

**STRUCTURE GEOTECHNICAL REPORT  
BOX CULVERT  
IL 173  
McHENRY COUNTY, ILLINOIS**

**Structure No. 056-0202**

10/14/2022

**Prepared for:**

Bowman Consulting Group Ltd.  
1001 Warrenville Road, Ste. 110  
Lisle, Illinois 60532

**Prepared by:**

INTERRA, INC.

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**STRUCTURE GEOTECHNICAL REPORT  
BOX CULVERT  
IL 173  
McHENRY COUNTY, ILLINOIS**

**1.0 INTRODUCTION**

Interra, Inc. (INTERRA) was tasked by Bowman Consulting Group Ltd. based in Lisle, Illinois to conduct subsurface soil investigation and prepare the Structural Geotechnical Report (SGR) for the improvement of culvert structure located under IL 173. The proposed improvement consists of removal headwall, wingwalls and approximately four feet of existing culvert at both ends. The culvert sections will be replaced and extended by a few additional feet including new cantilever wingwalls and headwalls.

**2.0 PROJECT SCOPE**

INTERRA's scope of work included drilling two (2) structure geotechnical borings to a depth of 30 feet each; performing associated laboratory tests on collected soil samples; preparation of Structure Geotechnical Report in accordance with IDOT Geotechnical Manual 2020.

**3.0 SITE DESCRIPTION**

The project section is located in Alden Township, McHenry County and defined as Section 31 T46N, R6E Third Meridian. The subject area is located on IL 173, approximately 4350 feet east of Harvard Hills Rd. The surface elevations of the boreholes are between 964.6 feet and 964.7 feet. The invert elevation of the Box Culvert structure is at approximately 956.2 feet.

**3.1 Mining Activity**

From the Illinois State Geological Survey (ISGS, 2021), McHenry County is not identified as coal producing area. Therefore, no past coal mining activities may have taken place at the project site.



### 3.2 *Seismic Considerations*

USGS National Seismic Hazard Maps (AASHTO LRFD, Figure 3.10.2.1-1) indicate a Peak Ground Acceleration (PGA) of 3.2% of gravity, with a 7% probability of exceedance in 75 years. The project area has no active, major faults (Kolata, 2005).

## 4.0 **FIELD INVESTIGATION**

The locations of the borings are presented in the Borehole Location Plan in Appendix A. The Boreholes are as marked in the field by INTERRA. Prior to drilling, the drilling sub-contractor Geocon Professional Services (GEOCON) contacted the local one-call utility clearance service (JULIE) to clear underground utilities. The borings were drilled with a truck mounted drill rig Diedrich D-50. INTERRA's engineer was present during the drilling to collect and log the soil samples. The borings were drilled, and samples were collected in general accordance with the guidelines in the IDOT Geotechnical Manual. Soil sampling was performed per AASHTO T-206, "Penetration Test and Split Barrel Sampling of Soils". Soil sampling was performed at 2.5-foot intervals up to a depth of 30 feet. The soil samples were taken in conjunction with the Standard Penetration Test where a driving resistance to a standard 2" split-spoon samples indicate relative density of granular materials and consistency of cohesive soils. Soil specimens from the borings were visually identified in accordance with the AASHTO and IDOT textural classification systems. Also, unconfined compressive strength tests were performed on cohesive samples using an Illinois modified RIMAC tester. Cohesive samples that could not be tested with a RIMAC tester were tested with a pocket penetrometer to estimate the unconfined compressive strength. Shelby tube samples were also collected at selected boring locations for performing laboratory tests. Water level readings were taken during drilling and immediately after drilling.

## 5.0 **LABORATORY TESTING**

All laboratory testing was performed in accordance with IDOT and/or AASHTO standard methods for testing. Moisture content tests (AASHTO T 265) were performed for all soil samples. Shelby Tube samples were tested for Unconfined Compressive Strength (ASTM

D 2166), Grainsize Analysis (AASHTO T 88) and Atterberg Limits (AASHTO T 89, 90). Laboratory test reports are presented in Appendix B.

Soil boring logs indicating the blow counts, moisture content and soil description have been prepared and included in Appendix A of this report.

## **6.0 SUBSURFACE CONDITIONS**

Boring IL-173-BCB-01 encountered 4.0 inches of asphalt and 7.0 inches of stones at the surface. This was underlain by stiff to soft sandy clay loam up to 5.5 feet. Below this was loose sandy loam up to 8.0 feet and medium stiff clay loam up to 10.5 feet. This was underlain by medium stiff sandy clay loam up to 13.0 feet. Medium dense sand was encountered between 13.0 feet and 23.0 feet. This was underlain by dense sandy loam up to 25.5 feet and stiff clay up to 28.0 feet. Stiff sandy loam was encountered between 28.0 feet and 30.0 feet. Boring was terminated at 30.0 feet.

Boring IL-173-BCB-02 encountered 4.0 inches of asphalt and 6.0 inches of stones at the surface. This was underlain by medium stiff sandy clay loam up to 3.0 feet, followed by very loose to medium dense sandy loam up to 10.5 feet. Below this was medium dense to dense sand and gravel up to 23.0 feet. This was underlain by stiff clay, up to 28.0 feet. Very stiff loam was encountered between 28.0 and 30.0 feet. Boring was terminated at 30.0 feet.

For detailed stratification, please refer to boring logs presented as Appendix A.

### Groundwater Information

Groundwater elevations were recorded during drilling and immediately after drilling at both boring locations. Boring IL-173-BCB-01 encountered ground water at 18.5 feet depth during drilling and at 29.0 feet at end of drilling. Boring IL-173-BCB-02 encountered ground water at 18.5 feet depth during drilling and at 28.5 feet at end of drilling. Since the boreholes were backfilled immediately after drilling, the water levels reported may not represent the long-term groundwater levels. Changes in water levels should be expected



due to seasonal variations and precipitation.

## **7.0 ANALYSIS AND RECOMMENDATIONS**

The following recommendations are developed based on the field investigation and laboratory testing, project information provided to INTERRA, IDOT Culvert Manual, Standard Specifications and the AASHTO LRFD Bridge Design Specifications, 9<sup>th</sup> Edition, 2020.

It is our understanding that the headwalls, wingwalls and approximately a four-foot section on the north and south ends of the existing box culvert will be removed and replaced with new culvert longer by a few additional feet, a new head wall and new horizontal cantilever wingwalls. We also understand that the replacement culvert will be the minimum length of 6 feet or half the length of the wingwalls.

### **BEARING CAPACITY AND SETTLEMENT**

Design loads for the proposed construction were not provided. However, for analyses purposes, it is estimated that the approximate bearing pressure applied to the foundation soils will be less 1500 psf at an approximate depth of 10 feet below the existing roadway grade. Foundation soils at this elevation consist of medium clay loam and sandy clay loam at the south end of the culvert medium dense sandy loam and sand at the north end of the culvert. We recommend a two-foot undercut at the south end and no undercuts at the north end. Unsuitable soil shall be replaced with rockfill in accordance with the following paragraph. Foundation soils can be designed for a factored bearing resistance of 3000psf, which includes an LRFD Resistance Factor of 0.45. Although the roadway grade will not be changing, some additional fill is anticipated on the replacement sections. Settlements are expected to be no greater than one (1) inch due to minimal additional fill.

However, if during construction additional unsuitable soils are encountered, the engineer should be contacted to determine the lateral and vertical extent of undercuts needed. The unsuitable soils will need to be removed and replaced with suitable material. We recommend undercutting unsuitable soils and replacing with Rockfill. A woven geotextile



fabric should be used below the aggregate improvement for ground stabilization (IDOT Section 1080.02). The aggregate shall be capped with six inches of CA7 and satisfy the Standard Specifications unless otherwise indicated in the Special Provisions. If the foundation soils become unstable due to construction equipment loadings during excavation or construction, a working platform may be needed. The need for such platform is dependent on the type, thickness and strength of the soils encountered, the method of water diversion selected by the Contractor, precipitation, construction sequence, and the time of the year the box culvert is constructed. The Engineer should make the determination that a working platform is required during excavation based on the field conditions.

### WINGWALLS

Plans indicate that existing wingwalls are horizontal. IDOT Culvert Manual requires that a portion of the barrel equal to the minimum of half the wingwall length or six (6) feet shall be poured monolithically with the wingwalls. Horizontal cantilever wingwalls are proposed.

The Wing walls at the box culvert should be designed for the lateral earth pressures and lateral pressures from live loads. In accordance with the culvert manual, Table 4.1.1.2-1, the earth pressure in horizontal ( $P_H$ ) is estimated to be 65 psf for a horizontal cantilever wingwall. Live load surcharge from traffic and other surcharges can be estimated using a surcharge equivalent to 2 feet of soil for wingwalls. IDOT Standard Specifications and details should be followed for drains and limits of free draining material behind the wall.

### STABILITY ANALYSES

Global slope stability analyses were conducted for the critical cross-section assuming wall height of 15 feet and a 3H:1V backfill. The LRFD resistance factor considered is 0.65, which is equivalent to slope stability factor of safety of 1.54. Slope stability analyses were conducted using SLIDE V7.0. Analyses indicated that the global slope stability factor of safety exceeded the minimum required value of 1.54 for both short and long-term loading conditions. Appendix C contains the results of the slope stability analyses.



## CHANNEL PROTECTION

Channel protection at culvert outlets can be achieved by providing a riprapped transition or apron from the culvert outlet to the natural channel. The riprap should have bedding and/or filter fabric under it and should be of sufficient size and depth for the anticipated flow. A length of protection of three times the anticipated velocity in feet per second is commonly used as a rule of thumb.

## SCOUR

As per All Bridge Designers Memo 14.2, design scour elevations for box culverts are no longer needed.

## **8.0 CONSTRUCTION CONSIDERATIONS**

The contractor can consider temporary ditches, sumps, granular drainage blankets and other methods to control surface water infiltration and ground water and provide a dry condition for construction.

The proposed construction will be in stages and Temporary Soil Retention System (TSRS) may be required to facilitate the removal of the existing wingwalls and construction of the new headwall and wingwalls. It is anticipated that temporary shoring will be required during the stage construction. Temporary shoring is feasible using simple cantilevered temporary sheet piling. Table 1 lists suggested lateral earth pressure and soil resistance parameters. All excavations must be performed in accordance with local and federal regulations.

**Table 1 - Recommended Soil Parameters for Temporary Soil Retention Systems**

Elevation (Depth below Proposed roadway	Soil Type	Saturated	Shear Strength (psf)	Friction Angle (deg)	Coulomb Active	At- Rest Earth	Passive Earth	Soil Modulus, s,	Epsilon 50 Strain





surface) Ref boring BCB-01		Unit Weight (pcf)	Undrained	Drained	Undrained	Drained	Earth Pr. Coeff, Ka	Pr. Coeff, K <sub>0</sub>	Pr. Coeff., K <sub>p</sub>	k (pci)	
0'-8'	Loose Sandy Loam	115	-	-	-	25	0.36	0.58	2.46	25	-
8'-13'	Medium Stiff Cohesive Soil	120	750	50	-	26	0.36	0.56	2.56	100	0.009
13'-25'	Med. Dense granular soils	125	-	-	-	30	0.30	0.50	3.00	60	-
25'-30'	Stiff Cohesive Soil	120	1500	75	-	28	0.33	0.53	2.77	500	0.007

## 9.0 CLOSURE

The analysis and recommendations submitted in this report are based upon the data obtained from two (2) soil borings performed at the locations indicated on the Borehole Location Plan, project information provided to INTERRA and from any other information discussed in this report. This report does not reflect any variations that may occur between these boreholes. In performing subsurface explorations, specific information is obtained at specific locations at specific times. It is a well-known fact that variations in soil and rock conditions exist on most sites between borehole locations. Also, groundwater levels vary from time to time. The nature and extent of variations may not become evident until the course of construction. If project characteristics change or if variations in the subsurface conditions appear evident, it will be necessary for a re-evaluation of the recommendations of this report.



We appreciate the opportunity to be of service to you. Should you need additional information or clarifications, please call us at (630) 754-8700.

Yours truly,  
**INTERRA, INC.**



Ashok Guntaka, EI  
Project Engineer



Reshma Chirakkara, Ph.D.  
Staff Engineer



Sanjeev Bandi, Ph.D., PE  
Project Manager



Sudhakar "Rao" Doppalapudi, PE  
QC/QA Reviewer

Exp 11/30/23

## REFERENCES

- AASHTO 2020, LRFD Bridge Design Specifications, 9<sup>th</sup> Edition 2020, American Association of State Highway and Transportation Officials, Washington, DC.
- IDOT 2020, Geotechnical Manual, Illinois Department of Transportation.
- IDOT 2016, Culvert Manual, Illinois Department of Transportation.
- IDOT 2016, Standard Specifications for Road and Bridge Construction. Illinois Department of Transportation.
- IDOT 2012, Bridge Manual, Bureau of Bridges and Structures, Illinois Department of Transportation.
- Kolata, D. R., 2005, Bedrock Geology of Illinois, Illinois Map 14, Illinois State Geological Survey.
- U.S.G.S. 2014, National Seismic Hazard Maps.  
<http://earthquake.usgs.gov/research/hazmaps/>
- Coduto, Donald P., 1994, Foundation Design, Prentice Hall, Inc.

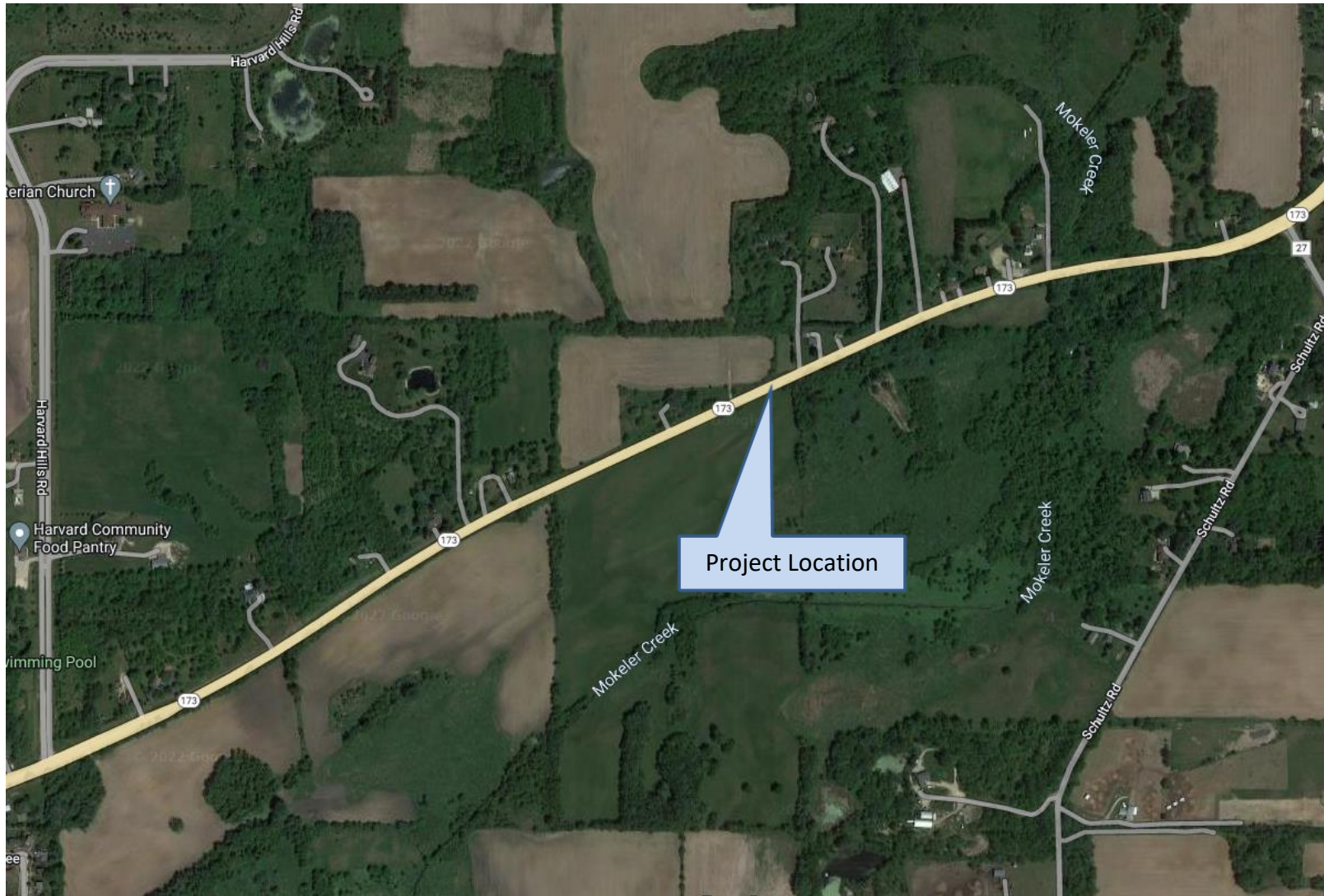


**Appendix A**

Site Location Map

Borehole Location Plan and Profiles

Soil Boring Logs



**SITE LOCATION MAP**  
IL 173 BOX CULVERT  
STRUCTURE NO: 056-0202  
MCHENRY COUNTY, ILLINOIS  
INTERRA Project No. 9244



**BOREHOLE LOCATION PLAN**  
IL 173 BOX CULVERT  
STRUCTURE NO: 056-0202  
MCHENRY COUNTY, ILLINOIS  
INTERRA Project No. 9244



**BOREHOLE LOCATION PLAN**  
IL 173 BOX CULVERT  
STRUCTURE NO: 056-0202  
MCHENRY COUNTY, ILLINOIS  
INTERRA Project No. 9244



# SOIL BORING LOG

Date 8/25/22

ROUTE IL-173 DESCRIPTION IL-173 Box Culvert LOGGED BY A. Boland

SECTION LOCATION 2098808.444,916354.429

COUNTY McHenry DRILLING METHOD Hollow Stem Auger HAMMER TYPE Automatic

STRUCT. NO. 056-0202  
Station 79+80

BORING NO. IL-173-BCB-01  
Station  
Offset  
Ground Surface Elev. 964.58 ft

DEPTH (ft)	BLOW S (1/6")	UCS (tsf)	MOIST (%)	Surface Water Elev. ft	Stream Bed Elev. ft	DEPTH (ft)	BLOW S (1/6")	UCS (tsf)	MOIST (%)
964.25									
963.67									
	4						6		
	2		15.6				7		10.6
	3	1.5 P					7		
				941.58					
	7						4		
	8		14.6				14		15.1
	6						28		
959.08									
	2						5		
	2		8.1				4		13.0
	3						6	1.5 P	
956.58									
	3								
	3		16.4						11.4
	4	0.5 P						1.9 B	
				934.58					
954.08									
	6								
	8		10.7						
	8								
951.58									
	6								
	9		8.3						
	10								
	6								
	7		11.3						
	8								
	5								
	6		15.5						
	7								

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)



# SOIL BORING LOG

Date 8/25/22

ROUTE IL-173 DESCRIPTION IL-173 Box Culvert LOGGED BY A. Boland

SECTION \_\_\_\_\_ LOCATION 2098825.830,916326.065

COUNTY McHenry DRILLING METHOD Hollow Stem Auger HAMMER TYPE Automatic

STRUCT. NO. 056-0202  
Station 79+80

BORING NO. IL-173-BCB-02  
Station \_\_\_\_\_  
Offset \_\_\_\_\_  
Ground Surface Elev. 964.70 ft

DEPTH (ft)	BLOW COUNT (/6")	UCS (tsf)	MOISTURE (%)	Surface Water Elev. ft	Stream Bed Elev. ft	DEPTH (ft)	BLOW COUNT (/6")	UCS (tsf)	MOISTURE (%)
964.37									
963.87									
961.70	4						7		
	3		13.5				12		11.9
	3	0.5 P					20		
941.70									
	3						2		
	1		9.9				4		12.6
	-5						-25	1.8 B	
	3						3		
	5		9.4				4		12.3
	5						6	1.5 B	
936.70									
	8								
	15		10.8						10.6
	-10						-30	3.0 B	
954.20									
	5								
	6		6.3						
	6								
	5								
	5		9.7						
	-15						-35		
	10								
	6		10.3						
	7								
	11								
	12		10.9						
	19								
-20							-40		

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)

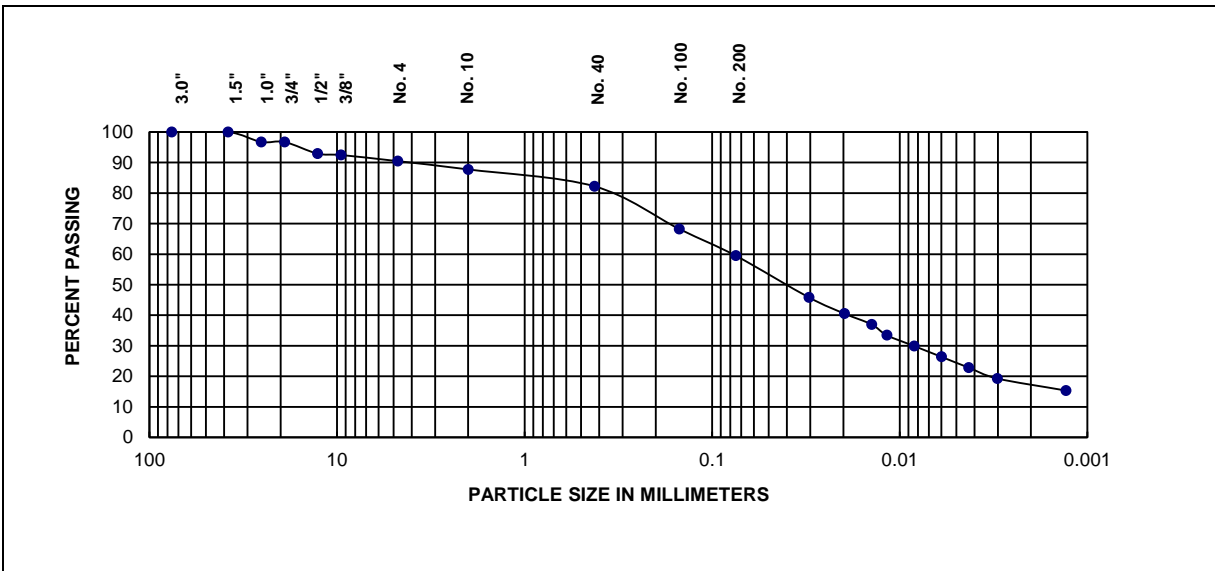


**Appendix B**  
Laboratory Test Reports



**GRAIN SIZE ANALYSIS  
AASHTO T 88**

<b>Project</b>	Geotechnical Investigation, Box Culvert at IL 173 and IL 176, PTB 195-016-WO 24, Lake County, IL						
<b>Client</b>	Bowman Consulting, 1001 Warrenville Road, Ste. 110, Lisle, IL 60532						
<b>File No.</b>	9244	<b>Sample #</b>	IL173 BCB 01-ST-12	<b>Date Tested</b>	8/31/2022	<b>Tested by</b>	BKP
						<b>Qc by</b>	AB
<b>Date Sample Received:</b>	8/25/2022						
<b>Sample Location</b>	28' - 30'						
<b>Sample Description</b>	Brown sandy loam, little gravel						



% + 3"	% Gravel	% Sand	Fines	
			% Silt	% Clay
0.0	12.2	28.3	41.6	17.9

For coarse-grained soils with <12% Fines	D60(mm)	D30(mm)	D10(mm)	Cu	Cc

Sieve Size	Percent Passing	Liquid Limit, L <sub>L</sub>	Plastic Limit, PL	Plasticity Index, PI
3.0"	100.0	19	11	8
1.5"	100.0			
1.0"	96.7	<b>AASHTO Classification:</b>  <b>IDH Classification:</b>		A-4(2)  Sandy Loam
3/4"	96.7			
1/2"	92.9			
3/8"	92.5			
No. 4	90.5			
No. 10	87.8			
No. 40	82.2			
No. 100	68.3			
No. 200	59.5			

<b>Remarks:</b>	

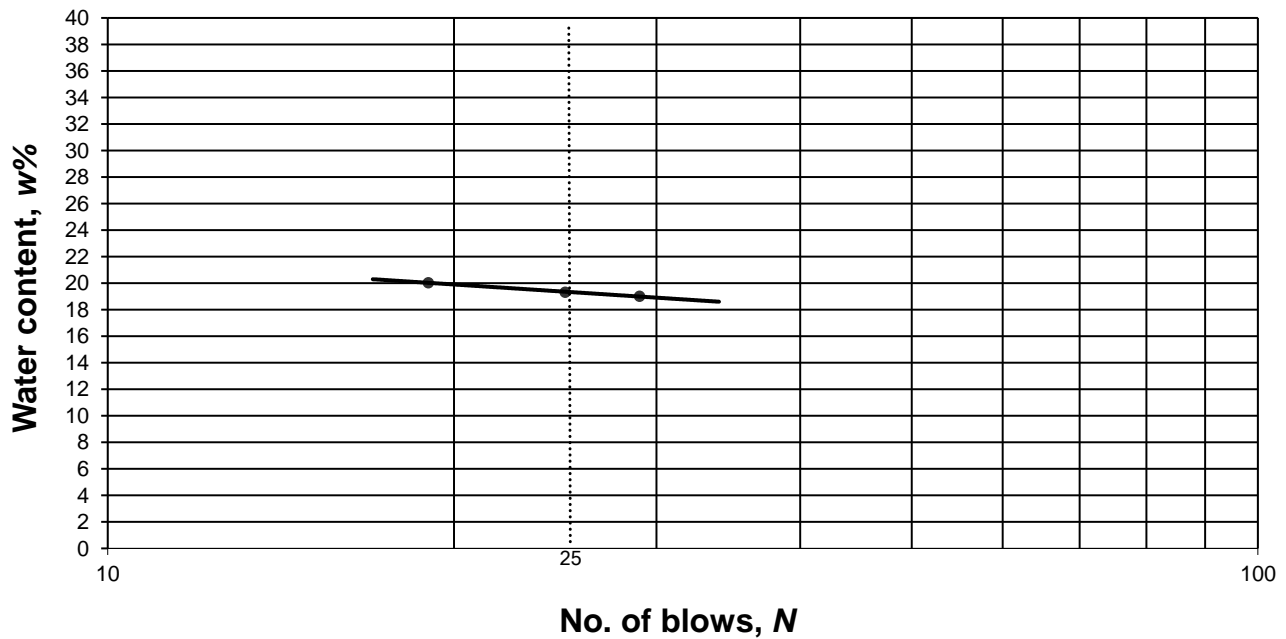


Atterberg Limits  
AAASHTO T 89,90

<b>Project</b>	Geotechnical Investigation, Box Culvert at IL 173 and IL 176, PTB 195-016-WO 24, Lake County, IL						
<b>Client</b>	Bowman Consulting, 1001 Warrenville Road, Ste. 110, Lisle, IL 60532						
<b>File No.</b>	9244	<b>Sample #</b>	IL173 BCB 01-ST-12	<b>Date Tested</b>	9/5/2022	<b>Tested By</b>	DG
						<b>Qc By</b>	AB

<b>Date Sample Recd.</b>	8/25/2022
<b>Sample Location</b>	28' - 30'
<b>Sample Description</b>	Brown sandy loam, little gravel

### LIQUID LIMIT DETERMINATION



<b>Results</b>					
<b>Liquid Limit, LL</b>	19	<b>Plastic Limit, PL</b>	11	<b>Plasticity Index, PI</b>	8

<b>Remarks</b>	
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**Moisture Content**  
AASHTO T265

<b>Project</b>	Geotechnical Investigation, Box Culvert at IL 173 and IL 176, PTB 195-016-WO 24, Lake County, IL						
<b>Client</b>	Bowman Consulting, 1001 Warrenville Road, Ste. 110, Lisle, IL 60532						
<b>File No.</b>	9244	<b>Sample #</b>	IL173 BCB 01-ST-12	<b>Date Tested</b>	8/29/2022	<b>Tested By</b>	AB
						<b>Qc By</b>	RC

<b>Date Sample Received</b>	8/25/2022
<b>Sample Location</b>	28' - 30'
<b>Sample Description</b>	Brown sandy loam, little gravel
<p>Can Number : 51-A</p> <p>Can Weight : 30.12 gm</p> <p>Can + Wet Sample Weight : 155.80 gm</p> <p>Can + Dry Sample Weight : 142.98 gm</p> <p>Moisture Content : <b>11.36</b> %</p>	

<b>Remarks</b>	
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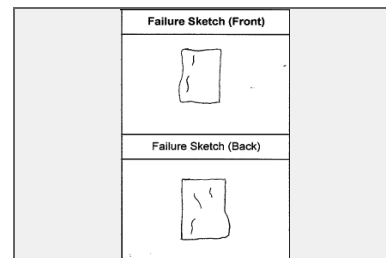


**UNCONFINED COMPRESSIVE STRENGTH (ASTM D 2166)**

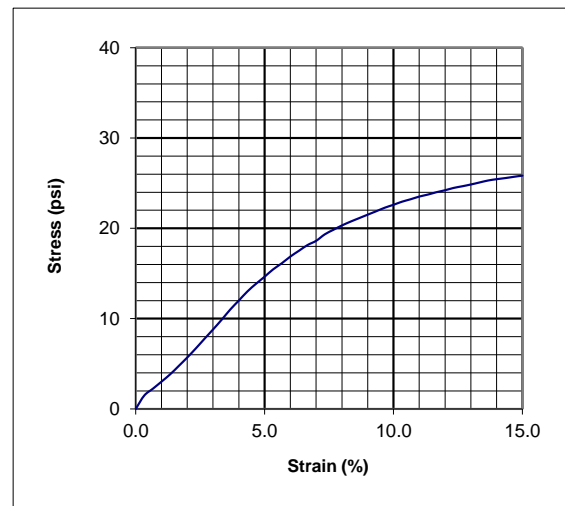
<b>Project</b>	Geotechnical Investigation, Box Culvert at IL 173 and IL 176, PTB 195-016-WO 24, Lake County, IL						
<b>Client</b>	Bowman Consulting, 1001 Warrenville Road, Ste. 110, Lisle, IL 60532						
<b>File No.</b>	9244	<b>Sample No.</b>	IL173 BCB 01-ST-12	<b>Date Tested</b>	8/29/22	<b>Tested By</b>	AB
						<b>QC By</b>	RC

<b>Date Sample Received</b>	8/25/22
<b>Description of Soil</b>	Brown sandy loam, little gravel
<b>Location</b>	28' - 30'

Type of Sample	ST
Average Height =	15.24 cm
Average Diameter =	7.19 cm
Height/Diameter Ratio =	2.12
Wet Sample Weight=	142.98 g
Wet Density =	0.23 g/cc
Moisture Content =	11.6 %
Dry Density =	0.21 g/cc
Strain Rate =	1.00 %/min



Failure Image



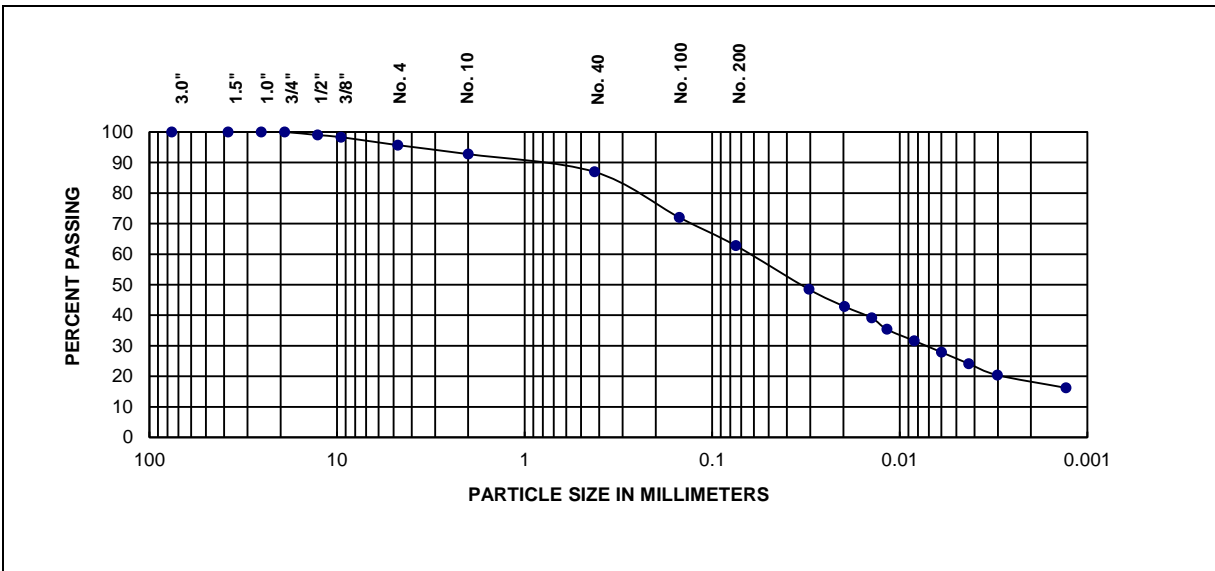
<b>Unconfined Compressive Strength =</b>	25.84 psi
	<b>1.86 tsf</b>
<b>Shear Strength =</b>	12.92 psi
	0.93 tsf
<b>Strain at Failure =</b>	15.0 %

Remarks:



**GRAIN SIZE ANALYSIS  
AASHTO T 88**

<b>Project</b>	Geotechnical Investigation, Box Culvert at IL 173 and IL 176, PTB 195-016-WO 24, Lake County, IL						
<b>Client</b>	Bowman Consulting, 1001 Warrenville Road, Ste. 110, Lisle, IL 60532						
<b>File No.</b>	9244	<b>Sample #</b>	IL173 BCB 02-ST-12	<b>Date Tested</b>	8/31/2022	<b>Tested by</b>	BKP
						<b>Qc by</b>	AB
<b>Date Sample Received:</b>	8/25/2022						
<b>Sample Location</b>	28' - 30'						
<b>Sample Description</b>	Brown loam, trace gravel						



% + 3"	% Gravel	% Sand	Fines	
			% Silt	% Clay
0.0	7.2	30.0	43.9	18.9

For coarse-grained soils with <12% Fines	D60(mm)	D30(mm)	D10(mm)	Cu	Cc

Sieve Size	Percent Passing	Liquid Limit, L <sub>L</sub>	Plastic Limit, PL	Plasticity Index, PI
3.0"	100.0	19	11	8
1.5"	100.0			
1.0"	100.0			
3/4"	100.0	<b>AASHTO Classification:</b>		A-4(2)
1/2"	99.0	<b>IDH Classification:</b>		Loam
3/8"	98.3			
No. 4	95.7			
No. 10	92.8			
No. 40	87.0			
No. 100	72.0			
No. 200	62.8			

Remarks:

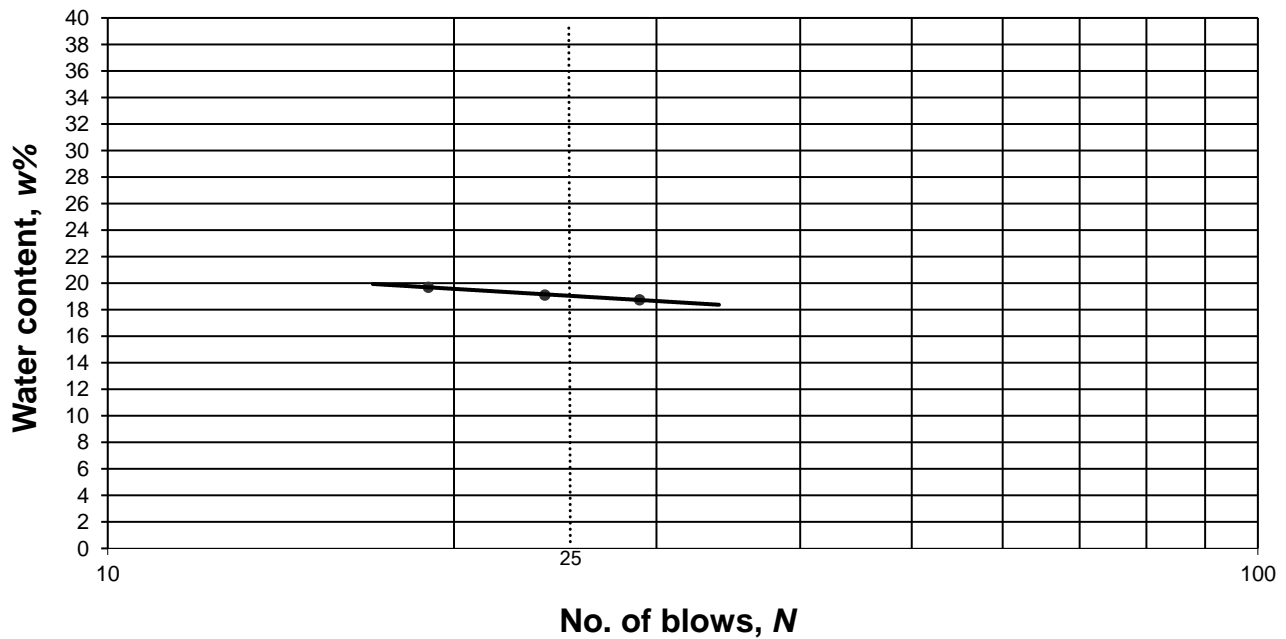


Atterberg Limits  
AAASHTO T 89,90

<b>Project</b>	Geotechnical Investigation, Box Culvert at IL 173 and IL 176, PTB 195-016-WO 24, Lake County, IL						
<b>Client</b>	Bowman Consulting, 1001 Warrenville Road, Ste. 110, Lisle, IL 60532						
<b>File No.</b>	9244	<b>Sample #</b>	IL173 BCB 02-ST-12	<b>Date Tested</b>	9/5/2022	<b>Tested By</b>	DG
						<b>Qc By</b>	AB

<b>Date Sample Recd.</b>	8/25/2022
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### LIQUID LIMIT DETERMINATION



<b>Results</b>					
<b>Liquid Limit, LL</b>	19	<b>Plastic Limit, PL</b>	11	<b>Plasticity Index, PI</b>	8

<b>Remarks</b>	
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**Moisture Content**  
AASHTO T265

<b>Project</b>	Geotechnical Investigation, Box Culvert at IL 173 and IL 176, PTB 195-016-WO 24, Lake County, IL						
<b>Client</b>	Bowman Consulting, 1001 Warrenville Road, Ste. 110, Lisle, IL 60532						
<b>File No.</b>	9244	<b>Sample #</b>	IL173 BCB 02-ST-12	<b>Date Tested</b>	8/29/2022	<b>Tested By</b>	AB
						<b>Qc By</b>	RC

<b>Date Sample Received</b>	8/25/2022
<b>Sample Location</b>	28' - 30'
<b>Sample Description</b>	Brown loam, trace gravel
<p>Can Number : 56-A</p> <p>Can Weight : 30.25 gm</p> <p>Can + Wet Sample Weight : 112.35 gm</p> <p>Can + Dry Sample Weight : 104.50 gm</p> <p>Moisture Content : <b>10.57</b> %</p>	

<b>Remarks</b>	
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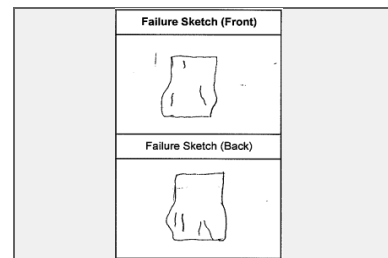


**UNCONFINED COMPRESSIVE STRENGTH (ASTM D 2166)**

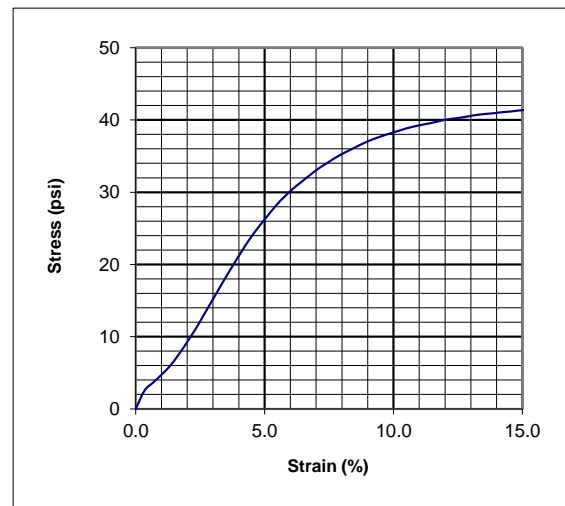
<b>Project</b>	Geotechnical Investigation, Box Culvert at IL 173 and IL 176, PTB 195-016-WO 24, Lake County, IL						
<b>Client</b>	Bowman Consulting, 1001 Warrenville Road, Ste. 110, Lisle, IL 60532						
<b>File No.</b>	9244	<b>Sample No.</b>	IL173 BCB 02-ST-12	<b>Date Tested</b>	8/29/22	<b>Tested By</b>	AB
						<b>QC By</b>	RC

<b>Date Sample Received</b>	8/25/22
<b>Description of Soil</b>	Brown loam, trace gravel
<b>Location</b>	28' - 30'

Type of Sample	ST	
Average Height =	14.99	cm
Average Diameter =	7.19	cm
Height/Diameter Ratio =	2.08	
Wet Sample Weight=	1428.79	g
Wet Density =	2.35	g/cc
Moisture Content =	10.8	%
Dry Density =	2.12	g/cc
Strain Rate =	1.00	%/min



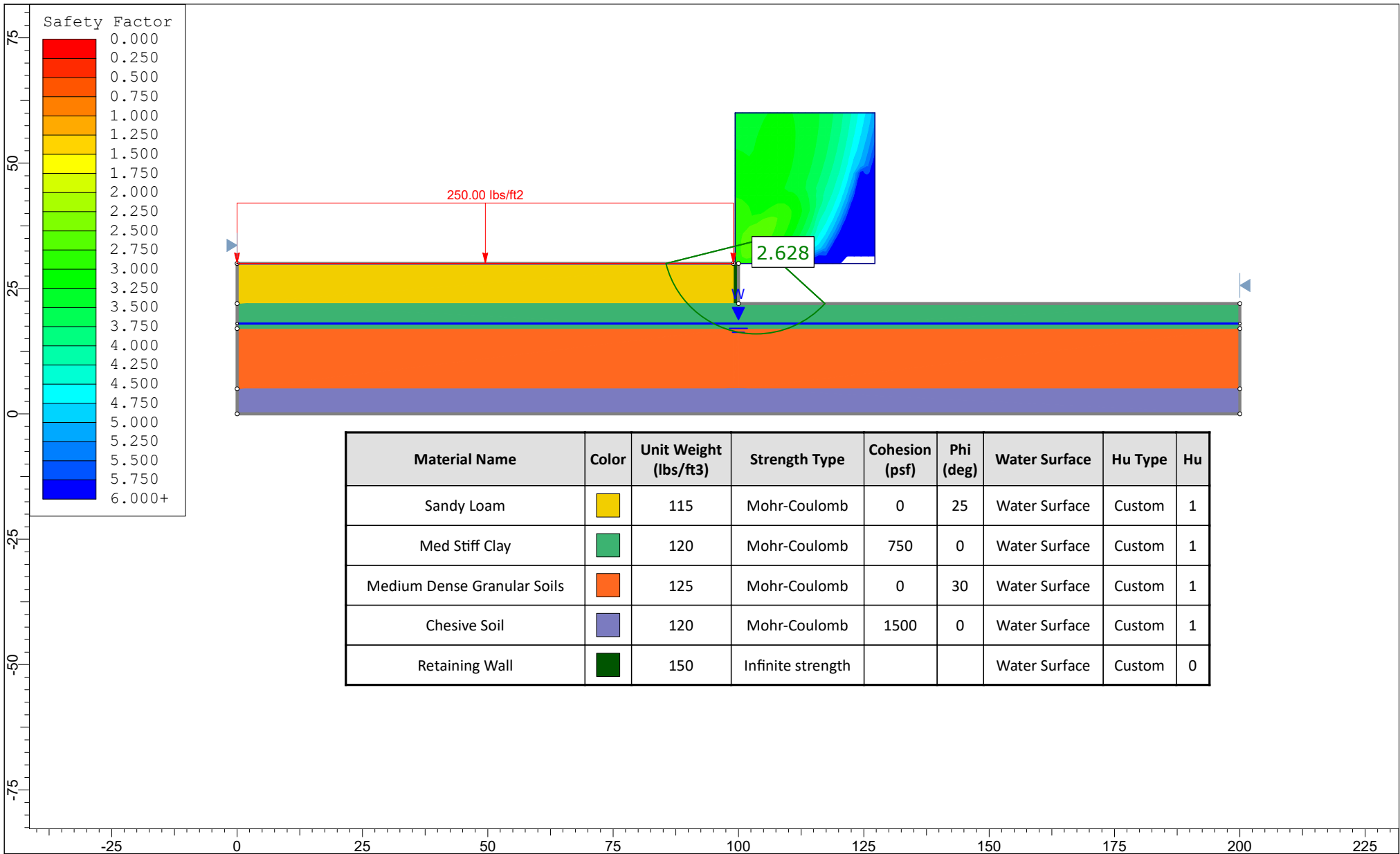
Failure Image









<b>Unconfined Compressive Strength =</b>	41.40 psi
	<b>2.98 tsf</b>
<b>Shear Strength =</b>	20.70 psi
	1.49 tsf
<b>Strain at Failure =</b>	15.3 %

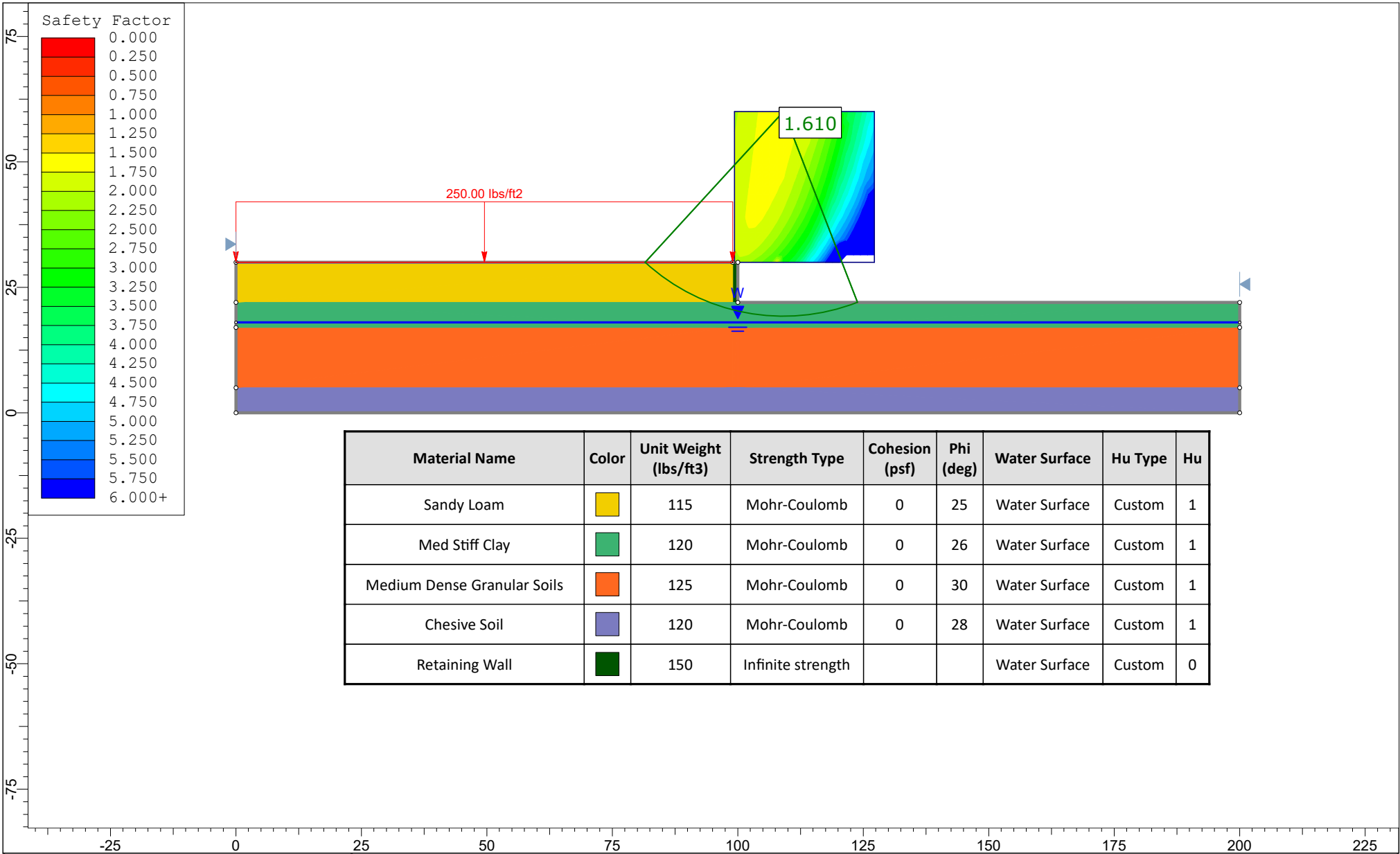
Remarks:






**Appendix C**  
Slope Stability Analyses




Material Name	Color	Unit Weight (lbs/ft3)	Strength Type	Cohesion (psf)	Phi (deg)	Water Surface	Hu Type	Hu
Sandy Loam		115	Mohr-Coulomb	0	25	Water Surface	Custom	1
Med Stiff Clay		120	Mohr-Coulomb	750	0	Water Surface	Custom	1
Medium Dense Granular Soils		125	Mohr-Coulomb	0	30	Water Surface	Custom	1
Chesive Soil		120	Mohr-Coulomb	1500	0	Water Surface	Custom	1
Retaining Wall		150	Infinite strength			Water Surface	Custom	0

	Project			Box Culvert Wing Wall-IL 173			
	Analysis Description			Global Stability Analysis-Short Term			
	Drawn By	Scale	Company	1:318			INTERRA, INC.
	Date	10/12/22		Retaining Wall-Short-Term Stability.slim			



Material Name	Color	Unit Weight (lbs/ft3)	Strength Type	Cohesion (psf)	Phi (deg)	Water Surface	Hu Type	Hu
Sandy Loam		115	Mohr-Coulomb	0	25	Water Surface	Custom	1
Med Stiff Clay		120	Mohr-Coulomb	0	26	Water Surface	Custom	1
Medium Dense Granular Soils		125	Mohr-Coulomb	0	30	Water Surface	Custom	1
Chesive Soil		120	Mohr-Coulomb	0	28	Water Surface	Custom	1
Retaining Wall		150	Infinite strength			Water Surface	Custom	0

	Project		
	Box Culvert Wing Wall-IL 173		
	Analysis Description		
	Global Stability Analysis-Long Term		
Drawn By	Scale	Company	
	1:318	INTERRA, INC.	
Date			
10/12/22			Retaining Wall-Long-Term Stability.slim