Prepared for:

Illinois Department of Transportation, District 2 819 Depot Avenue Dixon, Illinois 61021

Structure Designer:

Infrastructure Engineering, Inc. 33 West Monroe , Suite 1540 Chicago, Illinois 60603 (312) 425-9560

Prepared By:

Hanson Professional Services Inc. 13801 Riverport Drive, Suite 300 Maryland Heights, Missouri 63043 (314) 770-0467

kchepkoit@hanson-inc.com

Abbreviated Structure Geotechnical Report

F.A.I. Rte. 39 (I-39) Section (4-1, 5)R Winnebago County Job No. P-92-111-06 Contract No. 64C24 PTB No. 141-004 I-39/US 20 over Canadian National Railroad. Structure Nos. 101-0208 (EB) & 101-0209 (WB) Ex. Structure Nos. 101-0067 (EB) & 101-0068 (WB)

> Submitted February 2017 Revised March 2017



Original Report Date: 2/16/2017	Proposed SN:	101-0208/0209	Route:	FAI 39 (I-39)
Revised Date: 3/28/2017	Existing SN:	101-0067/0068	Section:	(4-1,5)R
Geotechnical Engineer: Kipkoech Che	County:	Winnebago		
Structural Engineer: Infrastructure En	ngineering, Inc.		Contract:	64C24

Indicate the proposed structure type, substructure types, and foundation locations (attach plan and elevation drawing):

The new structures will be three-span steel wide-flange bridges. The substructures will consist of pile-supported integral abutments and multiple column piers with crash walls and pile-supported footings. S.N. 101-0208 will replace existing S.N. 101-0067, which is the bridge carrying the eastbound traffic, and S.N. 101-0209 will replace existing S.N. 101-0068, which is the bridge carrying the westbound traffic. According to information provided by the structure designer, the estimated vertical factored substructure loads are 1,470 to 1,610 kips at the abutments and 3,810 to 3,750 kips at the piers. The general plan and elevation drawing for the new structures is attached.

Discuss the existing boring data, existing plans foundation information, new subsurface exploration and need for any additional exploration to be provided with SGR Technical Memo (attach all data and subsurface profile plot):

Underground coal mine information available from ISGS indicates that the project area has not been undermined.

Existing structure plans show the current structures are three span bridges. The substructures are pile-supported stub abutments and hammerhead piers with pile-supported footings. The existing structures were constructed in 1962 and rehabbed in the early 1990's, including deck replacement and substructure widening. The abutments are supported by metal shell and H-piles, and the piers are supported by treated timber piles and H-piles. Pile driving records from the original construction confirm that the existing piles are tipped either on bedrock or within glacial soils a few feet above bedrock. The existing piles were driven to consistent lengths at each substructure unit, except for the south abutment of the westbound bridge. The piles on the west side of the bridge drove up to 11 feet shorter than the piles on the east side of the bridge.

Topographic survey and aerial photographs indicate minor to moderate sloughing of the embankment side slopes at the north abutment. There is a small distressed area above the headwall to the twin 84-inch pipe culverts on the west side, and a much larger distressed area covering the entire height of the embankment of the east side. The area on the east side is above the culvert junction chambers. These areas do not appear to be deep-seated global geotechnical failures.

Four boring logs were provided to Hanson Professional Services Inc. (Hanson) by IDOT for Borings B-1h through B-4h, which were drilled in June 2008 according to the dates on the logs. The surficial soils in the borings generally consisted of silty clay loam with occasional loam, clay loam, sandy loam, and sand layers overlying approximately 5 feet of glacial till. In Borings B-4h and B-3h, which were located at the South Abutment, these soils extended to approximately El. 760 and were underlain by weathered rock and dolomite bedrock to the end of the boring. In Borings B-1h and B-2h, which were located at the North Abutment, these soils extended to approximately El. 747/746 and were underlain by weathered rock and dolomite bedrock to the boring. The bedrock in Borings B-4h, B-1h, and B-3h was cored for observation and testing.

Locations of the borings are shown on the attached Boring Location Plan. Stations and offsets on the boring logs are relative to the existing US 20 alignment. Boring locations along the current I-39 alignment are shown on the attached Subsurface Data Profile.

Provide the location and maximum height of any new soil fill or magnitude of footing bearing pressure. Estimate the amount and time of the expected settlement. Indicate if further testing, analysis, and/or ground improvement/treatment is necessary:

Both structures will require fill to accommodate widening beyond their current footprint. The height of the new embankment fill at the North Abutment is generally 2 to 4 feet above the existing pavement. Maximum fill is 16 feet at the right edge of new eastbound pavement. The maximum estimated magnitude of settlement that will occur due to this fill is approximately 0.25 inch.

The height of the new embankment fill at the South Abutment is generally 4 to 6 feet above the existing pavement. Maximum fill is 15 feet at the right edge of new eastbound pavement. The magnitude of settlement at the South Abutment is estimated to be less than at the North Abutment.

The estimated magnitude of settlement is acceptable for the proposed structures.

Identify any new cuts or fill slope angles and heights. Estimate the factor of safety against slope failure. Indicate if further testing, analysis or ground improvement/treatment is necessary:

The proposed construction will raise the existing embankment by 2 to 6 feet and widen the existing embankment footprint by approximately 25 feet on each side. The maximum heights of the new embankment are 46 feet along the right side of the south approach and 41 feet along the left side of the north approach. All slopes will be 1V:2H, which is the existing condition. Most of the new fill will be placed on the side slopes of the existing embankment. The proposed end slopes will require minimal regrading.

The worst-case global stability condition is located at the left side of the north approach and the right side of south approach due to the significantly weaker soils encountered in Boring B-2h. A slope stability analysis was completed of the left side slope at Sta. 2649+32 for north abutment and right side slope at Sta 2647+25 for south abutment. The global factor of safety of north and south abutments is 1.59 and 1.56, respectively. The global stability factor of safety meets IDOT and AASHTO requirements, and ground improvement/treatment is not necessary. A plot of the global stability analysis results is attached. Note soil profile from boring B-2h (located at the north abutment) was used in global stability analysis for south abutment because boring B-4h exhibited much better/stronger soil profile.

Indicate at each substructure, the 100-year and 200-year total scour depths in the Hydraulics report, the nongranular scour depth reduction, the proposed ground surface, and the recommended foundation design scour elevations:

N/A

Determine the seismic soil site class, the seismic performance zone, the 0.2 and 1.0 second design spectral accelerations and indicate if that the soils are liquefiable:

The seismic Site Class is C, the SPZ is 1, S_{DS} = 0.101g, and S_{D1} = 0.056g. The soils are not considered to be liquefiable for the design earthquake.

Confirm feasibility of the proposed foundation or wall type and provide design parameters. Attach a pile design table indicating feasible pile types, various nominal required bearings, factored resistances available and corresponding estimated lengths at locations where piles will be used. Provide factored bearing resistance and unit sliding resistance at various elevations and confirm no ground improvement/treatment is necessary where spread footings are proposed. Estimated top of rock elevations as well as preliminary factored unit side and tip resistance values shall be indicated when drilled shafts are proposed:

A Pile Design Table including data for several pile sizes at each substructure is attached. Steel H-piles that extend to bedrock are recommended based upon the relatively shallow bedrock encountered at the boring locations. Pile lengths were estimated for Pier 1 based on the pile driving records for the adjacent existing pier. Calculations based on Boring B-3h indicate that the pile length would be significantly shorter. It is assumed that there is significant rise in the bedrock towards the southwest corner of the site. Piles on the west side of the South Abutment and Pier 1 may reach refusal 10 feet or more above the estimated tip elevations.

Metal shell (MS) piles do not appear feasible based on the close proximity to top of rock and the risk of damaging the piles.

Shoes are required for all piles. A total of two test piles should be specified for these bridges. These test piles should be located at the South Abutment and Pier 2, both within the first phase of construction.

Calculate the estimated water surface elevation and determine the need for cofferdams (type 1 or 2), and seal coat:

N/A

Assess the need for sheeting or soil retention or temporary construction slope and provide recommendation for other construction concerns:

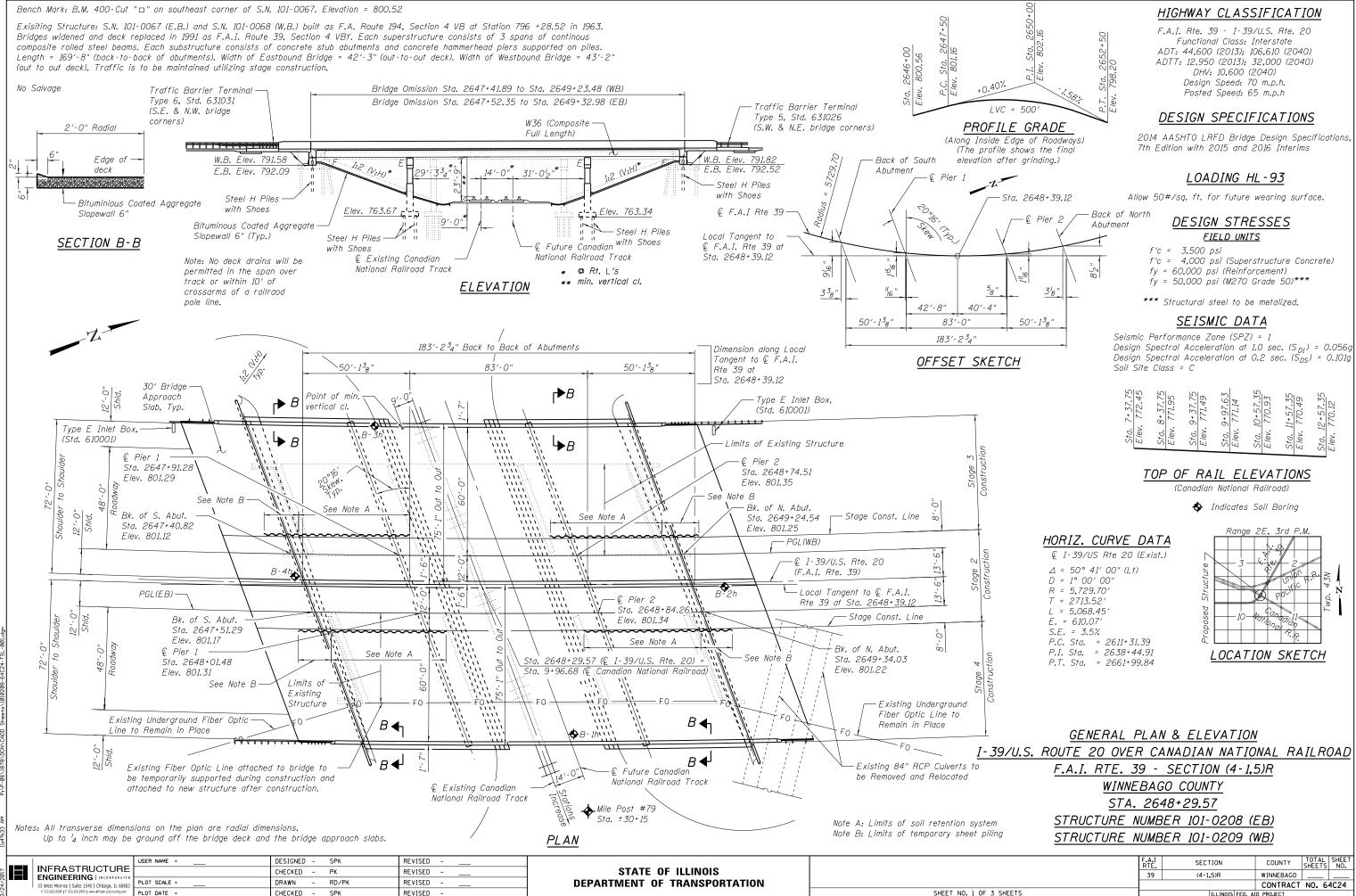
The proposed structures will be staged to maintain traffic on I-39 during construction. Temporary excavations with up to 10 feet retained height will be required to construct the abutments near active traffic lanes. There is not enough room to lay back temporary slopes perpendicular to traffic. Temporary sheet piling, designed in accordance with IDOT Design Guide 3.13.1 – Temporary Sheet Piling Design, is feasible within the existing embankments at the abutments.

Temporary excavations for the proposed piers will be located within the existing end slopes and will be up to 17 feet below existing ground. The proposed pier footings are located far enough from the existing and proposed abutments that temporary slopes flatter than 1V:1H may be excavated without undercutting the abutments. It should be possible for the contractor to configure temporary excavations that meet OSHA requirements. If it is desired to limit the footprint of temporary excavations within the end slope, a temporary soil retention system would be required. Temporary sheet piling is not feasible at the piers due to shallow bedrock.

Structure Nos. 101-0208 (EB) & 101-0209 (WB) Pile Design Parameters

	Cutoff Elevation		Factored Resistance Available,	Geotechnical Losses,	Nominal Required Bearing,	Estimated Pile Length
Location	(ft)	Pile Type	R _F (kips)	R _{Sdd} (kips)	R _N (kips)	(ft)
		HP 10x42	184	0	335	41
South		HP 12x53	230	0	418	41
Abutment	794.1	HP 12x63	273	0	497	42
B-4h	777.1	HP 12x74	324	0	589	42
D-411		HP 14x73	318	0	578	42
		HP 14x89	388	0	705	42
		HP 10x42	184	0	335	19
Dian 1		HP 12x53	230	0	418	19
Pier 1	765.7	HP 12x63	273	0	497	19
B-3h *	/03./	HP 12x74	324	0	589	20
D-311		HP 14x73	318	0	578	20
		HP 14x89	388	0	705	20
		HP 10x42	184	0	335	23
D' 2		HP 12x53	230	0	418	24
Pier 2	765.3	HP 12x63	273	0	497	24
B-1h	/03.3	HP 12x74	324	0	589	25
D-111		HP 14x73	318	0	578	24
		HP 14x89	388	0	705	25
		HP 10x42	184	0	335	52
		HP 12x53	230	0	418	53
North	704 5	HP 12x63	273	0	497	53
Abutment B-2h	794.5	HP 12x74	324	0	589	54
D-211		HP 14x73	318	0	578	53
		HP 14x89	388	0	705	54

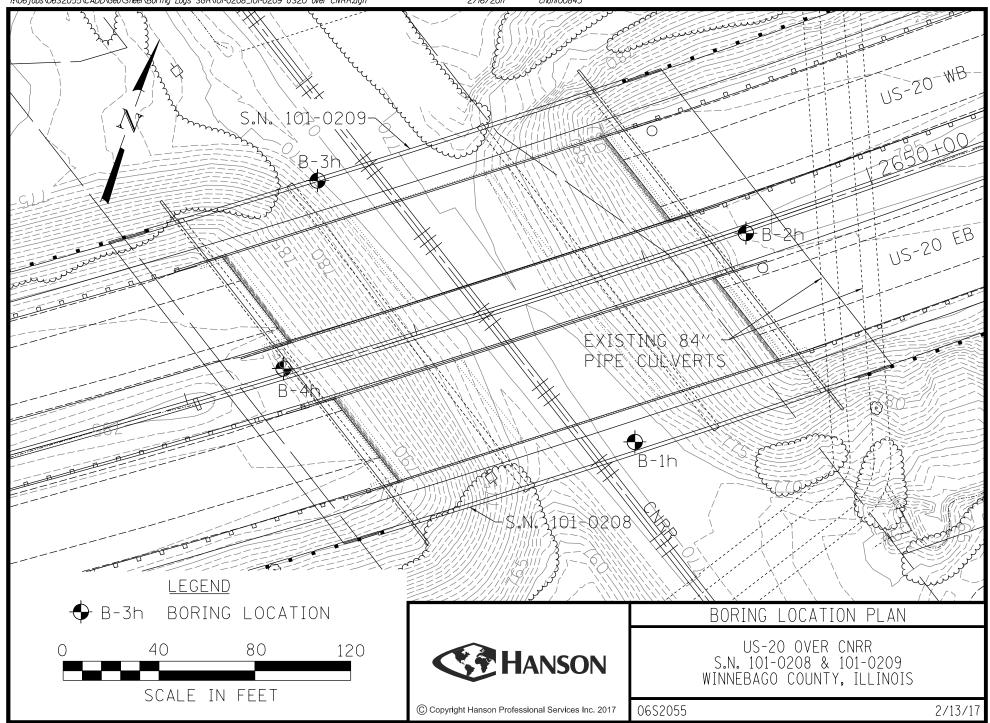
* Note: Pile driving records from existing structure were also considered at Pier 1. Existing timber piles have tips at Elev. 747 to $751\pm$.



Sta	<i>Sta.</i> 7+37.75	<i>Sta.</i> 8+37.75	Sta. 9+37.75	Sta. 9+97.63	Sta. 10+57.35	<u>Sta. 11+57.35</u>	<u>Sta. 12+57.35</u>
Elevent	<i>Elev.</i> 772.45	Elev. 771.95	Elev. 771.49	Elev. 771.14	Elev. 770.93	Elev. 770.49	Flav 770.12

<u>HORIZ. CURVE DATA</u>
€ I-39/US Rte 20 (Exist.)
$\begin{array}{l} \Delta = 50^{\circ} 41' \ 00'' \ (Lt) \\ D = 1^{\circ} \ 00' \ 00'' \\ R = 5,729,70' \\ T = 2713.52' \\ L = 5,068.45' \\ E. = 610.07' \\ S.E. = 3.5' \\ P.C. \ Sta. = 2611+31.39 \\ P.I. \ Sta. = 2638+44.91 \\ P.T. \ Sta. = 2661+99.84 \end{array}$

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Proposed				.,	na	10, R,	ρ" 9.	1 th		
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I:\06jobs\06S2055\CADD\Geo\Sheet\Boring Logs SGR\0I-0208_I0I-0209 US20 over CNRR.dgn

2/16/2017 chant00843

B-4h Sta. 2647+43, 3' LT 70.0 N Qu 71 0.5P 72 0.5P 737.0 N 7 0.5P 7 0.5P 7 1.2B 9 1.2B 9 1.9S 9 1.9S 10 1.8B 20.0 STIFF 12 2.5B 21.0 VERY STIFF 12 2.3B 20.0 VERY STIFF 12 1.4D 13 14D		B-2h Sta. 2649+44, 2' RT 795.1 N Qu wX 1.8P 11.0 STIFF dark brown LOAM 6 0.8P 16.0 MEDIUM gray SANDY LOAM 6 0.6P 22.0 SAND lens 9 0.9B 17.0 MEDIUM gray SANDY LOAM 11 1.1S 10.0 STIFF gray SANDY LOAM 12 0.9B 23.0 VERY STIFF gray/tan SILTY CLAY LOAM
131.4P14.0STIFF gray SILTY CLAY LOAM247.0MEDIUM tan SANDY LOAM72132.9B21.0VERY STIFF gray/brown SILTY CLAY LOAM151.8B16.0STIFF brown LOAM203.7B17.0LOAM lens172.5P18.0VERY STIFF gray CLAY LOAM TILL123.513.0VERY STIFF brown LOAM TILL123.513.0VERY STIFF brown LOAM TILL122.5P18.0VERY STIFF brown LOAM TILL760.027MEDIUM tan weathered LIMESTONE757.024MEDIUM tan weathered LIMESTONE753.5100/4"Auger Refusal at 43.5'753.5Dolomite: yellow tan buff, vuggy and pitted, very finely crystalline, chalky with washed out sand size particles and fractured throughout.748.5193Dolomite: as above t.s.f.: 745.1 to 744.6743.5ROD = 0%24%743.5Abandoned run - problems with water	769.8 N OU WX 769.8 0.5P 24.0 MEDIUM dark brown SILTY CLAY LOAM 769.8 7 1.5P 18.0 STIFF brown CLAY LOAM 19 1.1P 12.0 STIFF tan SANDY LOAM 20 1.8P 11.0 STIFF tan SANDY LOAM 760.3 100/5" VERY DENSE tan weathered LIMESTONE 100/5" VERY DENSE tan weathered LIMESTONE 100/2" Auger Refusal at 14' 755.8 97 Dolomite: yellow tan-buff, vuggy and pitted, rouge foot contains one-inch segments. 1.5.f.: 751.8 to 751.2 750.8 87 Rec. = 100% Net and y inclusions. 747.1 745.8 184 Rec. = 100% ROD = 62% Dolomite: as above, less pitted. 743.5	B-Ih 648+73. 70' RT 59.2 <u>N Qu wZ</u> 0.5P 14.0 MEDIUM dark brown LOAM 5 1.0P 13.0 MEDIUM/STIFF brown LOAM 4 1.1B 18.0 STIFF brown LOAM with SAND lens 4 0.2P 21.0 VERY SOFT brown SILTY CLAY LOAM 2 VERY STIFF brown SILTY CLAY LOAM 3 0.9B 19.0 MEDIUM dark gray LOAM with SAND lens 13 0.9B 19.0 MEDIUM dark gray LOAM
$Bottom of Hole = 58.5 feet$ $\frac{LEGEND}{N Standard \ Penetration \ Test \ N \ (blows/ft)}$ $Ou Unconfined \ Strength \ (tsf)$ $w'. \ Natural \ Moisture \ Content \ (%)$ $DD \forall \ Mater \ Surface \ Elevation \ Encountered \ in \ Boring \ DD \ = \ during \ drilling \ Dh \ = \ dr \ completion \ 24h \ = \ 24 \ hours \ after \ completion$ $Approximate \ Finish \ Grade \ Bottom \ of \ Footing$	733 728	according the stable is a base with fractured zone at 736.2. No testable segments. Baccording Rec. = 100% ROD = 10% ROD = 10% ROD = 10% ROD = 10% Bottom for Hole is a base, though medium to massively bedded. n.s.f.: 732.3 to 731.8 Rec. = 100% ROD = 58% Bottom of Hole = 41.0 feet
FILE NAME = DESIGNED - RCC USER NAME = DESIGNED - RCC PLOT SCALE = DRAWN - EJM PLOT SCALE = DRAWN - EJM	REVISED STATE OF ILLINOIS REVISED DEPARTMENT OF TRANSPOR REVISED DEPARTMENT OF TRANSPOR	

P9: TION D U C S Qu (tsf) P	2111- <u>Cherr</u> <u>Hc</u> M O I S T (%) 14.0 13.0	Groundwater Elev.: First Encounter 754.2 ft Y Upon Completion ft After Hrs. ft (ff MEDIUM tan LOAM TILL with SAND lens 747.20 VERY DENSE tan weathered LIMESTONE 745.20	2E 3 Diedr B L O W	Y <u>M</u> ich A U C S Qu
TION D U C S Qu (tsf) P 1.0 P 0.8	Cherr Hc 0 1 5 T (%) 14.0	Y Valley Twp 10 NE, SEC., TWP. 43N, RNG. Sullow Stem Auger HAMMER TYPE B-5 Surface Water Elev. ft Stream Bed Elev. 72.50 Groundwater Elev.: First Encounter Pirst Encounter 754.2 Upon Completion ft After Hrs. MEDIUM tan LOAM TILL with SAND lens 747.20 VERY DENSE tan weathered LIMESTONE 745.20	2E 3 Diedr 3 Diedr 4 C 5 C 6 C 7 W 1 S 1 S 12 13 20	ich A C S Qu (ts
TION D U C S Qu (tsf) P 1.0 P 0.8	Cherr Hc 0 1 5 T (%) 14.0	Y Valley Twp 10 NE, SEC., TWP. 43N, RNG. Sullow Stem Auger HAMMER TYPE B-5 Surface Water Elev. ft Stream Bed Elev. 72.50 Groundwater Elev.: First Encounter Pirst Encounter 754.2 Upon Completion ft After Hrs. MEDIUM tan LOAM TILL with SAND lens 747.20 VERY DENSE tan weathered LIMESTONE 745.20	2E 3 Diedr 3 Diedr 4 C 5 C 6 C 7 W 1 S 1 S 12 13 20	ich A C S Q (ts
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U C S Qu (tsf) P 1.0 P 0.8	M O I S T (%) 14.0	Surface Water Elev. ft ft Stream Bed Elev. 72.50 ft Groundwater Elev.: T First Encounter 754.2 ft Upon Completion ft ft After Hrs. ft MEDIUM tan LOAM TILL with 747.20 VERY DENSE tan weathered 745.20 LIMESTONE 745.20	B L O W S (/6") 2 3 12 13 20	U C S Q (ts 0.0
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1.0 P 0.8		VERY DENSE tan weathered	13 20	B
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The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer) The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206) BBS, from 137 (Rev. 8-99)

Illinois Depa of Transport	rtment tation RO	ск сс	RELC	DG	Ì	F	age <u>1</u>	of <u>1</u>
Division of Highways Illinios Department of Transport		Bridge over the	CC&P RR3	m W	J		Date	
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SECTION(201-3), K (4-1, 5) K				P. 43	N, RN	G . 2E		T
COUNTY Winnebago CORI	NG METHOD				R	R	CORE	S T
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	Core Diameter Top of Rock Elev74 Begin Core Elev74	2 in	E P T H	O R	V E R Y	Q D	l M E (min/ft)	E N G T H
Dolomite: yellow tan-buff, vuggy and p inclusions.		o chert	743.20	(#)	100	(70)	(min/n)	(tsf) 287.0
Dolomite: as above with fractured zone	۰ ۰						-	207.0
Dolomite: as above, though medium to				2	100	10	3.2	
t.s.f.: 732.3 to 731.8	massively bedded.		-40	3	100	58	2	200.0
End of Boring								

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Color pictures of the cores ______ Cores will be stored for examination until______ The "Strength" column represents the uniaxial compressive strength of the core sample (ASTM D-2938)

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Division of Highways Illinios Department of Tran	sportation/[9-2				6 Bridge over the CC&P RR, .3 m. of Perryville Road	-	000	Date	
						/ Valley Twp 10 NE, SEC., TWP.				' <u>'</u>
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STRUCT. NO Station		n	B L O	11	M O	Surface Water Elev Stream Bed Elev72.50	ft	DE	BL	
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Ground Surface Elev. 795.10 STIFF dark brown LOAM) ft	(ft)	(/6")	(tsf)	(%)	Upon Completion After Hrs	ft		(/6'')	(ts
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	786.10	-10	6	В			766.10	-30	5	8
STIFF gray SANDY LOAM	783.60		5 5 6	1.1 S	10.0	SOFT gray SILTY LOAM	763.60		2 1 6	0. P
SOFT gray LOAM with SAND lens	-		2			MEDIUM gray SANDY LOAM	. 55.00		6	
	- 781.10		2 3	0.4 B	23.0		761.10		8 10	0. B
VERY STIFF gray/tan SILTY CLAY LOAM	-	-15	3	2.7	20.0	STIFF gray LOAM with SAND lens		35	3	
	778.60		5 6	2.7 B	20.0		758.60		9 10	1. P
MEDIUM gray/brown SILTY CLAY LOAM			4	0.9	24.0	MEDIUM dark gray LOAM			4	0.
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The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer) The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206) BBS, from 137 (Rev. 8-99)

Illinois De	part	me	ent				Page <u>2</u> of <u>2</u>
V V / of Iransp	ortaf	ioi	n		S(DIL BORING LOG	
Division of Highways Illinios Department of Train ROUTE FAP 301			IPTIO	P92 N	2-111-(06 Bridge over the CC&P RR, .3 m. W. of Perryville Road LOG	Date <u>6/17/08</u> GED BY W. Garza
						/ Valley Twp 10 NE, SEC., TWP. 43N, RNG.	
						low Stem Auger HAMMER TYPE B-5	
STRUCT. NO Station		D E P	0	U C S	M O I	Surface Water Elev ft Stream Bed Elev72.50 ft	
BORING NO. B-2h Station 797+33 Offset 2.00ft Rt CL Ground Surface Elev. 795.10		T H (ft)	S	Qu (tsf)		Groundwater Elev.: First Encounter750.1 ft ▼ Upon Completion ft After Hrs ft	
VERY STIFF gray LOAM TILL			3 6 9		31.0	II3 II	
MEDIUM tan dirty moist SAND	753.10		10 11 14			-	
HARD gray SANDY LOAM TILL	750.60	V -45	11 23 29	4.2 S	9.0		
VERY STIFF olive-green SANDY LOAM TILL	745.60		5 22 28	3.1 P	12.0		
VERY DENSE tan weathered LIMESTONE	743.60	-50	100/6"				
VERY DENSE tan weathered LIMESTONE Auger Refusal at 52.5' End of Boring	742.60		00/1"		u 		
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The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetroence) The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206) BBS, ferral of the S-99)

Illinois De of Transpondent		10I	n		5(DIL BORIN	g log	Date 6/20/08
ROUTE FAP 301	DE	SCR	IPTIO	P92 N	-111-0	6 Bridge over the CC&P of Perryville Road	RR., .3 m. W.	
SECTION(201-3), K (4-1,								
COUNTY Winnebago E								
STRUCT. NO Station		D E P	L		M O	Surface Water Elev Stream Bed Elev	ft 72.50 ft	
BORING NO. B-3h Station 795+55 Offset 24.00ft Lt Pier Ground Surface Elev. 769.80) ft	T H	W S		І S T (%)	Groundwater Elev.: First Encounter Upon Completion	ft	
MEDIUM dark brown SILTY CLAY				0.5	24.0			
	767.30			Р				
STIFF brown CLAY LOAM			2	1.5 P	18.0			-
	765.80	5	4	<u>Р</u>				
STIFF tan SANDY LOAM	763,30		8 9 10	1.1 P	12.0			
STIFF tan SANDY LOAM TILL			7					
	760.30		9 11	1.8 P	11.0			
VERY DENSE tan weathered LIMESTONE	100.50	10	37 100/5''					
	758.30					-		
VERY DENSE tan weathered LIMESTONE			100/2"					
Auger Refusal at 14'	<u>_755.80</u>							
Borehole continued with rock coring.		 						
	-	_						
		-20						

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The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Peretropolated) The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206) BBS. from 17 (8-99)

Illinois Department of Transportation ROCK COF	RE LO	C		Ρ	age <u>1</u>	of <u>1</u>
Ulvision of Highways Illinios Department of Transportation/D-2				D	ate6	/20/08
P92-111-06 Bridge over the CC ROUTE FAP 301 DESCRIPTION of Perryville Roa	2&P RR., .3 ad	m. W	LO	GGE) BY _W	. Garza
SECTION(201-3), K (4-1, 5) K LOCATION Cherry Valley Twp 10 NE,				<u>G. 2E</u>		
COUNTY Winnebago CORING METHOD			R		CORE	s
STRUCT. NO CORING BARREL TYPE & SIZE Station Core Diameter 2 in	D E	0	E C O V	R Q	T I M	T R E N
BORING NO.B-3hTop of Rock Elev.760.30ftStation795+55Begin Core Elev.755.80ftOffset24.00ft Lt PierftftGround Surface Elev.769.80ft	P T H (ft)	R E (#)	E R Y (%)	D • (%)	E (min/ft)	G T H (tsf)
Delemiter will be to g	755.80	1	100	32	1.8	97.0
	750.80					
t.s.f.: 747.1 to 746.5	-20 	2	100	62	1.4	87.0
t.s.f.: 744.2 to 743.5	25 	3	-	83	2	184.0
End of Boring	740.80					

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Color pictures of the cores ______ Cores will be stored for examination until______ The "Strength" column represents the uniaxial compressive strength of the core sample (ASTM D-2938)

() Illinois Del of Transpo	parti	me ior	ent n		SC	DIL BORING LO	G		Page	1
Division of Highways Illinios Department of Trans	portation/E	D-2							Date	
						6 Bridge over the CC&P RR., .3 m. of Perryville Road				′_ <u>N</u>
SECTION(201-3), K (4-1, 5	5) K	L	.0CA1		Cherry	Valley Twp 10 NE, SEC., TWP.	43N, RN	I G . 2E	<u> </u>	
COUNTY Winnebago DI	RILLING	3 ME	THOD)	Hol	low Stem Auger HAMMER		CN	<u>1E-45</u>	Aut
STRUCT. NO.		D	В	U	M	Surface Water Elev.	ft	D	в	ι
Station		E P	L	C S	0	Surface Water Elev Stream Bed Elev72.50	ft	E P	L O	
BORING NO. B-4h			W S	A	S T	Groundwater Elev.:		T	W	
Station 795+32 Offset 3.00ft Lt CL		n	3	Qu		First Encounter 757.0 Upon Completion	ft⊻	H	S	Q
Ground Surface Elev. 797.00	ft	(ft)	(/6**)	(tsf)	(%)	After Hrs	ft	(ft)	(/6'')	(ts
						STIFF gray SILTY CLAY LOAM			4	1.
							775.50		9	F
	7 9 4.50									
MEDIUM brown LOAM	104.00	********	3			MEDIUM tan SANDY LOAM			5	
	793.00	_	3 4	0.5 P	13.0		773.00		13 11	
	100.00						773.00			
STIFF brown SILTY CLAY LOAM		5	1			VERY STIFF gray/brown SILTY		-25	3	
			2	1.2	19.0	CLAY LOAM			5	2.
	790.50		5	B			770.50		8	E
VERY LOOSE gray very moist			3						~	
dirty SAND			1		18.0	STIFF brown LOAM			2 6	1.
	788.00		1				768.00		9	E
_		-10						-30		
STIFF gray LOAM			2 3	1.9	15.0	VERY STIFF gray CLAY LOAM with SANDY LOAM lens			8	3.
	785.50		6	S	10.0		765.50		9	E
STIFF gray SILTY CLAY LOAM			3			VERY STIFF gray CLAY LOAM			4	
	783.00		4 6	1.8 B	20.0	TILL			8 9	2. F
	103.00						763.00			
VERY STIFF light brown CLAY		-15	2			VERY STIFF brown LOAM TILL		-35	2	
LOAM			5	2.5	21.0	THE OTHER DOWN COAVERILL			5	3.
	780.50	_	7	В			760.00	4	7	ļ
			~				760.00			
VERY STIFF gray SILTY CLAY LOAM			2			MEDIUM tan weathered			9	1

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer) The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206) BBS, from 137 (Rev. 8-99)

Date 042408 ROUTE FAP 301 DESCRIPTION 0 Pervilia Road LOGGED BY W. Garza SECTION (201-3), K (41, 5) K LOCATION Cherry Valley Twp10 NE, SEC, TWP, 43N, RNG, 2E COUNTY Winnebago DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME-45 Automatic, STRUCT, NO. Image: Country of the stem auger Note: Country of the stem auger The stem auger The stem auger The stem auger STRUCT, NO. Image: Country of the stem auger Image: Country of the stem auger The stem auger The stem auger The stem auger STRUCT, NO. Image: Country of the stem auger Image: Country of the stem auger The stem auger The stem auger The stem auger Station 30011 LCL Image: Country of the stem auger MEEDUM tan weathered 12 Image: Country of the stem auger VERY DENSE tan weathered 12 Image: Country of the stem auger The stem auger The stem auger The stem auger Station Station Station Station Station The stem auger The stem auger VERY DENSE tan weathered Image:	R	Illinois D of Trans)epartme	ent	(SOIL	BORIN	GIOG	Page <u>2</u> of <u>2</u>
P92-111-06 Bridge over the CC&P FR. 3 m. W. of Pertyville Road LOGGED BY W. Garza SECTION	Cir V	Division of Highwave							Date 6/24/08
COUNTY Winnebago DRILLING METHOD Hollow Stam Auger HAMMER TYPE CME-45 Automatic STRUCT. NO.				IPTION	P92-1	111-06 Brid	ige over the CC&F	P RR., .3 m. W.	
STRUCT. NO.	SECTION	(201-3), K (4	-1, 5) K	LOCAT		herry Valle	y Twp 10 NE, S	EC., TWP. 43N, R	NG.2E
Station	COUNTY	Winnebago		THOD		Hollow S	tem Auger	HAMMER TYPE	CME-45 Automatic
	STRUCT. NC Station BORING NO. Station Offset Ground Sur MEDIUM tan LIMESTONE VERY DENSI LIMESTONE Auger Refusa Borehole con	B 	D E P T H <u>755.50</u> 755.50 753.50 -45 45 45 45 45 45 45 45 45 45 45 45 45 	B L O W S (/6") 12 15 9 100/4"	U C S Qu	M Sur O Stu I S Gro T Fir Up	face Water Elev ream Bed Elev undwater Elev.: st Encounter _ on Completion	ft ft ft ⊻ft	

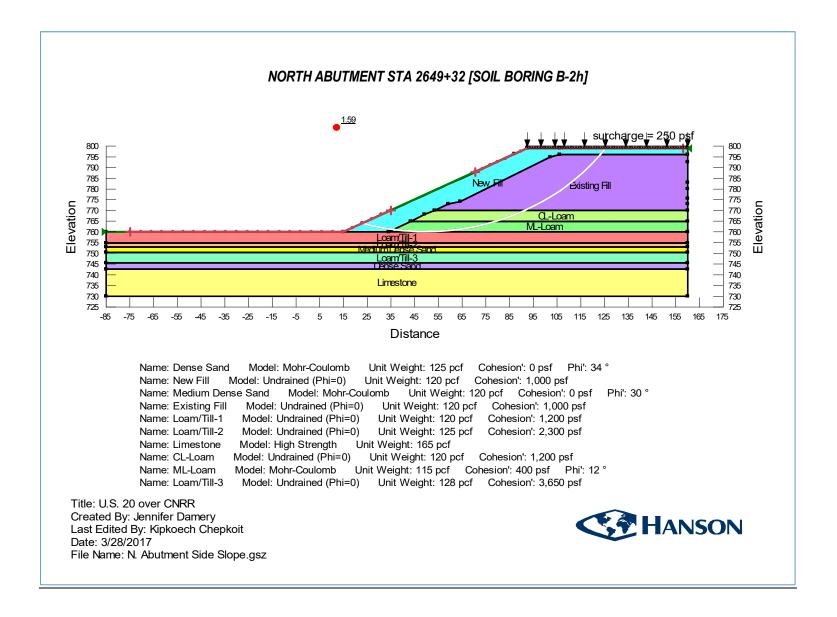
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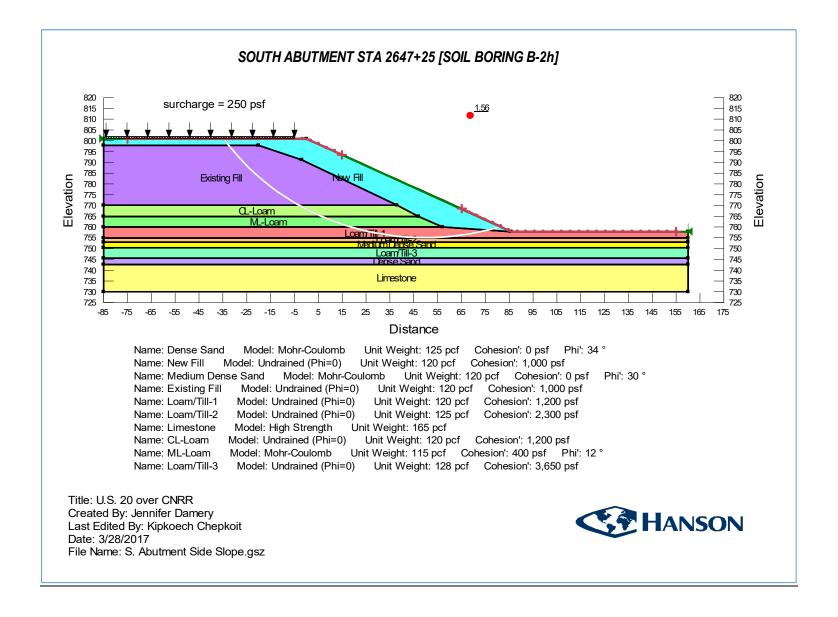
The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetro The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206) BBS. (Section 2019)

Illinois Department of Transportation ROCK COR	ELC)G	1	Ρ	age <u>1</u>	of <u>1</u>
Division of Highways Illinios Department of Transportation/D-2				D	ate _6	/24/08
P92-111-06 Bridge over the CC& ROUTE FAP 301 DESCRIPTION of Perryville Road	P RR., .3	m. vv.	_ LO	GGED) BY _W.	Garza
SECTION (201-3), K (4-1, 5) K LOCATION Cherry Valley Twp 10 NE, S	SEC., TW	P. 431	N, RN	G. 2E		
COUNTY Winnebago CORING METHOD			R	_	CORE	S
STRUCT. NO.		R E	ECOVERY(%)	R , Q D (%)	T I M E (min/ft)	T R E N G T H (tsf)
Dolomite: yellow tan-buff, vuggy and pitted, very finely crystalline, chalky with washed 75 out sand size particles and fractured throughout.	53.50	1	90	0	1	
74	48.50					
Dolomite: as above t.s.f.: 745.1 to 744.6		2	100	42	1.4	193.0
74						
Abandoned run - problems with water		3				
73	 			-		
End of Boring						

а 24 ж. д. н.

Color pictures of the cores ______ Cores will be stored for examination until______ The "Strength" column represents the uniaxial compressive strength of the core sample (ASTM D-2938)





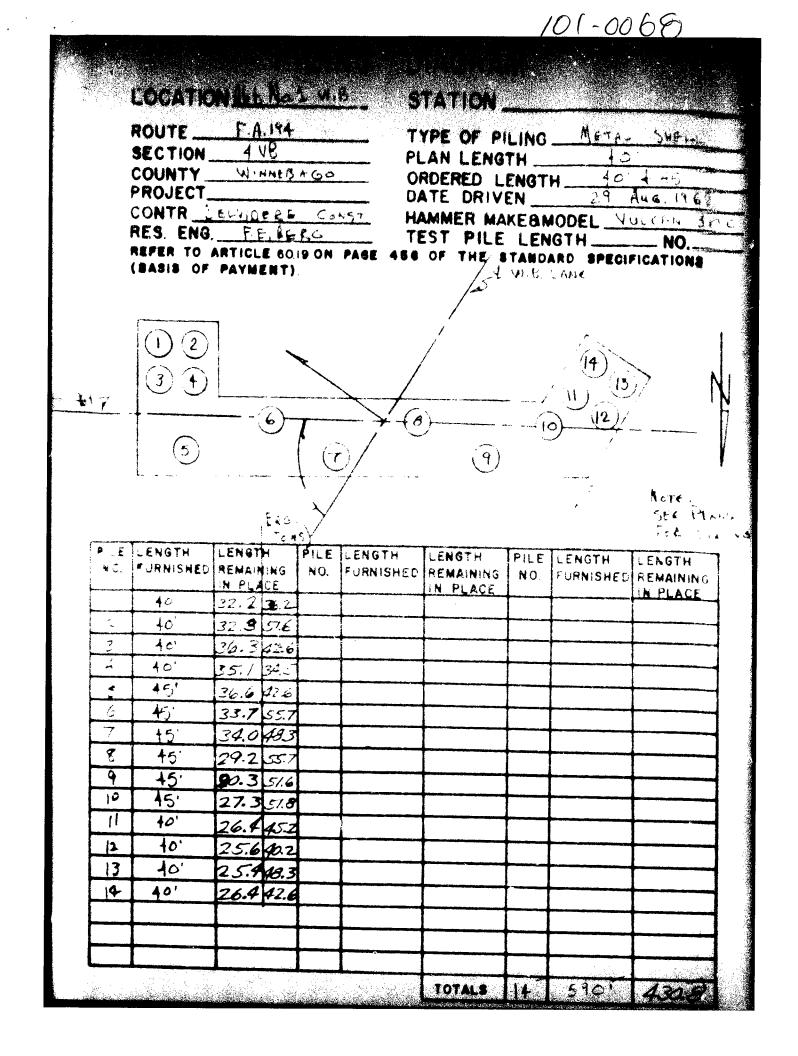
ROUTE FLA:114 TYPE OF PILING Metal Shell SECTION 4/8		LOCATIO					TATEON.			
COUNTY WINNEBASO ORDERED LENOTH 40° 2445 PROJECT DATE DRIVEN 29 Aug. 1968 CONTR BELVICERE Constr Ander 1968 DATE DATE DRIVEN 29 Aug. 1968 RESS ENG. f.E. BASE TEST PILE LENGTH NO. REPER TO ANTICLE GOID ON PAGE SSE OF THE STANDARD SPECIFICATIONS (BASIS OF PAYMENT). (1°) (2) (1°) (2) (1°) (2) (1°) (2) (1°) (2) (1°) (2) (1°) (2) (1°) (2) (1°) (1°) (2) (1°) (2) (1°) (2) (1°) (1°) (2) (1°) (2) (1°) (2) (1°) (1°) (2) (1°) (2) (1°) (2) (1°) (1°) (2) (1°) (1°) (2) (1°) (2) (1°) (2) (1°) (2) (2) (2) (2) (1°) (2)			1							SHELL
PROJECT		-			460	P	LAN LENG		and the second	And in case of the local data
CONTR BELVIDERE COUST. HAMMER MAKE MODEL VULCAN SQ RES. ENG. TE.BARE TEST PILE LENGTH NO. Repert to ARTICLE BOID ON PAGE 456 OF THE STANDARD SPECIFICATIONS (BABIS OF PAYMENT). AUX. NO. Image: Construct of the standard specifications Construct of the standard specifications Repert of the standard specifications Image: Construct of the standard specifications Image: Construct of the standard specifications Reperind the standard specifications Image: Construct of the standard specifications Image: Construct of the standard specifications Reperind the standard specifications Image: Construct of the standard specification of the standard specification of the standard specifications Reperind the standard specifications Image: Construct of the standard specification of	1	PROJECT_	-			D	ATE DRIV	EN	29	Aug. 1962
ABPER TO ARTICLE SQIBON PAGE 456 OF THE STANDARD SPECIFICATIONS (BABIS OF PAYMENT). Image: Comparison of the standard specifications (Comparison of the standard specifications) Image: Comparison of the standard specifications (DATE Image: Comparison of the standard specifications) Image: Comparison of the standard specifications of the standard specification	1	CONTR_B	ELVIO	ERE	Co	HIST. H	AMMER MA	KEAN	ODEL Vu	LCAN SO
(BABIE OF PAYMEENT). $(BABIE OF PAYMEENT).$ $(C E.E.LANG (I CON-) (I CON$										
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(ron 1) P. E LENGTH LENGTH NO. FURNISHED REMAINING NO. FURNISHED REMAINING NO. FURNISHED REMAINING IN PLACE I 4C' 37.5 Sol 2 2 4C' 37.0 36.2 2 4C' 37.0 36.2 2 4C' 37.0 36.2 3 40' 37.0 35.2 4 40 37.0 35.2 5 45' 38 2 42.4 5 45' 38.2 42.4 6 TEST $9u =$ 7 45' 35.6 450 8 45' 37.6 60.2 9 445' 37.6 60.2 9 445' 37.6 50.2 11 40' 37.6 37.4 12 40' 37.8 33.0 13 40' 35.8 60.2							· · · ·			ter HA
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5 45 38.2 42.6 6 TEST Property		FURNISHED 40'	REMAI IN PL 37.5	(FON H ING CE 382	Pile NO.		REMAINING			SEE PU: LENGTH REMAINING
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1 2 2	FURNISHED 40' 40'	REMAI IN PL 37.5 37.0 37.3	(ron H SCE 36.2 36.2 40.2	PILE NO.		REMAINING			SEE PU: LENGTH REMAINING
7 $45'$ 15.6 450 8 $45'$ 37.6 40.2 9 $45'$ 38.1 $4/4$ 10 10 $45'$ 36.7 450 10 11 $40'$ 37.6 $2/4$ 10 12 12 $40'$ 37.8 33.0 10 12 $40'$ 35.8 49.2 10	40. 1 2 2 4	FURNISHED 40' 40' 10	REMAI IN PL, 37.5 37.0 37.0 37.0	(TCN H ING CE 38.2 36.2 40.2 33.0	Pile NO.		REMAINING			SEE PU: LENGTH REMAINING
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10. 1 2 4 5	FURNISHED 40' 40' 40' 45'	REMAI IN PL. 37.5 37.0 37.3 37.0 38.2	(TCN H ING CE 38.2 36.2 40.2 33.0	Pile NO.		REMAINING			SEE PU: LENGTH REMAINING
9 45 38.1 $4/.4$ 10 11 10 45 36.7 450 11 11 40 37.6 $3/.4$ 12 12 $40'$ 37.2 33.0 13 13 $40'$ 35.4 49.2 14	10. 1 2 4 5	40' 40' 40' 40' 45' TEST Pu	REMAI IN PL. 37.5 37.0 37.0 37.0 38.2	(ron H ING CE 36.2 36.2 40.2 33.0 42.6	Pile NO.		REMAINING			SEE PU: LENGTH REMAINING
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	40. 1 2 2 4 5 6 7	FURNISHED 40' 40' 40' 40' 45' TEST QU 45'	REMAI IN PL, 37.5 37.0 37.3 37.0 38.2 38.2 35.6	(rch H GE 30:2 40.2 33.0 42.6 45.0	Pile NO.		REMAINING			SEE PU: LENGTH REMAINING
11 40' 37.6 37.4 12 40' 37.2 33.0 13 40' 35.2 40.2	40. 1 2 2 4 5 6 7 8	FURNISHED 40' 40' 40' 45' TEST QU 45' 45'	REMAI IN PL 37.5 37.0 37.0 37.0 38.2 35.6 37.6	(ron H GE 36.2 36.2 36.2 36.2 40.2 42.6 42.6 42.6 45.0 45.0	-) / Pile NO.		REMAINING			SEE PU: LENGTH REMAINING
12 40' 37.2 33.0 13 40' 35.8 40.2	•0. 	PURNISHED 40' 40' 40' 40' 45' TEST QU 45' 45' 45'	REMAI IN PL, 37.5 37.0 37.0 37.0 38.2 35.6 35.6 38.1	(ron H ING CE 36.2 36.2 36.2 36.2 40.2 33.0 42.6 450 450 450 450	-) / Pile NO.		REMAINING			SEE PU: LENGTH REMAINING
13 40' 35.8 10.2	+0. 1 2 1 4 5 6 7 8 9 10	PURNISHED 40' 40' 40' 40' 40' 40' 45' 45' 45' 45' 45'	REMAI IN PL 37.5 37.0 37.0 38.2 38.2 35.6 37.6 38.1 36.7	(ron H GE 36.2 40.2 42.6 42.6 45.0 45.0	-) / Pile NO.		REMAINING			SEE PU: LENGTH REMAINING
	+0. 1 2 3 4 5 6 7 8 9 10 11	-URNISHED 40' 40' 40' 40' 40' 45' 45' 45' 45' 45' 45' 45' 45'	REMAI IN PL 37.5 37.0 37.0 38.2 35.6 37.6 38.1 36.7 37.6	(ron H GE 36.2 36.2 36.2 36.2 36.2 36.2 40.2 42.6 45.0 42.6 45.0 45.0 45.0 21.4	-) / Pile NO.		REMAINING			SEE PU: LENGTH REMAINING
14 40' 35.9 KS.2	•0. 1 2 2 4 5 6 7 8 9 10 11 12	PURNISHED 40' 40' 40' 40' 40' 45' 45' 45' 45' 45' 45' 45' 40'	REMAI IN PL 37.5 37.0 37.0 37.0 38.2 35.6 37.6 38.1 36.7 37.6 37.6 37.6	(ron H GE 30.2 36.2 40.2 33.0 42.6 45.0 45.0 33.0 33.0 33.0	-) / Pile NO.		REMAINING			SEE PU: LENGTH REMAINING
	+0. 1 2 7 4 5 6 7 8 9 10 11 12 13	PURNISHED 40' 40' 40' 40' 45' 7EST QU 45' 45' 45' 45' 45' 45' 40' 40'	REMAI IN PL 37.5 37.0 37.0 38.2 35.6 37.6 38.1 36.7 37.6 37.6 37.6 37.6 37.6 37.6 37.6	(ron H Sol 2 30.2 36.2 36.2 40.2 40.2 42.6 42.6 45.0 42.6 45.0 42.6 45.0 42.6 45.0 45.0 45.0 45.0 2,4 45.0 33.0 40.2	-) / Pile NO.		REMAINING			SEE PU: LENGTH REMAINING
	+0. 1 2 7 4 5 6 7 8 9 10 11 12 13	PURNISHED 40' 40' 40' 40' 45' 7EST QU 45' 45' 45' 45' 45' 45' 40' 40'	REMAI IN PL 37.5 37.0 37.0 38.2 35.6 37.6 38.1 36.7 37.6 37.6 37.6 37.6 35.8	(ron H Sol 2 30.2 36.2 36.2 40.2 40.2 42.6 42.6 45.0 42.6 45.0 42.6 45.0 42.6 45.0 45.0 45.0 45.0 2,4 45.0 33.0 40.2	-) / Pile NO.		REMAINING			SEE PU LENGTH REMAINING

101-0067 Real to product to an inter MARCOMPLEING WITH THE MARKET P ROUTE EA 194 PLAN LENGTH SECTION 1/B ORDERED LENGTH _2 PROJECT F& 284 (17) DATE DRIVEN JALY 9 1964 HAMMER MAKEAMODEL 20 C. VULSA CONTR Balvidora Const TEST PILE LENGTH____ NO RES. ENG. L. Larkin REFER TO ARTICLE SOID ON PAGE 456 OF THE STANDARD SPECIFICATIONS (BASIS OF PAYMENT). 3.0 3.0 (4) (23) (ZZ) (70) E Para + 9 n ю 2:4 (5) (4) (7) (8) 3 4 ·†-Note Tast pile driven 160 TAN. TO EURIVE AT EB. 5- 796428,52 (& SURVEY PILE LENGTH LENGTH LENGTH PILE LENGTH LENGTH PILE LENGTH FURNISHED REMAINING NO. FURNISHED REMAINING NO. FURNISHED REMAINING NQ. IN PLACE IN PLACE IN PLACE 14.8 20' (28:0' 20 24 4 139 17 Ŧ 4.5 12 20 (27.4" 50 20 (27.4 z 145 20 (27.8) 53 /9 ≠ (28.6⁷ 3 4.2 20 20' (2967 5.6 4 20 (27,8 21 15.7 20' (262 20 (27.6 156 5 22 16. 20' (27,1 16.0 20 (28,1 20 20' (27,3' 163 27,5 20/28.4 16.0 20 (28. 17.2 24 76.6 20 (28.6 20' (26.5 16.1 10 <4 20 (27.5 11 128.6 149 lo' 12 49 22/ 13 `مر 15.Z 20 (225 20 28,2 14.7 4.2 Guile TOTALS 24 40 LA

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	COUNTY_PROJECT	and the second	anter the many beat stands that a	Winterstreet Frank Statistics (Street, St.		DERE				20	
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PILE BO.	LENGTH FURNISHED	LENGTH	rg ous) Pil	ELENG	STH NSHED	LENGT	(10+7 H DING	PILE NO.	LENGTH	1	
	1	LENGTH REMAININ	rg ous) Pil IG Ni E	E LENG	IISHED	REMAI	(Tory H DING ACE	PILE	LENGTH	LENG ED REMA IN PL	INING
	PURNISHED	LENGTH REMAINING	rg ous) Pil IG Ni E 6.4 10	E LENG	ISHED	REMAI IN PL 16.L	(TONT H ING CE 38.0	PILE	LENGTH	ED REMA	INING
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10(-0067)SITATION DUILING TYPE OF PILINC METAL Shell ROUTE FAINA PLAN LENGTH . 30 + 35 4VB SECTION ORDERED LENGTH WINNEBAGO COUNTY 10 + 11 September PROJECT F6-284(17) DATE DRIVEN CONTR BALMORRE CONST. CO. HAMMER MAKEBMODEL YULCAN 300 RES ENG FE BERG TEST PILE LENGTH ____ NO._ REPER TO ARTICLE GO. IS ON PAGE 456 OF THE STANDARD SPECIFICATIONS TEB LANG (BASIS OF PAYNENT). STA. 797 123.19 TOE [3] (2)1 BY-Pass 32'R & BY-PASS 14) 69°44' \bigcirc 3 (4) BK. ALT.2 12 6 (8) (b)(5) (9) 7 Nore: See Du FOR SPACING All Parise 520 ME- Robuspi (TOUS) PLE LENGTH LENGTH PILE LENGTH LENGTH PILE LENGTH LENGTH NO. FURN SHED REMAINING NO. FURNISHED REMAINING NO FURNISHED REMAINING IN PLACE IN PLACE IN PLACE 45 39.1 60+ 2 45 39 0 60+ -45 39 260+ 4= 39 3 404 4 45 27.0 60+ 5 45 40.5160+ 6 45 7 41.3 60+ TEST Ale 8 45' 9 42 0 60+ 45 10 +1.4' 60+ 45 H 41.8.60+ 45 12 42.260+ 13 45 41.1°Ko+ +2.4' 10+ 14 45 and the second 624

STATION STATE SALAS HORAND PRODUCTION Martha Hack Start & 1975 - 4 ROUTE 222/22 - The TYPE OF PILING CRED SOTED THE SECTION_ 416 PLAN LENGTH Sourt 1-15' And COUNTY LUNAN SE ORDERED LENGTH AGUT IN PROJECT / - - ----DATE DRIVEN CONTR BELYIDERE CONST. HAMMER MAKEBMODEL VULCAN Se RES. ENG. EPAUK BERG TEST PILE LENGTH_ REFER TO ARTICLE GOID ON PAGE NO 456 OF THE STANDARD SPECIFICATIONS (BASIS OF PAYMENT) & W. BNO LANE C. E. BND. LANE Bre Two ABUT. #2 PILE LENGTH LENGTH PILE LENGTH LENGTH PILE LENGTH FURNISHER LENGTH 10 REMAINING FURNISHED REMAINING NQ, NO. FURNISHED REMAINING LIN PLACE IN PLACE 1 30 / 32.61 25.4 IN PLACE 40'/30.4") 29.7 2 30'*(30.8)* 22.9 2 40/27.71 30.4 30 (30.0) 3 232 3 40 (30.0) 36.2 4 30/32.6/ 23.1 4 40'/208/ 22.0 5 **30'/3**0.0/ 25.7 S 401/30.01 27.1 6 30'/34.6/ 22.5 6 10/27.7/ 26.0 7 30/37.0) 23.4 40/220) 26.6 8 40/32 L 25.2 45/3001 28.0 611.6 285 9 401/27.7) 27.1 Ø 10/200 31.4 10 40 (30.0) 25.5 // 40 12201 29.2 // 40[30.8] 26.0 12 10/32 4 26,5 12 40/29.0 23.0 13 Ne M 2*0.8* 0/27.7 24.2 4 6 /3c.0 29.2 10/32.6 29.2 ar Creek Plac 115% CUP 210 it. Cree Plan 1239 COP (° (' , V , S. Carpe



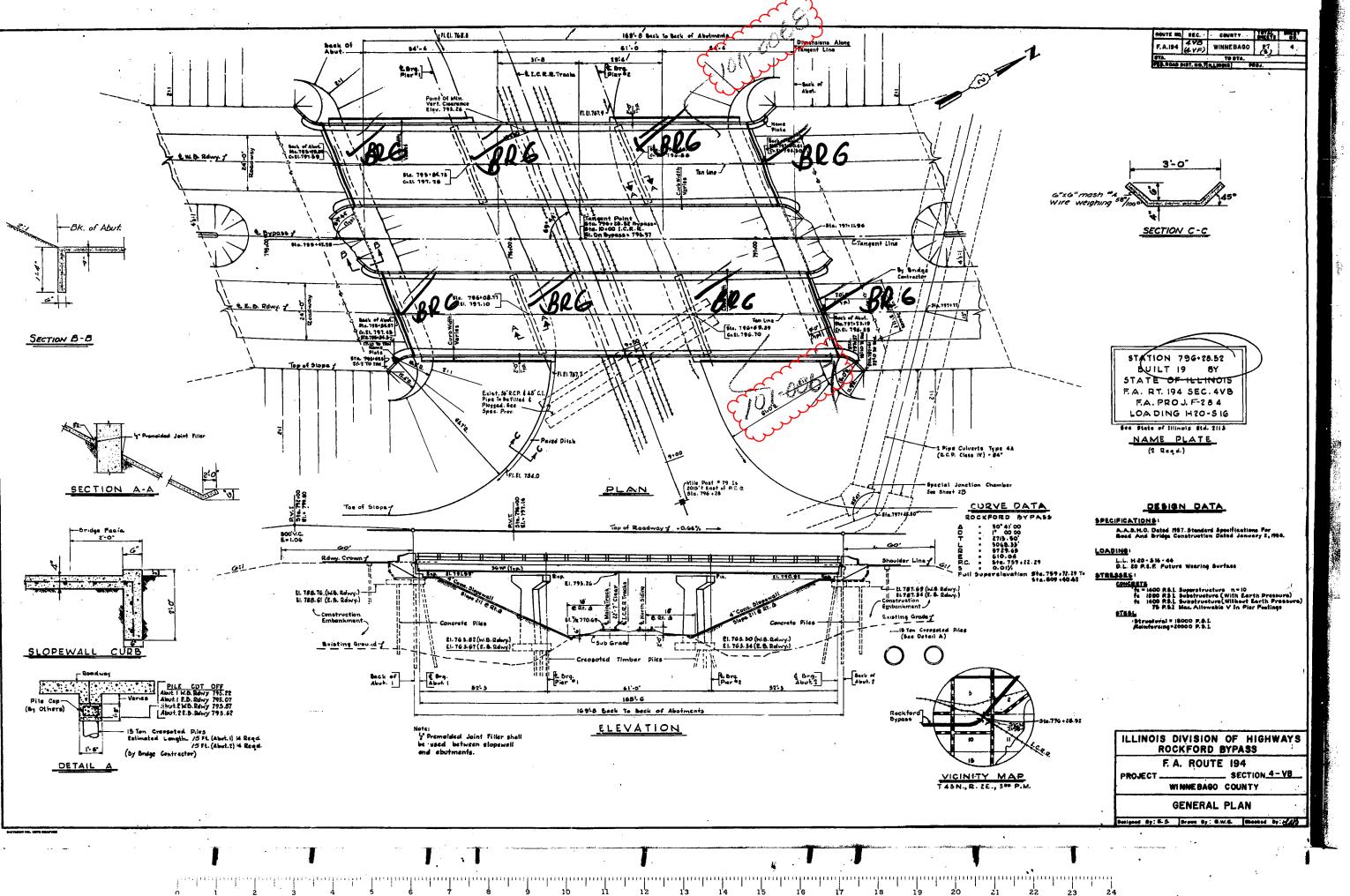
<u>101-0068</u> LOCATION ZOAL ME HOUSE STATION 20035 TYPE OF PILING PROLOTED IN AND ROUTE FA 194 SECTION 418 PLAN LENGTH . ORDERED LENGTH 20 COUNTY MULLERAGO PROJECT EG 284 (17 902 DATE DRIVEN 9 JULY HAMMER MAKEBMODEL 30 C PULCAN CONTR BALMOERE NO. TEST PILE LENGTH RES. ENG. LACKIN OF THE STANDARD SPECIFICATIONS REFER TO ARTICLE GOIS ON 3-01 1 6 (BASIS OF PAYMENT) 3.0 =/~~~ -14 (Z3) 4 -+ 24 <u>t</u> the f 2:64 (8)(5) (2 3 Z $\mathbf{1}$ 14 Nore TEST PILE OF VER f IN VICINITY FICE # Z E,B 1. TANGAN'T TO CURVE MAT STA. 176228.52 ZUBIEY LENGTH LENGTH LENGTH PILE LENGTH PILE LENGTH PILE LENGTH NO FURNISHED REMAINING NG. FURNISHED REMAINING FURNISHED REMAINING NO. IN PLACE IN PLACE IN PLACE 34 20(309 27.7 17 14.3 ZC 20' (31.0 15 c 25 (2907 34 18 2 \mathcal{C} 26 (3/.87 4.8 129.4 14 3 EE 20 (303 14.7 ko' (27.7) 15.7 12 16.9 (29,0 15.2 20 20' (242 21 (30.37 6 15.3 22 20 162 20' (21.4 (31,8 7 14,9 23 65 16.0 ZO' (213 15.2 24 zo' (31.87 20' (30.3 14.8 0 142 20' (31.0 20' (31.2 151 10 16.3 11 zo (29.9 20 (27,7 5.6 12 312' 20' 15.4 30.9 14.3 20` 14.0 20 (29 (20 690

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1 2	20 20 20	MEMAININ IN PLASE 13A 31 14.6 31	1.2	NG. 18 19	20'	REMAI IN PL 16.0 13.7	NING ACE 32.8 22.2	NO.	1	REMAINING
NQ. 1	PUPH SXED 20' 15'	NEMAIEIN IN PLACE 12A' 33 14.6' 3 14.1 22	€ 1.2 2.2	NC. 18 19 20	20' 15' 20'	REMAI IN PL 16.0 13.7 15.5	NING ACE 32.8 22.2 30.3	NO.	1	REMAINING
1 2	20 20 20	MENAIBIN IN PLACE 13A 31 14.4 31 14.1 33	6 2.2 2.2 2.1	18 19 20 21	20' 15' 20' 20'	NEMAI IN PL 16.0 13.7 15.5 16.9	NING ACE 32.8 22.2 30.3 34.7	NO.	1	REMAINING
1 2 3	20' 20' 15' 20' 20	MENAIBIN IN PLACE 13A 31 H.4' 7 14.1 23 16.1 33 15.0' 14	16 17 17 12 12 12 12 12 12 12 12 12 12 12 12 12	NG 18 19 20 21 22	20' 15' 20' 20' 20'	REMAI IN PL 16.0 13.7 15.5 16.9 17.0	NING ACE 32.8 22.2 30.3 34.7 23.2	NO.	1	REMAINING
1 2 3 4 9	20 20 15 20'	NEMAIEIN IN PLACE 13.4 33 14.1 22 16.1 32 15.0' 34 16.0' 34	16 2.2 2.2 2.1 2.1 2.1	NG. 18 19 20 21 22 21 22 23	20' 15' 20' 20' 20' 20' 20'	REMAI IN PL 16.0 13.7 15.5 16.9 17.0 17.2	11119 132 B 122.2 130.3 14.7 123.2 136.7	NO.	1	REMAINING
1 2 3 4 9 6	20 20 15 20 20 20 20 20'	MENAIBIN IN PLACE 13A' 31 14.1 22 16.1 32 15.D' 54 16.0 54 16A' 32	15 2.2 2.2 2.1 2.1 2.1 4.9	NG. 18 19 20 21 22	20' 15' 20' 20' 20'	REMAI IN PL 16.0 13.7 15.5 16.9 17.0 17.2	NING ACE 32.8 22.2 30.3 34.7 23.2	NO.	1	REMAINING
1 2 3 4 5 6 7	20 20 15 20 20 20 20	MENAIBIN M PLACE 13A 31 H.6' 7 14.1 23 16.1 33 16.0 34 16.0 34 16.4 3 16.4 3 17.1 35	15 12 27 2.2 2.1 2.1 4.9 5.7	NG. 18 19 20 21 22 21 22 23	20' 15' 20' 20' 20' 20' 20'	REMAI IN PL 16.0 13.7 15.5 16.9 17.0 17.2	11119 132 B 122.2 130.3 14.7 123.2 136.7	NO.	1	REMAINING
× Q 1 2 3 4 5 6 7 8	20' 20' 15' 20' 20' 20' 20' 20' 20' 20' 20' 20'	MEMAIBIN M PLACE 13A' 31 H. 6' 7 14.1 22 16.1 32 15.D' 54 16.0 54 16.A' 32 17.1 35	16 2.2 2.2 2.1 2.1 2.1 2.1 2.1 2.1 2.1 2.1	NG. 18 19 20 21 22 21 22 23	20' 15' 20' 20' 20' 20' 20'	REMAI IN PL 16.0 13.7 15.5 16.9 17.0 17.2	1119 32 B 22.2 30.3 34.7 23.2 36.1	NO.	1	REMAINING
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× Q 2 3 4 5 6 7 8 9 10	20 20 20 20 20 20 20 20 20 20 20 20 20 2	MENAIBIN M PLACE 13A' 33 H.6' 7 14.1' 20 16.1' 34 16.0' 34 16.0' 34 16.4' 3 17.1' 35 17.1' 35 17.1' 35 17.0' 35 15.6' M	5.8 5.8	NG. 18 19 20 21 22 21 22 23	20' 15' 20' 20' 20' 20' 20'	REMAI IN PL 16.0 13.7 15.5 16.9 17.0 17.2	1119 32 B 22.2 30.3 34.7 23.2 36.1	NO.	1	REMAINING
1 2 3 4 5 6 7 8 9 10	20 20 15 20 20 20 20 20 20 20 20 20 20 20 20 20	MEMAIEIN M. PLASE 13A' 31 H. C' 7 14.1' 22 16.1' 32 15.D' 34 16.0' 34 16.4' 32 17.1' 35 17.1' 35 17.0' 35 15.4' 14 16.2' 3	5.8 5.8	NG. 18 19 20 21 22 21 22 23	20' 15' 20' 20' 20' 20' 20'	REMAI IN PL 16.0 13.7 15.5 16.9 17.0 17.2	1119 32 B 22.2 30.3 34.7 23.2 36.1	NO.	1	REMAINING
1 2 3 4 5 6 7 8 9 10 11 12	20 20 20 20 20 20 20 20 20 20 20 20 20 2	MENAIBIN M. PLACE 13.A 31 H. C 7 14.1 22 16.1 32 16.0 34 16.0 34 16.0 34 16.0 34 16.0 34 16.0 34 16.0 34 16.1 35 17.1 37 17.1 37 17.1 37 17.2 3 15.4 4 15.2 3 15.4 4 15.2 3 15.2 4 15.2 3 15.2 3 15.3 15.2 3 15.2 3	5.8 5.8 5.2 2.2 2.1 2.2 2.1 2.2 2.1 2.2 2.1 2.2 5.8 5.8 5.8 5.8	NG. 18 19 20 21 22 21 22 23	20' 15' 20' 20' 20' 20' 20'	REMAI IN PL 16.0 13.7 15.5 16.9 17.0 17.2	1119 32 B 22.2 30.3 34.7 23.2 36.1	NO.	1	REMAINING
1 2 2 3 1 3 6 7 8 9 10 11 12 13	20 20 12 20 20 20 20 20 20 20 20 20 20 20 20 20	MEMAIEIN M. PLASE 13A' 31 H. C' 7 14.1' 22 16.1' 32 15.D' 34 16.0' 34 16.4' 32 17.1' 35 17.1' 35 17.0' 35 15.4' 14 16.2' 3	5.8 5.8 5.3 5.3	NG. 18 19 20 21 22 21 22 23	20' 15' 20' 20' 20' 20' 20'	REMAI IN PL 16.0 13.7 15.5 16.9 17.0 17.2	1119 32 B 22.2 30.3 34.7 23.2 36.1	NO.	1	REMAINING

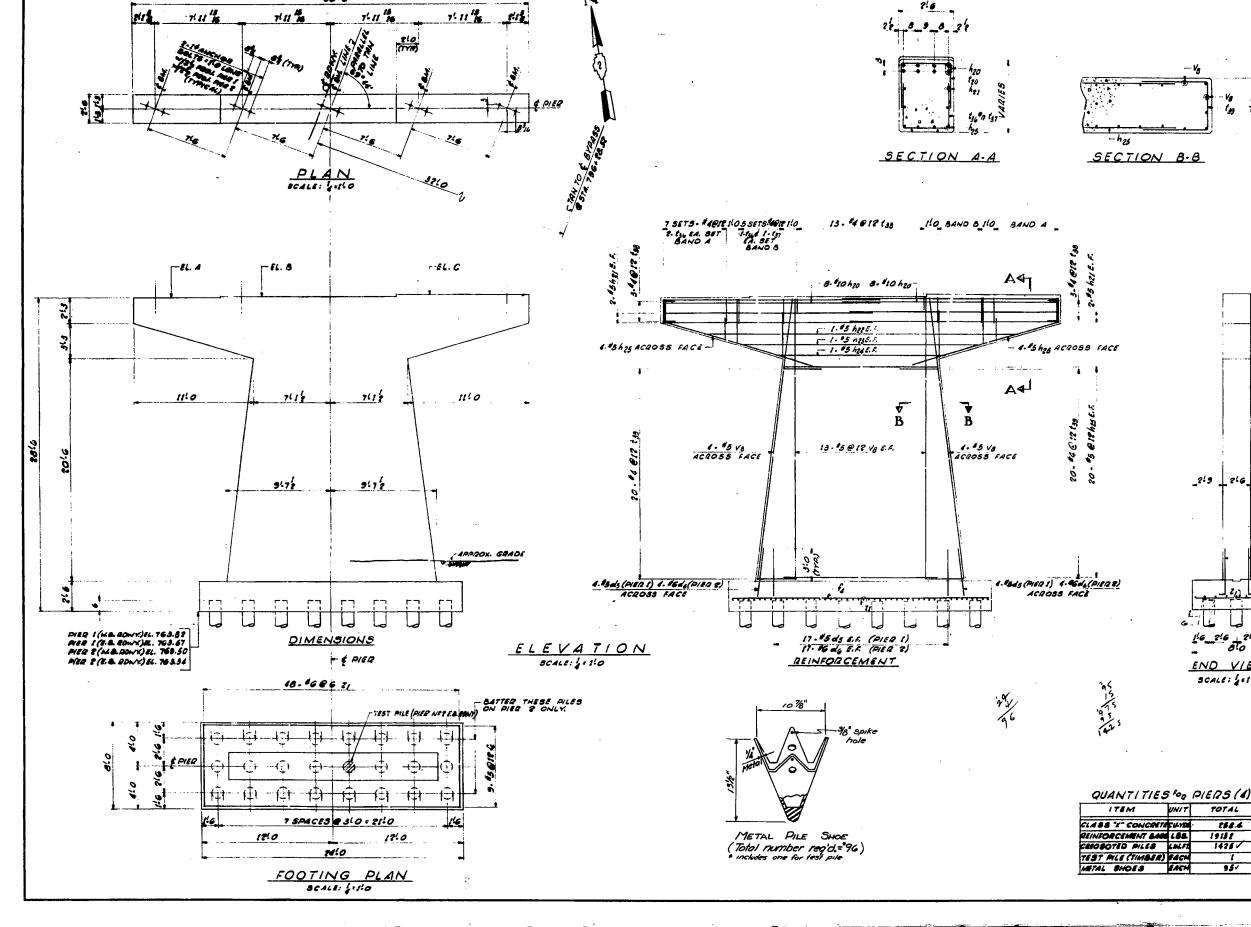
101-0068 STATION ALLES LOCATION Barrison 2 W.B. ROUTE ____EAMA TYPE OF PILING METHL SHELL PLAN LENGTH 30 4 35 416 SECTION 45 COUNTY ______ ORDERED LENGTH 7+10 Sebt. 1961 FO-284(17) DATE DRIVEN PROJECT_ HAMMER MAKESMODEL YULCH 30 5 CONTR BELVIDERE CONST. CO. NO TEST PILE LENGTH_ RES. ENG. P.H. Bong REFER TO ARTICLE SOID ON PAGE 456 OF THE STANDARD SPECIFICATIONS SE W.B. LANS (BABIS OF PAYMENT). г STA 797400.41 13 1 69044 32'L & BP. Ass 14 4 $\left(H\right)$ 3 Ba Mat 7 12 8 6 Ю) OTE SEA ANIS (5) 9 7 ON SAK NO. to Priva AT REFLAM. TO LBY-PARS 584 (taks) LENGTH LENGTH PILE LENGTH LENGTH PILE LENGTH LENGTH M. E NO. FURNISHED REMAINING REMAINING FUNNISHED REMAINING **#** Q. FURNISHED NO. IN PLACE IN PLACE IN PLACE 45 36.0 160+ 45 37.0 60+ E Į. 2 35.8 404 4 4 F. 36.4 601 ¥5 37.1 601 F 36.5160+ 45 6 36.4160+ 7 45 45 34.5 160+ 8 45 9 11.1.60+ 45 36 9 60+ 10 45 11 35,8760+ 45 12 38.6 60+ 45 39.6 60+ 15 4 +5 60+ 35.4

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