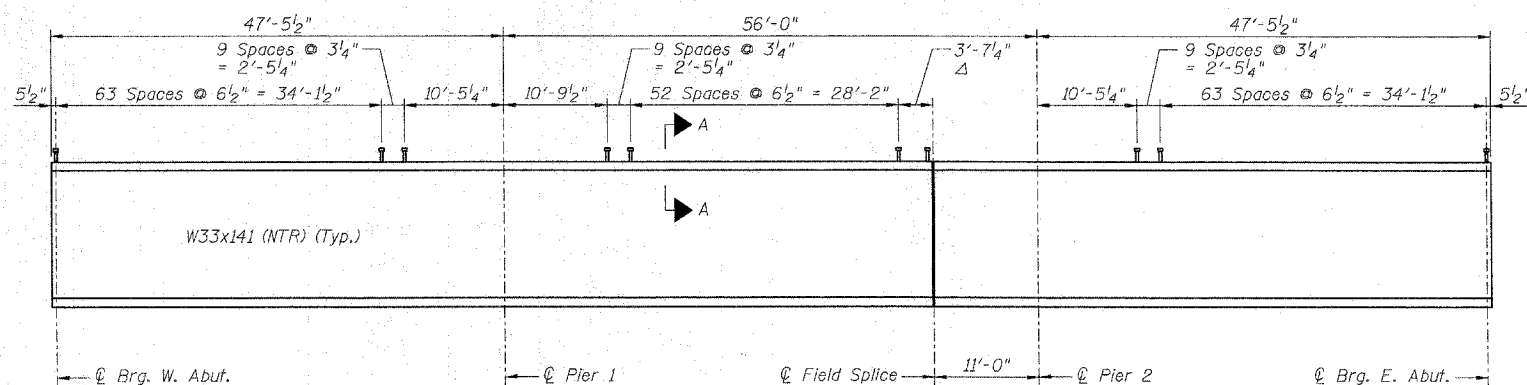


Contract #64B07



PROPOSED BEAM 1 & 12 ELEVATION

△ See Splice Detail
"NTR" denotes beams to which notch toughness requirements are applicable
Note: Shear stud spacing shown is to be used on both existing and new beams.

INTERIOR GIRDER MOMENT TABLE				
		0.4 Sp. 1 or 0.6 Sp. 3	Pier	0.5 Sp. 2
I_s	(in ⁴)	7450	7450	7450
$I_o(n)$	(in ⁴)	19305	-	19305
$I_o(3n)$	(in ⁴)	14260	-	14260
S_s	(in ³)	448	448	448
$S_o(n)$	(in ³)	640	-	640
$S_o(3n)$	(in ³)	580	-	580
Z	(in ³)	-	-	-
ρ	(k/')	0.90	1.05	0.90
$M \rho$	(k)	143	268	115
$s \rho$	(k/')	0.15	-	0.15
$M_s \rho$	(k)	27	-	27
$M \bar{L}$	(k)	337	189	342
M_{imp}	(k)	98	53	94
M_a	(k)	1164	872	1130
M_u	(k)	1834	-	1850
$f_s \rho$ non-comp	(ksi)	3.9	7.3	3.1
$f_s \rho$ comp	(ksi)	0.6	-	0.6
$f_s [M \bar{L} + M_{imp}]$	(ksi)	13.6	10.9	13.6
f_s (Overload)	(ksi)	18.1	18.2	17.3
f_s (Total)	(ksi)	-	23.7	-
VR	(k)	38.3	-	39.9

I_s, S_s : Non-composite moment of inertia and section modulus of the steel section used for computing f_s (Total and Overload) due to non-composite dead loads (in⁴ and in³).
 $I_o(n), S_o(n)$: Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing f_s (Total and Overload) due to short-term composite live loads (in⁴ and in³).
 $I_o(3n), S_o(3n)$: Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing f_s (Total and Overload) due to long-term composite (superimposed) dead loads (in⁴ and in³).
Z: Plastic Section Modulus of the steel section in non-composite areas (in³).
 ρ : Un-factored non-composite dead load (kips/ft.).
 $M \rho$: Un-factored moment due to non-composite dead load (kip-ft.).
 $s \rho$: Un-factored long-term composite (superimposed) dead load (kips/ft.).
 $M_s \rho$: Un-factored moment due to long-term composite (superimposed) dead load (kip-ft.).
 $M \bar{L}$: Un-factored live load moment (kip-ft.).
 M_{imp} : Un-factored moment due to impact (kip-ft.).
 M_a : Factored design moment (kip-ft.).
 M_u : Compact composite moment capacity according to AASHTO LFD 10.50.1.1 or compact non-composite moment capacity according to AASHTO LFD 10.48.1 (kip-ft.).
 f_s (Overload): Sum of stresses as computed from the moments below (ksi).
 f_s (Total): Sum of stresses as computed from the moments below on non-compact section (ksi).
VR: Maximum \bar{L} + impact horizontal shear range within the composite portion of the span for stud shear connector design (kips).

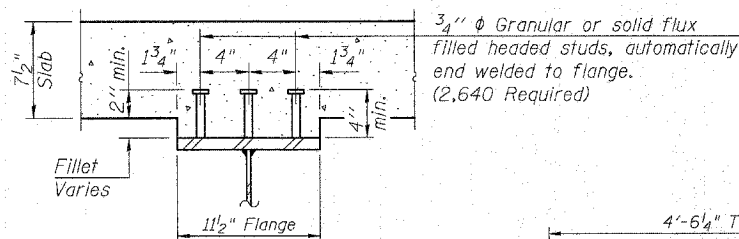
TOP OF BEAM ELEVATIONS

Location/Beam No.	1	12
Brg. W. Abut.	764.48	764.01
Pier 1	763.96	763.60
Field Splice	763.46	763.21
Pier 2	763.37	763.12
Brg. E. Abut.	762.98	762.72

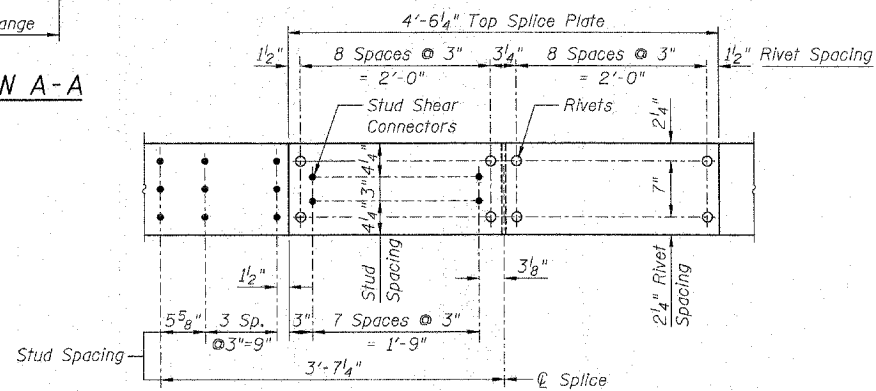
For fabrication only

INTERIOR GIRDER REACTION TABLE			
	Abut.	Pier	
R ρ	(k)	18.8	59.6
R \bar{L}	(k)	38.1	45.3
Imp.	(k)	11.1	12.8
R Total	(k)	68.0	117.7

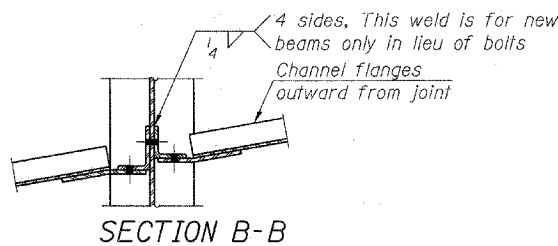
* Compact section
** Braced non-compact and partially braced section



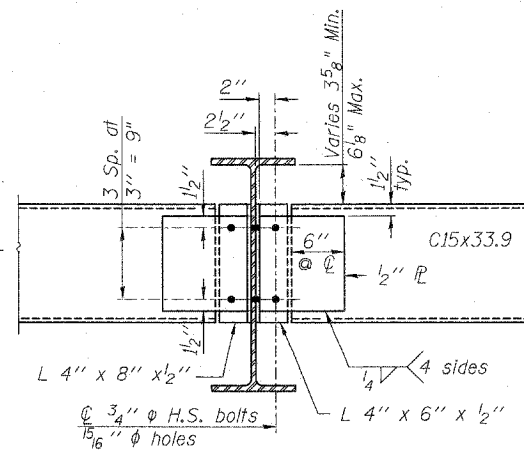
SECTION A-A



EXISTING SPLICE DETAIL



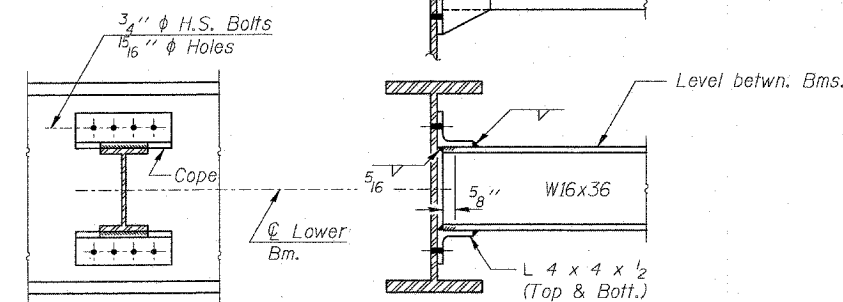
SECTION B-B



END DIAPHRAGM D

(20 Required)

Notes:
Two hardened washers required for each set of oversized holes.
Existing angles welded to existing beams to be removed using the air-arc method.
Bolt holes for proposed diaphragm connection to be field drilled in the existing beam using the proposed connection angle as the template. Cost included with Furnishing and Erecting Structural Steel.



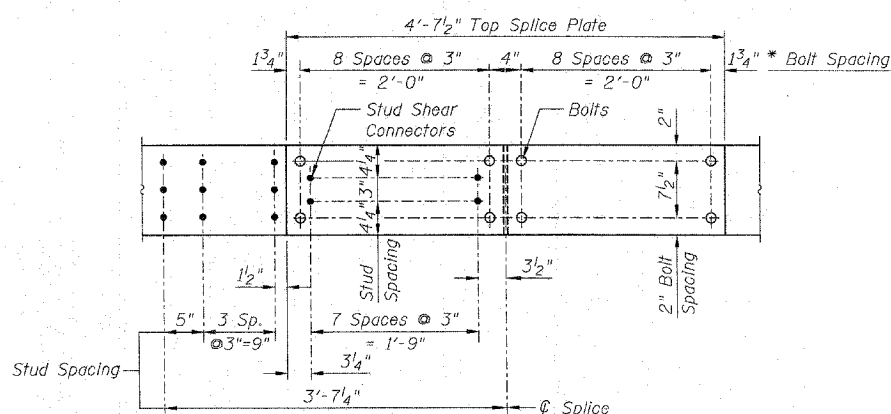
DIAPHRAGM D1

(12 Required)

Note:
Two hardened washers shall be required over all oversized holes for diaphragms.
Bolt holes for proposed diaphragm connection to be field drilled in the existing beam using the proposed connection angle as the template. Cost included with Furnishing and Erecting Structural Steel.

DESIGNED	LAS
CHECKED	DAZ
DRAWN	SAW
CHECKED	LAS

BEAM 1 & 12 SPLICE DETAIL



STRUCTURAL STEEL DETAILS

F.A.P. ROUTE 301 (US 20)

OVER PRAIRIE ROAD

SECTION (2HB-2)D

WINNEBAGO COUNTY

STATION 841+89.60

STRUCTURE NO. 101-0051 (W.B.)

STRUCTURE NO. 101-0052 (E.B.)