STRUCTURE GEOTECHNICAL REPORT MANHATTAN-MONEE ROAD CULVERT OVER DRAINAGE DITCH STATION 70+01.53 WILL COUNTY, ILLINOIS

For Quigg Engineering Inc. 111 S. Wacker Drive, Suite 3910 Chicago, IL 60606

> Submitted by Wang Engineering, Inc. 1145 North Main Street Lombard, IL 60148

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 Manhattan-Monee Road. T south side of the Manhatta three new retaining walls, Monee Road culvert. Beneath the pavement and up to 3 feet of medium stiff clay, silty clay to silty clay of 689 to 691 feet and mea With about the 30 inches feasible to construct the cu factored bearing resistance differential settlement of 0.3 We provided recommenda sections, cast-in-place T-typ 	proposed to the site near the existing culva The improvements include removing the exist an-Monee Road and replacing with a new 5- the existing gabion wall removal and aband topsoil, the general lithologic profile encount to stiff silty clay to silty clay loam fill and bu loam interbedded sand to sandy gravel. Ground soured at elevations of 671 to 689 feet. of the unstable soils removal and replacement lvert. Following the recommended treatment e of 4,000 psf. The long-term settlements and 5 inches or less. ations for the potential wingwall types include we walls, and sheet pile walls. are proposed to be sheet pile walls. We pro-	sting culvert under the driveway on the foot wide and 4-foot high box culvert, loning in place the existing Manhattan- ered during the investigation includes uried topsoil over medium stiff to hard undwater was observed at elevations int to elevation of 693 feet, it will be t, the culvert barrel can be designed a re estimated to be 0.5 inches with a luding horizontal, precast apron end
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STRUCTURE GEOTECHNICAL REPORT MANHATTAN-MONEE ROAD CULVERT OVER DRAINAGE DITCH STATION 70+01.53 WILL COUNTY, ILLINOIS FOR QUIGG ENGINEERING INC.

1.0 INTRODUCTION

This report presents the results of our subsurface investigations, laboratory testing, geotechnical evaluations, and recommendations to support the proposed improvements at the existing culvert, designated as SN 099-0441. The culvert site is located about 0.25 miles west of US Route 45 in Will County, Illinois. On the USGS *Manhattan Quadrangle 7.5 Minute Series* map, the project site is generally located at SE ¹/₄ of Section 18, NE ¹/₄ of Sec. 19, Township 34N, Range 11E of the Third Principal Meridian. A *Site Location Map* is presented as Exhibit 1.

The purpose of this investigation was to characterize the site soil and groundwater conditions, perform geotechnical analyses, and provide recommendations for the design and construction of the proposed improvements.

1.1 Proposed Improvements

Based on General Plan and Elevation (GPE) Drawing (Appendix D) dated June 5, 2019 and information provided by Accurate Group, Inc. (Accurate), Wang Engineering, Inc. (Wang) understands that the following improvements are proposed at the existing culvert, SN 099-0441:

- The existing culvert, SN 099-0441 currently has three plastic pipes inserted the length of the culvert barrel with grout filling voids around the pipes. This culvert will be filled with CLSM and abandoned in place;
- At the southeast corner of the existing culvert, SN 099-0441, there is an existing pipe culvert carrying the private driveway over the drainage ditch and running east to west direction. This pipe culvert will be removed and replaced with a new 5-foot wide and 4-foot high concrete box culvert with an out-to-out length of 39 feet. The proposed culvert will have invert elevations of 696.69 and 696.28 feet at upstream and downstream ends, respectively;



- A new retaining wall, designated as Wall No. 1 begins at proposed culvert northwest wingwall at Station 69+50 and ends at Station 69+73 running along south side of the Manhattan-Monee Road;
- A new retaining wall, designated as Wall No. 2 begins at the existing retaining wall at Station 69+84.75 and ends at Station 70+14.75 running along north side of the Manhattan Monee Road; and
- The existing gabion wall along north side of the Manhattan Monee Road will be removed and replaced with a new retaining wall, designated as Wall No.3. The new Wall No.3 begins at Station 70+86 and ends at Station 71+53.

1.2 Existing Structures

The existing culvert, SN 099-0441 is a single cell concrete box culvert currently having three 24 inches plastic pipes inserted for full length of culvert and grout filling the void around the pipes. The existing box culvert is 7-foot wide and 3-foot high with an out-to-out length of 33.9 feet along the centerline of culvert. There is a retaining wall running on the north side of Manhattan-Monee Road. The culvert carries one lane of traffic in each direction.

A 36-inches diameter pipe culvert carrying the private driveway over the drainage ditch is located at the southeast corner of existing culvert.

2.0 METHODS OF INVESTIGATION

The following sections outline the field and laboratory investigations performed by Wang.

2.1 Field Investigation

The field investigation consisted of four structure borings, designated as CB-03, CB-04, RW-01 and RW-02 drilled from elevations 700.7 to 702.7 feet to a depth of 30 feet below ground surface (bgs). In addition, we have considered Boring B-4 drilled by others in 1990. The subsurface investigation performed by Wang was completed on April 19 and 22, 2019.

For the existing gabion wall replacement, the field investigation consisted of two structure borings, designated as 3-RWB-1 and 3-RWB-2 and two geoprobe borings, designated as 3-HA-1 and 3-HA-2 drilled from elevations 697.9 to 703.1 feet to depths of 10 to 35 feet bgs. The field investigation was performed by Wang on June 5, 2019.



The as-drilled coordinates and elevations were obtained with a mapping-grade GPS unit. Stations and offsets were provided by Accurate. As-drilled boring locations are presented in the *Boring Logs* (Appendix A) and the as-drilled boring locations are shown in the *Boring Location Plan* (Exhibit 2).

ATV and truck-mounted drilling rigs, equipped with hollow stem augers, were used to advance and maintain open boreholes. Soil sampling was performed according to AASHTO T206, "*Penetration Test and Split Barrel Sampling of Soils*." The soil was sampled at 2.5-foot intervals to the boring termination depths. Jackhammer driven Geoprobe samplers were used to continuously sample the soil in the hand auger borings. Soil samples collected from each sampling interval were placed in sealed jars and transported to the laboratory for further examinations and laboratory testing.

Field boring logs, prepared and maintained by Wang geologist, include lithological descriptions, visual-manual soil (IDH Textural) classifications, results of Rimac and pocket penetrometer unconfined compressive strength tests (Q_u), and results of Standard Penetration Tests (SPT) recorded as blows per 6 inches of penetration.

Groundwater levels were measured while drilling and at completion of each boring. Each borehole was backfilled upon completion with soil cuttings and/or bentonite chips. The pavement surface was restored as close as possible to its original condition.

2.2 Laboratory Testing

The soil samples were tested in the laboratory for moisture content (AASHTO T265). Atterberg limits (AASHTO T89 and T90) and particle size analyses (AASHTO T88) were performed on selected samples. Tested samples were classified according to the IDH classification system. Field visual descriptions of the soil samples were verified in the laboratory. Laboratory test results are shown in the *Boring Logs* (Appendix A) and in the *Laboratory Test Results* (Appendix B).

3.0 INVESTIGATION RESULTS

Detailed descriptions of the soil conditions encountered during the subsurface investigation are presented in the attached *Boring Logs* (Appendix A) and in the *Soil Profile* (Exhibit 3). Please note that strata contact lines represent approximate boundaries between soil types. The actual transition between soil types in the field may be gradual in horizontal and vertical directions.



3.1 Lithological Profile

Borings CB-04 and RW-02, drilled on the roadway encountered 3 inches of asphalt over 9 inches of concrete. Borings 3-RWB-1 and 3-RWB-2, drilled on the roadway along the existing gabion wall encountered 14 and 15 inches of asphalt over sandy gravel aggregate base. Borings CB-03 and RW-01, drilled on the grassy area revealed 12 inches of topsoil at the surface. Geoprobe Borings 3-HA-1 and 3-HA-2, drilled in front of the gabion wall encountered running water at the surface over 6 inches of topsoil and stiff to hard silty clay. In descending order, the general lithologic succession encountered beneath the surface includes: 1) man-made ground (fill); and 2) medium stiff to hard clay silty clay to silty clay loam.

1) Man-made ground (fill)

Beneath the pavement and topsoil, the borings encountered up to 3 feet of stiff, black and brown silty clay loam and silt fill. The soil has unconfined compressive strength (Q_u) values of 1.3 to 1.7 tsf and moisture content values of 15 to 26%. Boring CB-04 revealed 2 feet of medium dense gravel with N value of 16 blows per foot and moisture content of 27%.

At elevations of 699.2 to 701.2 feet, Borings CB-04, RW-02, and 3-RWB-1 encountered 1.6 to 3.3 feet of silty clay loam buried topsoil with unconfined compressive strength (Q_u) values of 1.0 and 3.0 tsf and moisture content values of 30 and 37%.

2) Medium stiff to hard clay, silty clay to silty clay loam

Beneath the fill and buried topsoil, at elevations of 695.9 to 700.1 feet, the borings encountered medium stiff to hard, orange, brown, and gray clay, silty clay to silty clay loam interbedded with water-bearing, loose to medium dense sand to sandy gravel. The unit has Q_u values generally between 0.9 and 4.8 tsf and moisture content values between 14 and 29%; Boring CB-03 recorded lower Q_u values between 0.4 and 0.8 tsf with moisture content values of 16 to 55%. Laboratory index testing on samples from this layer showed liquid limit (L_L) values of 25 to 48% and plastic limit (P_L) values of 14 to 22%.

The interbedded 2 to 5 feet thick sand to sandy gravel has N-values of 5 to 14 blows per foot and moisture content values of 10 to 22%.



3.2 Groundwater Conditions

Groundwater was encountered while drilling at elevations of 689 to 695 feet within the sand and gravel layer (3.0 to 11.8 feet bgs). At the completion of drilling, groundwater was measured at elevations of 671 to 689 feet (14 to 30 feet bgs).

4.0 FOUNDATION ANALYSIS AND RECOMMENDATIONS

Geotechnical evaluations and recommendations for the proposed culvert, wingwalls, and retaining walls are included in the following sections.

4.1 Scour Considerations

The design scour elevation should be taken at the bottom of the cutoff wall (IDOT 2012). To prevent local erosion, we recommend placing stone riprap or a concrete apron at the ends of the proposed culvert. This will also prevent sediments from entering and accumulating in the culvert and minimize long term maintenance.

4.2 Culvert Foundation

Based on our subsurface investigation, the soils at the base of the culvert barrel are expected to be medium stiff silty clay with a Q_u value of 0.66 tsf and moisture content value of 55% followed by stiff to hard silty clay. Prior to placement of the culvert barrel, we recommend removing 2.5 feet of the medium stiff silty clay loam to an elevation of 693.0 feet. The replacement material should be the pay item *"Rockfill"* in accordance with the 2017 IDOT *Culvert Manual*. Rockfill material gradation and capping requirements should be as per IDOT District One Rockfill Special Provision, January 2010. The replacement material should extend a minimum of two feet beyond the edge of the box.

The soils at the culvert bearing level should be evaluated in the field to determine the actual undercut depth. The actual extent of the removal shall be determined in the field by a geotechnical soil inspector at the time of construction.

Following the recommended foundation treatment, the culvert barrel can be designed with a factored bearing resistance of 4,000 psf using a bearing resistance factor of 0.45 (AASHTO 2017).



4.3 Settlement

Following the recommended treatment as described in Section 4.2, we estimate the foundation soils will experience settlement up to 0.5 inches at the widening portion of the new culvert with the differential settlement of 0.5 inches or less. The settlement estimates are acceptable for the culvert structure.

4.4 Wingwalls

Based on the TSL plan, we understand the wingwalls at both culvert barrel ends will be horizontal cantilever wingwalls with a length of 7'-3". Other wingwall types suitable for this culvert include precast apron end sections, cast-in-place T-type or sheet pile walls.

Horizontal cantilever wingwalls should be designed based on the structural guidelines provided in Section 4.2 of the IDOT Culvert Manual (2017). Horizontal cantilever wingwalls should be founded at a minimum depth of 3.0 feet below the culvert invert elevations.

If precast apron end sections are selected, they should be as per IDOT Basesheet dated 2/17/2017 "*SCB-AES, Precast Concrete Box Culvert Apron End Section Details*" and constructed based on IDOT Standard Specifications.

If sheet pile wingwalls are selected, they can be designed based on our recommendations as described in Section 4.6 for the Retaining Wall No. 1.

For the cast-in-place T-type wingwalls, the footings should be established at a depth such that they would be at least 4 feet below culvert barrel invert elevation. Footings will be established at elevations 692.3 and 692.7 feet. Based on subsurface investigation, stiff to hard silty clay is expected to be encountered at the footing elevation. The T-type wingwalls can be designed based on a factored resistance of 4,000 psf and the information and typical sections shown in IDOT Section 4.4 (IDOT 2017).

4.5 Cast-In-Place or Precast Culvert Considerations

The results of the settlement evaluations indicate that both cast-in-place and precast culvert options are appropriate and feasible at the site. Following the recommended foundation treatment as described in Section 4.2, the differential settlement will be about 0.5 inches, which will not cause excessive separation of the precast sections.



4.6 Retaining Walls

Based on the TSL plan provided by Accurate, the proposed Retaining Walls No. 1 and No.2 will have out-to-out lengths of 23 and 30 feet, respectively. Based on the preliminary cross-section drawings, we estimate the Walls No.1 and No.2 will have approximate maximum retained heights of 2 and 5 feet, respectively. The existing gabion wall will be removed and replaced with Wall No.3. The proposed Wall No.3 will have out-to-out length of 67 feet and a maximum retained height of 5.5 feet. The walls are proposed to be sheet pile type with 2-foot concrete cap on the top.

We do not recommend the gravity wall types such as a cast-in-place cantilever concrete and Mechanically Stabilized-Earth walls due to the flowing surface water in ditches and the need of foundation excavations for wall construction. Thus, we provide recommendations for the design of flexible wall types including sheet pile wall.

We recommend the soil parameters shown in Tables 1 through 3 to be used for the design of the flexible/sheet pile walls. The embedment depth for the wall should be designed in accordance with the 2017 AASHTO LRFD guidelines considering a horizontal earth pressure load factor of 1.50 and a passive resistance factor of 0.75. In developing the design lateral pressure, the lateral pressure due to construction equipment surcharge load and traffic surcharge should be added to the lateral earth pressure. The active and passive earth pressure coefficients are provided for straight backfill behind and in front of the wall.

Reference Borings: CB-03 and RW-02					
Soil Description		Drained She Prope	0	Earth Pressure Coefficients ⁽¹⁾	
Elevation Range	Unit Weight, γ (pcf)	Cohesion (psf)	Friction Angle (°)	Active Pressure	Passive Pressure
M Stiff to Stiff SI CLAY FILL Surface to 696.5 feet	120	100	30	0.33	3.00
M Stiff SI CLAY EL 696.5 to 692.5 feet	115	0	28	0.36	2.77
Stiff to Hard SI CLAY EL 692.5 to 689.0 feet	120	100	30	0.33	3.00

Table 1: Geotechnical Parameters	for Design of Wall No.1
----------------------------------	-------------------------



Soil Description			Drained Shear Strength Properties		Earth Pressure Coefficients ⁽¹⁾	
Elevation Range	Unit Weight, γ (pcf)	Cohesion (psf)	Friction Angle (°)	Active Pressure	Passive Pressure	
M Dense SAND to GRAVEL EL 689.0 ⁽²⁾ to 686.5 feet	58 ⁽³⁾	0	31	0.32	3.12	
Stiff SI CLAY EL 686.5 to 670.7 feet	58 ⁽³⁾	100	30	0.33	3.00	

⁽¹⁾Straight slope; ⁽²⁾Groundwater elevation; ⁽³⁾Submerged Unit Weight

Table 2: Geotechnical Parameters for Design of Wall No. 2

	Reference Boring	s: RW-01, RW-0	02, and B-04		
Soil Description		Drained She Prope		Earth Pressure Coefficients ⁽¹⁾	
Elevation Range	Unit Weight, γ (pcf)	Cohesion (psf)	Friction Angle (°)	Active Pressure	Passive Pressure
Stiff SI CL LOAM FILL Surface to 696.5 feet	120	100	30	0.33	3.00
Stiff SI CLAY EL 696.5 to 690.5 feet	120	100	30	0.33	3.00
SAND EL 690.5 ⁽²⁾ to 689.0 feet	58 ⁽³⁾	0	30	0.33	3.00
M Stiff SI CLAY EL 689.0 to 687.5 feet	53 ⁽³⁾	0	28	0.36	2.77
Stiff to V Stiff SI CLAY EL 687.5 to 670.8 feet	58 ⁽³⁾	100	30	0.33	3.00

⁽¹⁾Straight slope; ⁽²⁾Groundwater elevation; ⁽³⁾Submerged Unit Weight



Soil Description		Drained Shear Strength Properties		Earth Pressure Coefficients ⁽¹⁾	
Elevation Range	Unit Weight, γ (pcf)	Cohesion (psf)	Friction Angle (°)	Active Pressure	Passive Pressure
Stiff to Hard SI CLAY Surface to 694.8 feet	120	100	30	0.33	3.00
SAND and SANDY GRAVEL EL 694.8 ⁽¹⁾ to 690.2 feet	53 ⁽²⁾	0	30	0.33	3.00
M Stiff to Stiff SI CLAY EL 690.2 to 682.1 feet	53 ⁽²⁾	0	29	0.35	2.88
Stiff to V Stiff SI CLAY EL 687.5 to 670.8 feet	58 ⁽²⁾	100	30	0.33	3.00

Table 3: Geotechnical Parameters for Design of Wall No. 3 Reference Borings: 3-HA-1, 3-HA-2, 3-RW-1, and 3-RW-2

⁽¹⁾Straight slope; ⁽²⁾Groundwater elevation; ⁽³⁾Submerged Unit Weight

The lateral deformation of the wall should also include deflection control at the top of flexible wall. The evaluations should be performed using the parameters shown in Tables 4 through 6 via p-y curve (COM624P, LPILE, and any other programs) method.

Reference Borings: CB-03 and RW-02					
Soil Description Elevation Range	Unit Weight, γ	Undrained Shear Strength, c _u	Estimated Friction Angle, Φ	Estimated Lateral Soil Modulus Parameter, k	Estimated Soil Strain Parameter, ε ₅₀
	(pcf)	(psf)	(°)	(pci)	(%)
M Stiff to Stiff SI CLAY FILL	120	1500	0	400	0.75
Surface to 696.5 feet					
M Stiff SI CLAY EL 696.5 to 692.5 feet	115	700	0	100	1.20
Stiff to Hard SI CLAY EL 692.5 to 689.0 feet	120	1500	0	400	0.75

Table 4: Recommended Parameters for Lateral Load Analysis of Wall No. 1



Soil Description	Unit	Undrained	Estimated	Estimated Lateral	Estimated Soil
Elevation Range	Unit Weight, γ (pcf)	Shear Strength, c _u (psf)	Friction Angle, Φ (°)	Soil Modulus Parameter, k (pci)	Strain Parameter, ε ₅₀ (%)
M Dense SAND to GRAVEL EL 689.0 ⁽¹⁾ to 686.5 feet	58 ⁽²⁾	0	31	60	
Stiff SI CLAY EL 686.5 to 670.7 feet	58 ⁽²⁾	1100	0	200	0.95

⁽¹⁾Groundwater elevation; ⁽²⁾Submerged Unit Weight

Undrai it Shea ht, γ Strengtl f) (psf) 0 1400	r Friction h, c_u Angle, c_u) (°)	n Soil Modulus	Strain
		· · · · · · · · · · · · · · · · · · ·	
) 0	400	0.80
0 1600) 0	500	0.75
⁽²⁾ 0	30	50	
(2) 900	0	200	1.05
(2) 1300) 0	300	0.85
	0 1600 (2) 0 (2) 900	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$

Reference Borings: RW-01, RW-02, and B-04

⁽¹⁾Groundwater elevation; ⁽²⁾Submerged Unit Weight



Soil Description Elevation Range	Unit Weight, γ (pcf)	Undrained Shear Strength, c _u (psf)	Estimated Friction Angle, Φ (°)	Estimated Lateral Soil Modulus Parameter, k (pci)	Estimated Soil Strain Parameter, ε ₅₀ (%)
Stiff to Hard SI CLAY Surface to 694.8 feet	120	1500	0	400	0.80
SAND and SANDY GRAVEL EL 694.8 ⁽¹⁾ to 690.2 feet	53 ⁽²⁾	0	30	30	
M Stiff to Stiff SI CLAY EL 690.2 to 682.1 feet	53 ⁽²⁾	1100	0	300	0.95
Stiff to V Stiff SI CLAY EL 687.5 to 670.8 feet	58 ⁽²⁾	1400	0	350	0.80

Table 6: Recommended Parameters for Lateral Load Analysis of Wall No. 3 Reference Borings: 3-HA-1, 3-HA-2, 3-RW-1, and 3-RW-2

⁽¹⁾Groundwater elevation; ⁽²⁾Submerged Unit Weight

4.7 Global Stability

We have analyzed the global stability of embankment behind the Retaining Wall No.1 at the most critical location where weaker soil layers were encountered with a maximum retained height of 10 feet. The analyses were performed with *Slide v6.0* and the results of the evaluations are provided in *Slope Stability Analysis* (Appendix C). We estimate the wall with an embedment depth of 4 feet has an undrained Factor of Safety (FOS) of 6.08 (Appendix C-1) and a drained FOS of 2.54 (Appendix C-2), satisfying the minimum FOS requirement of 1.7 (IDOT 2015); however, the wall designer should perform other analyses to determine the required embedment depth.

Considering similar soil conditions along Retaining Wall No. 2, Retaining Wall No.3, and wingwalls, we do not anticipate global stability concerns.

4.8 Stage Construction

Based on the TSL plan, Manhattan-Monee Road will be detoured and only open for local traffic during construction. The access to the private property driveway will be a temporary runaround during culvert replacement.



5.0 CONSTRUCTION CONSIDERATIONS

5.1 Site Preparation

The existing vegetation, surface topsoil, pavement, and debris should be cleared and stripped where the culvert and walls will be placed.

5.2 Excavation, Dewatering and Utilities

Excavations should be performed in accordance with local, state, and federal regulations. The potential effect of ground movements upon nearby roadways, structures, and utilities should be considered during construction. Any excavation that cannot be sloped 1:2 (V:H) should be properly shored with temporary sheet piling or temporary soil retention systems.

The groundwater was encountered at elevations of 689 to 691 feet, about 4 to 6 feet below the culvert base elevation. However, during our site visit, the surface water was observed in the ditches as well as in the culvert. Depending upon prevailing climate conditions and the time of the year when culvert construction take place, control runoff and maintenance of existing flows may require temporary water diversion and control. Any water that accumulates in open excavations by seepage or runoff should be immediately removed.

5.3 Filling and Backfilling

Fill used as embankment material and for replacement of any unstable or unsuitable soils encountered during construction should be pre-approved by the Engineer. The material used to backfill around and to a level at least 1 foot over the top of the culvert box, should be porous granular material conforming to the requirements specified in the IDOT 2019 Supplemental Specifications and Recurring Special Provisions, *Granular Backfill of Structures*.

5.4 Retaining Walls

The walls should be constructed as per IDOT Section 522 and in particular in accordance with 522.06. Difficulty in sheet pile driving should be expected between elevations 690 and 695 feet.



5.5 Earthwork Operations

The required earthwork can be accomplished with conventional construction equipment. Moisture and traffic will cause deterioration of exposed subgrade soils. Precautions should be taken by the Contractor to prevent water erosion of the exposed subgrade. A compacted subgrade will minimize water runoff erosion.

Earth moving operations should be scheduled to not coincide with excessive cold or wet weather (early spring, late fall or winter). Any soil allowed to freeze or soften due to the standing water should be removed. Wet weather can cause problems with subgrade compaction.

The retaining wall should be constructed according to the current IDOT Standard Specifications for Road and Bridge Construction (2016). It is recommended that an experienced geotechnical engineer be retained to inspect the exposed subgrade, monitor earthwork operations, and provide material inspection services during the construction phase of this project.



6.0 QUALIFICATIONS

The analysis and recommendations submitted in this report are based upon the data obtained from the borings drilled at the locations shown on the boring logs and in Exhibit 2. This report does not reflect any variations that may occur between the borings or elsewhere on the site, variations whose nature and extent may not become evident until the course of construction. If changes are planned to the proposed improvements as described in this report, we should be timely informed so that our recommendations can be adjusted accordingly.

It has been a pleasure to assist Quigg Engineering Inc and Accurate Group, Inc. this project. Please call if there are any questions, or if we can be of further service.

Respectfully Submitted,

WANG ENGINEERING, INC.

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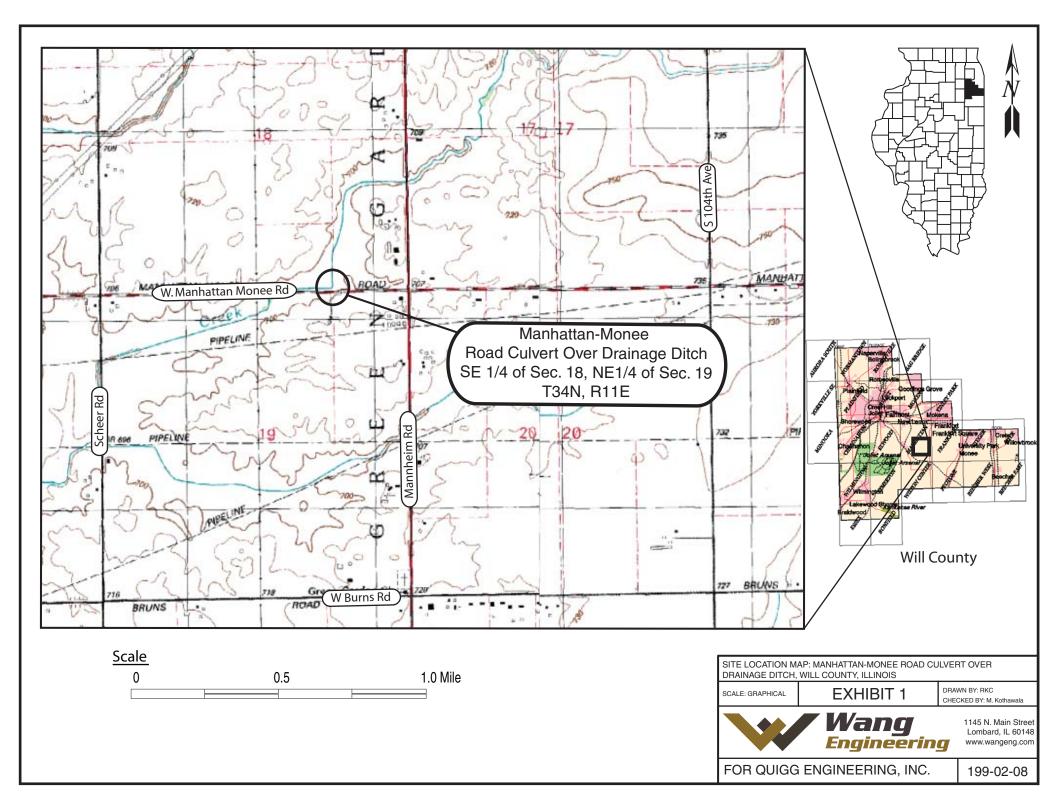
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- IDOT (2019) *Supplemental Specifications and Recurring Special Provisions*. Illinois Department of Transportation

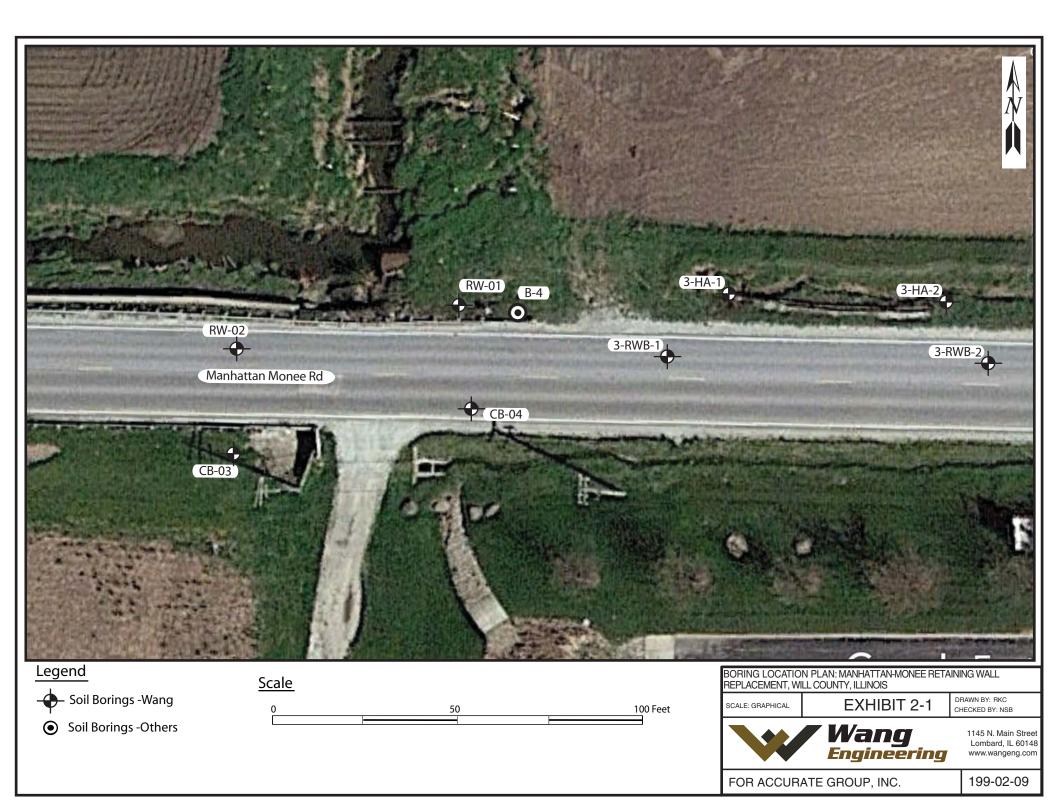


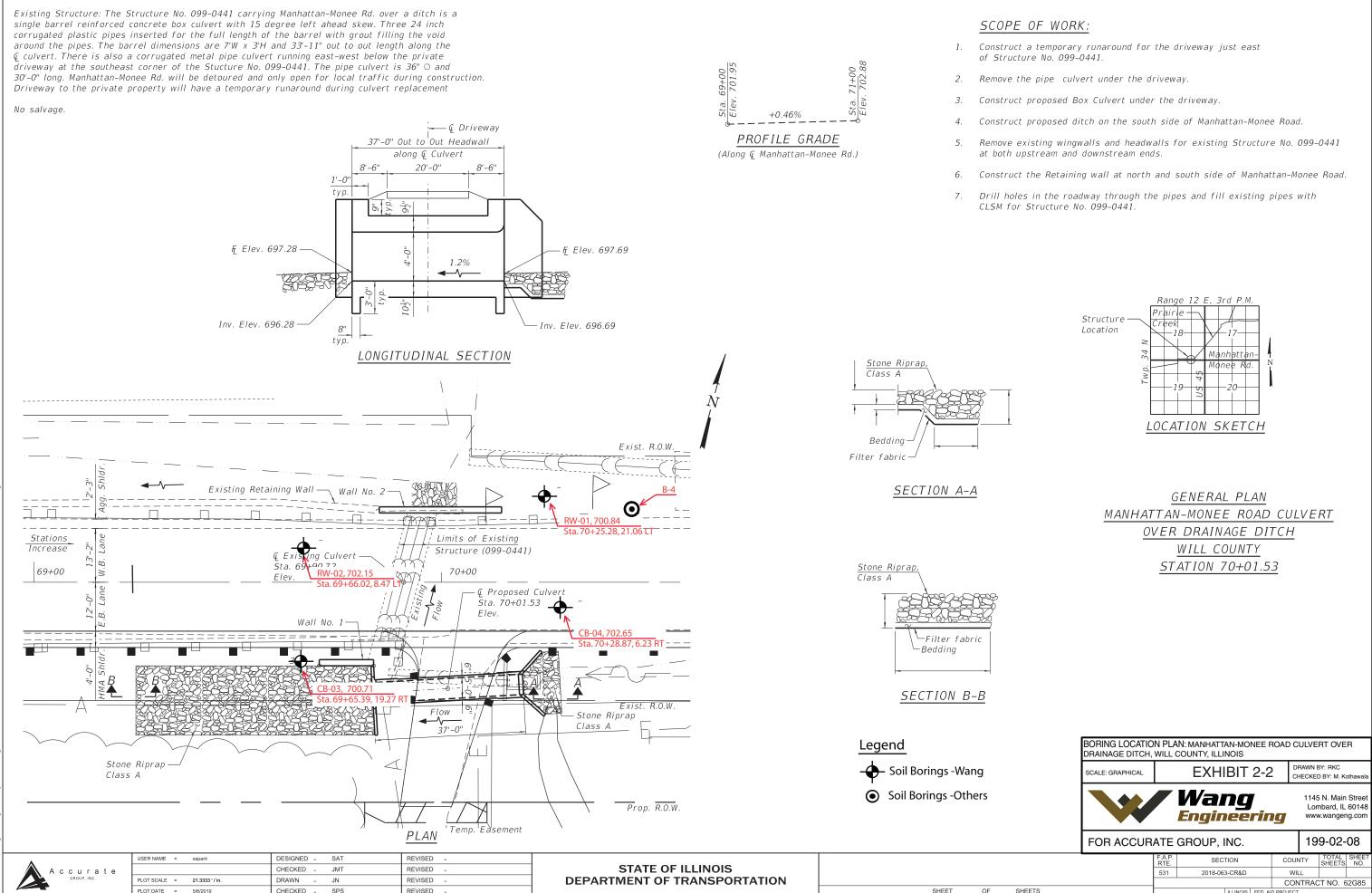
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EXHIBITS

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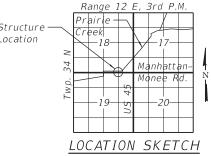


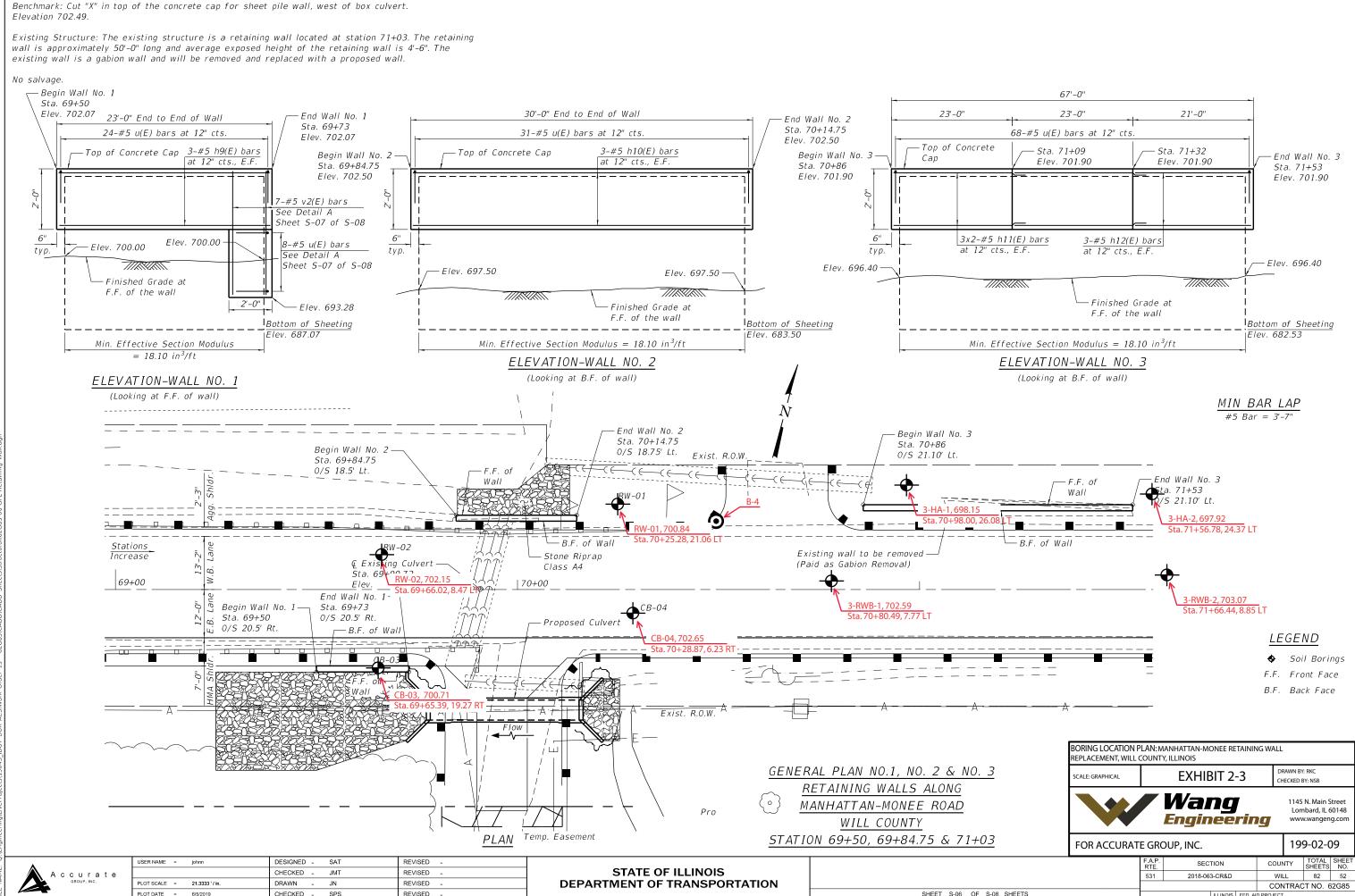




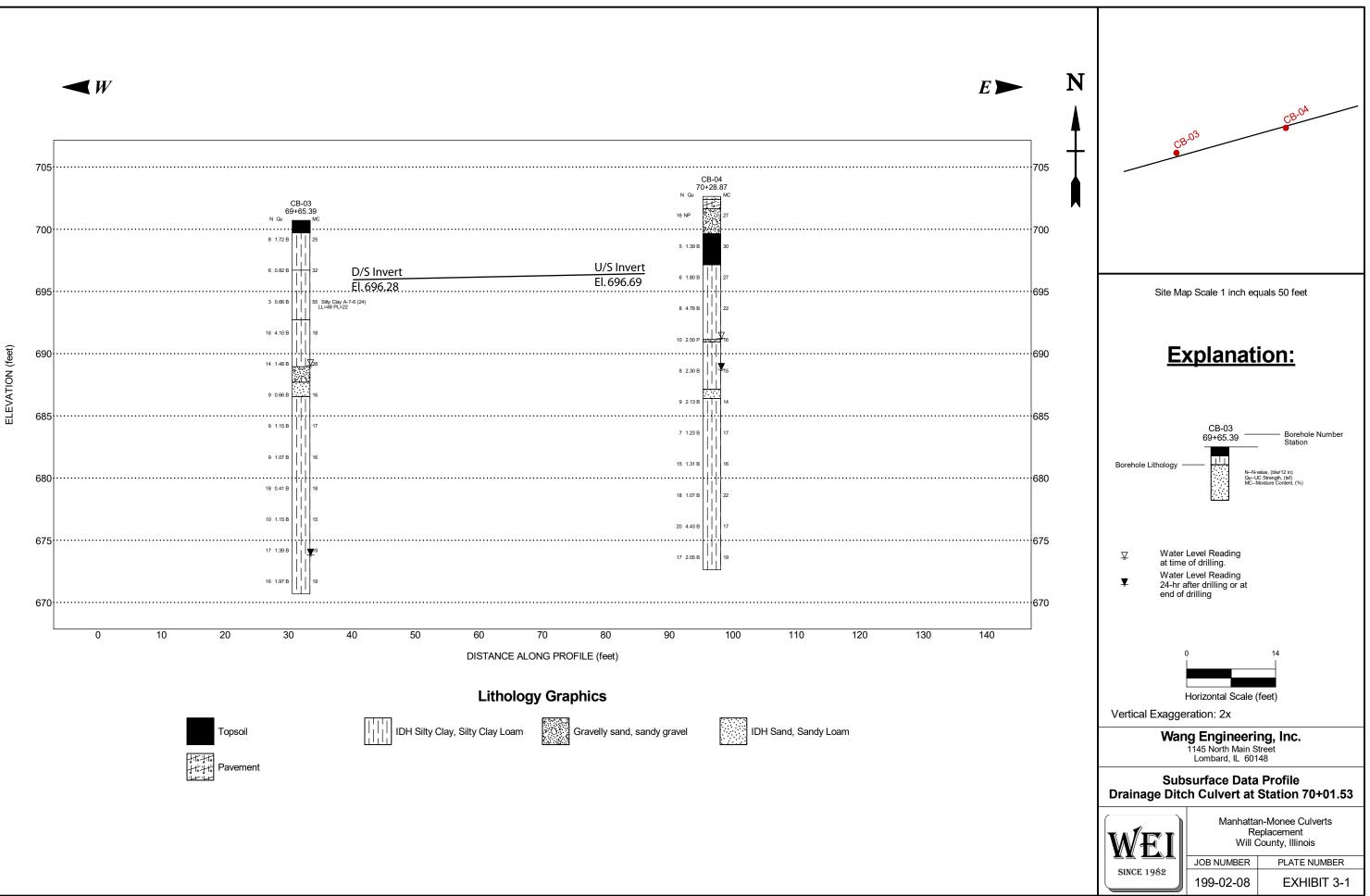
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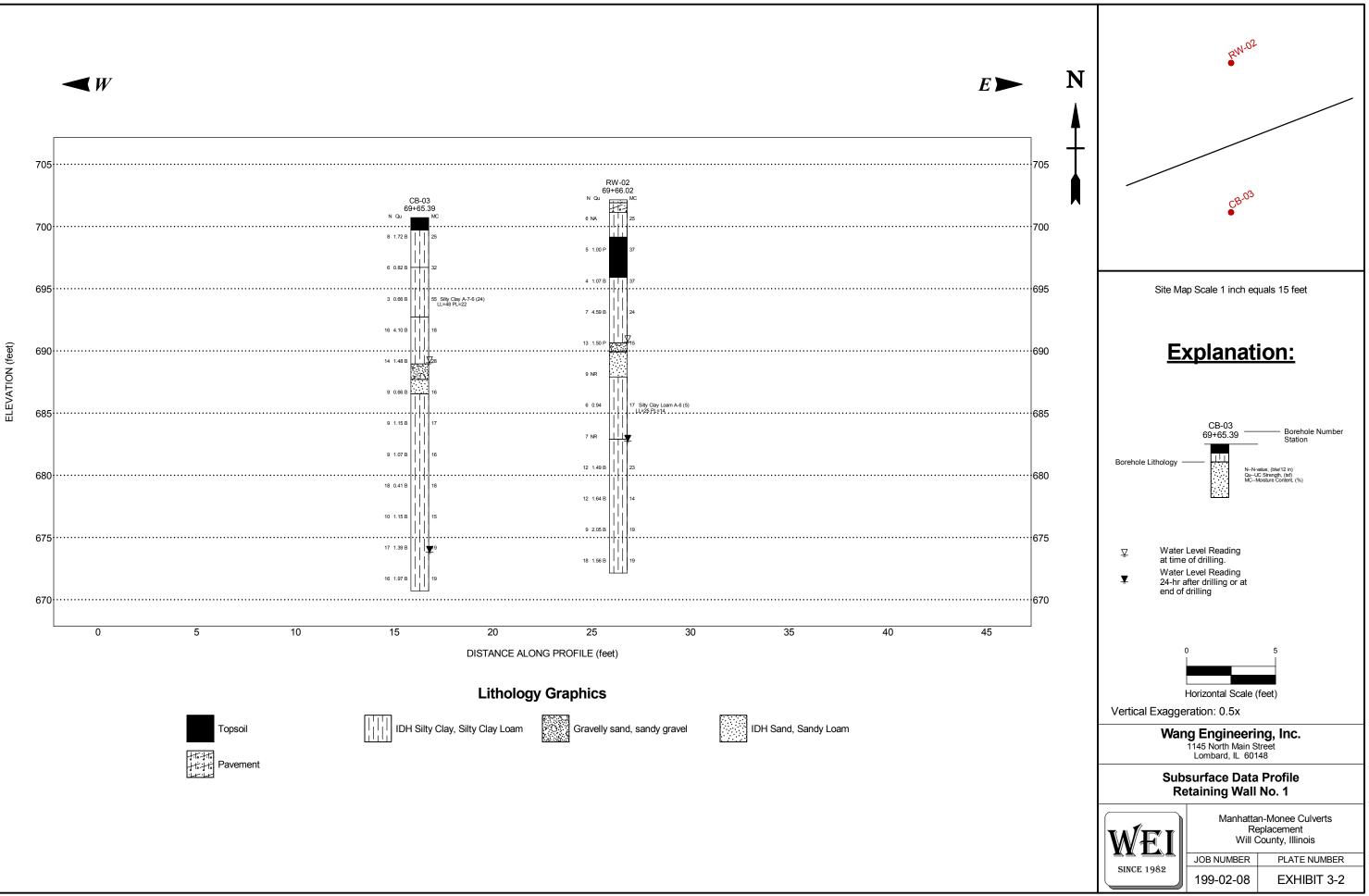
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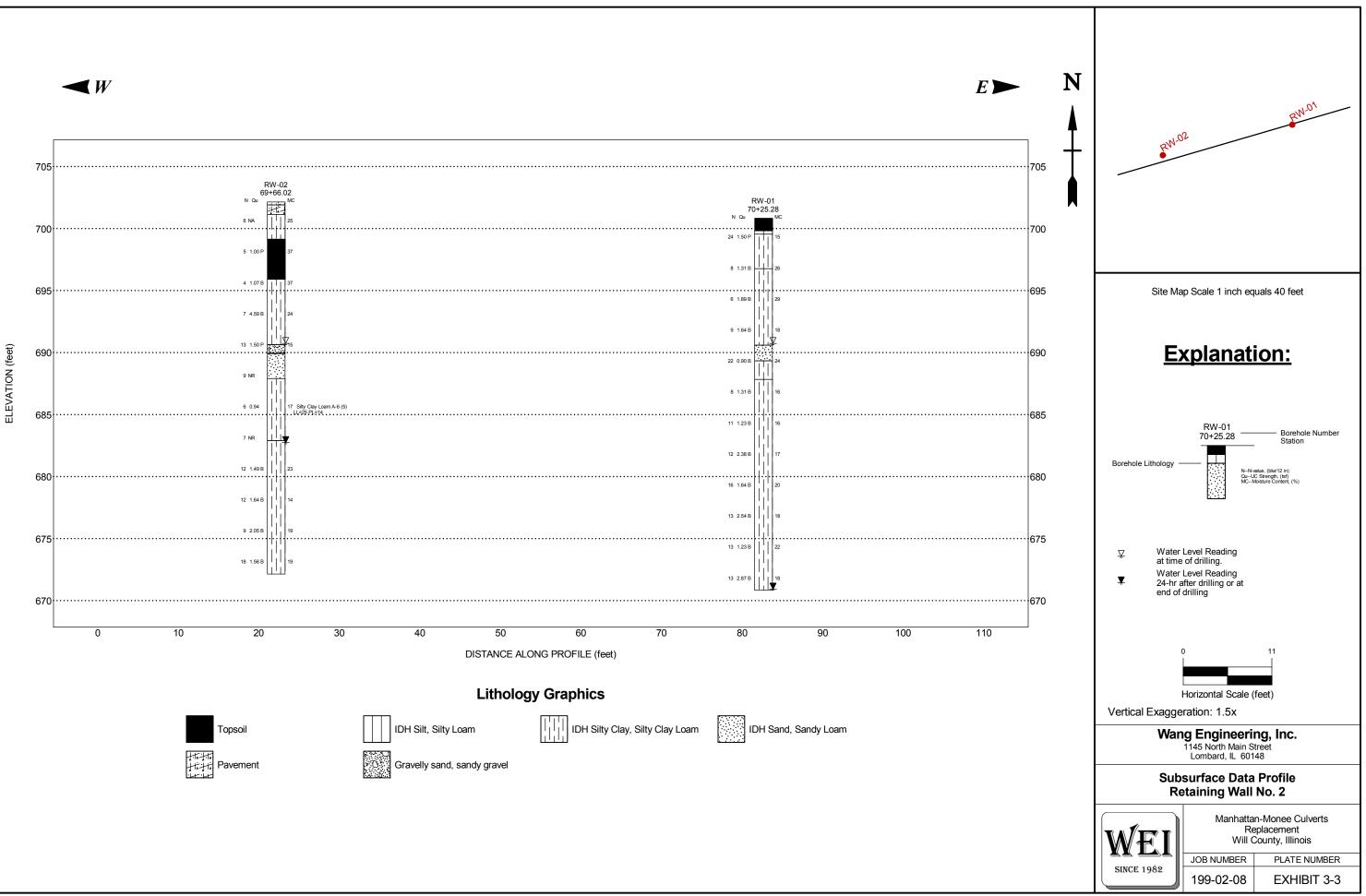




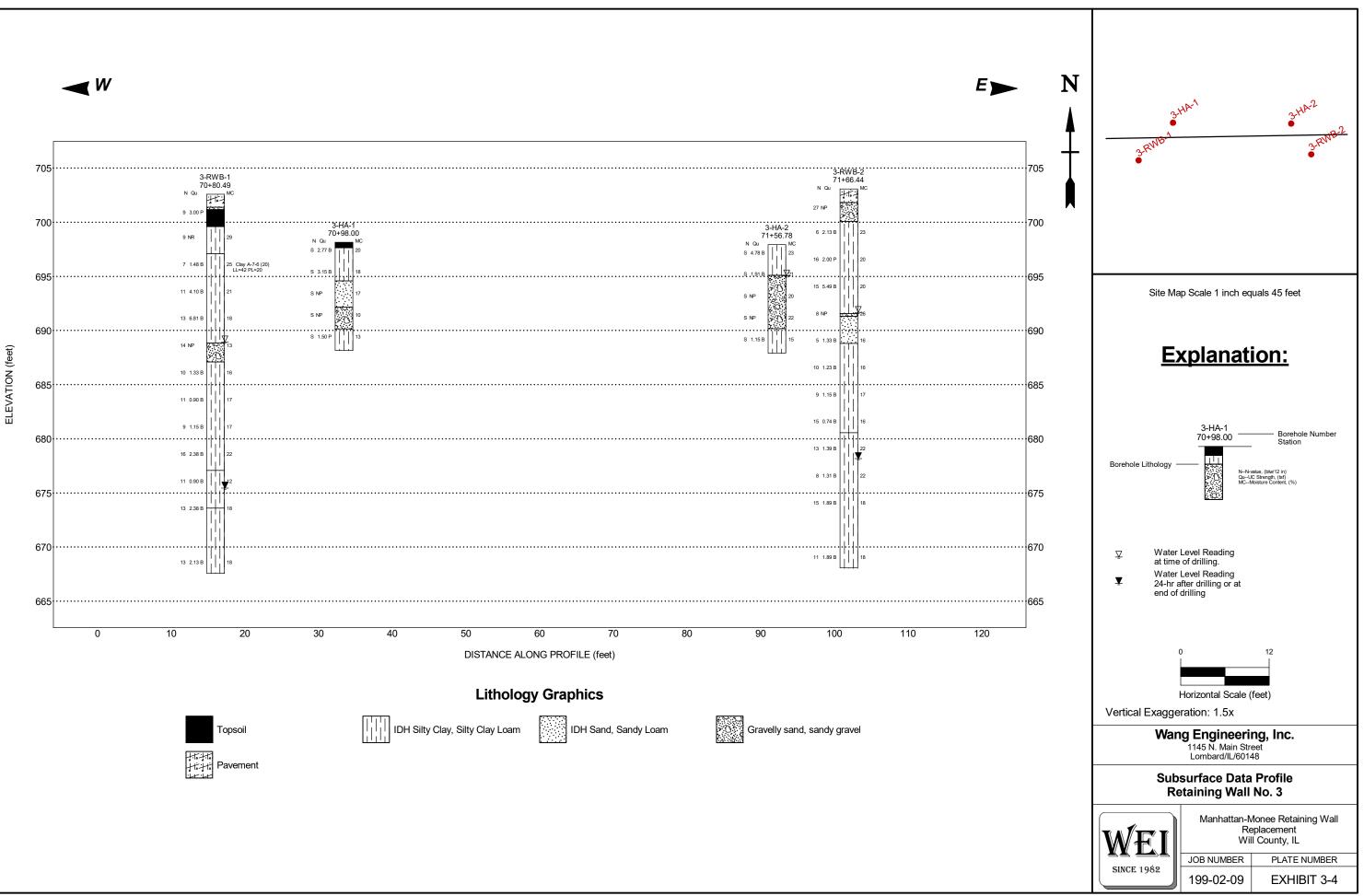
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APPENDIX A

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	Rela	ative Drilling Resistance
RDR	Term	Criter
1	Very Easy	No chatter, very little resistance, very fast and steady drill advance
2	Easy	No chatter, some resistance, fast and steady drill advance rate
3	Moderate	Some chatter, firm drill resistance, moderate advance
4	Hard	Frequent chatter, variable drill resistance, slow advance rate
5	Very Hard	Constant chatter, variable and very slow drill advance, nearly refusal

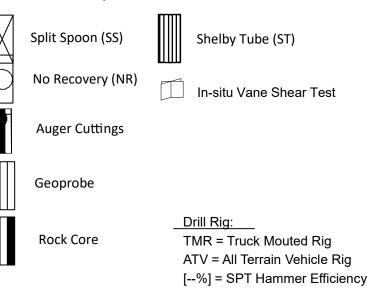
BORING LOG LEGEND

Proport	tional Terms (%)	Coars	e Gradation
Trace	1-10	Boulder	>200mm
Little	10-20	Cobble	200mm to 75mm
Some	20-35	Gravel	75mm to 2mm
And	35-50		

	e Density of esive Soils
N-Blows/12 inches	Relative Density Term
0-3	Very Loose
4-9	Loose
10-29	Medium Dense
30-49	Dense
50-80+	Very Dense

	Soil Moisture Conditions
Term	Appearance and Feel
Dry	Soil sample looks and feels powdery or dusty; no
Dry	indication of moisture. Free-running granular soils.
Damp	Cohesive soils cannot be molded easily without adding
Damp	water. Granular soil may not flow very easily.
	Soil is near the optimum moisture content. Cohesive
Moist	soils are near the plastic limit. Soil changes color slightly
	when exposed to air for a short period.
	One may feel a high degree of moisture, yet no free
Wet	water is visible. Water may become visible if the sample
wei	is squeezed. Cohesive soil appears weak and sticks to
	and/or stains hands. Granular soils tend to cohere.
	Applied to granular soils that have free surface water;
Saturated	water drains freely from the sample.

Sample Type Symbols



Consistency of Cohesive Soils

Unconfined Compressive Strength Qu, tsf	Consistency Term
<0.25	Very Soft
0.25-0.49	Soft
0.50-0.99	Medium Stiff
1.00-1.99	Stiff
2.00-3.99	Very Stiff
>4.00	Hard

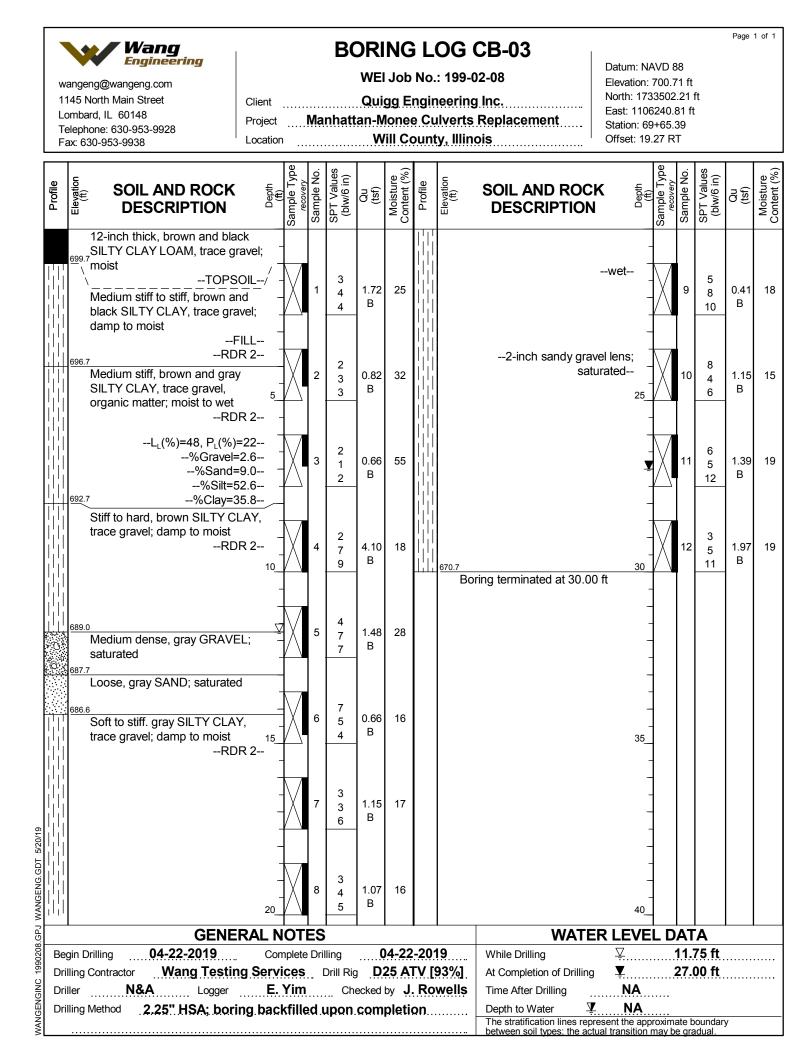
Rock Qu	ality Designation (RQD)
0-25%	Very Poor
25-50%	Poor
50-75%	Fair
75-90%	Good
90-100%	Excelent

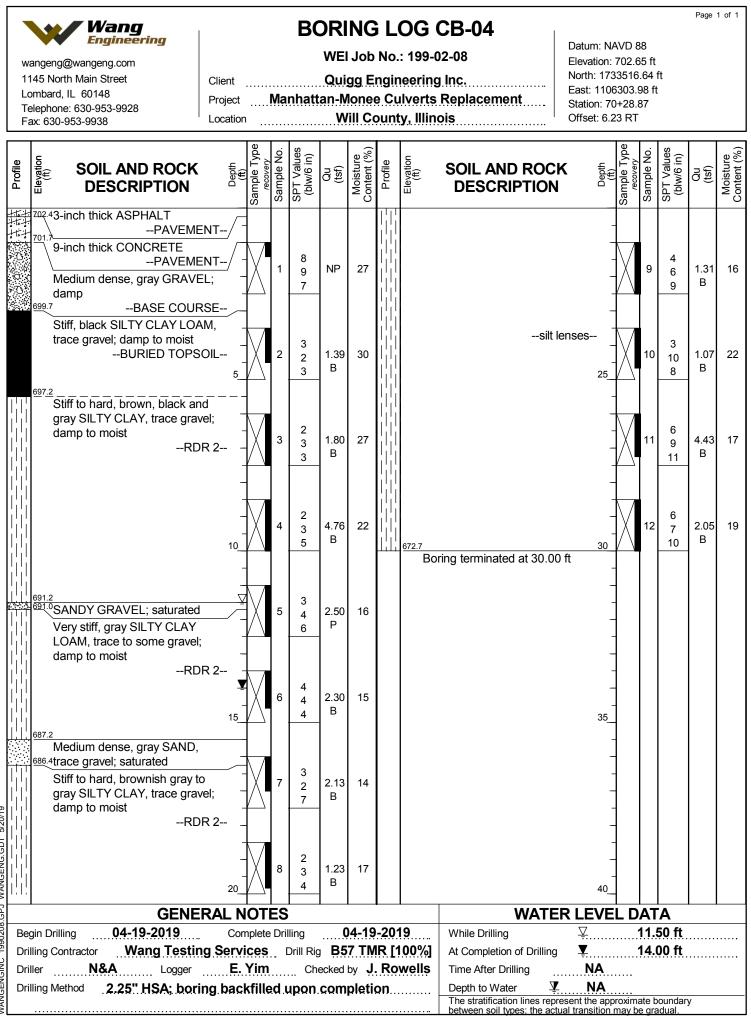
SPT = Standard Penetration Test

- Q_u = Unconfined Compressive Strength Test
 - P = Pocket Penetrometer
 - S = Shear failure (Rimac)
 - B = Bulge failure (Rimac)
- SSA = Solid Stem Auger
- HSA = Hollow Stem Auger
- N-Value (N-Blows/12 inches) is the sum of the second and the third SPT values

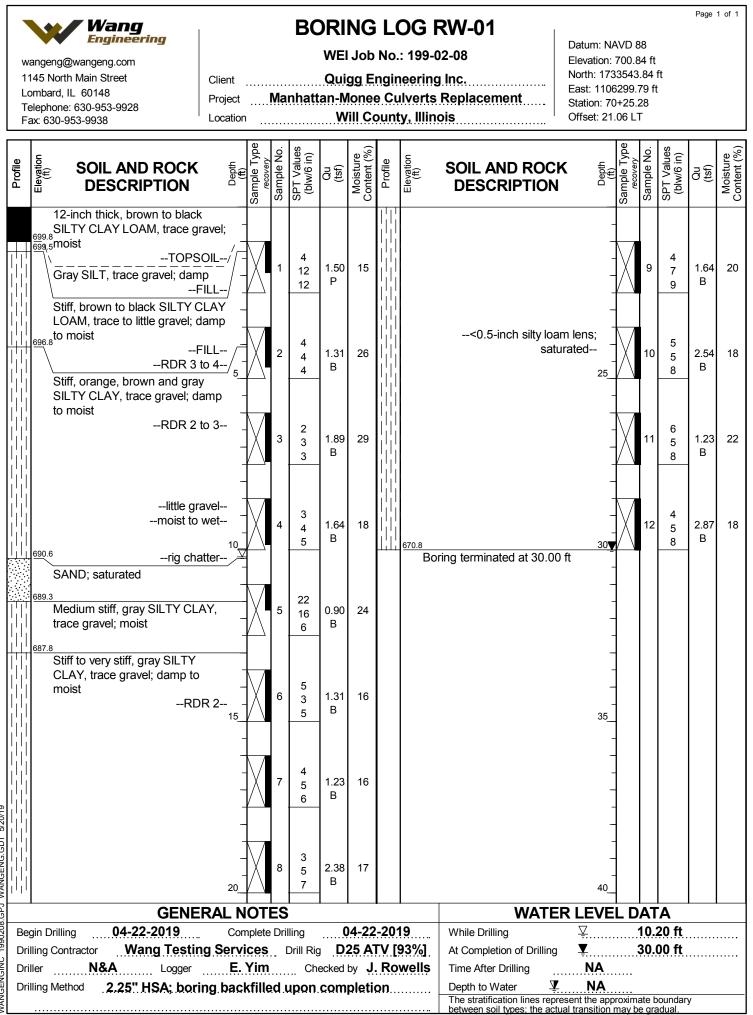
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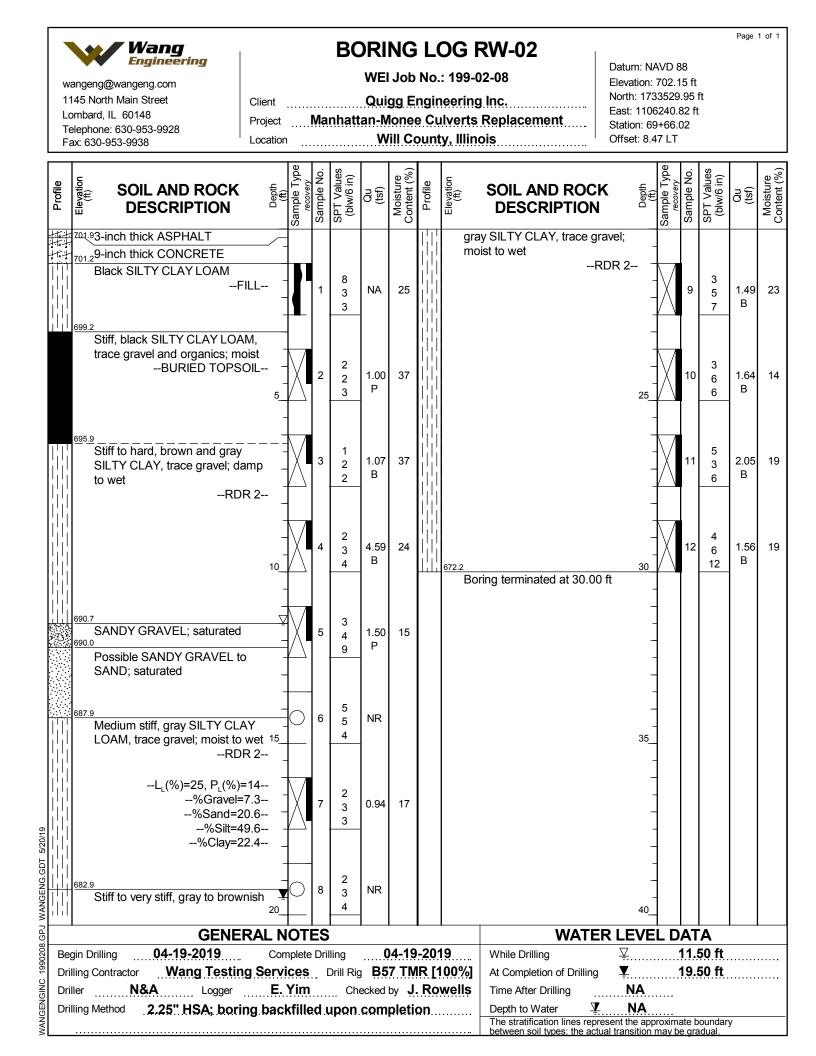




WANGENGINC 1990208.GPJ WANGENG.GDT 5/20/19



WANGENGINC 1990208.GPJ WANGENG.GDT 5/20/19





BORING LOG 3-HA-1

WEI Job No.: 199-02-09

wangeng@wangeng.com 1145 North Main Street Lombard, IL 60148 Telephone: 630-953-9928 Fax: 630-953-9938

Engin **^**...:~ Ir Elevation: 698.15 ft North: 1733550.46 ft East: 1106372.39 ft Station: 70+98.00 Offset: 26.08 LT

Datum: NAVD 88

Client	Quigg Engineering, Inc.
Project	Manhattan-Monee Retaining Wall Replacement
Location	Will County, IL

Profile		SOIL AND ROCK	Sample Type	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROO DESCRIPTIO		Sample Type	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
		CLAY LOAM, organic matter /	-	1	P U S H	2.77 B	20									
		CLAY		2	P U S H	3.15 B	18									
	69	SAND interbedded clay layer 5_	-	3	P U S H	NP	17									
		Gray, saturated SANDY GRAVEL		4	P U S H	NP	10									
		Stiff, gray, damp SILTY CLAY	-	5	P U S H	1.50 P	13									
/21/19			-													
WANGENGINC 1990209.GPJ WANGENG.GDT 6/21/19 D D D B		- - 20_	-													
9.GP			ΙΟΤ	ES						WAT	ER LEVE					
NC 199020	egr.7.6-inch thick, dark brown SILTY CLAY LOAM, organic matter TOPSOIL-/ Very stiff, brown, damp SILTY CLAY 1 P U 2.77 20 Running water on surface-/ Very stiff, brown, damp SILTY CLAY 2 P U 3.15 18 694.6 Gray, fine to medium, saturated SAND interbedded clay layer 5 0 8 1 P 1 0 8 18 692.2 Gray, saturated SANDY GRAVEL - 4 P 0 NP 17 690.2 Stiff, gray, damp SILTY CLAY - 6 9 1 5 13 690.2 Stiff, gray, damp SILTY CLAY - - 6 9 13 690.2 Stiff, gray, damp SILTY CLAY - - - - - - - - - 13 690.2 Stiff, gray, damp SILTY CLAY -						PRO	BE	While Drilling At Completion of Drillin	 Ig NA			RY IA	•••••		
	egr.,6-inch thick, dark brown SiLTY CLAY LOAM, organic matter TOPSOIL-/ Very stiff, brown, damp SiLTY CLAY I P U 2.77 20 egr.,6-inch thick, dark brown surface-/ Very stiff, brown, damp SiLTY CLAY I P U 3.15 18 egr.,6-inch thick, dark brown, damp SiLTY CLAY I P U 3.15 18 egr.,6-inch thick, dark brown, damp SiLTY CLAY I P U 3.15 18 egr.,6-inch thick, dark brown, damp SiLTY CLAY I P U 3.15 18 egr.,6-inch thick, dark brown, damp SiLTY Gray, saturated SANDY GRAVEL I P U I NP 17 egr.,2 Gray, saturated SANDY GRAVEL I P U I NP 10 egr.,2 Stiff, gray, damp SiLTY CLAY I<						iesd		Time After Drilling Depth to Water The stratification lines re between soil types; the a	Present the app	 roxima may b	ate b e gra	oundar	у		



BORING LOG 3-HA-2

WEI Job No.: 199-02-09

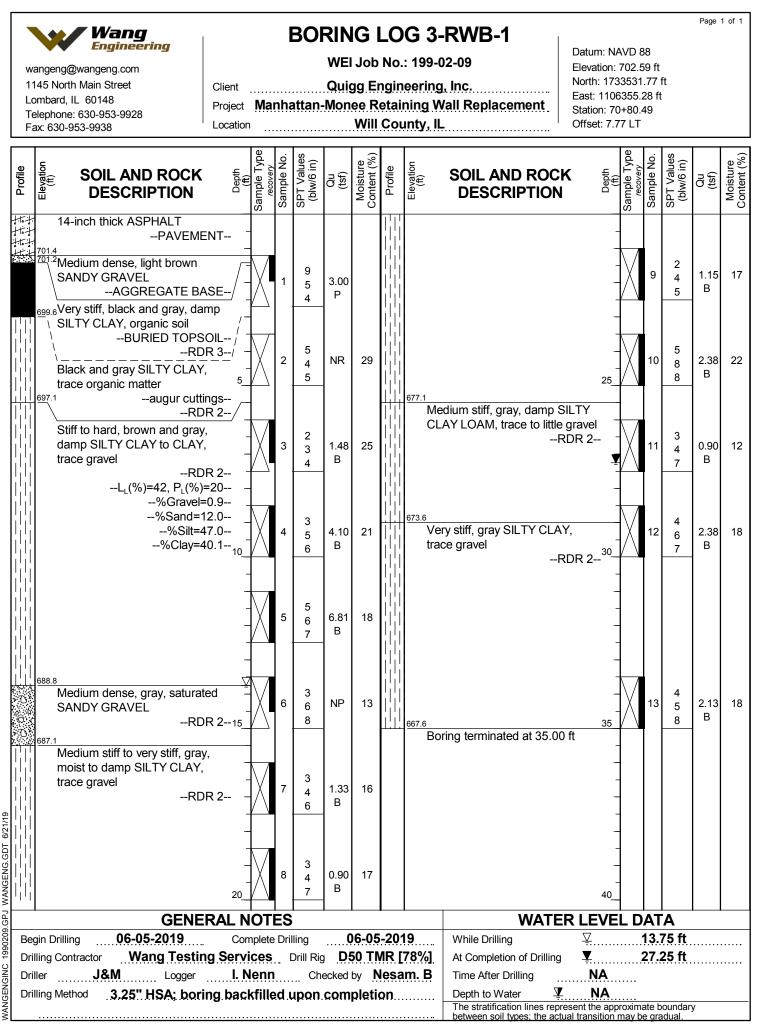
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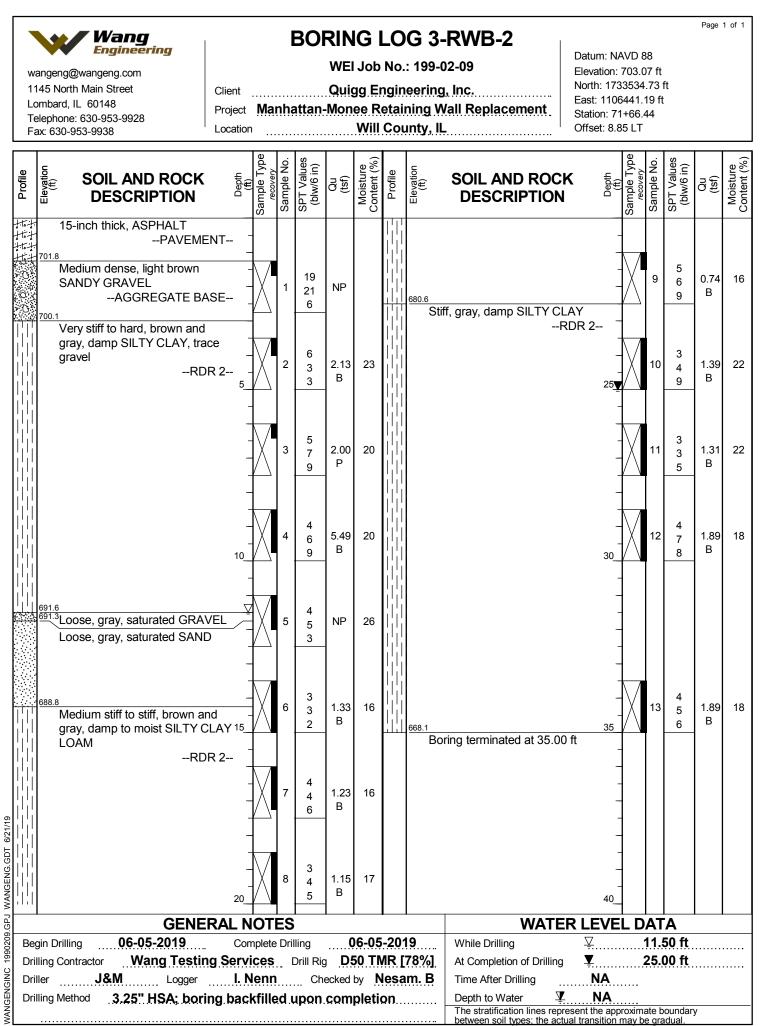
Client Quigg Engineering, Inc.

Datum: NAVD 88 Elevation: 697.92 ft North: 1733550.04 ft East: 1106431.19 ft Station: 71+56.78 Offset: 24.37 LT

Project Manhattan-Monee Retaining Wall Replacement
Location Will County, IL

Profile	SOIL AND RC DESCRIPTIO		(ft) Sample Type	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	Soil an Descr			Depth (ft)	Sample Type	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	Stiff to hard, brown, da CLAY Running water o		-	1	P U S H	4.78 B	23											
	695.1 Saturated SANDY GR/	AVEL RDR 2	-	2	P U S H	1.91 B	21											
		5		3	P U S H	NP	20											
	690.2 Stiff, gray SILTY CLAY	to SILTY		4	P U S H	NP	22											
	CLAY LOAM, trace gra	avel RDR 2 10		5	P U S H	1.15 B	15											
	Boring terminated at 10	J.00 π	-															
			-															
		15	- 5															
			-															
		20																
	GI	ENERAL		ES	۱ <u>ــــــــــــــــــــــــــــــــــــ</u>			<u> </u>	I		WAT	ER LE	EVE	L D		Ά		
Dril	gin Drilling 06-05-201	9	omplet vices	e Dri	lling Drill Rig	C		PRO	BE	While Drillin At Completic Time After D	g on of Drilli		NA		3.0	0 ft IA		
	lling Method 1" IDA Pne	umatic Ge	opro	be I	_B Sa	mple	er		·····	Depth to Wa The stratifica between soil	tion lines r	ŢI	NA ne appi	roxima	ate b e gra	oundar Idual.	y	





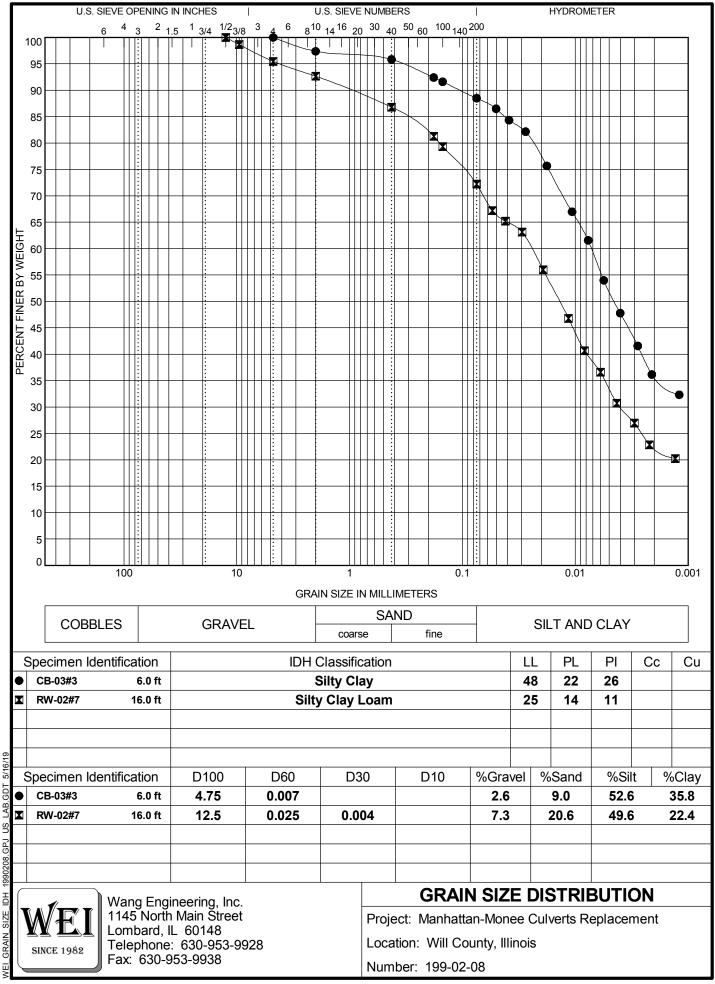
	099-	0441		l				
PSI A & H Flood	Eng	ineerii	ng	Industries, Ind BORING LOG	Sn.		1	Sh.
PROJECT					DateMarc	h 28, 19	90	
ROUTE Manhattan-Monee Road					Bored By	and the statement of		
SECWill	STA.	92	1+72	11' Left	Checked By			T
Boring NoB-4 Station94+72 Offset11'_Left	Blows	Qu Vs.f.	(%)M	Surface Water El. Groundwater El. at Completion After Hours	-9.01	vatior	Gu Vs.f.	/0/
Ground Surface 101.70 0 4"+ Asphalt over 6"+ 				Stiff gray CLA			6 1.5p 9 1 1.6b	2
CLAY with gravel and organi cs	10 11 12	3.5p 1.8b	35			-25	3 1 4	1
97.20 Very stiff black, orange- brown and gray silty CLAY with gravel and organics	4 6 7	2.5p 2.0s	21			1	9 1 / 3	2
94.70 Very stiff black, greenish	4 4 5	2.5p	25		69.7	1	7 8 1 1.3b	1!
Hard brown silty CLAY -10 	5 10 14	4.5+P 5.0s	21	Stiff to very s brown silty CLA				14
Very stiff to hard gray silty CLAY 87.20	8 12 16	3.5p 4.8s	16	Stiff gray silt	65.2		7 1.0p 9 1 1.0b	17
Very stiff to hard - <u>15</u> grayish brown silty clay 84.70	5 9 8	4.5+P 3.2b	17	Boring terminat below existing				
Stiff gray CLAY	5 7 8	2.0p 1.1b	18			-40		
-20	9 7 7	1.0p	20			-45		



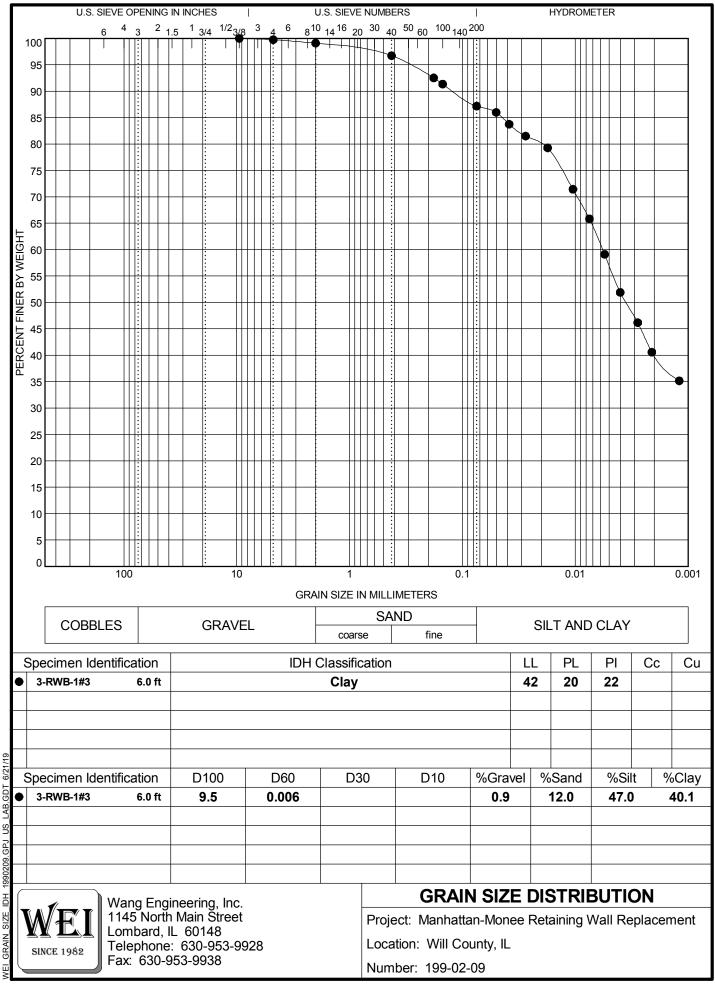
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APPENDIX B

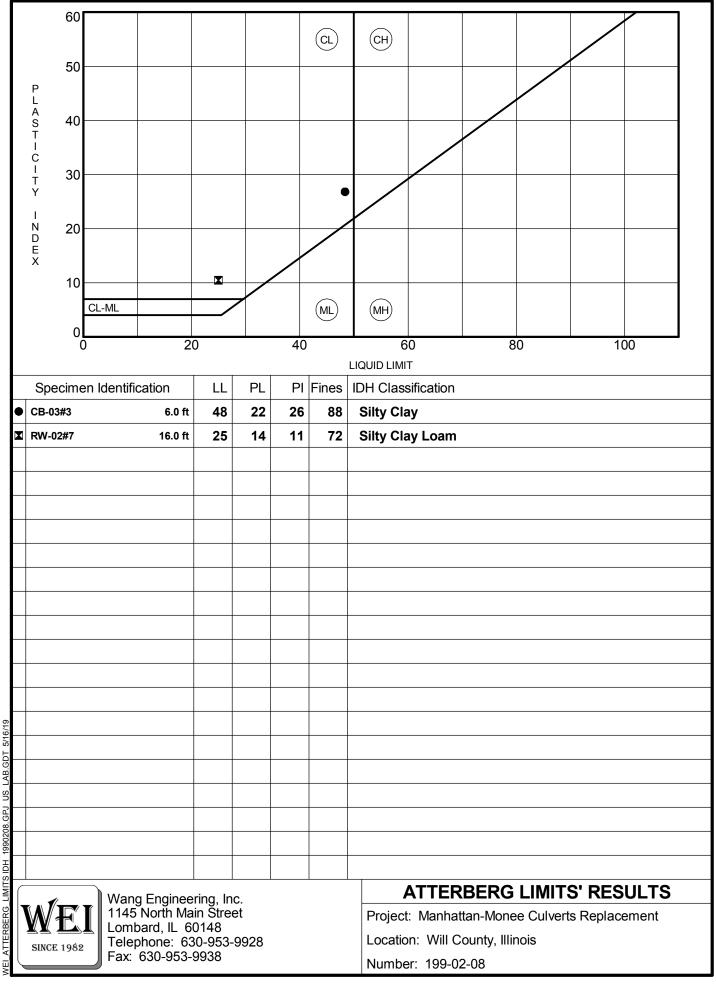
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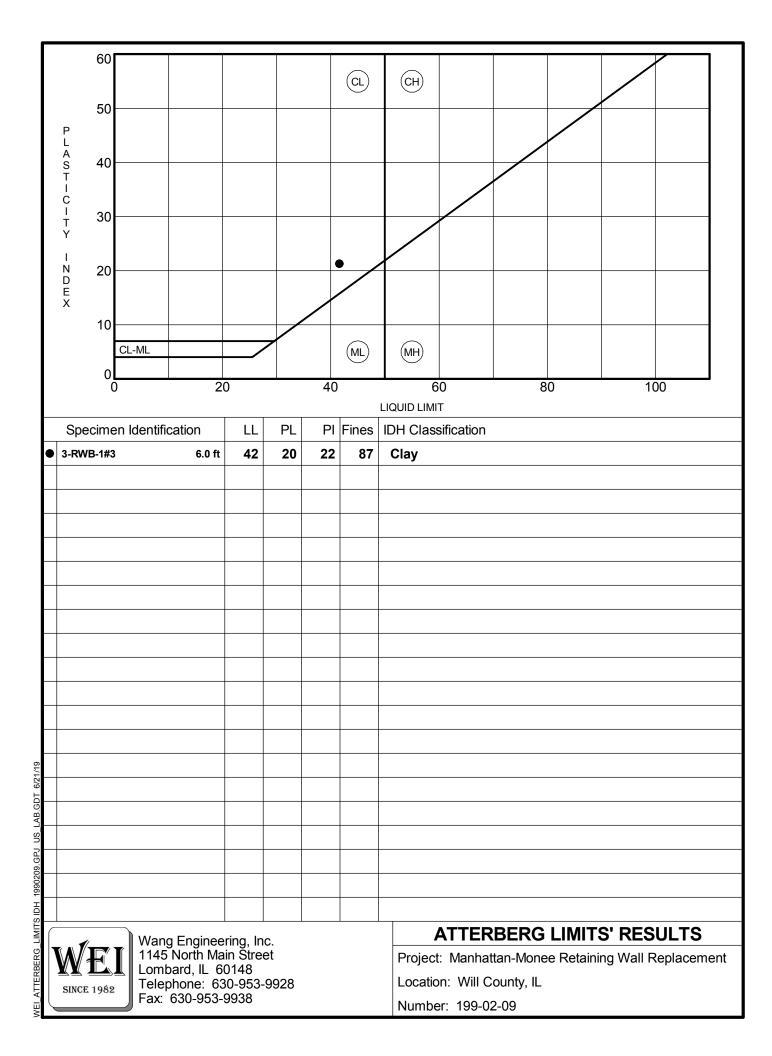
AB.GDT ŝ 1990208.GPJ Ы SIZE GRAIN



1990209.GPJ US ΗQ SIZE GRAIN



1990208.GPJ US LAB.GDT ATTERBERG LIMITS IDH

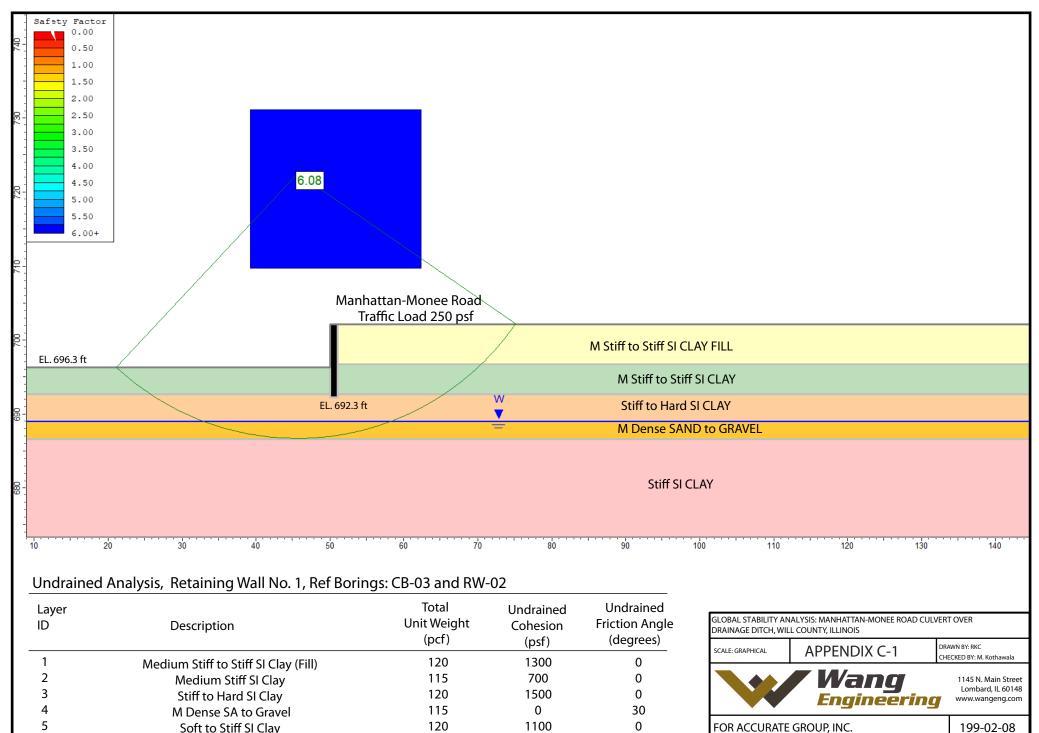




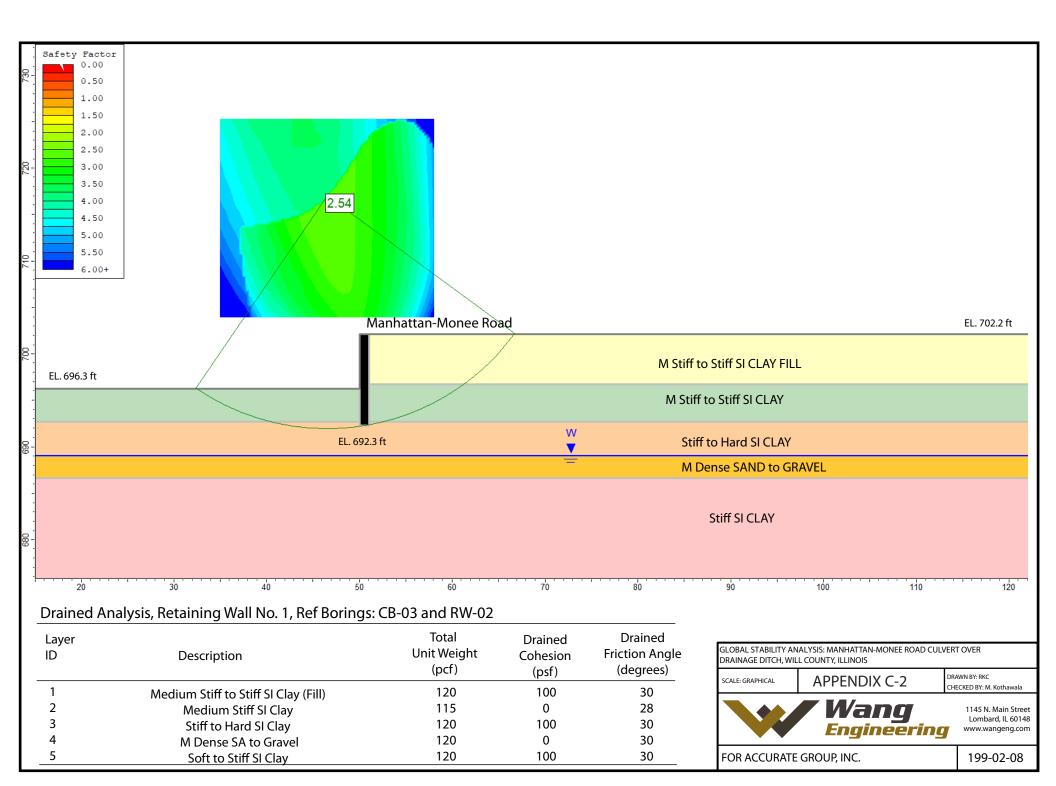
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APPENDIX C

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199-02-08

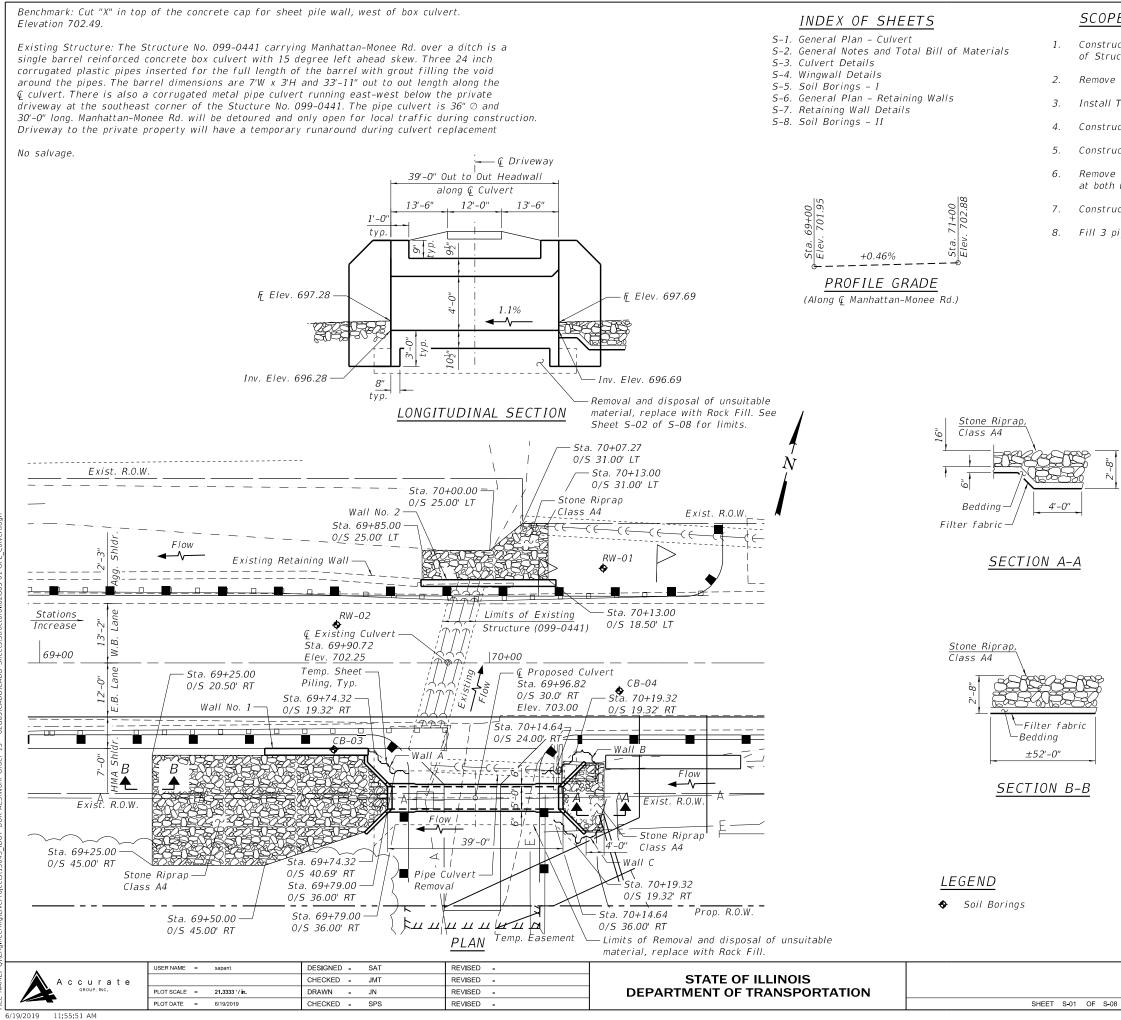




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APPENDIX D

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SCOPE OF WORK:

Construct a temporary runaround for the driveway just east of Structure No. 099-0441.

Remove the pipe culvert under the driveway.

Install Temporary Sheet Piling as shown on the plans.

Construct proposed Box Culvert under the driveway.

Construct proposed ditch on the south side of Manhattan-Monee Road.

Remove existing wingwalls and headwalls of existing Structure No. 099-0441 at both upstream and downstream ends.

Construct the Retaining wall along north and south side of Manhattan-Monee Road.

Fill 3 pipes of Structure No. 099-0441 with CLSM.

DESIGN SPECIFICATIONS 2017 AASHTO LRFD Bridge Design

Specifications, 8th Edition

DESIGN STRESSES

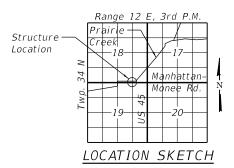
- FIELD UNITS
- f'c = 3,500 psi
- fy = 60,000 psi (Reinforcement)
- fy = 50,000 psi (M270 Grade 50)

PRECAST UNITS

- f'c = 5,000 psi
- fy = 60,000 psi (Reinforcement)
- fy = 65,000 psi (Welded Wire Fabric)

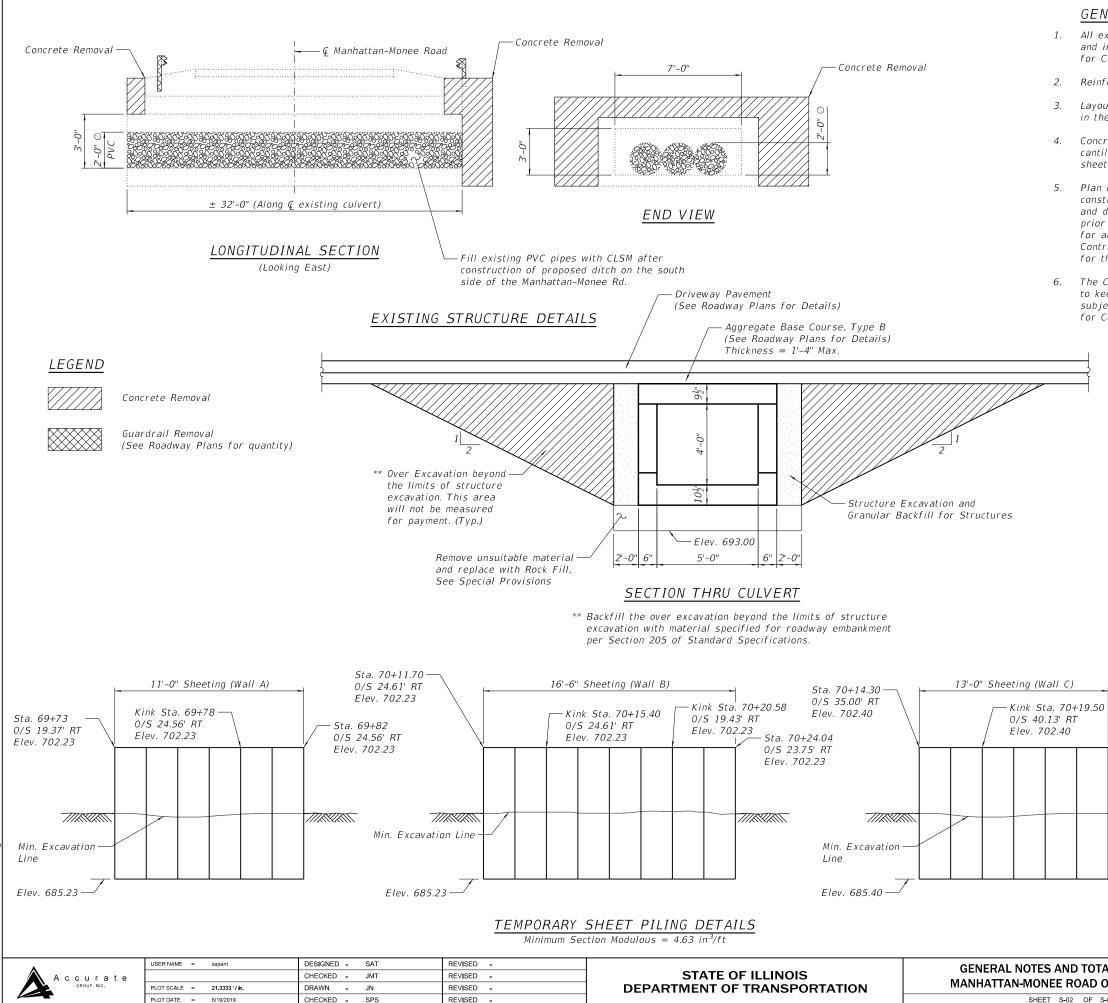
LOADING HL-93

Allow 50#/sq. ft. for future wearing surface.



<u>GENERAL PLAN</u> <u>MANHATTAN-MONEE ROAD</u> <u>DRIVEWAY CULVERT</u> <u>OVER DRAINAGE DITCH</u> <u>WILL COUNTY</u> STATION 69+96.82

	F.A.P. RTE	SEC.	TION		COUNTY	TOTAL SHEETS	SHEET NO.
	531	2018-06	3-CR&D		WILL	82	47
					CONTRAC	T NO. 6	2G85
S-08 SHEETS			ILLINOIS	FED. A	D PROJECT		



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3HEET 3-02 OF 3

GENERAL NOTES

1. All excavation required for construction of the culvert as shown in these plans and in accordance with the Standard Specifications shall be included in the cost for Concrete Box Culverts.

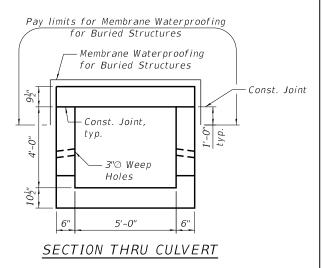
2. Reinforcement bars designated (E) shall be epoxy coated.

Layout of the slope protection system may be varied to suit ground conditions in the field as directed by the Engineer.

Concrete Sealer shall be applied to the top and outside face of the horizontal cantilever wingwalls and to the exposed concrete for the concrete cap of the sheet pile wall.

5. Plan dimensions and details relative to existing plans are subject to nominal construction variations. The Contractor shall field verify existing dimensions and details affecting new construction and make necessary approved adjustments prior to construction or ordering of materials. Such variations shall not be cause for additional compensation for a change in scope of the work, however, the Contractor will be paid for the quantity actually furnished at the unit price bid for the work.

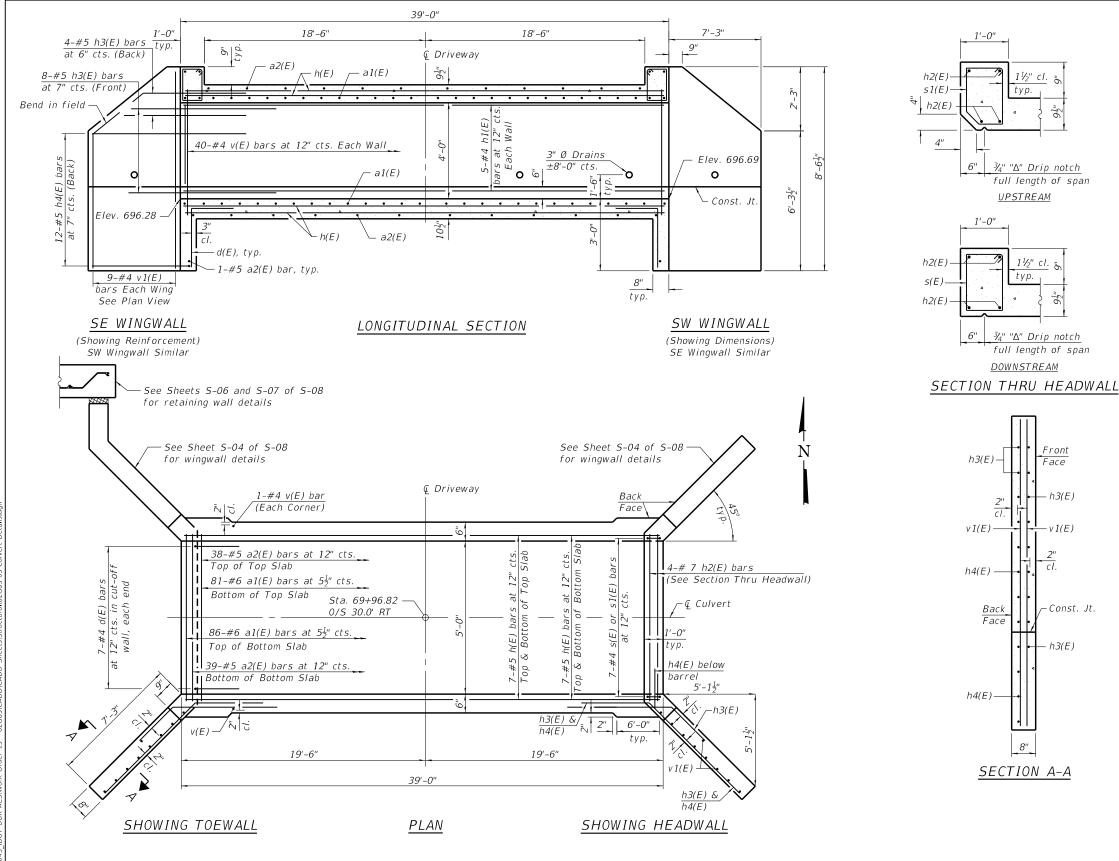
The Contractor shall be responsible to divert the stream flow during construction to keep construction area free of water. The method of water diversion shall be subject to the approval of the Engineer and the cost shall be included in the cost for Concrete Box Culverts.



TOTAL BILL OF MATERIAL (Culvert and Retaining Walls)

	ITEM	UNIT	TOTAL
	Stone Riprap, Class A4	Sq Yd	164
	Filter Fabric	Sq Yd	164
	Concrete Removal	Cu Yd	19.7
Sta. 70+24.23	Pipe Culvert Removal	Foot	30
/ 0/S 37.28' RT	Structure Excavation	Cu Yd	32.8
Elev. 702.40	Removal and Disposal of Unsuitable Material for Structures	Cu Yd	45
	Concrete Structures	Cu Yd	12.9
	Stud Shear Connectors	Each	234
	Reinforcement Bars, Epoxy Coated	Pound	6,640
	Temporary Sheet Piling	Sq Ft	689
///////////////////////////////////////	Permanent Sheet Piling	Sq Ft	2,135
	Concrete Box Culverts	Cu Yd	27.5
	Granular Backfill for Structures	Cu Yd	32.8
	Concrete Sealer	Sq Ft	614
	Controlled Low Strength Material	Cu Yd	12
	Membrane Waterproofing System for Buried Structures	Sq Yd	42
	Gabion Removal	Cu Yd	29
	Rock Fill	Cu Yd	45

		SECTION			COUNTY	TOTAL SHEETS	SHEET NO.
OVER UN-NAMED DITCH		2018-063-CR&D			WILL	82	48
					CONTRAC	CT NO. 6	2G85
-08 SHEETS			ILLINOIS	FED. A	D PROJECT		

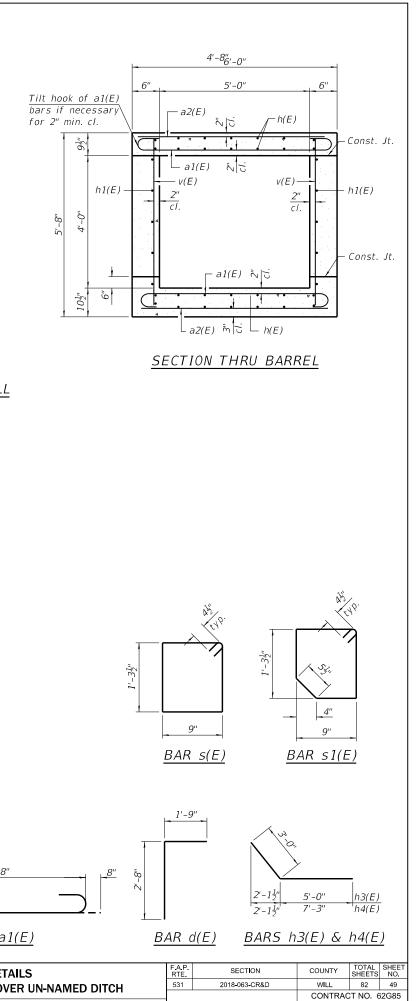


Notes:

A distance of half the length of the wingwall but not less than six feet of the barrel shall be poured monolithically with the wingwalls.

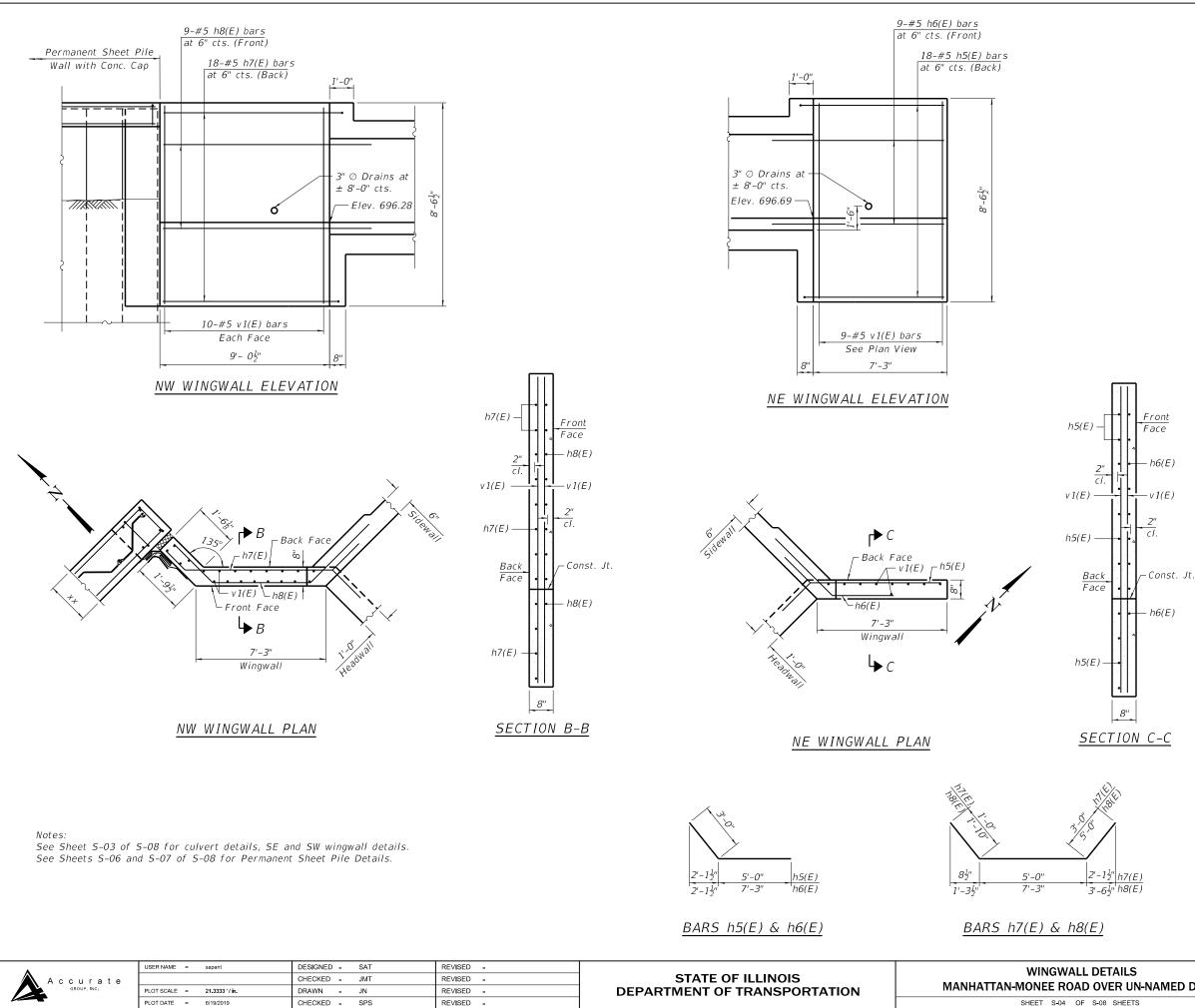
efau O	•	USER NAME = sapant	DESIGNED - SAT	REVISED -		CULVERT DETA
AME D	🛕 Accurate		CHECKED - JMT	REVISED -	STATE OF ILLINOIS	
DEL	GROUP, INC.	PLOT SCALE = 21.3333 ' / in.	DRAWN - JN	REVISED -	DEPARTMENT OF TRANSPORTATION	MANHATTAN-MONEE ROAD OVE
MO		PLOT DATE = 6/19/2019	CHECKED - SPS	REVISED -		SHEET S-03 OF S-08 S

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08 SHEETS

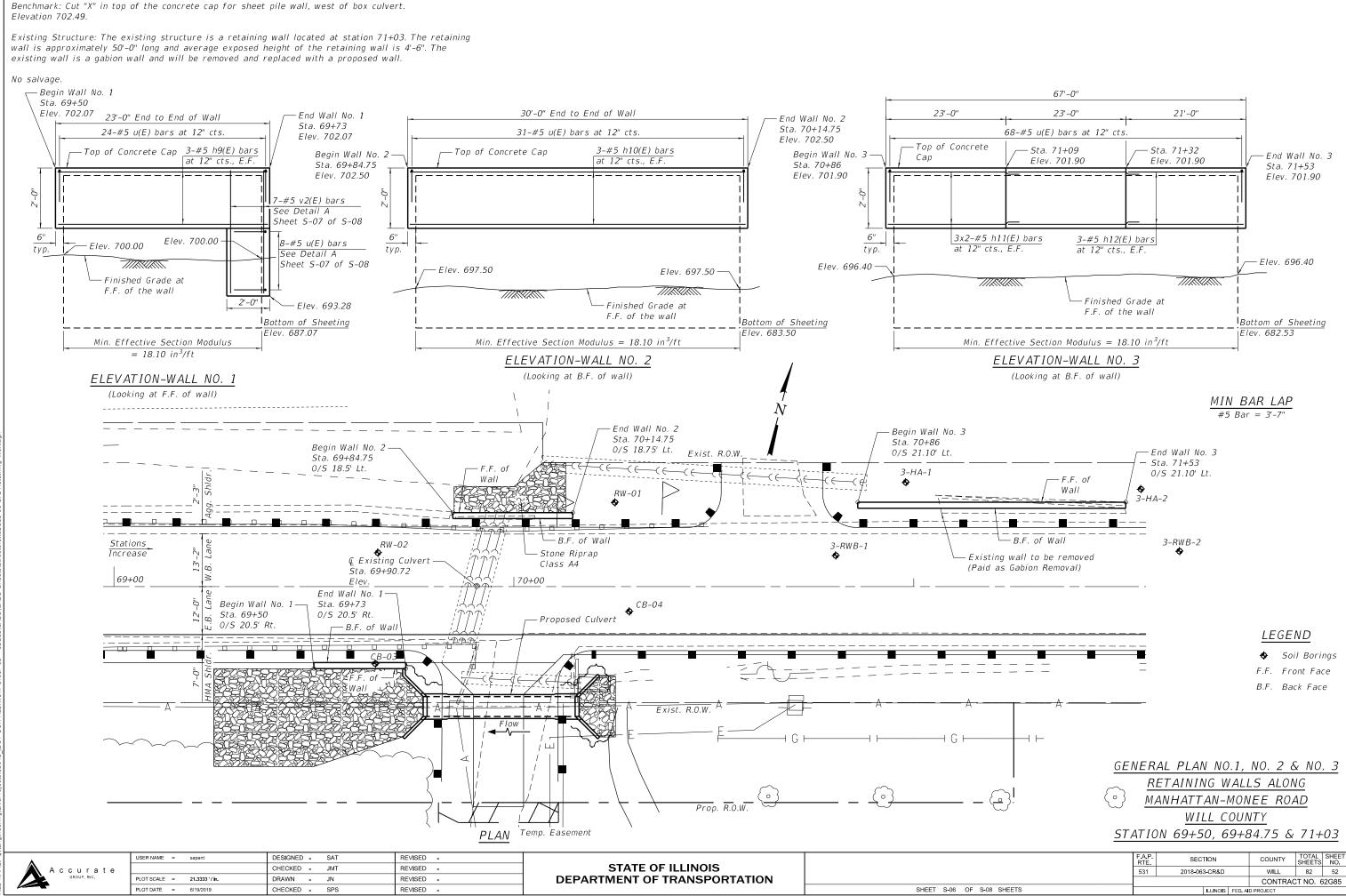
ILLINOIS FED. AID PROJECT



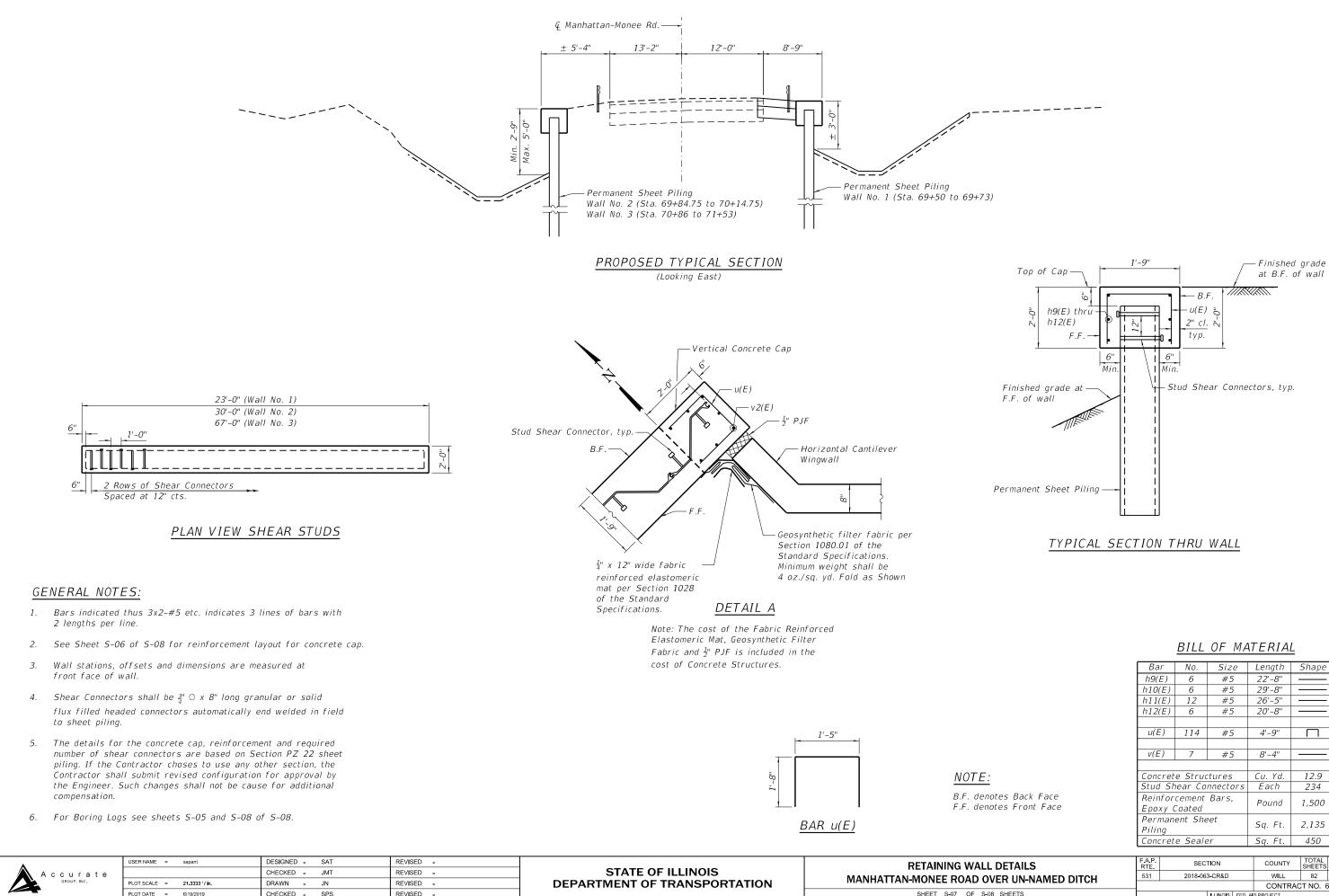
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BILL OF MATERIAL								
Bar	No.	Size	Length	Shape				
a1(E)	167	#6	6'-0''	്				
a2(E)	79	#5	5'-8''					
d(E)	14	#4	4'-5"					
h(E)	28	#5	38'-8"					
h1(E)	10	#4	38'-8"					
h2(E)	8	#7	5'-8''					
h3(E)	24	#5	8'-0''					
h4(E)	24	#5	10'-6"					
h5(E)	8	#5	10'-3"					
h6(E)	9	#5	8'-0''					
h7(E)	18	#5	11'-9"	\smile				
h8(E)	9	#5	13'-3"	\smile				
s(E)	7	#4	4'-10''					
s1(E)	7	#4	4'-8''	Ū				
(=)			5 1 11					
v(E)	84	#4	5'-4"					
v1(E)	59	#4	8'-3''					
<u> </u>			6 V /	27.5				
-		Culverts	Cu. Yd.	27.5				
	rcement Coated	: Bars,	Pound	5,140				
1 /	te Sea	ler	Sq. Ft.	164				

	F.A.P. RTE	SECTION COUNTY			COUNTY	TOTAL SHEETS	SHEET NO.
OVER UN-NAMED DITCH		2018-063-CR&D			WILL	82	50
					CONTRACT NO. 62G85		
S-08 SHEETS			ILLINOIS	FED. A	D PROJECT		



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	Bar	No.	Size	Length	Shape	
	h9(E)	6	#5	22'-8"		
	h10(E)	6	#5	29'-8''		
	h11(E)	12	#5	26'-5"		
	h12(E)	6	#5	20'-8"		
	u(E)	114	#5	4'-9"		
	(=)					
	v(E)	7	#5	8'-4"		
	_					_
	Concret	e Struc	tures	Cu.Yd.	12.9	
	Stud SI	near Co	nnectors	Each	234	
otes Back Face otes Front Face	Reinfor Epoxy		Bars,	Pound	1,500	
	Perman Piling	ent She	et	Sq. Ft.	2,135	
	Concret	e Seale	er	Sq. Ft.	450	
DETAILS	F.A.P. RTE	SEC.	TION	COUNTY	TOTAL SHEETS	SHEET NO.
/ER UN-NAMED DITCH	531	2018-06	3-CR&D	WILL	82	53
				CONTR	ACT NO. 6	62G85
3 SHEETS			ILLINOIS FED.	AID PROJECT		

SHEET S-07 OF S-08