



**Abbreviated Structure Geotechnical Report**

Original Report Date: 05/14/2021 Proposed SN: SN 006-0191 Route: FAI 80 (I-80)  
 Revised Date: \_\_\_\_\_ Existing SN: SN 006-0121 Section: (06-1HB)ES  
 Geotechnical Engineer: Rubino Engineering, Inc. (G21.019) County: Bureau County  
 Structural Engineer: EFK Moen Contract: No. 66K73

<p><b>Indicate the proposed structure type, substructure types, and foundation locations (attach plan and elevation drawing):</b> The proposed bridge configurations consists of a two-span steel plate girder bridge structure with 115-foot spans and a pier in the median. The new bridge will utilize 39-inch web plate girders on integral abutments and hammer spread footing pier supported by piles. A preliminary TSL drawing is attached.</p>
<p><b>Discuss the existing boring data, existing plans foundation information, new subsurface exploration and need for any additional exploration to be provided with SGR Technical Memo (attach all data and subsurface profile plot):</b> The existing plans indicate abutments are supported on concrete piles and the three piers are supported on 10-foot creosote pile-supported spread footings. The original 1961 logs included soil borings at both abutments and at all three piers. In June of 2020, two (2) soil borings by were by IDOT at the abutments and one (1) soil boring was taken at the center pier. Copies of the boring logs are attached.</p>
<p><b>Provide the location and maximum height of any new soil fill or magnitude of footing bearing pressure. Estimate the amount and time of the expected settlement. Indicate if further testing, analysis, and/or ground improvement/treatment is necessary:</b> The new profile of the bridge will change minimally. There are no cuts or fill proposed for this profile and, therefore, minimal settlement is anticipated under the existing embankments. No additional testing or treatment for settlement is anticipated.</p>
<p><b>Identify any new cuts or fill slope angles and heights. Estimate the factor of safety against slope failure. Indicate if further testing, analysis or ground improvement/treatment is necessary:</b> The proposed embankment slope below the bridge will be 1:2. In slope stability analyses, the drained (long-term construction) conditions control over the undrained (short-term construction) conditions. Rubino used the slope stability program Stedwin Version 2.88 to run the Modified Bishop Method. A factor of safety of 2 against slope failure was achieved in the drained condition. No additional analysis or treatment is recommended.</p>
<p><b>Indicate at each substructure, the 100-year and 200-year total scour depths in the Hydraulics report, the non-granular scour depth reduction, the proposed ground surface, and the recommended foundation design scour elevations:</b> Scour is not applicable because this is a grade separation structure.</p>
<p><b>Determining the seismic soil site class, the seismic performance zone, the 0.2 and 1.0 second design spectral accelerations and indicate if that the soils are liquefiable:</b> The seismic data is as follows: Seismic Soil Site Class = D ; Seismic Performance Zone = SPZ 1 ; Design Spectral Acceleration at 0.2 sec. (SDS) = 0.116; Design Spectral Acceleration at 1.0 sec. (SD1) = 0.061. Liquefaction is not applicable because SPZ = 1.</p>
<p><b>Confirm feasibility of the proposed foundation or wall type and provide design parameters. Attach a pile design table indicating feasible pile types, various nominal required bearings, factored resistances available and corresponding estimated lengths at locations where piles will be used. Provide factored bearing resistance and unit sliding resistance at various elevations and confirm no ground improvement/treatment is necessary where spread footings are proposed. Estimated top of rock elevations as well as preliminary factored unit side and tip resistance values shall be indicated when drilled shafts are proposed:</b> See the attached supplemental information.</p>
<p><b>Calculate the estimated water surface elevation and determine the need for cofferdams (type 1 or 2), and seal coat:</b> Water surface elevations and cofferdams/seal coat are not applicable because this is a grade separation structure.</p>
<p><b>Assess the need for sheeting or soil retention or temporary construction slope and provide recommendation for other construction concerns:</b> If the structure will be closed to all traffic during construction, then temporary sheet piling will not be needed to construct the abutments.</p>

Benchmark: Cross in concrete. Sta. 18+65.83, 17.63' right.  
Elevation 664.992

Existing Structure: S.N. 006-0121 originally built in 1962 as Section 06-1HB-2. The structure is a 4-span steel beam bridge on stub abutments founded on concrete piles and solid wall piers founded on timber piles. The length of the structure is 223'-2" bk. to bk. abutments. The width is 29'-8" out to out. Traffic to be detoured with the bridge closed during construction.

Salvage: None

**LOADING HL-93**  
Allow 50#/sq. ft. for future wearing surface.

**DESIGN SPECIFICATIONS**  
2020 AASHTO LRFD Bridge Design  
Specifications, 9th Edition

**DESIGN STRESSES**  
FIELD UNITS

$f'_c = 3,500$  psi  
 $f'_c = 4,000$  psi (Superstructure Concrete)  
 $f_y = 60,000$  psi (Reinforcement)  
 $f_y = 50,000$  psi (M270 Grade 50)

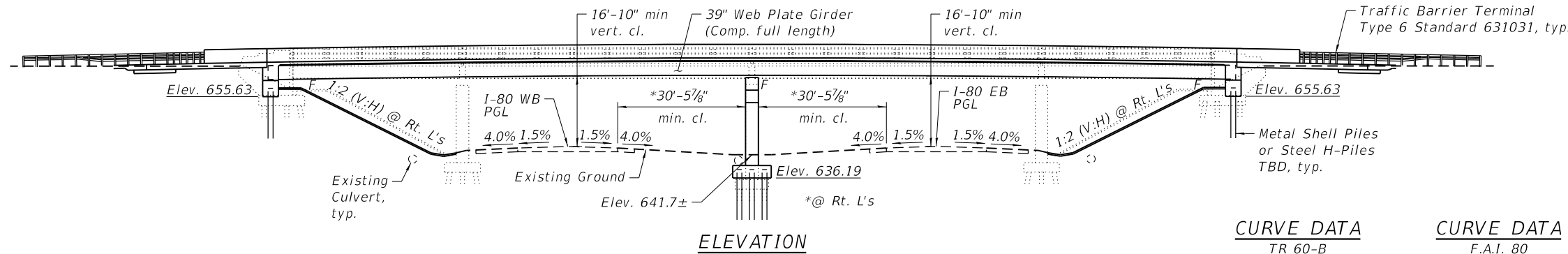
**SEISMIC DATA**

Seismic Performance Zone (SPZ) = 1  
Design Spectral Acceleration at 1.0 sec. (SD1) = g  
Design Spectral Acceleration at 0.2 sec. (SDS) = g  
Soil Site Class =

**HIGHWAY CLASSIFICATION**

TR 60-B (470 St. E.)  
Functional Class: Local  
ADT: 100 (2019); 137 (2032)  
ADTT: 3 (2019); 4 (2032)  
DHV:  
Design Speed: 30 m.p.h.  
Posted Speed: 30 m.p.h.  
2-Way Traffic  
Directional Distribution: 50:50

F.A.I. Rte. 80 (I-80)  
Functional Class: Interstate  
ADT: 17200 (2019); 17925 (2032)  
ADTT: 5848 (2019); 6095 (2032)  
DHV: 1720  
Design Speed: 70 m.p.h.  
Posted Speed: 70 m.p.h.  
2-Way Traffic  
Directional Distribution: 50:50

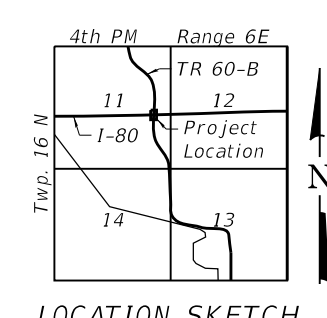
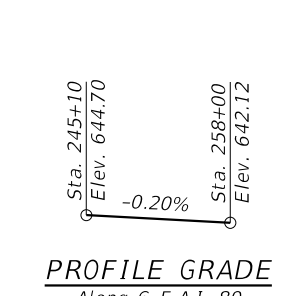
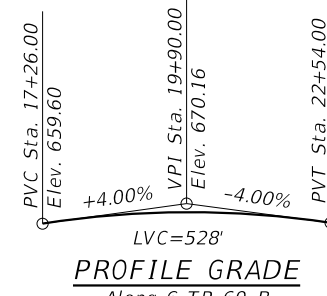
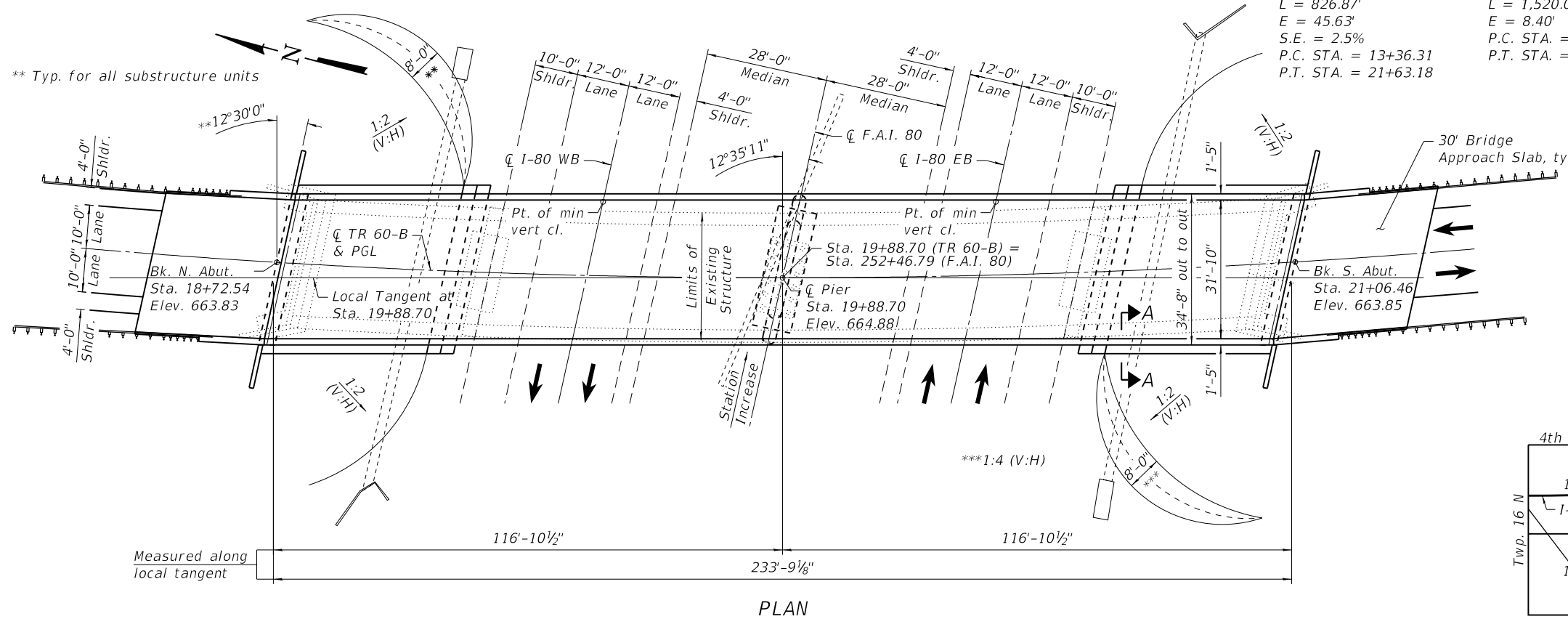


**CURVE DATA**

TR 60-B  
PI STA. = 17+56.32  
 $\Delta = 24^\circ 48' 11"$  (LT)  
 $D = 2^\circ 59' 59"$   
 $R = 1,910.08'$   
 $T = 420.01'$   
 $L = 826.87'$   
 $E = 45.63'$   
S.E. = 2.5%  
P.C. STA. = 13+36.31  
P.T. STA. = 21+63.18

**CURVE DATA**

F.A.I. 80  
PI STA. = 252+22.22  
 $\Delta = 2^\circ 32' 00"$   
 $D = 0^\circ 10' 00"$   
 $R = 34,377.50'$   
 $T = 760.12'$   
 $L = 1,520.00'$   
 $E = 8.40'$   
P.C. STA. = 244+62.10  
P.T. STA. = 259+82.10



**GENERAL PLAN & ELEVATION**  
TR 60-B (470 ST. E.) OVER I-80  
F.A.I. RTE. 80 - SEC. (06-1HB) ES  
BUREAU COUNTY  
STATION 19+88.70  
STRUCTURE NO. 006-0191

MODEL: Default  
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**EFK Moen**  
Civil Engineering Design

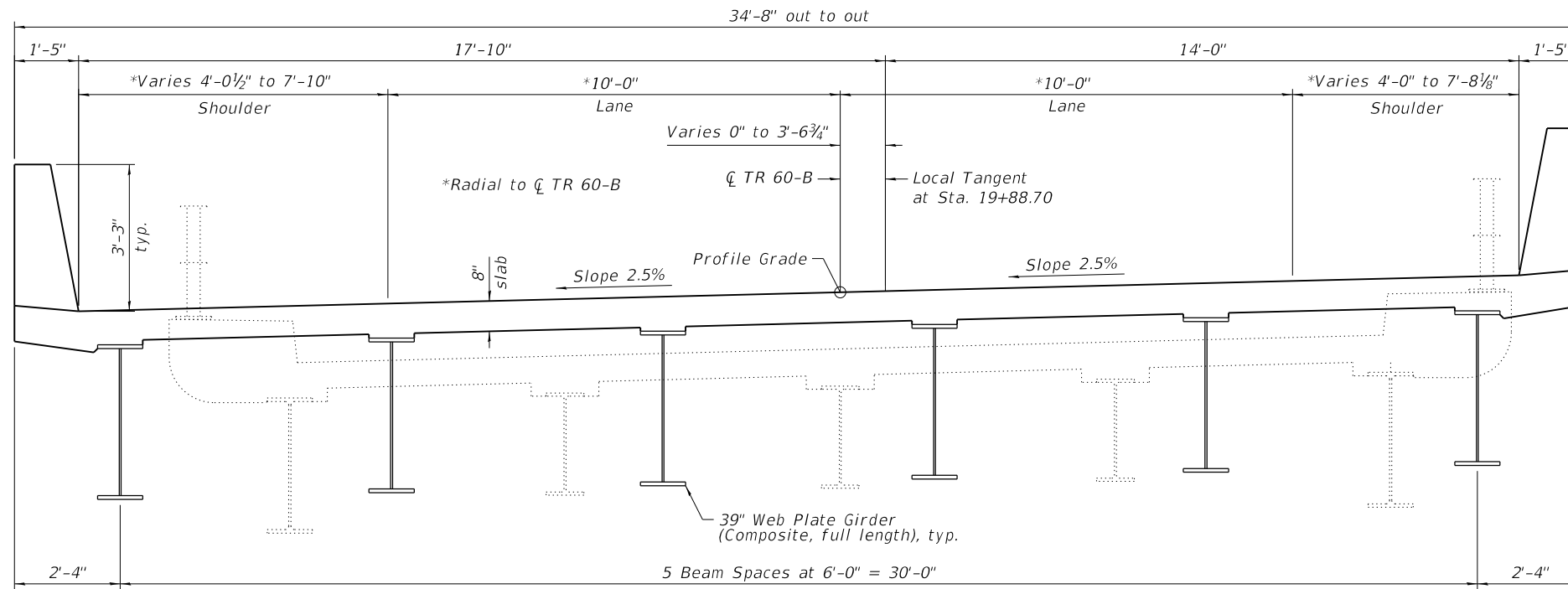
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DRAWN -	ACB	REVISED -	
CHECKED -	CDL	REVISED -	

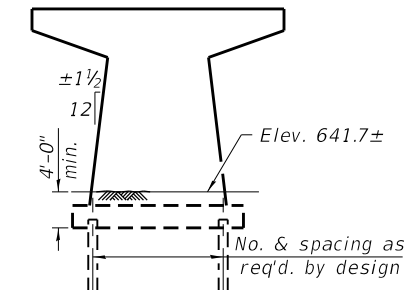
STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION

SHEET 1 OF 2 SHEETS

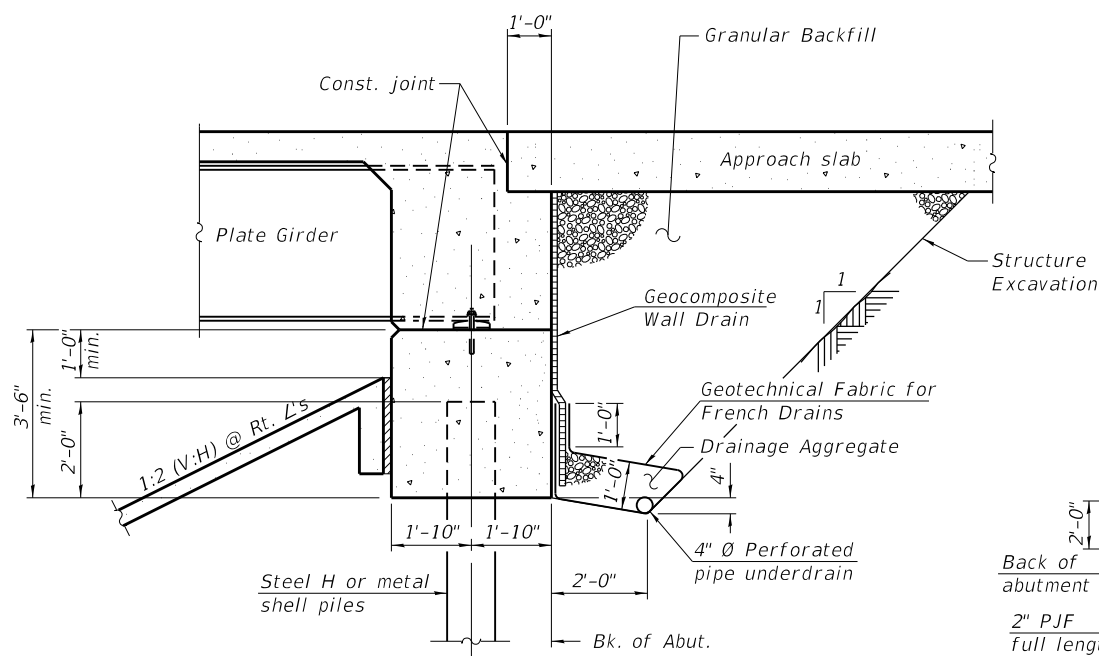
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80	(06-1HB) ES	BUREAU		
CONTRACT NO. 66K73				
ILLINOIS FED. AID PROJECT				



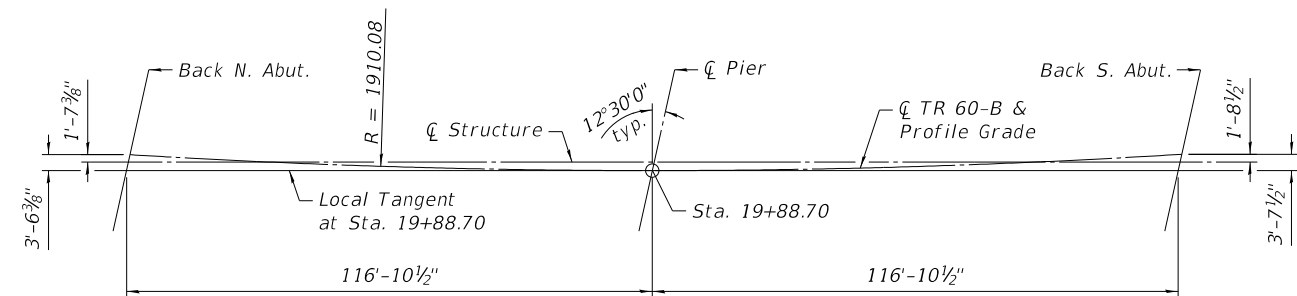
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(Looking South)



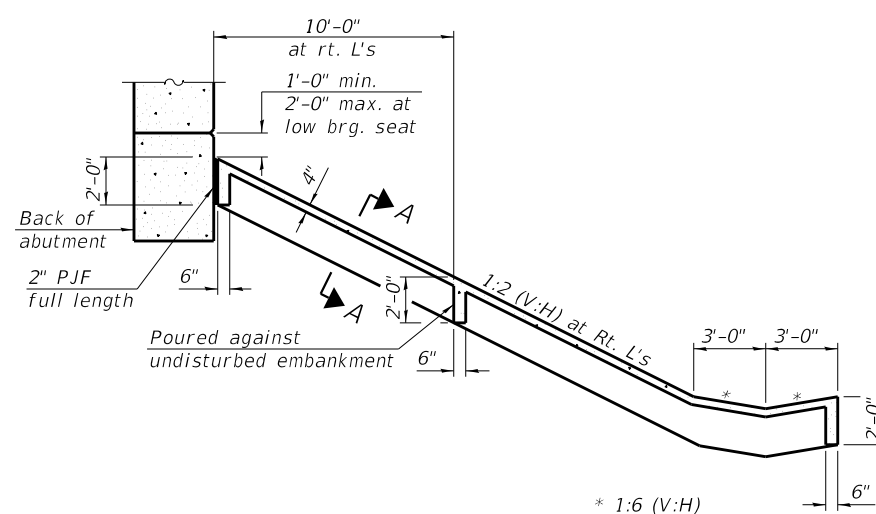
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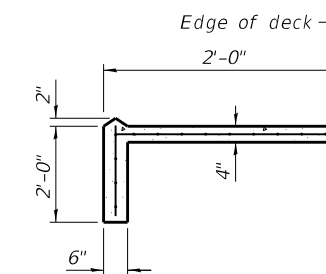
**SECTION THRU INTEGRAL ABUTMENT**  
(Horiz. dim. @ Rt. L's)



**OFFSET SKETCH**



**SECTION THRU CONCRETE SLOPEWALL**



**SECTION A-A**

**DETAILS**  
TR 60-B (470 ST. E.) OVER I-80  
F.A.I. RTE. 80 - SEC. (06-1HB) ES  
BUREAU COUNTY  
STATION 19+88.70  
STRUCTURE NO. 006-0191

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**EFK Moen**  
Civil Engineering Design

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PLOT DATE = 4/14/2021	DRAWN - ACB	REVISED -
	CHECKED - CDL	REVISED -

STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION

SHEET 2 OF 2 SHEETS

F.A.I. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
80	(06-1HB) ES	BUREAU		
CONTRACT NO. 66K73				
ILLINOIS FED. AID PROJECT				

G21.019 - WO 4 SN 006-0191 Bridge Installation









**Illinois Department of Transportation**

Division of Highways  
Illinois Department of Transportation

**SOIL BORING LOG**

Date 6/17/20

ROUTE TR 60-B DESCRIPTION TR 60-B over I-80, 4.78 miles East of the Henry County Line LOGGED BY Larry Myers

SECTION 06-1HB-2 LOCATION SE 1/4, SEC. 11, TWP. 16N, RNG. 6, 4<sup>th</sup> PM,

Latitude 41.38681, Longitude -89.76612

COUNTY Bureau DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME Automatic

STRUCT. NO. 006-0121 (Exist.)  
Station 252+46.79

BORING NO. 02 (N.E. Quad.)  
Station 18+99  
Offset 8.0 ft Lt.  
Ground Surface Elev. 661.90 ft

DEPTH H S	B L O W S	U C S Qu	M O I S T	Surface Water Elev. _____ ft	Stream Bed Elev. _____ ft	DEPTH H S	B L O W S	U C S Qu	M O I S T
(ft)	(/6")	(tsf)	(%)			(ft)	(/6")	(tsf)	(%)
	10								
	17		17						
	21								
	10								
	15		14						
	18								
	-45								
	10								
	15		16				13		
	21						16	4.4	13
							17	S	
					595.40				
	12								
	16		14						
	20								
	-50								
	11								
	14		15						
	22								
					609.90				
	8								
	10	4.1	13						
	11	S							
	-55								
	9								
	11	4.4	13						
	16	S							
	10								
	13	4.2	12						
	19	S							
	-60								

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

SOIL BORING 006-0121.GPJ IL\_DOT.GDT 9/2/20



**Illinois Department of Transportation**

Division of Highways  
Illinois Department of Transportation

**SOIL BORING LOG**

Date 6/18/20

ROUTE TR 60-B DESCRIPTION TR 60-B over I-80, 4.78 miles East of the Henry County Line LOGGED BY Larry Myers

SECTION 06-1HB-2 LOCATION SE 1/4, SEC. 11, TWP. 16N, RNG. 6, 4<sup>th</sup> PM,  
Latitude 41.38652, Longitude -89.76598

COUNTY Bureau DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME Automatic

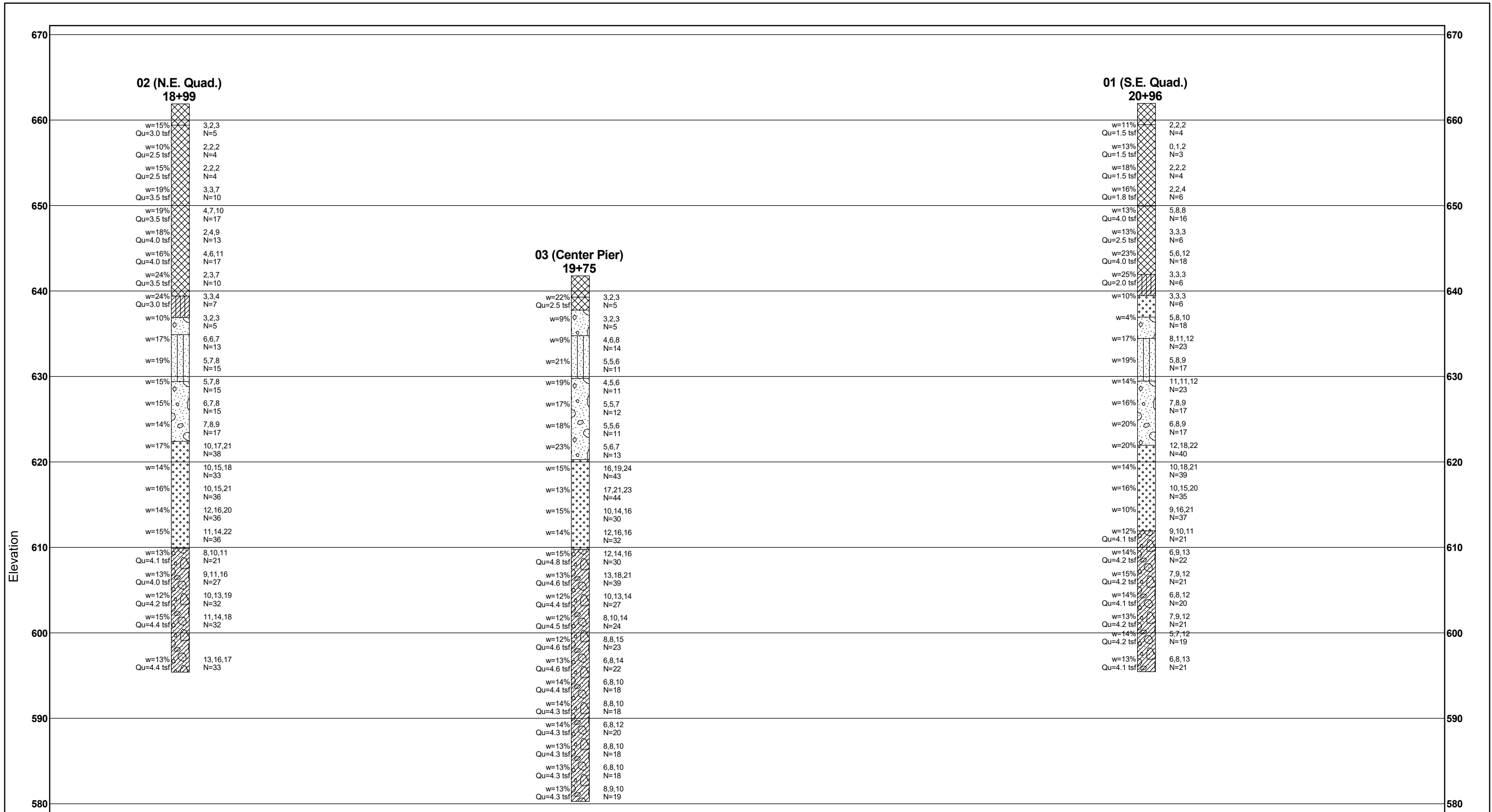
STRUCT. NO.	Station	DEPTH	BLOW	UCS	MOIST	Surface Water Elev.	Stream Bed Elev.	DEPTH	BLOW	UCS	MOIST						
BORING NO.	Station	Offset	Ground Surface Elev.	(ft)	(/6")	(tsf)	(%)	ft	ft	H	S	Qu	T	(ft)	(/6")	(tsf)	(%)
006-0121 (Exist.)	252+46.79		639.28														
03 (Center Pier)	19+75	21.0 ft Lt.	637.78	3													
				2	2.5												
				3	P												
			634.78	3													
				2													
				3													
			629.78	4													
				6													
				8													
				5													
				5													
				6													
			629.78	4													
				5													
				6													
				5													
				5													
				7													
				5													
				5													
				6													
			-20														

SOIL BORING 006-0121.GPJ IL\_DOT\_GDT 9/2/20

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)







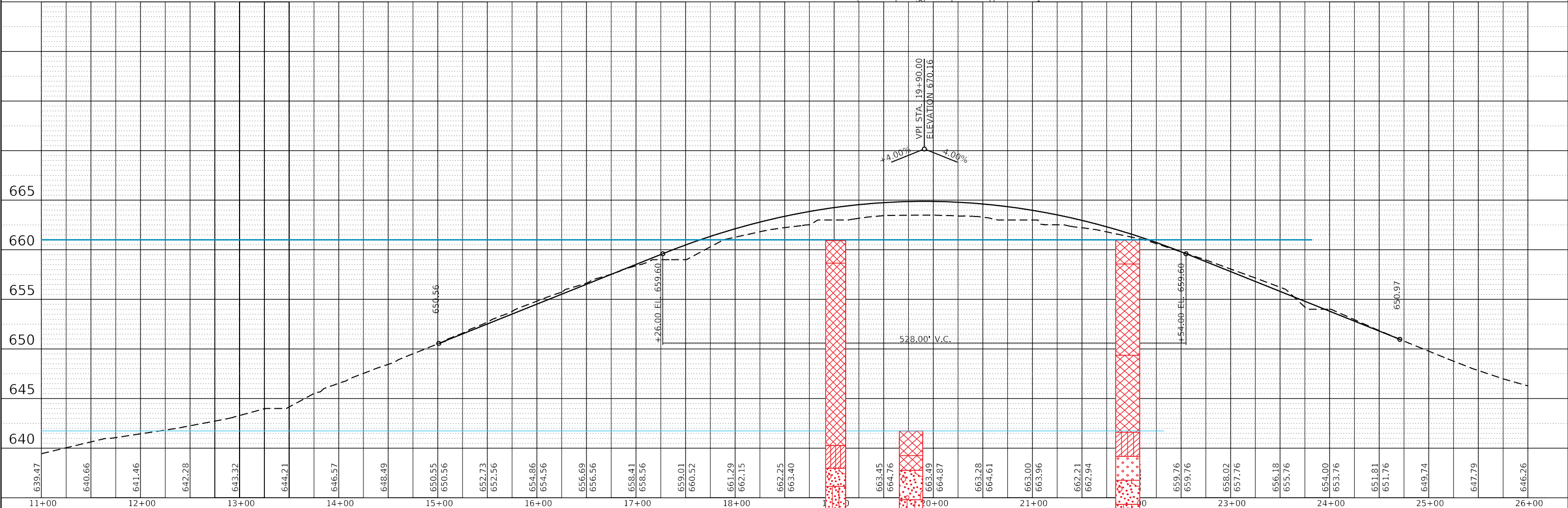
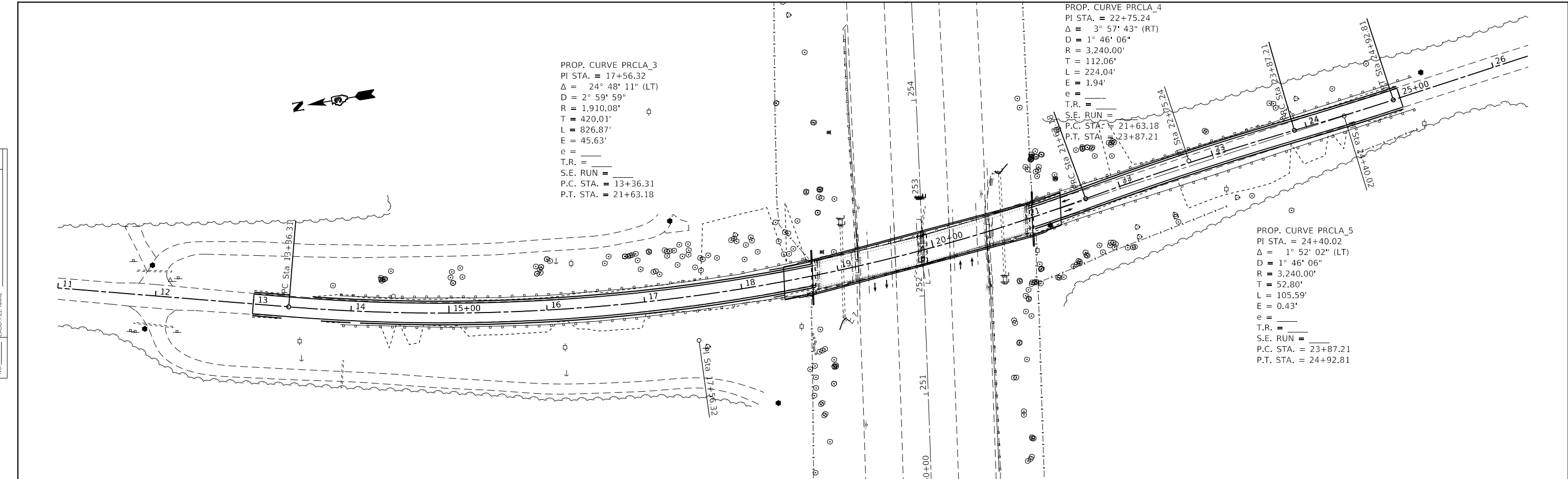
Rubino Engineering, Inc.  
 425 Shepard Drive  
 Elgin, IL 60123  
 Telephone: 847-931-1555  
 Fax: 847-931-1560

## Soil Profile

Rubino Job No.:  
 Project & location: TR 60-B over I-80, 4.78 miles East of the Henry County Line  
 Route: TR 60-B  
 County: Bureau  
 Section: 06-1HB-2

PLAN	SURVEYED	DATE
	PLOTTED	
	ALIGNED	
	CHECKED	
	GRADES	
	NOTATION	
	STRUCTURE	
	NO.	
	FILE NAME	

PROFILE	SURVEYED	DATE
	PLOTTED	
	GRADES	
	CHECKED	
	NOTATION	
	STRUCTURE	
	NO.	
	FILE NAME	



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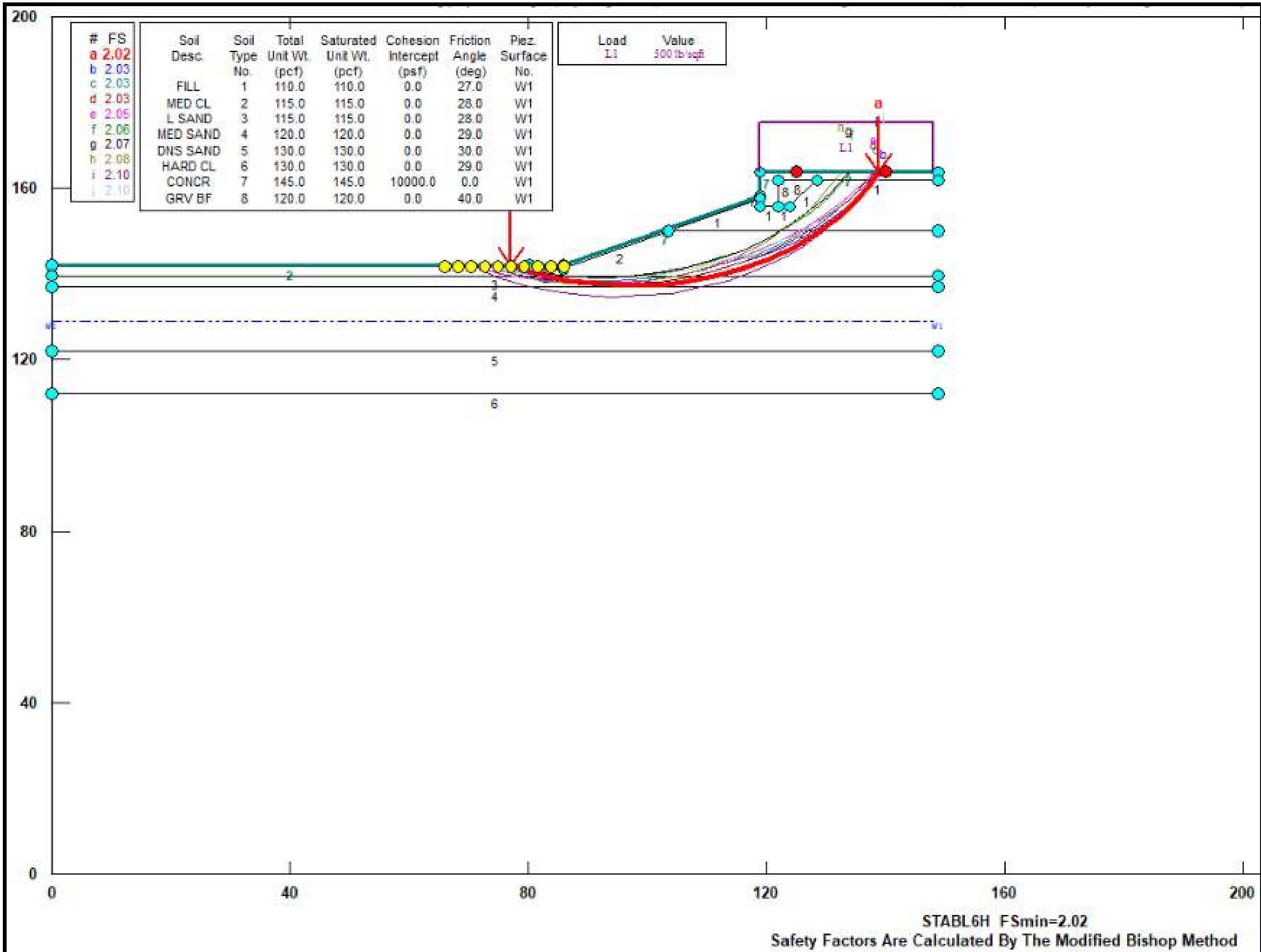
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	DATE -	REVISED -

STATE OF ILLINOIS  
 DEPARTMENT OF TRANSPORTATION

SCALE:	SHEET	OF	TOTAL SHEETS

TR 60B OVER I-80  
 PLAN AND PROFILE

F.A. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
CONTRACT NO.				
ILLINOIS FED. AID PROJECT				



STABL6H FSmin=2.02  
 Safety Factors Are Calculated By The Modified Bishop Method



### ***Integral Abutment Feasibility***

Integral abutments are the preferred end bent type due to elimination of the joints in the bridge decks, decreasing maintenance costs and increasing service life. The proposed structure length typically fits in the range of applicability for integral abutments; the soil at critical depth of 10 feet below the abutments is medium stiff to very stiff. The bottom abutment elevation is 655.63 feet. Critical depth for intergral abutment analysis is 10 feet below the bottom of the abutment elevation.

<b>Abutment</b>	<b>Soil Strengths at Critical Depth</b>	<b>Recommendation</b>
02 (NE Quad) STA 18+99	Qu between 2.5 – 4.0 tsf	Pre-bore with bentonite
01 (SE Quad) STA 20+96	Qu between 1.5 – 4.0 tsf	Pre-bore with bentonite

According to the IDOT ABD Memo 12.3, the integral abutment study only pertains to soils with Qu less than 3.0 tsf. See the attached IDOT BBS 145 spreadsheet for in Situ Integral Abutment Feasibility.

The IDOT Geotechnical Manual discusses pre-coring pile locations to 10 feet below the abutment and backfilling with bentonite pellets, which reduces the soils pressures on the pile during expansion. Rubino has input a Qu of 1.5 tsf over the critical depth in the intergral abutment spreadsheet. Rubino has also omitted the soil strength in the critical depth in the pile spreadsheets.

Utilizing a Qu value of 1.5 tsf for both bentonite and embankment conditions, the results show integral abutments are applicable for all pile sizes. See attached Bentonite/Embankment Integral Abutment Feasibility spreadsheet.

### ***Pile Discussion***

Metal shell piles and H-piles are both considered for integral abutment applications. Tables of estimated pile lengths are attached. Metal shell piles are recommended over H-piles due to bedrock not being encountered. Conical tips are recommended for metal shell piles in very stiff or dense soils. The proposed pile locations need to be checked for conflict with the existing piling. Existing piles should be cut off to an appropriate elevation to not interfere with the new abutment and pile system.

**GENERAL DATA**

STRUCTURE NUMBER===== SN 006-0121  
 STRUCTURE TYPE ===== MULTI-SPAN  
 STRUCTURE SKEW===== 12.5864 DEGREES  
 SUPER. DATA IN REFERENCE TO SUB. DATA ===== ABUT 1  
 TOTAL STRUCTURE LENGTH===== 233.76 FT  
 NUMBER OF SPANS ===== 2  
 END SPAN LENGTH ===== 116.88 FT  
 ADJACENT INTERIOR SPAN LENGTH ===== 0.01 FT

SUPERSTRUCTURE POSITIVE MOMENT REGION DATA (END OR MAIN SPAN)		
BEAM TYPE ===== PLATE GIRDER		
TOP FLANGE WIDTH =====	10.00	IN
TOP FLANGE THICKNESS =====	1.00	IN
WEB DEPTH =====	39.00	IN
WEB THICKNESS =====	1.00	IN
BOTTOM FLANGE WIDTH =====	10.00	IN
BOTTOM FLANGE THICKNESS =====	1.00	IN
BEAM SPACING PERP. TO CL =====	6.00	FT
SLAB THICKNESS =====	8.00	IN
SLAB F'C =====	4.00	KSI

SUPERSTRUCTURE POSITIVE MOMENT REGION DATA (ADJACENT SPAN)		
TOP FLANGE WIDTH =====	10.00	IN
TOP FLANGE THICKNESS =====	1.00	IN
WEB DEPTH =====	39.00	IN
WEB THICKNESS =====	1.00	IN
BOTTOM FLANGE WIDTH =====	10.00	IN
BOTTOM FLANGE THICKNESS =====	1.00	IN
BEAM SPACING PERP. TO CL =====	6.00	FT
SLAB THICKNESS =====	8.00	IN
SLAB F'C =====	4.00	KSI

ABUTMENT #1 DATA		
ABUTMENT NAME ===== S.E. Quard. Abutment		
ABUTMENT REFERENCE BORING =====	B-1	
BOTTOM OF ABUTMENT ELEVATION =====	655.63	FT
ESTIMATED NUMBER OF PILES AT ABUT. =====	6	
PILE SPACING PERP. TO CL =====	6	FT

ABUTMENT #2 DATA		
ABUTMENT NAME ===== N.E. Quad Abutment		
ABUTMENT REFERENCE BORING =====	B-2	
BOTTOM OF ABUTMENT ELEVATION =====	655.63	FT
ESTIMATED NUMBER OF PILES AT ABUT. =====	6	
PILE SPACING PERP. TO CL =====	6	FT

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #1				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
653.13	2.50	1.5		
650.63	2.50	1.8		
648.13	2.50	4.0		
645.63	2.50	2.5		

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #2				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
653.13	2.50	2.5		
650.63	2.50	3.5		
648.13	2.50	3.5		
645.63	2.50	4.0		

10.00 FT = TOTAL DEPTH ENTERED

10.00 FT = TOTAL DEPTH ENTERED

WEIGHTED AVERAGE Qu FOR ABUTMENT #1===== 2.45 TSF

WEIGHTED AVERAGE Qu FOR ABUTMENT #2===== 3.38 TSF

PILE STIFFNESS MODIFIER FOR ABUTMENT #1  
 = 1/(1.45-[0.3\*2.45])===== 1.40

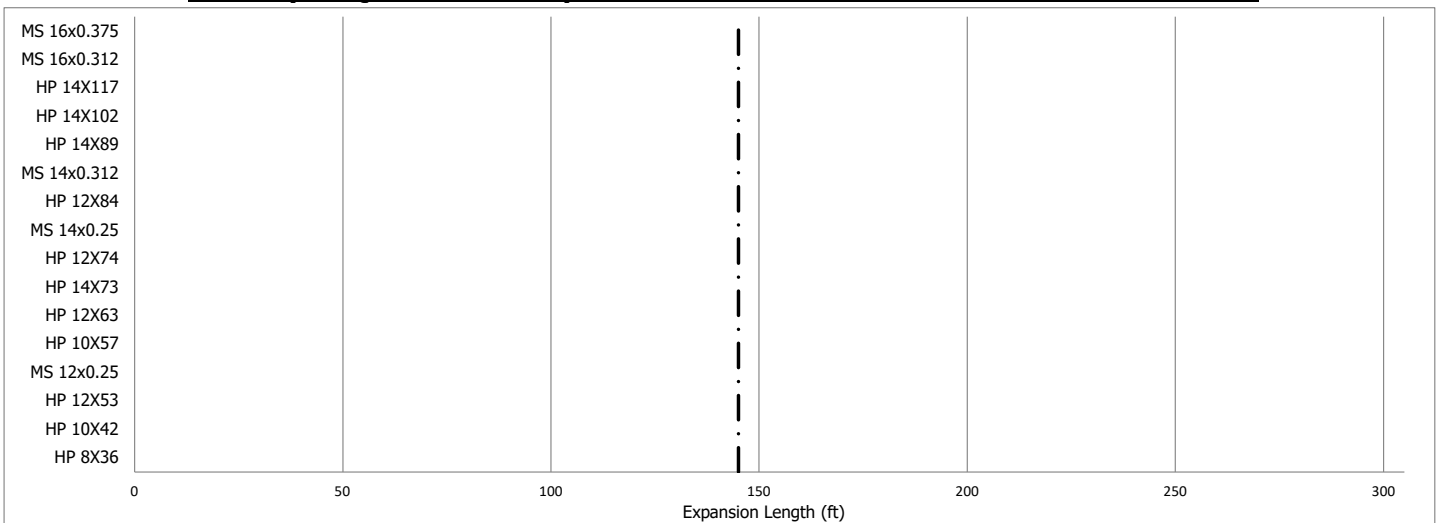
PILE STIFFNESS MODIFIER FOR ABUTMENT #2  
 = 1/(1.45-[0.3\*3.38])===== 2.29

**WEIGHTED AVG. Qu > 3.0 TSF WITH TRIB. LENGTH > 20%, INTEGRAL ABUTMENT STRUCTURE NOT ALLOWED**

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #1 = [1.4\*6\*0+2.29\*6\*233.76]/[1.4\*6+2.29\*6]===== 145.02 FT

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #2 = [2.29\*6\*0+1.4\*6\*233.76]/[2.29\*6+1.4\*6]===== 88.74 FT

**ABUT 1 (S.E. Quard. Abutment) - EXPANSION LENGTH LIMIT CHART - 12.6 DEG. SKEW**



----- = Estimated expansion length for the indicated abutment. Piles with an expansion length greater than this are suitable for consideration.  
 (Note: The same size pile should be used at both abutments.)

**GENERAL DATA**

STRUCTURE NUMBER===== SN 006-0121  
 STRUCTURE TYPE ===== MULTI-SPAN  
 STRUCTURE SKEW===== 12.5864 DEGREES  
 SUPER. DATA IN REFERENCE TO SUB. DATA ===== ABUT 1  
 TOTAL STRUCTURE LENGTH===== 233.76 FT  
 NUMBER OF SPANS ===== 2  
 END SPAN LENGTH ===== 116.88 FT  
 ADJACENT INTERIOR SPAN LENGTH ===== 0.01 FT

SUPERSTRUCTURE POSITIVE MOMENT REGION DATA (END OR MAIN SPAN)		
BEAM TYPE ===== PLATE GIRDER		
TOP FLANGE WIDTH =====	10.00	IN
TOP FLANGE THICKNESS =====	1.00	IN
WEB DEPTH =====	39.00	IN
WEB THICKNESS =====	1.00	IN
BOTTOM FLANGE WIDTH =====	10.00	IN
BOTTOM FLANGE THICKNESS =====	1.00	IN
BEAM SPACING PERP. TO CL =====	6.00	FT
SLAB THICKNESS =====	8.00	IN
SLAB F'C =====	4.00	KSI

SUPERSTRUCTURE POSITIVE MOMENT REGION DATA (ADJACENT SPAN)		
TOP FLANGE WIDTH =====	10.00	IN
TOP FLANGE THICKNESS =====	1.00	IN
WEB DEPTH =====	39.00	IN
WEB THICKNESS =====	1.00	IN
BOTTOM FLANGE WIDTH =====	10.00	IN
BOTTOM FLANGE THICKNESS =====	1.00	IN
BEAM SPACING PERP. TO CL =====	6.00	FT
SLAB THICKNESS =====	8.00	IN
SLAB F'C =====	4.00	KSI

ABUTMENT #1 DATA		
ABUTMENT NAME ===== S.E. Quard. Abutment		
ABUTMENT REFERENCE BORING =====	B-1	
BOTTOM OF ABUTMENT ELEVATION =====	655.63	FT
ESTIMATED NUMBER OF PILES AT ABUT. =====	6	
PILE SPACING PERP. TO CL =====	6	FT

ABUTMENT #2 DATA		
ABUTMENT NAME ===== N.E. Quad Abutment		
ABUTMENT REFERENCE BORING =====	B-2	
BOTTOM OF ABUTMENT ELEVATION =====	655.63	FT
ESTIMATED NUMBER OF PILES AT ABUT. =====	6	
PILE SPACING PERP. TO CL =====	6	FT

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #1				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
653.13	2.50	1.5		
650.63	2.50	1.5		
648.13	2.50	1.5		
645.63	2.50	1.5		

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #2				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
653.13	2.50	1.5		
650.63	2.50	1.5		
648.13	2.50	1.5		
645.63	2.50	1.5		

10.00 FT = TOTAL DEPTH ENTERED

10.00 FT = TOTAL DEPTH ENTERED

WEIGHTED AVERAGE Qu FOR ABUTMENT #1===== 1.50 TSF

WEIGHTED AVERAGE Qu FOR ABUTMENT #2===== 1.50 TSF

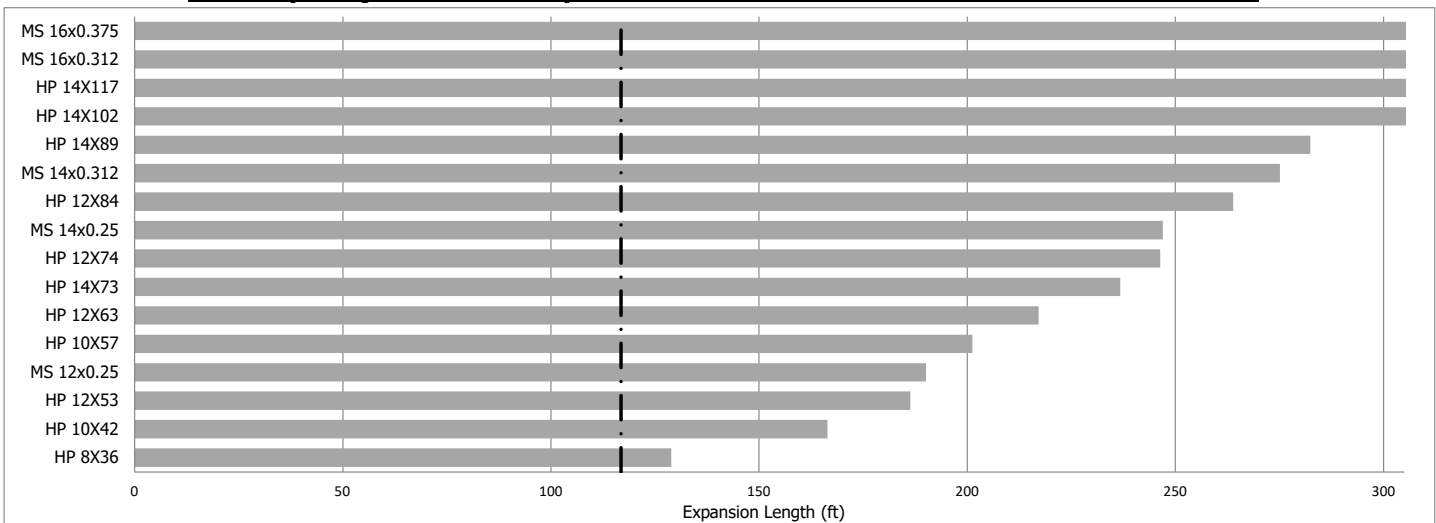
PILE STIFFNESS MODIFIER FOR ABUTMENT #1  
 = 1/(1.45-[0.3\*1.5])===== 1.00

PILE STIFFNESS MODIFIER FOR ABUTMENT #2  
 = 1/(1.45-[0.3\*1.5])===== 1.00

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #1 = [1\*6\*0+1\*6\*233.76]/[1\*6+1\*6]===== 116.88 FT

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #2 = [1\*6\*0+1\*6\*233.76]/[1\*6+1\*6]===== 116.88 FT

**ABUT 1 (S.E. Quard. Abutment) - EXPANSION LENGTH LIMIT CHART - 12.6 DEG. SKEW**



----- = Estimated expansion length for the indicated abutment. Piles with an expansion length greater than this are suitable for consideration.  
 (Note: The same size pile should be used at both abutments.)



**Pile Design Table for SE Abutment utilizing Boring #01**

Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)
<b>Metal Shell 12"Φ w/.25" walls</b>			<b>Steel HP 10 X 42</b>			<b>Steel HP 12 X 84</b>		
140	77	26	147	81	51	145	80	46
188	104	31	162	89	53	174	95	48
200	110	33	179	99	56	195	107	51
<b>Metal Shell 14"Φ w/.25" walls</b>			196	108	58	214	117	53
83	46	18	211	116	61	235	129	56
174	96	21	<b>Steel HP 10 X 57</b>			255	140	58
176	97	26	151	83	51	274	151	61
236	130	31	166	92	53	<b>Steel HP 14 X 73</b>		
250	138	33	184	101	56	158	87	43
<b>Metal Shell 14"Φ w/.312" walls</b>			200	110	58	167	92	46
83	46	18	216	119	61	201	110	48
174	96	21	<b>Steel HP 12 X 53</b>			234	129	51
176	97	26	138	76	46	255	140	53
236	130	31	166	91	48	280	154	56
250	138	33	187	103	51	303	166	58
350	193	46	205	113	53	324	178	61
379	209	48	225	124	56	<b>Steel HP 14 X 89</b>		
407	224	51	245	135	58	149	82	41
434	239	53	263	145	61	162	89	43
463	255	56	<b>Steel HP 12 X 63</b>			170	94	46
492	270	58	141	77	46	204	112	48
519	285	61	169	93	48	237	130	51
<b>Metal Shell 16"Φ w/.312" walls</b>			189	104	51	258	142	53
100	55	18	207	114	53	283	156	56
215	118	26	228	125	56	307	169	58
288	159	31	247	136	58	328	180	61
305	168	33	266	146	61	<b>Steel HP 14 X 102</b>		
408	224	46	<b>Steel HP 12 X 74</b>			152	83	41
441	243	48	143	79	46	165	91	43
474	261	51	172	94	48	172	95	46
504	277	53	192	105	51	207	114	48
538	296	56	210	116	53	240	132	51
570	313	58	231	127	56	262	144	53
601	330	61	251	138	58	287	158	56
<b>Metal Shell 16"Φ w/.375" walls</b>			270	148	61	311	171	58
100	55	18	<b>Steel HP 12 X 74</b>			332	183	61
215	118	26	143	79	46	<b>Steel HP 14 X 117</b>		
288	159	31	172	94	48	155	85	41
305	168	33	192	105	51	169	93	43
408	224	46	210	116	53	175	96	46
441	243	48	231	127	56	210	115	48
474	261	51	251	138	58	244	134	51
504	277	53	270	148	61	266	146	53
538	296	56	<b>Steel HP 8 X 36</b>			291	160	56
570	313	58	154	85	58	315	173	58
601	330	61	166	91	61	337	185	61
						<b>Precast 14"x 14"</b>		
						106	58	18
						222	122	21
						224	123	26

**Pile Design Table for North Abutment utilizing Boring #02**

	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)		Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)		Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)
<b>Metal Shell 12"Φ w/.25" walls</b>				<b>Steel HP 10 X 42</b>				<b>Steel HP 12 X 84</b>			
	142	78	26		150	83	51		148	81	41
	170	93	28		166	91	53		159	88	43
	181	99	31		169	93	56		171	94	46
	201	111	33		172	94	58		175	96	48
<b>Metal Shell 14"Φ w/.25" walls</b>					176	97	61		199	110	51
	157	86	23	<b>Steel HP 10 X 57</b>				218	120	53	
	176	97	26		154	85	51	222	122	56	
	212	117	28		170	94	53	226	124	58	
	225	124	31		173	95	56	231	127	61	
	251	138	33		176	97	58	<b>Steel HP 14 X 73</b>			
<b>Metal Shell 14"Φ w/.312" walls</b>					180	99	61		157	86	38
	157	86	23	<b>Steel HP 12 X 53</b>				169	93	41	
	176	97	26		150	83	43	182	100	43	
	212	117	28		161	89	46	196	108	46	
	225	124	31		168	92	48	204	112	48	
	251	138	33		191	105	51	238	131	51	
	373	205	48		209	115	53	261	143	53	
	404	222	51		213	117	56	265	146	56	
	544	299	53		216	119	58	269	148	58	
	560	308	56		222	122	61	276	152	61	
<b>Metal Shell 16"Φ w/.312" walls</b>				<b>Steel HP 12 X 63</b>				<b>Steel HP 14 X 89</b>			
	142	78	21		154	85	43		148	82	36
	190	105	23		165	91	46		161	88	38
	214	118	26		170	93	48		173	95	41
	259	143	28		193	106	51		187	103	43
	274	151	31		212	116	53		200	110	46
	306	168	33		215	118	56		208	114	48
	434	239	48		219	120	58		242	133	51
	470	259	51		224	123	61		265	146	53
	648	356	53	<b>Steel HP 12 X 74</b>				269	148	56	
<b>Metal Shell 16"Φ w/.375" walls</b>					157	86	43		273	150	58
	142	78	21		168	92	46		280	154	61
	190	105	23		172	95	48	<b>Steel HP 14 X 102</b>			
	214	118	26		196	108	51		151	83	36
	259	143	28		215	118	53		163	90	38
	274	151	31		219	120	56		176	97	41
	306	168	33		222	122	58		190	104	43
	434	239	48		228	125	61		203	112	46
	470	259	51						210	115	48
	648	356	53						245	135	51
	666	366	56						268	148	53
	684	376	58						272	150	56
	709	390	61						277	152	58
<b>Steel HP 8 X 36</b>									283	156	61
	137	76	61					<b>Steel HP 14 X 117</b>			
									155	85	36
									167	92	38
									181	99	41
									194	107	43
									207	114	46
									213	117	48
									249	137	51
									272	150	53
									276	152	56
									280	154	58
									287	158	61
								<b>Precast 14"x 14"</b>			
									152	84	21
									200	110	23
									225	124	26

**Pile Design Table for Center Pier utilizing Boring #03**

Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	
<b>Metal Shell 12"Φ w/.25" walls</b>			<b>Steel HP 10 X 42</b>			<b>Steel HP 12 X 84</b>			
390	215	46	251	138	56	325	178	56	
<b>Metal Shell 14"Φ w/.25" walls</b>			<b>Steel HP 10 X 57</b>			<b>Steel HP 14 X 73</b>			
407	224	41	257	141	56	383	210	56	
434	239	44	<b>Steel HP 12 X 53</b>			<b>Steel HP 14 X 89</b>			
<b>Metal Shell 14"Φ w/.312" walls</b>			312	172	56	387	213	56	
407	224	41	<b>Steel HP 12 X 63</b>			<b>Steel HP 14 X 102</b>			
434	239	44	315	173	56	392	216	56	
463	254	46	<b>Steel HP 12 X 74</b>			<b>Steel HP 14 X 117</b>			
491	270	49	320	176	56	398	219	56	
520	286	51	<b>Precast 14"x 14"</b>						
549	302	54	175      96      16						
<b>Metal Shell 16"Φ w/.312" walls</b>									
404	222	36							
440	242	39							
474	261	41							
505	278	44							
537	295	46							
570	313	49							
603	331	51							
636	350	54							
<b>Metal Shell 16"Φ w/.375" walls</b>									
404	222	36							
440	242	39							
474	261	41							
505	278	44							
537	295	46							
570	313	49							
603	331	51							
636	350	54							
668	368	56							
<b>Steel HP 8 X 36</b>									
199	109	56							

<b>EFK+Moen, LLC</b>	By: <a href="#">ACB</a>	Date: 1/26/2021	Job No.
Civil Engineering Design	Chkd By: <a href="#">CDL</a>	Date: 1/28/2021	20027.08
For: <a href="#">TR 60B over I-80</a>	Bckchk By:	Date:	Sht. No.

\\server18\PROJECTSSS4\20027.08 IDOT D3 PTB194-027 WO8 TR 60B over I-80 TS&L\Structural\TSL\{Prelim Loads and Elevations.xlsx}Summary-WF

### **Abutments**

Summary of Loads	(k)	Strength I		Extreme I		Service I	
		Factor	Factored Load	Factor	Factored Load	Factor	Factored Load
DC	455	1.25	569	1.25	569	1.00	455
DW	57	1.50	86	1.50	86	1.00	57
LL+I	202	1.75	353	0.00	0	1.00	202
EQ (T)	74	0.00	0	1.00	74	0.00	0
EQ (L)	74	0.00	0	1.00	74	0.00	0
WS (T)	12	0.00	0	0.00	0	0.30	4
WS (L)	0	0.00	0	0.00	0	0.30	0
WL (T)	6	0.00	0	0.00	0	1.00	6
WL (L)	2	0.00	0	0.00	0	1.00	2
<b>Total Vertical</b>			<b>1007</b>		<b>654</b>		<b>714</b>
<b>Total Transverse</b>			<b>0</b>		<b>74</b>		<b>10</b>
<b>Total Longitudinal</b>			<b>0</b>		<b>74</b>		<b>2</b>

### **Piers**

Summary of Loads	(k)	Strength I		Extreme I		Service I	
		Factor	Factored Load	Factor	Factored Load	Factor	Factored Load
DC	1252	1.25	1565	1.25	1565	1.00	1252
DW	222	1.50	333	1.50	333	1.00	222
LL+I	435	1.75	761	0.00	0	1.00	435
EQ (T)	214	0.00	0	1.00	214	0.00	0
EQ (L)	214	0.00	0	1.00	214	0.00	0
WS (T)	24	0.00	0	0.00	0	0.30	7
WS (L)	0	0.00	0	0.00	0	0.30	0
WL (T)	12	0.00	0	0.00	0	1.00	12
WL (L)	5	0.00	0	0.00	0	1.00	5
<b>Total Vertical</b>			<b>2659</b>		<b>1898</b>		<b>1909</b>
<b>Total Transverse</b>			<b>0</b>		<b>214</b>		<b>19</b>
<b>Total Longitudinal</b>			<b>0</b>		<b>214</b>		<b>5</b>

All loads are preliminary and subject to refinement during the TSL and final design.