

<b>Original Report Date:</b> <u>2/7/2024</u>	<b>Proposed SN:</b> <u>101-2053</u>	<b>Route:</b> <u>Bypass 20/I-39</u>
<b>Revised Date:</b> <u>4/4/2024</u>	<b>Existing SN:</b> <u>101-2025</u>	<b>Section:</b> <u>(201-3)K and (4-1,5)R</u>
<b>Geotechnical Engineer:</b> <u>Matt D. Masterson, PE</u>		<b>County:</b> <u>Winnebago</u>
<b>Structural Engineer:</b> <u>Matthew Hellenthal, PE, SE</u>		<b>Contract:</b> <u>64C24</u>

**Indicate the proposed structure type, substructure types, and foundation locations (attach plan and elevation drawing):** The proposed new structure carrying I-39/US Rte. 20 over Madigan Creek will be a triple barrel concrete box culvert. Each barrel has an interior cross section of 9' across by 9' high, with an approximate length of 313'-0". See Location Map - Exhibit A, and the TS&L drawing - Exhibit C for more details.

**Discuss the existing boring data, existing plans foundation information, new subsurface exploration and need for any additional exploration to be provided with SGR Technical Memo (attach all data and subsurface profile plot):** Three boring logs, labeled B-1d, B-2d, and B-3, were provided to Kaskaskia Engineering Group, LLC. by IDOT. Borings B-1d and Boring B-2d were drilled in April 2008. Boring B-3 was drilled in August 2020. Location of the borings are shown on the attached Boring Location Plan (Exhibit B). Boring B-3 was drilled in the roadway on top of the embankment. In general, the subsurface condition for B-3 can be stratified into three layers. The top layer consisted mostly of sandy loam and had N-values ranging from 12 to 25 blows per foot (bpf),  $Q_u$  values ranging from 0.8 to 4.5 tsf, and moisture contents ranging from 8.0 to 23.0 percent. The bottom of the top layer is at approximately El. 743. The middle layer consists of sand and sandy gravel with a bottom at approximately El. 732. The middle layer N-values ranged from 32 to 76 bpf, and no moisture contents were recorded. A third lower layer, which consisted of very dense sandy loam till, was encountered before termination. The boring was terminated at El. 716.62. The N-values for the bottom layer ranged from 17 to 51 bpf, with  $Q_u$  values between from 1.4 to 2.3 tsf, and moisture contents ranging from 9.0 to 26.0 percent. Borings B-1d and B-2d were drilled near the openings of the culvert, and were taken down to depths of 28.5 ft BGE and 26 ft BGE respectively. Both borings encountered loam/sandy loam/sand/silt down to approximately El 716.1. N-values of these soils ranged from 6 to 27 bpf, with  $Q_u$  values between 0.4 to 4.6 tsf, and moisture contents between 8 and 22 percent. Boring B-1d encountered very dense limestone at El 715.5 to termination at El 711. Blow counts for the limestone ranged from 47 bpf to 100 blows per 5" of penetration. Boring B-2d encountered hard Loam Till from El 716.1 to termination at El 711.6. N-values for the Loam Till ranged from 35 to 37 bpf, with UCS values between 4.6 and 6.3 tsf, and moisture contents of 8 percent. Detailed information regarding the nature and thickness of the soils encountered and the results of the field sampling and laboratory testing are shown on the Boring Logs - Exhibit D and Subsurface Profile - Exhibit E.

**Provide the location and maximum height of any new soil fill or magnitude of footing bearing pressure. Estimate the amount and time of the expected settlement. Indicate if further testing, analysis, and/or ground improvement/treatment is necessary:** The soil encountered in the boring at the anticipated bearing elevation of the culvert consist of a very dense Sandy Gravel. The assumed bearing elevation at the bottom of the culvert is El. 735.18ft +/- . The soil characteristics of Boring B-3 at the bearing elevation has a N-Value of 43 and a UCS of 0 tsf. The allowable bearing pressure for support of the new culvert in underlying, sandy gravel is estimated to be in excess of 45 ksf, using an LRFD Factor of 0.5. Sliding resistance was estimated at 187.5 psf. Applied pressures are not anticipated to be exceeded with the new construction. See Exhibit F for calculations performed.

Settlement calculations were done for the western portion of the culvert where new fill is being added. Settlement was calculated to be an estimated 0.5 inches for this portion of the culvert. The rest of the culvert will apply less or similar loading than the current existing load that will be removed, so no settlement is expected for this portion of the culvert. Due to the low magnitude of total settlement in only the western portion of the culvert, and thus use of a 2 foot unsuitable removal and replacement platform for uniform support of the culvert, no additional improvement/treatment is necessary. See Settlement Calculations - Exhibit G for additional details.

**Identify any new cuts or fill slope angles and heights. Estimate the factor of safety against slope failure. Indicate if further testing, analysis or ground improvement/treatment is necessary:** The slope geometries were analyzed in SLOPE/W for the upstream and downstream sides of the culvert, with a slope inclination of the fill slope of 1V:3H. For the upstream and downstream slopes, Boring B-3 was used for the soil parameters. Two conditions were modeled: end-of-construction (Undrained) and long-term (Drained). A critical factor of safety (F.O.S.) was calculated for each condition. According to the current standard of practice, the target F.O.S. is 1.5 for end-of-construction and long-term slope stability. The analysis for the upstream side of the culvert resulted in an end-of-construction F.O.S. of 3.5 and a long-term F.O.S. of 1.9. The analysis of the downstream side of the culvert resulted in an end-of-construction F.O.S. of 3.7 and a long-term F.O.S of 2.3. The results indicate that an acceptable F.O.S. will exist under undrained and drained conditions. No additional ground improvement/treatments are necessary for

long term support of the proposed slopes. Results of the slope stability analysis are attached in Exhibit H - Slope Stability Analysis.

**Indicate at each substructure, the 100-year and 200-year total scour depths in the Hydraulics report, the non-granular scour depth reduction, the proposed ground surface, and the recommended foundation design scour elevations:** Q100 for the proposed culvert is El. 745.66 and the Q500 is El. 746.73. A Q200 was not estimated for this structure. The upstream invert elevation is 737.38 ft. and the downstream invert elevation is 735.49 ft.

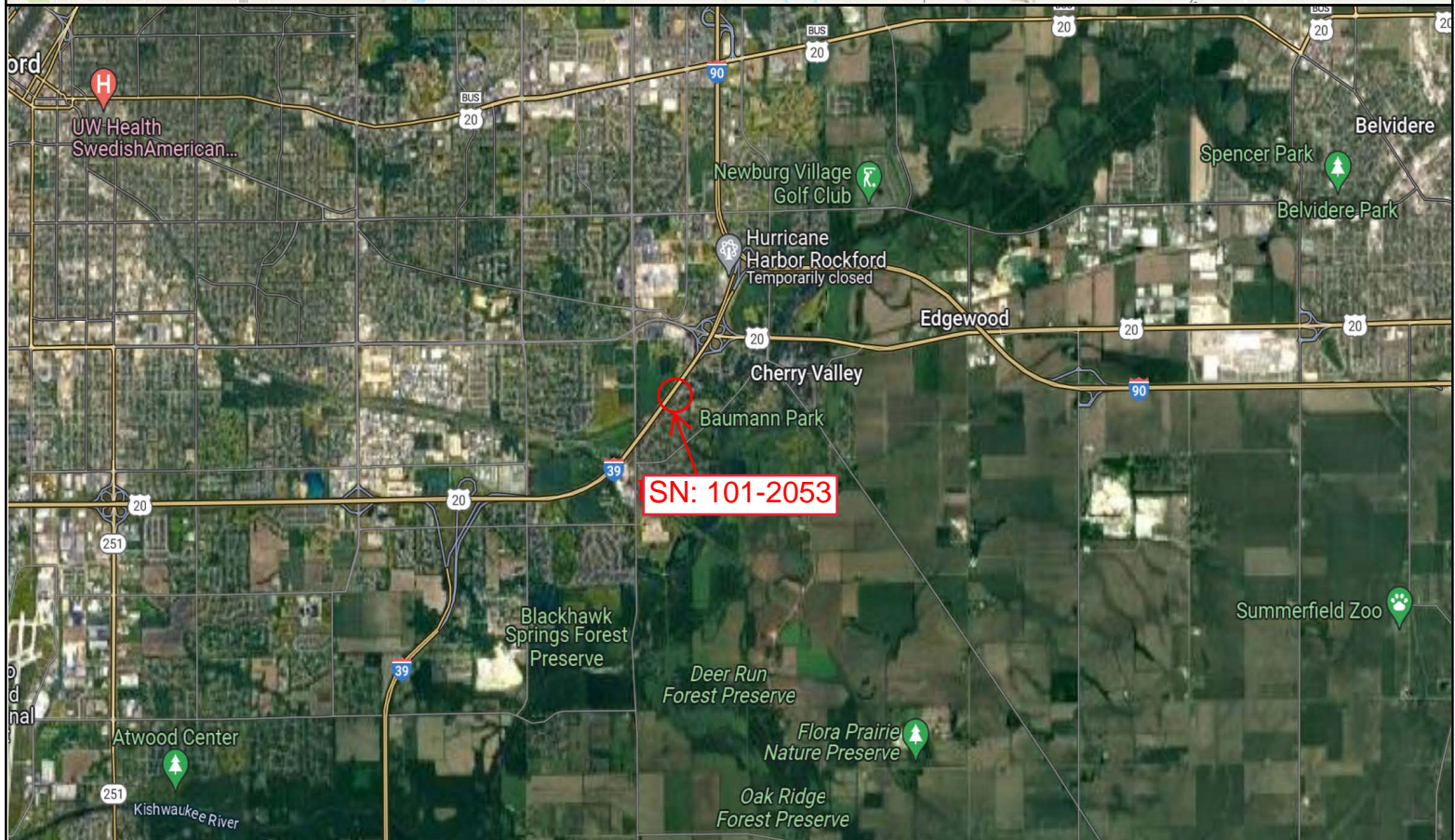
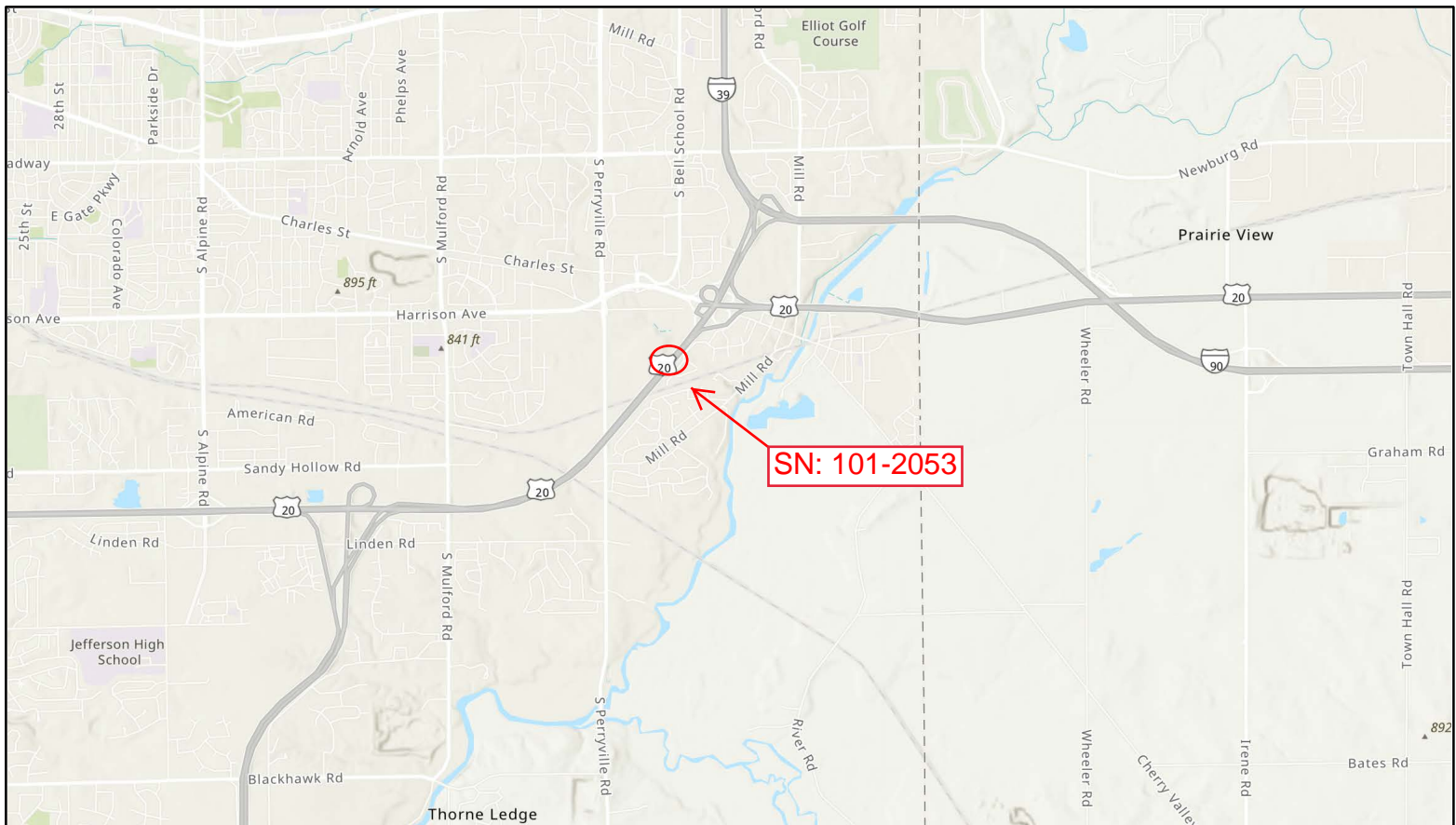
**Determining the seismic soil site class, the seismic performance zone, the 0.2 and 1.0 second design spectral accelerations and indicate if that the soils are liquefiable:** As per Bridge Manual v. 2012, Section 2.3.10, seismic data is not required for buried structures.

**Confirm feasibility of the proposed foundation or wall type and provide design parameters. Attach a pile design table indicating feasible pile types, various nominal required bearings, factored resistances available and corresponding estimated lengths at locations where piles will be used. Provide factored bearing resistance and unit sliding resistance at various elevations and confirm no ground improvement/treatment is necessary where spread footings are proposed. Estimated top of rock elevations as well as preliminary factored unit side and tip resistance values shall be indicated when drilled shafts are proposed:** The soils are sufficient for support of the proposed box culvert according to the analysis done for bearing capacity attached as Exhibit F.

**Calculate the estimated water surface elevation and determine the need for cofferdams (type 1 or 2), and seal coat:** E.W.S.E: 737.9

**Assess the need for sheeting or soil retention or temporary construction slope and provide recommendation for other construction concerns:** Temporary Soil Retention Systems may be required for support of any required Stage construction for retained heights greater than 15 feet and should be designed in accordance with IDOT Design Guide 3.13.1 - Temporary Sheet Piling Design.

**EXHIBIT A**  
**LOCATION MAP**



## LOCATION MAP

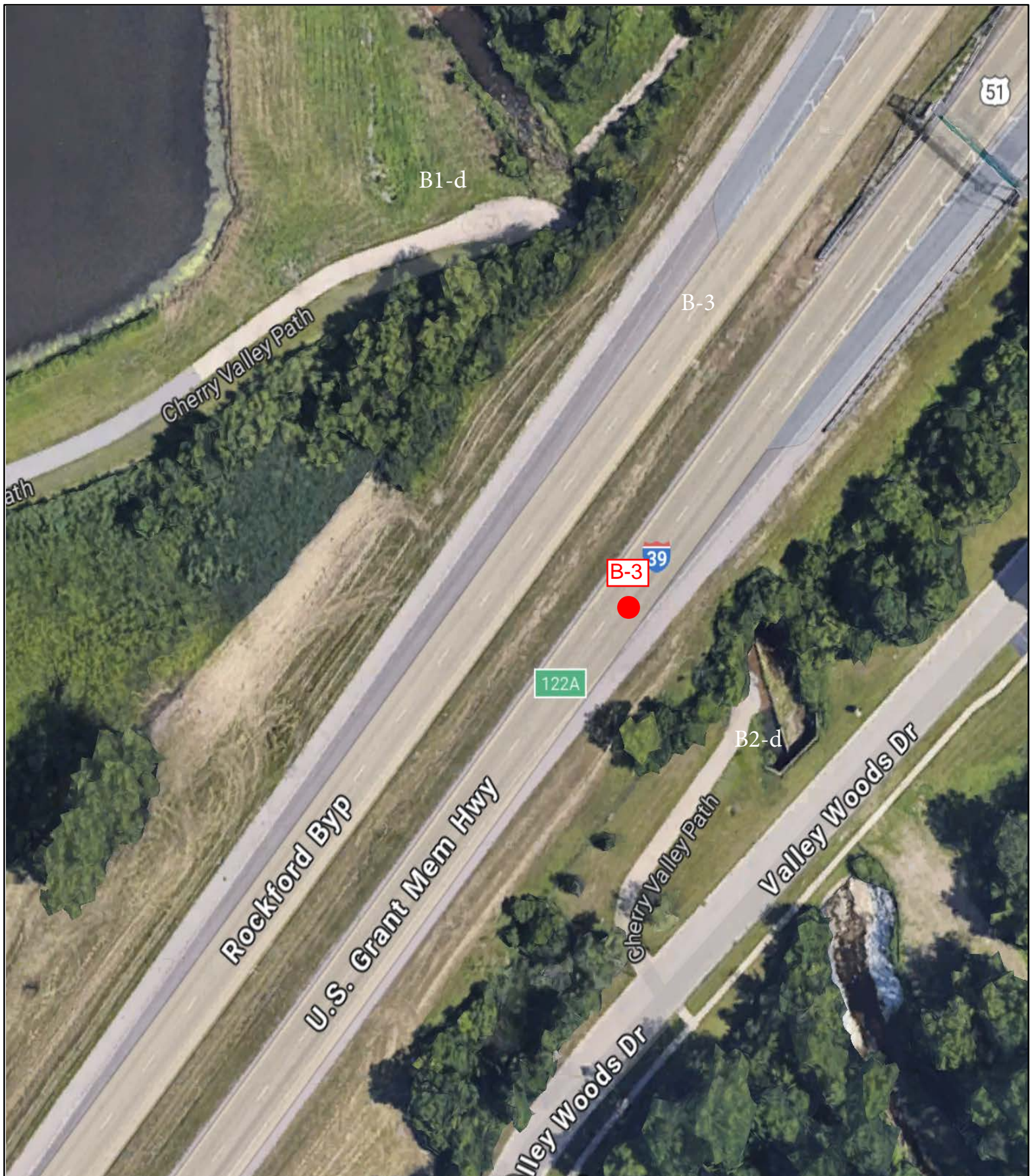
I-39 over Madigan Creek  
Section: (201-3)R & (4-1,5)R  
Winnebago County, Illinois

Exhibit No.

**A**

KEG JOB # 19-1138.00

**EXHIBIT B**  
**BORING PLAN**



**BORING PLAN**

**I-39 over Madigan Creek  
Section: (201-3)R & (4-1,5)R  
Winnebago County, Illinois**

**Exhibit No.**

**B**

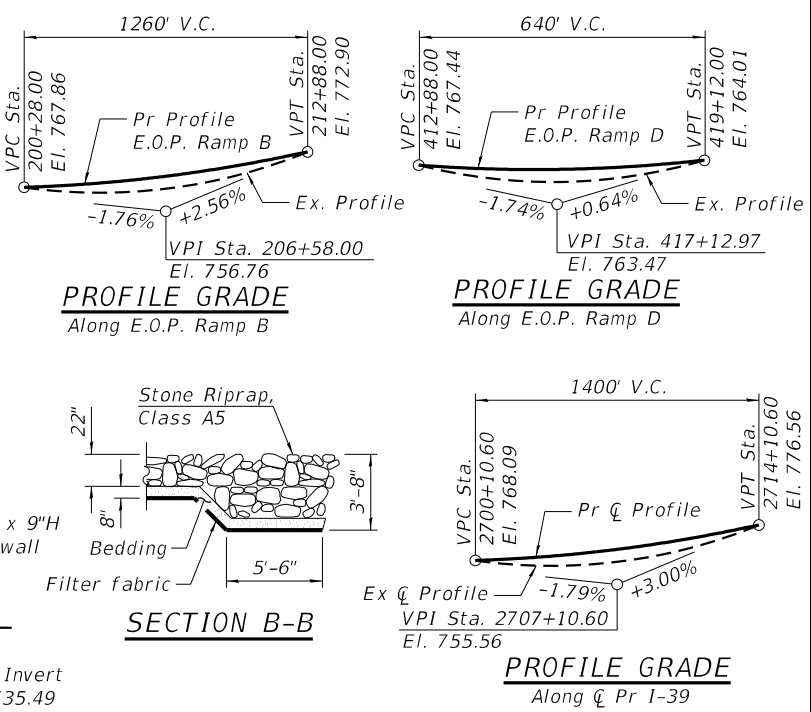
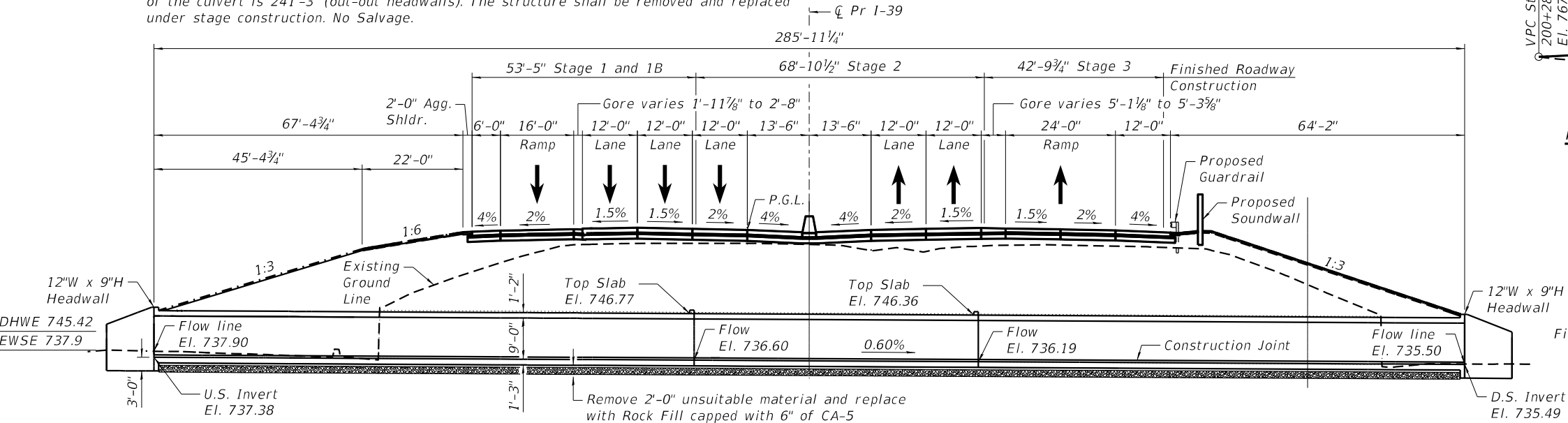
**KEG JOB #19-1138.00**

**EXHIBIT C**

**TYPE, SIZE AND LOCATION PLAN**

**Existing Structure:** The existing culvert S.N. 101-2025 was constructed in 1963 as a 12'-0"x10'-0" (WxH) double barrel reinforced concrete box culvert at Sta. 2708+77. Skewed 25° Left Ahead. The culvert consists of a 12" thick top slab, 13" bottom slab, 10" sidewalls with horizontal cantilever wingwalls and maximum fill height of approximately 16 feet. The overall length of the culvert is 241'-3" (out-out headwalls). The structure shall be removed and replaced under stage construction. No Salvage.

**Bench Mark: #405** Found cut "X" on the northwest bolt of east end of the overhead sign for "Belvidere Exit 122A" on exit ramp on I39 North. 42°14'10.2"N 88°58'06.7"W, El. 770.67



**WATERWAY INFORMATION**

Drainage Area = 5.8 Sq. Mi.									
Exist. Overtopping El. = 756.6 at Sta. 2706+00									
Prop. Overtopping El. = 756.6 at Sta. 2706+00									
Flood	Freq. Yr.	Q C.F.S.	Opening Sq. Ft.	Nat. H.W.E.	Exist.	Prop.	Exist.	Prop.	Headwater El.
	10	994	158	172					743.86
Design	50	1,382	196	212					745.42
Base	100	1,518	207	224					745.66
Max. Calc.	500	1,903	235	243					747.03

Existing 10-year outlet Velocity = 5.8 ft./s.  
Proposed 10-year outlet Velocity = 5.1 ft./s.

**LONGITUDINAL SECTION**

Looking North  
(Dimensions shown are at Right Angles to  $\bar{C}$  Pr. I-39)

**HIGHWAY CLASSIFICATION**

F.A.I. Rte. 39 - I-39/U.S. 20  
Functional Class: Interstate  
ADT: 54,096 (2024) ; 77,290 (2044)  
ADTT: 14,042 (2024); 20,063 (2044)  
DHV: 7,290 (2044)  
Design Speed: 70 m.p.h.  
Posted Speed: 65 m.p.h.  
2-Way Traffic  
Directional Distribution: 50:50

**DESIGN SPECIFICATIONS**

2020 AASHTO LRFD Bridge Design Specifications, 9th Edition

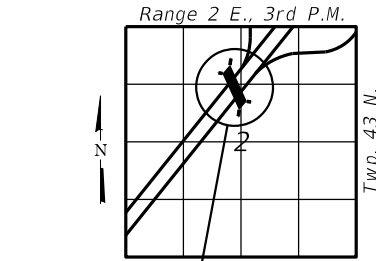
**DESIGN STRESSES**

**FIELD UNITS**

$f'_c$  = 3,500 psi  
 $f_y$  = 60,000 psi (Reinforcement)  
Precast Option Not Allowed

**LOADING HL-93**

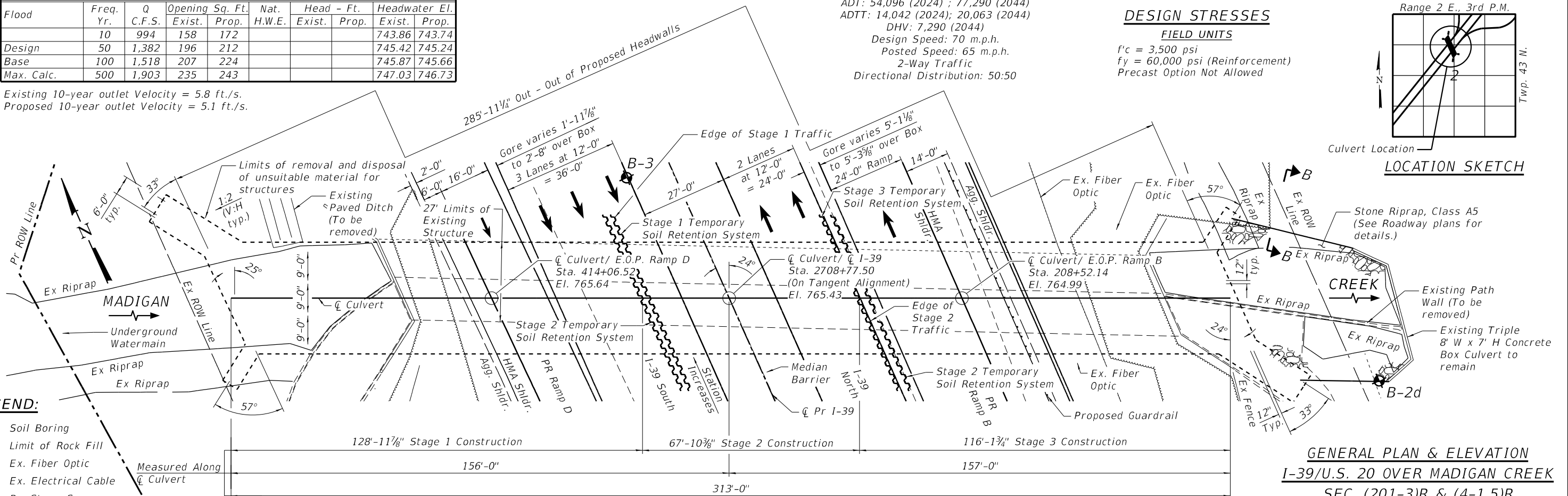
Allow 50#/sq. ft. for future wearing surface.



**LOCATION SKETCH**

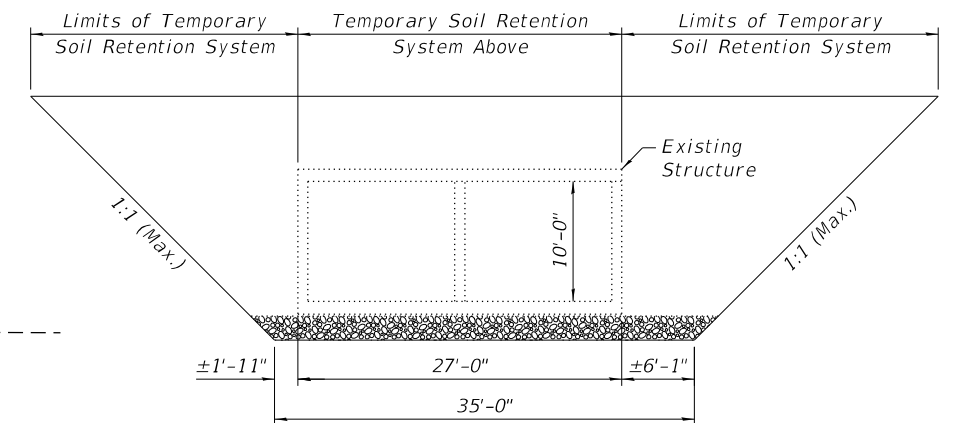
**LEGEND:**

- Soil Boring
- Limit of Rock Fill
- Ex. Fiber Optic
- Ex. Electrical Cable
- Pr. Storm Sewer
- Underground Watermain
- Pr. Access Control
- Ex. Access Control
- Stone Riprap
- Rock Fill

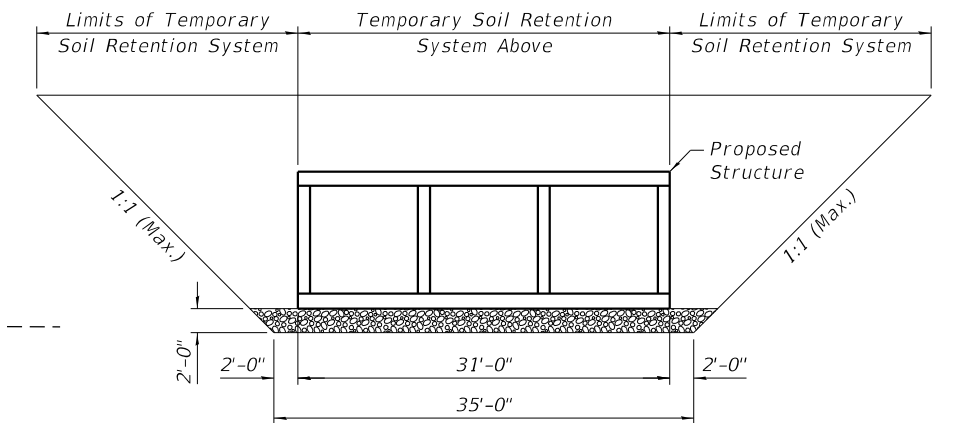


**PLAN VIEW**

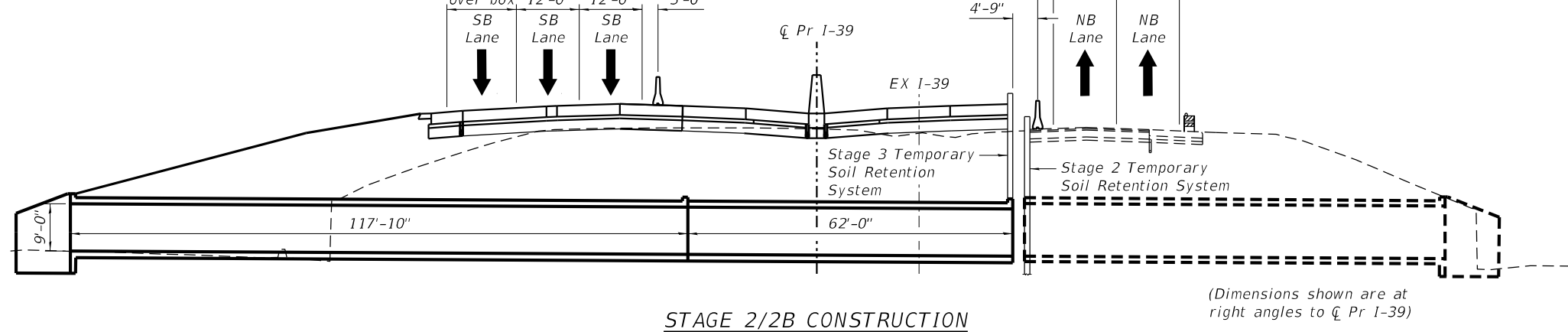
**GENERAL PLAN & ELEVATION**  
**I-39/U.S. 20 OVER MADIGAN CREEK**  
**SEC. (201-3)R & (4-1,5)R**  
**WINNEBAGO COUNTY**  
**STATION 2708+77.50**  
**STRUCTURE NO. 101-2053**



### STAGE 1B REMOVAL



### STAGE 1B CONSTRUCTION



STAGE 2/2B CONSTRUCTION

DETAILS 1  
STRUCTURE NO. 101-2053

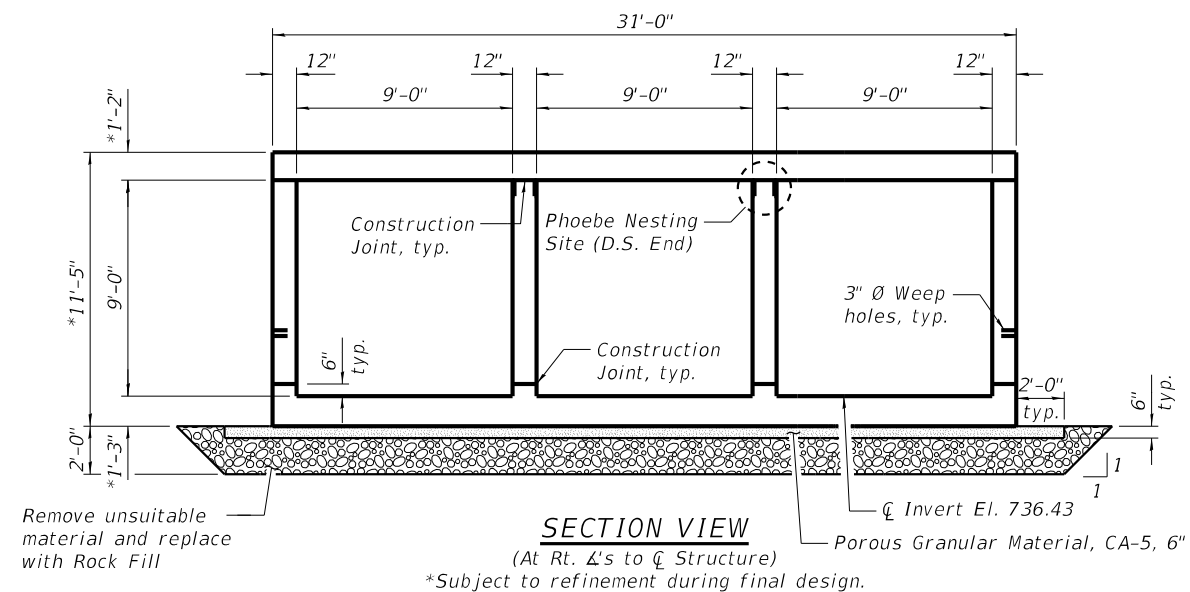
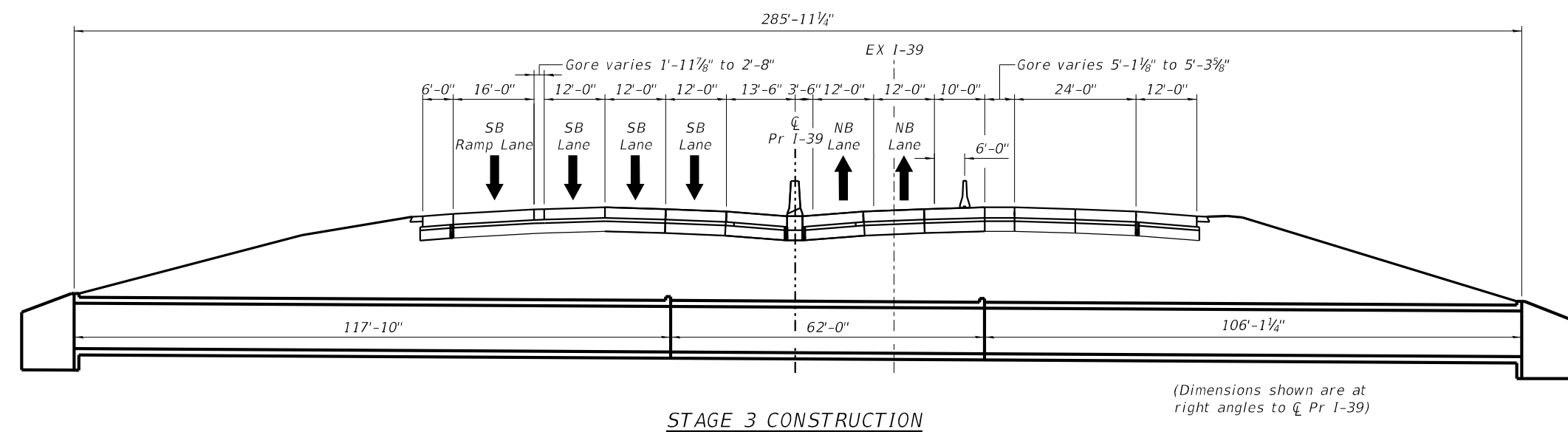
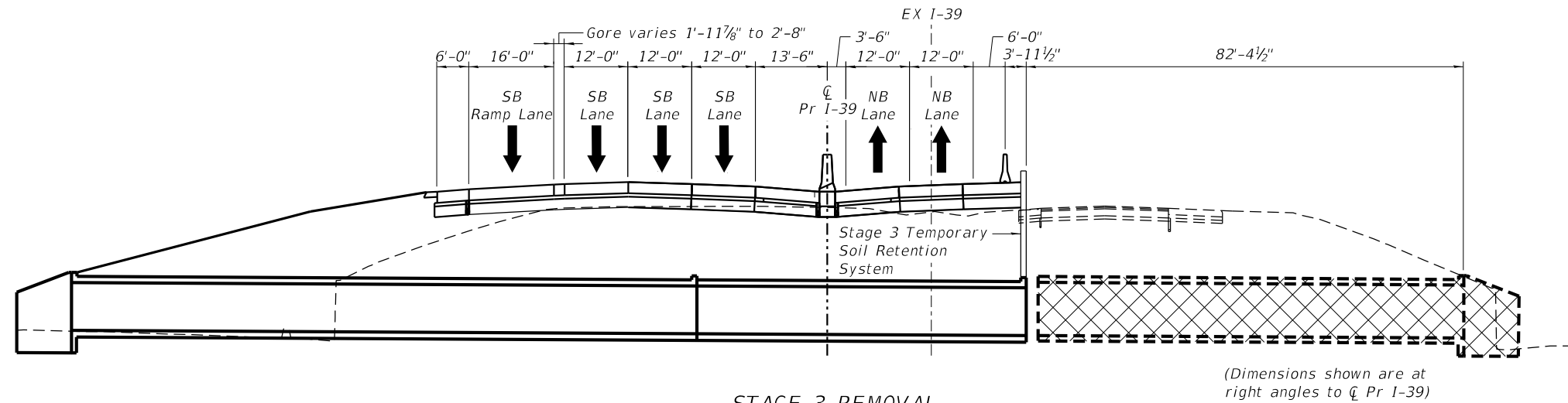
F.A.I. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
F.A.I. 39	(201-3)R & (4-1.5)R	WINNEBAGO	3	2
WHA # 1390D19		CONTRACT NO. 64C24		
	ILLINOIS	FED. AID PROJECT		



USER NAME = rona	DESIGNED - RB	REVISED -
	CHECKED -	REVISED -
PLOT SCALE =	DRAWN - RDA	REVISED -
PLOT DATE = 4/5/2024	CHECKED -	REVISED -

STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION

MODEL: TSI  
FILE NAME: S:\PROJECTS\2019\1390D19\_IDOT\2\DESIGN\STRUCTURE\01 SN 101-2053 - I-39 Over Madigan Creek\CAD SHEETS\ID64C62-1012053\_TSI.dgn



GENERAL PLAN & ELEVATION  
I-39/U.S. 20 OVER MADIGAN CREEK  
SEC. (201-3)R & (4-1,5)R  
WINNEBAGO COUNTY  
STATION 2708+77.50  
STRUCTURE NO. 101-2053



WILLETT HOFMANN  
ASSOCIATES, INC.  
ENGINEERING AND ARCHITECTURAL  
809 EAST 2ND STREET, DECATUR, IL 62521-0387  
TEL: 618-234-3551 FAX: 618-234-0895

USER NAME = rona  
PLOT SCALE =  
PLOT DATE = 4/5/2024

DESIGNED - RB  
CHECKED -  
DRAWN - RDA  
CHECKED -

REVISED -  
REVISED -  
REVISED -  
REVISED -

STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION

DETAILS 2  
STRUCTURE NO. 101-2053

STRUCTURAL SHEET NO. 3 OF 4 SHEETS

F.A.I. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
F.A.I. 39	(201-3)R & (4-1,5)R	WINNEBAGO	3	3
WHA # 1390D19		CONTRACT NO. 64C24		
ILLINOIS		FED. AID PROJECT		

**EXHIBIT D**  
**BORING LOGS**



# SOIL BORING LOG

ROUTE Bypass 20/I-39 DESCRIPTION P-92-111-06 Box Culvert over Madigan Creek on Bypass 20 LOGGED BY W. Garza

SECTION (201-3)K & (4-1,5)R LOCATION Cherry Valley, 2 NW. SEC., TWP. 43N RNG. 2E

COUNTY Winnebago DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME-45 Automatic

STRUCT. NO. Station	DEPTH H	BLOW S	UCS Qu	MOIST T	Surface Water Elev. Stream Bed Elev.	Groundwater Elev.: First Encounter Upon Completion After Hrs.	DEPTH H	BLOW S	UCS Qu	MOIST T
<u>857+18</u>	(ft)	(/6")	(tsf)	(%)	<u>2.50</u> ft <u>4.00</u> ft	<u>735.0</u> ft <u>Wash</u> ft <u>ft</u>	(ft)	(/6")	(tsf)	(%)
SOFT dark gray LOAM					MEDIUM gray SILT with fine SAND lens (continued)	718.5	3 4	0.8 P	19	
	737.5		0.4 P	22	STIFF gray SILTY CLAY TILL					
MEDIUM dark gray SANDY LOAM		2					13			
		2	0.6 P	20			11 8	1.1 P	18	
	735.5					715.5				
MEDIUM tan SAND with medium GRAVEL	▼ -5	5			VERY DENSE tan weathered LIMESTONE		21 25 22			
	733.5	8								
LOOSE/MEDIUM tan SAND										
		5			Wash VERY DENSE tan weathered LIMESTONE		100/5"			
	731.0	6 4				711.0				
Wash LOOSE tan dirty SAND					End of Boring					
	-10	3 4 8					-30			
STIFF tan/gray SILT	728.0									
		6								
	726.0	9 7	1.4 S	21						
MEDIUM gray SILT										
	-15	3 4 6					-35			
	723.5		0.7 B	17						
MEDIUM gray SILT										
		3								
	721.0	4 5	0.6 B	16						
MEDIUM gray SILT with fine SAND lens										
	-20	2					-40			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



# SOIL BORING LOG

ROUTE Bypass 20/I-39 DESCRIPTION P-92-111-06 Box Culvert over Madigan Creek on Bypass 20 LOGGED BY W. Garza

SECTION (201-3)K &(4-1,5)R LOCATION Cherry Valley, 2 NW. SEC., TWP. 43N RNG. 2E

COUNTY Winnebago DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME-45 Automatic

STRUCT. NO. \_\_\_\_\_  
Station 857+18

BORING NO. B-2d  
Station 2707+71  
Offset 175.5 ft RT  
Ground Surface Elev. 737.59 ft

D E P T H  (ft)	B L O W S  (/6")	U C S  (tsf)	M O I S T  (%)	Surface Water Elev. <u>2.50</u> ft	Stream Bed Elev. <u>4.00</u> ft	D E P T H  (ft)	B L O W S  (/6")	U C S  (tsf)	M O I S T  (%)
				Groundwater Elev.: First Encounter <u>733.1</u> ft ▼	Upon Completion <u>Wash</u> ft				
				After _____ Hrs. _____ ft					
MEDIUM dark gray LOAM				MEDIUM gray clean medium coarse SAND (continued)		10			
		0.5	13			12			
735.6		P		716.1					
MEDIUM dark gray dirt SAND & GRAVEL	2			HARD gray LOAM TILL		12			
	13					17	4.6	8	
	10					18	S		
733.6									
STIFF tan SANDY LOAM TILL	2			HARD gray LOAM TILL		11			
	9	1.4	10			18	6.3	8	
	6	P				19	S		
731.6				711.6					
STIFF tan SANDY LOAM TILL	6								
	11	1.0	9						
729.1	15	S		End of Boring					
STIFF tan SANDY LOAM TILL	5								
	7	1.7	8						
	8	S							
726.6									
VERY STIFF gray LOAM TILL	3								
	5	2.7	8						
724.1	9	B							
STIFF gray LOAM TILL	5								
	9	1.8	8						
	11	S							
721.6									
HARD gray LOAM TILL	8								
	10	4.6	8						
	17	S							
718.6									
MEDIUM gray clean medium coarse SAND	4								
-20						-40			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



# SOIL BORING LOG

ROUTE Bypass 20/I-39 DESCRIPTION P-92-111-06- Box Culvert carrying US Bypass 20 over Madigan Creek LOGGED BY W. Garza

SECTION (201-3)K &(4-1,5)R LOCATION Cherry Valley, 2 NW. SEC., TWP. 43N RNG. 2E

COUNTY Winnebago DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME-45 Automatic

STRUCT. NO.	DEPTH	BLOW	UCS	MOIST	Surface Water Elev.	ft	DEPTH	BLOW	UCS	MOIST
Station					Stream Bed Elev.	ft				
BORING NO. <u>B-3</u>					Groundwater Elev.:					
Station <u>2709+25</u>					First Encounter	<u>733.1</u> ft ▼				
Offset <u>14.0 ft LT</u>					Upon Completion	<u>722.6</u> ft ▼				
Ground Surface Elev. <u>762.62</u> ft	(ft)	(/6")	(tsf)	(%)	After <u>    </u> Hrs.	ft	(ft)	(/6")	(tsf)	(%)
MEDIUM gray LOAM			0.8 P	13	DENSE tan FINE SAND (continued)		16			
	760.6	7				740.6	21			
HARD tan SANDY LOAM		7	4.5 P	10	VERY DENSE tan moist SANDY GRAVEL		30			
		9					46			
	758.1					738.1				
VERY STIFF tan SANDY LOAM		9			DENSE tan moist SANDY GRAVEL		13			
		7	2.8 P	9			22			
		5			5' Run		21			
	755.6									
HARD tan SANDY LOAM		7								
		10	4.5 P	14						
		9								
	753.1					733.1 ▼				
HARD tan SANDY LOAM		9			VERY STIFF tan SANDY LOAM TILL top 6" SANDY GRAVEL		18			
		11	4.5 P	10			9	2.3 B	10	
		14			5' Run		8			
	750.6									
HARD tan SANDY LOAM		10								
		8	4.0 P	8						
		8								
	748.1					728.1				
VERY STIFF light brown CLAY LOAM		6			STIFF light gray SANDY LOAM TILL		3			
		6	3.5 B	23			8	1.4 S	26	
		9			5' Run		14			
	745.6									
MEDIUM gray SILTY CLAY LOAM with GRAVEL		4								
		4	0.8 P	23						
		9								
	743.1					723.1				
DENSE tan FINE SAND		15					26			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

Page 2 of 2

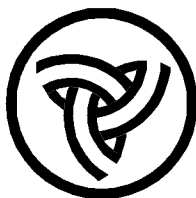
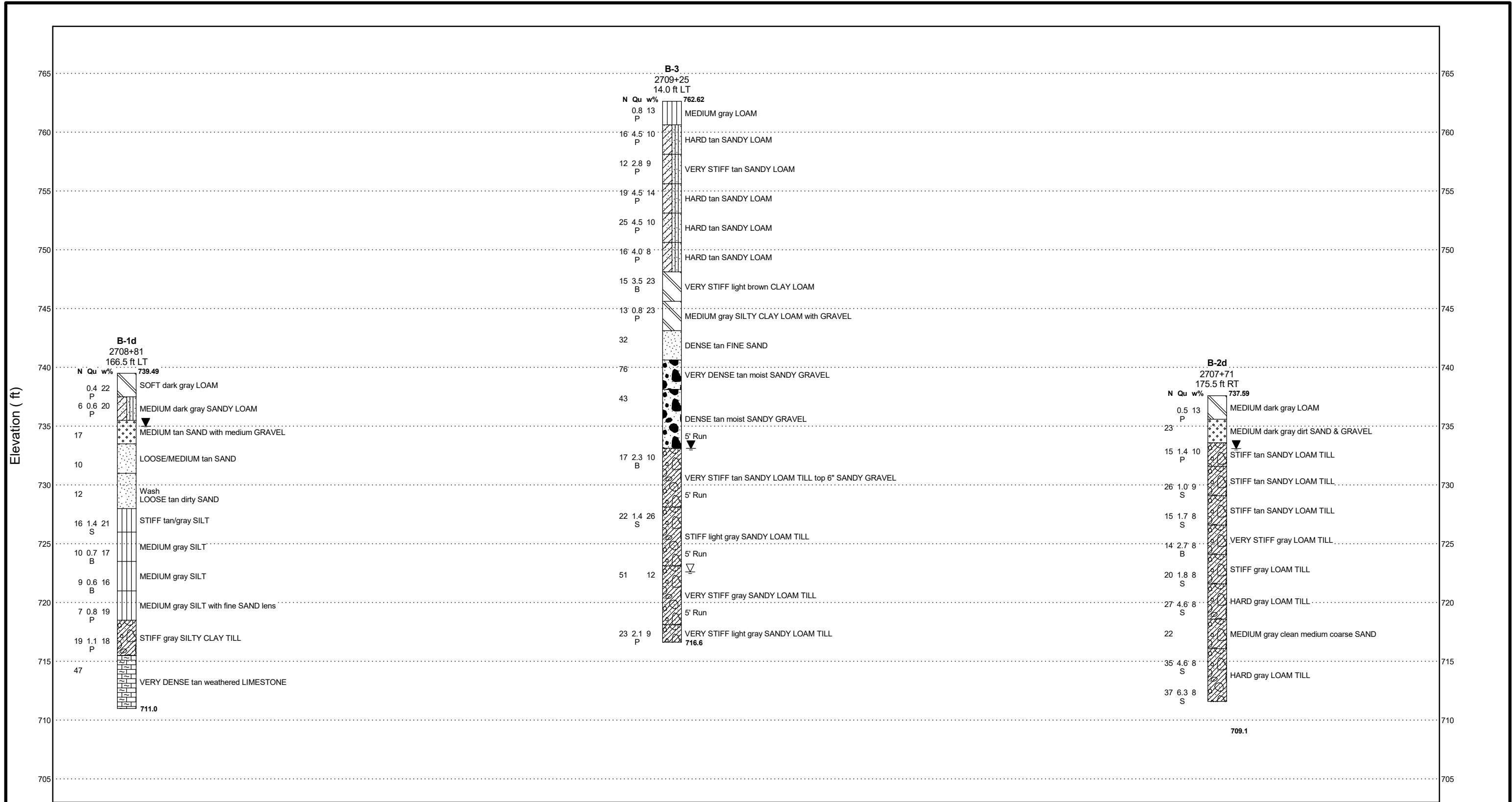
**Date** 8/3/20

**COUNTY** Winnebago **DRILLING METHOD** Hollow Stem Auger **HAMMER TYPE** CME-45 Automatic

STRUCT. NO. _____ Station _____		DEPTH (ft)	BLOWS (/6")	UCS Qu (tsf)	MOIST T (%)	Surface Water Elev. _____ ft Stream Bed Elev. _____ ft	
BORING NO. _____ B-3 Station _____ 2709+25 Offset _____ 14.0 ft LT Ground Surface Elev. _____ 762.62 ft						Groundwater Elev.: First Encounter _____ 733.1 ft ▼ Upon Completion _____ 722.6 ft ▼ After _____ Hrs. _____ ft	
VERY STIFF gray SANDY LOAM TILL			27 24		12		
5' Run (continued)							
718.1 VERY STIFF light gray SANDY LOAM TILL			7 10 13	2.1 P	9		
End of Boring							

BBS, form 137 (Rev. 8-99)

**EXHIBIT E**  
**SUBSURFACE PROFILE**



**Illinois Department  
of Transportation**  
Division of Highways

**NOT TO HORIZONTAL SCALE**

**SUBSURFACE PROFILE**

Route: Bypass 20/I-39  
Section: (201-3)K &(4-1,5)R  
County: Winnebago

## **EXHIBIT F**

### **BEARING RESISTANCE CALCULATIONS**

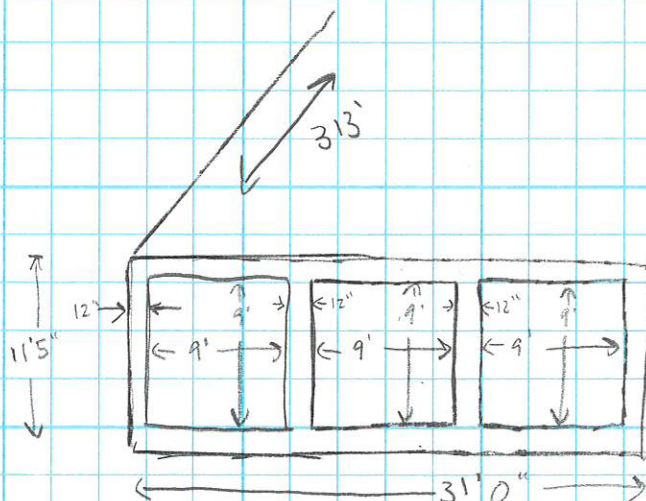
### Weight of Culvert

$$\text{Outer Volume} = (31') (11.4167') (313') \\ = 110,776 \text{ ft}^3$$

$$\text{Inner Volume} = 3 (9') (9') (313') \\ = 76,059 \text{ ft}^3$$

$$\text{Final Volume} = 110,776 - 76,059 \\ = 34,717 \text{ ft}^3$$

$$W_{\text{culvert}} = 34,717 \text{ ft}^3 \cdot 150 \frac{\text{lb}}{\text{ft}^3} \\ = 5,207,586 \text{ lb}$$



### Weight of Fill:

$$V_1 = (215.79') (13.3') (31') + (187.394') (5.74') (31') \\ = 122,315.1 \text{ ft}^3$$

$$V_2 = \frac{1}{2} (57.21') (19.07') (31') \\ = 16,910.4 \text{ ft}^3$$

$$V_3 = \frac{1}{2} (28.396') (5.74') (31') \\ = 2,526.39 \text{ ft}^3$$

$$V_4 = \frac{1}{2} (40') (13.3') (31') \\ = 8,246 \text{ ft}^3$$

$$V_{\text{Fill}} = 122,315.1 + 16,910.4 + 2,526.39 + 8,246 = 149,998 \text{ ft}^3$$

$$W_{\text{Fill}} = 149,998 \text{ ft}^3 \left( \frac{125 \text{ lb}}{\text{ft}^3} \right) = 18,749,737 \text{ lb}$$

### Weight of Wingwalls:

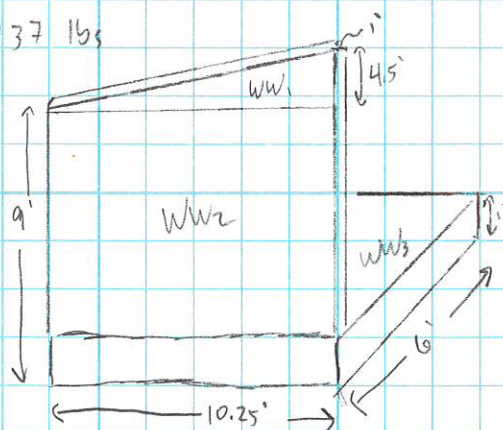
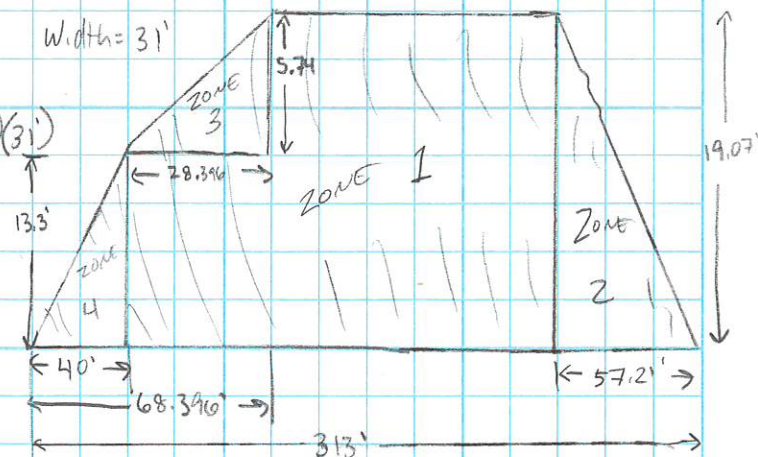
$$V_{\text{WW1}} = 4 \left( \frac{1}{2} (10.25') (4.5') (1) \right) = 92.25 \text{ ft}^3$$

$$V_{\text{WW2}} = 4 \left( \frac{1}{2} (8') (10.25') (1) \right) = 328 \text{ ft}^3$$

$$V_{\text{WW3}} = 4 \left( \frac{1}{2} (10.25') (6') (1) \right) = 246 \text{ ft}^3$$

$$\text{Total } V_{\text{WW}} = 92.25 + 328 + 246 = 666.25 \text{ ft}^3$$

$$\text{Final } W_{\text{WW}} = 666.25 \text{ ft}^3 \left( \frac{150 \text{ lb}}{\text{ft}^3} \right) = 99,938 \text{ lb}$$



Weight of Rock Fill:

$$V_{RF} = (0.5')(313')(31') = 4,851.5 \text{ ft}^3$$

$$W_{RF} = (4,851.5 \text{ ft}^3) \left( \frac{125 \text{ lb}}{\text{ft}^3} \right) = 606,438 \text{ lbs}$$

Weight of everything:

$$W_c = 5,287,586 \text{ lbs}$$

$$W_{fill} = 18,749,737 \text{ lbs}$$

$$W_{sur} = 99,938 \text{ lbs}$$

$$W_{RF} = 606,438 \text{ lbs}$$

$$W_{everything} = 24,743,699 \text{ lbs}$$

BEARING PRESSURE =  $P/A$

$$= \frac{24,743,699 \text{ lbs}}{(31')(313')} = \boxed{2,550 \text{ psf}}$$

BEARING CAPACITY (CONTINUOUS FOUNDATION - TERZAGHI)

$$q_{ult} = c' \bar{N}_c + \bar{\sigma}_{20}' \bar{N}_q + 0.5 \gamma' B \bar{N}_{\gamma}$$

$$q_{ult} = 0 + (62.6 \text{ pcf})(3.0')(61.5) + (0.5)(62.6 \text{ pcf})(31')(82.3)$$

$$q_{ult} = \boxed{91,405.4 \text{ psf}}$$

$$q_{allowable} = \frac{q_{ult}}{FOS} = \frac{91,405}{2} = \boxed{45,703 \text{ psf}}$$

$$q_{allowable} = 45,703 \text{ psf} > 2,550 \text{ psf}$$

**OK**

Bearing on sandy gravel:  
Elevation: 733.04 ft

$$c' = 0$$

$$\phi = 38^\circ$$

$$\gamma' = 125 \text{ pcf} - 62.4 = 62.6 \text{ pcf}$$

$$D_f = 3 \text{ ft}$$

$$B = 31 \text{ ft}$$

$$N_c = 77.5$$

$$N_q = 61.5$$

$$N_\gamma = 82.3$$

$$D = 3 \text{ ft}$$



208 E. Main Street  
Suite 100  
Belleville, Illinois 62220  
618.233.5877 phone  
618.233.5977 fax  
www.kaskaskiaeng.com

Project Title: Madison Creek Culvert Sheet: 3 of 3  
Project Number: 19-1138100  
Calculated By: CO Date: 4/1/24  
Checked By: \_\_\_\_\_ Date: \_\_\_\_\_  
Comments: \_\_\_\_\_

### SLIDING BEARING RESISTANCE

Sliding Bearing Resistance =  $\frac{1}{2} \sigma_v$  or cohesion  
Use lesser of two values

$$\frac{1}{2} \sigma_v = \frac{1}{2} (125 \text{ pcf})(3') = \boxed{187.5 \text{ psf}}$$

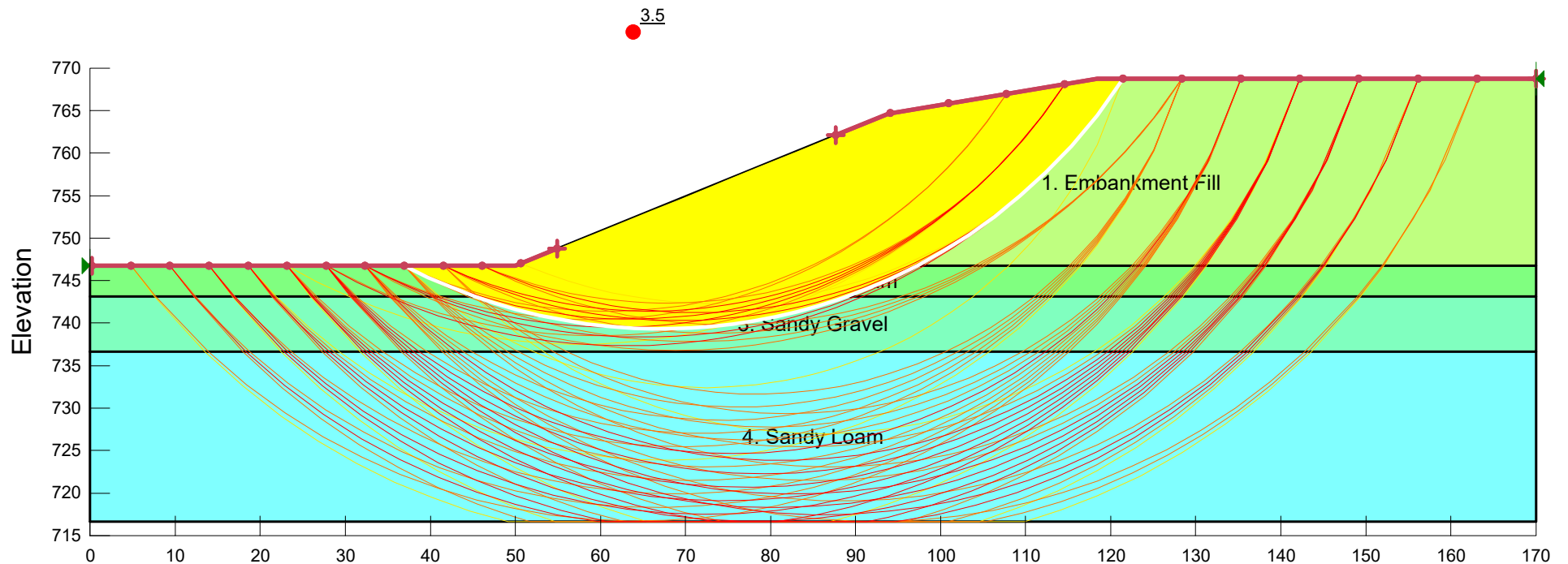
**EXHIBIT G**  
**SETTLEMENT CALCULATIONS**

Settlement Calculations - I-39 over Madigan Creek															
<div> <div>P (lb)=5541092</div> <div>γ (pcf)=125</div> <div>t (years)=50</div> </div>				<div> <div>D(ft)=3</div> <div>B (ft)=31</div> <div>L (ft)=71.484375</div> </div>				<div> <div>q (psf)=2500.475</div> <div>lep=0.574</div> <div>σzp (psf)=4250</div> <div>σzd (psf)=375</div> </div>				<div> <div>Correction Factor</div> <div>C1=0.912</div> <div>C2=1.540</div> <div>C3=0.961</div> </div>			
Layer	Soil Description	Soil Type	H (ft)	γ (pcf)	N	N60	zcl (ft)	βo (ksf)	β1 (ksf)	Es (psf)	p'o (psf)	les	lec	le	leh*H/Es
1	Sandy Loam Till	2	2.76	125	17	19	1.38	50	12	278000	172.50	0.142	0.217	0.153	1.52E-06
2	Sandy Loam Till	2	5	125	22	25	5.26	50	12	350000	657.50	0.261	0.263	0.261	3.73E-06
3	Sandy Loam Till	2	5	125	51	59	10.26	50	12	758000	1282.50	0.414	0.324	0.401	2.64E-06
4	Sandy Loam Till	2	5	125	23	26	15.26	50	12	362000	1907.50	0.567	0.384	0.540	7.46E-06
5															
6															
7															
8															
9															
10															
<div> <div>Soil Type: 1. Clean Sands (SW and SP)</div> <div>2. Silty Sands and Clayey Sands (SM and SC)</div> </div>												<div> <div>Σ=1.54E-05</div> <div>δ (ft)=4.40E-02</div> <div>δ (in)=0.5283245</div> </div>			
$\delta = C_1 C_2 C_3 (q - \sigma'_{zD}) \sum \frac{I_e H}{E_s}$															

## **EXHIBIT H**

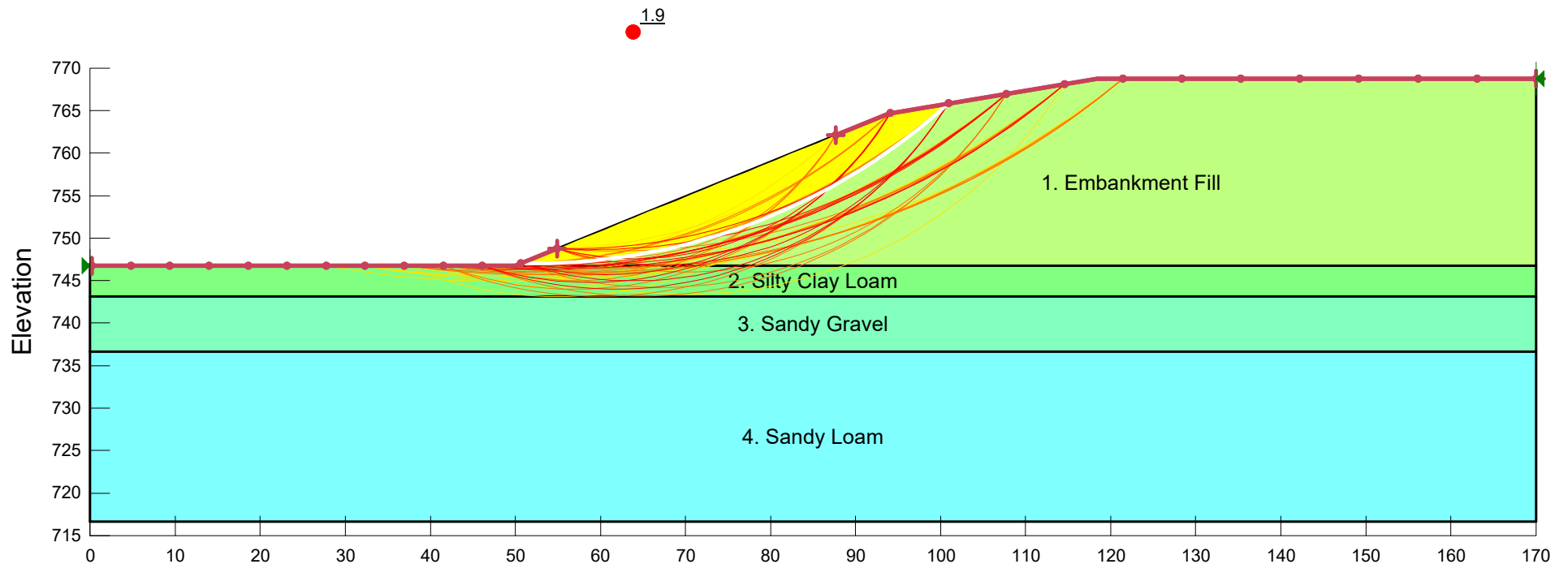
### **SLOPE/W SLOPE STABILITY ANALYSIS**

**I-39 over Madigan Creek Boring  
B-3 - Upstream End  
End-of-Construction  
(Undrained Analysis)**



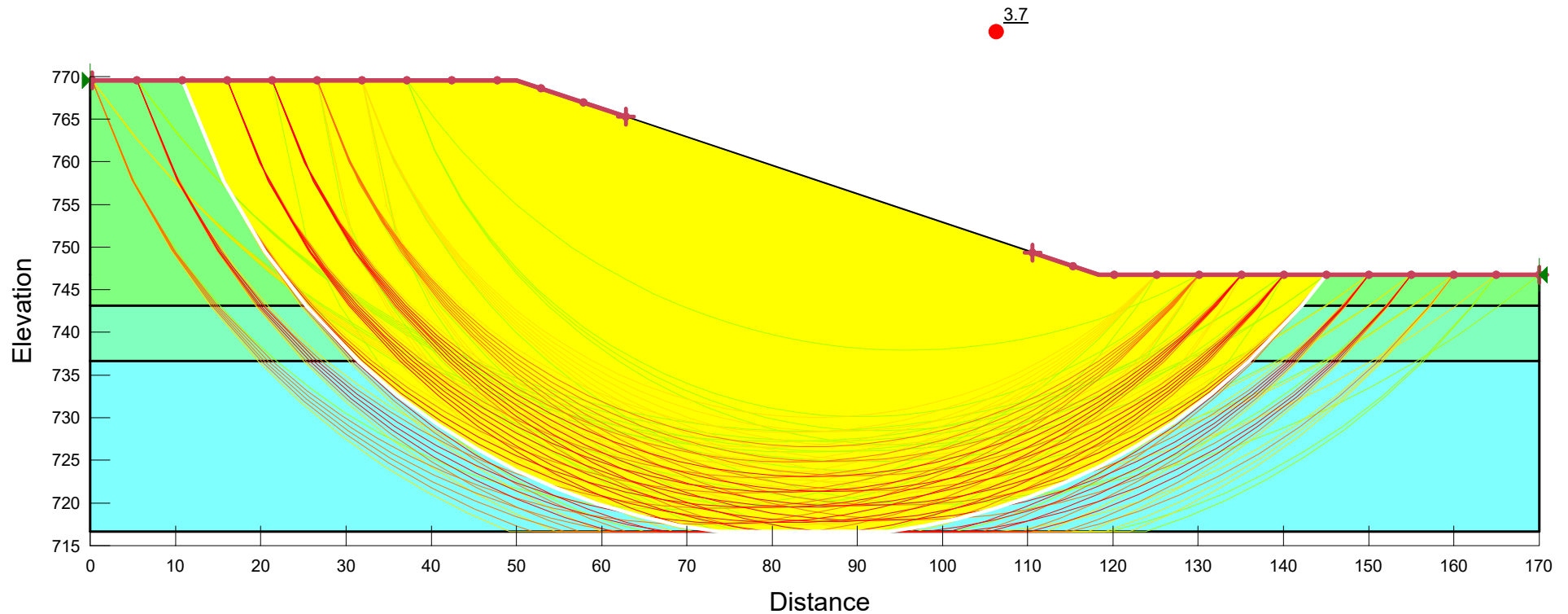
Color	Name	Slope Stability Material Model	Unit Weight (pcf)	Effective Cohesion (psf)	Effective Friction Angle (°)	Phi-B (°)
<span style="display:inline-block; width:15px; height:15px; background-color:yellow;"></span>	1. Embankment Fill	Mohr-Coulomb	125	1,000	0	0
<span style="display:inline-block; width:15px; height:15px; background-color:lightgreen;"></span>	2. Silty Clay Loam	Mohr-Coulomb	120	800	28	0
<span style="display:inline-block; width:15px; height:15px; background-color:mediumseagreen;"></span>	3. Sandy Gravel	Mohr-Coulomb	120	0	38	0
<span style="display:inline-block; width:15px; height:15px; background-color:cyan;"></span>	4. Sandy Loam	Mohr-Coulomb	120	1,750	0	0

**I-39 over Madigan Creek  
Boring B-3 - Upstream End  
Long Term (Drained Analysis)**



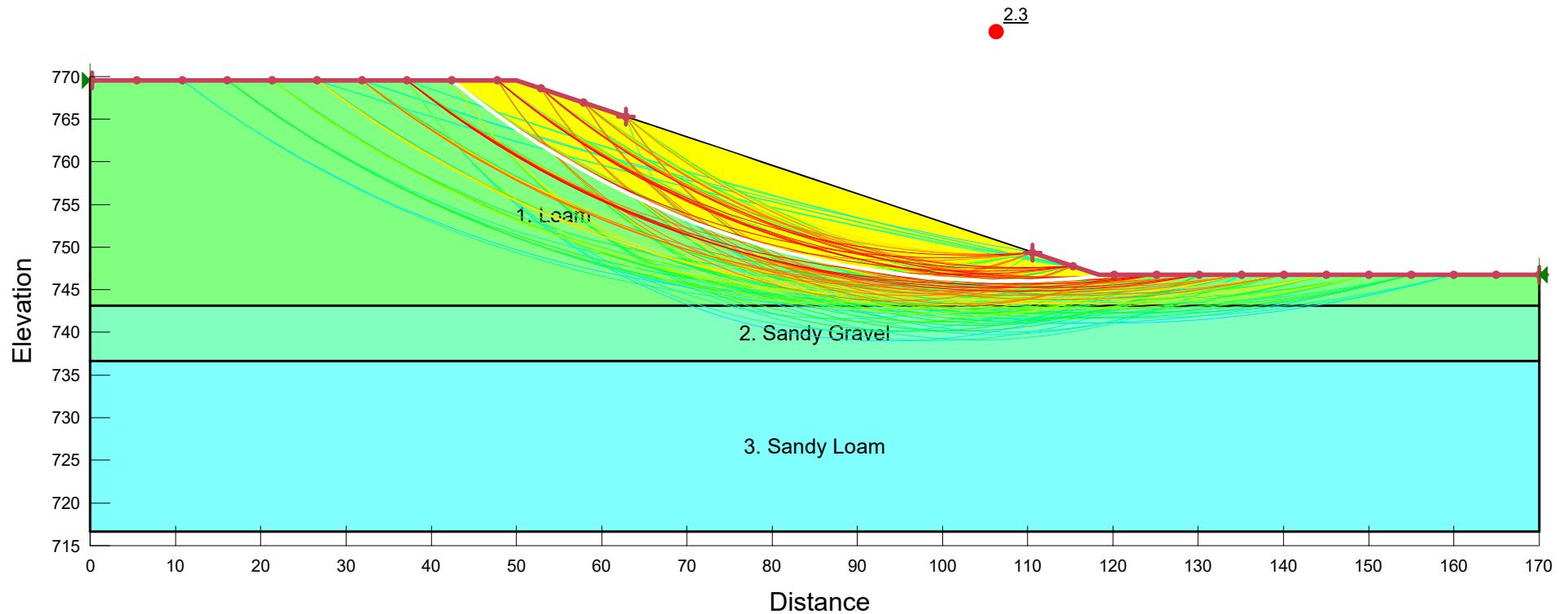
Color	Name	Slope Stability Material Model	Unit Weight (pcf)	Effective Cohesion (psf)	Effective Friction Angle (°)	Phi-B (°)
<span style="display:inline-block; width:15px; height:15px; background-color:yellow;"></span>	1. Embankment Fill	Mohr-Coulomb	125	100	26	0
<span style="display:inline-block; width:15px; height:15px; background-color:lightgreen;"></span>	2. Silty Clay Loam	Mohr-Coulomb	120	100	28	0
<span style="display:inline-block; width:15px; height:15px; background-color:mediumseagreen;"></span>	3. Sandy Gravel	Mohr-Coulomb	120	0	38	0
<span style="display:inline-block; width:15px; height:15px; background-color:cyan;"></span>	4. Sandy Loam	Mohr-Coulomb	120	0	30	0

**I-39 over Madigan Creek Boring  
B-3 - Downstream End  
End-of-Construction  
(Undrained Analysis)**



Color	Name	Slope Stability Material Model	Unit Weight (pcf)	Effective Cohesion (psf)	Effective Friction Angle (°)	Phi-B (°)
<span style="color: green;">■</span>	1. Loam	Mohr-Coulomb	120	800	28	0
<span style="color: yellow;">■</span>	2. Sandy Gravel	Mohr-Coulomb	120	0	38	0
<span style="color: cyan;">■</span>	3. Sandy Loam	Mohr-Coulomb	120	1,750	0	0

**I-39 over Madigan Creek  
Boring B-3 - Downstream End  
Long Term (Drained Analysis)**



Color	Name	Slope Stability Material Model	Unit Weight (pcf)	Effective Cohesion (psf)	Effective Friction Angle (°)	Phi-B (°)
<span style="color: green;">■</span>	1. Loam	Mohr-Coulomb	120	100	28	0
<span style="color: lightgreen;">■</span>	2. Sandy Gravel	Mohr-Coulomb	120	0	38	0
<span style="color: cyan;">■</span>	3. Sandy Loam	Mohr-Coulomb	120	0	30	0