

STATE OF ILLINOIS
DEPARTMENT OF TRANSPORTATION

	0.4 Span 1 0.6 Span 3 0.4 Span 4 0.6 Span 6	Pier 1 Pier 2 Pier 4 Pier 5	0.5 Span 2 0.5 Span 5
I_s	(in ⁴)	20,872	20,872
$I_o(n)$	(in ⁴)	72,612	72,612
$I_o(3n)$	(in ⁴)	49,826	49,826
S_s	(in ³)	954	954
$S_c(n)$	(in ³)	1568	1568
$S_c(3n)$	(in ³)	1396	1396
Z	(in ³)	1871	
ϕ	(k/')	0.998	1.014
$M\phi$	(k)	572.6	548.1
$s\phi$	(k/')	0.480	0.480
$M_s\phi$	(k)	324.1	366.5
M_L	(k)	745.5	837.9
M_I	(k)	166.4	166.2
$^{5/8}[M_L + M_I]$	(k)	152.3	167.7
M_o	(k)	3145.4	3369.0
M_u	(k)	5727.3	5727.3
$f_s \phi$ non-comp	(ksi)	7.2	6.9
$f_s \phi$ (comp)	(ksi)	2.8	3.2
$f_s \ ^{5/8}[M_L + M_I]$	(ksi)	11.7	12.8
f_s (Overload)	(ksi)	21.6	22.9
f_s (Total)	(ksi)		
VR	(k)	57.1	45.2

	N. Abut.	Piers 1, 2, 4 or 5	N. Brg. Pier 3 S. Brg. Pier 3
$R\phi$	(k)	53.1	55.5
R_L	(k)	42.3	42.3
R_I	(k)	9.4	9.4
R_{Total}	(k)	104.8	107.2

* Compact section
** Braced non-compact and partially braced section

I_s, S_s : Non-composite moment of inertia and section modulus of the steel section used for computing f_s (Total and Overload) due to non-composite dead loads (in⁴ and in³).

$I_o(n), S_o(n)$: Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing f_s (Total and Overload) due to short-term composite live loads (in⁴ and in³).

$I_o(3n), S_o(3n)$: Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing f_s (Total and Overload) due to long-term composite (superimposed) dead loads (in⁴ and in³).

Z : Plastic Section Modulus of the steel section in non-composite areas (in³).

ϕ : Un-factored non-composite dead load (kips/ft.).

$M\phi$: Un-factored moment due to non-composite dead load (kip-ft.).

$s\phi$: Un-factored long-term composite (superimposed) dead load (kips/ft.).

$M_s\phi$: Un-factored moment due to long-term composite (superimposed) dead load (kip-ft.).

M_L : Un-factored live load moment (kip-ft.).

M_I : Un-factored moment due to impact (kip-ft.).

M_o : Factored design moment (kip-ft.).

$1.3 [M\phi + M_s\phi + \frac{5}{8}(M_L + M_I)]$

M_u : Compact composite moment capacity according to AASHTO LFD 10.50.1.1 or compact non-composite moment capacity according to AASHTO LFD 10.48.1 (kip-ft.).

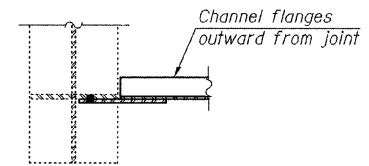
f_s (Overload): Sum of stresses as computed from the moments below (ksi).

$M\phi + M_s\phi + \frac{5}{8}(M_L + M_I)$

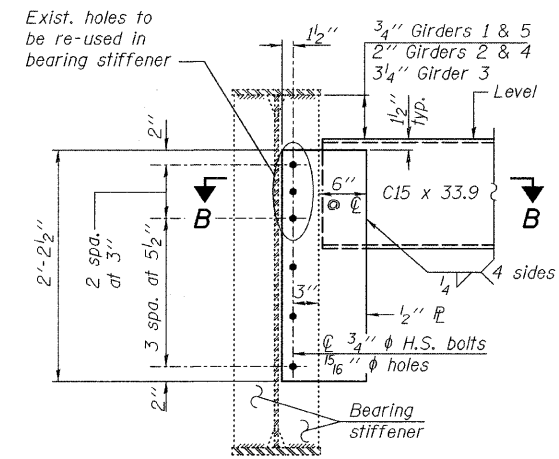
f_s (Total): Sum of stresses as computed from the moments below on non-compact section (ksi).

$1.3 [M\phi + M_s\phi + \frac{5}{8}(M_L + M_I)]$

VR: Maximum L + impact horizontal shear range within the composite portion of the span for stud shear connector design (kips).



SECTION B-B



END DIAPHRAGM
(16 required)

Location	Girder 1	Girder 2	Girder 3	Girder 4	Girder 5
⊙ Brg. N. Abut.	520.44	520.54	520.63	520.55	520.44
⊙ Brg. Pier 1	519.86	519.95	520.04	519.95	519.84
⊙ Brg. Pier 2	519.87	519.95	520.05	519.98	519.87
⊙ Pier 3	519.86	519.96	520.09	519.99	519.88
⊙ Brg. Pier 4	519.89	520.00	520.11	520.00	519.93
⊙ Brg. Pier 5	519.88	519.98	520.08	519.98	519.88
⊙ Brg. S. Abut.	519.89	519.99	520.09	519.99	519.89

***For information only. Elevations are based on survey results and represent the proposed elevation after bearings have been replaced.

NOTES:

- Two hardened washers required for each set of oversized holes.
- Existing and Proposed bolt holes in the existing bearing stiffeners shall be subpunched or subdrilled $\frac{15}{16}$ " diameter and reamed in the field to $\frac{15}{16}$ " diameter. Cost included with Furnishing and Erecting Structural Steel.
- All structural steel shall conform to the requirements of AASHTO M 270 Grade 50.

DESIGNED -	JLS
CHECKED -	MRB/KWS
DRAWN -	VH
CHECKED -	MRB/KWS

benesch

alfred benesch & company
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SHEET NO. S23	F.A.U. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
	341	04-00090-07-BR	WILL	57	31
S47 SHEETS	CONTRACT NO. 63442				
FED. ROAD DIST. NO.		ILLINOIS	FED. AID PROJECT		

STRUCTURAL STEEL REPAIRS 1 OF 2
STRUCTURE NO. 099-3298