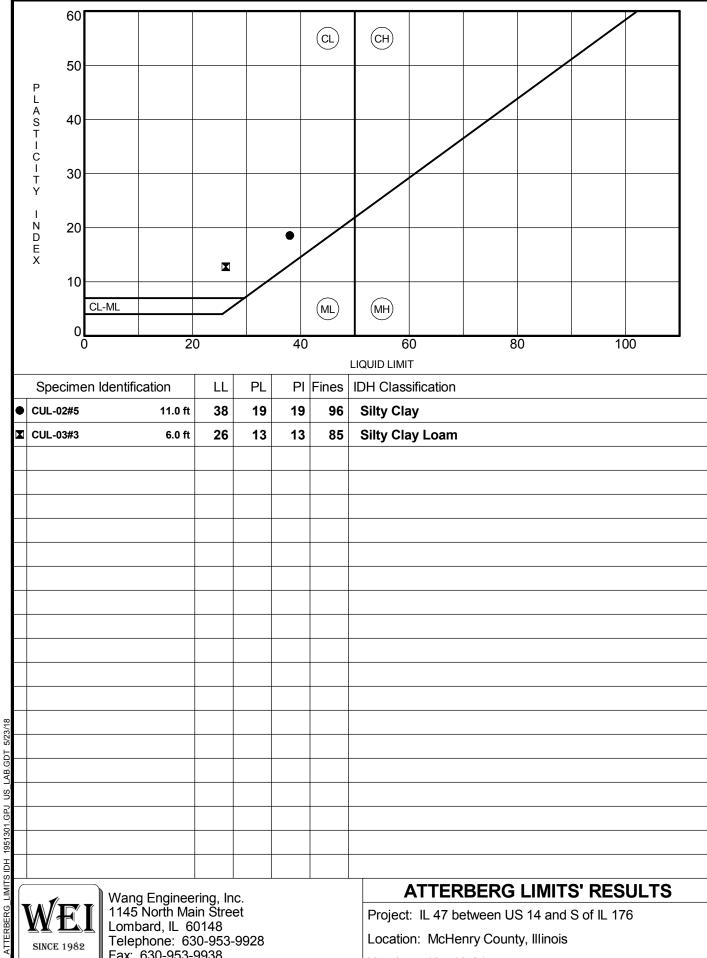
1145 North Main Street Lombard, IL 60148 Telephone: 630-953-9928

Fax: 630-953-9938

Project: IL 47 between US 14 and S of IL 176

Location: McHenry County, Illinois

Number: 195-13-01



SINCE 1982

Telephone: 630-953-9928 Fax: 630-953-9938

Location: McHenry County, Illinois

Number: 195-13-01



#### ONE-DIMENSIONAL CONSOLIDATION TEST **AASHTO T 216 / ASTM D 2435**

**Project: Illinois Route 47** Tested by: M. Snider Client: Strand Associates, Inc. Prepared by: M. Snider Soil Sample ID: Boring CUL-02ST, ST#1, 9 to 11 feet Test date: 12/15/2017 Sample Description: Gray SI CLAY WEI: 195-13-01 Initial sample height = 2.505 in 0.787 in Ring diameter = Initial sample mass = Ring mass = 110.25 g 63.49 g Initial water content = 44.02% Initial sample and ring mass = 173.74 g Initial dry unit weight = 75.20 pcf Tare mass = 63.49 g Final ring and sample mass = Initial void ratio = 1.157 161.65 g Initial degree of saturation = 98.89% Mass of wet sample and tare = 162.18 g Mass of dry sample and tare = 140.04 g Initial dial reading = Final sample mass = 98.69 g 0.01000 in Final dry sample mass = 76.55 g Final dial reading = 0.18018 in Final water content = 28.92% LL= % Final dry unit weight = 95.95 pcf PI =% Final void ratio = 0.691 % Sand= % Silt= Final degree of saturation = 100.00% Estimated specific gravity = % Clay= 2.60 **In-Situ Vertical Effective Stress =** 1400 psf **Compression and Swelling Indices** sf

Compression index $C_c =$	0.448	Preconsolidation pre	essure,s <sub>C</sub>
Field corrected C <sub>c</sub> =	0.491	Casagrande Method =	1835 psf
Swelling index $C_s =$	0.112	Over-Consolidation Ratio (OCR) =	1.31

Load number	Vertical stress	Dial reading	System deflection	Vertical strain	Void ratio	$C_{\rm v}$	Cae	Elapsed time
	psf	in	in	%		ft <sup>2</sup> /day	%	min
1	100.0	0.00932	0.00047	-0.03	1.158	N/A	N/A	720
2	200.0	0.01015	0.00066	0.10	1.155	0.1200	0.00	720
3	500.0	0.01597	0.00087	0.87	1.139	0.0506	0.14	720
4	1000.0	0.03003	0.00138	2.72	1.099	0.0267	0.37	960
5	2000.0	0.05713	0.00198	6.24	1.023	0.0205	0.79	960
6	4000.0	0.09524	0.00425	11.37	0.912	0.0190	0.98	1440
7	8000.0	0.13865	0.00648	17.17	0.787	0.0195	1.28	1440
8	16000.0	0.18529	0.00903	23.42	0.652	0.0194	1.42	1440
9	32000.0	0.22799	0.01063	29.05	0.531	0.0212	0.91	720
10	8000.0	0.22479	0.00809	28.32	0.546	N/A	N/A	2880
11	2000.0	0.20759	0.00386	25.60	0.605	N/A	N/A	720
12	500.0	0.18180	0.00183	22.06	0.681	N/A	N/A	1440

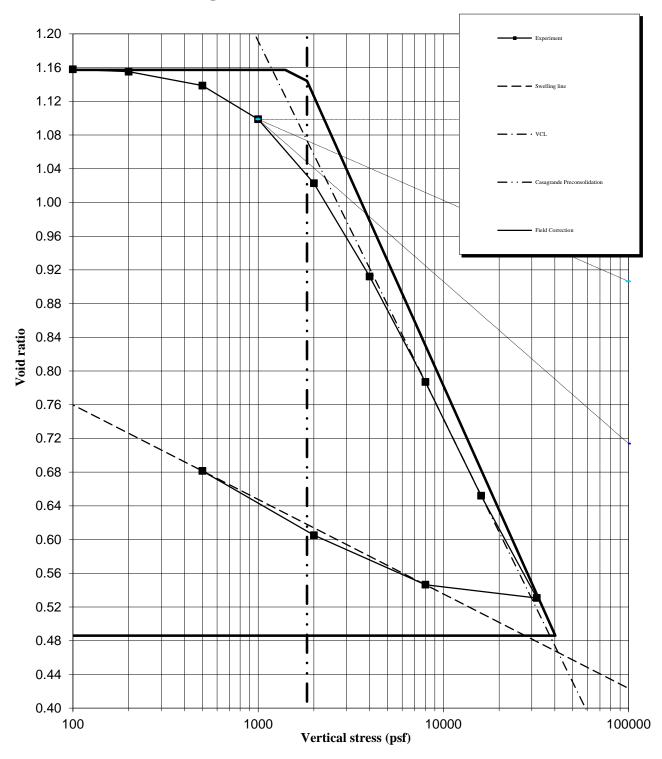
Prepared by: Dat	e:
Checked by: Dat	e:





#### **CONSOLIDATION CURVE**

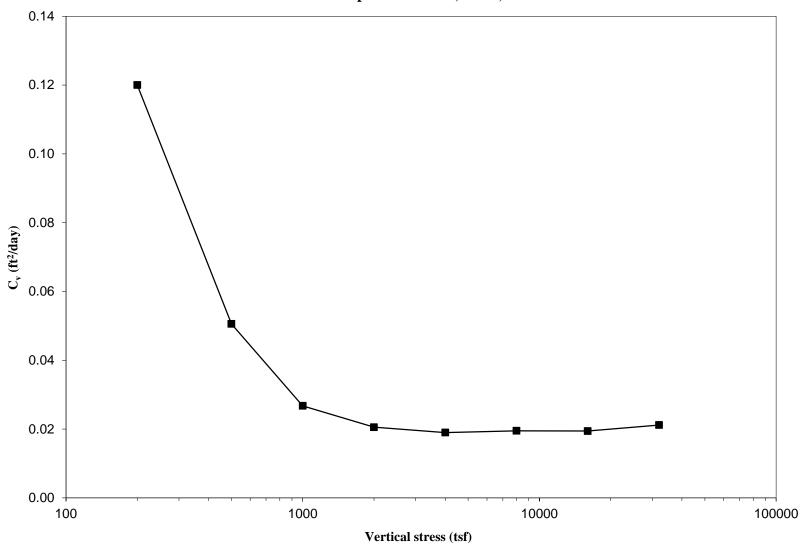
Sample CUL-02ST, ST#1, 9 to 11 feet







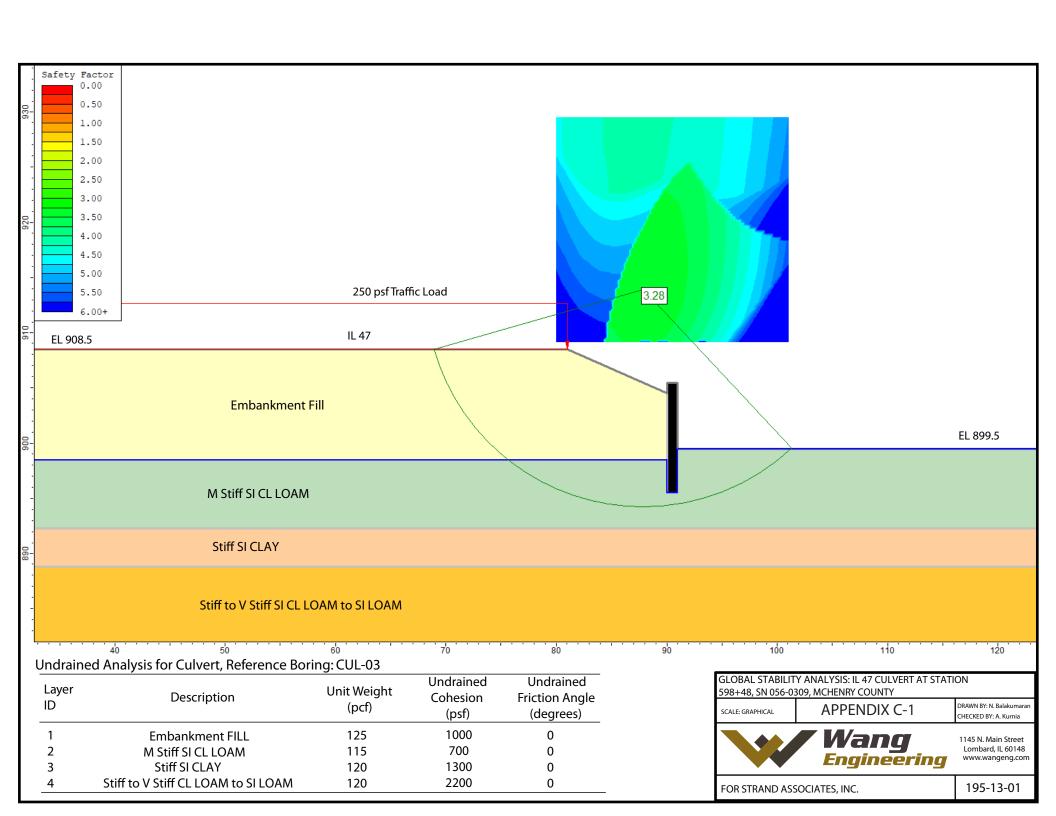
## CONSOLIDATION COEFFICIENT (C<sub>v</sub>) vs. VERTICAL STRESS Sample CUL-02ST, ST#1, 9 to 11 feet

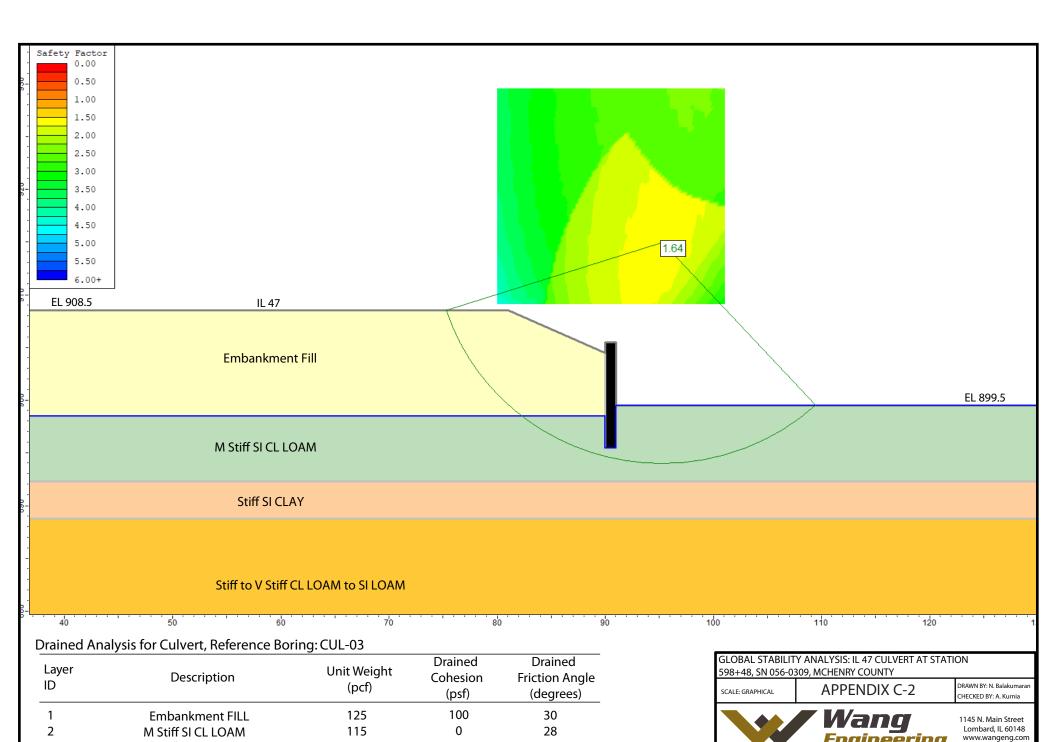






#### APPENDIX C





100

100

30

30

120

120

Stiff SI CLAY

Stiff to V Stiff CL LOAM to SI LOAM

3

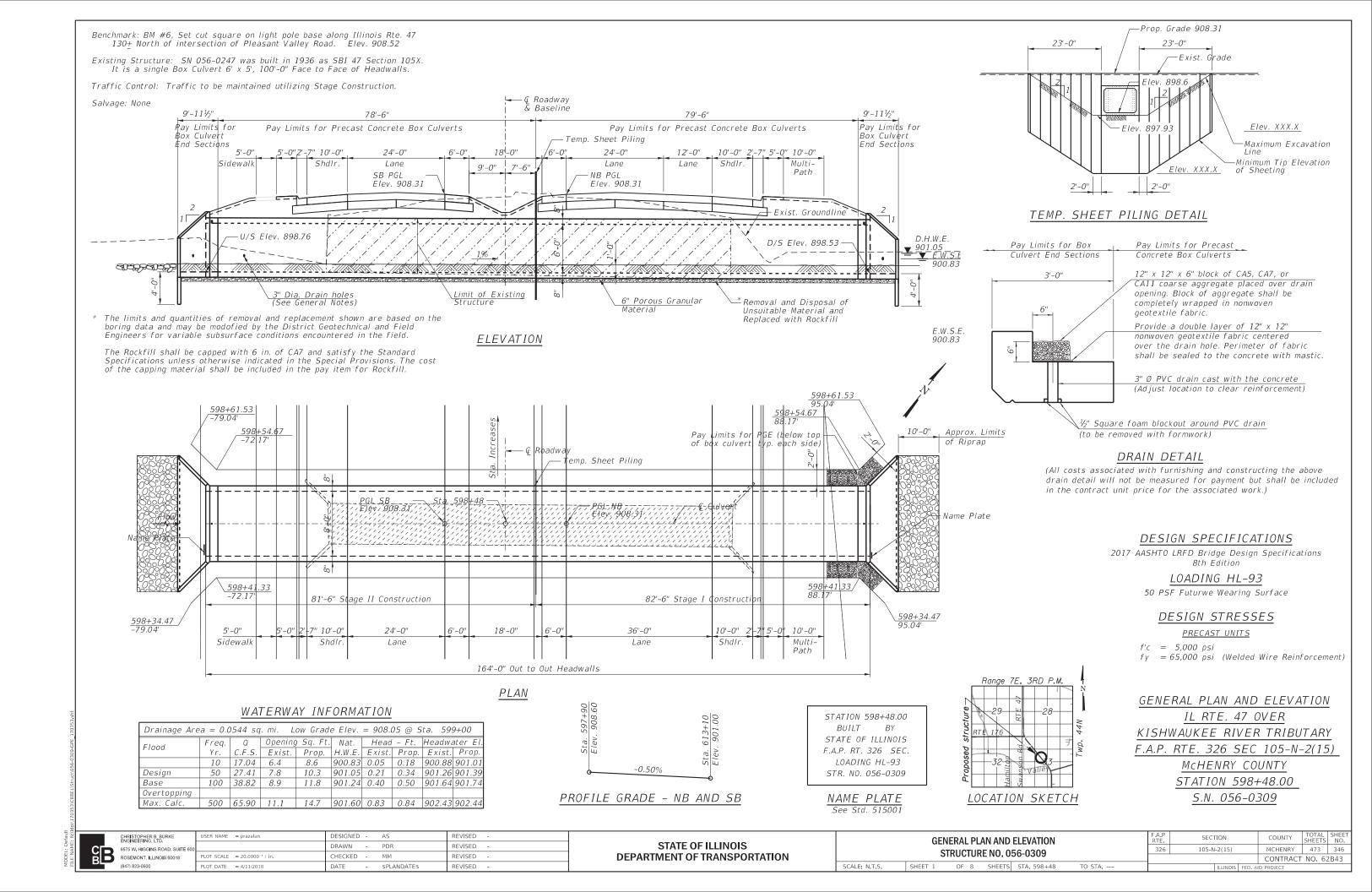
Engineering

FOR STRAND ASSOCIATES, INC.

195-13-01



#### APPENDIX D



#### GENERAL NOTES

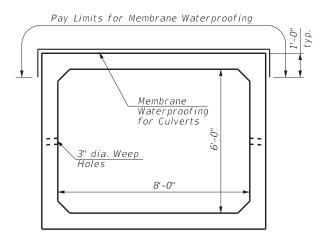
- 1 The design fill height for this box is 3'-0". The precast box culvert sections shall conform to the requirements of ASTM C 1577.
- 2. Drain holes shall be provided on exterior culvert walls for each precast box segment with a clear rise greater than 3 ft. The drain hole shall be located within 1/3 of the clear rise of the box culvert, shall not intercept the haunch, and shall conform to the requirements of Article 503.11 of the Standard Specification.
- 3. The 6 in. thick layer of porous granular material required for the precast concrete box culvert per Art. 540.06 of the Standard Specifications shall also apply to the end sections. Cost of the porous granular material will not be paid for separately but shall be included in the unit price of the work for which it is required.
- 4. Nonwoven geotextile fabric shall conform to the requirements of Art. 1080.01 of the Standard Specifications. The minimum weight of the fabric shall be 6 ounces per square yard.
- 5. Precast concrete box culverts and box culvert end sections shall be backfilled with Porous Granular Embankment below the top of the box culvert extending to a vertical plane 2 ft from the exterior sides of the culvert, 2 ft from the back face of the end sections, and not closer than 2 ft from the face of embankment.

#### INDEX OF SHEETS

- General Plan and Elevation
- 2 General Notes, Index of Sheets and Total Bill of Materials
- 3 Stage Construction Details
- 4 5 Precast Concrete Box Culvert Apron End Section Details
- 6 8 Existing Structure (For Information Only)

#### TOTAL BILL OF MATERIAL

ITEM	UNIT	TOTAL
Porous Granular Embankment	Cu. Yd.	247
Stone Riprap, Class A4	Sq. Yd.	56
Filter Fabric	Sq. Yd.	56
Removal of Existing Structures No. 1	Each	1
Structure Excavation	Cu. Yd.	566
Removal and Disposal of Unsuitable Material	Cu. Yd.	81
for Structures		
Name Plates	Each	1
Temporary Sheet Piling	Sq. Ft.	747
Box Culvert End Sections, Culvert No. 2	Each	2
Precast Concrete Box Culverts 8' X 6'	Foot	158
Membrane Waterproofing for Buried Structures	Sq. Yd.	207
Dewatering	L. Sum	0.25
Rock Fill	Cu. Yd.	81



MEMBER WATERPROOFING FOR PRECAST CULVERTS

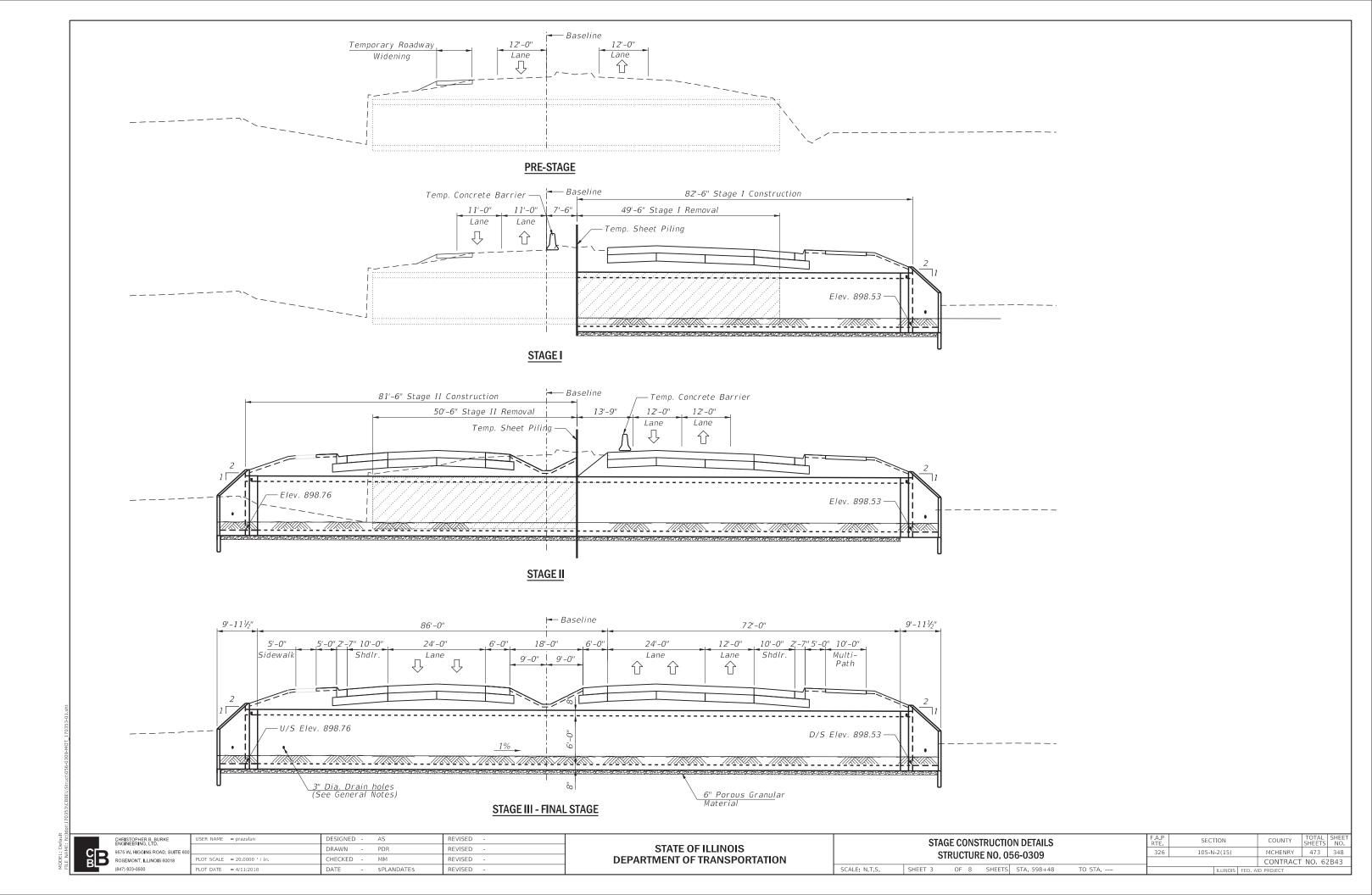
Forr Fill Height ≤ 3 ft.

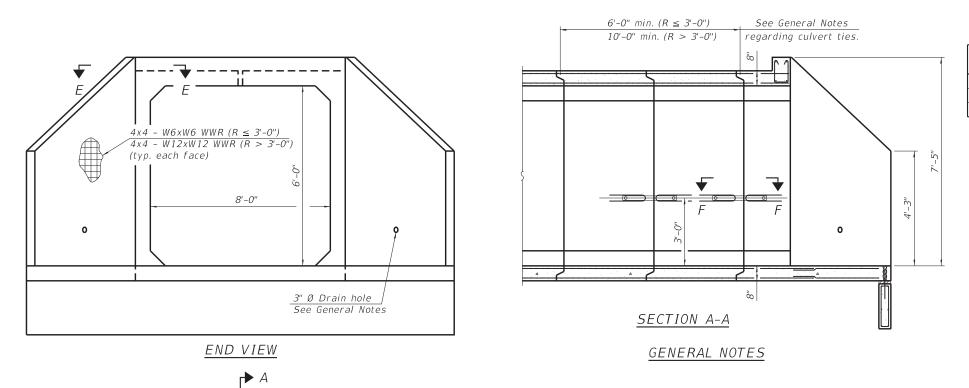
ßВ

CHRISTOPHER B. BURKE ENGINEERING, LTD.	USER NAME = prazalan	DESIGNED - AS	REVISED -
9575 W. HIGGINS ROAD, SUITE 600		DRAWN - PDR	REVISED -
ROSEMONT, ILLINOIS 60018	PLOT SCALE = 2.0000 / in.	CHECKED - MM	REVISED -
(847) 823-0500	PLOT DATE = 4/11/2018	DATE - \$PLANDATE\$	REVISED -

GENERAL N				HEETS AN RE NO. 0		L BILL OF MATERIALS 9
SCALE: N.T.S.	SHEET 2	OF	8	SHEETS	STA.	TO STA

F.A.P RTE	SEC <sup>-</sup>	ΓΙΟΝ		COUNTY	TOTAL SHEETS	SHEE NO.
326	105-N	I-2(15)		MCHENRY	473	347
				CONTRACT	NO. 62	2B43
		ILLINOIS	FED. A	ID PROJECT		





Culvert Ties (typ.)

1'-0"

#### APRON END SECTION DIMENSIONS

Span (S)	Rise (R)	Tt	Tb	Ts	А	В	С	D	Ε	Concrete Cu. Yd.	Culvert Ties Required
8'-0"	6'-0"	8"	8"	8"	7'-5"	4'-3"	6'-111½"	9'-10"	24'-21/4"	11.0	Yes

Two sets of apron end section dimensions are shown above for some box culvert sizes due to the top and bottom slabs having different thicknesses per ASTM C 1577 for design fill heights less than 2 ft.

PLAN

24'-21/4"

See Section D-D

\_\_\_\_

· ---

 $\vdash B$ 

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 $4x4 - W6xW6 WWR (Tb \le 5")$ 4x4 - W12xW12 WWR (Tb > 5")

(typ. top and bottom)

SCB-AES

2-17-2017

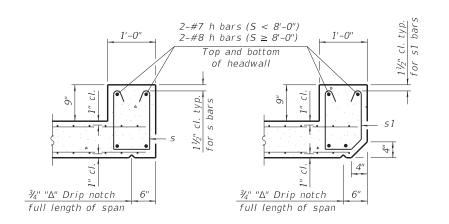
JSER NAME = prazalan DESIGNED - AS REVISED CHRISTOPHER B. BURKE ENGINEERING, LTD. DRAWN -PDR REVISED 9575 W. HIGGINS ROAD, SUITE 6 LOT SCALE = 2.0000 ' / in. CHECKED -REVISED ROSEMONT, ILLINOIS 60018 PLOT DATE = 4/11/2018 DATE REVISED \$PLANDATE\$

STATE OF ILLINOIS **DEPARTMENT OF TRANSPORTATION**  PRECAST CONCRETE BOX CULVERT APRON END 326 SECTION DETAILS - STRUCTURE NO. 056-0309 SHEET 4 OF 8 SHEETS STA. 598+48

SECTION COUNTY 105-N-2(15) MCHENRY 473 349 CONTRACT NO. 62B43

(Sheet 1 of 2)

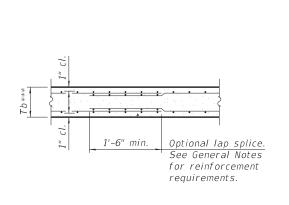
SCALE: N.T.S.



SECTION B-B (Top slab at downstream end)

SECTION E-E

SECTION B-B



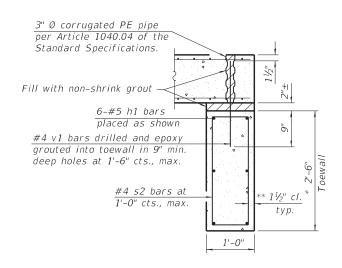
SECTION B-B

SECTION C-C

1'-6"

1" cl.

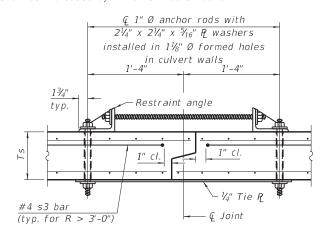
Bonded construction joint



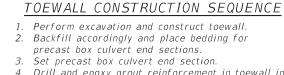
SECTION D-D

(Top slab at upstream end) (Bottom Slab)

\*\*\* This dimension shall be increased by 2" for CIP construction.



SECTION F-F (Showing culvert tie details)



- 4. Drill and epoxy grout reinforcement in toewall in accordance with Section 584 of the Standard Specifications.
- 5. Pressure grout voids using non-shrink grout conforming to Section 1024 of the Standard Specifications.
- \* The Contractor may furnish a precast or cast-in-place toewall. The Contractor shall be responsible for the strength and stability of the precast toewall during handling. Additional lifting points may be required depending upon the length of the toewall or the Contractor may need to modify the design of the toewall for the proposed handling method.
- $^{**}$  If soil conditions permit, the sides of the toewall may be poured directly against the soil. The clear cover on the sides of the toewall shall be increased to 3" by increasing the thickness of the toewall.

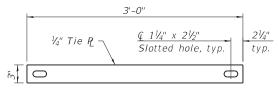
COUNTY

MCHENRY 473 350

CONTRACT NO. 62B43

### Q 11/4" Ø hole for 1" Ø anchor rod with <u>Ç</u> 1¼" Ø hole in 21/4" x 21/4" x 5/16" bottom leg of angle

#### RESTRAINT ANGLE DETAIL





9"

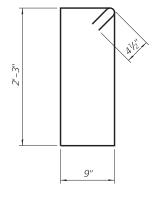
BAR s

31/8"

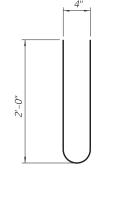
#4 s or s1 bars at spacing = Tt

(Spacing need not be less than 8")

BAR s1



BAR s2



BAR s3

TIE PLATE DETAIL

1" Ø anchor rods for the culvert ties shall conform to the requirements of ASTM F1554, Grade 105. Structural steel for the tie plate and restraint angle shall conform to the requirements of Article 1006.04 of the Standard Specifications. All components of the culvert tie detail shall be galvanized according to the requirements of AASHTO M 111 or M 232 as applicable.  $2\frac{1}{4}$ "  $\times 2\frac{1}{4}$ "  $\times 2\frac{1}{4}$ "  $\times 2\frac{1}{6}$ " plate washers shall be provided under each nut required for the anchor rods. Anchor rods connecting precast sections shall be brought to a snug tight condition followed by an additional  $lac{1}{2}$  turn on one of the nuts for anchor rods installed in the walls. Match marks shall be provided on the bolt and nut to verify relative rotation between the bolt and the nut. Holes in the walls for the culvert tie assembly may be drilled using core bits in lieu of using formed holes.

SCALE: N.T.S.

CHRISTOPHER B. BURKE ENGINEERING, LTD. 9575 W. HIGGINS ROAD, SUITE ROSEMONT, ILLINOIS 60018

JSER NAME = prazalan DESIGNED -AS REVISED DRAWN -PDR REVISED OT SCALE = 2.0000 ' / in. HECKED -REVISED DATE REVISED LOT DATE = 4/11/2018 SPLANDATES

STATE OF ILLINOIS **DEPARTMENT OF TRANSPORTATION** 

(Sheet 2 of 2)		
PRECAST CONCRETE BOX CULVERT APRON END	F.A.P RTE	SECTION
SECTION DETAILS - STRUCTURE NO. 056-0309	326	105-N-2(15)
SECTION DETAILS - STRUCTURE NO. 030-0303		
SHEET 5 OF 8 SHEETS STA. 598+48 TO STA		ILLINOIS FE