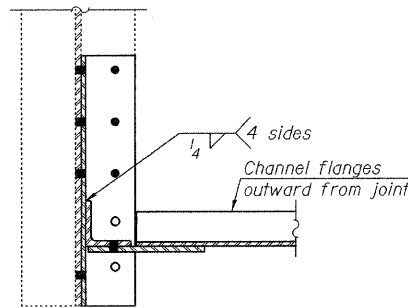
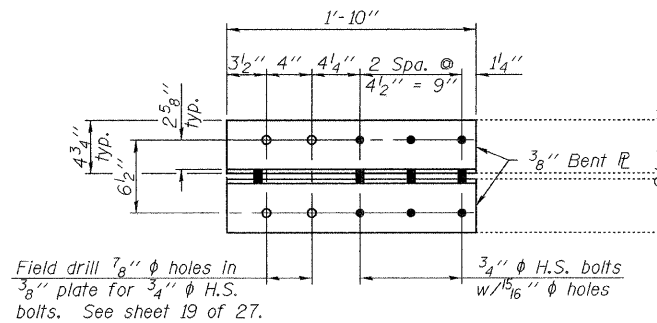


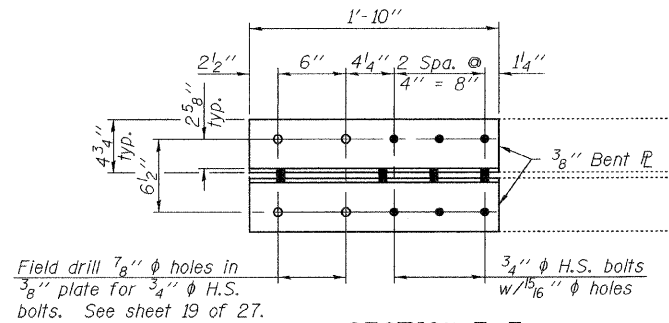
STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION



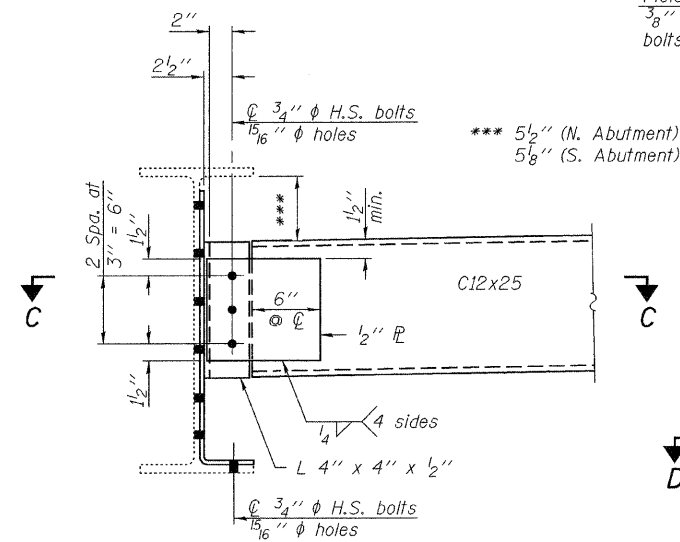
SECTION C-C



SECTION D-D

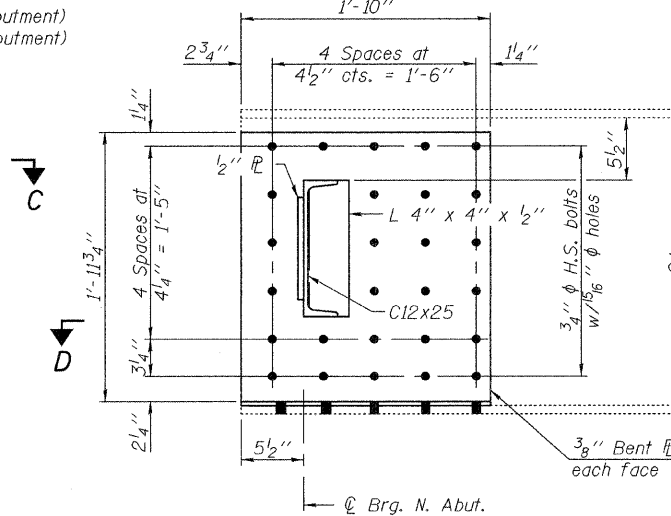


SECTION E-E

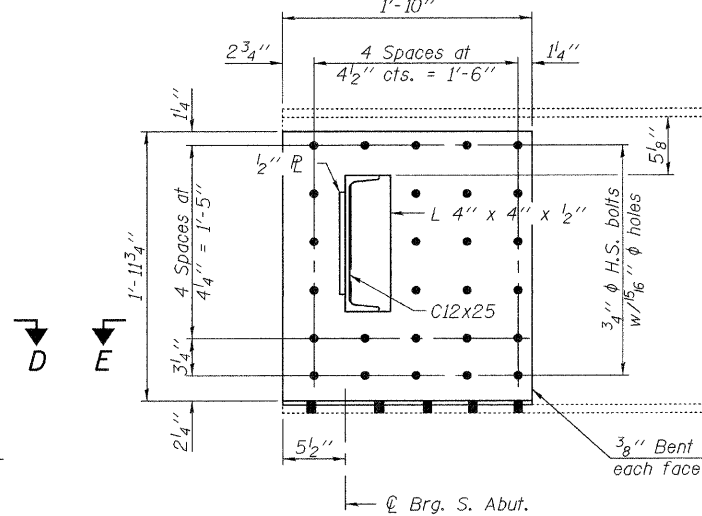


DIAPHRAGM D

Note:  
Two hardened washers required for each set of oversized holes.



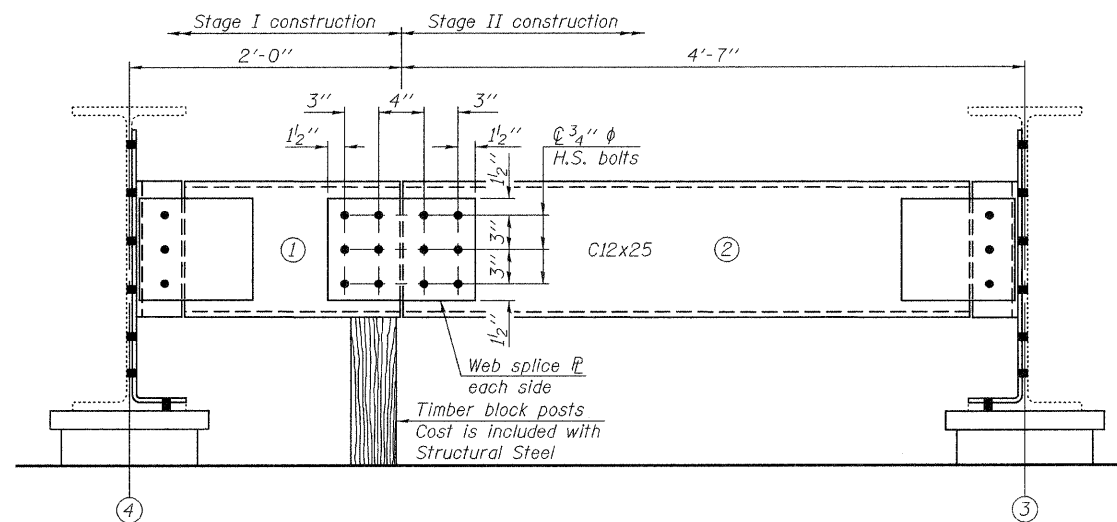
NORTH END OF  
BEAM ELEVATION



SOUTH END OF  
BEAM ELEVATION

END DIAPHRAGM STAGE  
CONSTRUCTION SEQUENCE

- 1.) Order diaphragm in two sections.
- 2.) Attach section ① of diaphragm to beam (See Diaphragm D for connection).
- 3.) Place timber block posts between section ① of diaphragm and abutment bearing section.
- 4.) Attach section ② of diaphragm to both beam (See Diaphragm D for connection) and section ① of diaphragm during stage II construction with splice plates.
- 5.) Remove timber block posts.



DIAPHRAGM D1

(North diaphragm D1 looking South, South diaphragm D1 similar)

INTERIOR BEAM MOMENT TABLE			
	0.4 Sp. 1 or 0.6 Sp. 3	Pier 1 or Pier 2	0.5 Sp. 2
$I_s$	(in <sup>4</sup> ) 3270	3270	3270
$I_c(n)$	(in <sup>4</sup> ) 10045	-	10045
$I_c(3n)$	(in <sup>4</sup> ) 7488	-	7488
$S_s$	(in <sup>3</sup> ) 243	243	243
$S_c(n)$	(in <sup>3</sup> ) 382	-	382
$S_c(3n)$	(in <sup>3</sup> ) 345	-	345
$\phi$	(k/')	1.075	0.781
$M_D$	(k)	201.6	70.7
$s_D$	(k/')	-	0.294
$M_{sD}$	(k)	-	41.7
$M_L$	(k)	122.2	253.2
$M_{IM}$	(k)	36.0	73.0
$S_3 [M_L + i]$	(k)	263.7	543.7
$M_o$	(k)	604.9	852.9
$M_u$	(k)	-	1115.6
$f_s \phi$ non-comp	(ksi)	10.0	3.5
$f_s \phi$ (comp)	(ksi)	-	1.5
$f_s S_3 [M_L + M_I]$	(ksi)	13.0	17.1
$f_s$ (Overload)	(ksi)	23.0	22.1
$f_s$ (Total)	(ksi)	29.9	-
VR	(k)	-	37.5

INTERIOR BEAM REACTION TABLE		
	Abut.	Pier
$R_D$	(k) 17.3	53.0
$R_L$	(k) 32.2	39.1
$R_I$	(k) 9.7	11.8
$R_{Total}$	(k) 59.2	103.9

\* Compact section  
\*\* Braced non-compact and partially braced section

$I_s, S_s$ : Non-composite moment of inertia and section modulus of the steel section used for computing  $f_s$  (Total and Overload) due to non-composite dead loads (in.4 and in.3).  
 $I_c(n), S_c(n)$ : Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing  $f_s$  (Total and Overload) due to short-term composite live loads (in.4 and in.3).  
 $I_c(3n), S_c(3n)$ : Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing  $f_s$  (Total and Overload) due to long-term composite (superimposed) dead loads (in.4 and in.3).  
 $\phi$ : Un-factored non-composite dead load (kips/ft.).  
 $M_D$ : Un-factored moment due to non-composite dead load (kip-ft.).  
 $s_D$ : Un-factored long-term composite (superimposed) dead load (kips/ft.).  
 $M_{sD}$ : Un-factored moment due to long-term composite (superimposed) dead load (kip-ft.).  
 $M_L$ : Un-factored live load moment (kip-ft.).  
 $M_I$ : Un-factored moment due to impact (kip-ft.).  
 $M_o$ : Factored design moment (kip-ft.).  
 $1.3 [M_D + M_{sD} + \frac{5}{8} (M_L + M_I)]$   
 $M_u$ : Compact composite moment capacity according to AASHTO LFD 10.50.1.1 or compact non-composite moment capacity according to AASHTO LFD 10.48.1 (kip-ft.).  
 $f_s$  (Overload): Sum of stresses as computed from the moments below (ksi).  
 $M_D + M_{sD} + \frac{5}{8} (M_L + M_I)$   
 $f_s$  (Total): Sum of stresses as computed from the moments below on non-compact section (ksi).  
 $1.3 [M_D + M_{sD} + \frac{5}{8} (M_L + M_I)]$   
 VR: Maximum + impact horizontal shear range within the composite portion of the span for stud shear connector design (kips).

STRUCTURAL STEEL DETAILS  
STRUCTURE NO. 037-0018 (N.B.)

DESIGNED	Michael D. Rolape
CHECKED	Nicholas R. Barnett
DRAWN	Michael B. Mossman
CHECKED	M.D.R./N.R.B./G.R.A.

EXAMINED	September 29, 2009	Thomas J. Damagalki
PASSED		Ralph E. Anderson

SHEET NO. 18	F.A.I. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
27 SHEETS	74	37-4HB-1	HENRY	148	111
			CONTRACT NO. 64264		
ILLINOIS FED. AID PROJECT					