

INTERIOR BEAM MOMENT TABLE

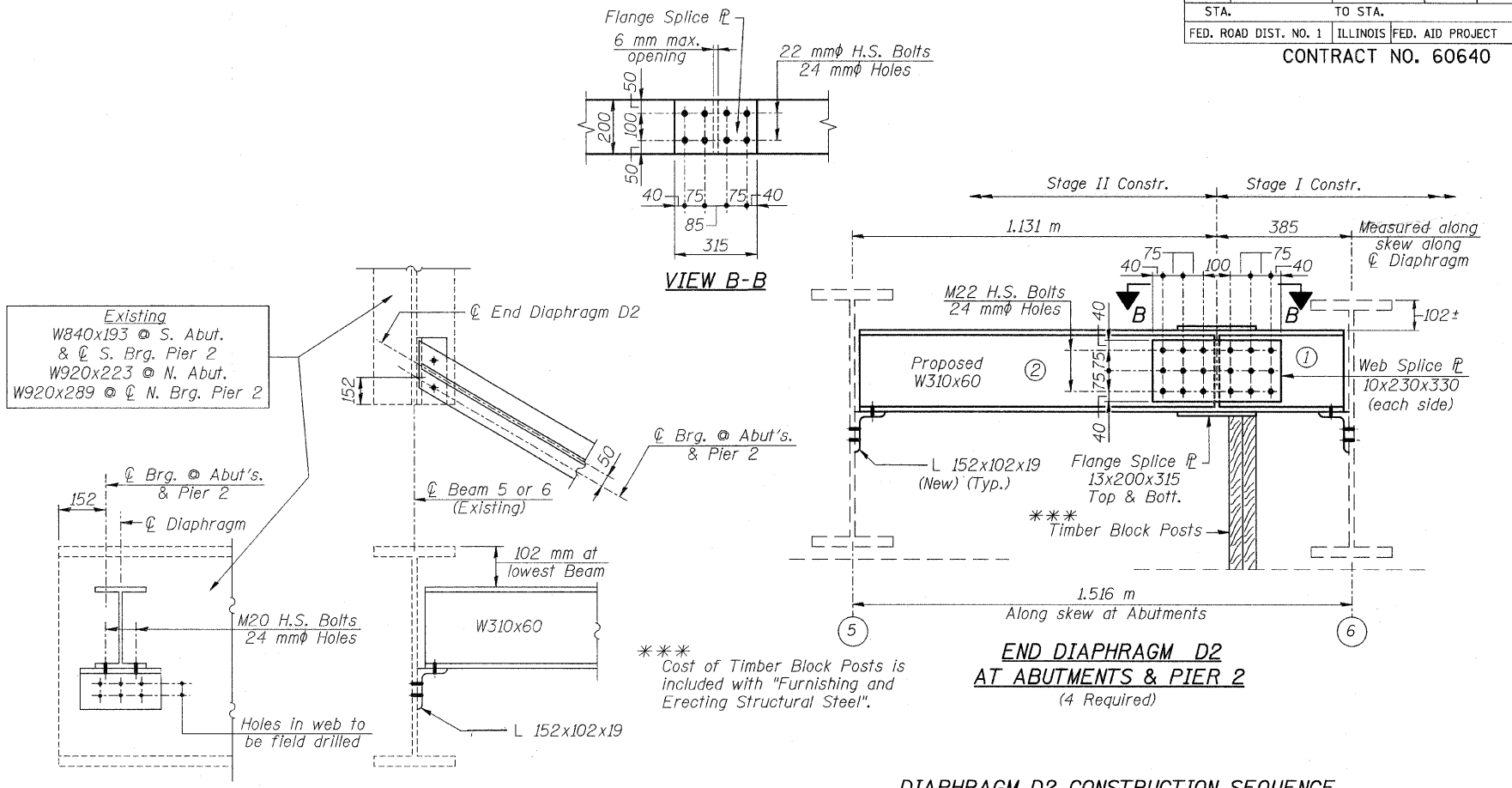
	0.5 Sp. 3	0.4 Sp. 2	Pier 2	0.6 Sp. 1
I_s (10^6 mm^4)	3,412	7,886	14,547	7,181
$I_c (n)$ (10^6 mm^4)	10,001	18,870	-	16,762
$I_c (3n)$ (10^6 mm^4)	7,134	13,174	-	11,882
S_s (10^3 mm^3)	8,947	19,674	29,355	16,874
$S_c (n)$ (10^3 mm^3)	13,200	26,495	-	22,824
$S_c (3n)$ (10^3 mm^3)	11,995	23,825	-	20,522
Z (10^3 mm^3)	-	-	30,143	-
M_D (kN.m)	12.99	15.16	21.49	14.97
M_L (kN.m)	398	968	2,688	720
s_D (kN/m)	6.57	6.42	-	6.42
$M_s D$ (kN.m)	202	477	-	380
M_L (kN.m)	570	1,166	936	1,018
M (Imp) (kN.m)	162	256	209	231
$S_3 [M_L + M(IMP)]$ (kN.m)	1,220	2,370	1,908	2,082
M_a (kN.m)	2,366	4,960	5,975	4,137
M_u (kN.m)	4,073	7,426	-	6,543
$f_s D$ non-comp (MPa)	44.5	49.2	91.6	42.7
$f_s D$ (comp) (MPa)	16.8	20.0	-	18.5
$f_s S_3$ (k+Imp) (MPa)	92.5	89.5	65.0	91.2
f_s (Overload) (MPa)	153.8	158.7	156.6	152.4
f_s (Total) (MPa)	-	-	203.6	-
VR (kN)	219	238	-	242

* Compact Braced Section
 ** Non-Compact Section

NOTES:
 I_s and S_s are the Moment of Inertia and Section Modulus of the steel section used in computing f_s (Total and Overload).
 $I_c(n)$ and $S_c(n)$ are the Moment of Inertia and section modulus of the Composite Section used in computing stresses due to Live Load.
 $I_c(3n)$ and $S_c(3n)$ are the Moment of Inertia and Section Modulus of the Composite Section used in computing stresses due to Superimposed Dead Load. (See AASHTO 10.38).
 VR is the maximum $L +$ Impact Shear Range in span.
 Z is the Plastic Section Modulus used to determine the fully Plastic Moments in the Non-Composite areas.
 The Plastic Moment Capacity (M_u) is computed according to AASHTO 10.48.1 & 10.50.1.1.
 f_s (Total) (Non-Compact Section) the sum of the stresses due to $1.3[M_D + M_s D + 5/3(M_L + M(IMP))]$.
 f_s (Overload) is the sum of the stresses due to $M_D + M_s D + 5/3(M_L + M(IMP))$.
 M_D - moment due to Dead Loads on Non-Composite Section.
 $M_s D$ - moment due to Dead Loads on Composite Section.
 M_L - moment due to Live Load on Non-Composite or Composite Section.
 $M(IMP)$ - moment due to Live Load Impact on Non-Composite or Composite Sections.
 M_a (Applied Moment) = $1.3[M_D + M_s D + 5/3(M_L + M(IMP))]$

INTERIOR BEAM REACTION TABLE

	South Abutment	Pier 2		Pier 1	North Abutment
		Sp. 3	Sp. 2		
R_D (kN)	153	153	250	827	218
R_L (kN)	171	171	186	302	183
Imp. (kN)	48	48	41	68	42
R (Total) (kN)	372	372	477	1,197	443



NOTES:
 Two hardened washers shall be required over all oversize holes for diaphragms.
 All dimensions are in millimeters (mm) except as noted.

- DIAPHRAGM D2 CONSTRUCTION SEQUENCE**
- Order Diaphragm D2 in two sections with lengths of 1.11m and 365.
 - Attach Section ① of Diaphragm to Beam 6 and Top Flange Splice Plate during Stage I Construction.
 - Place Timber Block Posts between Section ① of Diaphragm and Abutment Bearing Seat.
 - Attach Section ② of Diaphragm to both Beam 5 and Top Flange Splice Plate during Stage II Construction.
 - Attach Web Splice Plates to Sections ① and ② of Diaphragms.
 - Remove Timber Block Posts.
 - Attach Bottom Flange Splice Plate to Sections 1 and 2 of Diaphragms.

REVISIONS	
NAME	DATE

ILLINOIS DEPARTMENT OF TRANSPORTATION

STRUCTURAL STEEL DETAILS
 CENTRAL AVENUE (F.A.U. RTE. 2798)
 OVER
 INTERSTATE 90 (KENNEDY EXPWY.) & C.T.A.
 F.A.I. RTE. 90 SECTION: 1213B-1
 COOK COUNTY STATION 1+000.000
 STRUCTURE NO. 016-0659

SCALE: NONE DRAWN BY: D.L./F.M.
 DATE: JANUARY 16, 2009 CHECKED BY: B.M.S./J.C.M.

CHRISTIAN-ROGE & ASSOC., INC.
 CHICAGO ILLINOIS