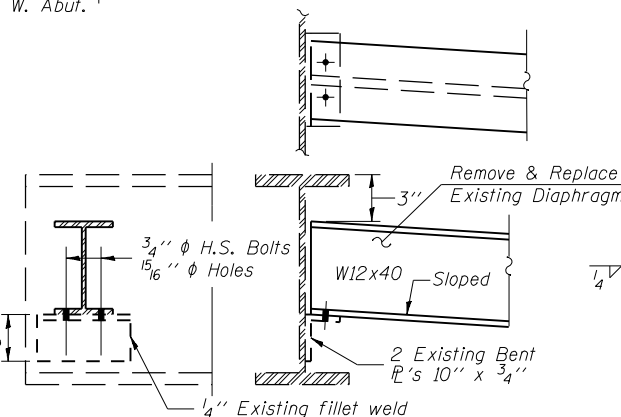


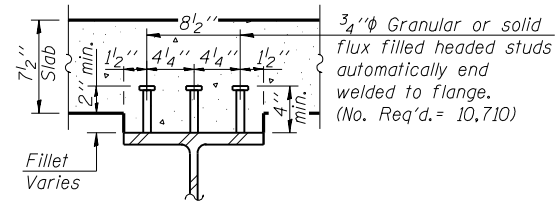
BEAM ELEVATION

"NTR" denotes members to which notch toughness requirements are applicable. For dimensions b thru k see sheet 20 of 44.

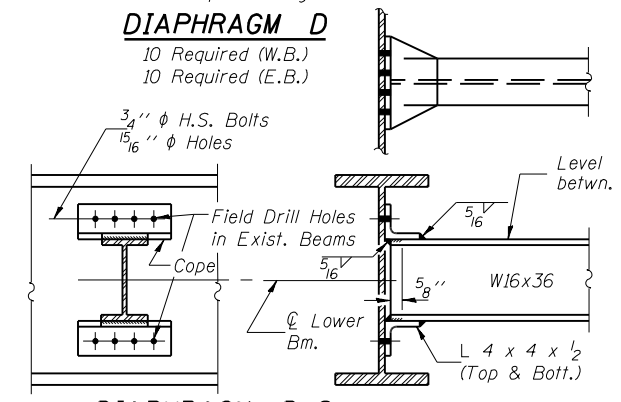


DIAPHRAGM D-1

2 Required (W.B.)
2 Required (E.B.)

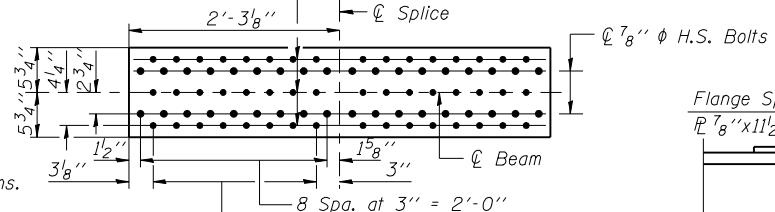


SECTION A-A



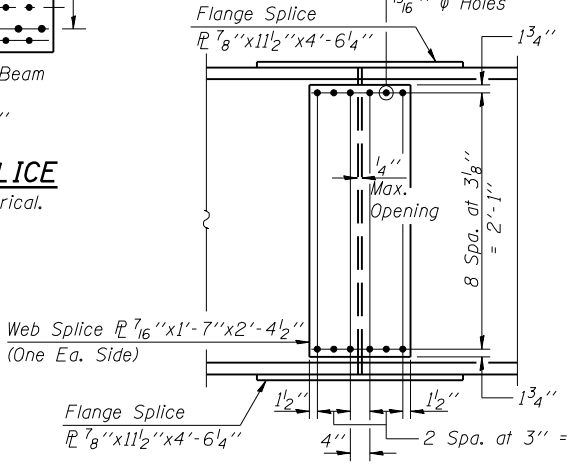
DIAPHRAGM D

10 Required (W.B.)
10 Required (E.B.)



SHEAR STUD LAYOUT AT SPLICE

H.S. Bolts and Stud patterns are symmetrical.



FIELD SPLICE DETAIL

H.S. Bolts shall conform to AASHTO M-164 Specifications (ASTM A325)

BEAM DIMENSIONS

(Measured Along Centerline of Beam)

Line No.	Beam 1	Beam 2	Beam 3	Beam 4	Beam 5	Beam 6	Beam 7	Beam 8	Beam 9	Beam 10	Beam 11	Beam 12	Beam 13	Beam 14
l	11'-1 7/16"	11'-1 7/8"	11'-0 7/8"	11'-0 5/8"	11'-0 1/2"	11'-0"	10'-11 3/4"	10'-8 5/8"	10'-8 1/2"	10'-8 1/8"	10'-7 3/4"	10'-7 5/8"	10'-7 1/4"	10'-7 1/16"
m	12'-1 1/2"	12'-1 1/2"	12'-1 3/8"	12'-1 1/4"	12'-1 1/8"	12'-1 1/8"	12'-1"	12'-0 3/8"	12'-0 1/4"	12'-0 1/8"	12'-0"	11'-11 7/8"	11'-11 7/8"	11'-11 3/4"
n	11'-11 1/2"	11'-11 1/4"	11'-10 7/8"	11'-10 1/2"	11'-10 1/8"	11'-9 3/4"	11'-9 5/8"	11'-6 1/2"	11'-6 1/4"	11'-5 7/8"	11'-5 7/8"	11'-5 1/2"	11'-5 1/8"	11'-5"
o	11'-6 1/8"	11'-6 1/8"	11'-6 1/8"	11'-6 1/8"	11'-6"	11'-6"	11'-5 3/4"	11'-5"	11'-4 7/8"	11'-4 3/4"	11'-4 1/2"	11'-4 1/2"	11'-4 1/2"	11'-4 3/8"
p	13'-2 5/8"	13'-2 1/4"	13'-1 7/8"	13'-1 1/2"	13'-1 1/4"	13'-0 7/8"	13'-0 1/2"	12'-9"	12'-8 5/8"	12'-8 1/2"	12'-8 1/4"	12'-8"	12'-7 3/8"	12'-7 1/4"
q	11'-8"	11'-8"	11'-7 5/8"	11'-7 1/2"	11'-7 1/2"	11'-7 1/2"	11'-7 3/8"	11'-6 1/2"	11'-6 1/2"	11'-6 1/4"	11'-6"	11'-5 7/8"	11'-5 7/8"	11'-6 5/8"
r	6 3/8"	6 1/8"	6"	5 5/8"	5 1/8"	4 7/8"	4 1/2"	5 3/4"	5 3/8"	5 1/8"	5"	4 3/4"	4 3/8"	3 7/16"

	0.4 Sp. 1 or 0.6 Sp. 4	Pier #1 or #3	0.5 Sp. 2 or Sp. 3	Pier #2
Is (in ⁴)	6710	6710	6710	6710
Ic (n) (in ⁴)	21228	-	21228	-
Ic (3n) (in ⁴)	15074	-	15074	-
Ss (in ³)	406	406	406	406
Sc (n) (in ³)	665	-	665	-
Sc (3n) (in ³)	591	-	591	-
Sr (in ³)	18.9	18.9	18.9	18.9
φ (k/ft.)	0.81	1.08	0.81	1.08
M _D (k)	168.2	369.0	134.9	354.8
s _D (k/ft.)	0.27	-	0.27	-
M _{sD} (k)	58.5	-	47.6	-
M _L (k)	305.7	243.4	289.8	248.1
M (Imp) (k)	76.4	48.7	72.5	49.6
5 ₃ [M _L +M(Imp)] (k)	636.8	486.8	603.8	496.2
Ma (k)	1122.6	1112.5	1022.2	1106.3
M _{D1} (k)	0.5	0.0	0.35	0.0
f _{sD} non-comp (k.s.i.)	5.0	10.9	4.0	10.5
f _{sD} (comp) (k.s.i.)	1.2	-	1.0	-
f _{s53} [M _L +M(Imp)] (k.s.i.)	11.5	14.4	10.9	14.7
f _i (k.s.i.)	0.3	0.0	0.2	0.0
f _s (Overload) (k.s.i.)	17.7	25.3	15.9	25.2
f _s (Total) (k.s.i.)	23.0	32.9	20.7	32.8
F _{cr} (Overload) (k.s.i.)	34.2	34.2	34.2	34.2
VR (k)	56.2	-	58.4	-
F _{cr} (k.s.i.)	35.9	36.0	35.9	36.0

F_{cr} Critical average flange stress (smaller of F_{cr1} or F_{cr2} for partially braced flanges and F_y for continuously braced flanges) computed according to the 2003 AASHTO Guide Specifications for Horizontally Curved Steel Girder Highway Bridges (Sections 5.2, 5.3 and 5.4).

F_{cr} (Overload) Critical average flange stress at overload computed according to the 2003 AASHTO Guide Specifications for Horizontally Curved Steel Girder Highway Bridges Section 9.5. I_s and S_s are the moment of inertia and section modulus of the steel section used in computing f_s (Total & Overload).

I_{c(n)} and S_{c(n)} are the moment of inertia and section modulus of the composite section used in computing stresses due to Live Load.

I_{c(3n)} and S_{c(3n)} are the moment of inertia and section modulus of the composite section used in computing stresses due to superimposed dead loads. (see AASHTO 10.38)

VR is the maximum Live Load + Impact shear range in span.

M_D Moment due to dead loads on non-composite section.

M_{sD} Moment due to dead loads on composite section.

M_L Moment due to live load on non-composite or composite section.

M (Imp) Moment due to live load impact on non-composite or composite section.

Ma (Applied Moment)=1.3[M_D + M_{sD} + 5₃(M_L + M(Imp))].

f_s (Overload) is the sum of the stresses due to M_D + M_{sD} + 5₃(M_L + M(Imp)).

f_s (Total) is the sum of the stresses due to 1.3[M_D + M_{sD} + 5₃(M_L + M(Imp))].

S_{b1} is the section modulus for one flange for lateral flange bending.

M_{D1} is the lateral bending moment for flange (factored).

f_i is the calculated normal stress at the edge of flange due to lateral bending (factored).

M_L and R_L include the effects of centrifugal force and superelevation.

	E.&W. Abut.	Piers #1 & #3	Pier #2
R _D (k)	22.5	70.6	68.3
R _L (k)	41.5	49.4	49.2
Imp. (k)	12.4	14.8	14.7
R (Total) (k)	76.4	134.8	132.2

Corporate License Number 184-001-084

STRUCTURAL STEEL DETAILS
F.A.I. 72 OVER UNION PACIFIC RAILROAD
SECTION (84-9-4)A,HBK,BY,BY-1
SANGAMON COUNTY
STATION 608+51.98
STR NO. 084-0074 EB - 084-0075 WB

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HANSON
JOB# 96S2002B
DATE 01/12/06

MMW 06/27/03
DAP 07/17/03
JMM 10/27/03
LAYOUT
DRAWN
REVIEWED

Location	Beam	Beam #1	Beam #14
⊙ Brg. W. Abut.		631.16	632.81
⊙ Pier #1		631.25	632.95
⊙ Splice #1		631.27	632.99
⊙ Pier #2		631.31	633.09
⊙ Splice #2		631.33	633.12
⊙ Pier #3		631.30	633.15
⊙ Splice #3		631.29	633.16
⊙ Brg. E. Abut.		631.28	633.20

* For Fabrication only.