### STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION

INTERIOR GIRDER MOMENT TABLE							
		0.4 Sp. 1	Pier	0.5 Sp. 2			
Is	(in4)	10926	18227	13797			
Ic (n)	(in4)	27333		31856			
Ic (3n)	(in4)	20641		24064			
Ss	(in 3)	502	814	627			
Sc (n)	(in <sup>3</sup> )	703		834			
Sc (3n)	(in 3)	645		769			
Ζ	(in <sup>3</sup> )						
Q (A	(/ft.)	0.742	1.251	0.766			
M₽	('k)	72	- <i>127</i> 5	582			
sl (k	(/ft.)	0.450		0.450			
Ms₽	('k)	72		402			
M4	('k)	412	- 492	735			
M (Imp)	('k)	107	- 113	147			
<sup>5</sup> 3[M \( + M(Imp) ]	('k)	865	- 1008	1470			
Ма	('k)	1312	- 2968	3190			
Mu	('k)	2888		4000			
fs₽ non-comp	(ksi)	1.7	- 18 <b>.</b> 8	11.1			
fs₽(comp)	(ksi)	1.3		6.3			
fs5 <sub>3</sub> (4+Imp)	(ksi)	14.8	- 14.9	21.2			
fs (Overload)	(ksi)	17.8	- 33.7	38.6			
fs (Total)	(ksi)		- 43.8				
VR	(k)	47.0		42.0			

INTERIOR GIRDER REACTION TABLE						
		Abut.	Pier			
R₽	(k)	22	134			
R4	(k)	32	53			
Imp.	(k)	9	13			
R (Total)	(k)	63	200			

Is and Ss are the moment of inertia and section modulus of the steel section used in computing fs (Total & Overload).

 $\mathit{Ic}_{(n)}$  and  $\mathit{Sc}_{(n)}$  are the moment of inertia and section modulus of the composite section used in computing stresses due to Live Load.

 $Ic_{(3n)}$  and  $Sc_{(3n)}$  are the moment of inertia and section modulus of the composite section used in computing stresses due to superimposed dead loads. (see AASHTO 10.38)

VR is the maximum Live Load + Impact shear

Z is the plastic section modulus used to determine the fully plastic moments in the non-composite areas.

Ma (Applied Moment)=1.3[M $^{Q}$  + Ms $^{Q}$  +  $^{5}$ 3(M $^{4}$  + M(Imp))]. The Plastic Moment capacity (Mu) is computed according to AASHTO 10.48.1 and 10.50.1.1.

fs (Overload) is the sum of the stresses due

DESIGNED D.J.T. & S.D.S.

CHECKED J.J.P. & S.D.S.

DRAWN L.M.G. & D.L.H.

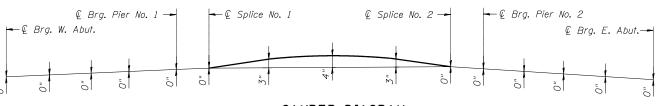
CHECKED D.J.T. & S.D.S.

to MQ + MsQ +5 $_3(MQ$  + M(Imp)). fs (Total) (Non-compact section) is the sum of the stresses due to 1.3[MQ + MsQ +  $5_3(M4 + M(Imp))$ ].

TOP OF WEB ELEVATIONS *								
Girder	€ Brg. W. Abut.	ℚ Brg. Pier No. 1	© Splice 1	© Splice 2	ℚ Brg. Pier No. 2	€ Brg. E. Abut.		
1	529.31	529.52	529.56	529.60	529.54	529.22		
2	529.42	529.63	529.67	529.71	529.65	529.33		
3	529.51	529.72	529.76	529.80	529.74	529.43		
4	529.51	529.72	529.76	529.80	529.74	529.43		
5	529.42	529.63	529.67	529.71	529.65	529.33		
6	529.31	529.52	529.56	529,60	529 <b>.</b> 54	529,22		

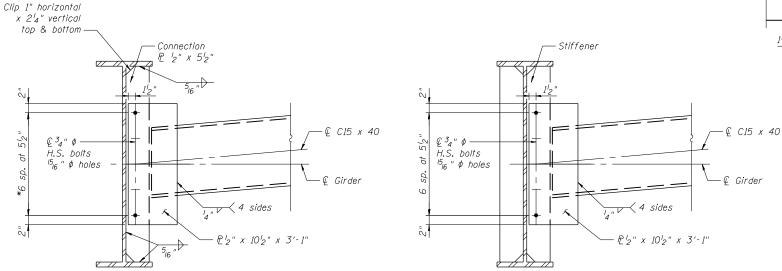
Top of web elevations at the splices have been adjusted for dead load deflection.





### CAMBER DIAGRAM

\*  $2^{3}_{16}$ " vertical x  $^{15}_{16}$ " slotted holes in connection  $P_{c}$  at south side of Girder 3 only. Provide 516" hardened washers for all slotted holes. The bolts for slotted holes shall only be finger tightened prior to pouring the Stage II deck then fully tightened after completion of the pour. The top of the slotted holes shall be located at the final diaphragm bolt locations.



## DIAPHRAGM Di

Two hardened washers required for each set of oversized holes. All diaphragms shall be installed as steel is erected and secured with erection pins and bolts except as otherwise noted. Individual diaphragms at supports may be temporarily disconnected to install bearing anchor rods. Load carrying components designated "NTR" shall conform to the Supplemental Requirements for Notch Toughness, Zone 2.

STRUCTURAL STEEL DETAILS IL ROUTE 10 OVER PRAIRIE CREEK F.A.P. ROUTE 717 - SECTION 101B-1 LOGAN COUNTY STATION 254+75.91 STRUCTURE NO. 054-0507

SHEET NO.

27

⊢*Fill P*2 <sup>3</sup>8" x 12" x 2′-3"

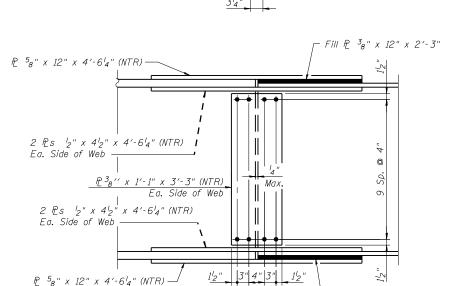
49

SHEET NO. 11

23 SHEETS

# DIAPHRAGM D 55 Required



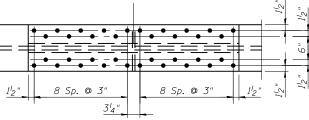


F.A.P. 717

101B-1

Contract #72A04

LOGAN



#### FIELD SPLICE DETAIL (Splice 1 shown Splice 2 similar by rotation thru 180°)