

# Roadway Geotechnical Report

IDOT PTB 163-017  
IL 171 and 95<sup>th</sup> Street  
Willow Springs, Illinois

Prepared for



Illinois Department of Transportation  
Contract Number: 60R94

Project Design Engineer Team:  
Ames Engineering, Inc.

Geotechnical Consultant:



November 4, 2024



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November 4, 2024

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Roadway Geotechnical Report  
IL 171 and 95th Street, Willow Springs, IL  
IDOT PTB 163-017

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Dear Mr. Regis:

Attached is a copy of the Roadway Geotechnical Report for the above referenced project. The report provides a description of the site investigation, site conditions and construction recommendations for the proposed improvements. The site investigation included advancing thirty nine (39) soil borings to depths ranging from 10 to 40 feet.

Should you have any questions or require additional information, please call us at 630-994-2600.

Sincerely,

A handwritten signature in blue ink, appearing to read "Min Zhang".

Min Zhang, P.E.  
Sr. Project Engineer

A handwritten signature in blue ink, appearing to read "Ala E Sassila".

Ala E Sassila, Ph.D., P.E.  
Principal

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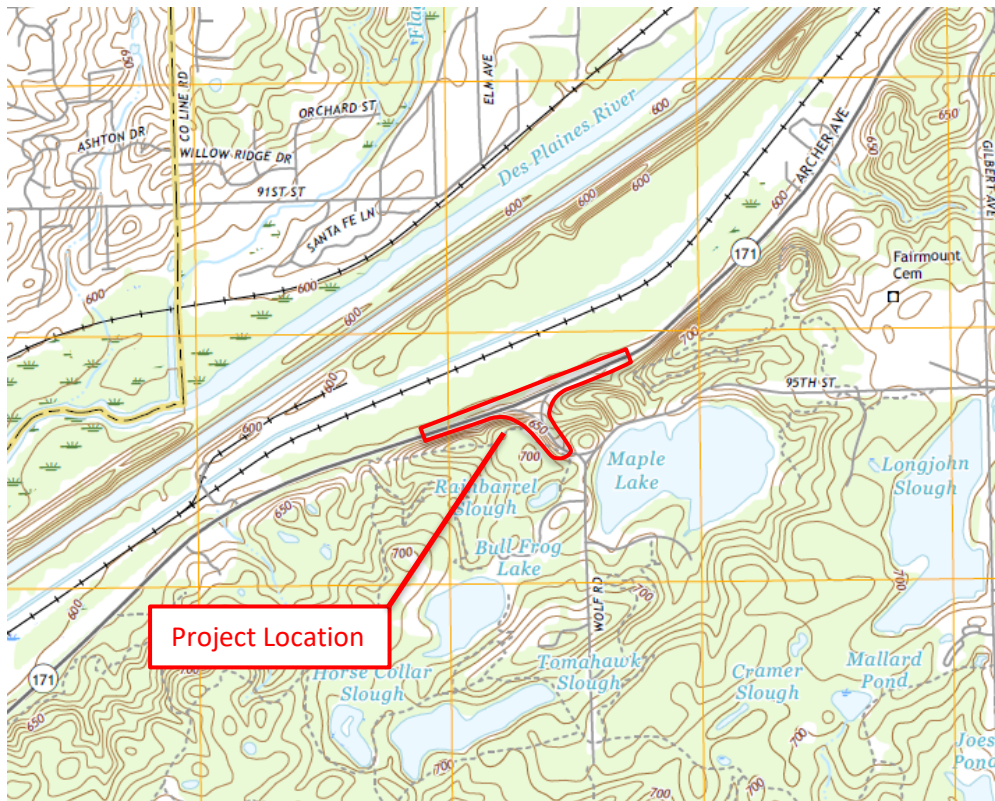
### **Appendices**

Appendix A	General Plans, Elevations, and Details
Appendix B	Soil Boring Location Plan and Subsurface Profile
Appendix C	Soil Boring Logs
Appendix D	Laboratory Test Results
Appendix E	Slope Stability Analyses Exhibits
Appendix F	IDOT Highway Standard 878001-11

Roadway Geotechnical Report  
IL 171 and 95th Street  
Willow Springs, Illinois  
IDOT PTB 163-017

## 1.0 INTRODUCTION

GSG Consultants, Inc. (GSG) completed a subsurface investigation and geotechnical analysis for the construction of the proposed improvements along IL 171 at the intersection with 95<sup>th</sup> Street in Willow Springs, Illinois. The purpose of this site investigation was to explore the subsurface conditions along the proposed improvements limits, to determine engineering properties of the subsurface soil, and to develop design and construction recommendations for the project. **Exhibit 1** shows the general project location.



**Exhibit 1 – Project Location Map**  
(Source: USGS Topographic Maps, [usgs.gov](https://usgs.gov))

The general scope of the overall project is to raise the grade of IL 171 for a new intersection with 95<sup>th</sup> Street. The profile of IL 171 will be raised approximately 18 feet at the new realigned intersection. A retaining wall will be required along the northern right-of-way of IL 171 due to limited right-of-way available for slope reconfiguration. The remainder of the embankment will



be sloped away from the newly aligned 95<sup>th</sup> Street. The overall project will also include constructing one (1) new culvert, roadway improvements including new embankment construction, realigning the IL 171 and 95<sup>th</sup> Street intersection and new traffic signals at the intersection. The proposed retaining wall and culvert will be discussed in separate reports.

### 1.1 Proposed Roadway Information

Based on drawings (dated March 22, 2024) and design information (dated March 27, 2024) (**Appendix A**) provided by Collins Engineers, Inc. (Collins), the proposed project will include reconstructing and raising the profile grade of IL 171 near the intersection with 95<sup>th</sup> Street; realigning 95<sup>th</sup> Street to create a T-intersection with IL 171; and reconstructing and realigning the existing 95<sup>th</sup> Street ramps to IL 171. Subsequent to the road realignment, new traffic signals at the intersection of IL 171 and 95<sup>th</sup> Street will also be constructed. The improvements addressed in this report will include the following:

- Construction of IL 171 embankment from Station 316+00 to 335+00;
- Construction of 95<sup>th</sup> Street from Station 191+00 to 200+00;
- Traffic sign structures at the new intersection of IL 171 and 95<sup>th</sup> Street

The proposed IL 171 profile will have a new maximum embankment height of 18 feet, with the greatest fill height at the intersection with 95<sup>th</sup> Street. The new embankment will be constructed with a 3% grade. It is anticipated that along 95<sup>th</sup> Street between Station 191+00 and 197+00, the proposed profile will be relatively consistent with the existing roadway profile, and that minimal cut and fill (less than 3 feet) would be required. Between Station 197+00 and 200+00, it is anticipated that up to 18 feet of new fill will be required.

### 1.2 Site Geology

GSG reviewed several published documents to determine the regional geological setting in the area of the site. The site is in southwest Cook County, in Willow Springs, Illinois. The surficial deposits in this area are typically glacial drift deposited during the Wisconsin Glacial Age and sediments deposited by various high-level states of the Des Plaines River. The subsurface profile in the site consists of deposits of clay, gravel, sand, and silt extending to approximately 50 to 100 feet below ground surface, at which point bedrock is generally encountered. This is consistent with the soil borings completed. Underlying the surficial deposits, the bedrock consists of the Silurian System, Niagaran Series, which consists of almost entirely dolomite that varies from extremely argillaceous, silty and cherty to exceptionally pure.

### 1.3 Climatic Conditions

The geotechnical field exploration was performed between June 9 and 21, 2021. The climate conditions for the months of March to June are summarized in **Table 1**. The data in this table was obtained from the National Weather Service Forecast Office website for Chicago, Illinois and the surrounding area. The data was evaluated to determine any effects of temperature and precipitation on the water table level and soil moisture content that was encountered at the site at the time the borings were performed.

For the months included in the study, the precipitation average rate was higher in June, but below average in March through May. The average monthly temperatures were higher than the average in the months of March, April, and June, and was lower in May. It is our opinion that the climatic conditions for the site at the time the exploration was performed did not have a direct impact on the soil moisture contents or water table levels that were recorded during the field exploration.

**Table 1 – Climate Conditions**

Date (M-Y)	Precipitation (in.)		Temperature (F°)	
	Total	Departure	Average	Departure
March – 2021	1.25	-1.20	44.2	+5.2
April – 2021	0.71	-3.04	51.9	+2.2
May – 2021	1.79	-2.73	60.2	-0.4
June – 2021	6.78	2.68	74.3	+3.7

## 2.0 SITE SUBSURFACE EXPLORATION PROGRAM

This section describes the subsurface exploration program and laboratory testing program completed as part of this project. The proposed locations and depths of the soil borings were selected in accordance with IDOT requirements and review with Ames Engineering, Inc. (Ames) available design information at the time of the field activities. The borings were completed in the field based on field conditions and accessibility.

### 2.1 Subsurface Exploration Program

Soil borings were completed between June 9 and June 21, 2021. The exploration program included advancing twenty-seven (27) retaining wall borings (RWB) to depths between 14 and 40 feet. These borings were spaced approximately 75 feet apart along the length of the proposed IL 171 retaining wall. An additional seven (7) subgrade stability borings (SSB) were completed for the proposed embankment along IL 171 to depths between 10 and 15 feet. Three (3) subgrade borings (SGB) were completed along 95<sup>th</sup> Street to depths of 10 feet. At the proposed T-intersection of IL 171 and 95<sup>th</sup> Street, two (2) traffic sign borings (TSB) were completed to depths of 25 feet.

The coordinates and existing ground surface elevations shown on the soil boring logs were obtained by GSG using handheld surveying equipment. The coordinates and surface elevations of borings SSB-02, SGB-02, and SGB-03 were estimated using internet resources. The as-drilled locations of the soil borings are shown on the Soil Boring Location Map and Subsurface Profiles (**Appendix B**). **Table 2** presents a list of the borings used for the analysis for the proposed improvements.

**Table 2 - Summary of Borings**

Boring ID	Station*	Offset*	Northing	Easting	Depth (ft)	Surface Elevation (ft)
RWB-01	316+01.26	43.32 RT	1839443.234	1102341.754	20.0	611.6
RWB-02	316+84.34	43.02 RT	1839469.640	1102420.528	20.0	611.5
RWB-03	317+44.00	43.11 RT	1839488.306	1102477.187	20.0	612.0
RWB-04	318+08.19	42.74 RT	1839508.831	1102538.006	14.0**	612.0
RWB-05	318+80.90	38.55 RT	1839535.671	1102605.716	19.0**	612.4
RWB-06	319+63.02	29.88 RT	1839569.708	1102680.946	17.5**	612.0
RWB-07	320+28.98	29.59 RT	1839590.722	1102743.476	29.0	612.5

Boring ID	Station*	Offset*	Northing	Easting	Depth (ft)	Surface Elevation (ft)
RWB-08	321+11.99	36.09 RT	1839611.032	1102824.576	25.0	613.0
RWB-09	321+80.29	39.38 RT	1839630.595	1102890.575	20.5**	613.3
RWB-10	322+42.24	42.24 RT	1839653.739	1102962.597	30.0	613.4
RWB-11	323+30.65	41.78 RT	1839681.051	1103033.379	32.0**	613.6
RWB-12	324+04.38	39.86 RT	1839710.073	1103101.778	40.0	613.4
RWB-13	324+53.54	38.61 RT	1839729.882	1103147.158	35.0**	613.4
RWB-14	325+28.22	36.74 RT	1839760.709	1103215.753	40.0	612.4
RWB-15	326+03.57	34.52 RT	1839793.032	1103284.381	35.0	611.9
RWB-16	326+75.53	36.03 RT	1839820.826	1103350.769	35.0	612.1
RWB-17	327+37.52	33.68 RT	1839848.100	1103406.487	26.5**	611.5
RWB-18	328+14.34	34.07 RT	1839878.888	1103476.869	22.5**	611.0
RWB-19	328+84.22	35.55 RT	1839905.862	1103541.354	25.0	610.6
RWB-20	329+60.01	35.99 RT	1839936.188	1103610.814	20.0	610.3
RWB-21	330+34.08	36.40 RT	1839965.836	1103678.685	20.0	610.0
RWB-22	331+11.20	36.05 RT	1839997.416	1103749.049	20.0	609.9
RWB-23	331+80.73	36.47 RT	1840025.219	1103812.782	20.0	609.6
RWB-24	332+52.64	36.43 RT	1840054.406	1103878.494	19.0	609.2
RWB-25	333+26.85	36.39 RT	1840084.529	1103946.322	20.0	608.9
RWB-26	333+92.54	38.85 RT	1840108.906	1104007.369	20.0	608.8
RWB-27	334+79.35	37.63 RT	1840145.215	1104086.231	20.0	608.9
SGB-01	196+00***	5.00 RT***	1839465.135	1103326.205	15.0	637.6
SGB-02	194+00***	5.00 LT***	1839193.635	1103469.063	10.0	662.0
SGB-03	191+00***	5.00 RT***	1839041.080	1103725.423	10.0	672.0
SSB-01	318+77.07	77.35 RT	1839497.630	1102614.277	15.0	612.1
SSB-02	320+79.71	72.03 RT	1839566.820	1102805.087	15.0	613.0
SSB-03	322+74.75	68.36 RT	1839627.867	1102986.274	15.0	613.8
SSB-04	324+66.67	70.07 RT	1839705.874	1103171.425	15.0	613.1
SSB-05	326+71.10	75.35 RT	1839783.084	1103362.659	15.0	612.1

Boring ID	Station*	Offset*	Northing	Easting	Depth (ft)	Surface Elevation (ft)
SSB-06	328+74.56	67.03 RT	1839873.163	1103545.280	13.0**	610.7
SSB-07	330+73.63	68.02 RT	1839952.958	1103727.658	10.0	610.1
TSB-01	324+27.35	107.05 RT	1839656.500	1103148.529	25.0	620.1
TSB-02	325+40.62	96.64 RT	1839710.613	1103250.896	25.0	618.2

\* Based on drawings provided by Collins (dated March 22, 2024)

\*\* Borings terminated upon encountering practical auger refusal

\*\*\* 95<sup>th</sup> Street stationing based on preliminary drawings provided by Ames (dated March 2022)

The soil borings were drilled using truck-mounted Diedrich D-50 (hammer efficiency 92%) and CME-75 (hammer efficiency 91%) drill rigs using 3¼-inch I.D. hollow stem augers and an automatic hammer. Soil sampling was performed according to AASHTO T 206, "Penetration Test and Split Barrel Sampling of Soils." Soil samples were obtained at 2.5-foot intervals to depths of 30 feet below grade in borings RWB-13 through RWB-16, and then at 5-foot intervals thereafter to the respective termination depths. In the remaining borings, soil samples were obtained at 2.5-foot intervals to the boring termination depths or upon encountering auger refusal. Water level measurements were made in each boring when evidence of free groundwater was detected on the drill rods or in the samples. The boreholes were also checked for free water immediately after auger removal, and before filling the open boreholes with soil cuttings.

Bedrock coring was attempted upon encountering auger refusal in borings RWB-12 and RWB-19 at depths of 11.5 and 32 feet, respectively. However, bedrock was not encountered during this process, and the borings were subsequently drilled to the planned termination depths, and no bedrock cores were taken.

GSG's field representative inspected, visually classified, and logged the soil samples during the subsurface exploration activities and performed unconfined compressive strength tests on cohesive soil samples using a calibrated Rimac compression tester and a calibrated hand penetrometer in accordance with IDOT procedures and requirements. Representative soil samples collected from each sample interval, were placed in jars, and were returned to the laboratory for further testing and evaluation.

## 2.1 Laboratory Testing Program

All samples were inspected in the laboratory to verify the field classifications. A laboratory testing program was undertaken to characterize and determine engineering properties of the subsurface soils encountered in the project area. The following laboratory tests were performed on representative soil samples:

- Moisture content ASTM D2216 / AASHTO T-265
- Atterberg Limits ASTM D 4318 / AASHTO T-89 / AASHTO T-90
- Dry Unit Weight ASTM D7263
- Particle Size Analysis ASTM D422 / AASHTO T-88

The laboratory tests were performed in accordance with test procedures outlined in the IDOT Geotechnical Manual (2020), and per ASTM and AASHTO requirements. Based on the laboratory test results, the soils encountered were classified according to the AASHTO and the Illinois Division of Highways (IDH) classification systems. The results of the laboratory testing program are included in the **Appendix D Laboratory Test Results** and are also shown along with the field test results in **Appendix C Soil Boring Logs**.

## 2.2 Subsurface Soil Conditions

The subsurface soil conditions were evaluated based on the results of both the site investigation and laboratory results. Detailed descriptions of the subsurface soils, as well as the surface elevations, are provided in the Soil Boring Logs. The soil boring logs provide specific conditions encountered at each boring location, including soil descriptions, stratifications, penetration resistance, elevations, location of the samples, water levels (when encountered), and laboratory test data. Variations in the general subsurface soil profile were noted during the drilling activities. The stratifications shown on the boring logs represent the conditions only at the actual boring locations and represent the approximate boundary between subsurface materials; however, the actual transition may be gradual.

### IL 171 Borings (RWB-01 thru RWB-27, and SSB-01 thru SSB-07)

Borings RWB-01 thru RWB-27 and SBSB-01 thru SSB-07 were drilled off the shoulder of the existing pavement along IL 171. The surface elevations of the borings ranged between 608.9 and 613.8 feet. Borings RWB-01 thru RWB-04, RWB-10 thru RWB-15, RWB-20 thru RWB-25, and RWB-27 initially noted between 3 to 18 inches of topsoil. Boring RWB-26 was completed within the



existing roadway shoulder and noted 6 inches of asphalt over 6 inches of concrete. The remaining borings did not encounter any topsoil or pavement materials.

Beneath the surficial materials, borings RWB-01 thru RWB-06, RWB-10, RWB-16, RWB-17, RWB-19 thru RWB-22, RWB-24, RWB-25, SSB-02, and SSB-04 thru SSB-07 noted native loose to extremely dense brown and gray cohesionless soils (sand, sandy clay loam, silty sand, gravel, silt, and loam) to depths extending to 3.5 feet below existing grade in borings RWB-01 thru RWB-06, RWB-10, SSB-02, and SSB-04; to a depth of 6 feet below existing grade in borings SSB-05; to a depth of 18.5 feet below existing grade in borings RWB-16 and RWB-17; and to the boring termination depths in RWB-19 thru RWB-22, RWB-24, RWB-25, SSB-06, and SSB-07. In the remaining borings, native soft to hard brown cohesive soils (silty clay, silty clay loam, and clay loam) were encountered to depths between 6 and 26 feet below existing grade. Beneath the initial layers in the borings, interbedded layers of cohesive and cohesionless soils were encountered to the boring termination depths. Gravel and cobbles were noted throughout the borings at various depths.

The cohesionless soils (sand, sandy clay loam, silty sand, gravel, silt, and loam) along IL 171 had SPT blow count 'N' values between of 4 blows per foot (bpf) and 50 blows for 1 inch. The cohesive soils along IL 171 had unconfined compressive strength vales ranging between 0.25 and 10.0 tsf, with most values ranging between 1.0 and 4.5 tsf.

### **95<sup>th</sup> Street Borings (SGB-01, SGB-02, and SGB-03)**

Borings SGB-01, SGB-02, and SGB-03 were drilled along the existing 95<sup>th</sup> Street alignment south of IL 171. The surface elevations of the borings ranged between 637.6 and 672.0 feet as the roadway slopes upwards away from IL 171. Boring SGB-01 initially encountered 3 inches of topsoil. Borings SGB-02 and SGB-03 initially encountered 12 to 13 inches of asphalt underlain by 8 to 9 inches of concrete. Beneath the surficial materials in boring SGB-01, brown and gray to gray medium dense to dense cohesionless soils (sandy clay loam and silt) were encountered to a depth of 13.5 feet below existing grade. Beneath these soils and below the pavement in borings SGB-02 and SGB-03, stiff to hard brown and gray to gray silty clay and silty clay loam soils were encountered to the boring termination depths.

The brown and gray to gray silty clay had unconfined compressive strengths ranging between 1.5 and 4.2 tsf. The cohesionless soils in borings SGB-01 had SPT 'N' values between of 13 and 23 blows per foot (bpf).

### **Traffic Signal Borings (TSB-01 and TSB-02)**

Borings TSB-01 and TSB-02 were drilled through in the grass area between IL 171 and the 95<sup>th</sup> Street ramps. The surface elevations of the borings ranged between 618.2 and 620.2 feet. The borings each noted 3 inches of topsoil at the surface. Beneath the surficial layers, boring TSB-01 encountered loose to medium dense brown silt to a depth of 8.5 feet below existing grade. Beneath these soils and from the ground surface in boring TSB-02, medium stiff to hard brown and gray to gray silty clay and silty clay loam soils were encountered to a depth of 23.5 feet in boring TSB-01 and to the termination depth in TSB-02. Boring TSB-01 then noted dense gray silt to the boring termination depth. Wood and roots fragments were noted in boring TSB-02 at depths of 6.5 and 9 feet below existing grade.

The brown and gray to gray silty clay soils had unconfined compressive strengths ranging between 0.8 and 4.5 tsf. The cohesionless soils in borings TSB-01 had SPT 'N' values between 8 and 15 blows per foot (bpf).

### **2.3 Groundwater Conditions**

Water levels were checked in each boring to determine the general groundwater conditions present at the site and were measured while drilling and after each boring was completed. Groundwater was noted in boring RWB-01 at a depth of 8.5 feet (603.1 feet), RWB-03 at a depth of 11 feet (601.0 feet), RWB-10 at a depth of 28.5 feet (584.9 feet), and RWB-14 at a depth of 33.5 feet (578.9 feet). Groundwater was not encountered in the remaining borings either while drilling or after drilling. No delayed groundwater readings were obtained, and the borings were backfilled immediately upon completion.

Based on the color change from brown and gray to gray and moisture contents of the samples, it is anticipated that the long-term groundwater level is below the bottom of the shallow depth borings completed along the project corridor. In borings RWB-01 thru RWB-10 and SSB-01 thru SSB-03, the long-term groundwater level could range between elevations 586.0 to 605.0 feet. Perched water may also be present within any confined granular layers throughout the borings. Water level readings were made in the boreholes at times and under conditions shown on the boring logs and stated in the text of this report. However, it should be noted that fluctuations in groundwater level may occur due to variations in rainfall, other climatic conditions, or other factors not evident at the time measurements were made and reported herein.

### 3.0 GEOTECHNICAL ANALYSES AND RECOMMENDATIONS

This section provides GSG's geotechnical analysis and recommendations for the design of the proposed roadway improvements based on the results of the field exploration and laboratory testing. Subsurface conditions in unexplored locations may vary from those encountered at the boring locations. If the alignment or proposed grades change, we request that you contact GSG to re-evaluate our recommendations.

#### 3.1 Drainage Characteristics

The drainage characteristics of the site were evaluated per the IDOT Geotechnical Manual, Section 6.3.4.1, based on the subgrade soil type and moisture condition, depth of water table, project topography, the proposed profile grade line, and depth and grade of drainage ditches along the roadway. The proposed roadway improvements along IL 171 and along 95<sup>th</sup> Street near the intersection with IL 171 (Station 197+00 to 200+00) will be supported on new engineered fill having a fill height greater than 3 feet. Fill soils that are cohesive (A-6) or granular in nature with a fill height greater than 3 feet are classified as Good drainage material; therefore, a Good classification should be used for the subgrade soils for the areas of elevated embankment.

The following road sections may be supported on new engineered fill thicknesses of less than 3 feet. **Table 3** summarizes the drainage classification for these sections based on the subgrade soil characteristics.

**Table 3 - Summary of Drainage Classification**

Road Section	Station	Subgrade soil description	Drainage Characteristics
95th Street (SGB-01)	Sta. 191+00 to Sta. 197+00	Sandy Clay Loam	Fair
95th Street (SGB-02 and SGB-03)		Silty Clay	Poor to Fair

#### 3.2 Frost Susceptibility

The frost susceptibility of the subgrade soils was evaluated per Section 6.3.2.2.3 of the IDOT Geotechnical Manual. The maximum anticipated frost penetration depth below pavement in northern Illinois for extreme weather conditions is 45 to 60 inches. The frost susceptibility was evaluated for the soils encountered that would be within the proposed roadway subgrade. The frost class for the subgrade soils in these areas was assigned using Table 6.3.2.2.3-1, Frost Susceptibility Classification of Soils, in the IDOT Geotechnical Manual.

Along IL 171 and 95<sup>th</sup> Street, the new sloped embankment and inner core of the embankment fill will likely be cohesive in nature and will have a Frost Class of F3 (high frost susceptibility). However, the majority of the proposed roadway will be built on embankment which will be elevated more than 5 feet and will have a proper drainage system. Based on the proposed drainage conditions for the site and the anticipated deeper long-term groundwater level below existing subgrade, frost heave is not a concern.

For the areas identified in **Table 3**, the subgrade soils generally consisted of cohesive and granular soils containing fine grained material and were found to have a Frost Class of F3 (high frost susceptibility). In our opinion, there is no concern potential frost action due to groundwater capillary rise, due to the anticipated depth of the groundwater within the project limits. Therefore, GSG does not recommend any corrective measures regarding frost susceptibility.

### 3.3 Subgrade Support Rating

The subgrade support rating (SSR) was determined based on the physical properties of in-situ soils present beneath the proposed pavement section. The SSR includes three categories (poor, fair, and granular), and are used to determine the depth of soil treatment to provide a stable working platform that is required to prevent excessive rutting, and moisture related problems during construction activities. Granular soils have the highest rating and provide a stable working platform that may require less than a 12-inch-thick improved subgrade layer, while poor subgrade may require more than 12 inches to provide stable subgrade during construction activities. The new inner core of the embankment along IL 171 and 95<sup>th</sup> Street will likely be cohesive in nature and will have a Subgrade Support Rating (SSR) rating of Poor. It is recommended that a Subgrade Support Rating of Poor be used for the elevated section of roadway for this project. The near surface soils described in **Table 3** consisted of cohesive and granular soils containing fine grained material. These soils have a Subgrade Support Rating (SSR) of Poor to Fair.

### 3.4 Illinois Bearing Ratio

The Illinois Bearing Ratio (IBR) is a measure of the support provided by the roadbed soils for the new pavement. Along the elevated sections of IL 171 and 95<sup>th</sup> Street, portions of the inner core embankment fill and sloped embankment fill will likely consist of cohesive soils, therefore it is recommended to use an IBR value of 2, based on typical IBR values for Illinois soils-Table 5.5.16-1 of the IDOT Geotechnical Manual, for the roadway pavement design and correlate to the

subgrade resilient modulus based on the AASHTO recommended pavement design formula for fine grained soils ( $M_r = 1,500 \times \text{IBR}$ ).

For the soils described in **Table 3**, it is recommended that an IBR value of five (5) be used for the roadway pavement design where granular soils are present. It is recommended that an IBR value of two (2) be used for the roadway pavement design where clay soils are present.

### **3.5 Organic Content**

Typically, soils with an organic content in excess of 10 percent are considered unsuitable to remain below proposed pavement areas. Based on the soil borings, it is not anticipated that highly organic soils will be encountered in subgrade soils for the proposed roadway.

### **3.6 Shrinkage Factor**

Based on IDOT and FHWA references, a shrinkage factor of 15% may be used for newly placed cohesive soils. For dry sand, a shrinkage factor of 10% may be used.

## **4.0 EMBANKMENT RECOMMENDATIONS**

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This section provides GSG's geotechnical recommendations for the design of the proposed improvements based on the results of the field exploration, laboratory testing, and geotechnical analysis. As part of the project plans, new embankments will be constructed that will require new fill heights of up to 18 feet. The largest fill heights will be located near the proposed intersection of IL 171 and 95<sup>th</sup> Street. For the design and construction of the new embankments, the existing subgrade soils were evaluated for potential settlement due to the anticipated loading. The proposed embankment was also analyzed for global stability. Design and construction recommendations for the proposed embankment are in the following sections.

### **4.1 Proposed Embankments**

GSG understands that new engineered fill will be used to construct the new embankment for the reconstructed IL 171 and 95<sup>th</sup> Street intersection. It is anticipated that the majority of the roadway embankment along IL 171 will be retained by a retaining wall along the north side of existing IL 171, while 95<sup>th</sup> street will be supported on sloped embankments. Recommendations for the proposed retaining wall are included in a separate report.

### **4.2 Embankment Settlement**

Based on the variable heights, shapes, and soil conditions across the length of the mainline embankment, the analysis was broken into several sections to evaluate the anticipated amount of primary settlement. Each analysis section was selected based on the overall height of the embankment, the anticipated loading and influence zone of the embankment due to the variable shapes, or the soil conditions encountered in the soil borings along each section of IL 171 and 95<sup>th</sup> Street. Due to the predominantly granular nature of the site soils, significant long term consolidation settlement is not anticipated; however, the low strength, high plasticity and moisture content clays encountered in borings RWB-14 through RWB-16 may be subject to high settlements. The maximum estimated primary settlements were calculated as shown in **Table 4**.



**Table 4 – Estimated Settlement Summary**

Roadway Area	Boring IDs / Roadway Station*	Maximum Embankment Height*	Anticipated Total Primary Settlement	Anticipated Subgrade Materials
IL 171	RWB-03 thru RWB-13, SSB-01 thru SSB-04 / Sta. 317+80.13 to Sta. 324+75	16.5	1.3	Stiff to Very Stiff Silty Clay and Loose to Medium Dense Sand
IL 171	RWB-14 thru RWB-16, SSB-05 Sta. 324+75 to Sta. 327+25	18	3.5	Soft to Stiff Silty Clay and Loose Silt
IL 171	RWB-17 thru RWB-25, SSB-06 & SSB-07 / Sta. 327+25 to Sta. 333+27.91	15	< 1.0	Loose to Medium Dense Sand and Stiff Silty Clay
95 <sup>th</sup> Street	SGB-01 thru SGB-03 / Sta. 191+00 to 197+00	<5	< 1.0	Stiff to Very Stiff Silty Clay
95 <sup>th</sup> Street	RWB-11 thru RWB-15, SSB-04 / Sta. 197+00 to 200+00	18	3.5	Soft to Stiff Silty Clay and Loose Silt

\*Based on drawings (dated 03/22/2024) and design information (dated 03/27/2024) provided by Collins

Based on experience with similar soil conditions, 90% of the primary consolidation will occur within approximately 9 to 12 months from the date of loading. It is recommended that settlement plates be installed near the intersection of IL 171 and 95<sup>th</sup> Street where the greatest fill height is anticipated and midpoints of the embankments to monitor settlement and help the design section engineer determine when acceptable settlement rates and settlement amounts have been achieved.

### 4.3 Embankment Settlement Treatment and Recommendations

Due to the anticipated magnitude of total settlement for several sections of the alignment, special design recommendations should be considered. This should mitigate the impact of differential settlement along the proposed roadway alignment and any impacts to the construction schedule.

#### 4.3.1 Staged Construction

Due to the magnitude of fill heights that are proposed for the roadway construction, segments of the project could utilize controlled rate of loading or staged construction. With staged construction, a portion of the embankment is constructed to allow for soil consolidation and pore water pressure dissipation which would increase soil strength prior to completion of the full embankment/fill construction. For the initial construction, allowing the partially constructed

embankment to remain in place for varying amounts of time, prior to the final stage construction will result in different amounts of settlement after construction. The longer the initial stage construction remains in place as a surcharge over the underlying soils, the less settlement is anticipated to occur post construction.

Proper instrumentation, as outlined in IDOT Geotechnical Manual (2020) in *Section 6.4.4.6-Instrumentation and Control of Embankment Construction*, will be required to monitor the state of stress in the soil during the loading period, to ensure that loading does not proceed so rapidly as to cause a shear failure.

#### **4.3.2 Maintenance**

A maintenance program will likely be necessary throughout the construction stage to account for movement of the new embankments. This will require additional quantities of fill materials to be placed during construction, which should be accounted for when estimating earthwork quantities. The site improvement alternative selected will determine how long and how much maintenance may be necessary.

#### **4.3.3 Ground Improvement Recommendations**

Based on the anticipated embankment settlements noted in **Table 4** in the vicinity of borings RWB-13 to RWB-17, additional ground modification should also be considered. The installation of rammed aggregate piers, stone columns or rigid inclusions below the embankment could be considered to stabilize the site and minimize long term settlement. Additional ground improvement would be necessary for only a portion of the embankment where excessive settlement is anticipated. Based on the engineering analysis, the ground improvements are recommended between IL 171 Stations 324+75 and 327+25.

Aggregate columns can also act as wick drains in accelerating drainage at the site, and decrease the time frame for consolidation settlement. Typical column diameters range from 18 to 36 inches and, in general, are most economical for sites requiring column lengths less than 35 feet deep and preferably about 20 feet deep below the surface, such as this site.

Rigid inclusions (RIs) are columns of grout used to reinforce the ground to increase bearing resistance and reduce settlement of a structure or embankment. Rigid Inclusions are constructed with an auger displacement tool or vibrated pipe tool that displaces soil laterally, producing very little spoils. Grout mixes for rigid inclusions shall consist of Portland cement, sand, and water,

and may also contain coarse aggregate, a mineral admixture and/or approved fluidifier. Geogrid or geotextile and reinforcing steel can also be used to increase the strength of the inclusions. Typical inclusion diameters range from 12 to 18 inches. The rigid inclusions reinforce the soil rather than function as distinct structural elements or piles. The improved ground has increased stiffness and therefore improved settlement and bearing characteristics.

In addition to the stone columns or rigid inclusions, a load transfer layer consisting of compacted material with geogrid reinforcement would be necessary to transfer the embankment load to the columns. The embankment construction and fill placement could then be completed after the installation of the columns and the load transfer layer.

This site improvement technique would provide a stable platform for construction of the embankment by transferring the embankment and MSE wall loads to the lower medium dense to extremely dense granular materials and limit the influence on the compressible materials. Based on the subsurface conditions the stone columns should be designed to bear within the medium dense to extremely dense granular soils approximately 26 feet below the existing native grade, in accordance with *GBSP 71-Aggregate Column Ground Improvement* provided within the IDOT guidelines.

The installation of this ground improvement method could have significant initial costs for the project; however, there would be limited impact on the construction schedule, and little to no long-term maintenance costs.

#### **4.4 Slope Stability Analyses and Recommendations**

Slope stability analyses were performed in areas where sloped embankments are proposed along reconstructed 95<sup>th</sup> Street. For the proposed improvements, the maximum fill height will be 18 feet near the intersection with IL 171 (95<sup>th</sup> Street stations 199+00 to 200+00). Based on the estimated widths and elevations of the proposed 95<sup>th</sup> Street embankment, it is anticipated that the side slopes will be approximately 14:1 (H:V). For the areas of the project that will include retaining walls, analyses of these areas were completed within the retaining wall SGR.

Slide2 is a comprehensive slope stability analysis software used to evaluate the proposed sloped embankments for the project based on the limit equilibrium method. The proposed sloped embankments were analyzed based on the plans provided by Ames and Collins (**Appendix A**) and the soils encountered while drilling. Circular failure analyses were evaluated using the simplified

Bishops analyses methods for the proposed slope geometry. Based on the proposed geometry and the soil borings, global stability analyses were performed. The analyses are summarized in **Table 5**.

**Table 5 – Global Slope Stability Analyses Results**

Analysis Exhibit	Location	Embankment Height (ft)	Side Slope (H:V)	Analysis Type	Factor of Safety	Minimum Factor of Safety
Exhibit 1	95 <sup>th</sup> Street, Station 199+50, Left side of embankment	18.0	14:1	Circular – Short Term	14.2	1.5
Exhibit 2				Circular – Long Term	8.2	1.5
Exhibit 3	95 <sup>th</sup> Street, Station 199+50, Right side of embankment	18.0	14:1	Circular – Short Term	6.3	1.5
Exhibit 4				Circular – Long Term	7.3	1.5

Based on the analyses performed, the proposed slopes meet the minimum factor of safety of 1.5. Copies of the Slope Stability Analysis exhibits are included in **Appendix E**.

## 5.0 GEOTECHNICAL ROADWAY DESIGN RECOMMENDATIONS

This section provides GSG's geotechnical recommendations for the design of the proposed roadway improvements based on the results of the field exploration, laboratory testing, and geotechnical analysis.

### 5.1 Subgrade Treatment and Recommendations

Based on the existing site conditions, undercuts may be necessary along sections of the proposed improvements to provide a stable platform for the embankment construction. The preliminary recommended undercuts and locations are summarized in **Table 6**. These locations are shown on the soil profiles included in **Appendix B**. The depth, location, and extent of the proposed undercuts should be field verified during construction. All potentially unstable soils should be tested with a cone penetrometer and treated in accordance with Article 301.04 of the SSRBC and the undercut guidelines in the IDOT Subgrade Stability Manual.

**Table 6 – Preliminary Recommended Undercuts**

Roadway	Approximate Roadway Stations	Lateral Limits	Boring IDs	Soil Description	Remedial Undercut/Scarify and Recompact		Comments
					Elevation (feet)	Depth* (feet)	
IL 171	316+25 to 317+25	Embankment Footprint	RWB-02	Loose Brown Sand	609.5	0.0 -2.0	'N' value < 7 bpf
IL 171	321+45 to 322+10	Embankment Footprint	RWB-09 &SSB-03	Medium Stiff Brown Silty Clay	610.0	3.0-3.5	q <sub>u</sub> < 2.0 tsf
IL 171	324+75 to 327+25**	Embankment Footprint	SSB-04, RWB-14&15	Medium Stiff Brown Silty Clay & Loose Brown Sandy Clay Loam	611.0 - 612.0	0.0 – 2.0	'N' value < 7 bpf & q <sub>u</sub> < 2.0 tsf
IL 171	329+75 to 331+50	Embankment Footprint	RWB-20 & RWB-21	Loose Brown Sand, Silty Sand, & Silt	608.0	0.0 – 2.0	'N' value <7 bpf

\*Depth measured from existing ground surface

\*\* Undercut may not be required if ground improvement measures used as discussed in Section 4.3.3

Approved structural fill includes IDOT Porous Granular Embankment (PGE), or suitable borrow materials, as specified in the Borrow Material and Compaction Requirements section of this report. It is also recommended that a woven geotechnical fabric be placed at the base of the undercut. The geotextile fabric should consist of a woven material meeting the requirements of

Section 1080.02 of the IDOT SSRBC (2022) and should be placed in accordance with Section 210 of the IDOT SSRBC (2022).

## 5.2 Drainage Recommendations

The embankment fill with proper drainage systems should be designed using a Good drainage classification. The groundwater depth is significantly deeper than the anticipated frost depth of 45 to 60 inches for the northern Illinois region, and as such no subgrade saturation is anticipated due to capillary action. GSG anticipates that storm drainage system constructed along the sides of the proposed roads should be sufficient to provide good drainage and therefore we do not anticipate the need of any additional underdrains for this project. For the roadway sections described in **Table 3**, a drainage classification of Poor to Fair should be used.

## 5.3 Traffic Signal Foundations

GSG understands that new traffic signal structures will be installed at the intersection of IL 171 and 95<sup>th</sup> Street. Based on estimated mast arm lengths, **Table 7** summarizes design requirements for the depth and diameter of foundations per the IDOT Highway Standard 878001-11 (**Appendix F**).

**Table 7 – Proposed Traffic Signal Structure Summary**

Mast Arm Length <sup>1</sup> (feet)	Anticipated Foundation Depth <sup>2</sup>	Anticipated Foundation Diameter <sup>2</sup>
30.0	13' 6"	30"
	11- 0"	36"
40.0	13' 0"	36"

<sup>1</sup> Estimated length

<sup>2</sup> Based on IDOT Highway Standard 878001-11.

Based on the proposed roadway grading, it is anticipated that the traffic signal foundations will bear within new clay fill, constructed as part of the elevated embankment sections of IL 171 and 95<sup>th</sup> Street; these soils will be compacted in accordance with IDOT specifications (SSRBC) and will meet the required unconfined compressive strengths (Qu) above 1.0 tsf. Therefore, the IDOT standard is valid for borings TSB-01 and TSB-02 and can be used for the design of the traffic signal foundations. If granular materials are used in the embankment construction, it is recommended that the drilled shafts at borings TSB-01 and TSB-02 be installed using a temporary casing.

Soils must be visually inspected at each location to confirm the presence of new clay fill; if



different soils are encountered during construction the engineer must be notified to provide a revised design. The lateral resistance of the upper 3.5 feet of soils in the frost penetration zone should be neglected in design.

#### **5.4 Lateral Earth Pressure and Loading**

Drilled shafts for the proposed structure are normally loaded laterally by wind forces. The ability of the shaft to resist the wind loads is dependent on the passive pressures that develop in the soils along the shaft and the shaft diameter. Lateral loads on the drilled shafts should be analyzed for the maximum moments and lateral deflections. Software such as L-Pile are normally used to determine the required shaft depth to resist the lateral loads, the actual maximum moment and the anticipated shaft deflection. If the shaft deflection is excessive or if the embedment is inadequate to provide “fixity”, the shaft embedment could be increased to help address these issues. The shaft diameter should be increased if the deflection or the maximum moment is higher than the shaft designed resistance.

## **6.0 CONSTRUCTION CONSIDERATIONS**

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All work performed for the proposed project should conform to the requirements in the IDOT Standard Specifications for Road and Bridge Construction (SSRBC, 2022) along with the Illinois Tollway Supplemental Specifications, and the IDOT Subgrade Stability Manual (2005). Any deviation from the requirements in the manuals above should be approved by the design engineer.

### **6.1 Topsoil Removal**

GSG recommends completely stripping the topsoil to a minimum depth of 12 inches or any greater full depth encountered within the limits of the proposed embankment and roadway areas and stockpiling it per Section 211.03 of the IDOT SSRBC. Topsoil thicknesses of up to 18 inches could be anticipated in the project limits. The topsoil should be separated from other materials being stockpiled onsite for reuse or haul off. If the topsoil is to be reused, mechanical and chemical analyses for nutrients should be performed in order to determine the suitability and nature of treatment required for the topsoil prior to reuse for this project.

### **6.2 Embankment and Pavement Subgrade Preparation**

The stability of the embankment subgrade should be evaluated immediately prior to placement of any new engineered fill in accordance with the Section 205 - Embankment of IDOT SSRBC to determine if additional treatment is required.

After the subgrade areas are exposed, the inspection should include visual inspection and performing a proof roll using heavy equipment or heavily loaded tandem axle dump truck with a minimum gross weight of 25 tons to check for deflection or rutting. Areas with excessive rutting and deflection shall be evaluated using a dynamic cone penetrometer (DCP) and static cone penetrometer (SCP) to determine the depth of required treatment in accordance with the IDOT Subgrade Stability Manual (2005) and IDOT SSRBC (2022), Section 301. The subgrade should be prepared in accordance with Sections 205-Embankment and Section 301-Subgrade preparation, of the IDOT SSRBC (2022).

Treatment for unstable and unsuitable soils encountered during proof rolling and subgrade evaluation may include the use of a geotextile fabric, removal and replacement with approved structural fill for small areas, or the use of additive materials, such as lime, cement or fly ash. Subgrade improvements should be based on the recommendations in the Subgrade Treatment and Recommendations Section 5.1 of this report or based on field evaluation of the materials

during construction. Field evaluation of the subgrade soils should be conducted in accordance with the procedures outlined in the IDOT Geotechnical Manual and Subgrade Stability Manual, and under the supervision of a licensed geotechnical engineer.

### **6.3 Site Excavation and Construction Safety**

Site excavations are expected to encounter various types of soils as described in the Subsurface Exploration section of this report. The contractor will be responsible to provide a safe excavation during the construction activities of the project. All excavations should be conducted in accordance with applicable federal, state, and local safety regulations, including, but not limited to the Occupational Safety and Health Administration (OSHA) excavation safety standards. Excavation stability and soil pressures on temporary shoring are dependent on soil conditions, depth of excavations, installation procedures, and the magnitude of any surcharge loads on the ground surface adjacent to the excavation. Excavation near existing structures and underground utilities should be performed with extreme care to avoid undermining existing structures. Excavations should not extend below the level of adjacent existing foundations or utilities unless underpinning or other support is installed. It is the responsibility of the contractor for field determinations of applicable conditions and providing adequate shoring for all excavation activities.

### **6.4 Borrow Material and Compaction Requirements**

If borrow material is to be used for onsite construction, it should conform to Section 204 “Borrow and Furnish Excavations” of the IDOT Standard Specifications for Road and Bridge Construction (2022). Imported or on-site fill materials should be evaluated using Table 8.4-1 of the IDOT Geotechnical Manual, Requirements of Borrow Soils for the top 24 inch, and Section 204, “Borrow and Furnish Excavations” of the IDOT SSRBC.

The fill material should be free of organic matter and debris and should be placed and compacted in accordance with Section 205, Embankment, of the IDOT SSRBC (2022). Earth-moving operations should be avoided during excessively cold or wet weather to avoid freezing or softening subgrade soils. Fill should be placed in lifts and compacted according to Section 205, Embankment (IDOT, 2022).

### **6.5 Groundwater Management**

It is anticipated that the long-term groundwater level is below the bottom of the borings for the majority of the project corridor. In borings RWB-01 thru RWB-10 and SSB-01 thru SSB-03, the

long-term groundwater level could range between elevations 586.0 to 605.0 feet. GSG does not anticipate significant groundwater related issues during construction activity, however perched water may be encountered in any confined granular layers. If rainwater run-off or perched water is accumulated at the base of excavation, the contractor should remove accumulated water using conventional sump pit and pump procedures and maintain a dry and stable excavation. The location of the sump should be determined by the contractor based on field conditions. During earthmoving activities at the site, grading should be performed to ensure that drainage is maintained throughout the construction period. Water should not be allowed to accumulate in the foundation area either during or after construction. Undercut and excavated areas should be sloped toward one corner to facilitate removal of any collected rainwater or surface run-off. Grades should be sloped away from the excavations to minimize runoff from entering.

If water seepage occurs during construction or where wet conditions are encountered, such that the water cannot be removed with conventional sumping, we recommend placing open grade stone similar to IDOT CA-7 to stabilize the bottom of the excavation below the water table. The CA-7 stone should be placed to 12 inches above the water table, in 12-inch lifts, and should be compacted with the use of a heavy smooth drum roller or heavy vibratory plate compactor until stable. The remaining portion of the excavation should be backfilled using approved structural fill.

## **7.0 LIMITATIONS**

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This report has been prepared for the exclusive use of the Illinois Department of Transportation and its Design Section Engineer. The recommendations provided in the report are specific to the project described herein and are based on the information obtained from the soil boring locations within the proposed project limits. The analyses have been performed and the recommendations have been provided in this report are based on subsurface conditions determined at the location of the borings. This report may not reflect all variations that may occur between boring locations or at some other time, the nature and extent of which may not become evident until during the time of construction. If variations in subsurface conditions become evident after submission of this report, it will be necessary to evaluate their nature and review the recommendations presented herein.

**APPENDIX A**  
**GENERAL PLANS, ELEVATIONS, AND DETAILS**



Bench Mark: A 2" metal disk in concrete located in grass median at 95th Street and IL Route 171 lying 36' south of south pavement edge along IL Route 171 and 29' northwest of west pavement edge along east leg for 95th Street. Elev. 608.57.

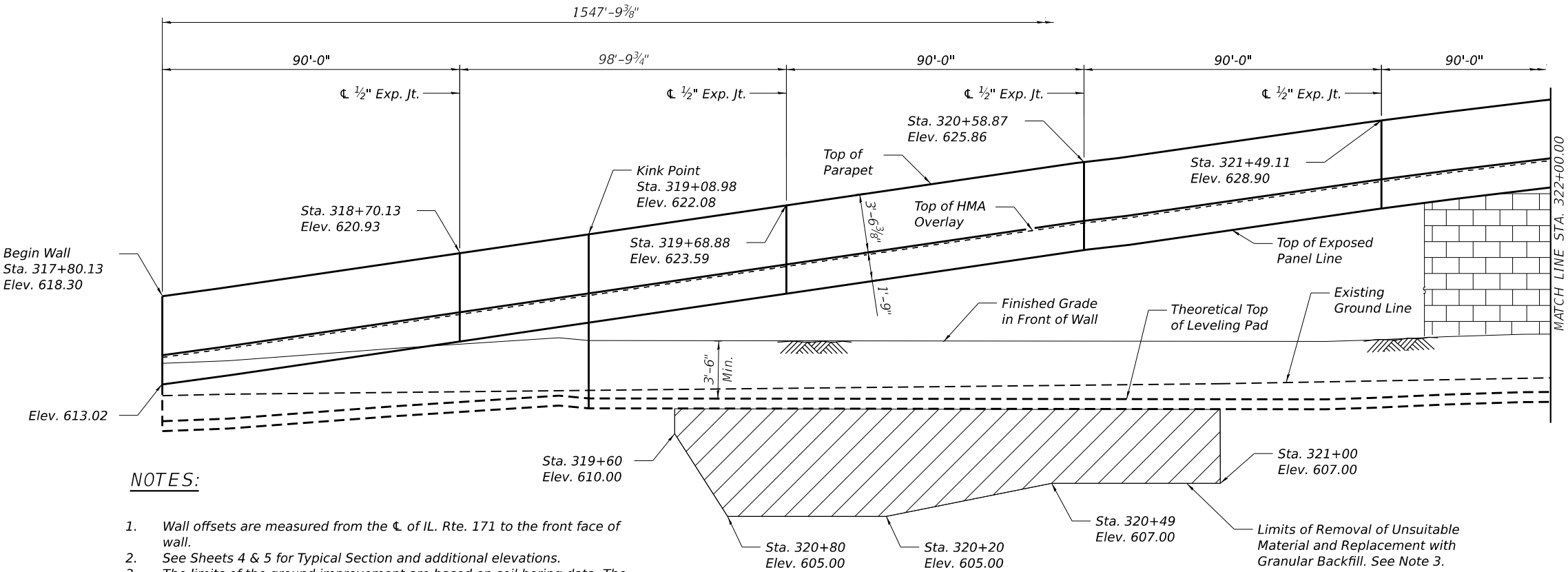
Existing Structure: None

Traffic to be detoured during construction.

DESIGN SPECIFICATIONS  
2020 AASHTO LRFD Bridge Design  
Specifications, 9th Edition

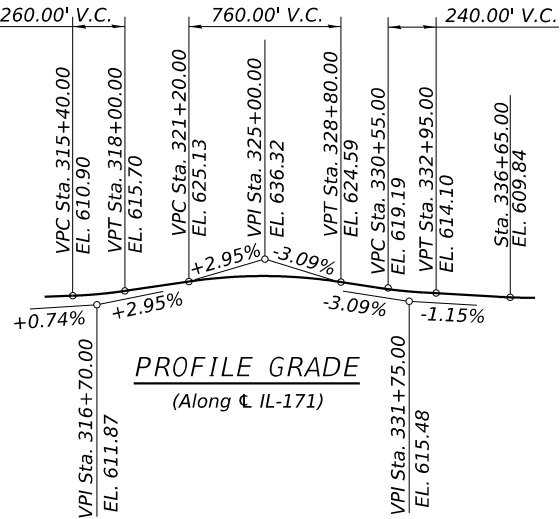
DESIGN STRESSES  
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f<sub>c</sub> = 3,500 psi  
f<sub>y</sub> = 60,000 psi (Reinforcement)  
PRECAST UNITS  
f<sub>c</sub> = 4,500 psi (precast panels)

HIGHWAY CLASSIFICATION  
F.A.U. 3565 - IL Rte. 171  
Functional Class: Minor Arterial  
ADT: 13,000 (2021); 17,200 (2038)  
ADTT: 780 (2021); 1,030 (2038)  
DHV: 1,720 (2038)  
Design Speed: 55 m.p.h.  
Posted Speed: 55 m.p.h.  
2-Way Traffic  
Directional Distribution: 50/50



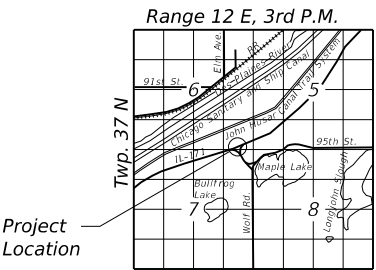
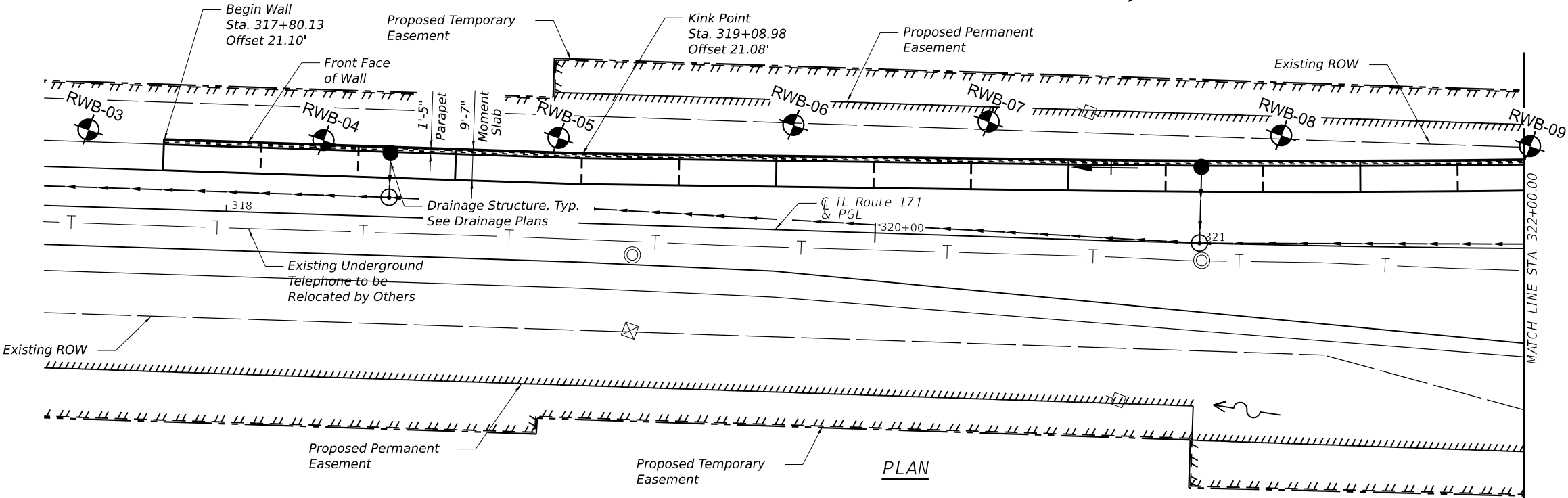
NOTES:

- Wall offsets are measured from the  $\Delta$  of IL. Rte. 171 to the front face of wall.
- See Sheets 4 & 5 for Typical Section and additional elevations.
- The limits of the ground improvement are based on soil boring data. The extent of the ground improvement to be verified in the field (See Roadway Plans and SGR).



CURVE DATA

P.I. Sta. = 323+29.13  
 $\Delta$  = 5° 35' 37" (LT)  
D = 1° 01' 23"  
R = 5,600.00  
T = 273.57'  
L = 546.70'  
E = 6.68'  
P.C. Sta. = 320+55.56  
P.T. Sta. = 326+02.26



GENERAL PLAN AND ELEVATION I  
RETAINING WALL NO. 1 ALONG  
ILLINOIS ROUTE 171 (ARCHER AVE.)  
F.A.U. RTE. 3565 - SEC U-1-N  
COOK COUNTY  
STA. 317+80.13 STA. 333+27.91  
STRUCTURE NO. 016-2310

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**COLLINS**  
**ENGINEERS**

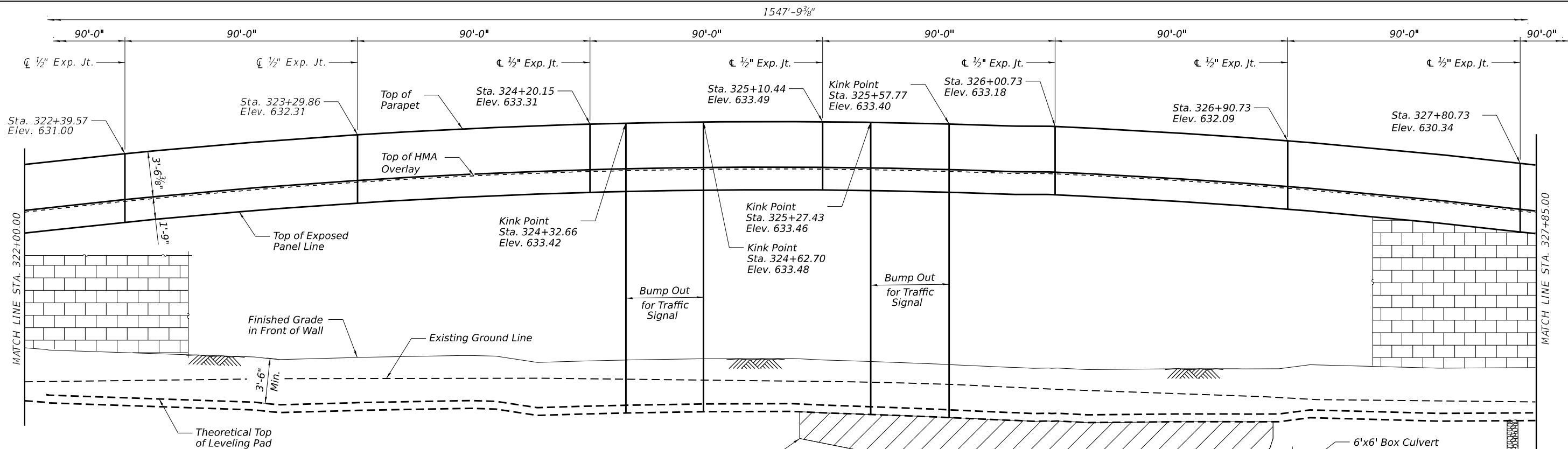
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	CHECKED - EKM	REVISED -

STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION

GENERAL PLAN AND ELEVATION  
STRUCTURE NO. 016-2310

SHEET 1 OF 5 SHEETS

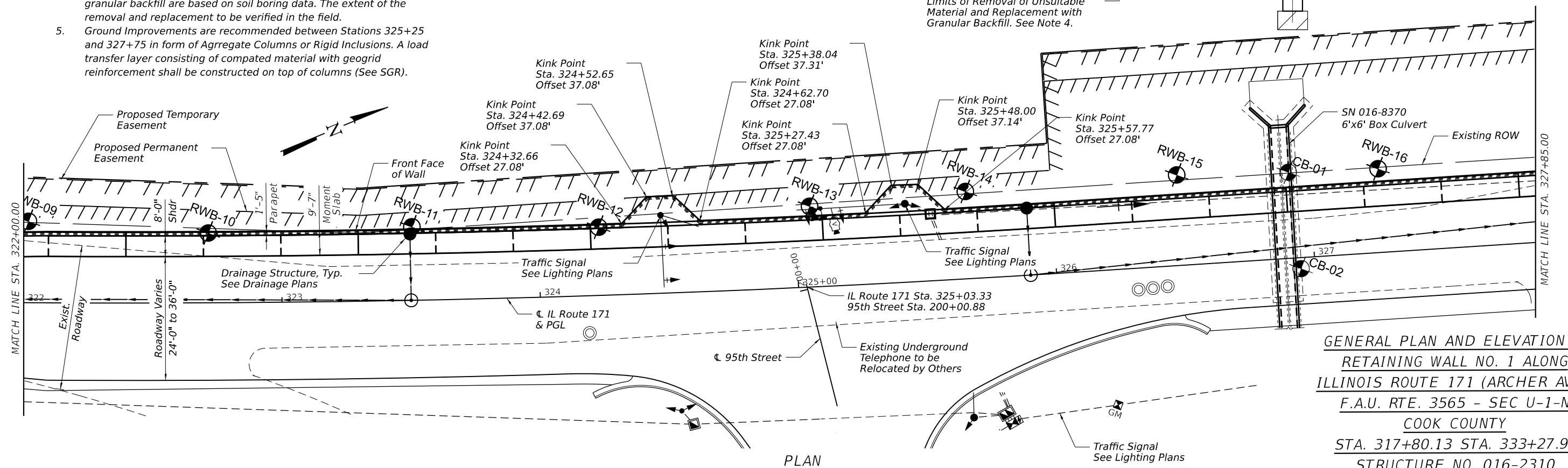
F.A.U. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
3565	U-1-N	COOK	5	1
CONTRACT NO. 60R94				
ILLINOIS FED. AID PROJECT				



**NOTES:**

1. Wall offsets are measured from the  $\text{CL}$  of IL. Rte. 171 to the front face of wall.
2. See SN 016-8370 Plans for south culvert details.
3. See Sheets 4 & 5 for Typical Section and additional elevations.
4. The limits of the removal of unsuitable material and replacement with granular backfill are based on soil boring data. The extent of the removal and replacement to be verified in the field.
5. Ground Improvements are recommended between Stations 325+25 and 327+75 in form of Aggregate Columns or Rigid Inclusions. A load transfer layer consisting of compacted material with geogrid reinforcement shall be constructed on top of columns (See SGR).

**ELEVATION**  
(Looking Northwest at Front Face of Wall)



**GENERAL PLAN AND ELEVATION II**  
**RETAINING WALL NO. 1 ALONG**  
**ILLINOIS ROUTE 171 (ARCHER AVE.)**  
**F.A.U. RTE. 3565 - SEC U-1-N**  
**COOK COUNTY**  
**STA. 317+80.13 STA. 333+27.91**  
**STRUCTURE NO. 016-2310**

**COLLINS**  
**ENGINEERS**

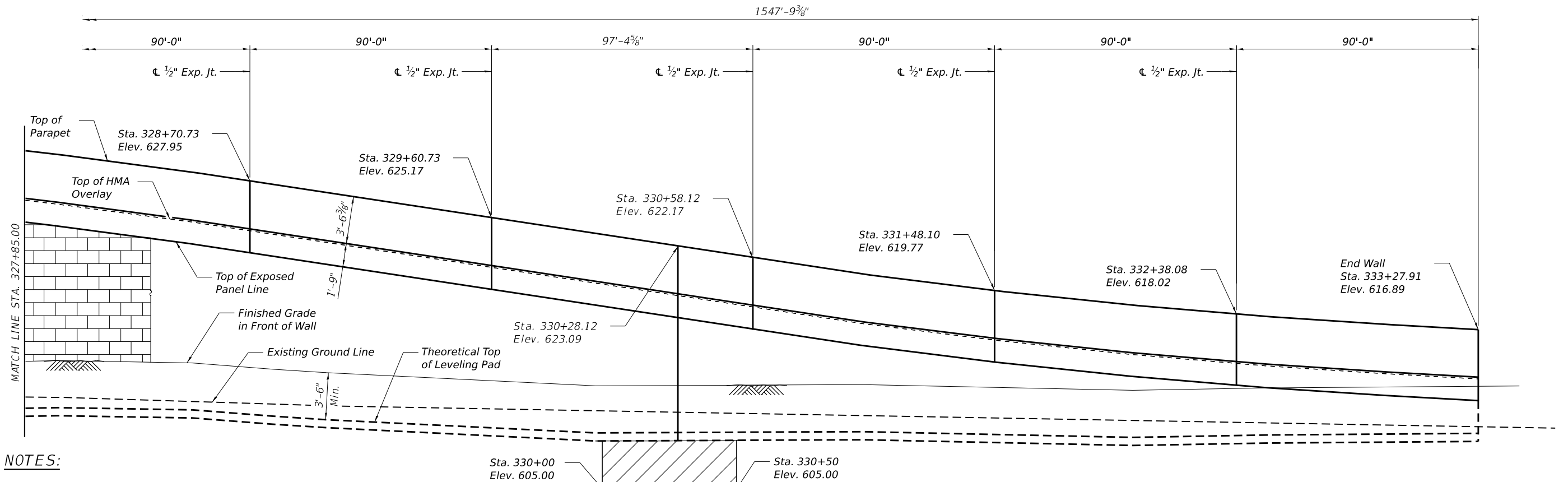
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**STATE OF ILLINOIS**  
**DEPARTMENT OF TRANSPORTATION**

**GENERAL PLAN AND ELEVATION**  
**STRUCTURE NO. 016-2310**

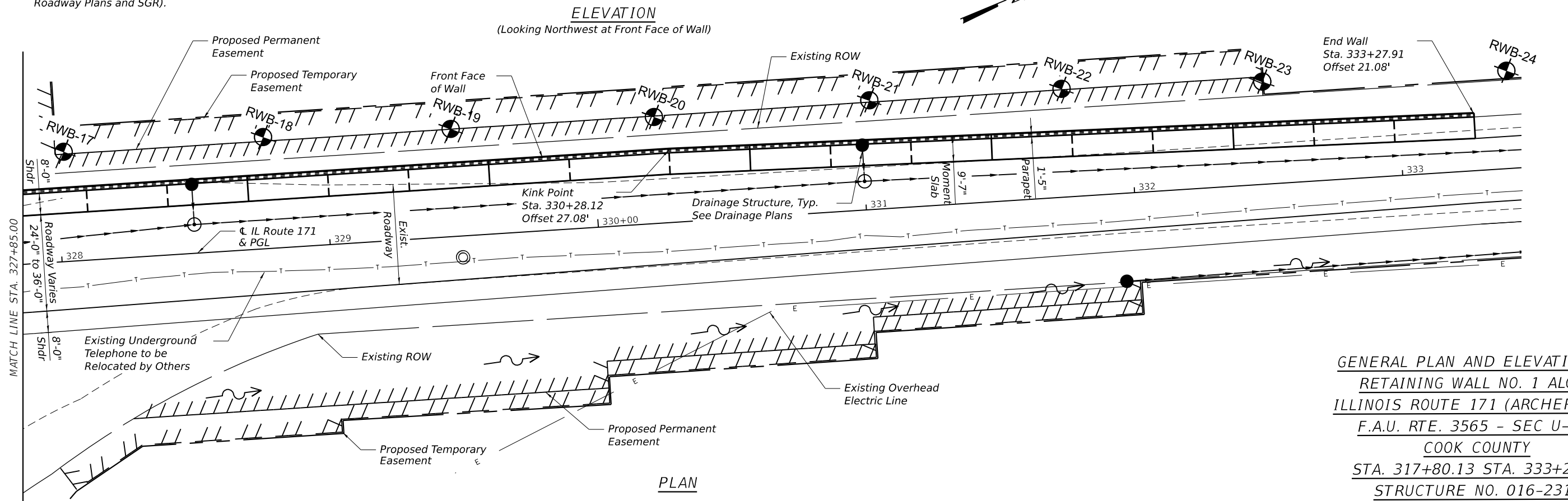
SHEET 2 OF 5 SHEETS

F.A.U. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
3565	U-1-N	COOK	5	2.
CONTRACT NO. 60R94				
ILLINOIS FED. AID PROJECT				



**NOTES:**

1. Wall offsets are measured from the  $\text{CL}$  of IL. Rte. 171 to the front face of wall.
2. See Sheets 4 & 5 for Typical Section and additional elevations.
3. The limits of the ground improvement are based on soil boring data. The extent of the ground improvement to be verified in the field (See Roadway Plans and SGR).



GENERAL PLAN AND ELEVATION III  
RETAINING WALL NO. 1 ALONG  
ILLINOIS ROUTE 171 (ARCHER AVE.)  
F.A.U. RTE. 3565 - SEC U-1-N  
COOK COUNTY  
STA. 317+80.13 STA. 333+27.91  
STRUCTURE NO. 016-2310

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**COLLINS**  
**ENGINEERS**

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		CHECKED	-	EKM	REVISED	-

STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION

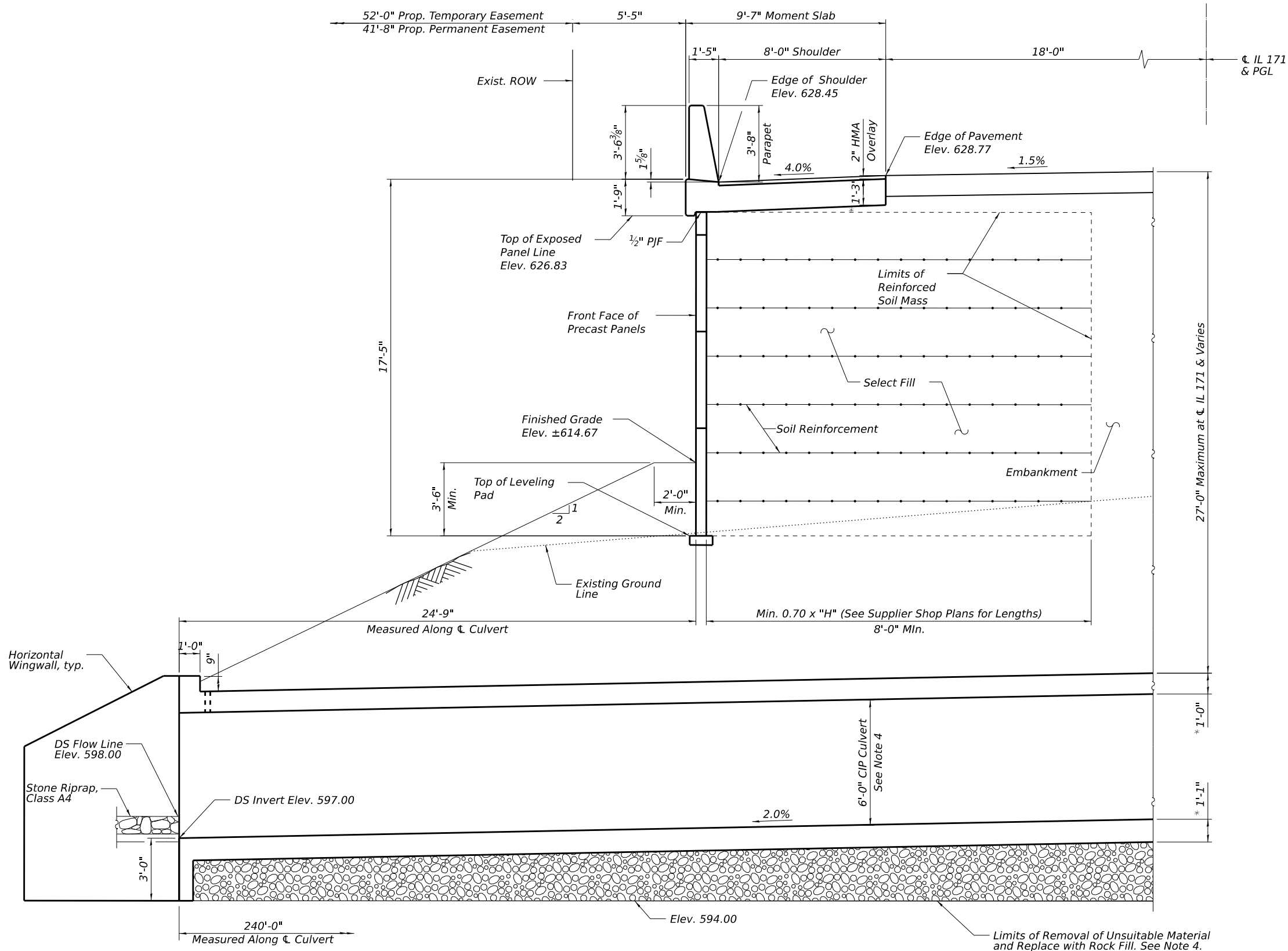
GENERAL PLAN AND ELEVATION  
STRUCTURE NO. 016-2310

SHEET 3 OF 5 SHEETS

F.A.U. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
3565	U-1-N	COOK	5	3
CONTRACT NO. 60R94				
ILLINOIS FED. AID PROJECT				



MODEL: Default  
FILE NAME: I:\13117 - Ames-IDOT IL171 at 95th Street\CADD\CADD\_Sheets\160R94-006-section\_2.dgn



**NOTES:**

- Overexcavation beyond Structure Excavation and Removal of Unsuitable Material is not measured for payment.
- Backfill overexcavation with same material as used for select fill in MSE wall.
- The MSE wall supplier's internal stability design shall account for the anchorage slab's bearing pressure surcharge of 1.0 ksf and horizontal bearing pressure of 0.5kips/ft of wall.
- The limits of the ground improvement are based on soil boring data. The extent of the ground improvement to be verified in the field (See SGR).

**SECTION AT SOUTH CULVERT**

\*Slab thickness may be refined in final design

**SECTION AT CULVERT**  
**RETAINING WALL NO. 1 ALONG**  
**ILLINOIS ROUTE 171 (ARCHER AVE.)**  
**F.A.U. RTE. 3565 - SEC U-1-N**  
**COOK COUNTY**  
**STA. 317+80.13 TO STA. 333+27.91**  
**STRUCTURE NO. 016-2310**

**COLLINS**  
**ENGINEERS**

USER NAME	=	DESIGNED	-	AMS	REVISED	-
		CHECKED	-	EKM	REVISED	-
PLOT SCALE	=	DRAWN	-	DR	REVISED	-
PLOT DATE	=	CHECKED	-	EKM	REVISED	-

**STATE OF ILLINOIS**  
**DEPARTMENT OF TRANSPORTATION**

**RETAINING WALL SECTIONS II**  
**STRUCTURE NO. 016-2310**

SHEET 5 OF 5 SHEETS

F.A.U. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
3565	U-1-N	COOK	5	5
CONTRACT NO. 60R94				
ILLINOIS FED. AID PROJECT				

**APPENDIX B**  
**SOIL BORING LOCATION PLAN AND SUBSURFACE PROFILES**



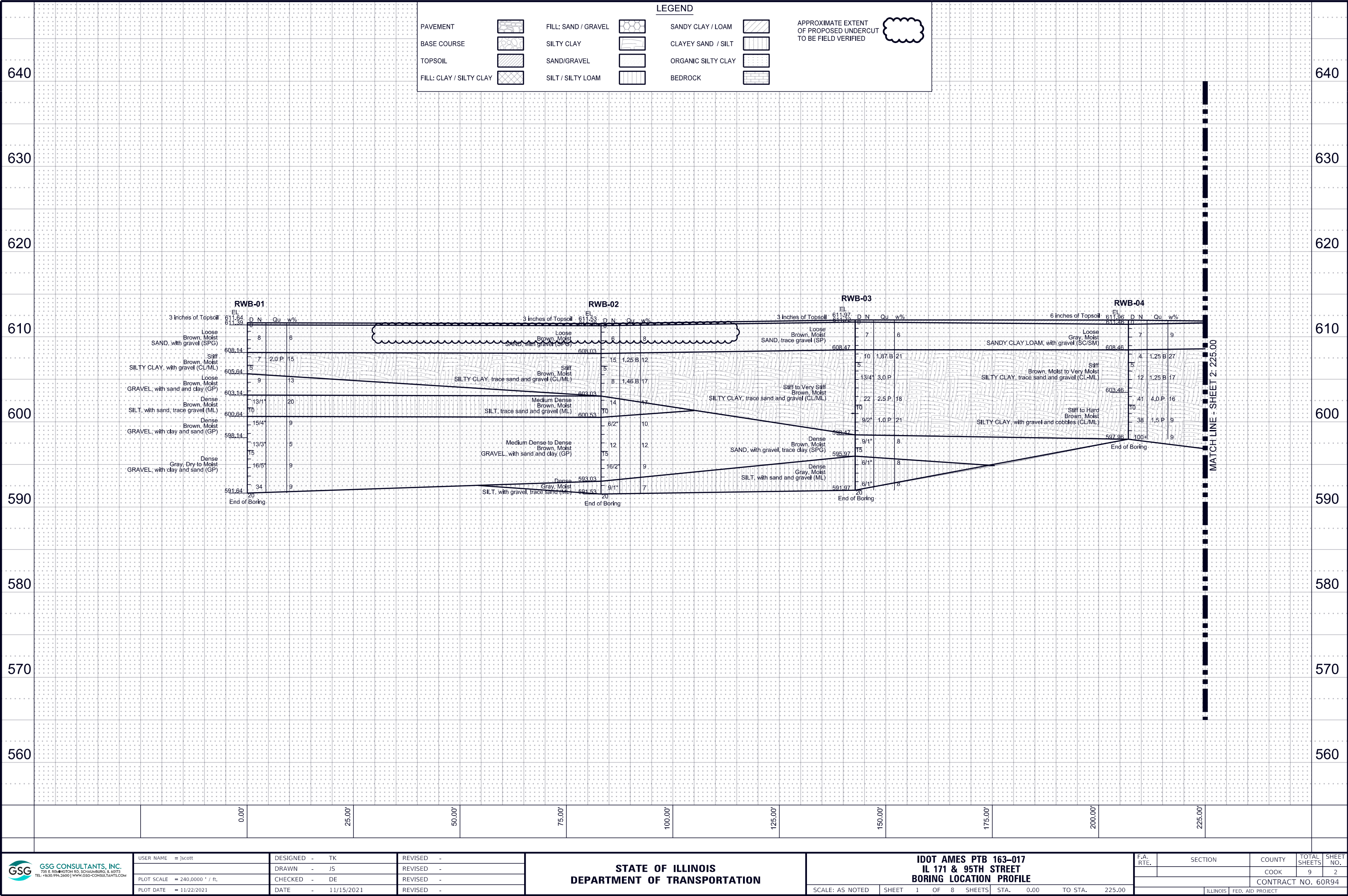


LEGEND

-  RETAINING WALL BORINGS
-  SUBGRADE STABILITY BORINGS
-  SUBGRADE BORINGS
-  TRAFFIC SIGNAL BORINGS

 <div><b>GSG CONSULTANTS, INC.</b> 725 E REMINGTON RD. SCHAMBERG, IL 60193 TEL: +1630.994.2600   WWW.GSG-CONSULTANTS.COM</div>	USER NAME = jscott		DESIGNED - TK	REVISED -	<b>STATE OF ILLINOIS</b> <b>DEPARTMENT OF TRANSPORTATION</b>				<b>IDOT AMES PTB 163-017</b> <b>IL 171 &amp; 95TH STREET</b> <b>BORING LOCATION PLAN</b>				F.A. RTE.	SECTION		COUNTY	TOTAL SHEETS	SHEET NO.
	PLOT SCALE = 1440,0000 ' / ft.		DRAWN - NN	REVISED -											COOK	1	9	
	PLOT DATE = 11/15/2021		CHECKED - DE	REVISED -											CONTRACT NO. 60R94			
			DATE - 11/15/2021	REVISED -	SCALE: 1:60				SHEET 1 OF 1 SHEETS	STA.	TO STA.	ILLINOIS FED. AID PROJECT						

MODEL: Default  
FILE NAME: Trailblaze DOT Ames Engineering 163-017 Geotechnical Exhibits DGNs (PTB 163-017) Retaining Wall Profile-01.dgn



USER NAME = jscott

DESIGNED - TK

REVIS

DRAWN - JS

REVIS

CHECKED - DE

REVIS

PLOT DATE = 11/22/2021

DATE - 11/15/2021

REVIS

STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION

SCALE: AS NOTED  
SHEET 1 OF 8 SHEETS  
STA. 0.00 TO STA. 225.00

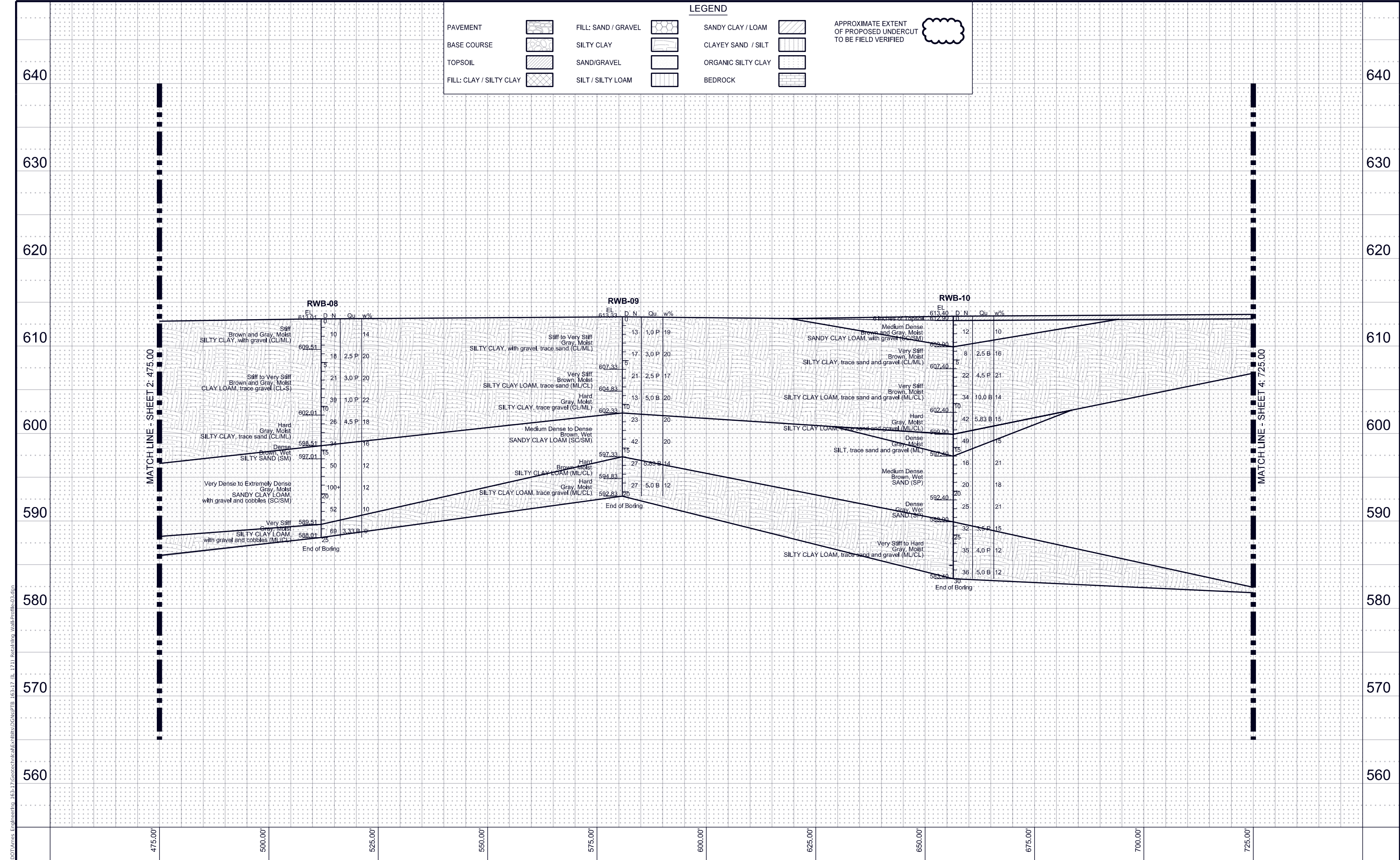
IDOT AMES PTB 163-017  
IL 171 & 95TH STREET  
BORING LOCATION PROFILE

F.A. RTE.  
SECTION  
COUNTY  
COOK  
CONTRACT NO. 60R94  
ILLINOIS FED. AID PROJECT

TOTAL SHEETS 9  
SHEET NO. 2

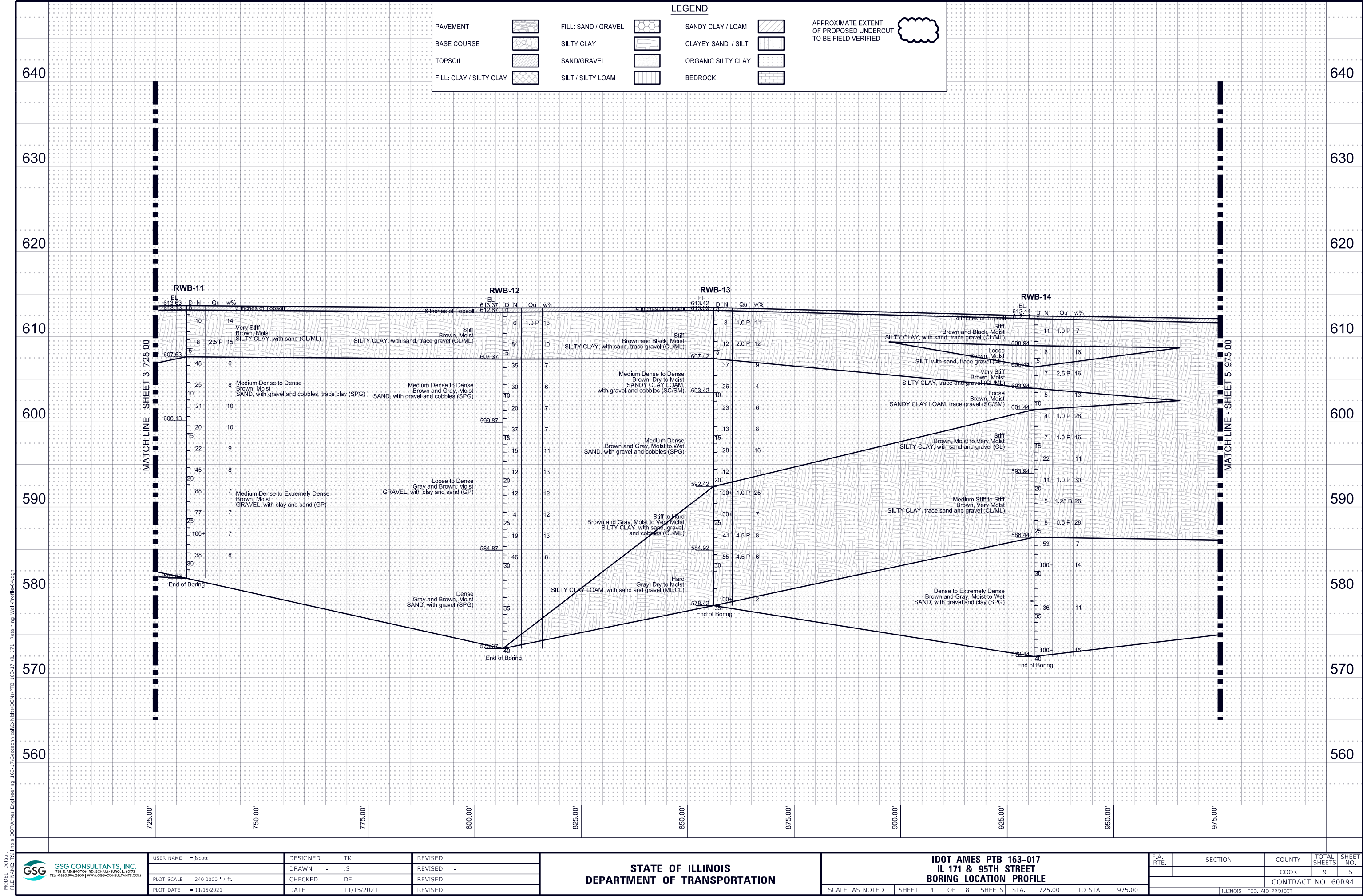






MODEL: Default  
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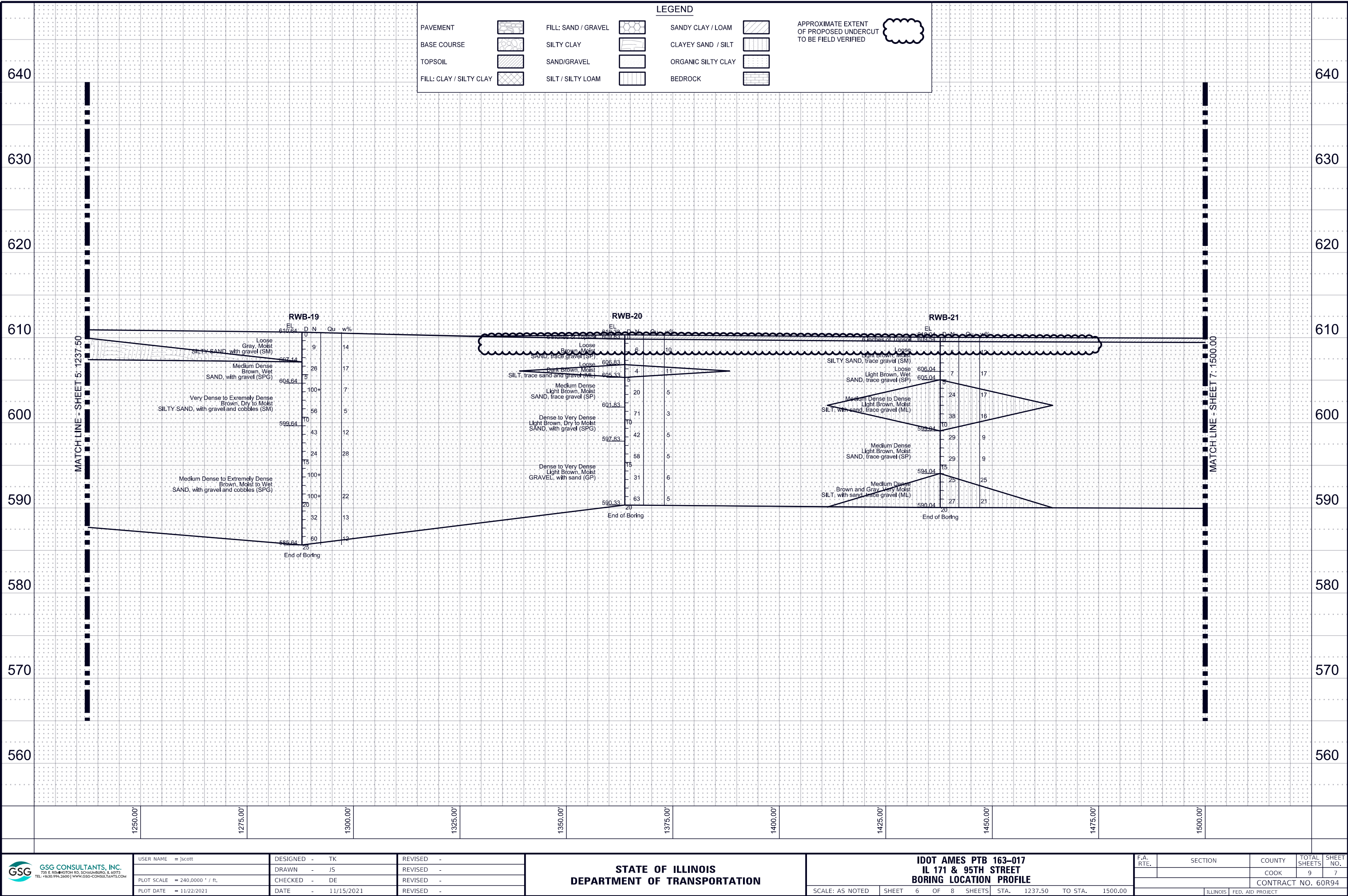








MODEL: Default  
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USER NAME = jscott

DESIGNED - TK

REVISD -

DRAWN - JS

REVISD -

CHECKED - DE

REVISD -

DATE - 11/15/2021

REVISD -

STATE OF ILLINOIS

DEPARTMENT OF TRANSPORTATION

SCALE: AS NOTED

SHEET 6 OF 8 SHEETS

STA. 1237.50 TO STA. 1500.00

IDOT AMES PTB 163-017

IL 171 & 95TH STREET

BORING LOCATION PROFILE

F.A. RTE.

SECTION

COUNTY

TOTAL SHEETS

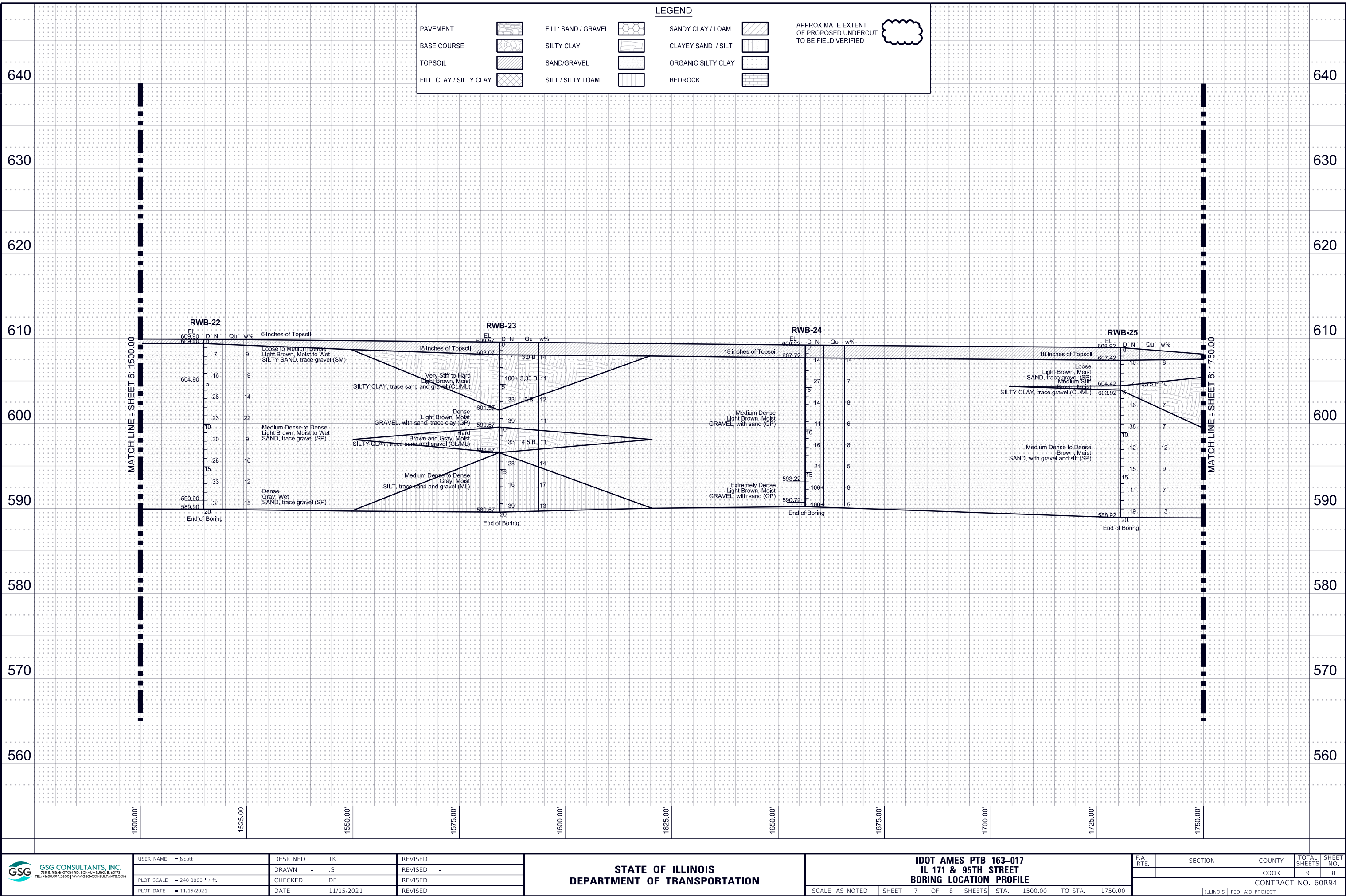
SHEET NO.

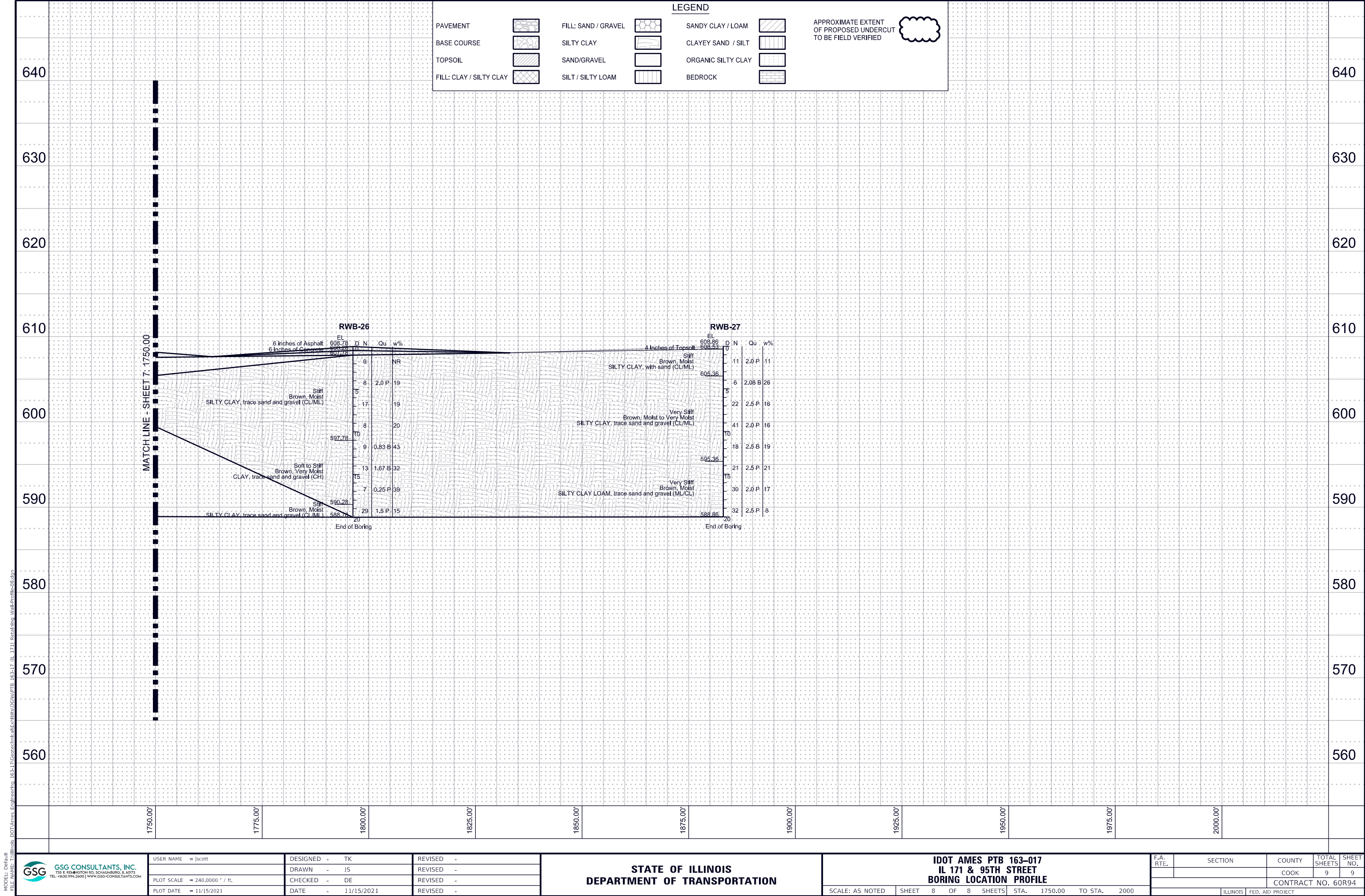
CONTRACT NO. 60R94

ILLINOIS FED. AID PROJECT



MODEL: Default  
FILE NAME: Trailblaze DOT\Ames Engineering 163-017\Geotechnical\Exhibits\Drawings\PTB 163-017 (IL 171) Retaining Wall\Profile-07.dgn





640

630

620

610

600

590

580

570

560

640

630

620

610

600

590

580

570

560

MATCH LINE - SHEET 7: 1750.00

RWB-26

EL 608.78

6 inches of Asphalt

6 inches of Concrete

607.78

9

NR

8

2.0 P 19

17

19

8

20

9

0.83 B 43

13

1.67 B 32

7

0.25 P 39

29

1.5 P 15

20

End of Boring

EL 608.86

4 Inches of Topsoil

608.53

11

2.0 P 11

6

2.08 B 26

22

2.5 P 16

41

2.0 P 16

18

2.5 B 19

21

2.5 P 21

30

2.0 P 17

32

2.5 P 8

20

End of Boring

SILTY CLAY, trace sand and gravel (CL/ML)

Brown, Moist

Stiff

SILTY CLAY, trace sand and gravel (CL/ML)

CLAY, trace sand and gravel (CH)

Soft to Stiff

Brown, Very Moist

SILT

Brown, Moist

SILTY CLAY, trace sand and gravel (CL/ML)

SILTY CLAY, trace sand and gravel (CL/ML)

Brown, Moist

Very Stiff

SILTY CLAY LOAM, trace sand and gravel (ML/CL)

Very Stiff

Brown, Moist

1750.00

1775.00

1800.00

1825.00

1850.00

1875.00

1900.00

1925.00

1950.00

1975.00

2000.00

MODEL: Default

FILE NAME: Trailblaze DOT\Ames Engineering 163-17\Geotechnical\Exhibits\Drawings\PTB 163-17 IL 171 Retaining Wall\Profile-05.dgn

GSG CONSULTANTS, INC.

715 E. 8th Avenue, Suite 200, Schaumburg, IL 60195

TEL: 630.994.2600 | WWW.GSG-CONSULTANTS.COM

USER NAME = jscott

DESIGNED - TK

REVIS

DRAWN - JS

REVISED -

CHECKED - DE

REVISED -

DATE - 11/15/2021

REVISED -

STATE OF ILLINOIS

DEPARTMENT OF TRANSPORTATION

IDOT AMES PTB 163-017

IL 171 & 95TH STREET

BORING LOCATION PROFILE

SCALE: AS NOTED

SHEET 8 OF 8 SHEETS

STA. 1750.00 TO STA. 2000

F.A. RTE.

SECTION

COUNTY

TOTAL SHEETS

SHEET NO.

COOK

9

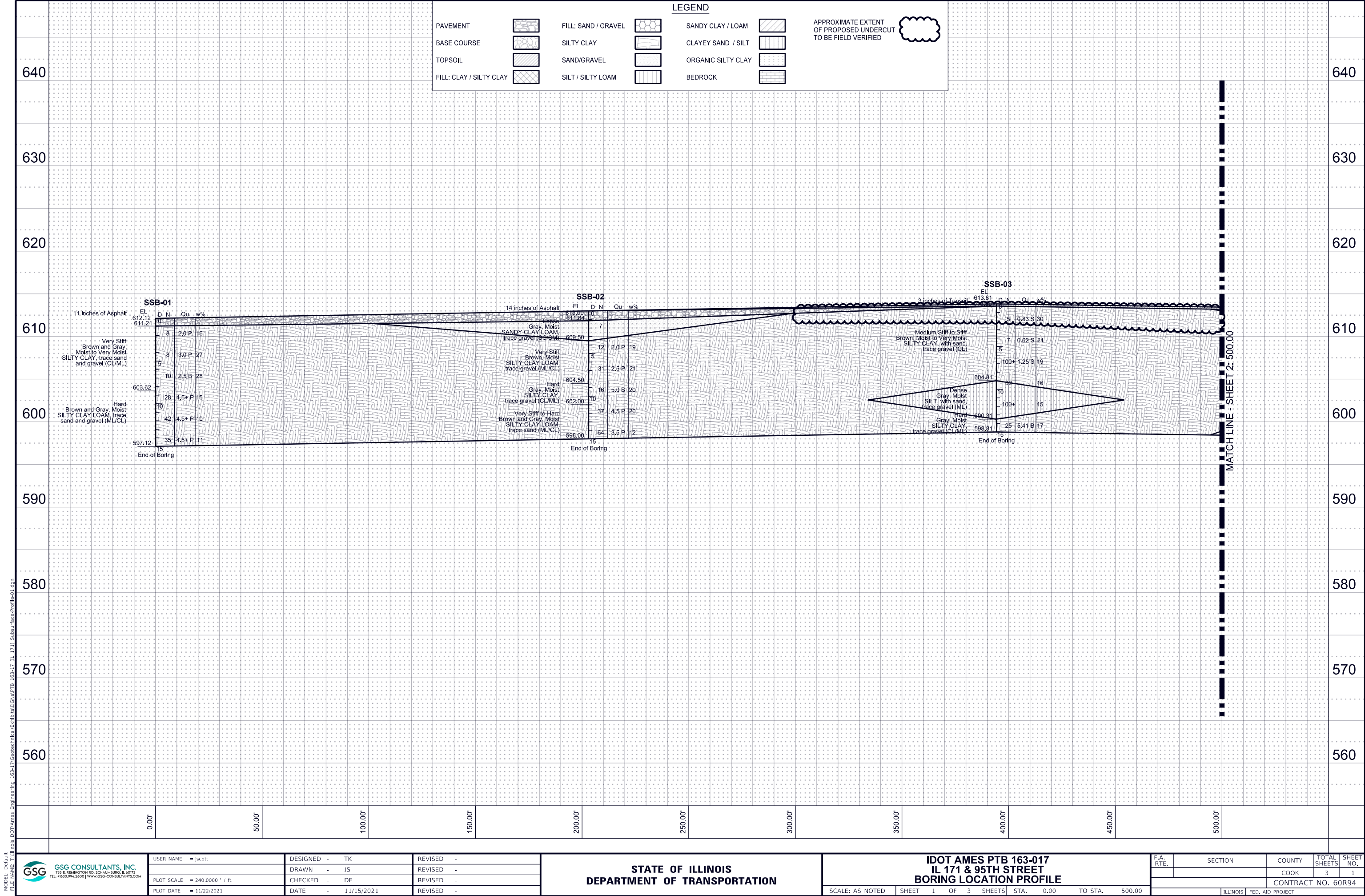
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CONTRACT NO. 60R94

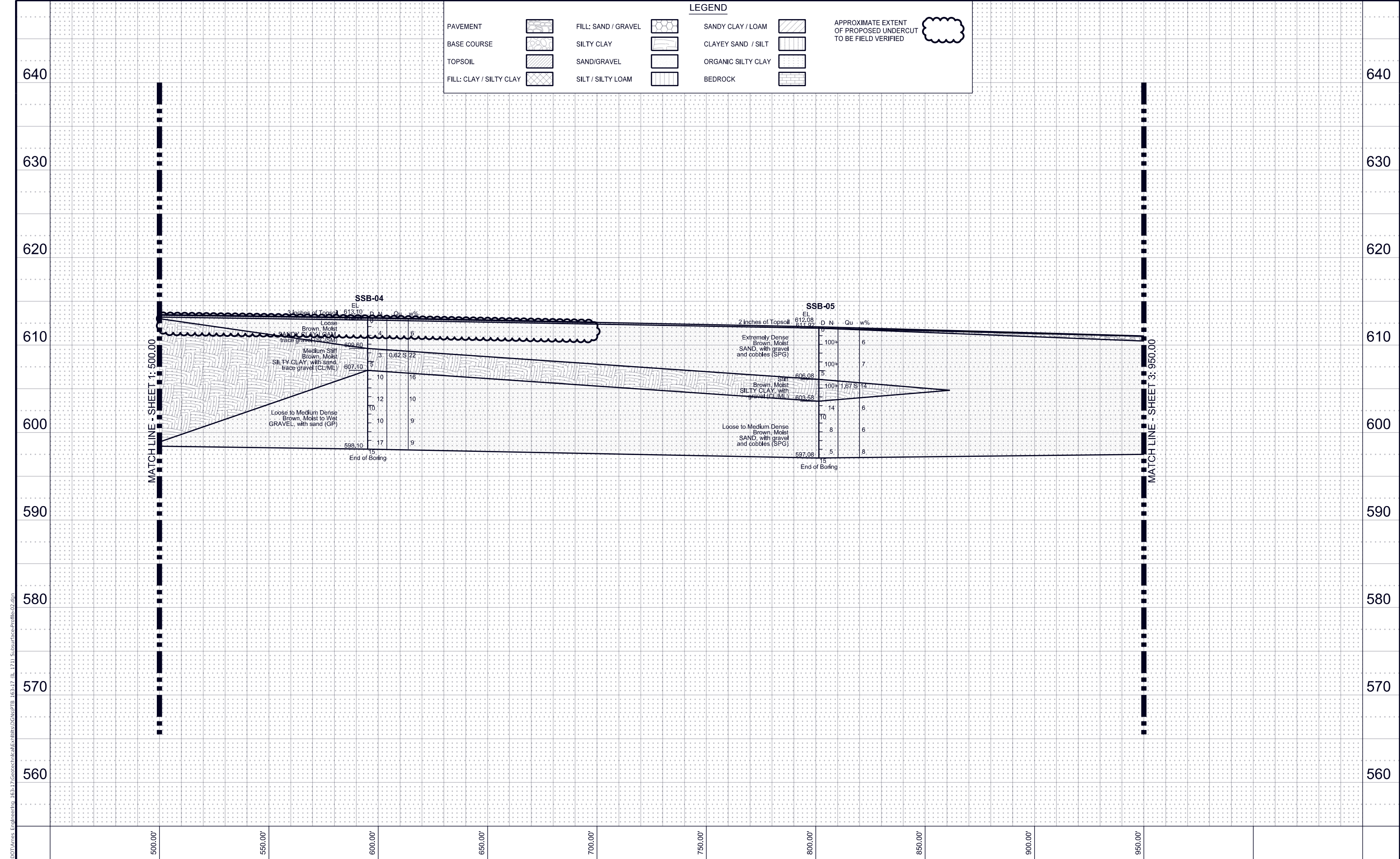
ILLINOIS

FED. AID PROJECT

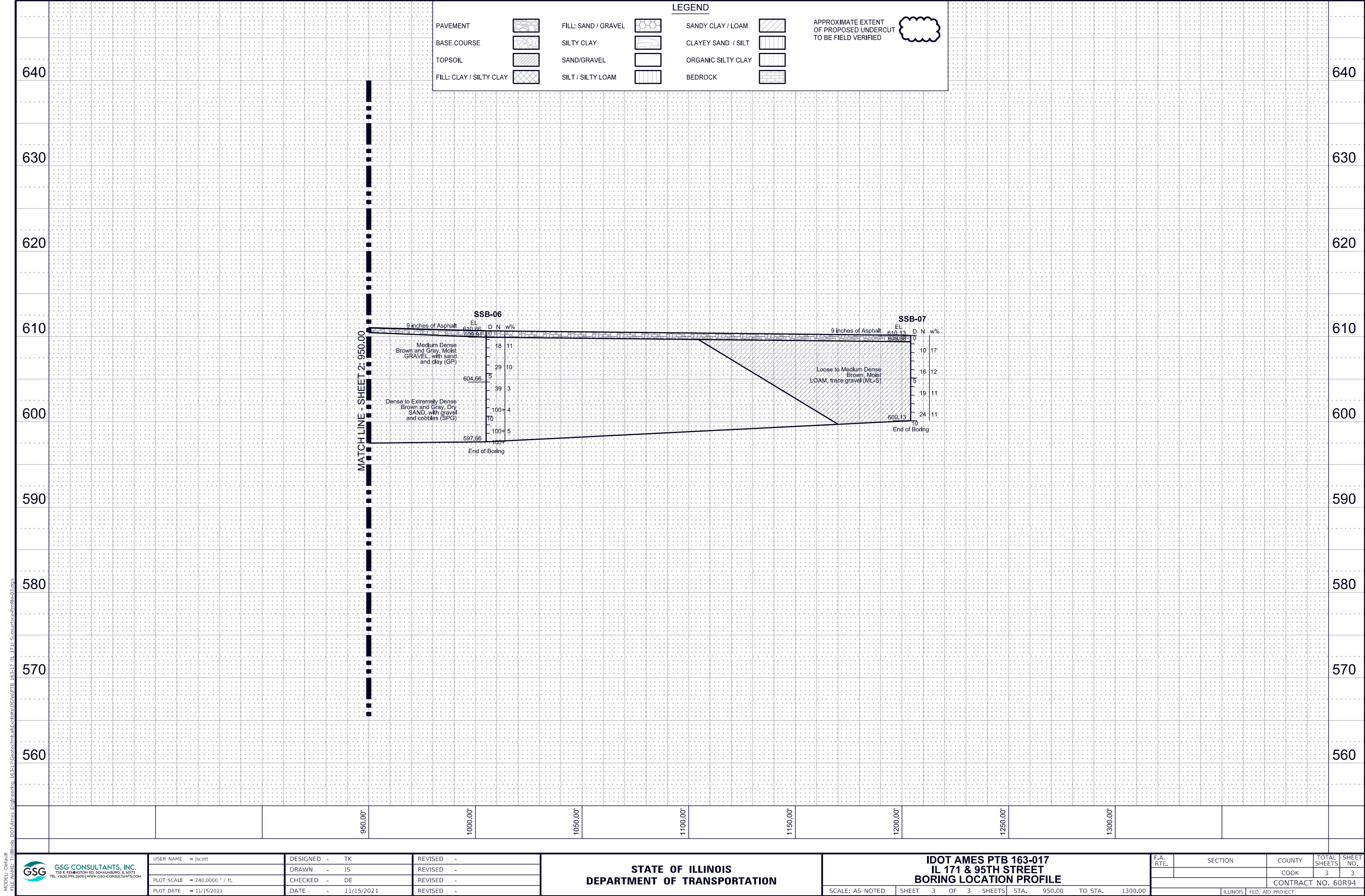








MODEL: Default  
FILE NAME: TrailRoads DOT\Ames Engineering 163-017\Geotechnical\Exhibits\DC\Exh163-017 IL 171 Subsurface Profile-02.dgn



GSG CONSULTANTS, INC.  
715 E. 8th Avenue, Suite 200, Schaumburg, IL 60195  
TEL: 815.309.9944 FAX: 815.309.9945 | WWW.GSG-CONSULTANTS.COM

USER NAME = jscott

DESIGNED - TK

DRAWN - JS

PLOT SCALE = 240,0000 ' / ft.

PLOT DATE = 11/15/2021

DESIGNED - TK

DRAWN - JS

CHECKED - DE

DATE - 11/15/2021

REVISED -

REVISED -

REVISED -

REVISED -

STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION

IDOT AMES PTB 163-017  
IL 171 & 95TH STREET  
BORING LOCATION PROFILE

SCALE: AS NOTED

SHEET 3 OF 3 SHEETS

STA. 950.00 TO STA. 1300.00

F.A. RTE.

SECTION

COUNTY

TOTAL SHEETS

SHEET NO.

COOK

3

3

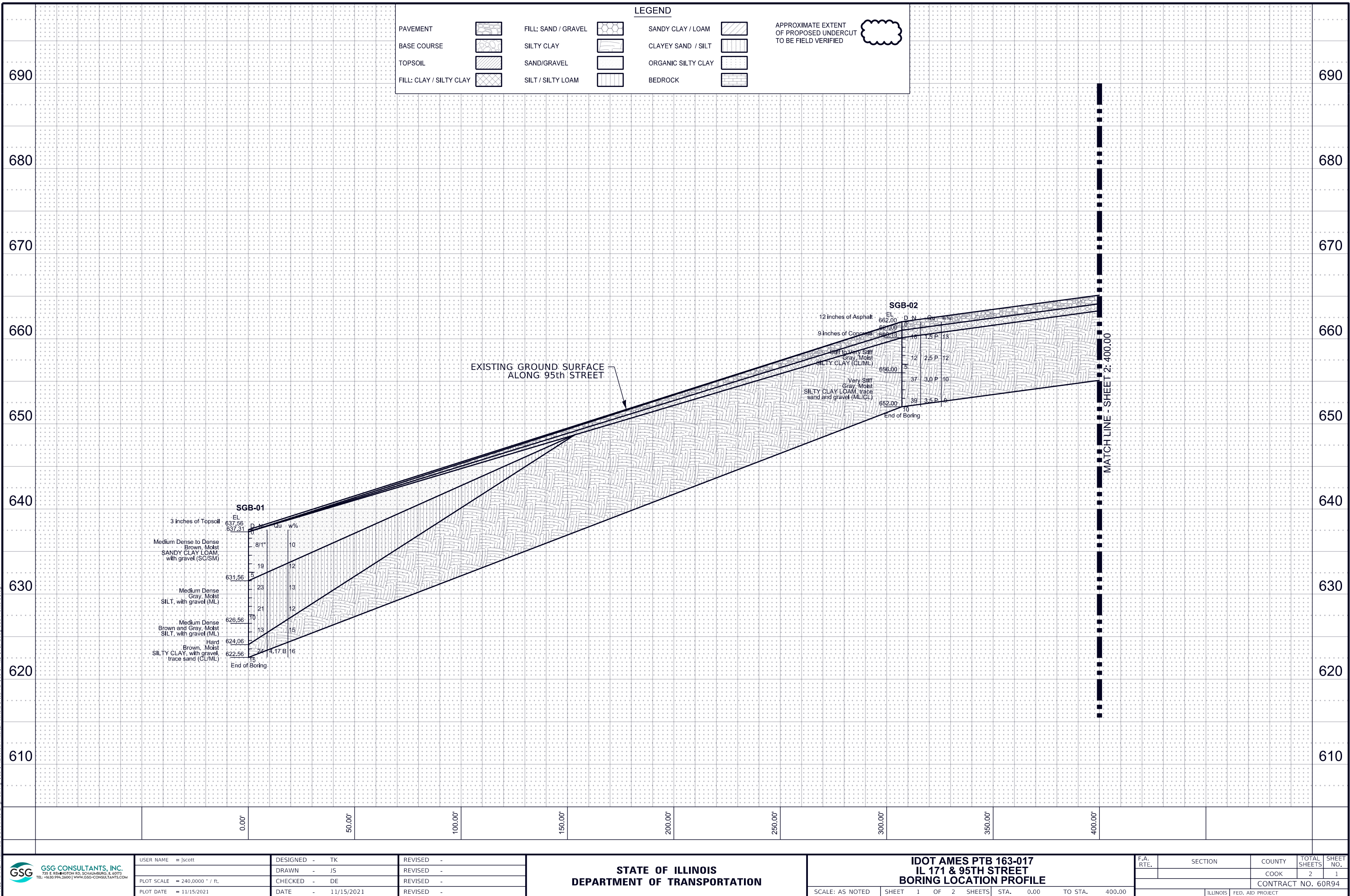
CONTRACT NO. 60R94

ILLINOIS

FED. AID PROJECT

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FILE NAME: Trailblazers DOT Ames Engineering 163-171 Geotechnical Exhibits DGNs (PTB 163-171) Subsurface Profile-03.dgn

MODEL: Default  
FILE NAME: Trilliams DOT\Ames Engineering 163-17\Geotechnical\Borings\PTB 163-17 IL 171 Subgrade-profile-01.dgn



USER NAME = jscott

DESIGNED - TK

DRAWN - JS

CHECKED - DE

DATE - 11/15/2021

REVISED -

REVISED -

REVISED -

REVISED -

STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION

IDOT AMES PTB 163-017  
IL 171 & 95TH STREET  
BORING LOCATION PROFILE

SCALE: AS NOTED

SHEET 1 OF 2 SHEETS

STA. 0.00 TO STA. 400.00

F.A. RTE.

SECTION

COUNTY

TOTAL SHEETS

SHEET NO.

COOK

2

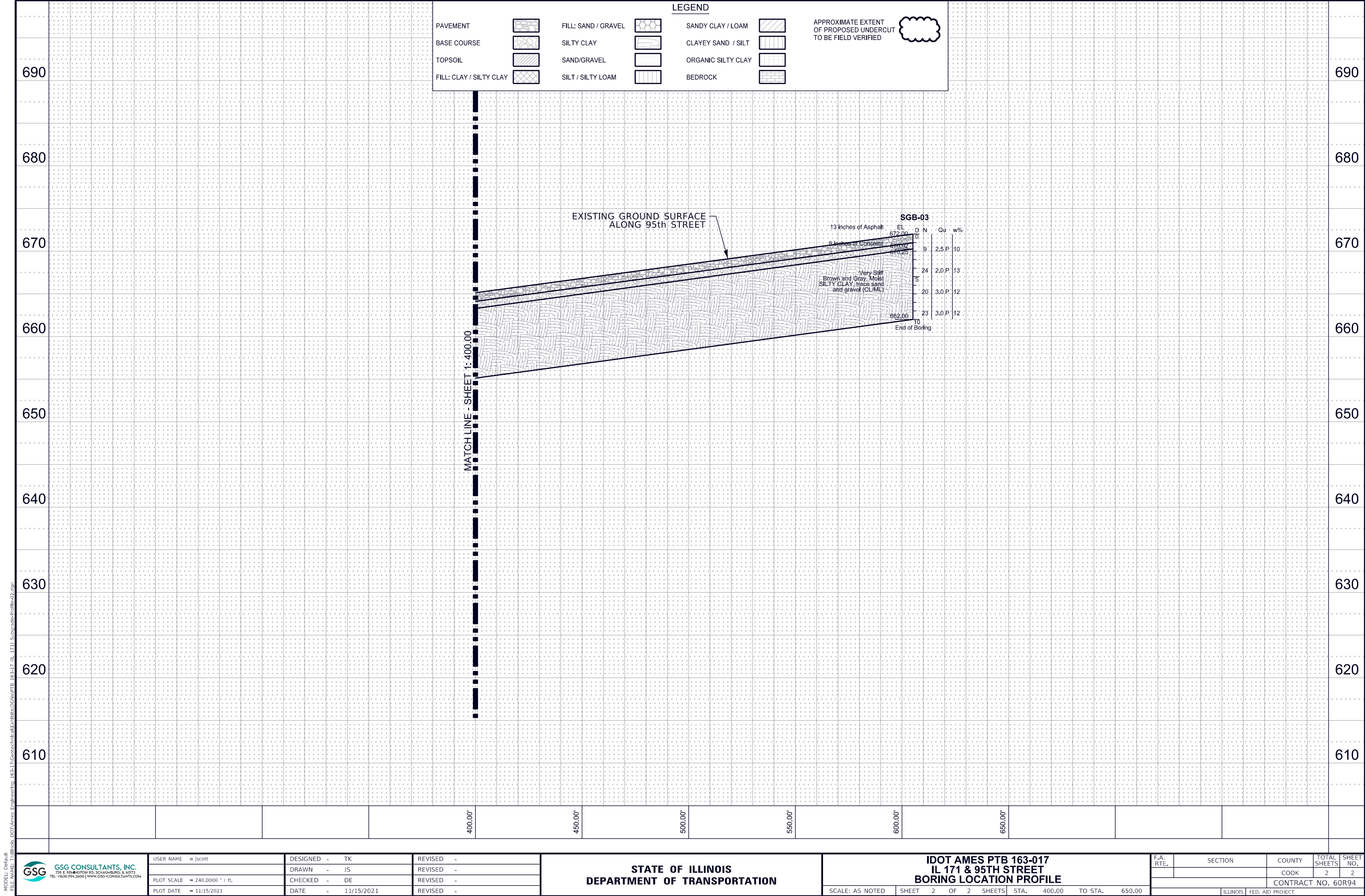
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CONTRACT NO. 60R94

ILLINOIS

FED. AID PROJECT





USER NAME = jscott

DESIGNED - TK

REVIS

DESIGNED - TK

REVIS

DESIGNED - TK

REVIS

DESIGNED - TK

REVIS

DRAWN - JS

CHECKED - DE

DATE - 11/15/2021

DRAWN - JS

CHECKED - DE

DATE - 11/15/2021

REVIS

REVIS

REVIS

REVIS

REVIS

REVIS

REVIS

REVIS

STATE OF ILLINOIS

DEPARTMENT OF TRANSPORTATION

IDOT AMES PTB 163-017

IL 171 & 95TH STREET

BORING LOCATION PROFILE

SCALE: AS NOTED

SHEET 2 OF 2 SHEETS

STA. 400.00 TO STA. 650.00

F.A. RTE.

SECTION

COUNTY

TOTAL SHEETS

SHEET NO.

COOK

2

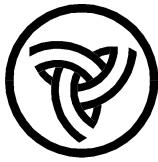
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CONTRACT NO. 60R94

ILLINOIS

FED. AID PROJECT

**APPENDIX C**  
**SOIL BORING LOGS**



# Illinois Department of Transportation

Division of Highways  
GSG Consultants, Inc.

## SOIL BORING LOG

Page 1 of 1

Date 6/17/21

ROUTE 95th Street DESCRIPTION Retaining Wall Boring LOGGED BY JB

SECTION IL 171 & 95th Street LOCATION IL 171, SEC. 22, TWP. 37N, RNG. 12E,

Latitude 41.7161228, Longitude -87.900791  
Diedrich D-50

COUNTY COOK DRILLING RIG HSA HAMMER TYPE AUTO  
DRILLING METHOD HSA HAMMER EFF (%) 92

STRUCT. NO. SN 016-2310  
Station Sta. 317+80.13 to 333+27.91

BORING NO. RWB-01  
Station 316+1.26  
Offset 43.32ft RT  
Ground Surface Elev. 611.64 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
-------------------------------	--------------------------------	----------------------------	------------------------------

Surface Water Elev. N/A ft  
Stream Bed Elev. N/A ft  
Groundwater Elev.:  
First Encounter 603.1 ft ▼  
Upon Completion N/A ft  
After N/A Hrs. N/A ft

3 inches of Topsoil	611.39			
Loose				
Brown, Moist		8		
SAND, with gravel (SPG)		5		6
		3		
	608.14			
Stiff		3		
Brown, Moist		3	2.0	15
SILTY CLAY, with gravel (CL/ML)		4	P	
		-5		
	605.64			
Loose		6		
Brown, Moist		5		13
GRAVEL, with sand and clay (GP)		4		
	603.14 ▼			
Dense		11		
Brown, Moist		13/1"		20
SILT, with sand, trace gravel (ML)				
		-10		
	600.64			
Dense		11		
Brown, Moist		15/4"		9
GRAVEL, with clay and sand (GP)				
	598.14			
Dense		13		
Gray, Dry to Moist		13/3"		5
GRAVEL, with clay and sand (GP)				
		-15		
		16/5"		
				9
		15		
		16		9
		18		
	591.64 -20			

End of Boring

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)

The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, form 137 (Rev. 8-99)



# Illinois Department of Transportation

Division of Highways  
GSG Consultants, Inc.

## SOIL BORING LOG

Page 1 of 1

Date 6/17/21

ROUTE 95th Street DESCRIPTION Retaining Wall Boring LOGGED BY JB

SECTION IL 171 & 95th Street LOCATION IL 171, SEC. 22, TWP. 37N, RNG. 12E,

Latitude 41.7161942, Longitude -87.900502

COUNTY COOK DRILLING RIG Diedrich D-50 HAMMER TYPE AUTO

DRILLING METHOD

HSA

HAMMER EFF (%)

92

STRUCT. NO. SN 016-2310  
Station Sta. 317+80.13 to 333+27.91

BORING NO. RWB-02  
Station 316+84.34  
Offset 43.02ft RT  
Ground Surface Elev. 611.53 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
-------------------------------	--------------------------------	----------------------------	------------------------------

Surface Water Elev. N/A ft  
Stream Bed Elev. N/A ft

Groundwater Elev.:  
First Encounter None ft  
Upon Completion N/A ft  
After N/A Hrs. N/A ft

3 inches of Topsoil	611.28			
Loose				
Brown, Moist		6		
SAND, with gravel (SPG)		3		8
		3		
	608.03			
Stiff		5		
Brown, Moist		8	1.3	12
SILTY CLAY, trace sand and		7	B	
gravel (CL/ML)		-5		
		2		
		3	1.5	17
		5	B	
	603.03			
Medium Dense		7		
Brown, Moist		8		17
SILT, trace sand and gravel (ML)		6		
		-10		
	600.53			
Medium Dense to Dense		13		
Brown, Moist		13		10
GRAVEL, with sand and clay (GP)		6/2"		
		11		
		6		12
		6		
		-15		
		16/2"		
				9
	593.03			
Dense		18		
Gray, Moist		9/1"		7
SILT, with gravel, trace sand (ML)				
	591.53	-20		

End of Boring

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)

The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, form 137 (Rev. 8-99)



# Illinois Department of Transportation

Division of Highways  
GSG Consultants, Inc.

## SOIL BORING LOG

Page 1 of 1

Date 6/17/21

ROUTE 95th Street DESCRIPTION Retaining Wall Boring LOGGED BY JB

SECTION IL 171 & 95th Street LOCATION IL 171, SEC. 22, TWP. 37N, RNG. 12E,

Latitude 41.7162446, Longitude -87.9002941  
Diedrich D-50

COUNTY COOK DRILLING RIG HSA HAMMER TYPE AUTO  
DRILLING METHOD HSA HAMMER EFF (%) 92

STRUCT. NO. SN 016-2310  
Station Sta. 317+80.13 to 333+27.91

BORING NO. RWB-03  
Station 317+44.00  
Offset 43.11ft RT  
Ground Surface Elev. 611.97 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
-------------------------------	--------------------------------	----------------------------	------------------------------

Surface Water Elev. N/A ft  
Stream Bed Elev. N/A ft  
Groundwater Elev.:  
First Encounter 601.0 ft ▼  
Upon Completion N/A ft  
After N/A Hrs. N/A ft

3 inches of Topsoil	611.72			
Loose				
Brown, Moist		4		
SAND, trace gravel (SP)		4		6
		3		
	608.47			
Stiff to Very Stiff		4		
Brown, Moist		5	1.9	21
SILTY CLAY, trace sand and		5	B	
gravel (CL/ML)		-5		
Little recovery at 6-7.5 feet		13/4"		
			3.0	
			P	
		12		
		12	2.5	18
		10	P	
	-10			
		8		
		11	1.0	21
		9/2"	P	
	598.47			
Dense		18		
Brown, Moist		28		8
SAND, with gravel, trace clay		9/1"		
(SPG)		-15		
	595.97			
Dense		6		
Gray, Moist		20		8
SILT, with sand and gravel (ML)		6/1"		
		23		
		25		8
		6/1"		
	591.97	-20		

End of Boring

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)

The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

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<b>ROUTE</b>	95th Street	<b>DESCRIPTION</b>	Retaining Wall Boring	<b>LOGGED BY</b>	EH
--------------	-------------	--------------------	-----------------------	------------------	----

**SECTION** IL 171 & 95th Street **LOCATION** IL 171, SEC. 22, TWP. 37N, RNG. 12E,

COUNTY	COOK	DRILLING RIG	Latitude 41.7163001, Longitude -87.900071	
		DRILLING METHOD	Diedrich D-50	HAMMER TYPE
			HSA	AUTO
				HAMMER EFF (%)
				92

**STRUCT. NO.** SN 016-2310  
**Station** Sta. 317+80.13 to 333+27.91

<b>BORING NO.</b>	RWB-04
<b>Station</b>	318+8.19
<b>Offset</b>	42.74ft RT
<b>Ground Surface Elev.</b>	611.96

D E P T H	B L O W S	U C S  Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

Surface Water Elev.	N/A	ft
Stream Bed Elev.	N/A	ft
Groundwater Elev.:		
First Encounter	None	ft
Upon Completion	N/A	ft
After N/A Hrs.	N/A	ft

[illegible]

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, form 137 (Rev. 8-99)



# Illinois Department of Transportation

Division of Highways  
GSG Consultants, Inc.

## SOIL BORING LOG

Page 1 of 1

Date 6/17/21

ROUTE 95th Street DESCRIPTION Retaining Wall Boring LOGGED BY EH

SECTION IL 171 & 95th Street LOCATION IL 171, SEC. 22, TWP. 37N, RNG. 12E,

Latitude 41.7163728, Longitude -87.8998225  
Diedrich D-50

COUNTY COOK DRILLING RIG HSA HAMMER TYPE AUTO  
DRILLING METHOD HSA HAMMER EFF (%) 92

STRUCT. NO. SN 016-2310  
Station Sta. 317+80.13 to 333+27.91

BORING NO. RWB-05  
Station 318+80.90  
Offset 38.55ft RT  
Ground Surface Elev. 612.42 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
-------------------------------	--------------------------------	----------------------------	------------------------------

Surface Water Elev. N/A ft  
Stream Bed Elev. N/A ft  
Groundwater Elev.:  
First Encounter None ft  
Upon Completion N/A ft  
After N/A Hrs. N/A ft

Medium Dense Gray, Moist SANDY CLAY LOAM, with gravel (SC/SM)	7 5 9		7
608.92	3		
Stiff Gray and Brown, Moist SILTY CLAY, with sand and gravel (CL/ML)	3 4 -5	1.0 P	20
606.42	5		
Stiff to Hard Brown, Moist SILTY CLAY LOAM, trace sand and gravel (ML/CL)	8 11	2.5 P	15
	5 8 10 -10		18
	7 13 14		15
598.92	12		
Stiff to Very Stiff Brown, Dry to Moist CLAY LOAM, with gravel and cobbles (CL-S)	48 37 -15	3.0 P	11
	11 50/5"	1.0 P	12
593.42	50/4"		5
Split-spoon refusal at 19 feet			
End of Boring			
-20			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, form 137 (Rev. 8-99)



# Illinois Department of Transportation

Division of Highways  
GSG Consultants, Inc.

## SOIL BORING LOG

Page 1 of 1

Date 6/16/21

ROUTE 95th Street DESCRIPTION Retaining Wall Boring LOGGED BY EH

SECTION IL 171 & 95th Street LOCATION IL 171, SEC. 22, TWP. 37N, RNG. 12E.

COUNTY COOK DRILLING RIG Diedrich D-50 Latitude 41.7164652, Longitude -87.8995463  
DRILLING METHOD HSA HAMMER TYPE AUTO  
HAMMER EFF (%) 92

STRUCT. NO. SN 016-2310  
Station Sta. 317+80.13 to 333+27.91

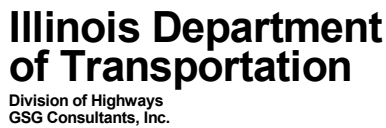
BORING NO. RWB-06  
Station 319+63.02  
Offset 29.88ft RT  
Ground Surface Elev. 611.98 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
-------------------------------	--------------------------------	----------------------------	------------------------------

Surface Water Elev. N/A ft  
Stream Bed Elev. N/A ft  
Groundwater Elev.:  
First Encounter None ft  
Upon Completion N/A ft  
After N/A Hrs. N/A ft

Medium Dense Gray, Moist SILTY SAND, with gravel (SM)	7		
	9		5
	10		
608.48			
Stiff Brown, Moist SILTY CLAY, trace sand and gravel (CL/ML)	3		
	4	1.0	14
	4	P	
	7		
	10	1.5	15
	8	P	
	4		
	5	1.0	20
	13	P	
-10			
	7		
	7	1.5	16
	7	P	
598.48			
Very Stiff to Hard Brown, Moist CLAY LOAM, with gravel (CL-S)	8		
	42	4.5	7
	29	P	
-15			
	6		
	17	3.0	13
	42	P	
594.48			
Auger refusal at 17.5 feet			
End of Boring			
-20			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

Page 1 of 1

**Date** 6/16/21

Stiff Brown, Moist CLAY LOAM, with gravel (CL-S)					591.49			
	6				Medium Dense to Very Dense	12		
	7	1.5	10		Brown, Moist	13		13
	6	P			SANDY CLAY LOAM, with gravel and cobbles (SC/SM)	13		
	2					12		
	2	1.0	17			33		9
	3	P				28		
	-5					-25		
					586.49			
	5				Hard	10		
	7	2.0	16		Gray, Moist	15	4.5	11
	7	P			SILTY CLAY LOAM, with gravel (ML/CL)	26	P	
603.99					583.99			
Very Stiff to Hard	4				Extremely Dense	583.49	50/6"	10
Brown, Moist	7	2.5	17		Brown and Gray, Moist			
SILTY CLAY LOAM, trace sand and gravel (ML/CL)	9	B			SAND, with gravel (SPG)			
	-10				Split-spoon refusal at 29 feet	-30		
					End of Boring			
	6							
	10	4.5	18					
	12	P						
598.99								
Hard	4							
Gray, Moist	7	6.3	17					
SILTY CLAY, trace sand and gravel (CL/ML)	10	B				-35		
596.49								
Stiff	12							
Gray, Moist	19	1.0	16					
SILTY CLAY LOAM, trace sand and gravel (ML/CL)	18	P						
593.99								
Dense	14							
Brown, Moist	15		14					
SAND, trace gravel (SP)	15					-40		

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# Illinois Department of Transportation

Division of Highways  
GSG Consultants, Inc.

## SOIL BORING LOG

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Date 6/9/21

ROUTE 95th Street DESCRIPTION Retaining Wall Boring LOGGED BY EH

SECTION IL 171 & 95th Street LOCATION IL 171, SEC. 22, TWP. 37N, RNG. 12E,

COUNTY COOK DRILLING RIG Diedrich D-50 Latitude 41.7165766, Longitude -87.8990195  
DRILLING METHOD HSA HAMMER TYPE AUTO HAMMER EFF (%) 92

STRUCT. NO. SN 016-2310  
Station Sta. 317+80.13 to 333+27.91

BORING NO. RWB-08  
Station 321+11.99  
Offset 36.09ft RT  
Ground Surface Elev. 613.01 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)	Surface Water Elev. <u>N/A</u> ft	Stream Bed Elev. <u>N/A</u> ft	Groundwater Elev.: First Encounter <u>None</u> ft Upon Completion <u>N/A</u> ft After <u>N/A</u> Hrs. <u>N/A</u> ft	D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
	9		14					27		
	6							24		10
	4							28		
609.51				589.51						
	4							14		
	8	2.5	20					34	3.3	9
-5	10	P		588.01			-25	35	B	
	5									
	10	3.0	20							
	11	P								
	28									
	18	1.0	22							
-10	21	P					-30			
602.01										
	15									
	14	4.5	18							
	12	P								
	10									
598.51										
	16		16							
-15	18						-35			
597.01										
	12									
	20		12							
	30									
	30									
	50/2"		12							
-20							-40			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, form 137 (Rev. 8-99)



# Illinois Department of Transportation

Division of Highways  
GSG Consultants, Inc.

## SOIL BORING LOG

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Date 6/9/21

ROUTE 95th Street DESCRIPTION Retaining Wall Boring LOGGED BY EH

SECTION IL 171 & 95th Street LOCATION IL 171, SEC. 22, TWP. 37N, RNG. 12E,

COUNTY COOK DRILLING RIG Diedrich D-50 Latitude 41.7166294, Longitude -87.8987774  
DRILLING METHOD HSA HAMMER TYPE AUTO HAMMER EFF (%) 92

STRUCT. NO. SN 016-2310  
Station Sta. 317+80.13 to 333+27.91

BORING NO. RWB-09  
Station 321+80.29  
Offset 39.38ft RT  
Ground Surface Elev. 613.33 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)	Surface Water Elev. <u>N/A</u> ft	Stream Bed Elev. <u>N/A</u> ft	Groundwater Elev.: First Encounter <u>None</u> ft Upon Completion <u>N/A</u> ft After <u>N/A</u> Hrs. <u>N/A</u> ft	D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
	8	1.0	19							
	7	P								
	6									
	6									
	7	3.0	20							
	10	P								
	-5									
	6									
	9	2.5	17							
	12	P								
	3									
	5	5.0	20							
	8	B								
	-10									
	6									
	10		20							
	13									
	4									
	10		20							
	32									
	-15									
	13									
	11	5.8	14							
	16	B								
	10									
	13	5.0	12							
	14	B								
	-20									

Stiff to Very Stiff  
Gray, Moist  
SILTY CLAY, with gravel, trace sand (CL/ML)

607.33

Very Stiff  
Brown, Moist  
SILTY CLAY LOAM, trace sand (ML/CL)

604.83

Hard  
Gray, Moist  
SILTY CLAY, trace gravel (CL/ML)

602.33

Medium Dense to Dense  
Brown, Wet  
SANDY CLAY LOAM (SC/SM)

Cobbles at 13.5-15 feet

597.33

Hard  
Brown, Moist  
SILTY CLAY LOAM (ML/CL)

594.83

Hard  
Gray, Moist  
SILTY CLAY LOAM, trace gravel (ML/CL) (continued)  
Auger refusal at 20.5 feet  
End of Boring

592.83

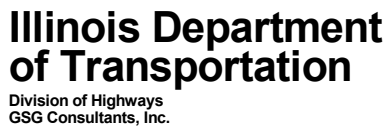
-25

-30

-35

-40

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

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**Date** 6/16/21

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# Illinois Department of Transportation

Division of Highways  
GSG Consultants, Inc.

## SOIL BORING LOG

Page 1 of 1

Date 6/15/21

ROUTE 95th Street DESCRIPTION Retaining Wall Boring LOGGED BY EH

SECTION IL 171 & 95th Street LOCATION IL 171, SEC. 22, TWP. 37N, RNG. 12E,

Latitude 41.7167659, Longitude -87.8982534  
CME-75

COUNTY COOK DRILLING RIG CME-75 DRILLING METHOD HSA HAMMER TYPE AUTO HAMMER EFF (%) 91

STRUCT. NO. SN 016-2310  
Station Sta. 317+80.13 to 333+27.91

BORING NO. RWB-11  
Station 323+30.65  
Offset 41.78ft RT  
Ground Surface Elev. 613.63 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)	Surface Water Elev. <u>N/A</u> ft	Stream Bed Elev. <u>N/A</u> ft	D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
				Groundwater Elev.:					
				First Encounter <u>None</u> ft					
				Upon Completion <u>N/A</u> ft					
				After <u>N/A</u> Hrs. <u>N/A</u> ft					
6 inches of Topsoil <u>613.13</u>				Medium Dense to Extremely Dense					
Very Stiff				Brown, Moist			16		
Brown, Moist	9			GRAVEL, with clay and sand (GP)			42		7
SILTY CLAY, with sand (CL/ML)	5		14	(continued)			46		
	5								
	3						15		
	3	2.5	15				43		7
	5	P					34		
	-5					-25			
<u>607.63</u>							21		
Medium Dense to Dense	11						50/5"		7
Brown, Moist	24		6						
SAND, with gravel and cobbles, trace clay (SPG)	24								
	10						19		
	14		8				25		8
	11					-30	13		
	-10								
	8								
	10		10						
	11			Auger refusal at 32 feet <u>581.63</u>					
				End of Boring					
<u>600.13</u>									
Medium Dense to Extremely Dense	9								
Brown, Moist	11		10						
GRAVEL, with clay and sand (GP)	9								
	-15					-35			
	13								
	12		9						
	10								
	16								
	23		8						
	22								
	-20					-40			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

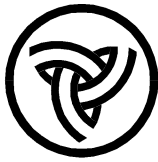
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**Date** 6/21/21

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# Illinois Department of Transportation

Division of Highways  
GSG Consultants, Inc.

## SOIL BORING LOG

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Date 6/14/21

ROUTE 95th Street DESCRIPTION Retaining Wall Boring LOGGED BY EH

SECTION IL 171 & 95th Street LOCATION IL 171, SEC. 22, TWP. 37N, RNG. 12E,

Latitude 41.7168983, Longitude -87.8978358  
CME-75

COUNTY COOK DRILLING RIG HSA HAMMER TYPE AUTO  
DRILLING METHOD HSA HAMMER EFF (%) 91

STRUCT. NO. SN 016-2310  
Station Sta. 317+80.13 to 333+27.91

BORING NO. RWB-13  
Station 324+53.54  
Offset 38.61ft RT  
Ground Surface Elev. 613.42 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)	Surface Water Elev. <u>N/A</u> ft	Stream Bed Elev. <u>N/A</u> ft	D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
				Groundwater Elev.:					
				First Encounter <u>None</u> ft					
				Upon Completion <u>N/A</u> ft					
				After <u>N/A</u> Hrs. <u>N/A</u> ft					
4 inches of Topsoil	613.09								
Stiff				592.42					
Brown and Black, Moist	5			Stiff to Hard		2			
SILTY CLAY, with sand, trace	2	1.0	11	Brown and Gray, Moist to Very		3	1.0	25	
gravel (CL/ML)	6	P		Moist		50/5"	P		
				SILTY CLAY, with sand, gravel,					
	4			and cobbles (CL/ML)		50/4"			
	6	2.0	12					7	
	-5	P				-25			
607.42									
Medium Dense to Dense	12					20			
Brown, Dry to Moist	17		9			15	4.5	8	
SANDY CLAY LOAM, with gravel	20					26	P		
and cobbles (SC/SM)									
	18			584.92		12			
	16		4	Hard		23	4.5	6	
	10			Gray, Dry to Moist		32	P		
603.42 -10				SILTY CLAY LOAM, with sand		-30			
Medium Dense				and gravel (ML/CL)					
Brown and Gray, Moist to Wet	6								
SAND, with gravel and cobbles	9		6						
(SPG)	14								
	6					50/3"			
	6		8						
	7							2	
-15				Auger refusal at 35 feet	578.42	-35			
				End of Boring					
	14								
	10		16						
	18								
	8								
	7		11						
-20	5					-40			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

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**Date** 6/14/21

BBS, form 137 (Rev. 8-99)

<b>ROUTE</b>	95th Street	<b>DESCRIPTION</b>	Retaining Wall Boring	<b>LOGGED BY</b>	EH
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**SECTION** IL 171 & 95th Street **LOCATION** IL 171, SEC. 22, TWP. 37N, RNG. 12E,

**Latitude** 41.7170697, **Longitude** -87.897332

COUNTY	COOK	DRILLING RIG	CME-75	HAMMER TYPE	AUTO
		DRILLING METHOD	HSA	HAMMER EFF (%)	91

**STRUCT. NO.** SN 016-2310  
**Station** Sta. 317+80.13 to 333+27.91

<b>BORING NO.</b>	RWB-15
<b>Station</b>	326+3.57
<b>Offset</b>	34.52ft RT
<b>Ground Surface Elev.</b>	611.88

DEPTH	BLOWS	UCS	MOST
(ft)	(/6")	(tsf)	(%)

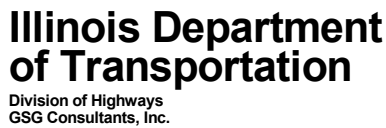
Surface Water Elev.	N/A	ft
Stream Bed Elev.	N/A	ft
Groundwater Elev.:		
First Encounter	None	ft
Upon Completion	N/A	ft
After N/A Hrs.	N/A	ft

D E P T H	B L O W S	U C S  Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

6 inches of Topsoil	611.28				Soft to Stiff Brown, Moist to Very Moist CLAY, trace sand and gravel (CH) (continued)				
Stiff to Hard		5					WOH		
Brown and Gray, Moist		4	4.5	12			1	0.4	25
SILTY CLAY, with sand (CL/ML)		5	P				9	B	
		2			Cobbles at 23.5-25 feet		3		
		2	1.3	22			12	0.5	15
	-5	6	B			-25	10	P	
		3				585.88	5		
		2	1.0	17	Medium Dense Brown, Moist SAND, with gravel (SPG)		6		11
		2	P				12		
Cobbles at 8.5-10 feet		9					28		
		17		13			16		8
	-10	5				-30	10		
Cobbles at 11-12.5 feet		2							
		3		19					
		2							
Cobbles at 13.5-15 feet		10					13		
		4		13			10		9
	-15	5				576.88	14		
					End of Boring	-35			
	595.88								
Soft to Stiff		2							
Brown, Moist to Very Moist		5	1.3	38					
CLAY, trace sand and gravel (CH)		5	B						
		6							
		4	0.8	33					
	-20	7	B			-40			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

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**Date** 6/9/21

[illegible]

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**Date** 6/9/21

[illegible]

BBS, form 137 (Rev. 8-99)

<b>ROUTE</b>	95th Street	<b>DESCRIPTION</b>	Retaining Wall Boring	<b>LOGGED BY</b>	EH
--------------	-------------	--------------------	-----------------------	------------------	----

**SECTION** IL 171 & 95th Street **LOCATION** IL 171, SEC. 22, TWP. 37N, RNG. 12E,

**Latitude** 41.7173026, **Longitude** -87.8966253  
**Diedrich D-50** **HAMMER TYPE**

COUNTY	COOK	DRILLING RIG	Diedrich D-50	HAMMER TYPE	AUTO
		DRILLING METHOD	HSA	HAMMER EFF (%)	92

**STRUCT. NO.** SN 016-2310  
**Station** Sta. 317+80.13 to 333+27.91

<b>BORING NO.</b>	RWB-18
<b>Station</b>	328+14.34
<b>Offset</b>	34.07ft RT
<b>Ground Surface Elev.</b>	611.02

D E P T H	B L O W S	U C S  Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

Surface Water Elev.	N/A	ft
Stream Bed Elev.	N/A	ft
Groundwater Elev.:		
First Encounter	None	ft
Upon Completion	N/A	ft
After N/A Hrs.	N/A	ft

D E P T H	B L O W S	U C S  Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

[illegible]

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

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# Illinois Department of Transportation

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GSG Consultants, Inc.

## SOIL BORING LOG

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Date 6/21/21

ROUTE 95th Street DESCRIPTION Retaining Wall Boring LOGGED BY EH

SECTION IL 171 & 95th Street LOCATION IL 171, SEC. 22, TWP. 37N, RNG. 12E,

Latitude 41.7173758, Longitude -87.8963887  
CME-75

COUNTY COOK DRILLING RIG CME-75 DRILLING METHOD HSA HAMMER TYPE AUTO HAMMER EFF (%) 91

STRUCT. NO. SN 016-2310  
Station Sta. 317+80.13 to 333+27.91

BORING NO. RWB-19  
Station 328+84.22  
Offset 35.55ft RT  
Ground Surface Elev. 610.64 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)	Surface Water Elev. <u>N/A</u> ft	Stream Bed Elev. <u>N/A</u> ft	Groundwater Elev.: First Encounter <u>None</u> ft Upon Completion <u>N/A</u> ft After <u>N/A</u> Hrs. <u>N/A</u> ft	D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
607.14	6		14					7		
	4							12		13
	5							20		
604.64	5							15		
	10		17					32		12
-5	16					585.64	-25	28		
604.64	20		7							
	50/2"									
	15									
	18		5							
-10	38						-30			
599.64	14									
	15		12							
	28									
	5									
	12		28							
-15	12						-35			
	50/5"									
	50/6"									
			22							
-20							-40			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, form 137 (Rev. 8-99)





# Illinois Department of Transportation

Division of Highways  
GSG Consultants, Inc.

## SOIL BORING LOG

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Date 6/9/21

ROUTE 95th Street DESCRIPTION Retaining Wall Boring LOGGED BY DM

SECTION IL 171 & 95th Street LOCATION IL 171, SEC. 22, TWP. 37N, RNG. 12E,

Latitude 41.717458, Longitude -87.8961337

COUNTY COOK DRILLING RIG CME-75 DRILLING METHOD HSA HAMMER TYPE AUTO HAMMER EFF (%) 91

STRUCT. NO. SN 016-2310  
Station Sta. 317+80.13 to 333+27.91

BORING NO. RWB-20  
Station 329+60.01  
Offset 35.99ft RT  
Ground Surface Elev. 610.33 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
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Surface Water Elev. N/A ft  
Stream Bed Elev. N/A ft  
Groundwater Elev.:  
First Encounter None ft  
Upon Completion N/A ft  
After N/A Hrs. N/A ft

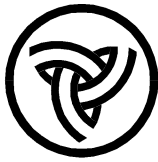
6 inches of Topsoil	609.83			
Loose				
Brown, Moist		4		
SAND, trace gravel (SP)		2		10
		4		
	606.83			
Loose		3		
Dark Brown, Moist		2		11
SILT, trace sand and gravel (ML)	605.33	2		
	-5			
Medium Dense				
Light Brown, Moist		7		
SAND, trace gravel (SP)		8		5
		12		
	601.83			
Dense to Very Dense		14		
Light Brown, Dry to Moist		35		3
SAND, with gravel (SPG)		36		
	-10			
		18		
		17		5
	597.83	25		
Dense to Very Dense				
Light Brown, Moist		13		
GRAVEL, with sand (GP)		18		5
	-15	40		
		19		
		18		6
		13		
		18		
		28		5
	590.33	35		
	-20			

End of Boring

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)

The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, form 137 (Rev. 8-99)



# Illinois Department of Transportation

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GSG Consultants, Inc.

## SOIL BORING LOG

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Date 6/9/21

ROUTE 95th Street DESCRIPTION Retaining Wall Boring LOGGED BY DM

SECTION IL 171 & 95th Street LOCATION IL 171, SEC. 22, TWP. 37N, RNG. 12E,

Latitude 41.7175384, Longitude -87.8958845

COUNTY COOK DRILLING RIG CME-75 HAMMER TYPE AUTO

DRILLING METHOD HSA

HAMMER EFF (%) 91

STRUCT. NO. SN 016-2310  
Station Sta. 317+80.13 to 333+27.91

BORING NO. RWB-21  
Station 330+34.08  
Offset 36.40ft RT  
Ground Surface Elev. 610.04 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
-------------------------------	--------------------------------	----------------------------	------------------------------

Surface Water Elev. N/A ft  
Stream Bed Elev. N/A ft  
Groundwater Elev.:  
First Encounter None ft  
Upon Completion N/A ft  
After N/A Hrs. N/A ft

6 inches of Topsoil	609.54			
Loose				
Light Brown, Moist		4		
SILTY SAND, trace gravel (SM)		3		12
		2		
	606.04	5		
Loose		3		17
Light Brown, Wet		4		
SAND, trace gravel (SP)	605.04	-5		
Medium Dense to Dense				
Light Brown, Moist		6		
SILT, with sand, trace gravel (ML)		10		17
		14		
		6		
		17		16
		21		
	-10			
	599.04			
Medium Dense		11		
Light Brown, Moist		14		9
SAND, trace gravel (SP)		15		
		9		
		14		9
		15		
	-15			
	594.04			
Medium Dense		10		
Brown and Gray, Very Moist		12		25
SILT, with sand, trace gravel (ML)		13		
		10		
		14		21
		13		
	590.04	-20		

End of Boring

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)

The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, form 137 (Rev. 8-99)

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**Date** 6/9/21

BBS, form 137 (Rev. 8-99)



# Illinois Department of Transportation

Division of Highways  
GSG Consultants, Inc.

## SOIL BORING LOG

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Date 6/9/21

ROUTE 95th Street DESCRIPTION Retaining Wall Boring LOGGED BY DM

SECTION IL 171 & 95th Street LOCATION IL 171, SEC. 22, TWP. 37N, RNG. 12E,

Latitude 41.7176995, Longitude -87.8953923

COUNTY COOK DRILLING RIG CME-75 DRILLING METHOD HSA HAMMER TYPE AUTO HAMMER EFF (%) 91

STRUCT. NO. SN 016-2310  
Station Sta. 317+80.13 to 333+27.91

BORING NO. RWB-23  
Station 331+80.73  
Offset 36.47ft RT  
Ground Surface Elev. 609.57 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
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Surface Water Elev. N/A ft  
Stream Bed Elev. N/A ft  
Groundwater Elev.:  
First Encounter None ft  
Upon Completion N/A ft  
After N/A Hrs. N/A ft

18 inches of Topsoil				
608.07	3			
Very Stiff to Hard	2	3.0	14	
Light Brown, Moist	5	B		
SILTY CLAY, trace sand and gravel (CL/ML)				
Cobbles at 3.5-5 feet	50/4"			
		3.3	11	
	-5	B		
	11			
	13	5.0	12	
	20	B		
601.57				
Dense				
Light Brown, Moist	14			
GRAVEL, with sand, trace clay (GP)	22		11	
599.57	17			
-10				
Hard				
Brown and Gray, Moist	9			
SILTY CLAY, trace sand and gravel (CL/ML)	16	4.5	11	
	17	B		
596.57				
Medium Dense to Dense				
Gray, Moist	10			
SILT, trace sand and gravel (ML)	14		14	
	14			
-15				
	6			
	6		17	
	10			
	12			
	19		13	
	20			
589.57	-20			

End of Boring

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)

The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, form 137 (Rev. 8-99)



# Illinois Department of Transportation

Division of Highways  
GSG Consultants, Inc.

## SOIL BORING LOG

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Date 6/9/21

ROUTE 95th Street DESCRIPTION Retaining Wall Boring LOGGED BY DM

SECTION IL 171 & 95th Street LOCATION IL 171, SEC. 22, TWP. 37N, RNG. 12E,

Latitude 41.7177787, Longitude -87.895151

COUNTY COOK DRILLING RIG CME-75 DRILLING METHOD HSA HAMMER TYPE AUTO HAMMER EFF (%) 91

STRUCT. NO. SN 016-2310  
Station Sta. 317+80.13 to 333+27.91

BORING NO. RWB-24  
Station 332+52.64  
Offset 36.43ft RT  
Ground Surface Elev. 609.22 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
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Surface Water Elev. N/A ft  
Stream Bed Elev. N/A ft  
Groundwater Elev.:  
First Encounter None ft  
Upon Completion N/A ft  
After N/A Hrs. N/A ft

18 inches of Topsoil				
	607.72	3		
Medium Dense		4		14
Light Brown, Moist		10		
GRAVEL, with sand (GP)				
		5		
		12		7
	-5	15		
		12		
		8		8
		6		
		6		
		4		6
	-10	7		
		9		
		9		8
		7		
		20		
		12		5
	-15	9		
	593.22			
Extremely Dense		10		
Light Brown, Moist		50/3"		8
GRAVEL, with sand (GP)				
Cobbles at 16-17 feet				
	590.72			
		50/6"		5
Auger refusal at 19 feet				
End of Boring				
	-20			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

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# Illinois Department of Transportation

Division of Highways  
GSG Consultants, Inc.

## SOIL BORING LOG

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Date 6/9/21

ROUTE 95th Street DESCRIPTION Retaining Wall Boring LOGGED BY DM

SECTION IL 171 & 95th Street LOCATION IL 171, SEC. 22, TWP. 37N, RNG. 12E,

Latitude 41.7178604, Longitude -87.894902

COUNTY COOK DRILLING RIG CME-75 DRILLING METHOD HSA HAMMER TYPE AUTO HAMMER EFF (%) 91

STRUCT. NO. SN 016-2310  
Station Sta. 317+80.13 to 333+27.91

BORING NO. RWB-25  
Station 333+26.85  
Offset 36.39ft RT  
Ground Surface Elev. 608.92 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
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Surface Water Elev. N/A ft  
Stream Bed Elev. N/A ft  
Groundwater Elev.:  
First Encounter None ft  
Upon Completion N/A ft  
After N/A Hrs. N/A ft

18 inches of Topsoil				
	607.42	5		
Loose		7		8
Light Brown, Moist		3		
SAND, trace gravel (SP)				
		5		
	604.42	5	0.8	10
Medium Stiff	603.92	2	P	
Brown, Moist				
SILTY CLAY, trace gravel				
(CL/ML)		8		
Medium Dense to Dense		8		7
Brown, Moist		8		
SAND, with gravel and silt (SP)				
		5		
		18		7
	-10	20		
		9		
		7		12
		5		
		8		
		7		9
	-15	8		
		6		
		6		7
		5		
		3		
		7		13
	588.92	12		
	-20			

End of Boring

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)

The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

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<b>ROUTE</b>	95th Street	<b>DESCRIPTION</b>	Retaining Wall Boring	<b>LOGGED BY</b>	EH
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**SECTION** IL 171 & 95th Street **LOCATION** IL 171, SEC. 22, TWP. 37N, RNG. 12E,

**Latitude** 41.7179265, **Longitude** -87.894678  
Diedrich D-50 **HAMMER TYP**

COUNTY	COOK	DRILLING RIG	Diedrich D-50	HAMMER TYPE	AUTO
		DRILLING METHOD	HSA	HAMMER EFF (%)	92

**STRUCT. NO.** SN 016-2310  
**Station** Sta. 317+80.13 to 333+27.91

<b>BORING NO.</b>	RWB-26
<b>Station</b>	333+92.54
<b>Offset</b>	38.85ft RT
<b>Ground Surface Elev.</b>	608.78

DEPTH	BLOW COUNTS	U C S  Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

Surface Water Elev.	N/A	ft
Stream Bed Elev.	N/A	ft
Groundwater Elev.:		
First Encounter	None	ft
Upon Completion	N/A	ft
After N/A Hrs.	N/A	ft

D E P T H	B L O W S	U C S  Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

6 inches of Asphalt	608.28				gravel (CL/ML)				
6 inches of Concrete	607.78				End of Boring				
Stiff		10							
Brown, Moist		5		NR					
SILTY CLAY, trace sand and gravel (CL/ML)		4							
		4							
		4	2.0	19					
	-5	4	P				-25		
Cobbles at 6-7.5 feet		8							
		10		19					
		7							
Cobbles at 8.5-10 feet		3							
		3		20					
	-10	5					-30		
	597.78								
Soft to Stiff		3							
Brown, Very Moist		5	0.8	43					
CLAY, trace sand and gravel (CH)		4	B						
		8							
		7	1.7	32					
	-15	6	B				-35		
Cobbles at 16-17.5 feet		3							
		3	0.3	39					
		4	P						
	590.28								
Stiff		4							
Brown, Moist		12	1.5	15					
SILTY CLAY, trace sand and		17	P						
	588.78	-20					-40		

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, form 137 (Rev. 8-99)



# Illinois Department of Transportation

Division of Highways  
GSG Consultants, Inc.

## SOIL BORING LOG

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Date 6/10/21

ROUTE 95th Street DESCRIPTION Retaining Wall Boring LOGGED BY EH

SECTION IL 171 & 95th Street LOCATION IL 171, SEC. 22, TWP. 37N, RNG. 12E,

Latitude 41.718025, Longitude -87.8943884

COUNTY COOK DRILLING RIG Diedrich D-50 HAMMER TYPE AUTO

DRILLING METHOD

HSA

HAMMER EFF (%)

92

STRUCT. NO. SN 016-2310  
Station Sta. 317+80.13 to 333+27.91

BORING NO. RWB-27  
Station 334+79.35  
Offset 37.63ft RT  
Ground Surface Elev. 608.86 ft

D E P T H (ft)	B L O W S (/6")	U C S  Qu (tsf)	M O I S T (%)
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Surface Water Elev. N/A ft  
Stream Bed Elev. N/A ft  
Groundwater Elev.:  
First Encounter None ft  
Upon Completion N/A ft  
After N/A Hrs. N/A ft

4 inches of Topsoil	608.53			
Stiff				
Brown, Moist		2		
SILTY CLAY, with sand (CL/ML)		3	2.0	11
		8	P	
	605.36			
Very Stiff		5		
Brown, Moist to Very Moist		2	2.1	26
SILTY CLAY, trace sand and		4	B	
gravel (CL/ML)		-5		
		19		
		14	2.5	16
		8	P	
		8		
Cobbles at 8.5-10 feet		20	2.0	16
		21	P	
	-10			
		17		
		12	2.5	19
		6	B	
	595.36			
Very Stiff		14		
Brown, Moist		10	2.5	21
SILTY CLAY LOAM, trace sand		11	P	
and gravel (ML/CL)		-15		
		10		
		20	2.0	17
		10	P	
		14		
		12	2.5	8
		20	P	
	588.86	-20		

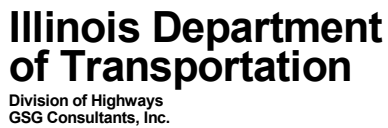
End of Boring

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)

The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

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**Date** 6/17/21

Surface Water Elev.	N/A	ft
Stream Bed Elev.	N/A	ft
Groundwater Elev.:		
First Encounter	None	ft
Upon Completion	N/A	ft
After N/A Hrs.	N/A	ft

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**Date** 6/17/21

Surface Water Elev.	N/A	ft
Stream Bed Elev.	N/A	ft
Groundwater Elev.:		
First Encounter	None	ft
Upon Completion	N/A	ft
After N/A Hrs.	N/A	ft

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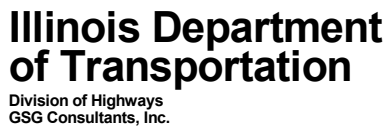
Page 1 of 1

**Date** 6/17/21

Surface Water Elev.	N/A	ft
Stream Bed Elev.	N/A	ft
Groundwater Elev.:		
First Encounter	None	ft
Upon Completion	N/A	ft
After N/A Hrs.	N/A	ft

[illegible]

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**Date** 6/18/21

Surface Water Elev.	N/A	ft
Stream Bed Elev.	N/A	ft
Groundwater Elev.:		
First Encounter	None	ft
Upon Completion	N/A	ft
After N/A Hrs.	N/A	ft

11 inches of Asphalt				
	611.21			
Very Stiff		6		
Brown and Gray, Moist to Very Moist		5	2.0	16
SILTY CLAY, trace sand and gravel (CL/ML)		3	P	
		3		
		3	3.0	27
	-5	5	P	
		4		
		4	2.5	28
		6	B	
	603.62			
Hard		7		
Brown and Gray, Moist		11	4.5	15
SILTY CLAY LOAM, trace sand and gravel (ML/CL)	-10	17	P	
		9		
		23	4.5	10
		19	P	
		10		
		17	4.5	11
	597.12	18	P	
End of Boring	-15			
	-20			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, form 137 (Rev. 8-99)

<b>ROUTE</b>	95th Street	<b>DESCRIPTION</b>	Embankment Stability Boring	<b>LOGGED BY</b>	EH
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**SECTION** IL 171 & 95th Street **LOCATION** IL 171, SEC. 22, TWP. 37N, RNG. 12E,

**Latitude** 41.7164556, **Longitude** -87.8990917  
Diedrich D-50 **HAMMER TYPE**

COUNTY	COOK	DRILLING RIG	Diedrich D-50	HAMMER TYPE	AUTO
		DRILLING METHOD	HSA	HAMMER EFF (%)	92

STRUCT. NO.	N/A
Station	N/A

D E P T H	B L O W S	U C S  Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

Surface Water Elev.	N/A	ft
Stream Bed Elev.	N/A	ft

<b>BORING NO.</b>	SSB-02
<b>Station</b>	320+79.71
<b>Offset</b>	72.03ft RT
<b>Ground Surface Elev.</b>	613.00

<b>Groundwater Elev.:</b>			
<b>First Encounter</b>		<u>None</u>	<b>ft</b>
<b>Upon Completion</b>		<u>N/A</u>	<b>ft</b>
<b>After</b>	<b>N/A Hrs.</b>	<u>N/A</u>	<b>ft</b>

[illegible]

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

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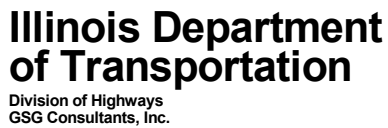
Page 1 of 1

**Date** 6/21/21

Surface Water Elev.	N/A	ft
Stream Bed Elev.	N/A	ft
Groundwater Elev.:		
First Encounter	None	ft
Upon Completion	N/A	ft
After N/A Hrs.	N/A	ft

[illegible]

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**Date** 6/21/21

Surface Water Elev.	N/A	ft
Stream Bed Elev.	N/A	ft
Groundwater Elev.:		
First Encounter	None	ft
Upon Completion	N/A	ft
After N/A Hrs.	N/A	ft

BBS, form 137 (Rev. 8-99)

<b>ROUTE</b>	95th Street	<b>DESCRIPTION</b>	Embankment Stability Boring	<b>LOGGED BY</b>	JB
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**SECTION** IL 171 & 95th Street **LOCATION** IL 171, SEC. 22, TWP. 37N, RNG. 12E,

**Latitude** 41.7170413, **Longitude** -87.8970454  
Diedrich D-50 **HAMMER TYPE**

COUNTY	COOK	DRILLING RIG	Diedrich D-50	HAMMER TYPE	AUTO
		DRILLING METHOD	HSA	HAMMER EFF (%)	92

STRUCT. NO.	N/A
Station	N/A

D E P T H	B L O W S	U C S  Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

<b>Surface Water Elev.</b>	<u>          N/A          </u>	<b>ft</b>
<b>Stream Bed Elev.</b>	<u>          N/A          </u>	<b>ft</b>

<b>BORING NO.</b>	SSB-05
<b>Station</b>	326+71.10
<b>Offset</b>	75.35ft RT
<b>Ground Surface Elev.</b>	612.08

<b>Groundwater Elev.:</b>			
<b>First Encounter</b>		<u>None</u>	<b>ft</b>
<b>Upon Completion</b>		<u>N/A</u>	<b>ft</b>
<b>After</b>	<b>N/A Hrs.</b>	<u>N/A</u>	<b>ft</b>

[illegible]

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

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# Illinois Department of Transportation

Division of Highways  
GSG Consultants, Inc.

## SOIL BORING LOG

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Date 6/18/21

ROUTE 95th Street DESCRIPTION Embankment Stability Boring LOGGED BY EH

SECTION IL 171 & 95th Street LOCATION IL 171, SEC. 22, TWP. 37N, RNG. 12E,

Latitude 41.717286, Longitude -87.8963749

COUNTY COOK DRILLING RIG Diedrich D-50 HAMMER TYPE AUTO  
DRILLING METHOD HSA HAMMER EFF (%) 92

STRUCT. NO. N/A  
Station N/A

BORING NO. SSB-06  
Station 328+74.56  
Offset 67.03ft RT  
Ground Surface Elev. 610.66 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
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Surface Water Elev. N/A ft  
Stream Bed Elev. N/A ft  
Groundwater Elev.:  
First Encounter None ft  
Upon Completion N/A ft  
After N/A Hrs. N/A ft

9 inches of Asphalt	609.91			
Medium Dense Brown and Gray, Moist GRAVEL, with sand and clay (GP)	7 10 8		11	
	8 14 15		10	
	-5			
	604.66			
Dense to Extremely Dense Brown and Gray, Dry SAND, with gravel and cobbles (SPG)	25 19 20		3	
	41 50/2"		4	
	-10			
	25 22 50/4"		5	
Split-spoon refusal at 13 feet	597.66			
End of Boring	50/1"			
	-15			
	-20			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, form 137 (Rev. 8-99)

<b>ROUTE</b>	95th Street	<b>DESCRIPTION</b>	Embankment Stability Boring	<b>LOGGED BY</b>	EH
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**SECTION** IL 171 & 95th Street **LOCATION** IL 171, SEC. 22, TWP. 37N, RNG. 12E,

COUNTY	COOK	DRILLING RIG	Latitude 41.7175024, Longitude -87.8957054
		DRILLING METHOD	Diedrich D-50
			HSA
			HAMMER TYPE
			AUTO
			HAMMER EFF (%)
			92

STRUCT. NO.	N/A
Station	N/A

<b>BORING NO.</b>	SSB-07
<b>Station</b>	330+73.63
<b>Offset</b>	68.02ft RT
<b>Ground Surface Elev.</b>	610.13

D E P T H	B L O W S	U C S  Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

Surface Water Elev.	N/A	ft
Stream Bed Elev.	N/A	ft
Groundwater Elev.:		
First Encounter	None	ft
Upon Completion	N/A	ft
After N/A Hrs.	N/A	ft

[illegible]

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

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**Date** 6/17/21

[illegible]

BBS, form 137 (Rev. 8-99)

<b>ROUTE</b>	95th Street	<b>DESCRIPTION</b>	Traffic Sign Boring	<b>LOGGED BY</b>	JB
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**SECTION** IL 171 & 95th Street **LOCATION** IL 171, SEC. 22, TWP. 37N, RNG. 12E,

**Latitude** 41.716844, **Longitude** -87.8974561  
Diedrich D-50 **HAMMER TYPE**

COUNTY	COOK	DRILLING RIG	Diedrich D-50	HAMMER TYPE	AUTO
		DRILLING METHOD	HSA	HAMMER EFF (%)	92

STRUCT. NO.	N/A
Station	N/A

<b>BORING NO.</b>	TSB-02
<b>Station</b>	325+40.62
<b>Offset</b>	96.64ft RT
<b>Ground Surface Elev.</b>	618.16

D E P T H	B L O W S	U C S  Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

Surface Water Elev.	N/A	ft
Stream Bed Elev.	N/A	ft
Groundwater Elev.:		
First Encounter	None	ft
Upon Completion	N/A	ft
After N/A Hrs.	N/A	ft

D E P T H	B L O W S	U C S  Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

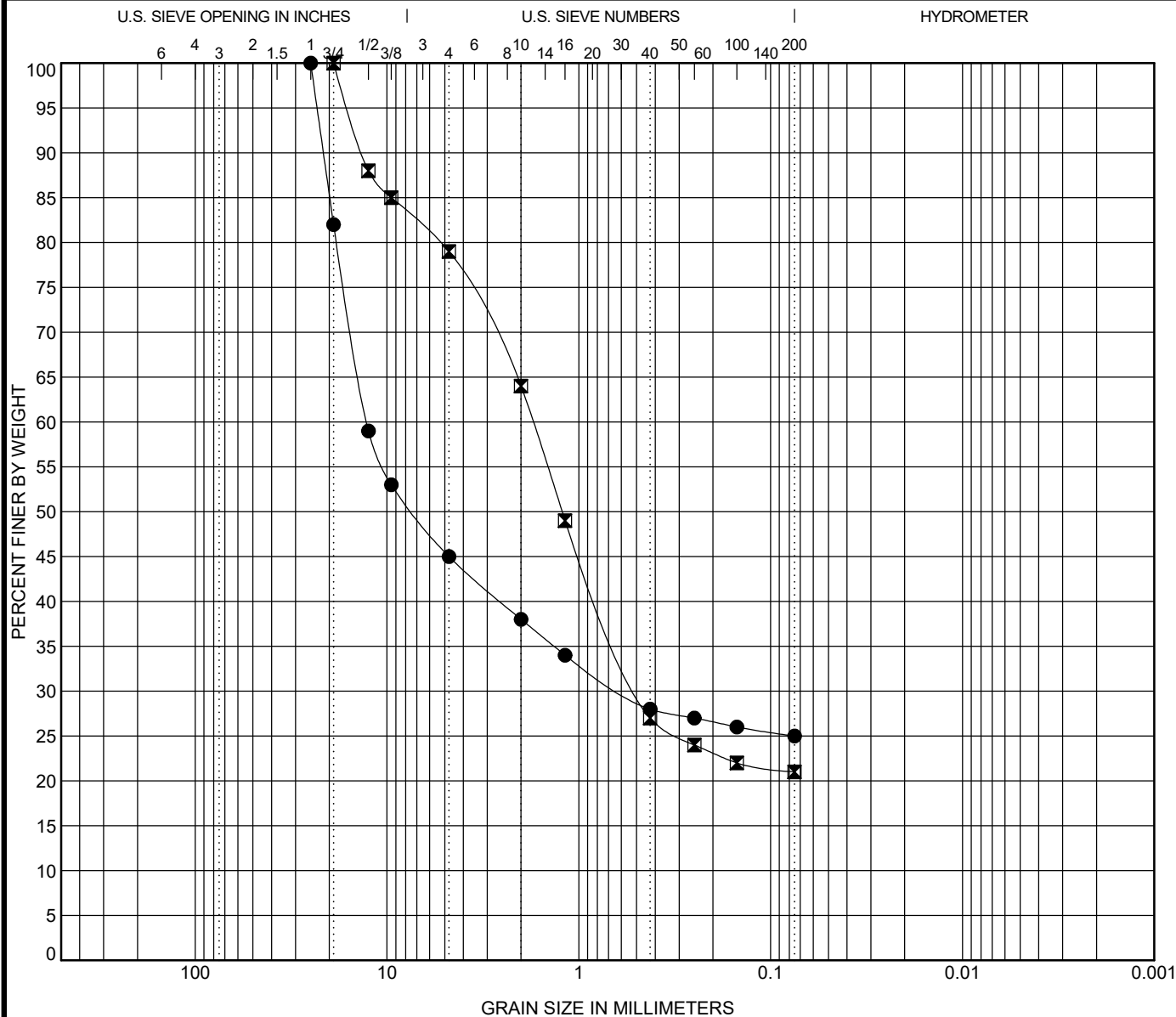
3 inches of Topsoil	617.91				Stiff to Very Stiff				
Medium Stiff to Stiff					Brown and Gray, Moist				
Brown, Moist		6			SILTY CLAY, with sand and		8		
SILTY CLAY, trace gravel		6	2.0	15	gravel (CL/ML) (continued)		9	2.5	12
(CL/ML)		8	P				9	B	
						594.66			
		6			Very Stiff		6		
		8	2.0	18	Gray, Moist		9	2.5	11
	-5	9	P		SILTY CLAY, with sand and	593.16	11	B	
					gravel (CL/ML)	-25			
					End of Boring				
		6							
Wood and root fragments at 6.5		10	2.0	22					
feet		8	P						
		4							
Wood and root fragments at 9 feet		4	0.8	21					
	-10	6	B			-30			
	607.16	2							
Medium Stiff		3	0.8	17					
Brown and Gray, Moist		4	B						
SILTY CLAY, with sand, trace									
gravel (CL/ML)									
	604.66	2							
Stiff		3	1.5	18					
Gray, Moist		4	B			-35			
SILTY CLAY, trace gravel (CL)	-15								
	602.16	5							
Stiff to Very Stiff		5	1.5	14					
Brown and Gray, Moist		7	B						
SILTY CLAY, with sand and									
gravel (CL/ML)									
		5							
		9	3.5	13					
	-20	9	B			-40			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)  
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, form 137 (Rev. 8-99)

**APPENDIX D**  
**LABORATORY TEST RESULTS**





COBBLES	GRAVEL		SAND			SILT OR CLAY
	coarse	fine	coarse	medium	fine	

Specimen Identification			Classification				LL	PL	PI	Cc	Cu
●	RWB-18	18.50									
☒	RWB-25	11.00									

Specimen Identification			D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay
●	RWB-18	18.50	25	12.73	0.597		55.0	20.0	25.0	
☒	RWB-25	11.00	19	1.737	0.489		21.0	58.0	21.0	

GSG Consultants, Inc  
735 Remington Road  
Schaumburg, IL 60173  
(630) 994-2600  
Fax: (312) 733-5612

## GRAIN SIZE DISTRIBUTION

Route: IL 171

Section: IL 171 & 95th Street

County: COOK



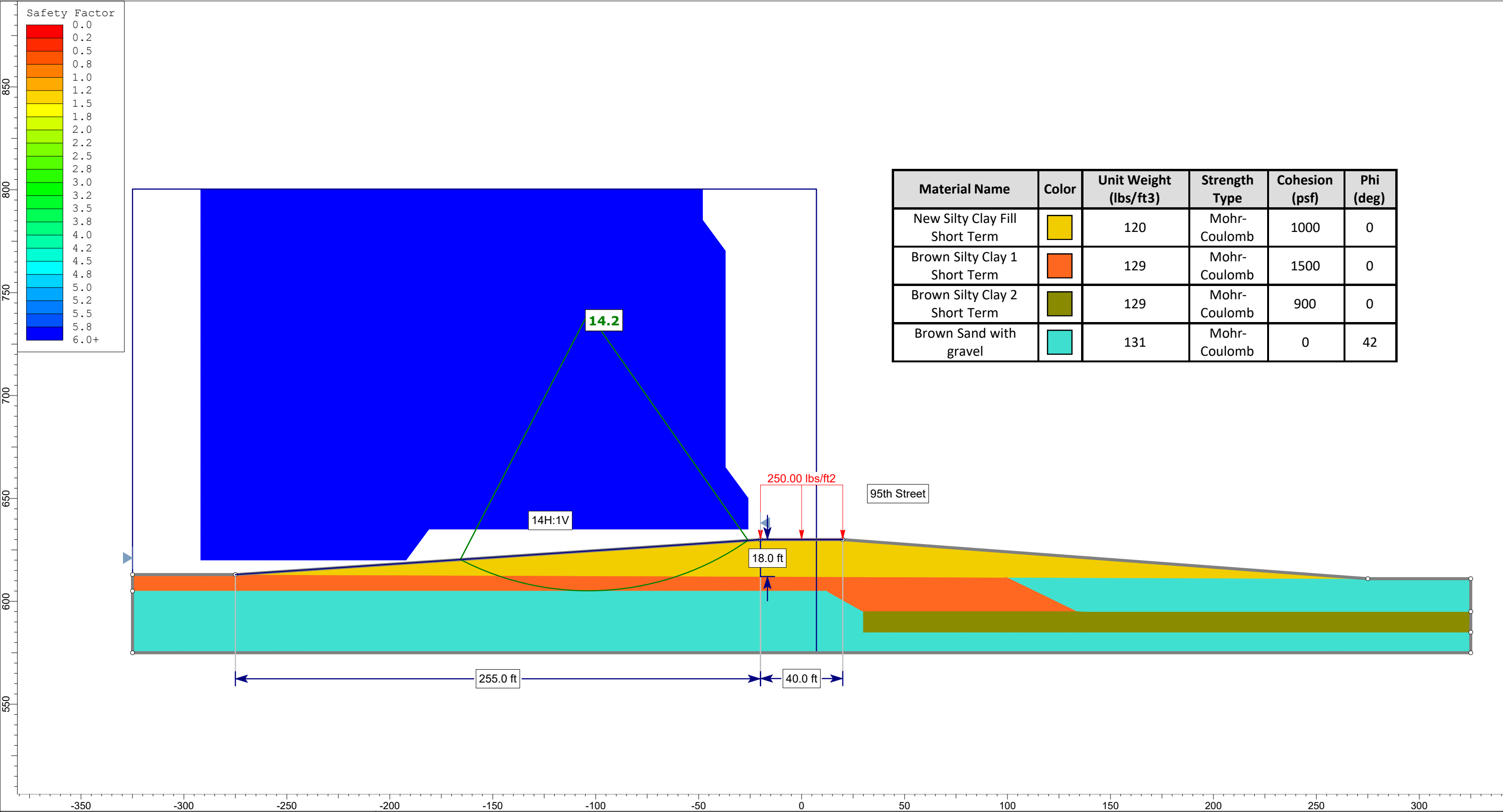
735 Remington Road  
Schaumburg, IL 60173  
Tel: 630.994.2600  
www.gsg-consultants.com

**Table D1 – PTB 163-17 Test Results – Dry Unit Weight**

Boring ID	Sample Depth (ft)	Dry Unit Weight (pcf)	Wet Unit Weight (pcf)	Soil Classification
SGB-02	3.5-5	132.6	148.1	CL/ML
SGB-03	6-7.5	130.5	145.9	CL/ML
RWB-04	6-7.5	120.3	140.7	CL/ML
RWB-09	3.5-5	112.3	136.9	CL/ML
RWB-14	11-12.5	93.3	124.1	CL
RWB-15	16-17.5	81.2	110.0	CH



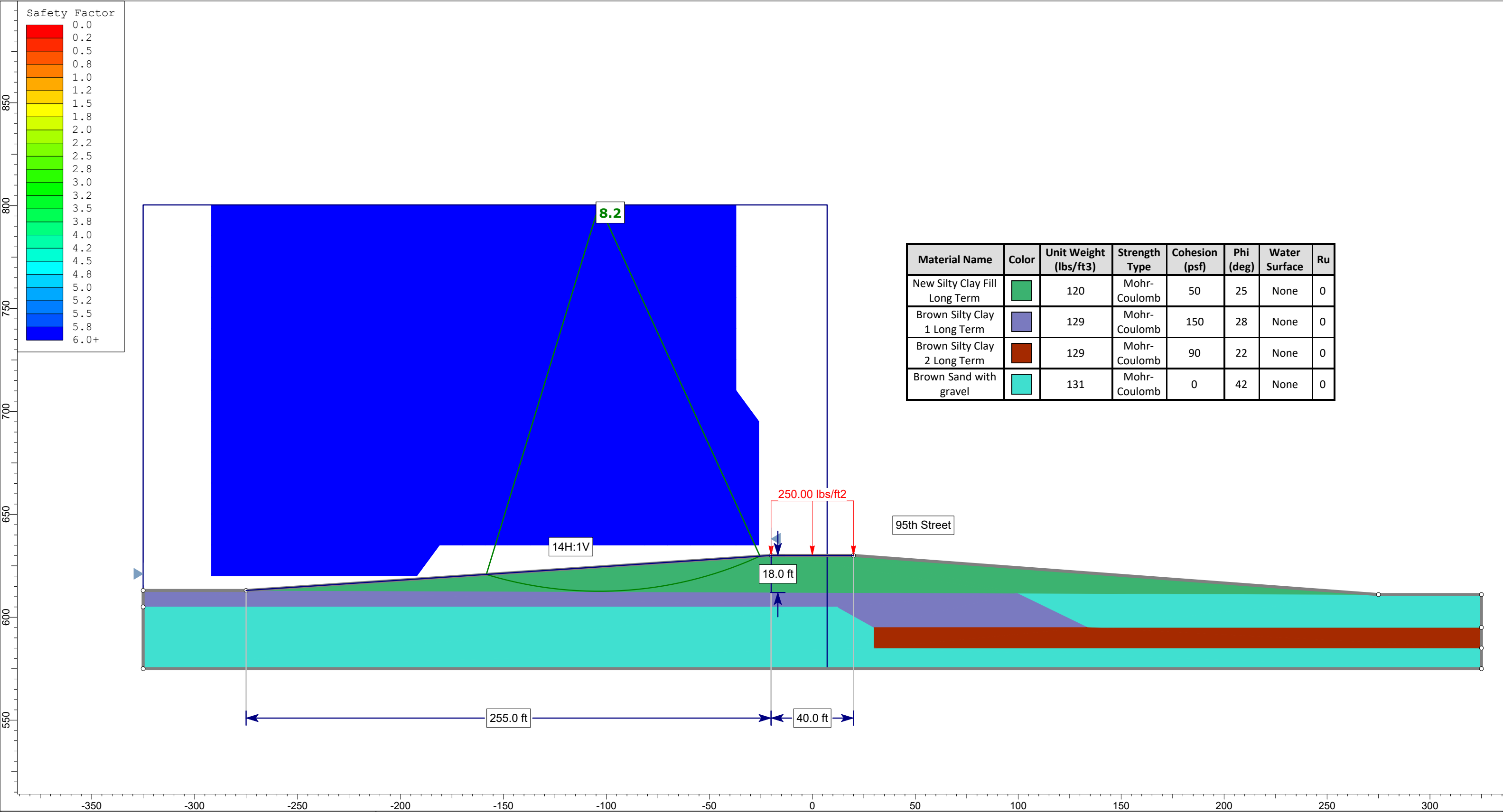
**APPENDIX E**  
**SLOPE STABILITY ANALYSES EXHIBITS**

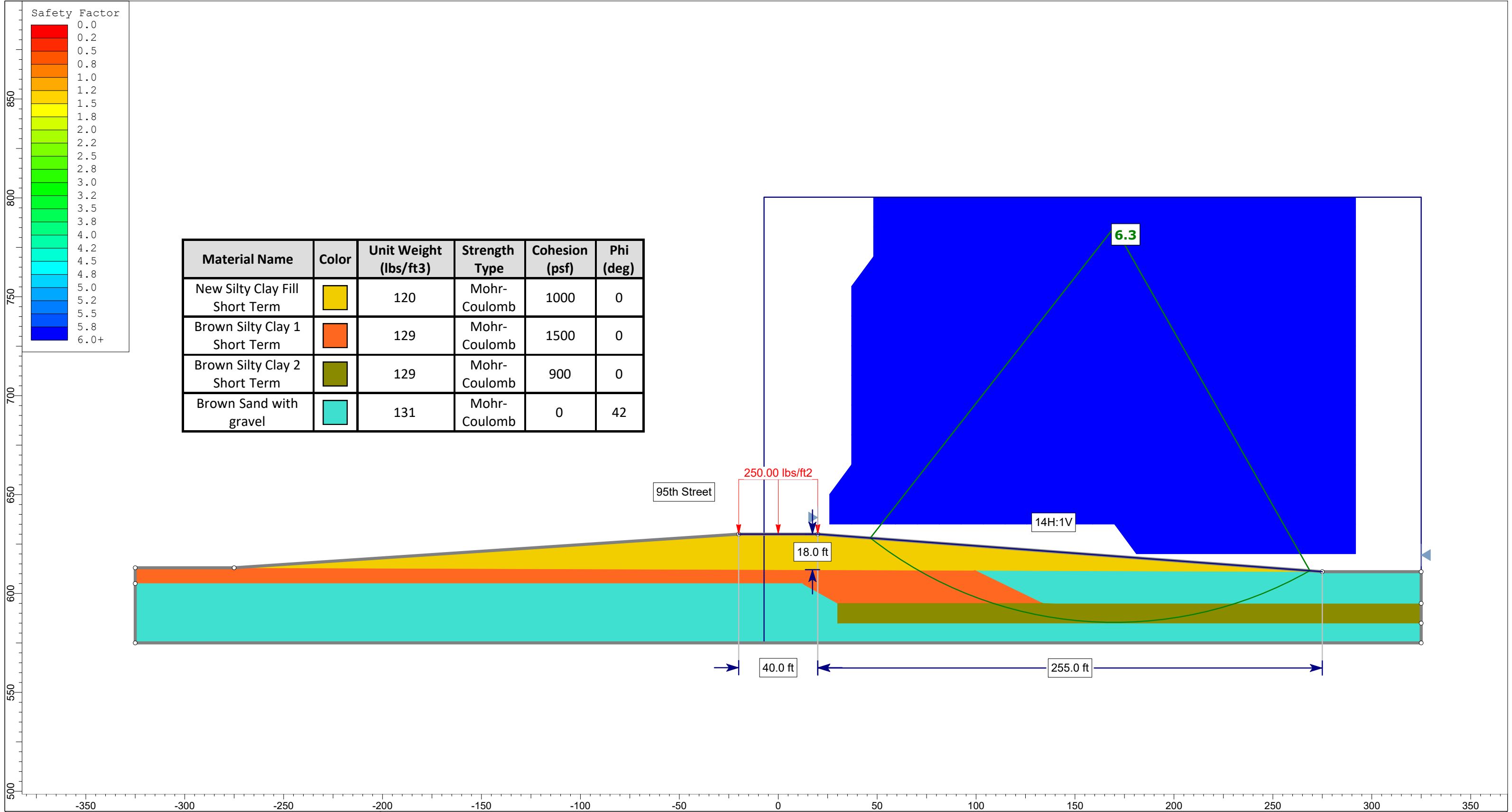


Material Name	Color	Unit Weight (lbs/ft3)	Strength Type	Cohesion (psf)	Phi (deg)
New Silty Clay Fill Short Term	<div></div>	120	Mohr-Coulomb	1000	0
Brown Silty Clay 1 Short Term	<div></div>	129	Mohr-Coulomb	1500	0
Brown Silty Clay 2 Short Term	<div></div>	129	Mohr-Coulomb	900	0
Brown Sand with gravel	<div></div>	131	Mohr-Coulomb	0	42

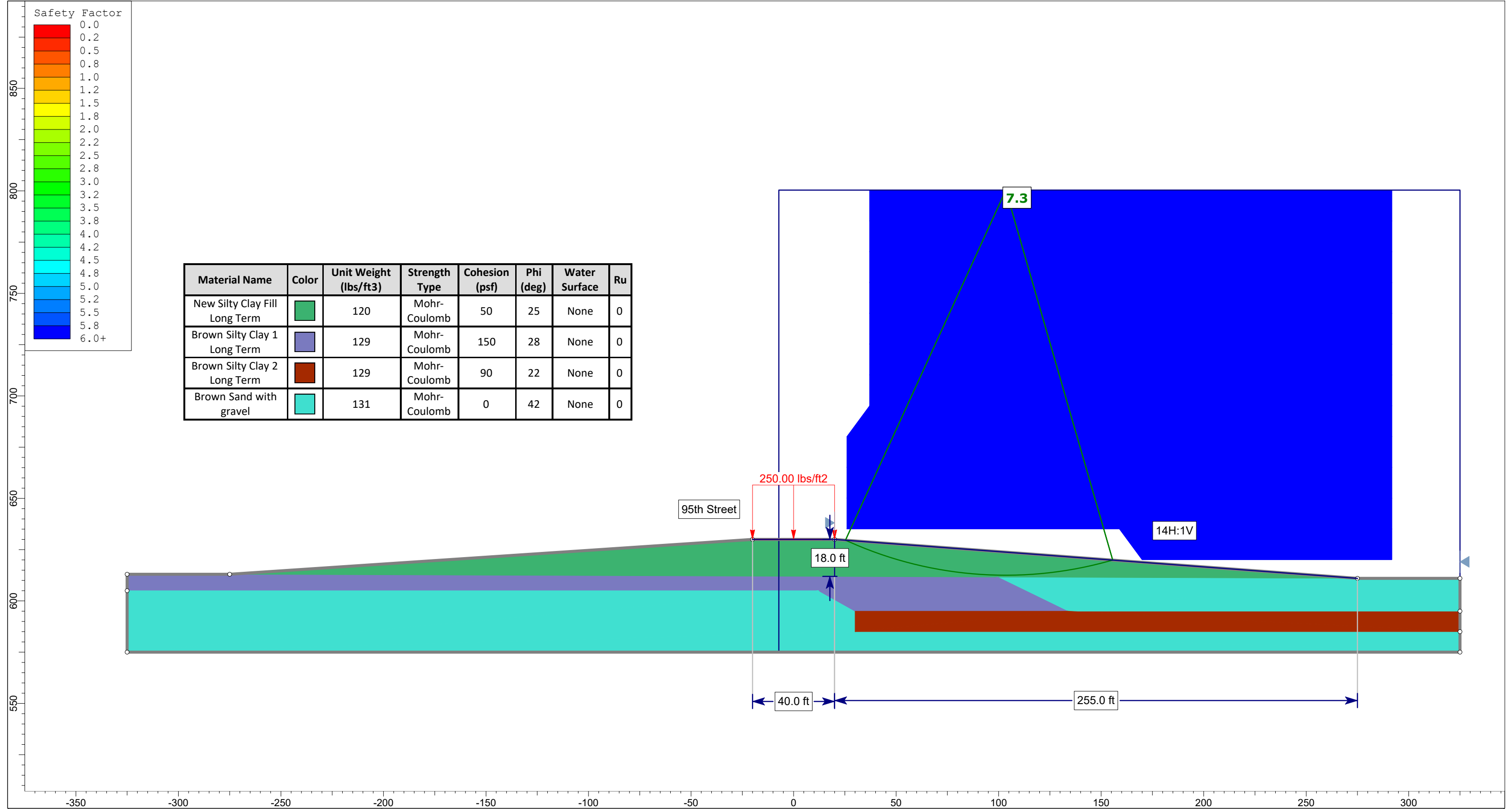


Project	IDOT PTB 163-017: 95th Street Embankment at IL 171		
Analysis Description	Exhibit 1 - Left Side of Embankment at Station 199+50 - Slope Circular Failure Short Term		
Drawn By	TEK	Company	GSG Consultants, Inc.
Date	10/27/2021 4:04:05 PM	File Name	95th street at 199+50.slmd





Project		IDOT PTB 163-017: 95th Street Embankment at IL 171	
Analysis Description		Exhibit 3 - Right Side of Embankment at Station 199+50 - Slope Circular Failure Short Term	
Drawn By		TEK	Company GSG Consultants, Inc.
Date		10/27/2021 4:19:17 PM	File Name 95th street at 199+50 - Copy.slmd



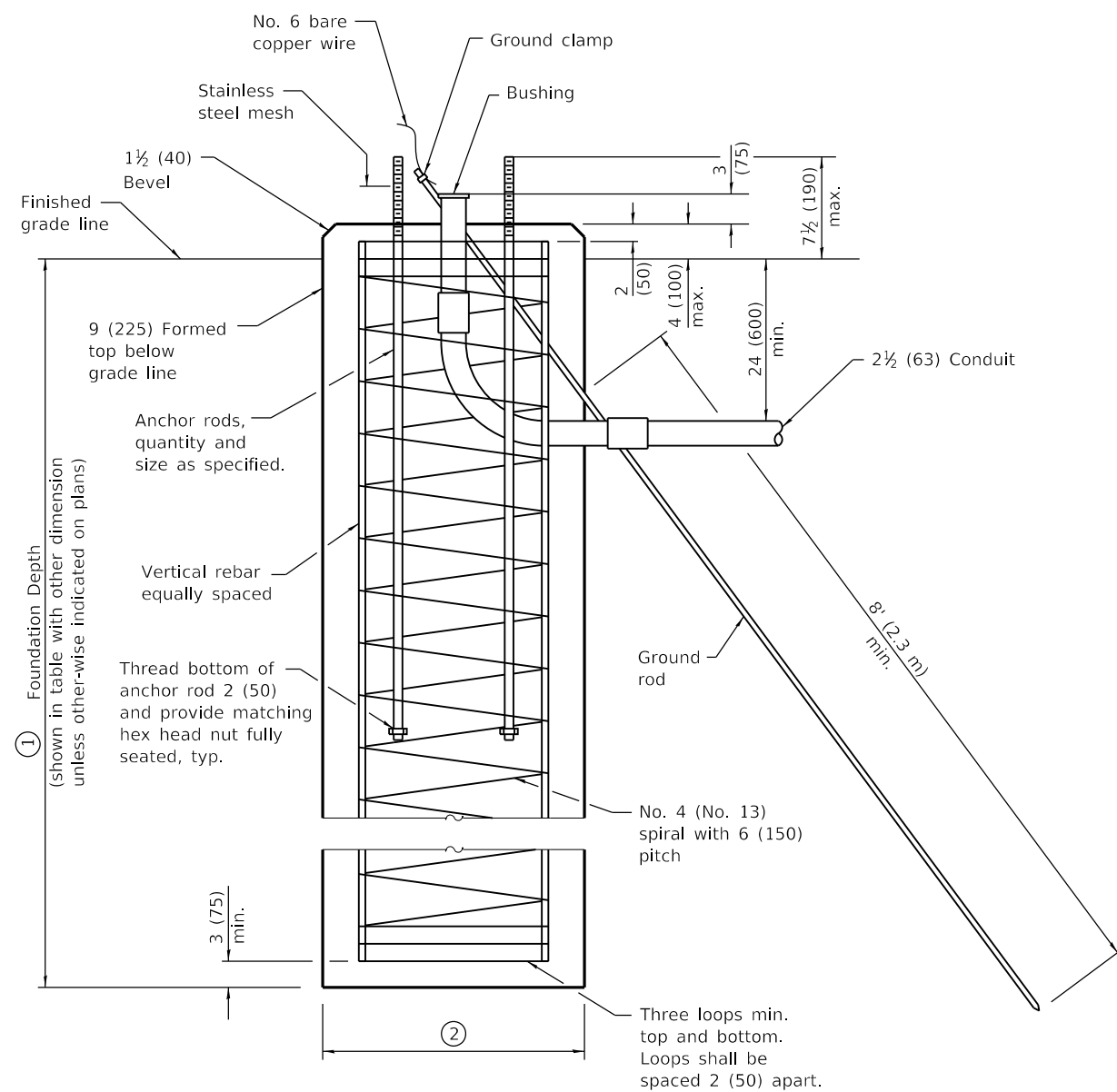
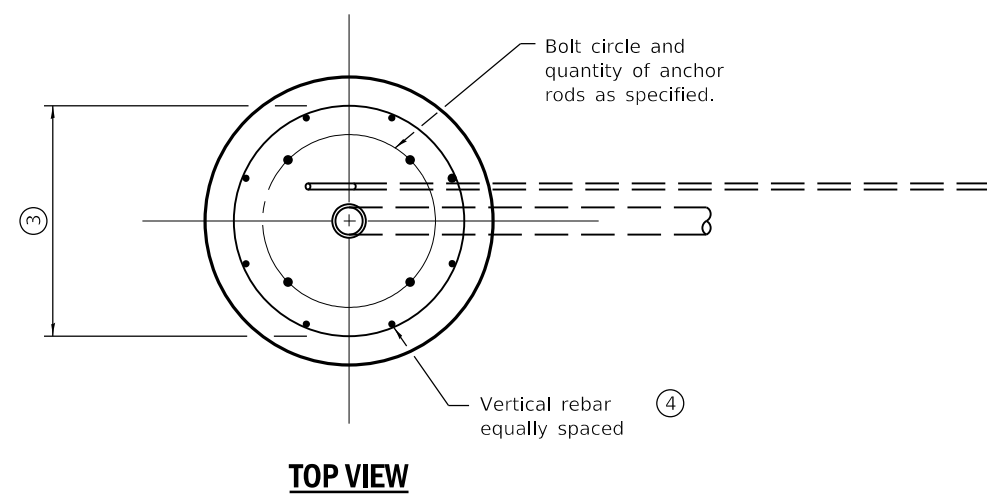
Material Name	Color	Unit Weight (lbs/ft3)	Strength Type	Cohesion (psf)	Phi (deg)	Water Surface	Ru
New Silty Clay Fill Long Term	<div></div>	120	Mohr-Coulomb	50	25	None	0
Brown Silty Clay 1 Long Term	<div></div>	129	Mohr-Coulomb	150	28	None	0
Brown Silty Clay 2 Long Term	<div></div>	129	Mohr-Coulomb	90	22	None	0
Brown Sand with gravel	<div></div>	131	Mohr-Coulomb	0	42	None	0



Project	IDOT PTB 163-017: 95th Street Embankment at IL 171		
Analysis Description	Exhibit 4 - Right Side of Embankment at Station 199+50 - Slope Circular Failure Long Term		
Drawn By	TEK	Company	GSG Consultants, Inc.
Date	10/27/2021 4:20:20 PM	File Name	95th street at 199+50 - Copy.slmd

**APPENDIX F**  
**IDOT HIGHWAY STANDARD 878001-11**





\* For standard and combination mast arm assemblies. Foundation depths for standard dual mast arms with the longest arm length upto and including 55' (16.8 m) shall be increased by 1' (0.3 m) of that shown in the table, based on the longer of the two arms.

These foundation depths are for sites which have cohesive soils (clayey silt, sandy clay, etc.) along the length of the shaft, with an average Unconfined Compressive Strength (Qu) > 1.0 tsf (100 kpa). This strength shall be verified by boring data prior to construction or with testing by the Engineer during foundation drilling. The Bureau of Bridges & Structures should be contacted for a revised design if other conditions are encountered.