DESCRIPTION OF PROJECT:

SECTION 82-14VB INCLUDES THE FURNISHING AND PARRICATING OF STRUCTURAL STEEL AND THE COMPLETE CONSTRUCTION OF THE FOLLOW-

	TWO-4 SPAN CONTINUOUS UNITS SPANS: 94'-120'-120'-94'	MALIND PLATE GROEES WITH POLLED FLOORBEANS AND STRUCKERS ON R. C. PERS  THE PROPERTY OF THE PR				
ROADWAYS BAND C	EIGHT - 1 SEAN CONTINUOUS UNITS SEASS: 2 8 17 - 100 - 17  1 EACH: 2 - 100 - 17  90 - 110 - 10  90 - 110 - 10  90 - 110 - 10  90 - 110 - 10  90 - 110 - 10  90 - 110 - 10  90 - 110 - 10  90 - 110 - 10  90 - 110 - 10  90 - 110 - 10  90 - 110 - 10  90 - 110 - 10  90 - 110 - 10  90 - 110 - 10  90 - 110 - 10  90 - 110 - 10  90 - 110 - 110 - 10  90 - 110 - 110 - 10  90 - 110 - 110 - 10  90 - 110 - 110 - 10  90 - 110 - 110 - 10  90 - 110 - 110 - 10  90 - 110 - 110 - 10  90 - 110 - 110 - 10  90 - 110 - 110 - 10  90 - 110 - 110 - 10  90 - 110 - 110 - 10  90 - 110 - 110 - 10  90 - 110 - 10  90 - 110 - 10  90 -					
	TWO SIMPLE SPANS 6-77"	COMPOSITE WF ON R.C. PIERS				
	ONE SIMPLE SPAN - 110°	COMPOSITE I LATE GIRDER ON				
ROADWAYS	ONE SIMPLE SPAN - VARIES FROM 118-10 1/8 TO 93-3 1/2	R.C. PIERS				
ROADWAY A	ONE-4 SEAN CONTINUOUS UNIT SPANS: 120 -155'-155'-120'	CURVED WELDED PLATE GIRDERS WITH ROLLED FLOORBEAMS AND STRINGERS ON R.C. PIERS				
RAMP M	ONE-+ SHAN CONTINUOUS UNIT SPANS: +6'-122'-+6'					

## STATE OF ILLINOIS DEPARTMENT OF PUBLIC WORKS AND BUILDINGS DIVISION OF HIGHWAYS PLANS FOR PROPOSED FEDERAL AID HIGHWAY

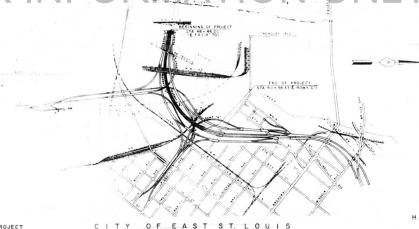
F.A. I. ROUTE 70 SECTION 82-3HVB PROJECT I-IG-70-1(€9)0

POPLAR STREET BRIDGE APPROACHES

ST. CLAIR COUNTY

C-98-059-64

OR INFORMATION ONLY



LOCATION OF SECTION INDICATED THUS: W 2/2 W

FA. I .- 70 82-3HVB ST. CLAIR 289 FED ROAD DIV NO 4 | ILLINOIS | PROJECT I-IG-70-1(6910

H. W. LOCHNER, INC ENGINEERS CHICAGO, ILLINOIS

2259

FOR INDEX OF SHEETS AND SUMMARY OF QUANTITIES

THIS SECTION AT SO INCLUDES ROUGH GRAINING, DRAIDIGE AND ELECTRICAL FACILITIES AND ALL APPURTERNANT AND COLLATERAL WERE NECESSARY TO OMPLETE HIS PROJECT, AS SHOWN ON THE PLANS.

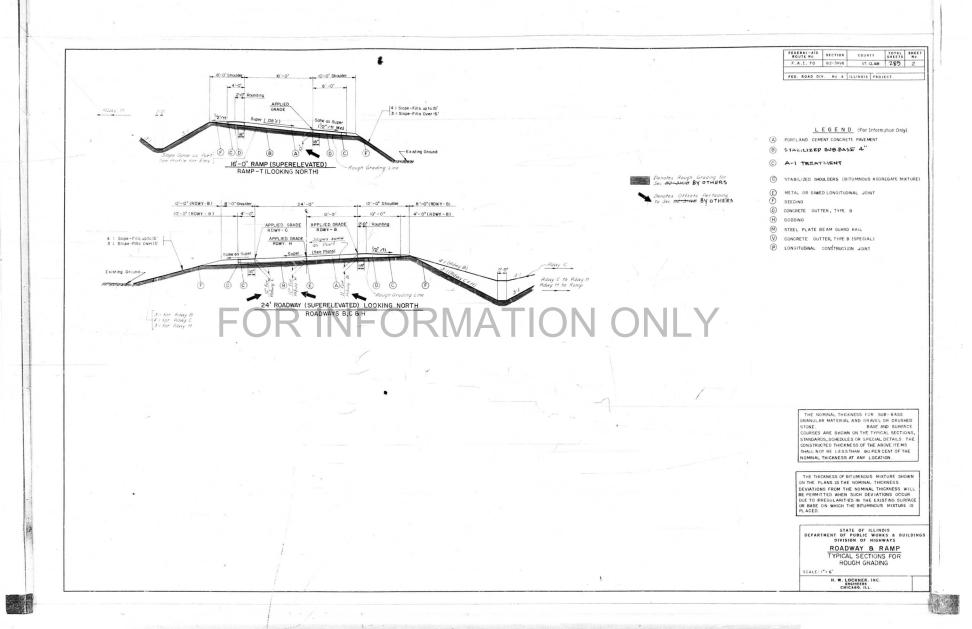
LENGTH OF PROJECT

REINFORCED CONCRETE

3190.33 FT. = .604MILES ROAD CLASSIFICATION 4454 -T-50 LOCATION PLAN

CONTELECT NO. 2 1130

ST CLAIR COUNTY SECTION 82-3HVB FA.I. ROUTE 70 PROJECT I-IG-70-1(69)0



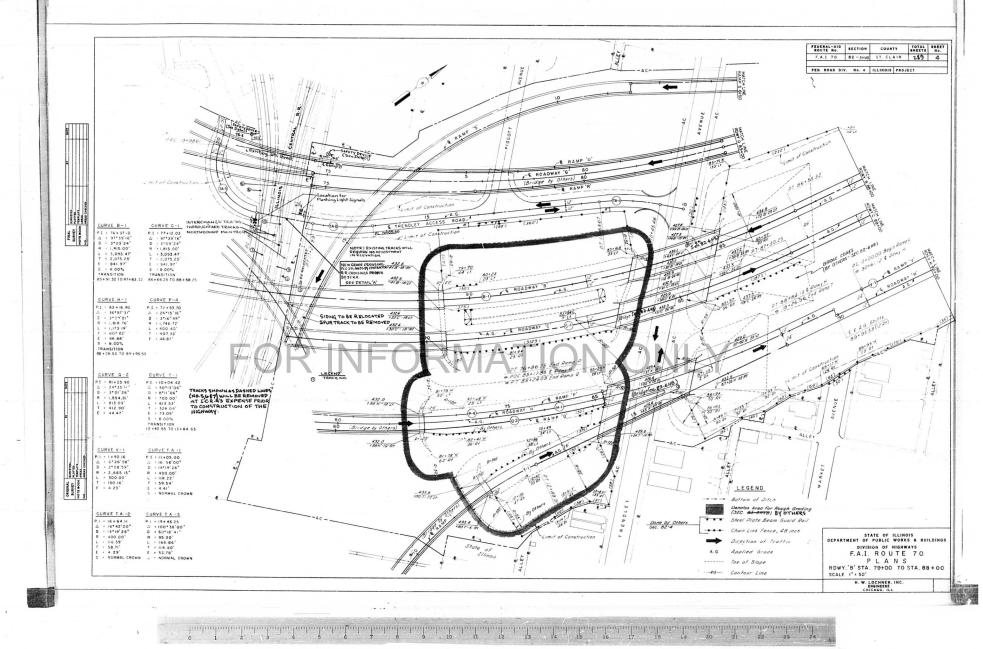
SECTION COUNTY TOTAL SHEET NO. SUMMARY OF QUANTITIES F. A. I. - 70 82 - 3 HVB ST. CLAIR 289 SECTION 82-3HVB FED. ROAD DIV. NO. 4 ILLINGIS PROJECT QUANTITY INDEX OF SHEETS 1G 10.88 % CODE NO. SECTION 82-3HVB QUANTITY I IG TOTAL UNIT ITEM CODE NO. SHEET NO. TITLE SHEET NO. 32 EACH LUMINAIRE, MERCURY VAPOR: WITH BUILT IN REGULATOR BALLAST: 170 AND 171 ABUTMENTS TYPICAL SECTION FOR ROUGH GRADING 01600 400 WATTS 1.02403 28,357 172 THRU 211 PIERS 25 272 3085 32 EACH LAMP, MERCURY VAPOR 400 WATTS. INDEX OF SHEETS, SUMMARY OF QUANTITIES, GENERAL NOTES 212 THRU 214 RAILROAD PROFILE 15 TYPE H33-1CD L02812 121 34,38 3C,30,3E,3F3G3H C6 PLAN - F.A.I. ROUTE 70 RDWY 'B' STA. 79+00 TO STA. 88+00 105 13 118 EXPANSION BOLTS 7/8 INCH THE THREE PAL BORING LOGS 0.9 EACH HAND HOLE, TYPE "A" 1.03263 PROFILE - F. A. I. ROUTE 70 RDWY 'B' STA. 79+49.83 TO STA. 103+00 9,451 CLASS A EXCAVATION FOR STRUCTURES 050001 CONCRETE PILE DETAILS CONTROL INSTALLATION (CONTROL LUMP L05064 CEN ER NO. 1) FROFILE - F.A.I. ROUTE 70 RDWY 'C' STA. 80+37. 83 TO STA. 102+50 18,986 2,318 261 THRU 276 RAILROAD TRESTUS 687 84 771 L04100 LIN FT TRENCH AND BACKFILL 30.571 3.732 24,303 PROTECTIVE COAT 052021 277 THRU 281 CROSS SECTION SHEETS 3,023 369 3,392 ELECTRIC CABLE IN CONDUIT. POUND FURNISHING & ERECTING STRUCTURAL STEEL 282 282 A 282 B STANDARD DRAWINGS 1686-2, 7213, 1527-2 10,024,474 1,223,814 11,243 290 (NE OPRENE-RUBBER INSULATED) 1/C NO. 10 05400 106036 PLAN - PROFILE & TYPICAL GRADING SECTION - RAMP O STANDARD DRAWINGS 2209 44,560 5,440 50000 TREATED TIMBER 057001 LIN FT ELECTRIC CABLE IN CONDUIT, 600 V (NEOPRENE-RUBBER INSULATED) 1/C NO. 6 1.136 1.726 15,862 PLAN OF EXISTING CONDITIONS & UTILITIES (PIGGOTT AVE. TO 284 1284 9 STANDARD DRAWINGS 1971-3, 2205 -/ 855.5 2500 HARDWARE 057001 106038 STANDARD DRAWINGS 2113-1 3,969,400 3537,519 431,871 DRAINAGE PLANS - RDWY 'B' STA. 79+00 TO STA. 88+00 POUND REINFORCEMENT BARS 059001 984 730 6714 LIN FT ELECTRIC CABLE IN CONDUIT, 600 V (NCOPRENE-RUBBER INSULATED) 1/C NO. 2 286 4286 A STANDARD DRAWINGS 2117 and 2126-1 DETAILS FOR JUNCTION BOX 'G' 390 48 438 LIN FT FURNISHING CREOSOTED PILES 20.1 TO 38 FEET STANDARD DB WING 2167-2 DETAILS FOR JUNCTION BOX 'H' 176 22 198 LIN FT ELECTRIC CABLE IN CONDUIT, 600V (NEOPRENE-RUBBER INSULATED) 1/C NO. 3/0 390 48 438 LIN FT DRIVING TIMBER PILES STANDARD DRAWING 2148-4 DETAILS FOR JUNCTION BOX 'K' STANDARD DRAWING 2177-3 104.076 12,706 116.782 LIN FT DRIVING CONCRETE PILES 06004 DETAILS FOR HINCTION BOY ! 1265 154 419 LIN FT ELECTRIC CABLE IN CONDUIT, 5.0 KV 104,076 12,706 116,782 LIN FT FURNISHING CONCRETE PILES 06004 (POLYETHYLENE INSULATED) 1.05065 68 76 TEST PILE CONCRETE 06004 25 LIN FT ELECTRIC CONDUCTOR IN CONDUIT 1.8 0.2 NAME PLATES 06100 (BARE ANNEALED COPPER) NO. 8 ELECTRICAL PLANS - RDWY 'B' STA. 48+48 TO STA. 58+50 LUMINAIRE MERCURY VAPOR 0.2 2 ELECTRICAL PLANS - RDWY 'B' STA. 58+50 TO STA. 66+50 1.8 EACH LO4969 UNDER PASS TYPE 175 WATTS
LAMP MERCURY VAPOR 175 WATTS LO 4987
TYPE H39-12KB AND SEWER PIPE, CLASS II - 27 ELECTRICAL PLANS - RDWY 'B' STA. 66+50 TO STA. 79+49.83 1.8 0.2 HJAB ELECTRICAL DETAILS - LIGHT STANDARDS ON BRIDGES & 513 63 576 LIN FT \*ELECTRIC CONDUCTOR IN CONDUIT AND SEWER PIPE, CLASS II, 64 (BARE ANNEALED COPPER NO. 6 (ALUMINUM POLE) ELECTRICAL DETAILS - ATTACHING CONDUITS & JUNCTION BOXES TO BRIDGES 24 -220 THE STORM SEWER, TYPE ), REINE CONGRETE CULVERT, STORM DRAIN SYSTEM GROUNDING L05066 SCHEMATIC WIRING DIAGRAM FOR CONTROL CENTER ELECTRICAL DETAILS - SERVICE POLES & CONTROL CENTER #1 Z01023 FOR HIGHWAY SIGNING EFFECTIVE MARCH 1, 1963 SHALL GOVERN THE TYPICAL GROUNDING DETAILS LOCATION & DETAILS FOR UNDERPASS LUMINAIRE RIGHT OF WAY PLANS (FOR INFORMATION ONLY) 0.8 Z20326 ALL ELEVATIONS REFER TO U.S.G.S. MEAN SEA LEVEL DATUM. Z20424 THE PROFILE GRADE LINE REFERS TO THE GRADE ELEVATION AT THE POINT SHOWN ON THE TYPICAL SECTIONS AND PLANS. RIGHT OF WAY PLANS (FOR INFORMATION ONLY Z20494 RIGHT OF WAY PLANS (FOR INFORMATION ONLY) ALL EXPOSED EXISTING PAVEMENT SHALL BE REMOVED WITHIN THE LIMITS OF RIGHT OF WAY, OR AS DIRECTED BY THE ENGINEER. X02791 RIGHT OF WAY PLANS (FOR INFORMATION ONLY) WHERE A CONSTRUCTED EMBARKMENT SLOPE INTERSECTS EXISTING PAYEMENT, THE PAYEMENT SHALL BE REMOVED TO A POINT WHERE THE CONSTRUCTED EMBARKMENT IS TWO FEET ABOVE THE EXISTING PAYEMENT. RIGHT OF WAY PLANS (FOR INFORMATION ONLY) 650 REMOVAL & REPLACEMENT 84 774 SLOPE WALL 4 INCH 083002 5UM OF EXISTING TRACK FACILITIES X02792 LIST OF BENCH MARKS, TIES TO TRAVERSE LINE AND GENERAL PLAN OF TRAVERSE LINE 52 20 PAILROAD PROTECTIVE SERVICE FOIDS BUILDINGS WITHIN R.O.W. LIMITS HAVE BEEN REMOVED OR ARE IN THE PROCESS OF BEING REMOVED DOWN TO EXISTING GROUND LEVEL AND BASEMENTS BACKFILLED WITH DEBRIS FILL. ALIGNMENT PLAN - RDWY 'C' STA. 48+48 TO STA. 71+00 335 CONDUIT IN TRENCH, 3-INCH DIA., PERMANENT BARRICADES 27 3 30 GALVANIZED STEEL 1.00008 Z 01378 FACH ENGINEER'S FIELD OFFICE ALIGNMENT PLAN - RDWY 'C' STA. 71+00 TO STA. 93+0 01 35 320 CONDUIT ATTACHED TO STRUCTURE. Z 01379 THE FOLLOWING UTILITY COMPARIES HAVE FACILITIES WITHIN THE LIMITS OF COME PRUCTION WHICH HAVE REQUIRE ADULTMENTS CASES STLODIS AND INTERUBAN WATER COMPANY LILINGUS FOWER COMPANY SOUTHWESTERN BELL TELEPHONE COMPANY UNION ELECTRIC COMPANY UNION ELECTRIC COMPANY EACH ENGINEER'S FIELD LABORATORY 0-1 1-1/4 INCH DIA., GALVANIZED STEEL LINFT STORM SEWER TYPES, (QCP) CLITT 18" 1.00054 178 22 200 LINET. STORM SEWERTHPE 2 (ROP) CLIE!15" ,891 841 LIN FT CONDUIT ATTACHED TO STRUCTURE, 2-INCH DIA., GALVANIZED STEEL L00056 KEY PLAN, GENERAL NOTES AND BILL OF MATERIAL CATCH BASIN TYPE A with TYPE & Grate CONDUIT ATTACHED TO STRUCTURE, 2-1/2 INCH DIA., GALVANIZED STEEL 37 THRU 41 GENERAL PLANS STATE OF ILLINOIS 1.00057 42 THRU 50 PLAN AND ELEVATION DEPARTMENT OF PUBLIC WORKS & BLDGS THE PLUS AND MINUS SKINS SHOWN ON THE PROFILE GRADES ARE DETERMINED BY THE DIRECTION OF PROPOSED TRAFFIC. CONDUIT IN CONCRETE 1 1/4" DIA GALVANIZED STEEL 51 THRU 58 GEOMETRIC LAYOUTS DIVISION OF HIGHWAYS 1.00111 59 THRU 79 SLABS INDEX OF SHEETS 389 47 436 CONDUIT IN CONCRETE, 3-INCH DIA., 80 THRU 98 PARAPET AND HANDRAIL ASBESTOS CEMENT SUMMARY OF QUANTITIES 640 IN . FT. TEMPORARY WOVEN WIRE FENCE, 4' ZOIISE GENERAL NOTES IF THRU 169 FRAMING FLANS AND STEEL DETAILS 29 3 32 POLE, ALUMINUM, ANCHOR BASE, 30 FT. MH, 4 FT. MAST ARM F. A. I. RT. 70 ST. CLAIR CO. SECTION B2-3HVB H. W. LOCHNER, INC. ENGINEERS \* NON- PARTICIPATING CHICAGO

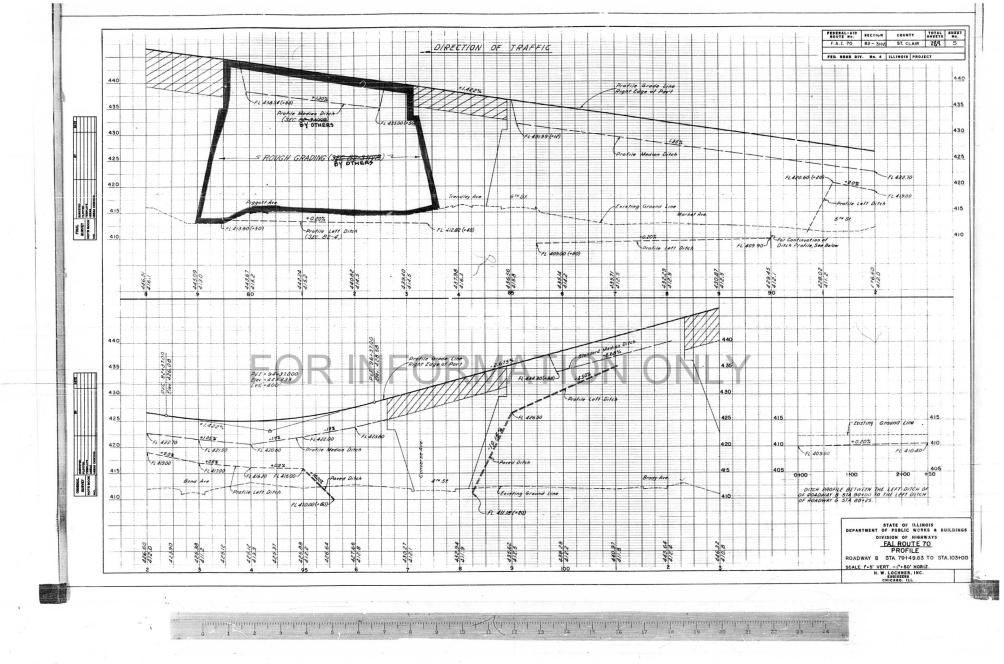
NON- PARTICIPATING 7/275-DOW-Deleted aPM

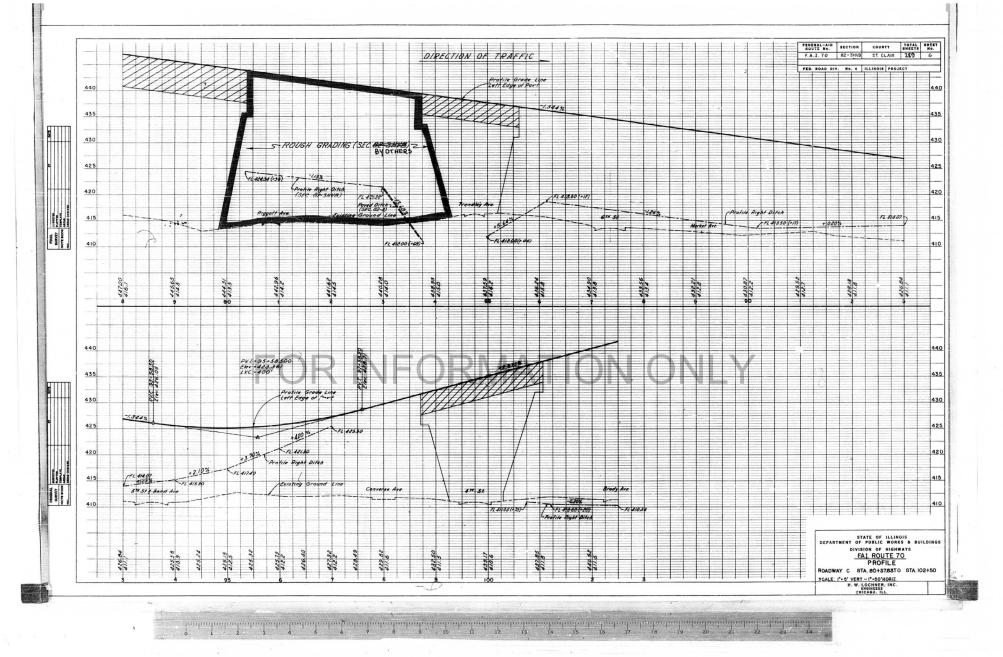
Permanent Borricades Edied

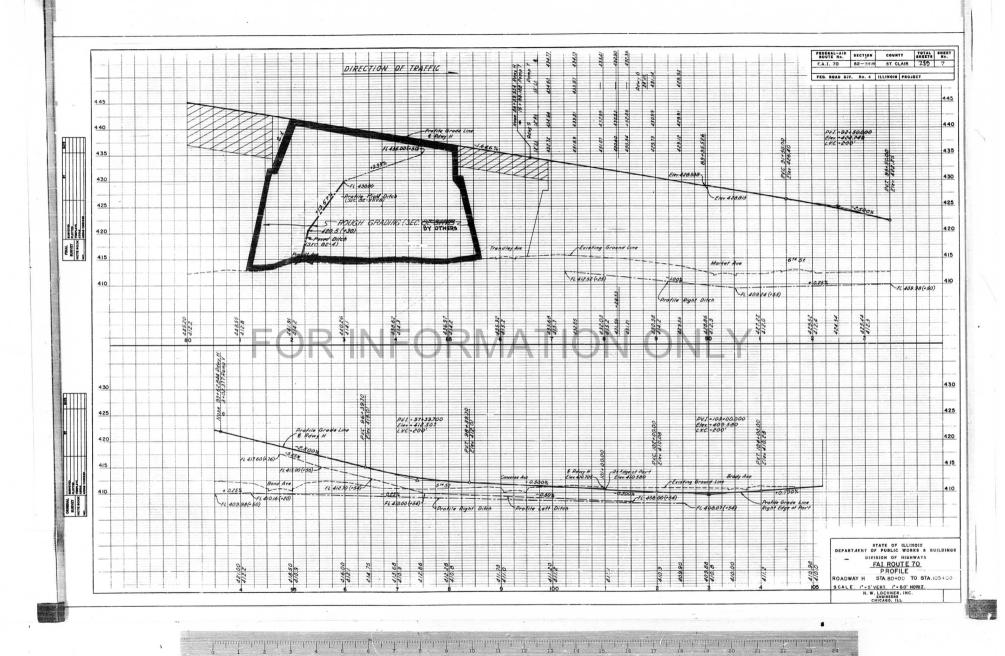
Revised CIX Conc. from 21,150 3 Cy+ 0 21,30 ECY with white Freshed 640 len P. M. W. P.

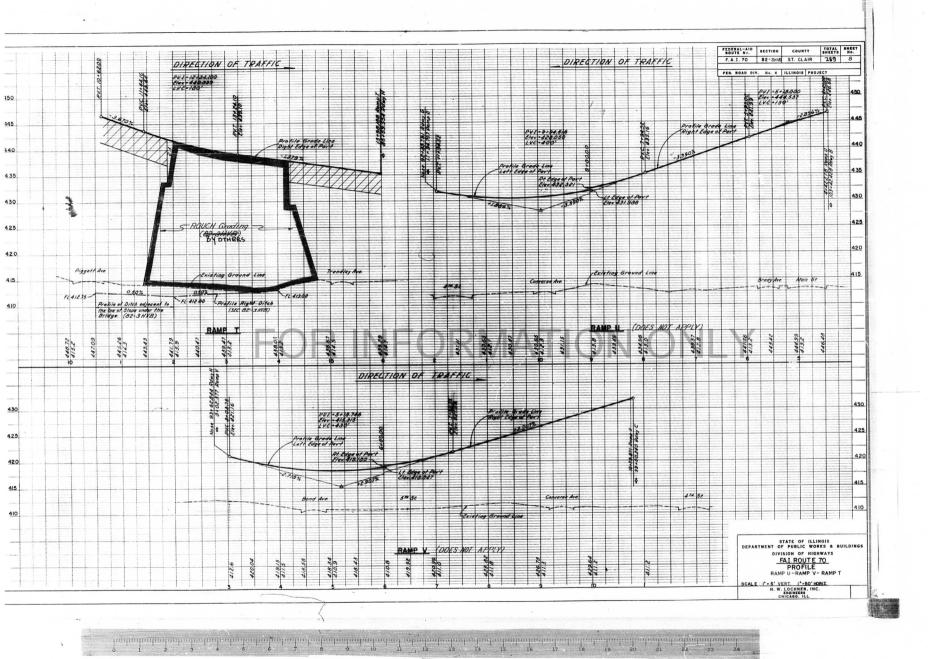
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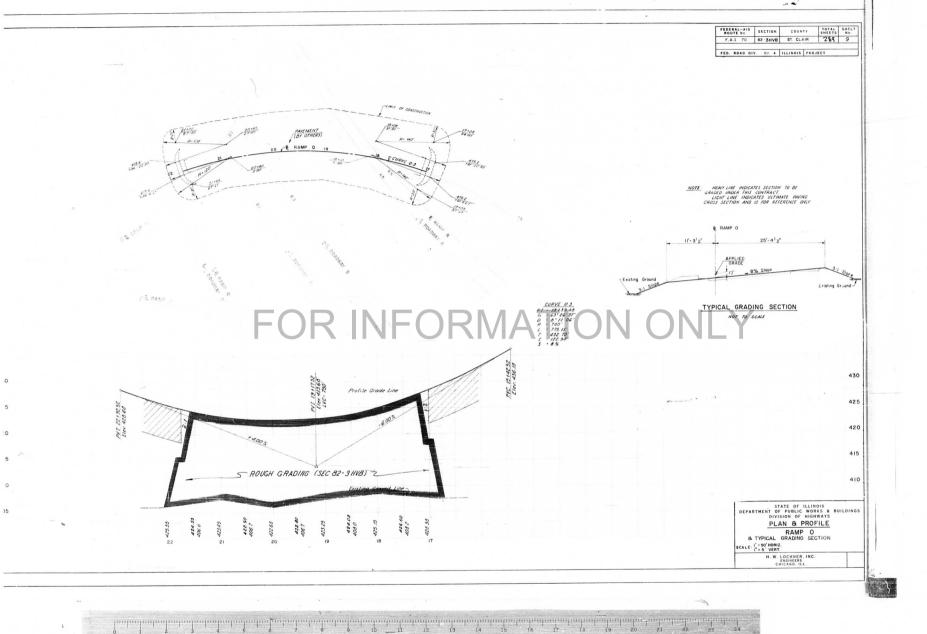


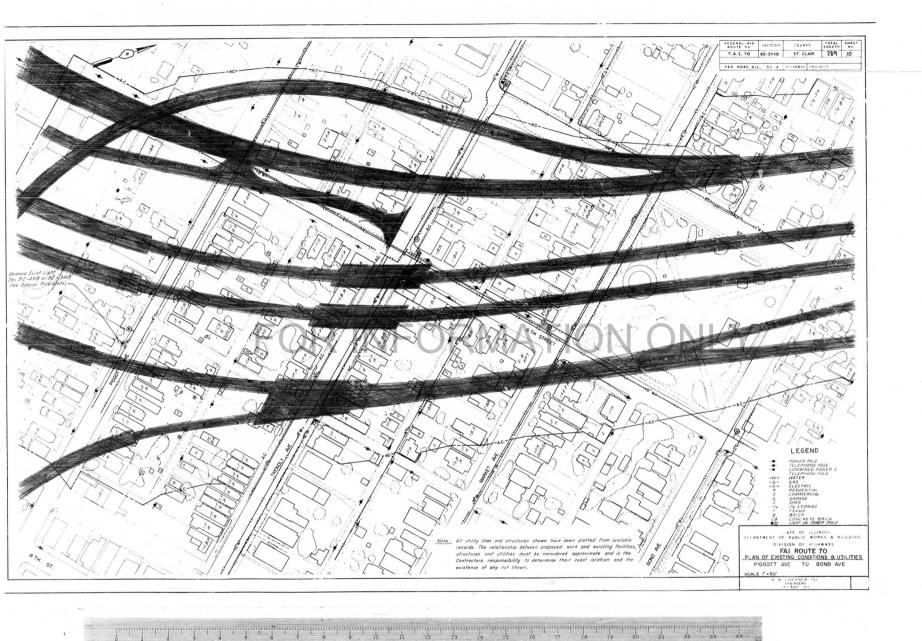


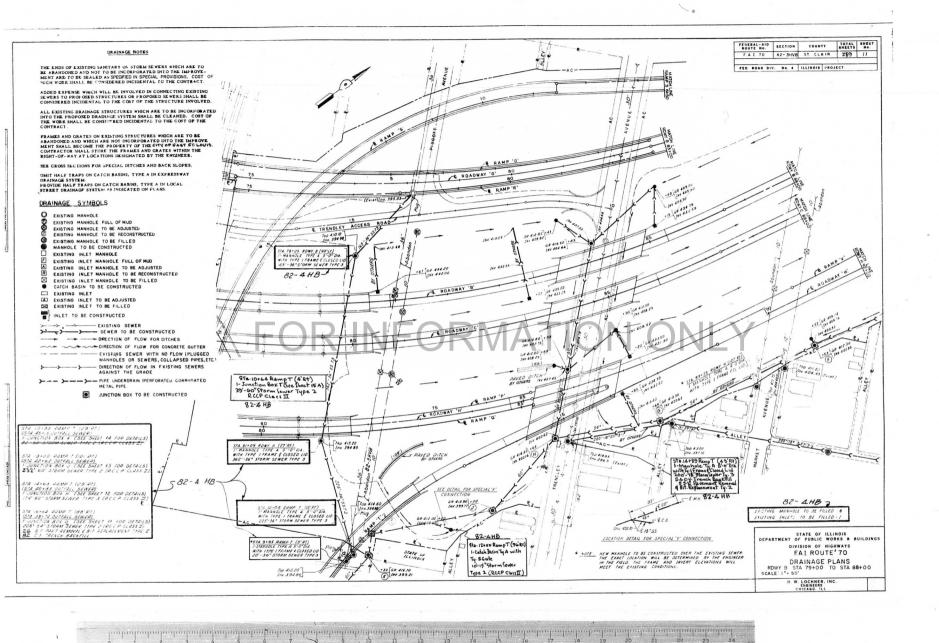


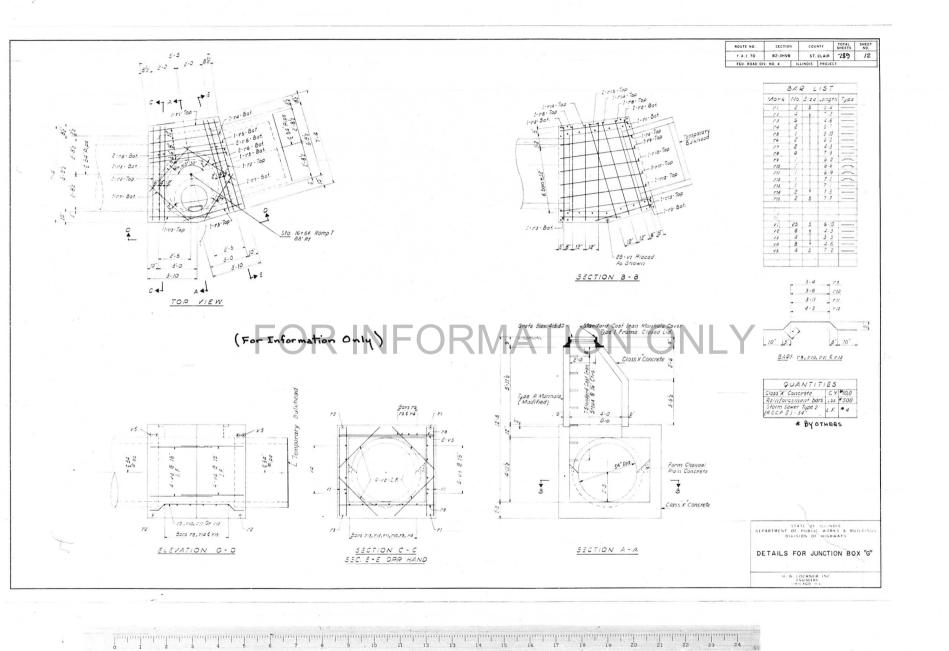


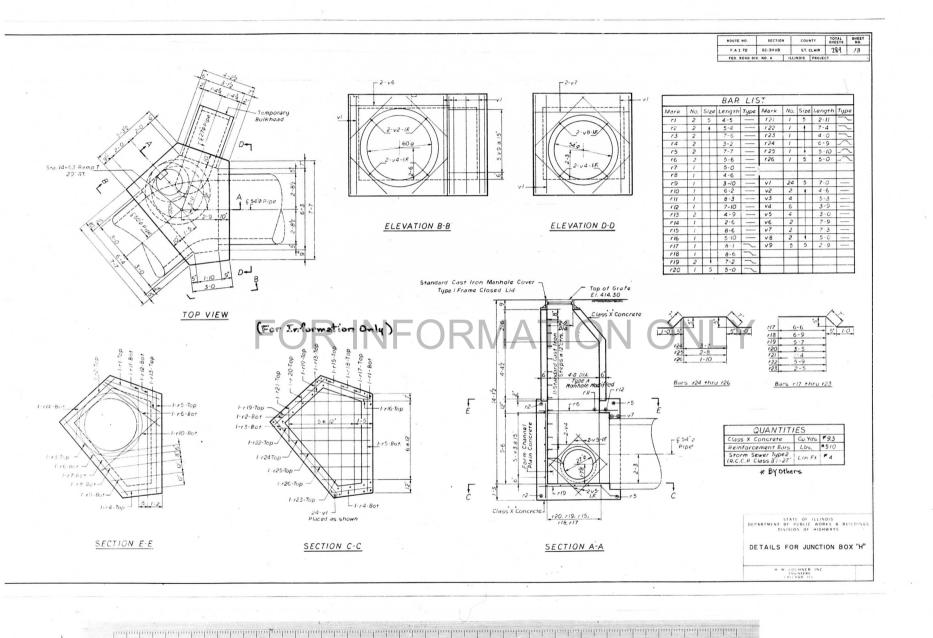


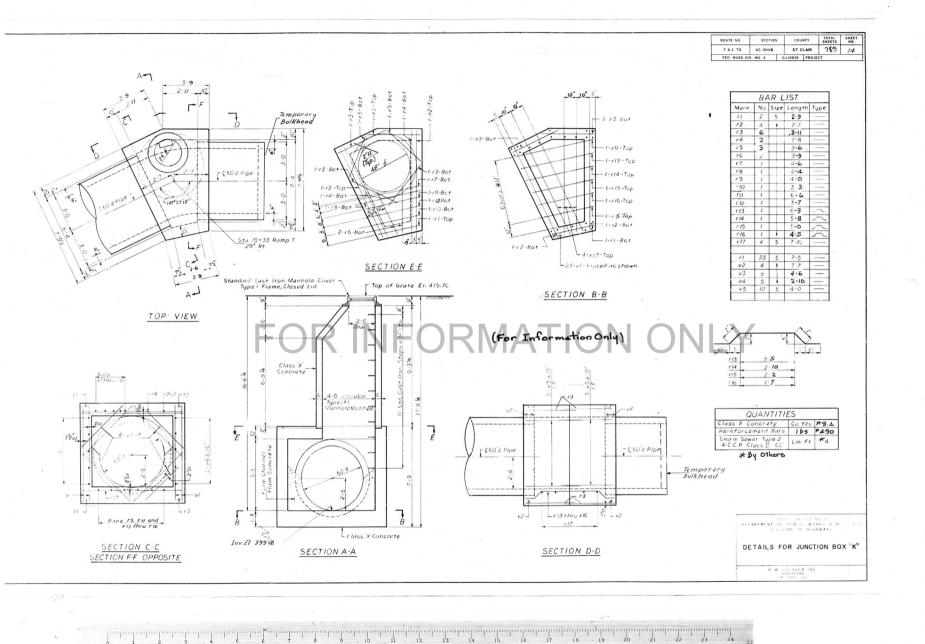


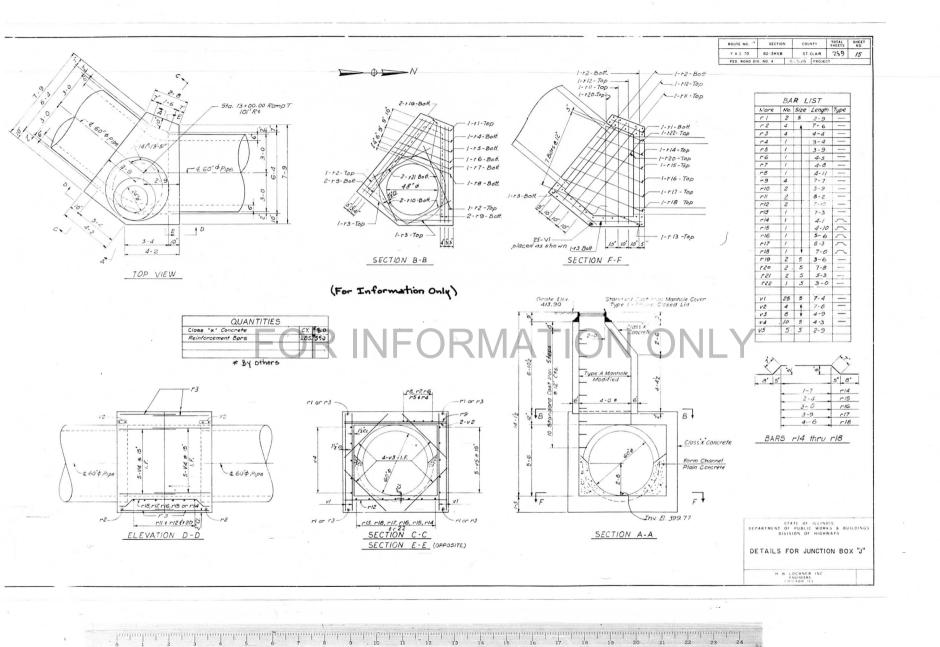


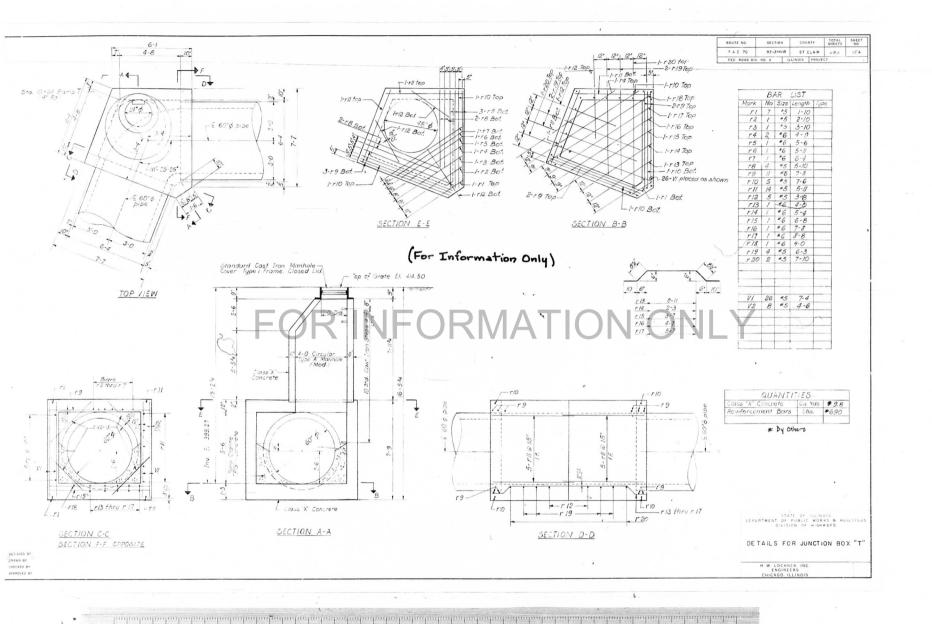


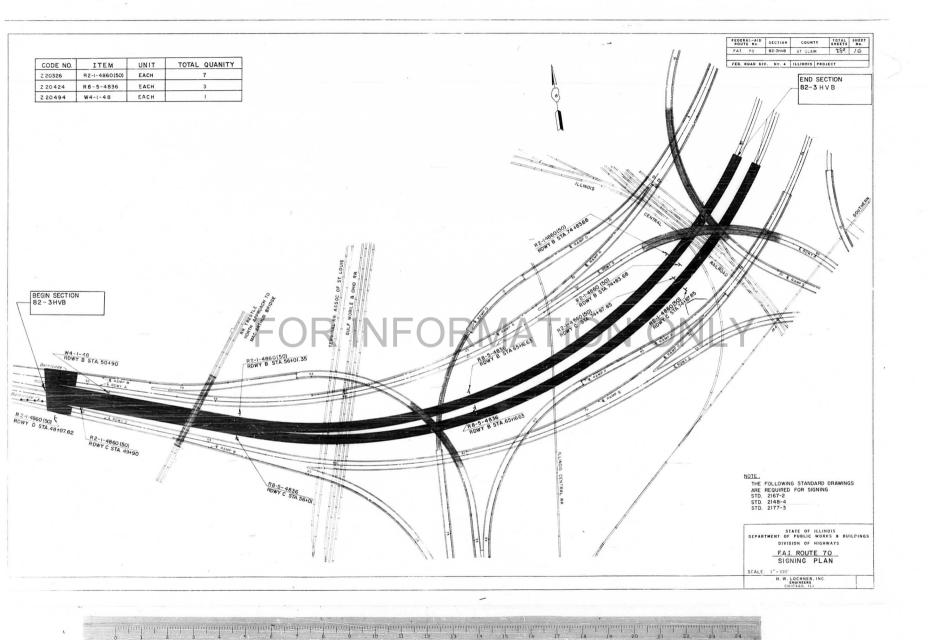


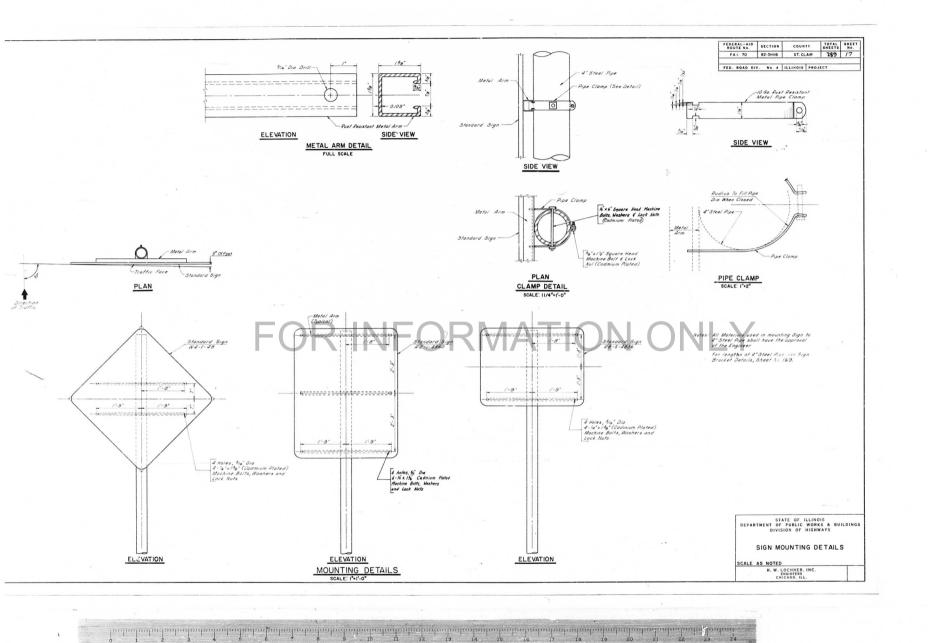


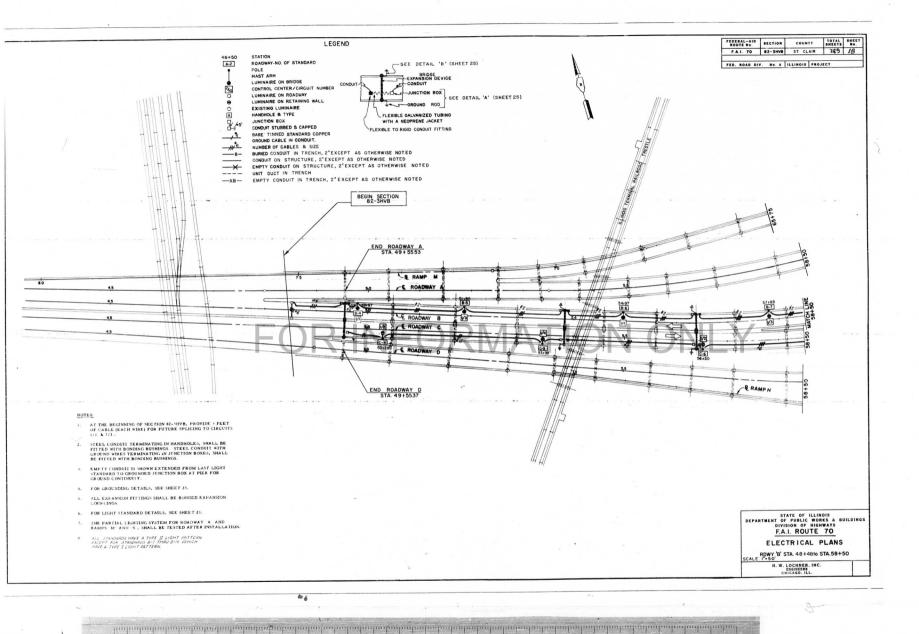


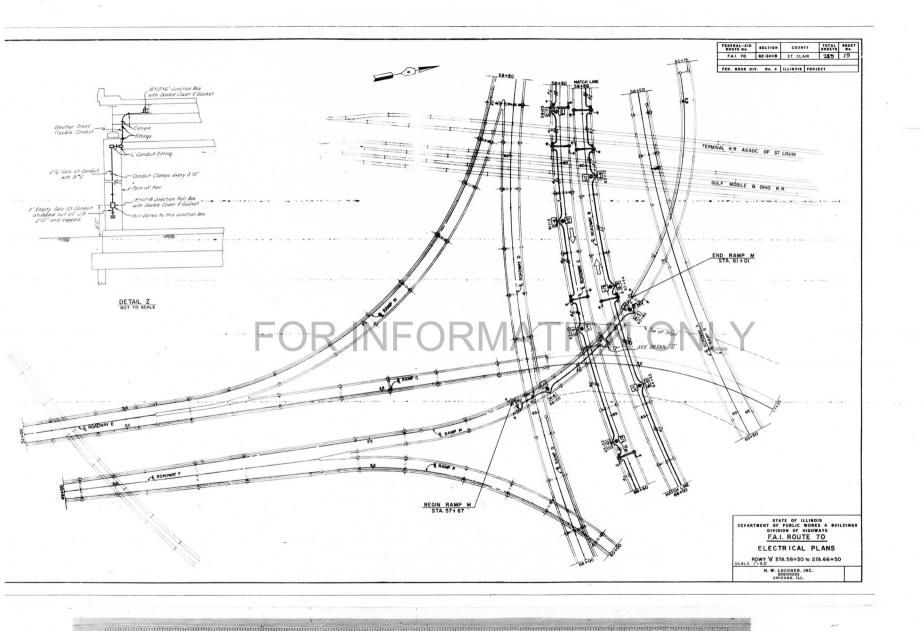


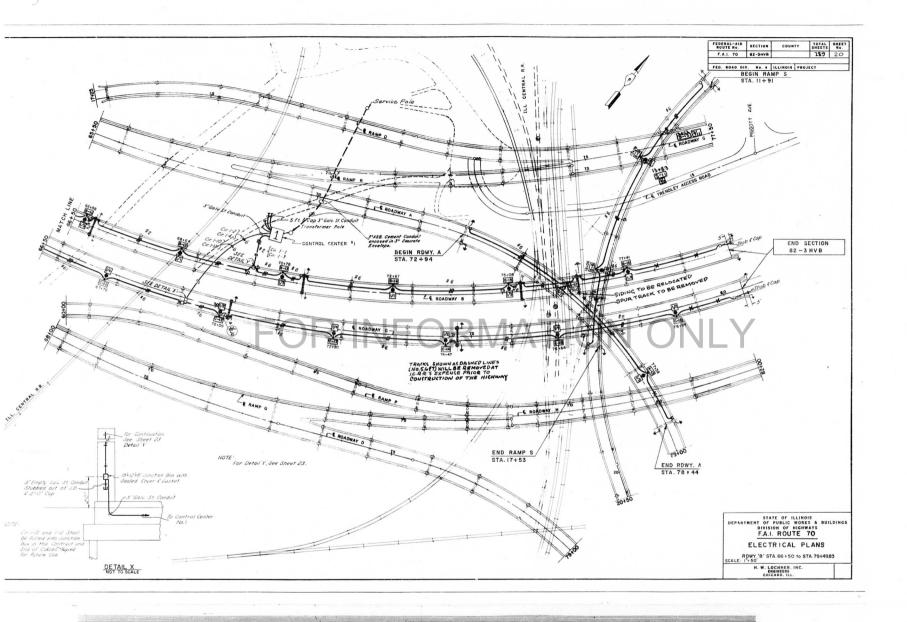


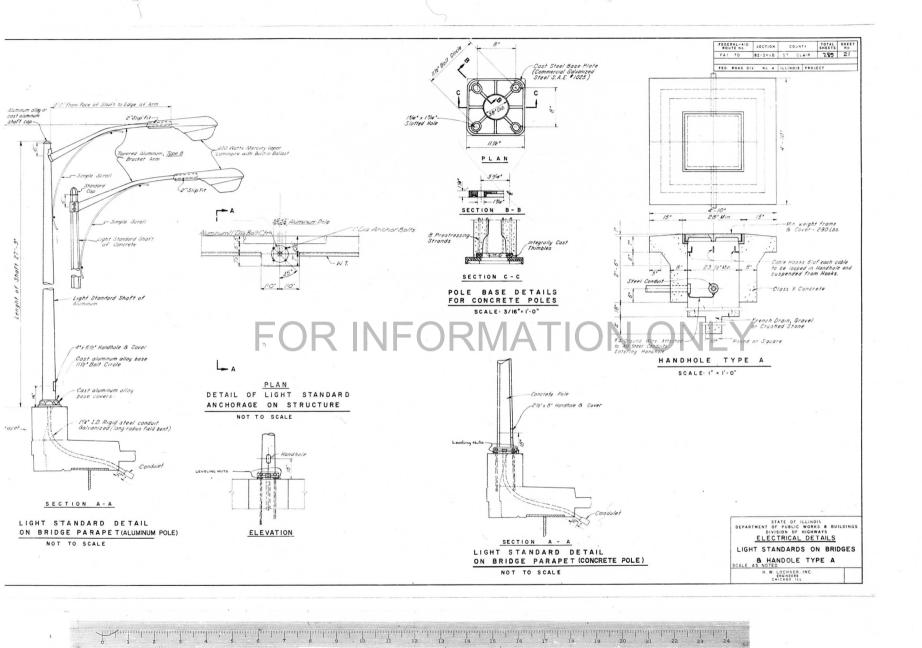


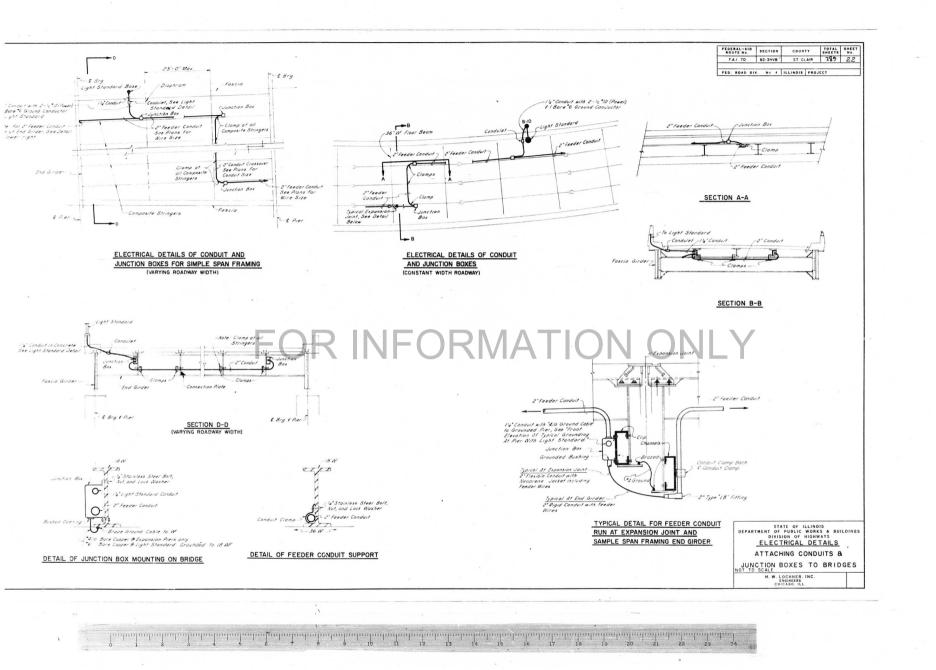










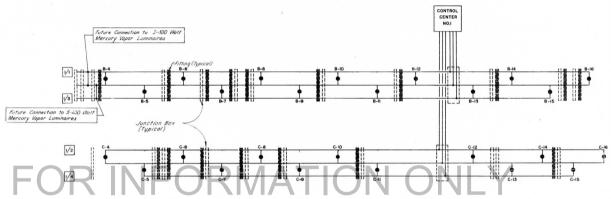


FEDERAL-AID SECTION COUNTY SHEETS NO.

F.A.1 70 82-3HVB ST. CLAIR 7.89 23 FED. ROAD DIV. No. 4 ILLINOIS PROJECT

Secret Cover & Gasket - '2' Conduit Fitting - Conduit Clamps, every 5'-0" 2" Galv. St. Conduit for 1-3 Wire Circuit #6 2½" Galv. St. Conduit for 2-3 Wire Circuits, or 1-3 Wire Circuit Larger than #6 S Face of Pier 5-12" x 10" x8" Junction Full Box Sealed Cover & Gasket

> DETAIL'Y'
> TYPICAL SERVICE FEED AT PIER NOT TO SCALE



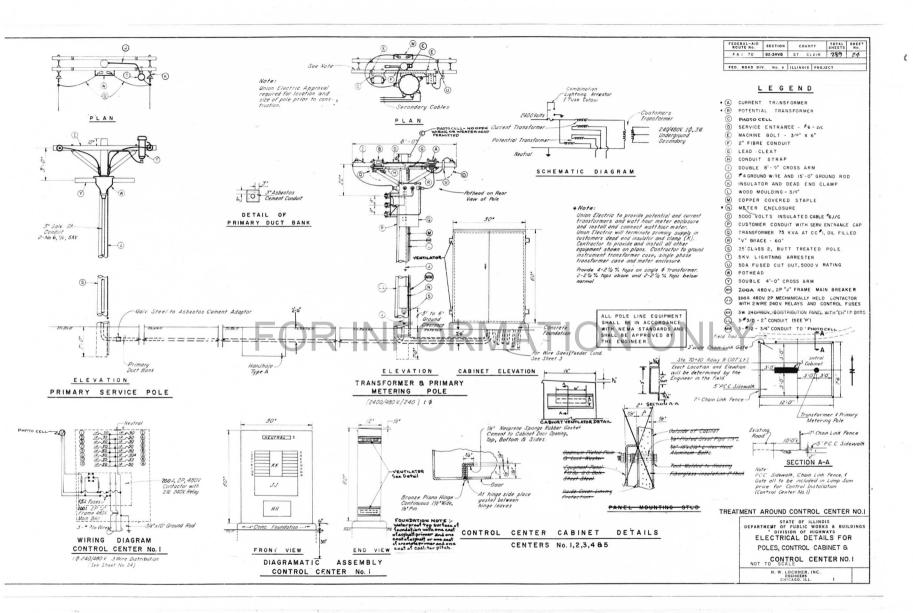
SCHEMATIC WIRING DIAGRAM

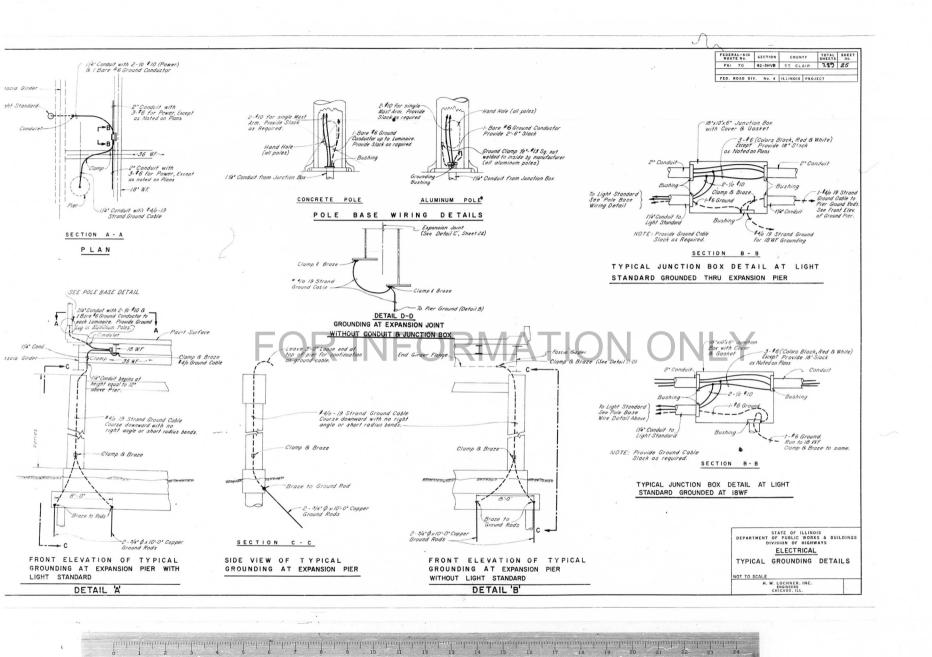
(240/480V, 10,3 Wire)

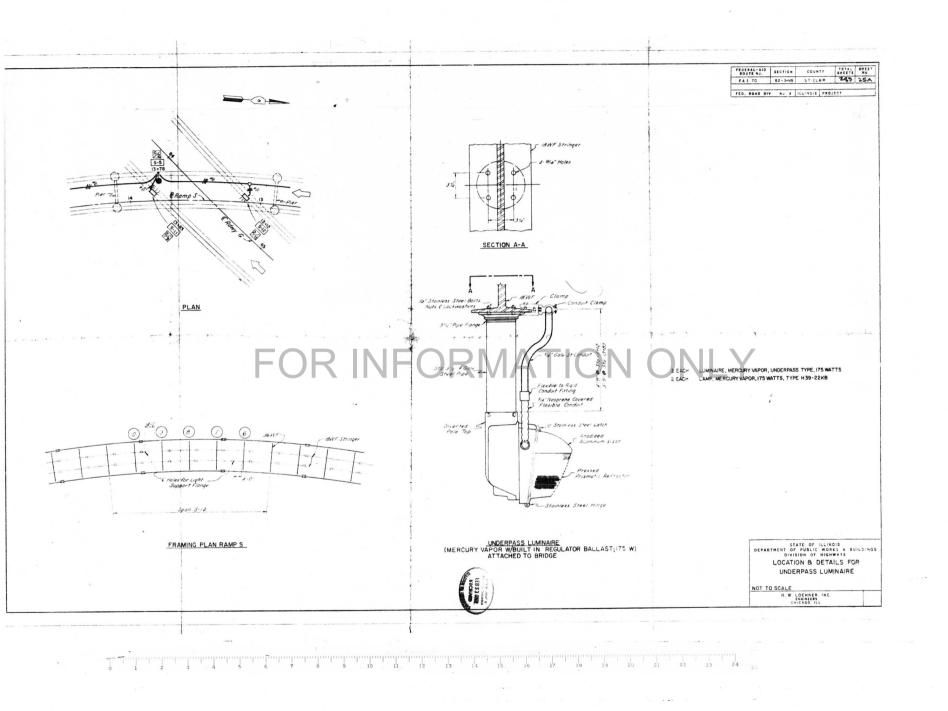
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 19 19 20 21 62 23 24

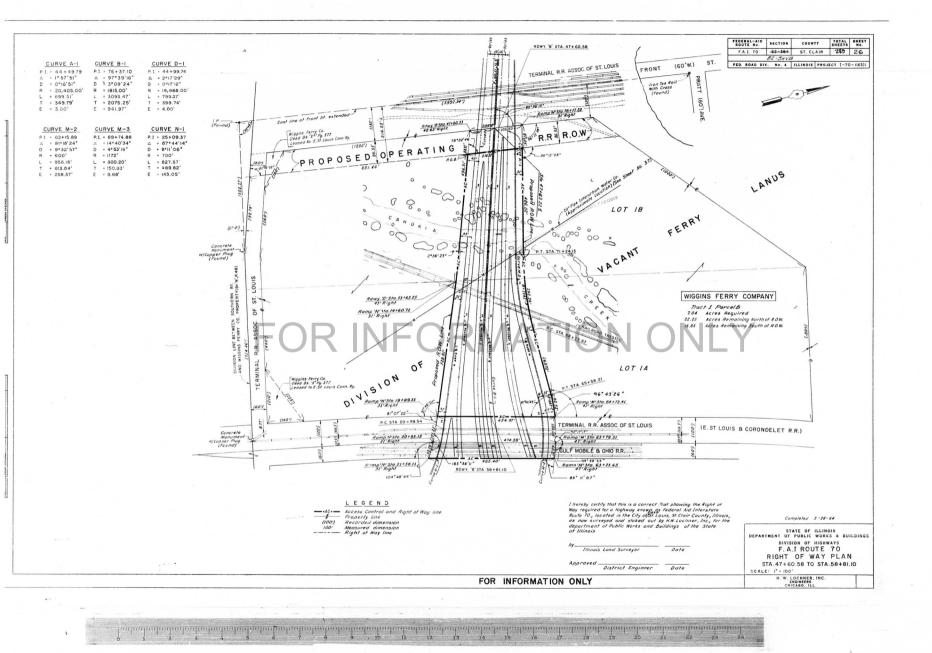
STATE OF ILLINOIS
DEPARTMENT OF PUBLIC WORKS & BUILDINGS
DIVISION OF HIGHWAYS
ELECTRICAL DETAILS

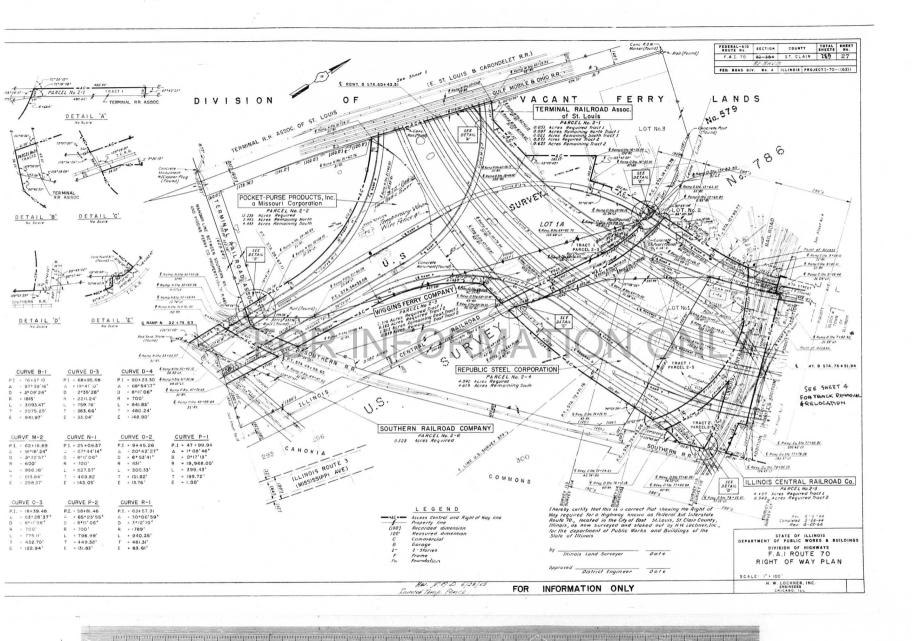
TYPICAL SERVICE FEED AT PIER 8 SCHEMATIC WIRING DIAGRAM FOR CONTROL CENTER NO.1 H. W. LOCHNER. INC. ENGINEERS CHICAGO. ILL.

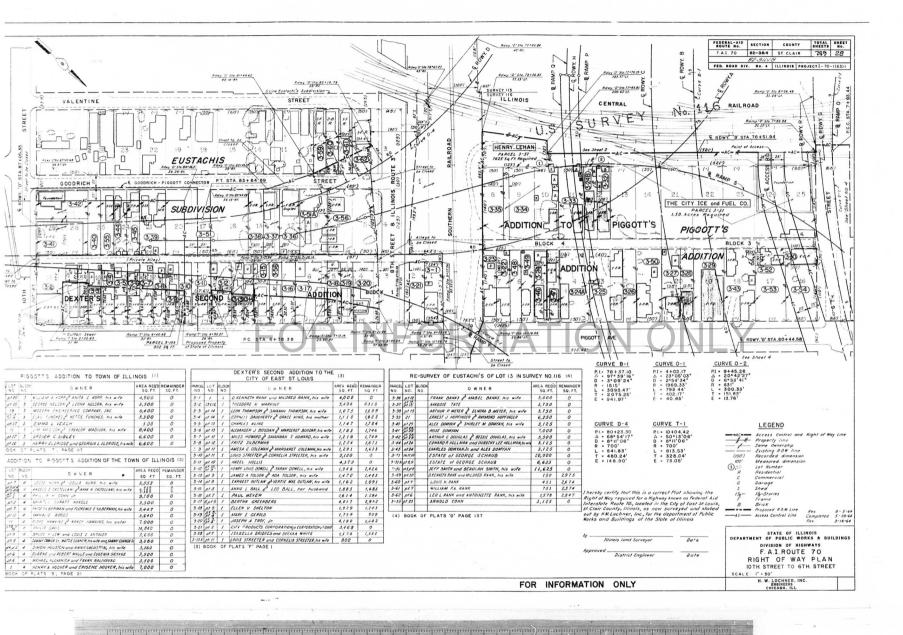


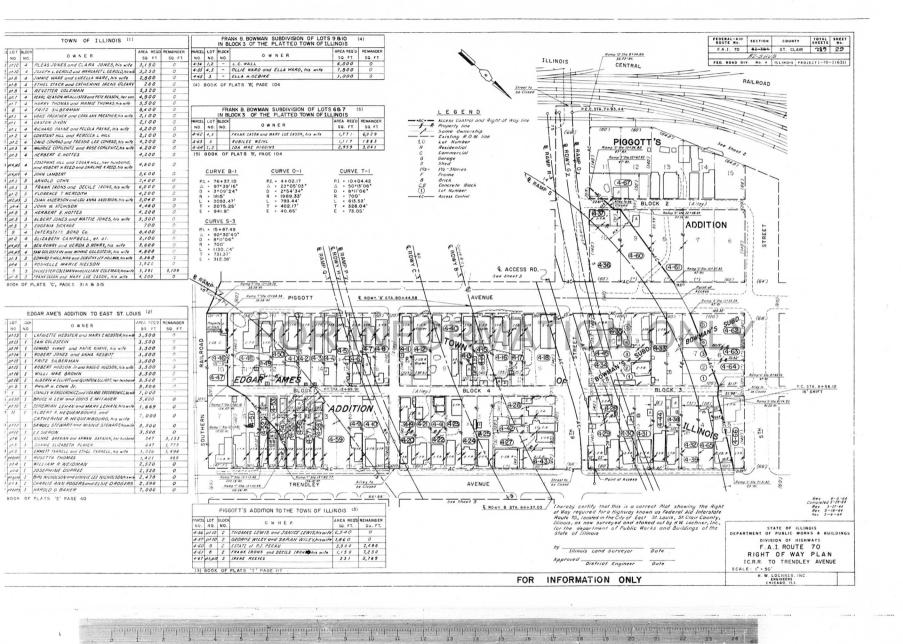


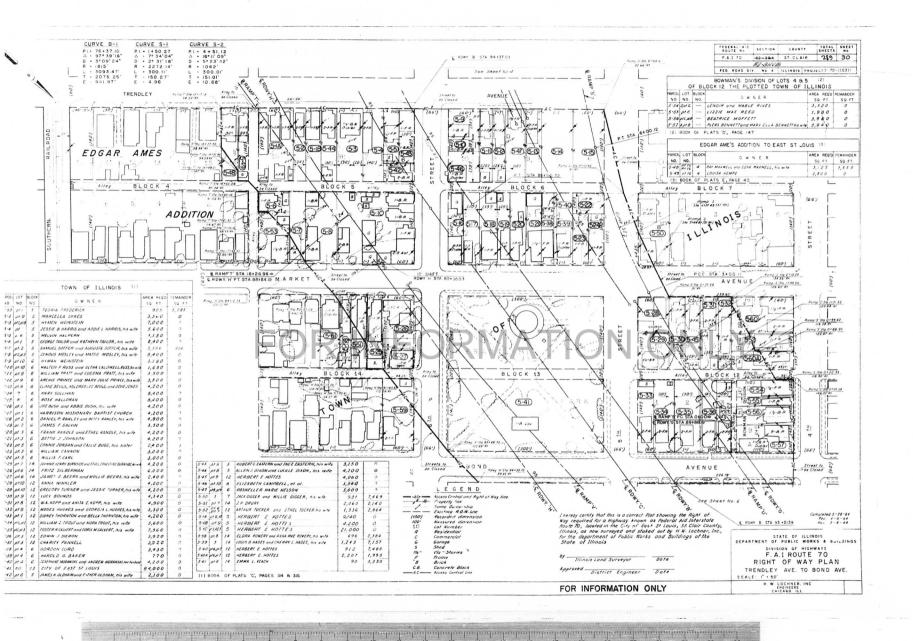


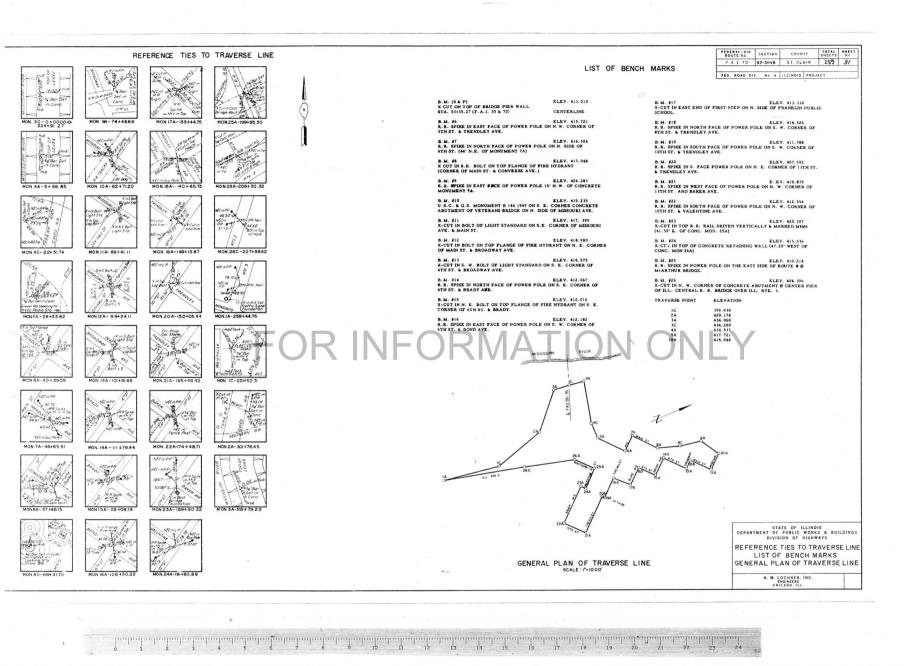


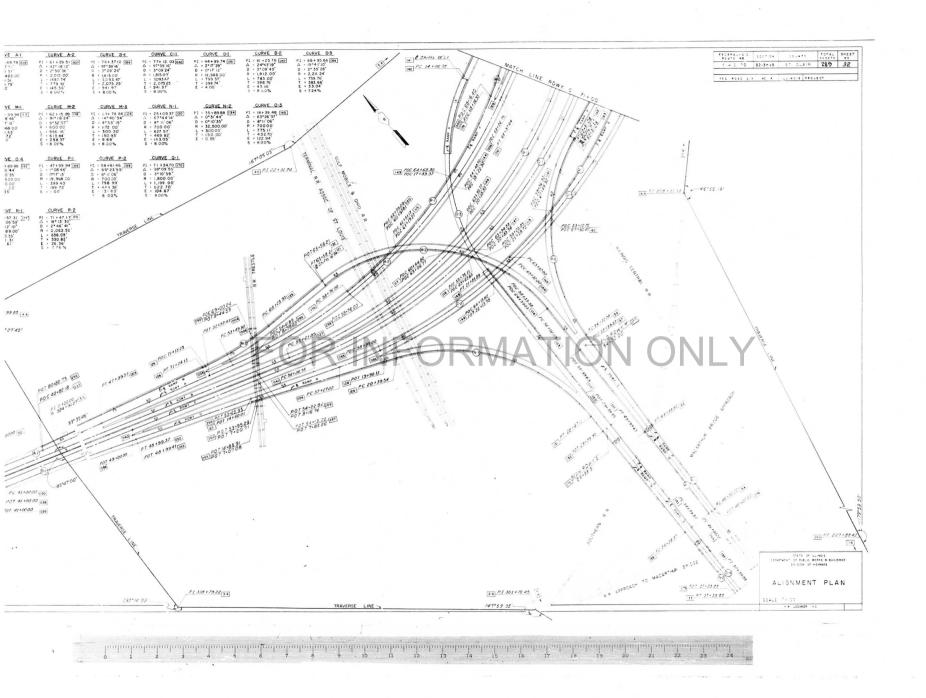


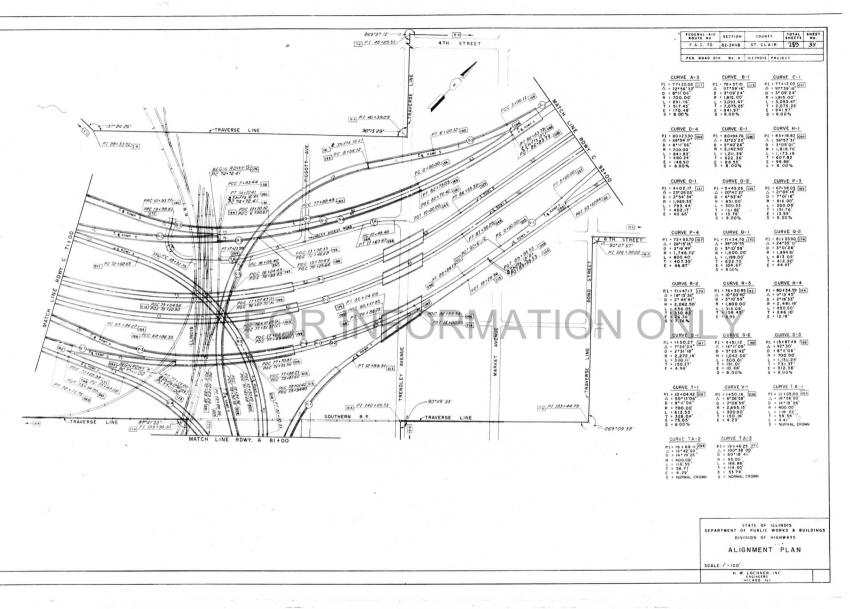










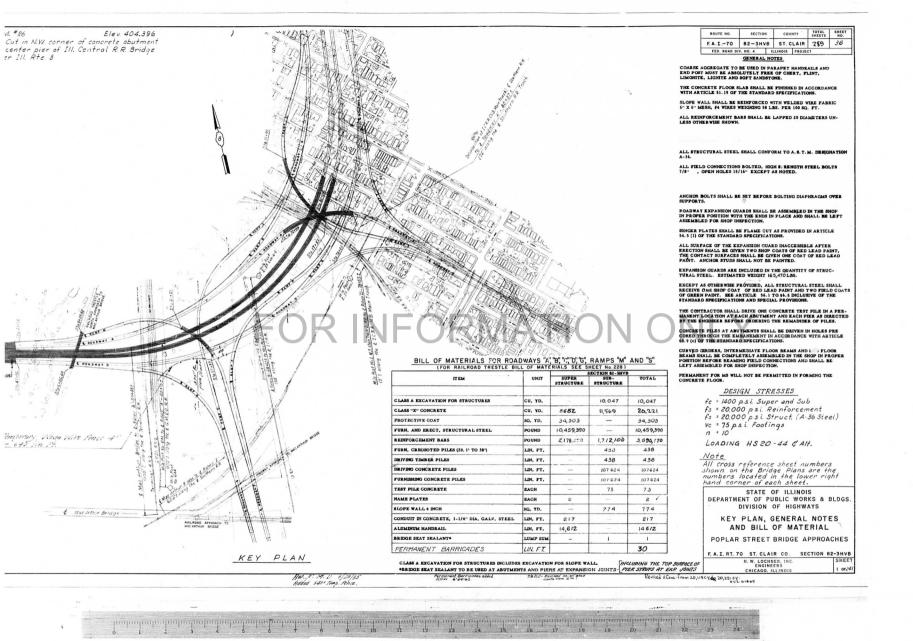


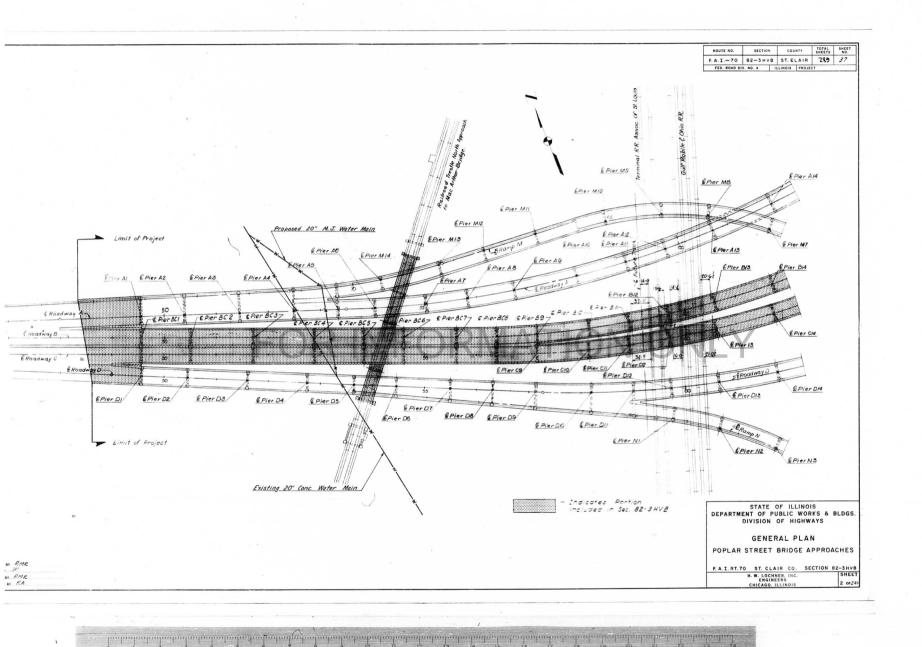
FEDERAL-AID SECTION COUNTY SHEET NO. FALL 70 82-3HVB ST. CLAIR SHEET NO. 74L 70 82-3HVB ST. CLAIR 72 72 34

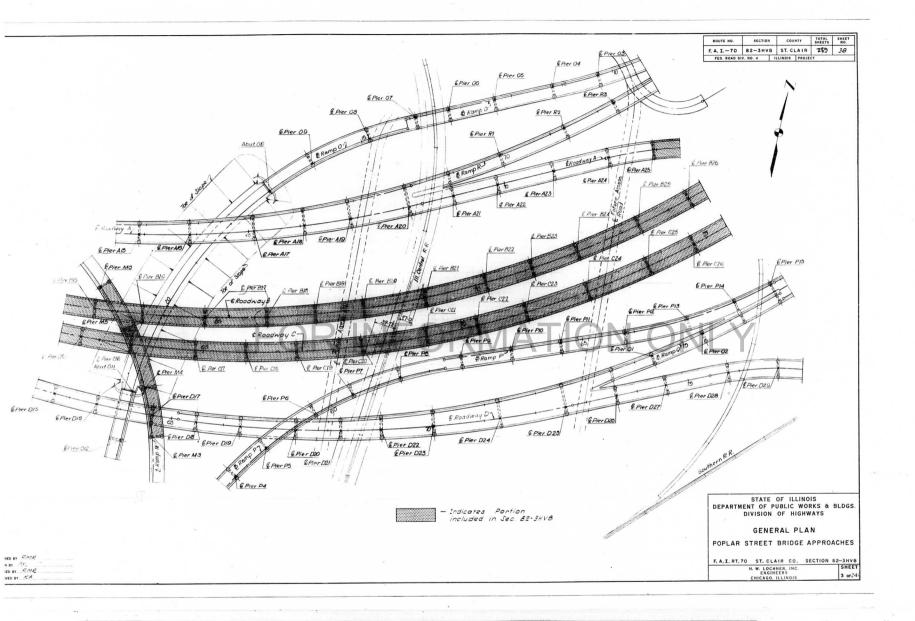
			1	1	700-00 - 00-00 - 00-00 - 00-00 - 00-00 - 00-00 - 00-00 - 00-00 - 00-00 - 00-00 - 00-00 - 00-00 - 00-00 - 00-00	02-3HVB 31. CEMIN 259 34						
COORI		DESCRIPTION	POINT CODE NO	COORDINATE NORTH EAST	DESCRIPTION	CODE NO	COORDINATE NORTH EAST	DESCRIPTION		t	FED. ROAD DI	V. No. 4 ILLINOIS PROJECT
NORTH	EAST	POINT LOCATIONS			DWAY "A"		ROAD	WAY "D"				
		TRAVERSE POINT	017	9,670.926 33,450.174	P.I. CURVE A-3	062	9,004.502 33,045.131	NOSE RDWY "D" & RAMP "Q"				
3,585.015 5,770.707	31, 748, 167	TRAVERSE POINT	018	9,289.695 33,800.024	P. T. CURVE A-3	063	9,076.907 33,262.414	P.C. CURVE D-4	POINT CODE NO	NORTH	DINATE EAST	DESCRIPTION
7,707,391	31, 473, 777	TRAVERSE POINT	019	9, 017, 044 34, 050, 227	P. O. T. RDWY. "A" NOSE 20' LT.	064	9,267.890 33,703.100	P.1. CURVE D-4	CODE NO	HOMEL		MAX "H"
	30, 191, 148	TRAVERSE POINT	020	9,030.566 34,064.963	NOSE RDWY. "A" & RAMP "T"	065	8,925.526 34,039.88	P. T. CURVE D-4			-	1
8,827.340	663400000000000000000000000000000000000	TRAVERSE POINT	021	8, 198. 565 34, 801. 328	P.C. CURVE A-4	066	8,853.313 34,110.91	P.O.T. RDWY. "D" NOSE 19' LT.	100	10, 373. 793	33,961.554	P.O.T. RDWY. "H"
9, 438. 510	30, 227. 520		022		P.I. CURVE A-4	067	8,866.638 34,124.46	NOSE RDWY "D" & RAMP "S"	101	10,734.205	34, 032. 453	P.O.T. RDWY. "H" NOSE 20' LT.
10,030.665	30, 323. 293	TRAVERSE POINT	023		P.R. C. CURVE A-4 & 5	068	8,461.458 34,496.37	P.C. CURVE D-5	102	10,738.063	34, 012. 828	NOSE RDWY. "H" & RAMP "Y"
9,673.297	31, 915. 572	TRAVERSE POINT	024		P.I. CURVE A-5	069	8,318.877 34,636.63	P.I. CURVE D-5	103	11,614.254	34, 205. 572	P.O.T. RDWY. "H" & SHIFTS 14" RT.
9,676.088	32,517.646	TRAVERSE POINT	025		P. T. CURVE A-5	070	8, 171. 519 34, 771. 85	P.C.C. CURVE D-5 & 6	104	11,611.552	34, 219. 309	P. C. CURVE "-2
10,495.902	33, 401. 150	TRAVERSE POINT			L	071		P.I. CURVE D-6	105	11,743,077	34, 245, 182	P.I. CURVE H-2
10,957.004	32, 977. 137	TRAVERSE POINT		ROA	DWAY "B"	072		P.R. C. CURVE D-6 & 7	106	11,737.272	34, 266, 446	
11,693.731	33,767.717	TRAVERSE POINT	026	9, 531. 766 30, 003. 011	P.O.T. BEGIN RDWY. "B"; BEGIN RDWY. "A" 24' LT.	073		P.I. CURVE D-7	107	11,751,762	34, 241, 326	P. O. C. RDWY. "H" NOSE 29' LT.
12,543.360	34, 017. 374	TRAVERSE POINT	027	9,061.065 31,387.008	P.C. CURVE B-1	074		P. T. CURVE D-7	108	11,833.916		NOSE RDWY. "H" & 4TH ST.
13, 343. 702	34, 181. 316	TRAVERSE POINT	028	8, 392. 855 33, 351. 732	P.I. CURVE B-1				100	11,033.910	34, 343. 755	P. T. CURVE H-2 END RDWY. "H"
13,769.336	34, 885. 169	TRAVERSE POINT	029	10,429.078 33,752.290	P. T. CURVE B-1		ROADWAY "E"					
13,276.148	35, 338. 540	TRAVERSE POINT	030	12,084.459 34,077.930	P. O. T. RDWY. "B" NOSE 27' LT.	075	8,062.906 32,133.03	NOSE & BEGIN ROADWAY "E"	109	7, 560, 147	32, 216. 633	AMP "M"
12,677.994	34,689.002	TRAVERSE POINT	031	12,089.671 34,051.437	NOSE RDWY "B" & RAMP "U"	076	7,263.307 32,105.85		110			P.C. CURVE M-1 BEGIN RAMP "M"
12,406,926	34,937.255	TRAVERSE POINT	032	12,526.713 34,164.928	P.C. CURVE B-2	-		12' RT. END RAMP "O" 12' LT.	1	7, 759. 505	32, 228. 652	F.I. CURVE M-1
11,741.037	34, 211. 759	TRAVERSE POINT	033	12,942.279 34,246.676	P.I. CURVE B-2		R	OADWAY "F"	111	7,959.065	32, 236, 680	P. T. CURVE M-1
11,203.440	34, 709. 666	TRAVERSE POINT	034	13,258.700 34,528.201	P.C.C. CURVE B-2 & 3	077	8, 357. 753 32, 276. 74	NOSE & END ROADWAY "F"	112	8,358.718	32, 252. 759	P.O. T. RAMP "M" NOSE 24' RT.
10,714.228	34, 179. 991	TRAVERSE POINT	035	13, 787.672 34,998.836	P.I. CURVE B-3	078	7,559.424 32,228.61	P. O. T. RDWY. "F" BEGIN RAMP "M"	113	8,560.973	32, 260. 896	P.C. CURVE M-2
10,188.208	34, 663. 578	TRAVERSE POINT	036	13,942.851 35,689.652	P. T. CURVE B-3			12' LT. BEGIN RAMP "P" 12' RT.	114	8,788.678	32, 225. 787	P.O.C. INT. B's RAMP "M" & RDWY "D"
9, 692. 583	34, 139. 968	TRAVERSE POINT	037	13,977.261 35,842.835	P. O. T. END RDWY."B"		R	OADWAY "G"	115	8, 872. 468	32, 188. 084	P. O. C. INT. B's RAMP "M" & RAMP "O"
9,068.283	34, 714. 069	TRAVERSE POINT				079	9,722.515 33,140.019	1	116	8,914.692	32, 162, 744	P.O.C. INT. 2's RAMP "M" & RDWY "C"
9, 306. 467	34, 646. 499	TRAVERSE POINT		-	DWAY "C"			RDWY. "G"	117	8,970.590	32, 121. 155	P. O. C. INT. & * RAMP "M" & RDWY "B"
7,871.390	35,688.703	TRAVERSE POINT	038	9,501.471 29,992.707	P. O. T. BEGIN RDWY. "C"; BEGIN RDWY. "D" 24' RT.	080	10, 173. 819 33, 568. 56	P.I. CURVE G-1	116	9, 174. 319	32,285.573	PAIR CURVE M-2
7,261,928	35, 023, 359	TRAVERSE POINT	039	9, 243, 878 30, 750, 102	P. O. T. RDWY, "C" NOSE 20" RT.	081	10, 390, 904 33, 571, 150	P. O.C. RDWY."G"; BEGIN RAMP "O" 12' LT.; END RAMP "R"	119	9, 103, 040	31, 964.252	P.O.C. INT. &'. RAMP "M" & RDWY "A"
8, 398. 236	33,981.698	TRAVERSE POINT	040	9, 224. 943 30, 743. 662	NOSE RDWY, "C" & RDWY, "D"			12' RT.	120	9, 114. 796	31,943.187	P.O.C. INT. E's RAMP "M" & RAMP "R"
8,513,438	34, 107. 622	TRAVERSE POINT	041	9,006,642 31,447,643	P. G. CURVE C-1	082	10,784.471 33,688.69	P. T. CURVE G-1 & SHIFTS 12' LT.	121	9, 185. 002	31,671.824	P. T. CURVE M-2 B SHIFTS 14 RT.
9, 132. 298	33, 547, 932	TRAVERSE POINT	042.	8, 338. 433 33, 412, 368	P.I. CURVE C-1	083	10,786.787 33,676.91	•	122	9,200.999	31, 672, 102	
8,558.278	12, 941, 500	TRAVERSE POINT	043	10, 374, 655 33, 812, 925		083		A CASTANAS CANADA CANAD	123	9, 205, 624	31, 406, 420	P. O. T. RAMP "M" P. G. CURVE M-3
6,654.238	32, 484, 566	TRAVERSE POINT	046	12,542.256 34,239.327	P. T. CURVE C-1 P. C. CURVE C-2		10,788.331 33,669.06		124	9,208.251	31, 255, 515	
6,634.236	32, 404. 300	TRATEROE FORT	047			085	11, 375. 504 33, 792. 720		125			P. I. CURVE M-3
	ROA	DWAY "A"	047		P.I. CURVE C-2	086	11, 371. 837 33, 811. 36	NOSE RDWY "G" & RAMP "U"	125	9,246.127	31, 120. 713	P. O. C. RAMP "M" NOSE 19' LT.
9,554.488	30,010.739	P.C. CURVE A-1	048		P. T. CURVE C-2	087	11,751.131 33,866.61	P. O. T. RDWY. "G" & SHIFTS 14' RT. TO088	126	9,249.024	31, 110. 199	P. T. CURVE M-3
9,441.860	30, 341. 898	P.I. CURVE A-1	V-7	13,670.326 35,576.100	P. O. T. END RDWY "C"	088	11,748.429 33,880.354	P.C. CURVE G-2			RAI	MP "N"
9, 347, 648	30,676.723	P. T. CURVE A-1		ROA	DWAY "D"	089	11,941.019 33,918.240	P.I. CURVE G-2	127	9,027.324	31, 167. 486	P.O.T. BEGIN RAMP "N"
9,209.599	31,110.253	P. O. T. RDWY. "A" NOSE 19' LT.	050	9,478.749 29,984.979	P.C. CURVE D-1; BEGIN RDWY. "D"	090	11,940.444 33,954.05	P. O. C. RDWY. "G" NOSE 32' LT.	128	8,814.404	31,652.966	P. O. T. RAMP "N" NOSE 24' LT.
9,227.787	31, 115. 751	NOSE RDWY."A" & RAMP "M"	051	9,350.038 30,363.427	P.I. CURVE D-1	091	11,956.861 33,926.586	NOSE RDWY. "G" & RELOC. MAIN	129	8,794.560	31,698.214	P. C. CURVE N-1
9,181.391	31,203.570	P.C. CURVE A-2	052	9, 206, 298 30, 736, 426	P. T. CURVE D-1	092	12,073.982 34,062.625	P. T. CURVE G-2 END RDWY. "G"	130	8,605.857	32, 128. 476	P.I. CURVE N-1
8,955.809	31,949.832	P.I. CURVE A-2	053	9,206.281 30,736.470	P. O. T. RDWY. "D" NOSE 20" LT.				131	8, 136, 177	32, 116. 347	P. T. CURVE N-1
9, 286, 586	32, 643. 767	P. O. C. RDWY. "A" NOSE 19' LT.	054	8,908.693 31,508.701	P.C. CURVE D-2		_	OADWAY "H"	132	8,063.351	32, 115. 044	P. O. T. RAMP "N" NOSE 18' LT.
9, 303, 782	32,635.665	NOSE ROWY. "A" & RAMP "R"	055	8,855.631 31,668.038	P.O.C. RDWY. "D" NOSE 20' RT.	093	9,264.459 33,358.652	NOSE & P.C. CURVE H-1 BEGIN RDWY. "H"	133	7,563.587	32, 102.670	P. C. CURVE N-2
9,291.246	12, 653, 592	P. T. CURVE A-2	056	8,836.384 31,662.605	NOSE RDWY "D" & RAMP "N"	094	9,670.480 33,810.971	P. I. CURVE H-1	134	7,413.630	32, 098, 957	P.I. CURVE N-2
9,448.297	32,983.090	P.C. CURVE A-3	057	8,765.306 31,880.787	P.I. CURVE D-2	095			135	7,263.714	32, 093, 860	P. T. CURVE N-2 END RAMP "N"
9, 516, 340	33, 274, 838	P.O.C. INT. B's RDWY."A"& RDWY."B"	058	8,791.367 32,278.692	P.C.C. CURVE D-Z & 3; BEGIN		9,916.936 33,821.977	P. O. C. RDWY. "H"; END RAMP "P" 12' LT.; END RAMP "O" 12' RT.			.,	The same state of the same sta
9,509.797	33, 360.223	P.O.C. INT. B's RDWY."A" & RDWY."C"	059	8,816.441 32,661.531	P.I. CURVE D-3	096	10,049,688 33,871.477	P. O. C. RDWY. "H" NOSE 19' RT.				
9,469,823	13,535,360	P.O.C. INT. B's RDWY."A" & RAMP "P"	060	8,969.015 33,013,548	P.T. CURVE D-3	097	10,043.752 33,889.496	NOSE RDWY "H" & RAMP "T"			DEPAR	STATE OF ILLINOIS TMENT OF PUBLIC WORKS & BUILDINGS
9,464,140	33, 549, 676		061	8, 986, 151 33, 053, 085	P. O. T. RDWY "D" NOSE 20" LT.	098	10,266.870 33,928.290	P. T. CURVE H-1; END RAMP "T" 24' RT.				DIVISION OF HIGHWAYS
		P.O.C. INT. B . RDWY "A" & RDWY. "H"		-, . 30. 131 33, 053. 065	T. S. I. ADWI D ROLL EV DI.	099	10, 376. 109 33, 949. 780	P.O.T. RDWY. "H" B SHIFTS 12' RT.				LIST OF COORDINATE POINTS
9,458.229	33,563.668	P.O.C. INT. B's RDWY."A" & RAMP "Q"					23,747.100	TO 100				AND DESCRIPTIONS
			1									H W LOCHNER INC.
												H. W. LOCHNER, INC. ENGINEERS CHICAGO, ILL

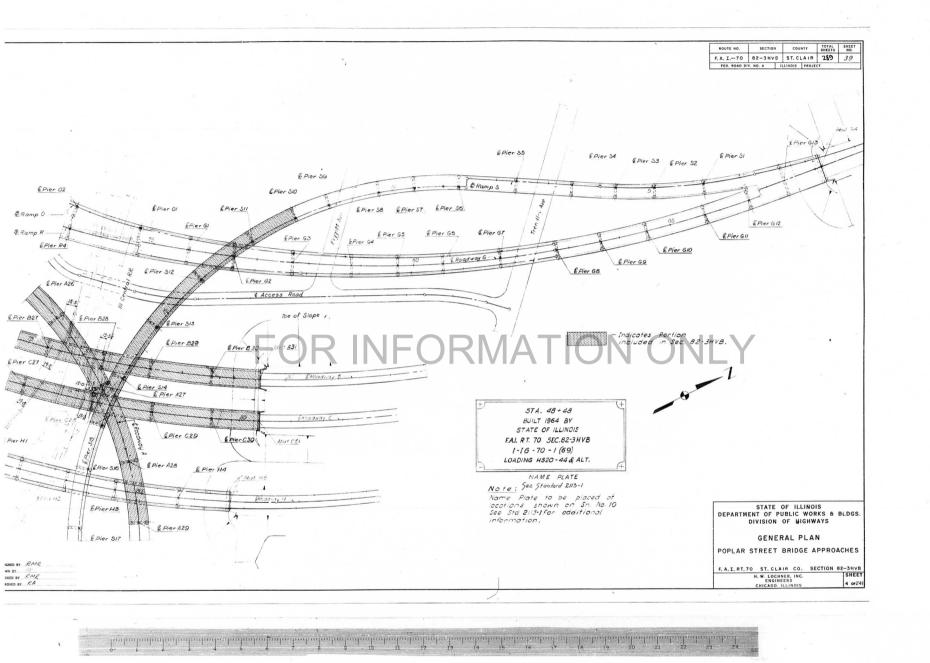
FEDERAL-AID ROUTE No.	SECTION	COUNTY	SHEETS	SHEE!
F.A.I. 70	82-3HVB	ST. CLAIR	289	35

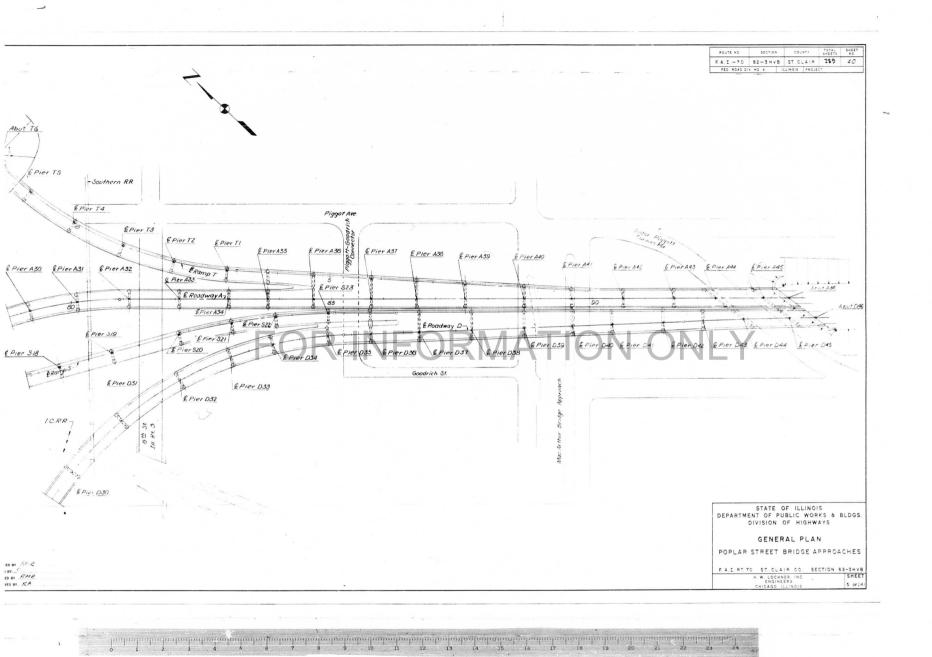
												1			
NT NO	COORDINATE NORTH EAST		DESCRIPTION	POINT COORDINATE CODE NO RTH EAST DESCRIPTION POINT COOR NO RTH EAST DESCRIPTION					FED. ROAD	ROAD DIV. No. 4 IfLINGIS PROJECT					
		RAN	(P 0			RAMP "R"			RAMP U		<u>-U</u> -				1
	10, 395, 424 33, 560		P.C. CURVE 0-1 BEGIN RAMP "O"	180	9,717.006	33, 145. 821	P. T. CURVE R-2 NOSE 8' LT. &	222	11,366.401	33, 829. 574	P.C. CURVE U-2	POINT CODE NO	COO NORTH	RDINATE EAST	DESCRIPTION
	10.022.872 33,408		P.I. CURVE O-1				SHIFTS 16' RT. TO 181	223	11,222,450	33,787.077	P. I. CURVE U-2			TRENDLE	Y ACCESS ROAD
	9,739.548 33,121	. 112	P.C.C. CURVE O-1 & 2 NOSE 24' LT.	181	9,705.989	33, 157, 423	P.C. CURVE R-3	224	11,075.179	33,758.107	P. T. CURVE U-2 END RAMP "U"	267	9,754.363	33, 289. 097	P.C. CURVE T.A 2
	9, 632, 592 33, 015	. 360	P.I. CURVE O-2	182	9,820.889	33, 266. 529	P.I. CURVE R-3				MP V	268	9,703.759	33, 259. 329	P.I. CURVE T.A2
	9,570.645 32,876	. 749	P. T. CURVE O-2	183	9,953.082	33, 353. 884	P. C. C. CURVE R-3 & 4 P. I. CURVE R-4	225	10,442.781	33,950.665	P. G. CURVE V-1 BEGIN RAMP "V"	269	9,663.844	33, 216. 275	P. T. CURVE T. A2
	9,442.932 32,59	0.979	P.O.T. RAMP 'O' & SHIFTS 16' LT.	184	10, 158. 406	33, 489. 564		226	10, 590, 116	33, 979. 648	P. L. CURVE V-1	270	9,589,223	33, 135. 785	P.C. CURVE T.A3
	9,428.325 32,59	. 507	P.C. CURVE O-3	185	10, 386. 383	33, 582. 266	P. T. CURVE R-4 END RAMP "R"	227	10,719,774	11.991.898		271	9,511.381	33, 051. 821	P.I. CURVE T.A3
1	9, 186.777 32, 306	. 954	P. O. C. INT. L' RAMP "O" & RAMP "R"			RA	MP "S"	228	11, 291, 888	34, 037, 091	P. T. CURVE V-1 NOSE 21' RT.	272	9,608.266	32,990.809	P.R.C. CURVE T.A3
	9,158.717 32,28		P.O.C. INT. & RAMP "O' RDWY. "A"	186	11,085.817	33, 723. 510	P.C. CURVE S-1 BEGIN RAMP "5"	229	11,290.582	34, 053, 037	P. O. T. & SHIFTS 16' RT. TO 229 P. C. CURVE V-2				
	9,251.777 32,202		P.I. CURVE O-3	187	10, 938. 369	33, 694. 504	P.I. CURVE S-1	231	11,599.428	14,078.318	P. L. CURVE V-2				TREET ACCESS ROAD
	8,980.104 32,200		P. O. C. INT. 2 . RAMP "O" & RDWY "B"	188	10,796.025	33, 646. 333	P. C. C. CURVE S-1 & 2 NOSE 24' LT.	232	11,903.479	34, 138, 129	P. T. CURVE V-2 END RAMP "V"	273	11,945.082	34, 434. 874	M INTS. OF 4TH ST. & 4TH TO 5TH ACCESS ROAD
	8, 917. 304 32, 194		P. O. C. INT. E's RAMP "O" & RDWY "C"	189	10,652.983	33, 597. 925	P.I. CURVE S-2		11,742.4.7	74,174,147	THE STATE OF THE PARTY T	274	11,712.879	34, 648. 240	P.C. 4TH TO 5TH ACCESS ROAD
	8,819.484 32,18		P. T. CURVE O-1	190	10,529.104	33, 511. 562	P. T. CURVE S-2			RELOCATE	D MAIN STREET	275	11,676.088	34,682.046	P.1. 4TH TO 5TH ACCESS ROAD
	8,787.628 32,18		P.O.T. INT. & RAMP "O' & RDWY."D" P.O.T. RAMP "O'NOSE 18' RT.	191	10, 319, 101	33, 365. 157	P.O.T & SHIFTS 16' LT. TO 192	233	12,677.994	34,689.002	P. O. T. BEGIN RELOC. MAIN & TRAVERSE POINT 12-A	276	11,642.256	34, 645. 280	P. T. 4TH TO 5TH ACCESS ROAD
	8,062.128 32,15		P. C. CURVE O-4	192	10, 309. 951	33, 378. 283	P.C. CURVE S- 3	234	11,967,160	33.917.102	P. O. T. MAIN ST. NOSE 14' LT.				
	7,562,677 32,12		P.C. CURVE 0-4	193	9,709.987	32, 960. 015	P.I. CURVE S-3	235	11,898.009	33,842.010	P. O. T. & SHIFTS 5' RT. TO 236			RELOCAT	TED 2ND STREET
	7,412.815 12,12		P. I. CURVE O-4 END RAMP "O"	194	9,881.823	33,253.063	P.O.C. INT. B's RAMP"S" & RAMP "O"	236	11,901.687	33, 838. 623	P. C. CURVE R.M1	278	13,736.915	34, 914. 939	& INTS. OF MISSOURI & RELOC. 2ND
+	7,262.899 32,11	7.045	7.1. 00212 0-1210 11111	195	9,853.629	33,254.754	P.O.C. INT. B's RAMP "S" & RDWY "G"	237	11,858.594	33, 791. 829	P.I. CURVE R.M1	279	13,671.814	34, 806. 155	P. C1 RELOCATED 2ND STREET
		RAM	P P	196	9,821.463	33, 258. 085	P.O.C. INT. B's RAMP "S" & RAMP "R"	238	11,800.219	33,766.550	P. T. CURVE R.M1	280	13,639.767	34,752.604	P. I1 RELOCATED 2ND STREET
	7,558.702 32,24	0.590	P.C. CURVE P-1 BEGIN RAMP "P"	197	9,580.943	33, 334, 475	P.O.C. INT. &'s RAMP "S" & RDWY "B"	239	11,627.416	13,691.720	P. C. CURYE R. M2	281	13,585.693	34,721.417	P. T1 RELOCATED 2ND STREET
	7,758.061 32,25	2.608	P. I. CURVE P-1	198	9,510.142	33, 377. 694	P. O. C. INT. & . RAMP "S" & RDWY "A"	240	11,569.090	33,666.463	P. I. CURVE R. M2	282	13,531.753	34, 190. 356	P. C2 RELOCATED 2ND STREET
	7,957.140 32,26	8.612	P. T. CURVE P-1	199	9, 508. 367	33, 378. 932	P. D.C. INT. B' RAMP "S" & RDWY "C"	241	11,526.018	13, 619, 722	P. T. CURYE R. M2	283	13,461.896	34,650.117	P. I2 RELOCATED 2ND STREET
	8,355.830 32,30	0.663	P. O. T. RAMP 'P' NOSE 24' LT.	200	9, 399. 660	33, 472. 994	P.O.C. INT. & RAMP "S" & RAMP "P"					284	13,420.503	34, 580. 958	P. T2 RELOCATED 2ND STREET
	8,388.180 32,30	3.263	P.C. CURVE P-2	201	9, 389. 047	33,484.537	P.O.C. INT. B'S RAMP "S" & RDWY. "H"				AVENUE EXTENSION				
1	8,836.115 12,33	9.273	P.I. CURVE P-2	202	9, 378, 699	33, 496, 311	P.O.C. INT. 2's RAMP "S" & RAMP "Q"	243	12, 572, 157	34, 785, 931	P. O. T. BEGIN GOLLINSVILLE EXT.				INOIS TERMINAL R.R. TRESTLE
	8, 816. 372 32, 49	5.573	P.O.C. INT. & RAMP "P"-L-RDWY. "D"	203	9, 318. 407	33, 577, 728	P. T. CURVE S-3	245	12,428.411	34,469.657	P. C. CURVE CE-1	285	9,016.923	31, 191. 202	
	8,834.512 32,51	3.601	P. O. C. INT. & RAMP "P" & RAMP "Q"	204	9, 159, 822	33, 827, 894	P. C. CURVE S-4	246	12,419.544	34,451.756	P. O. C. COLLINSVILLE EXT.	286	9,027.971	31, 199. 179	ILL. TERM. R.R. & RDWY. "D"
	8,989.851 32,76	1.518	P. T. CURVE P-2 % SHIFTS 16' LT.	205	9,079.032	33, 955, 339	P.I. CURVE S-4	247	12.436.280	34, 442, 761	NOSE COLLINSVILLE EXT. & MAIN ST.	287	9,078.690	31, 235. 803	ILL. TERM. R.R. & RDW" "C"
	9,004.885 32,75	6.064	P. O. T. RAMP 'P'	206	8,967.855	34, 057. 364	P. T. CURVE S-4	248	12,444,372	34, 435, 309	P. O. T. MAIN ST. NOSE II' LT.	289	9,105.826	31, 255. 397	ILL. TERM. R.R. & RDWY "B"
			P. C. CURVE P-3	207	8,879.484	34, 138, 460	P. O. T. RAMP "S" NOSE 19' RT.	249	12,408,528	34, 425, 911	P.I. CURVE CE-1		9, 156. 793	31,292.200	ILL. TERM. R.R. & RDWY "A"
	9,126.399 33,08		P.I. CURVE P-3	208	8, 326. 991	34,645.472	P. O. T. END RAMP "S"	250	12, 375, 977	34, 190, 561	P. T. CURVE CE-1 END COLL. AVE. EXT.	290	9,209.435	31, 330. 213	ILL. TERM. R.R. & RAMP "M"
	9,178.316 33,23 9,278.028 33,34		P.C.C. CURVE P-344 NOSE 18' RT.			BAN	P "T"		16, 313. 77.	74, 774, 747	P. I. COXTE CET END COME. ATM. DATE			INTERSECT	ONS OF CROSS ROADS
	9,545,581 33,65		P. J. CURVE 4							RELOCAT	ED 4TH STREET	291	12,931.515	34, 456. 354	C. BRDWY AVE & 3RD ST.
	9,921,551 33,81		P. T. CURVE 4, END RAMP "P"	209	8,633.827	34, 418, 185	P.O.T. BEGIN RAMP "T"	252	12, 194. 655	34,948.914	P.C. CURYE R4-1	292	12,983.317	34, 408, 835	C. BRDWY AVE & RDWY "C"
4				210	9,045.699	34, 083. 591	P.O.T. RAMP "T" NOSE 24" LT.	253	12, 140. 200	34,890.000	P.I. CURVE R4-1	293	13,034.241	34, 362. 120	C. BRDWY AVE & RDWY "B"
		RA	MP C	211	9, 158. 809	33,991.704	P.C. CURVE T-1	254	12, 123. 189	34,812.055	P. T. CURVE R4-1	294	13,555.127	35, 081. 862	C. MISSOURI AVE & RDWY "C"
	8,803.341 32,27	7.908	P.C. CURVE Q-1; BEGIN RAMP "Q"	212	9,413.422	33, 784. 864	P.I. CURVE T-1	255	12,094.941	34, 686. 315	P.C. CURVE R4-2	295	13,653.137	34, 991. 866	C. MISSOURI AVE & RDWY "B"
	8,844.037 12,89	9.272	P.I. CURVE Q-1	213	9,735.293	33, 848. 181	P. T. CURVE T-1	256	12,077.321	34,607.885	P. I. CURVE R4-2			MISCELLA	NEOUS POINTS
	9,025.469 13,03	3.488	P. O. C. RAMP "Q" NOSE 24' RT.	214	10,040.085	33,908.138	P.O.T. RAMP "T" NOSE 19" LT.	257	12,022.847	34, 548, 773	P. T. CURVE R4-2 & SHIFTS 20' RT TO 258	296	9,507.993	30, 187. 240	END RAMP "M"
	*,257.774 33,36	2.660	F.T. CURVE Q-1 NOSE 6' LT., & SHIFTS 12' RT. TO 173	215	10, 262. 237	53, 951. 839	F. V. I. ERU RAMP I	258	12,037.554	34, 535, 220	P.O.T. & 4TH STREET	297	9,496.506	30, 183.768	P.O.C. RDWY "A", END RAMP
	9,251,064 31,37	0.676	P. C. CURVE Q-2			RA	MP "U"	259	11, 848.623	34, 330. 202	P.O.T. & SHIFTS 5' RT. TO 260				"M" 12' LT.
		3.910	P.I. CURVE O-2	216	12,522.030	34, 139. 547	P.C. CURVE U-1 BEGIN RAMP "U"	260	11, 852.300	34, 326. 814	P.O.T. & 4TH STREET	298	9,038.521	31, 171. 801	P. O. T. RDWY. "D" BEGIN RAMP "N" 12' RT.
		1.050	P. T. CURVE Q-2 END RAMP "Q"	217	12, 374. 759	34, 110, 576	P.I. CURVE U-1	261	11,763.528	34,230.483	P.O.T. 2 4TH STREET NOSE 16' LT.	299	9,096.256	31,721.224	P.O.C. RDWY. "A" BEGIN RAMP "R"
4	13.63			218	12,230.807	34,068.079	P. T. CURVE U-1								12' LT.
		. RAM	PR	219	12,096.466	34,028.419	P.O.T. RAMP "U" NOSE 24' LT.				Y ACCESS ROAD	300	9, 320. 517	32, 626. 669	P.O.C. RAMP "R" NOSE 19' RT.
	9,108.250 31,72	1.614	F.C. CURVE R-1 BEGIN RAMP "R"	220			P. O. T. & SHIFTS 16' LT. TO 1220	263	10,257.494	33,620.551	P. O. T. BEOLN TRENDLEY ACCESS ROAD			050	STATE OF ILLINOIS ARTMENT OF PUBLIC WORKS & BUIL
	4,0-2 110 32,20	2.669	P.I. CURVE R-1	1220			F. O. T. RAMP "U"	264	10, 226, 724	33, 587. 090	P.G. GURVE T.A1			DEP	DIVISION OF HIGHWAYS
	4, 120 444 32,62	6.624	F.C.C. CURVE R-1 & 2	221	11, 366. 457	33, 829. 591	P.O.T. RAMP "U" NOSE 19' RT.	265	10, 186. 422	33,543.261	P.L CURVE T.AI				LIST OF COORDINATE POINT
	3,4** 112 12,91	+.022	F. I. CURVE R-2					266	10,135.100	33,513.070	P. T. CURVE T.A1				AND DESCRIPTIONS
-									1,2,			-	·	-	H. W. LOCHNER, INC. ENGINEERS CHICAGO, ILL
															CHICAGO. ILL

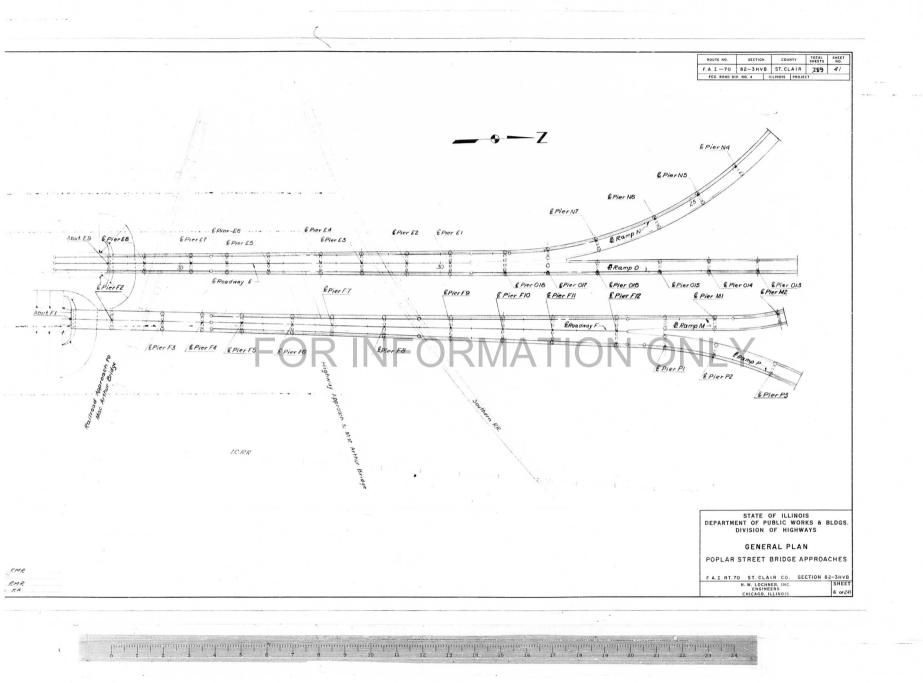


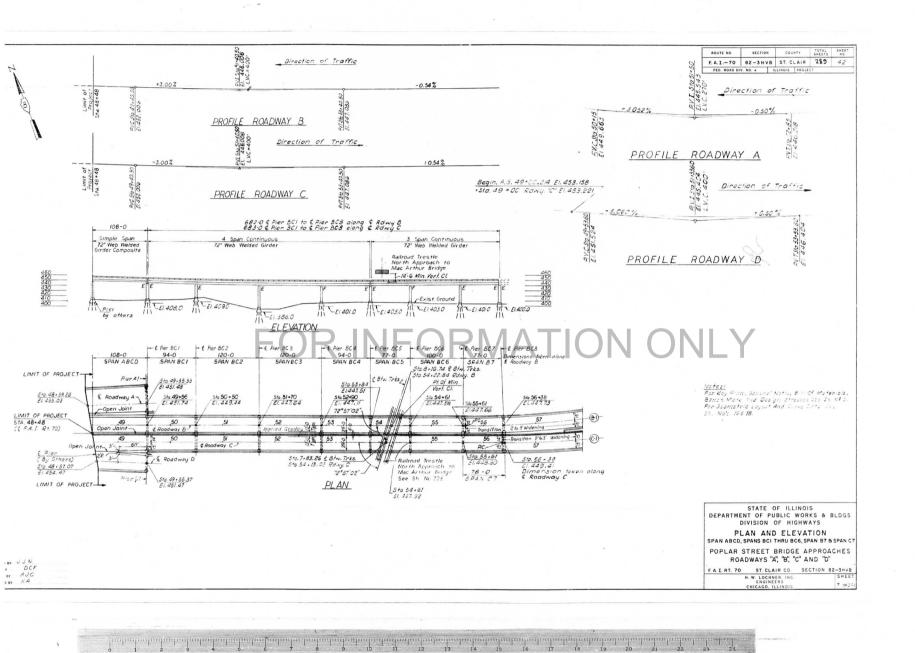


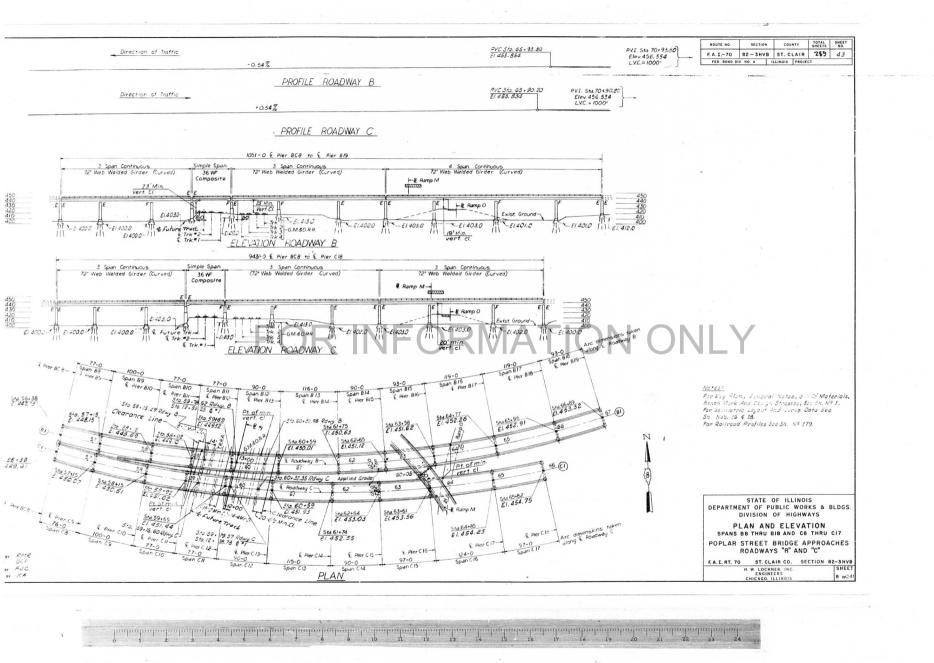


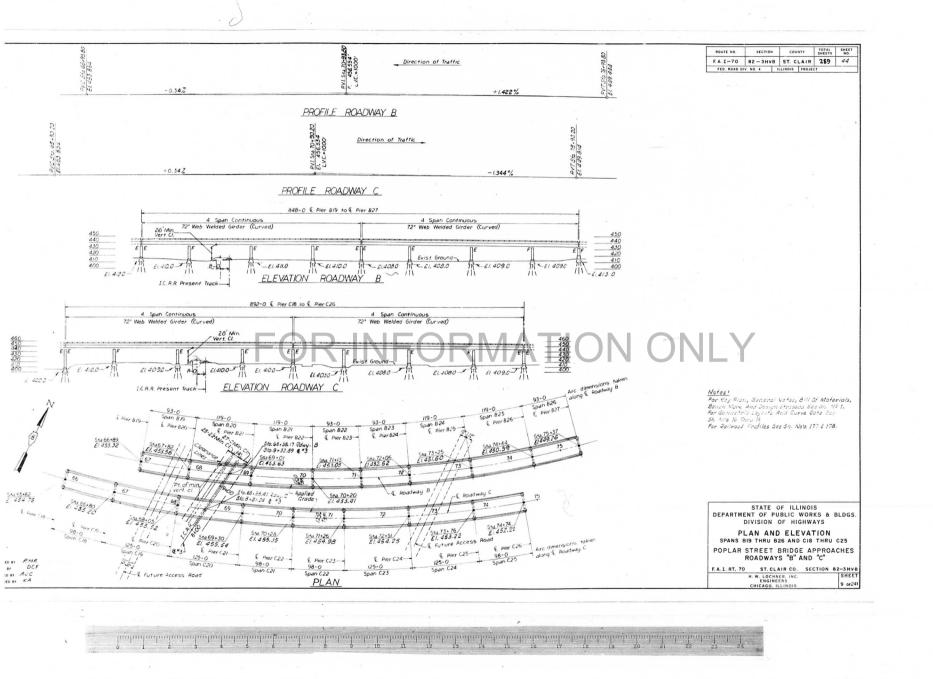


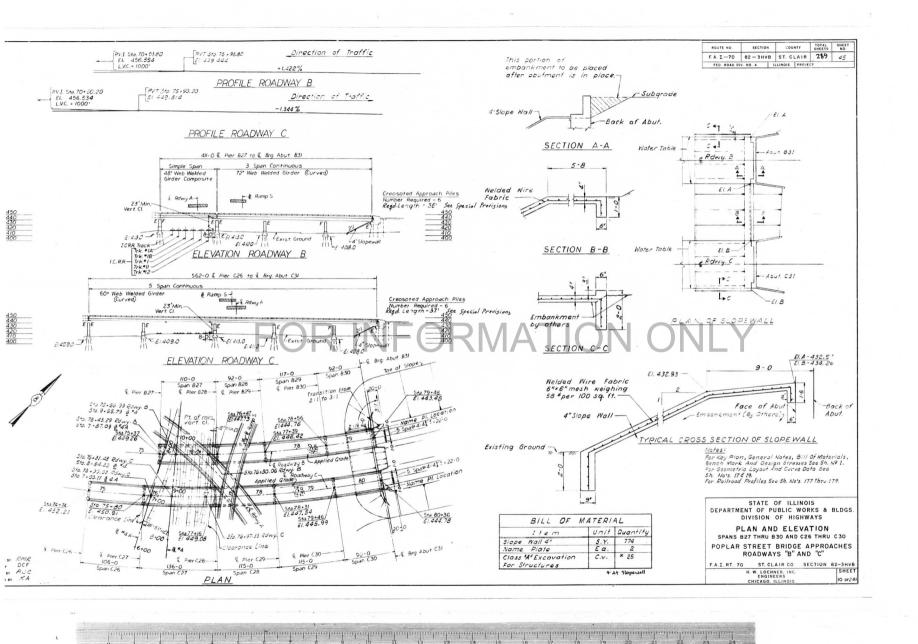


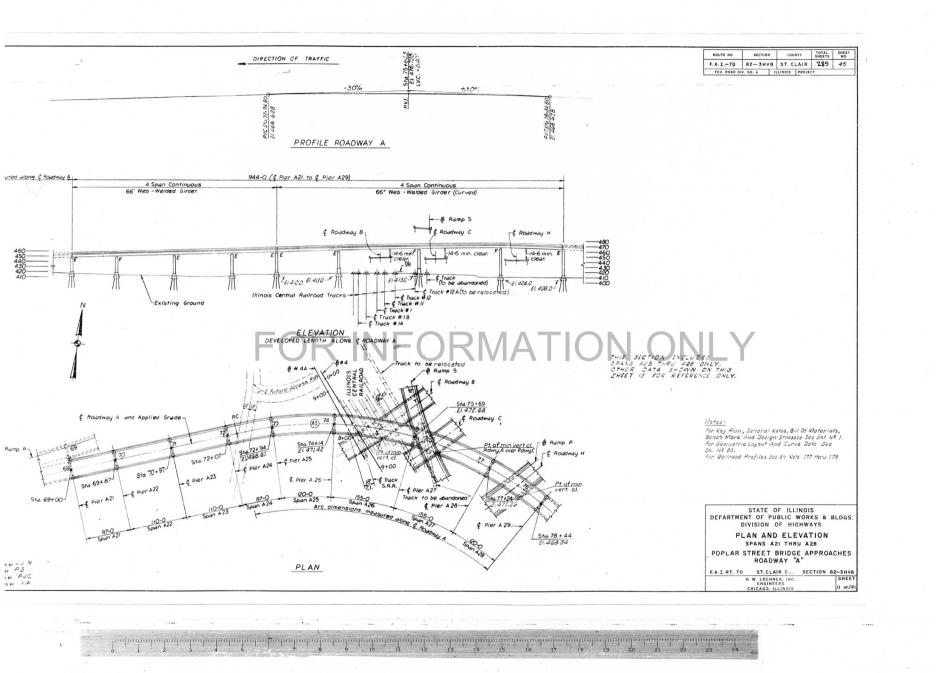


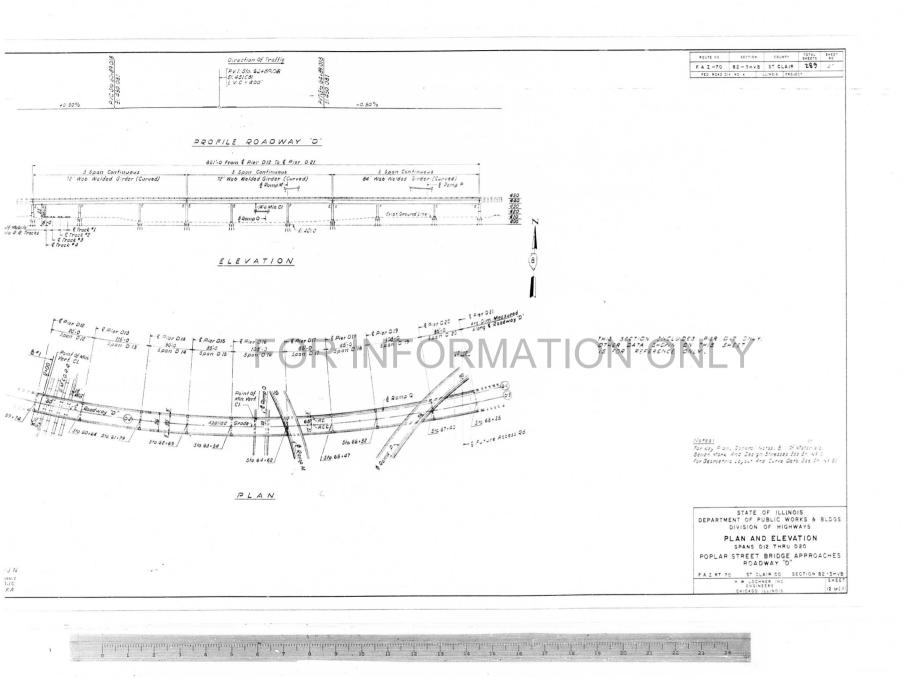


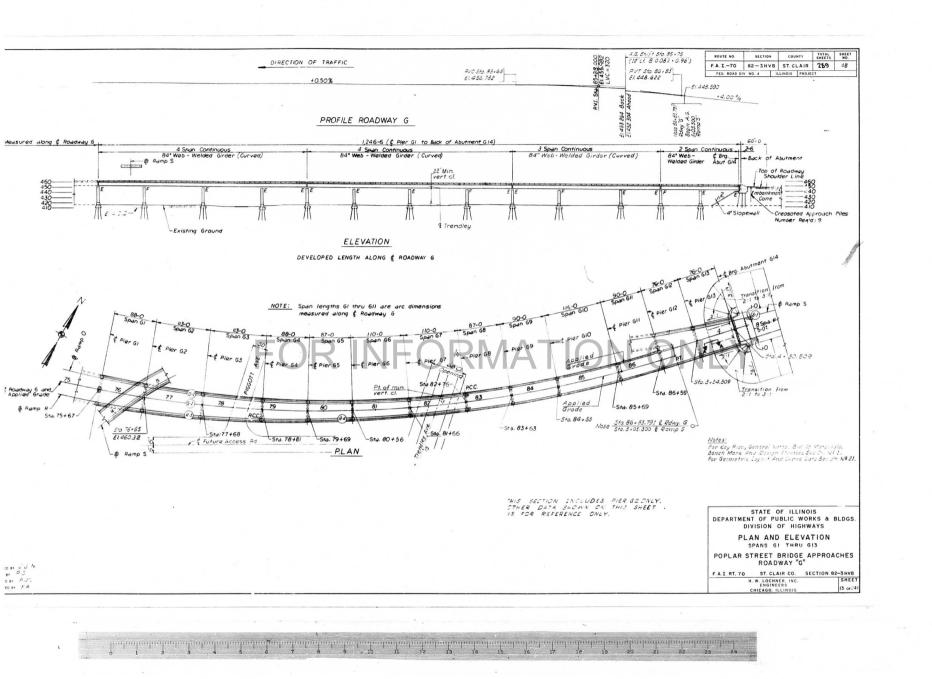










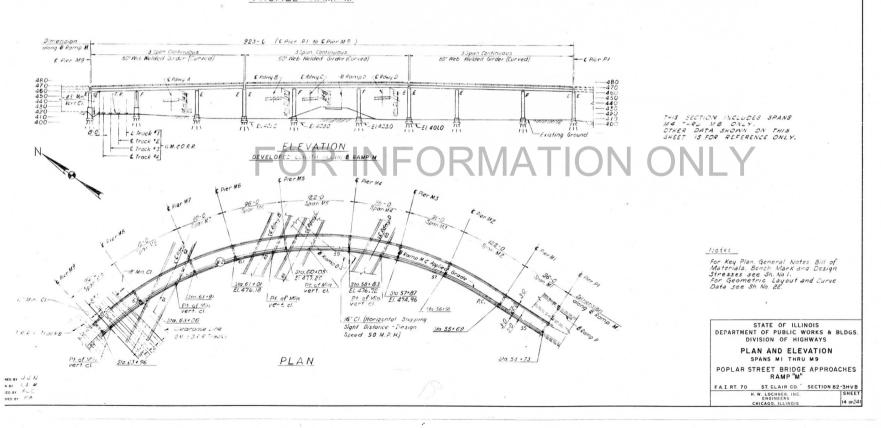


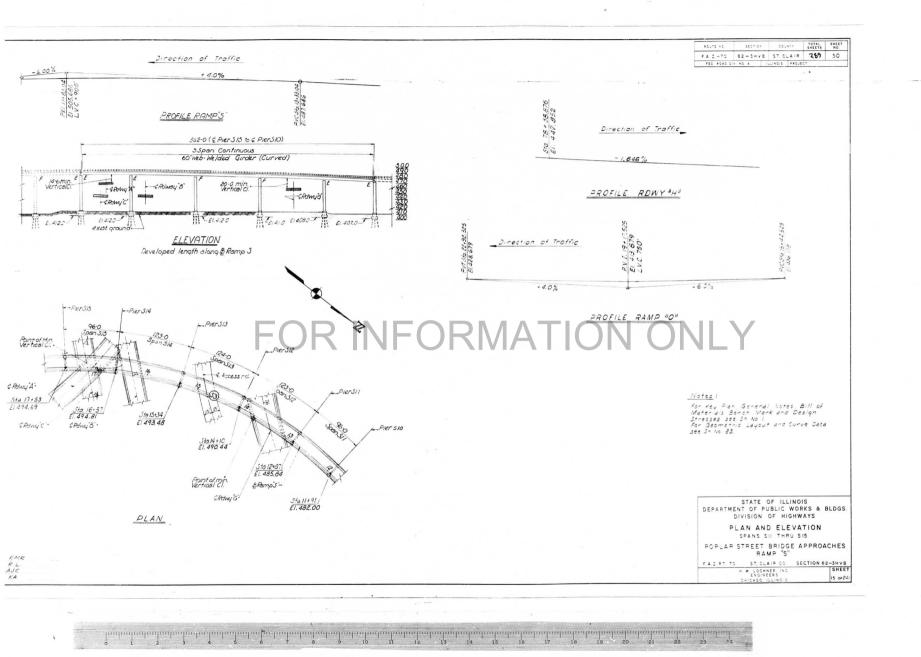
					ROUTE NO.	SECTION	COUNTY	TOTAL	SHEET NO.
w.)	Direction of Traffic				F. A. I70	82-3HVB	ST. CLAIR	289	49
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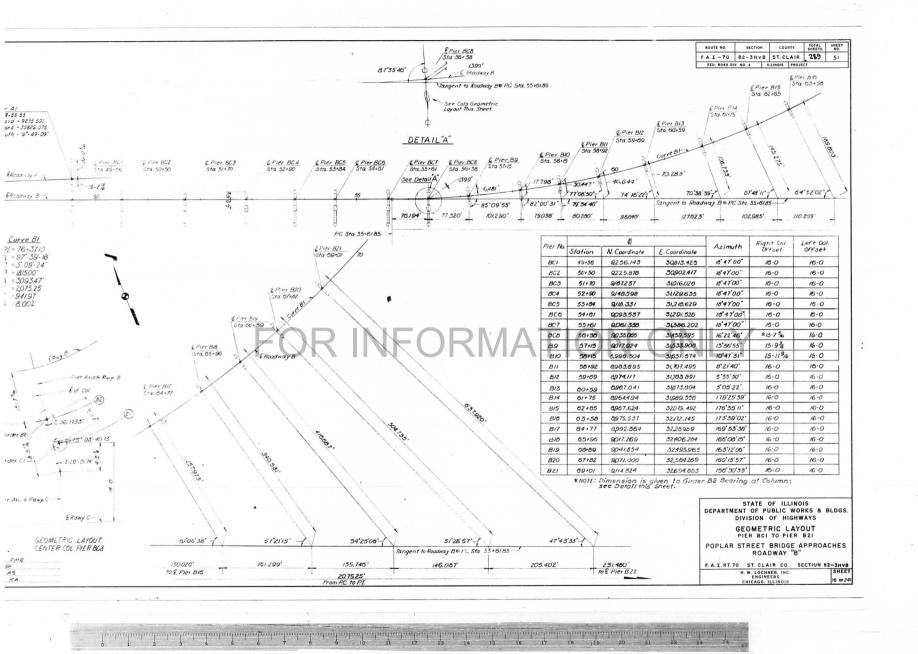
## PROFILE RAMP M

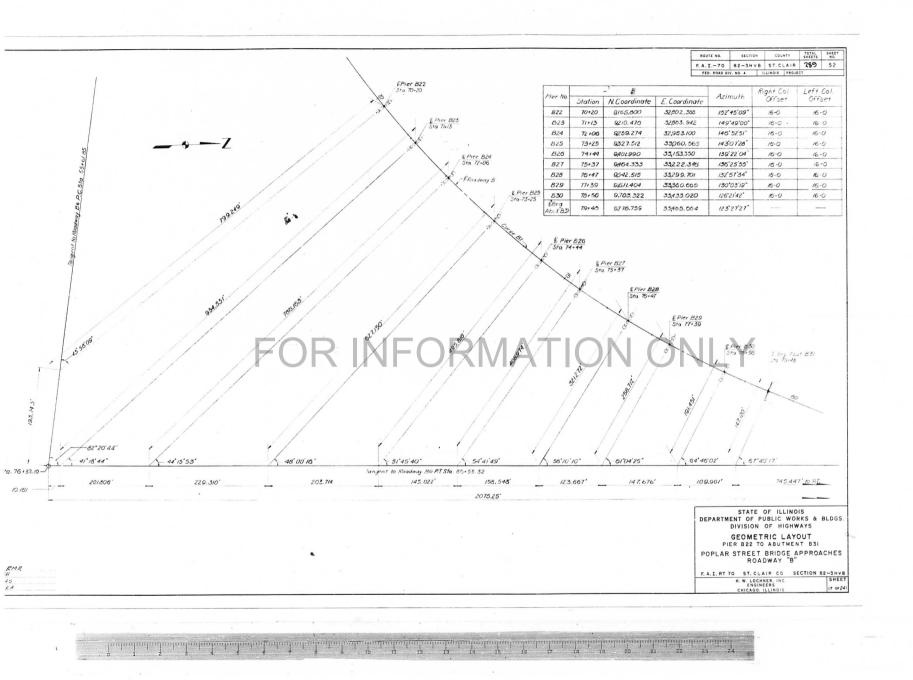
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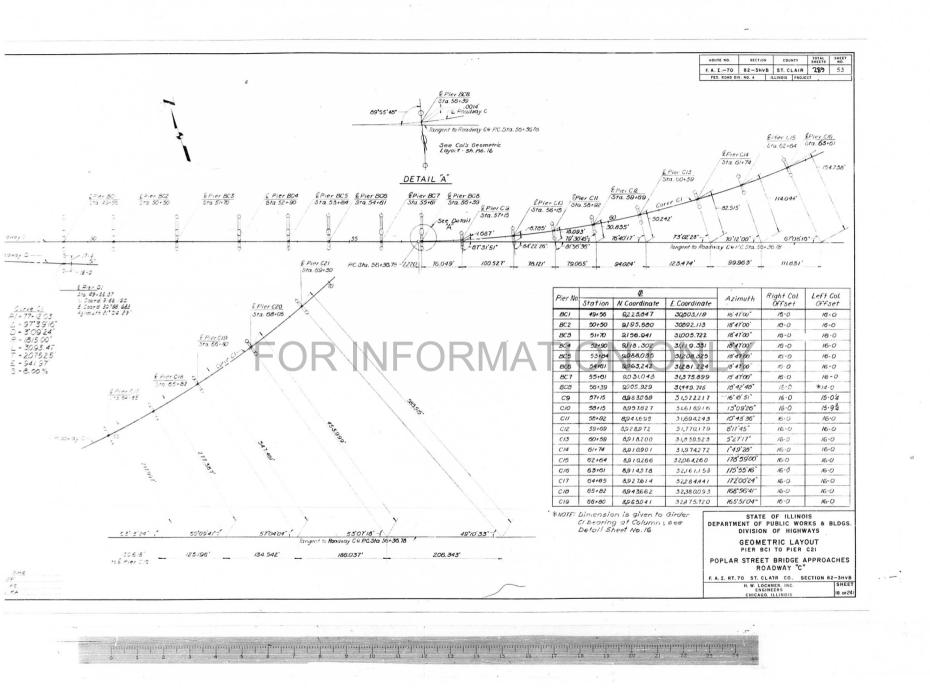
277 510, 63-50.165 El. 467. 839

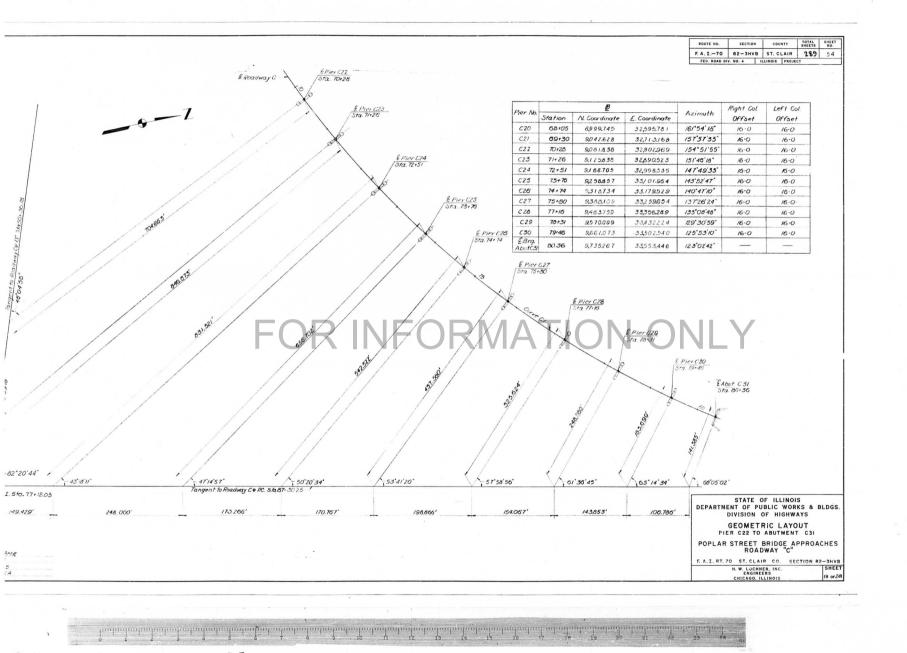


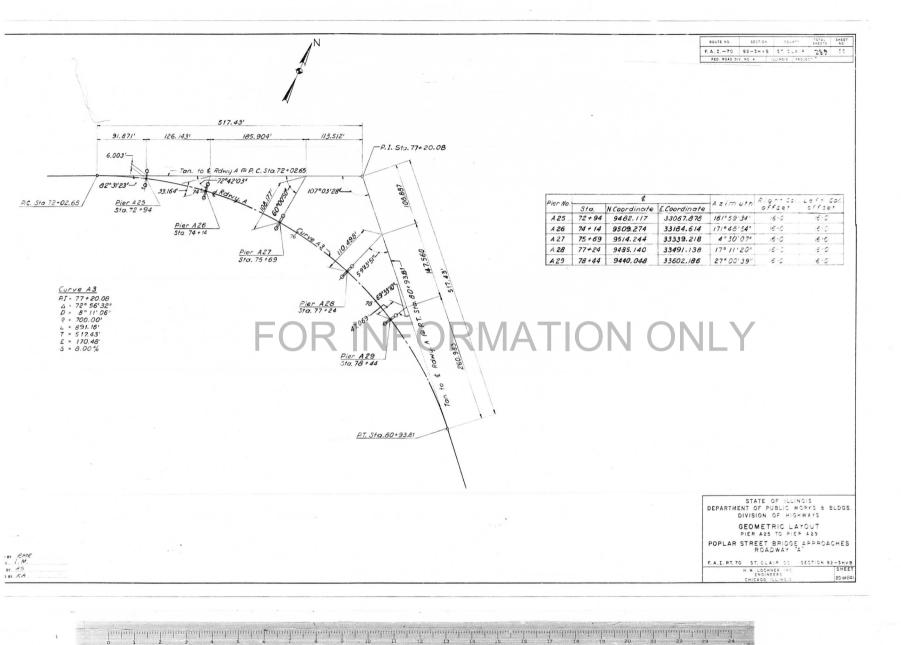


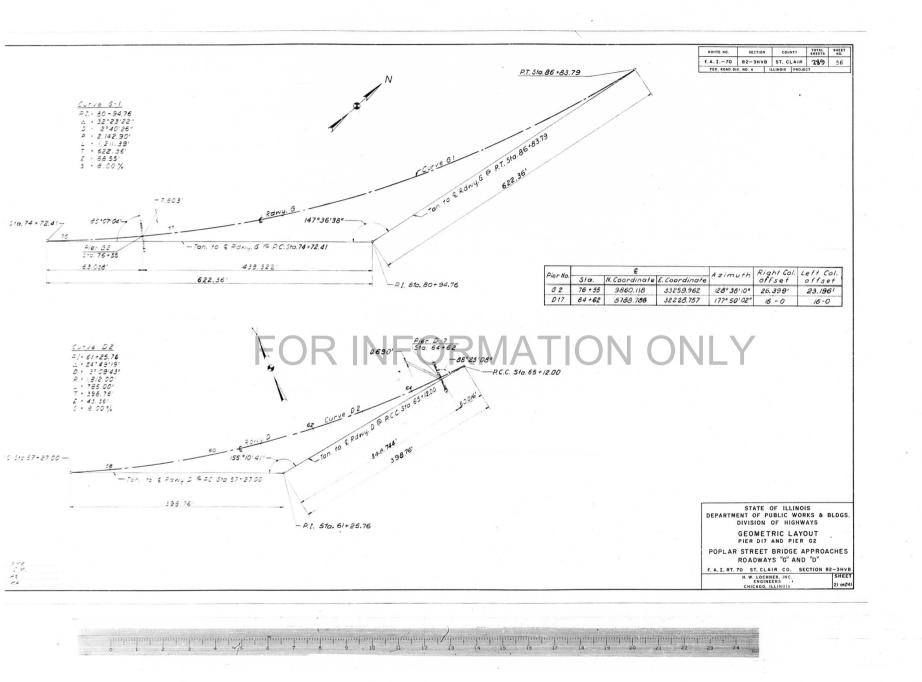


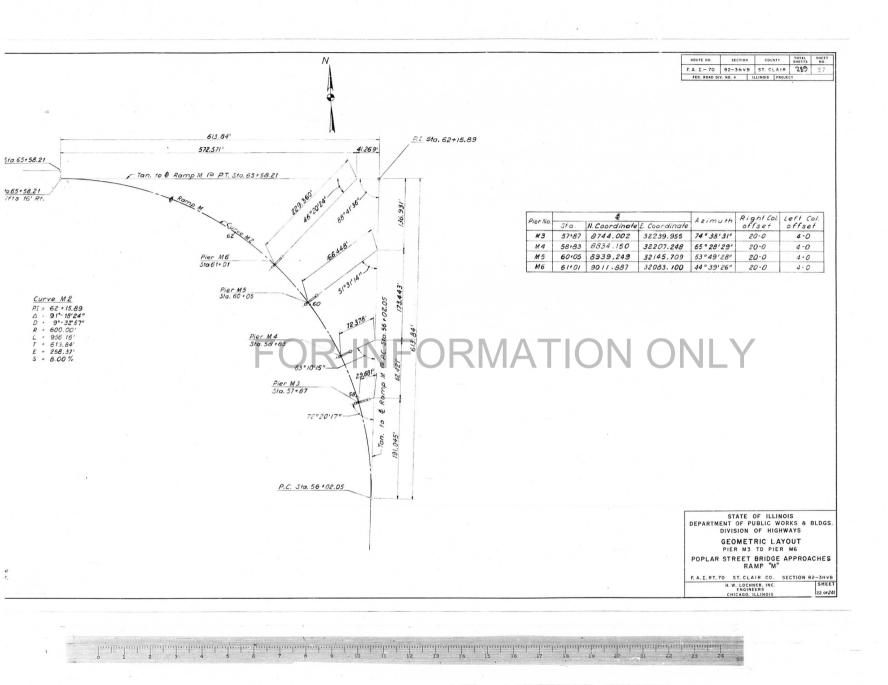


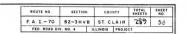


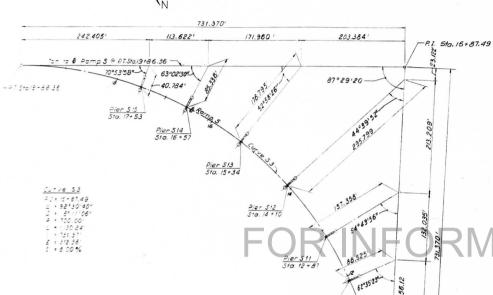












BH AMA H 1 W SH AS BH KA Pier 510 Sta. 11+91

P.C. Sta. 8 + 56.12 -

Pier No.		. Æ		Azimuth	Right Col.	Left Col.	
	Sta.	N. Coordinate	E. Coordinate	AZIMUTA	offset		
510	11+91	1.0000.657	33258.456	97°28'20"	20-0	4-0	
511	12+87	9904. 916	33252.527	89°36'53"	20.0	4-0	
512	14+10	9782.623	33264./28	79°32'49"	20-0	4-0	
513	15 + 34	9663.305	33297.281	69°23'51"	20-0	4-0	
5 /4	16 + 57	9552.556	33350.429	59° 19' 47"	20-0	4-0	
5 /5	17+53	9473.596	33404.898	51°28'19"	20-0	4-0	

RMATION ONLY

STATE OF ILLINOIS
DEPARTMENT OF PUBLIC WORKS & BLDGS.
DIVISION OF HIGHWAYS

GEOMETRIC LAYOUT PIER SIO TO PIER SIS

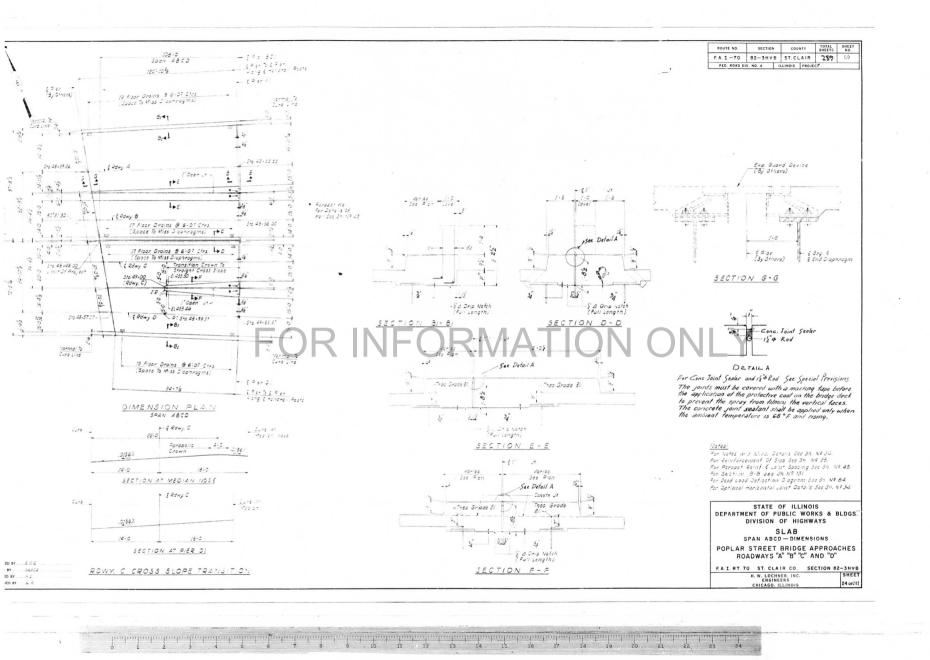
POPLAR STREET BRIDGE APPROACHES RAMP "S"

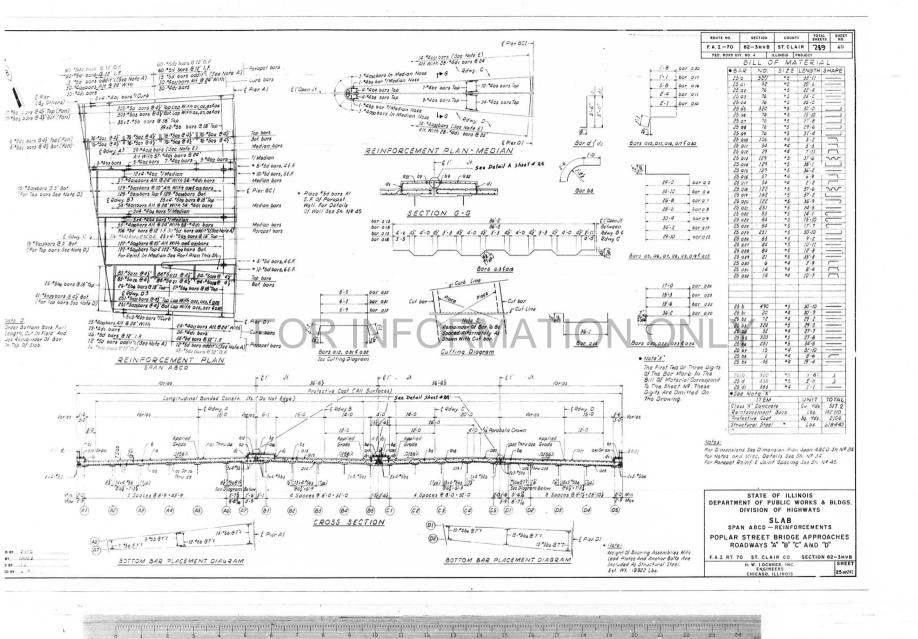
F. A. I. RT. 70 ST. CLAIR CO. SECTION 82-3HVB
H. W. LOCHNER. INC.
ENGINEERS
CHICAGO. ILLINOIS 23-0F241

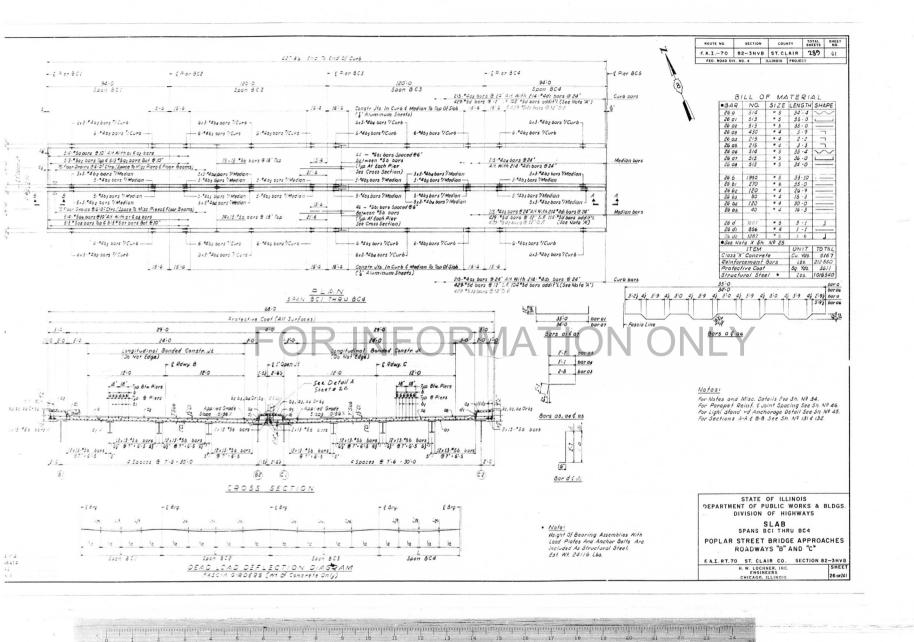
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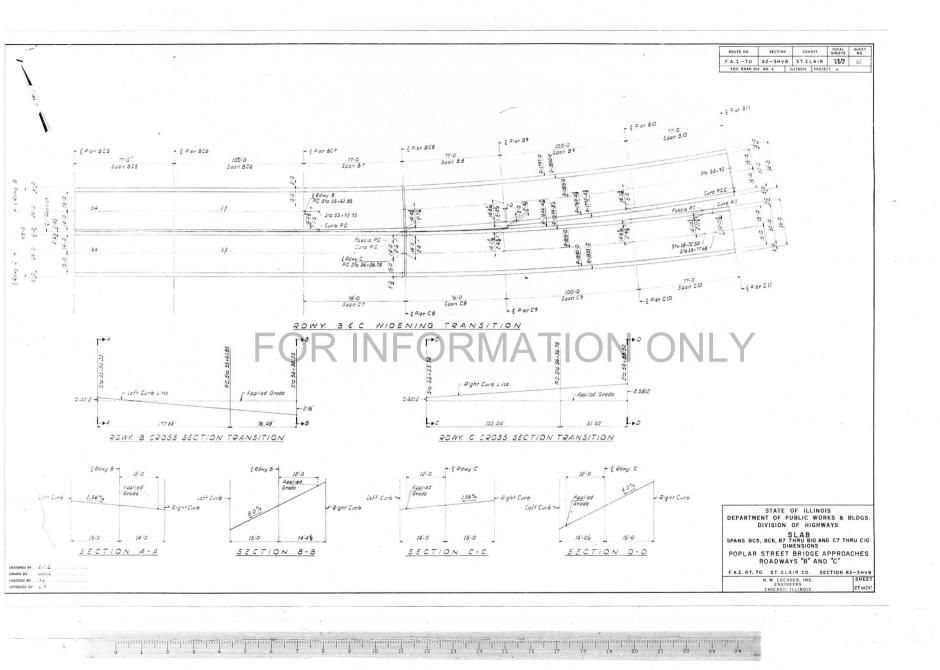
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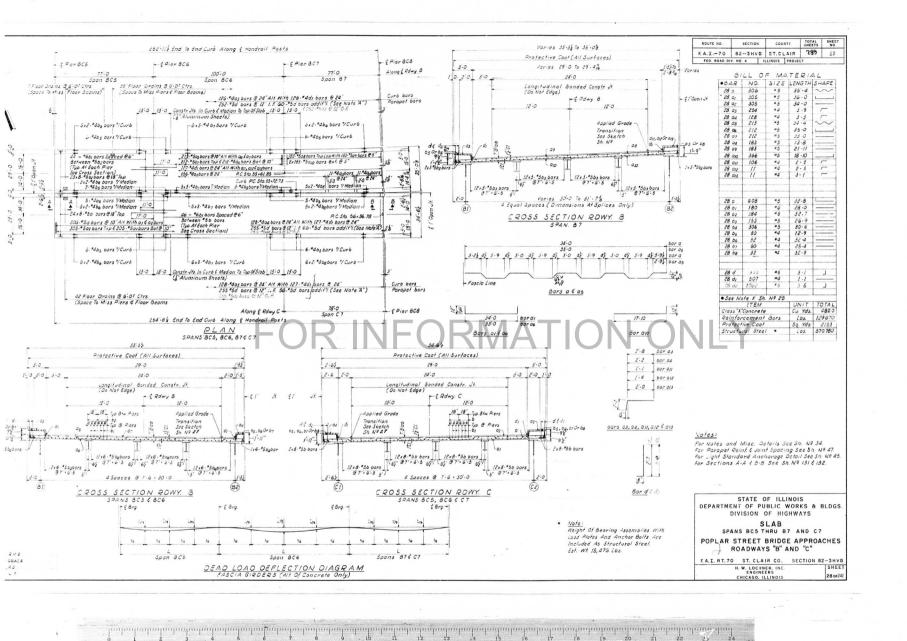
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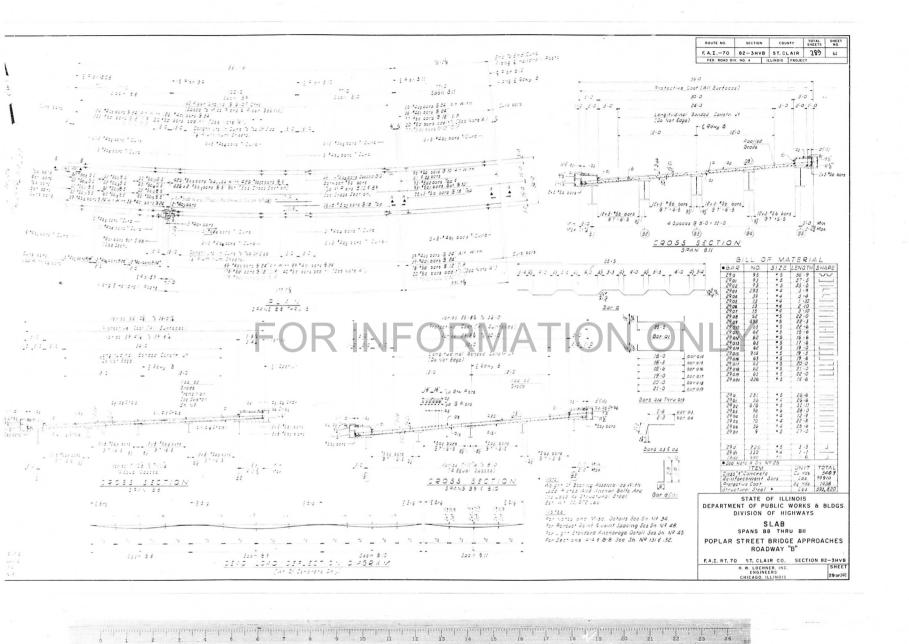


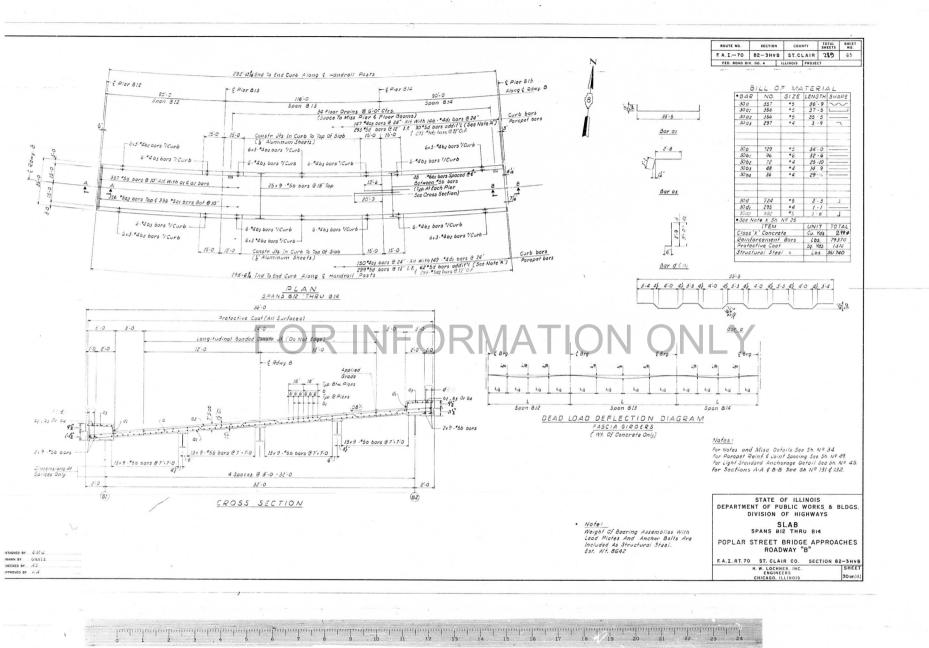


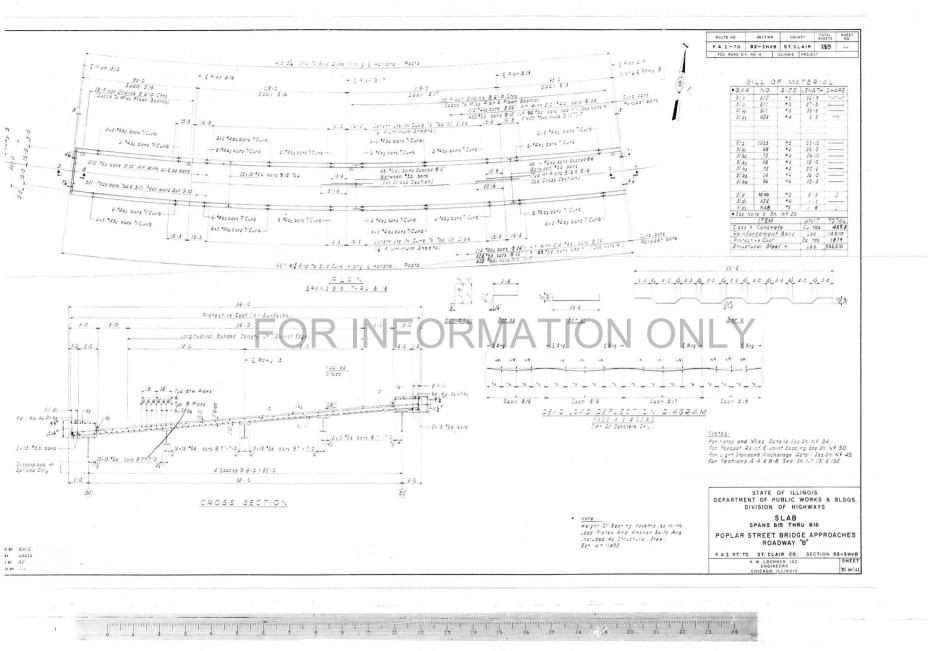


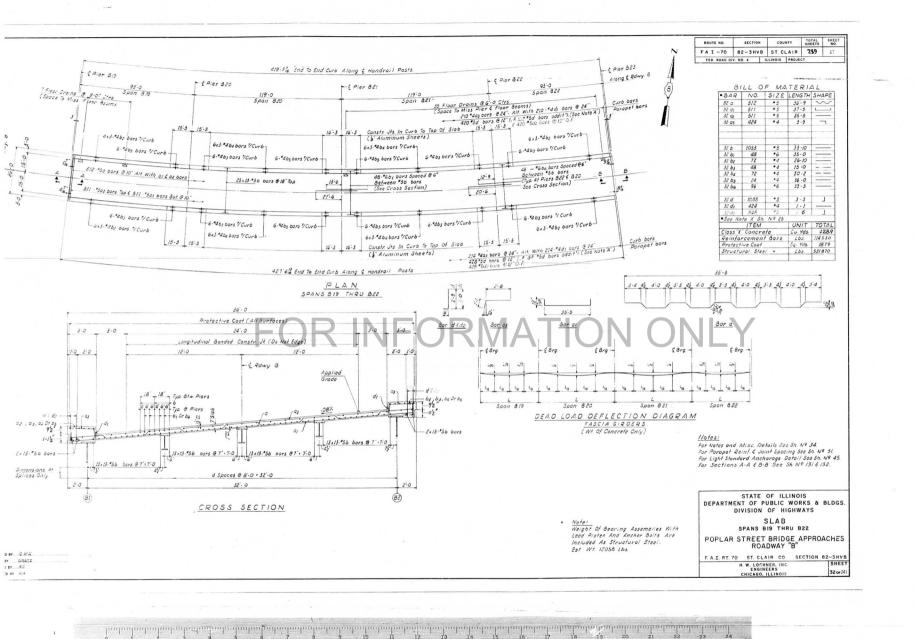


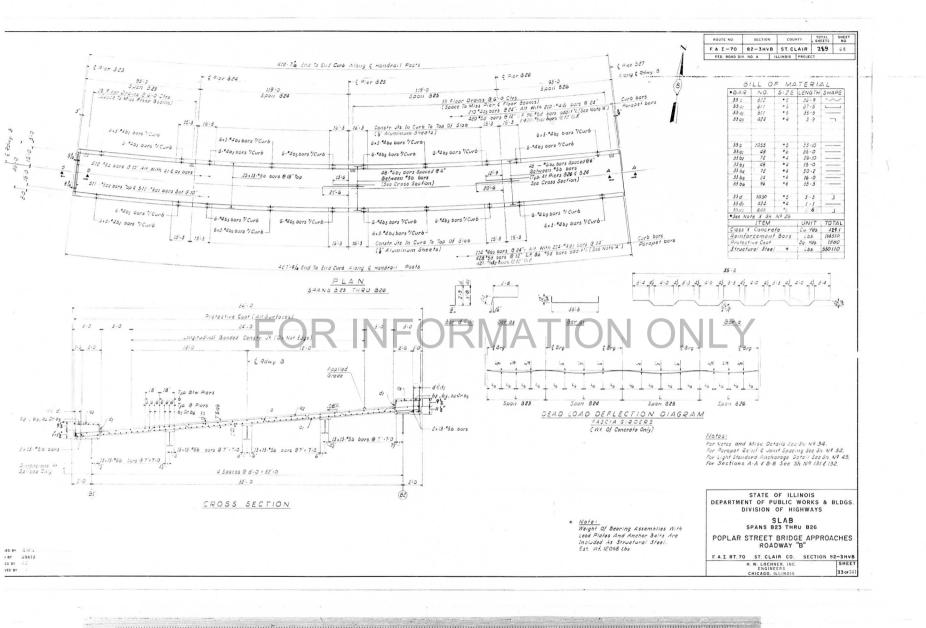


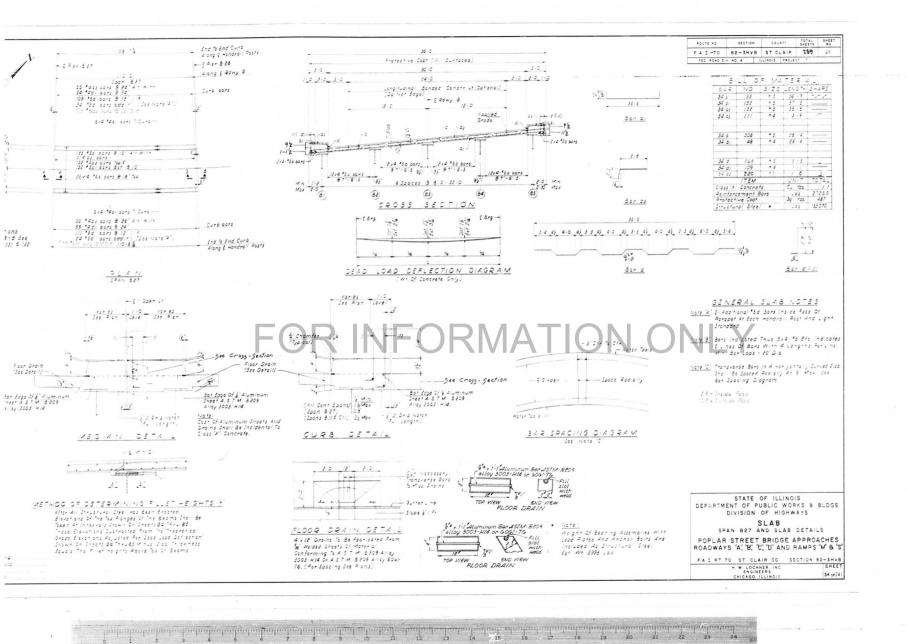


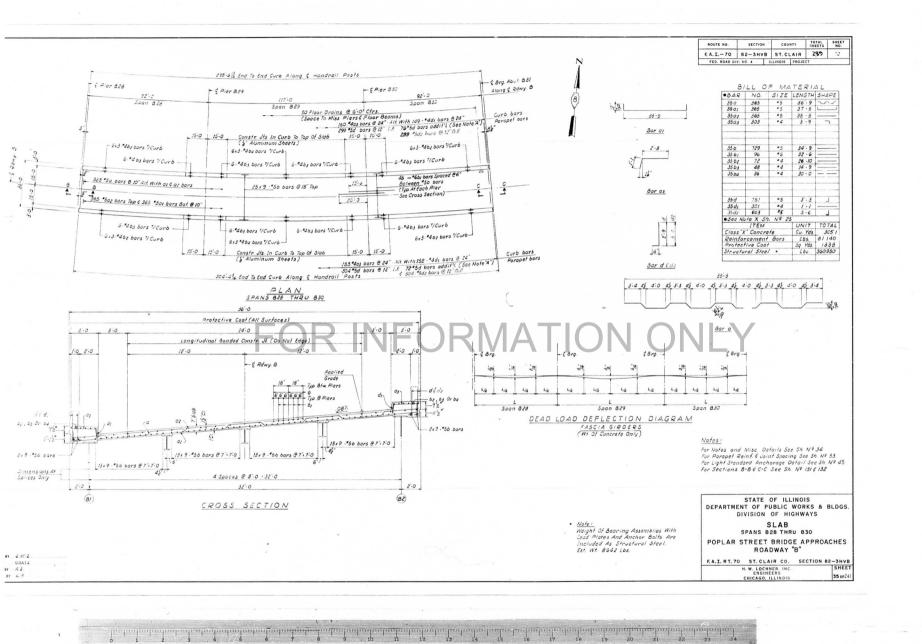


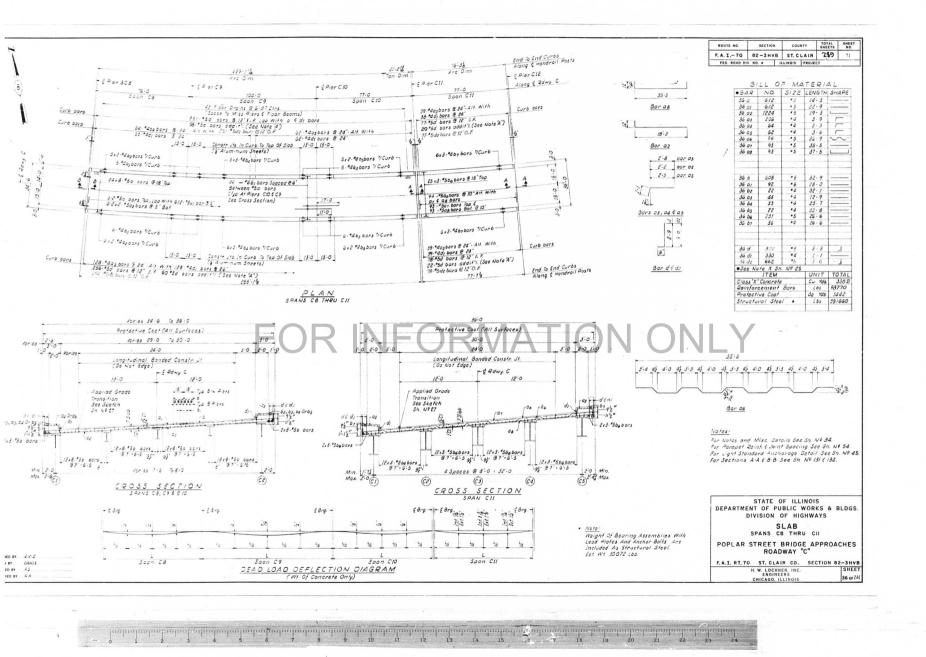


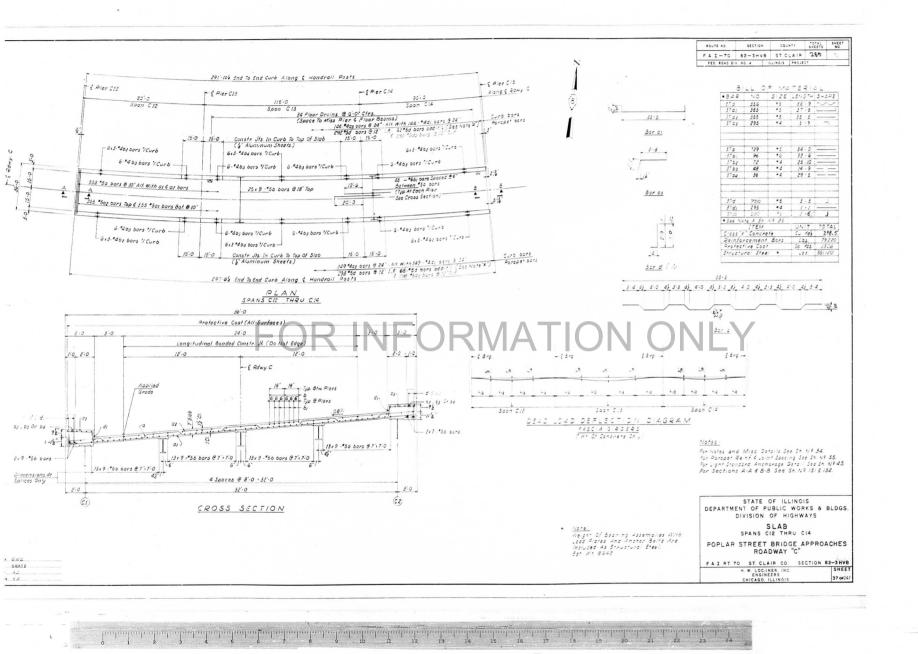


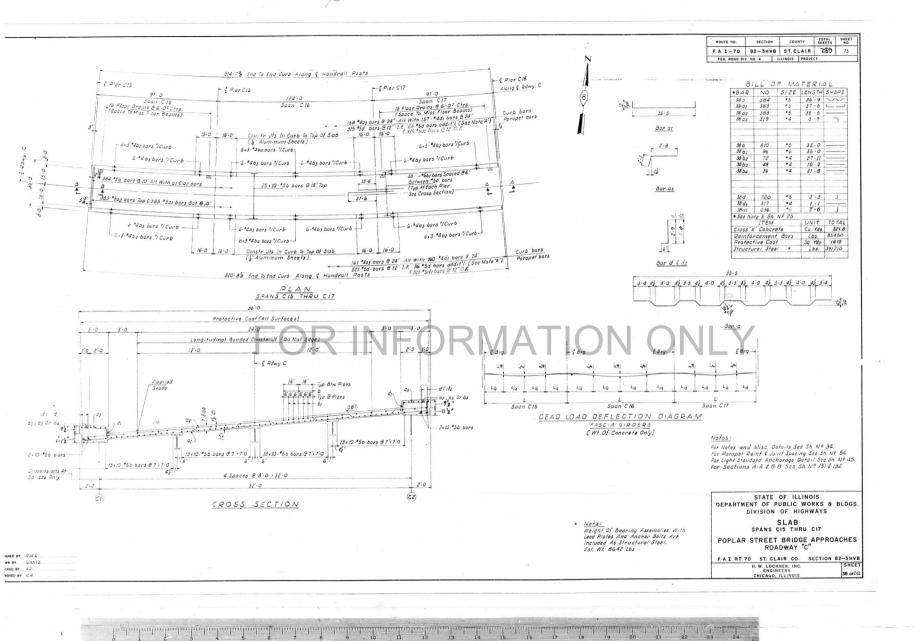




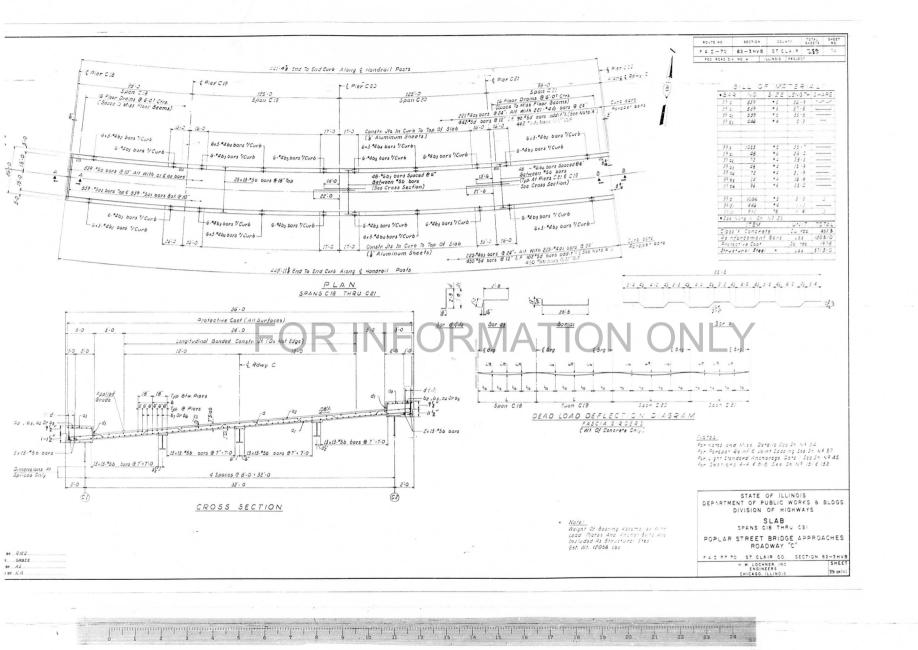


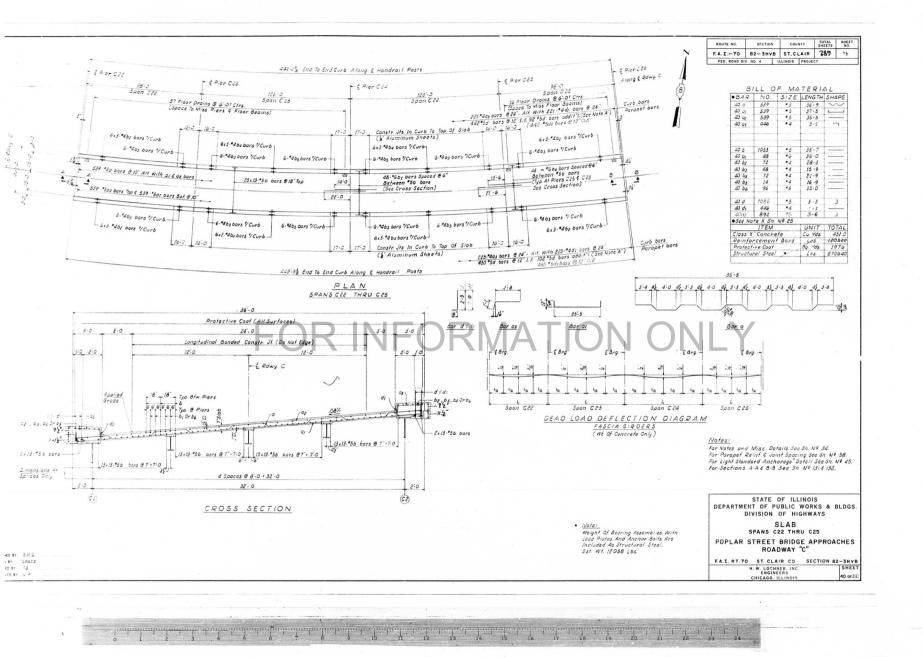


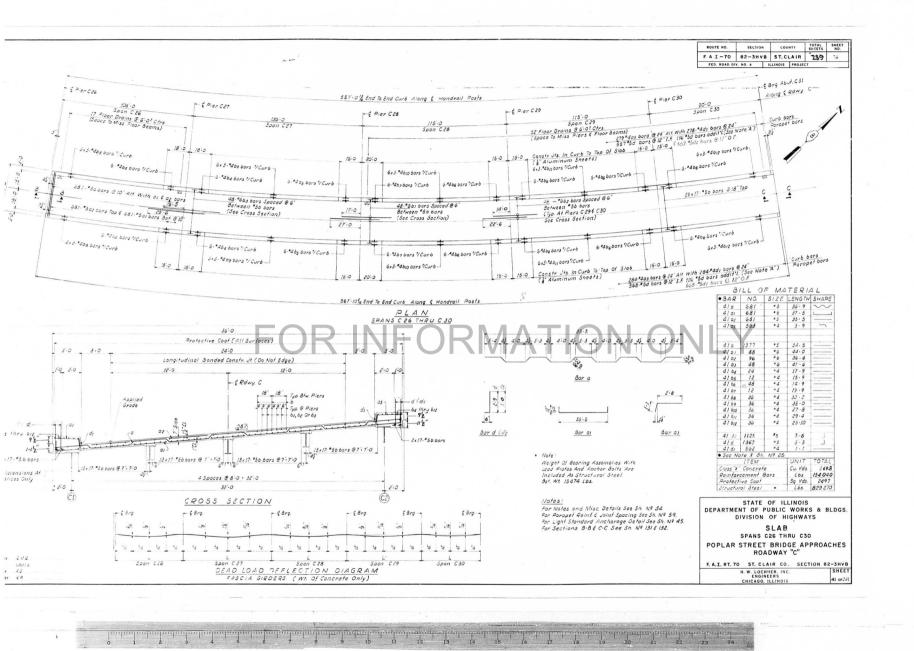


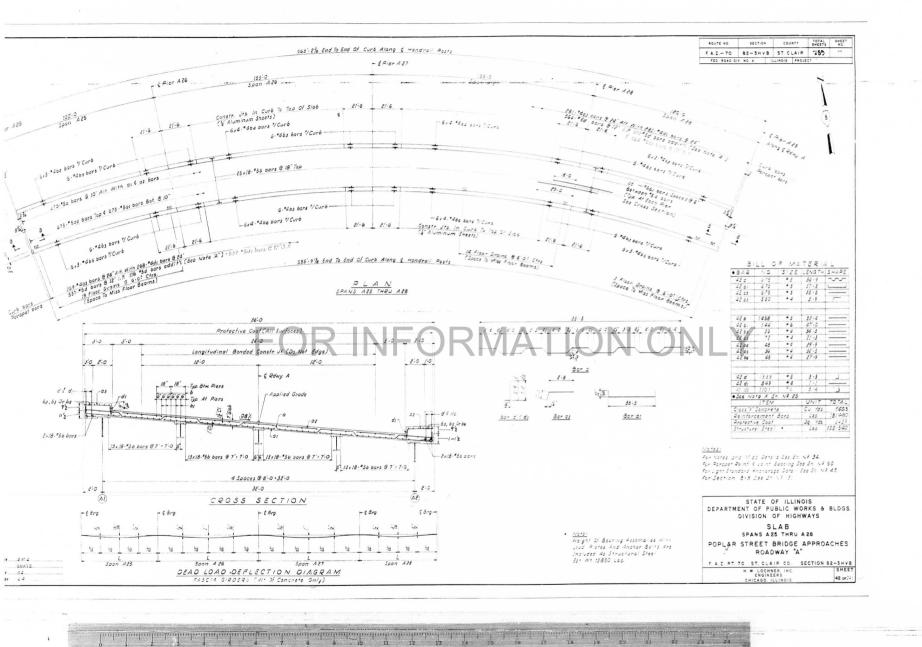


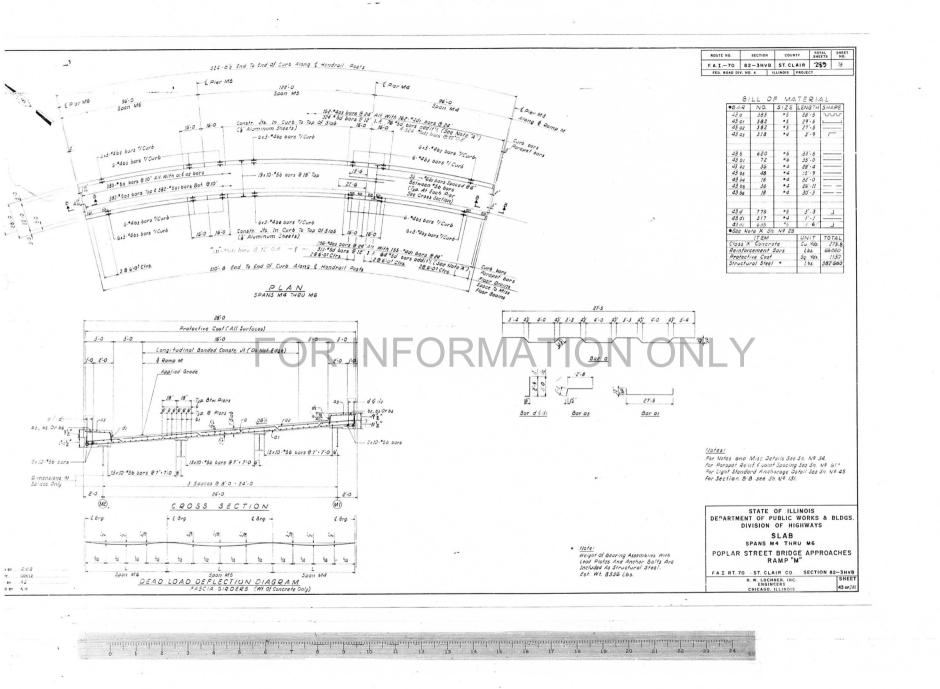
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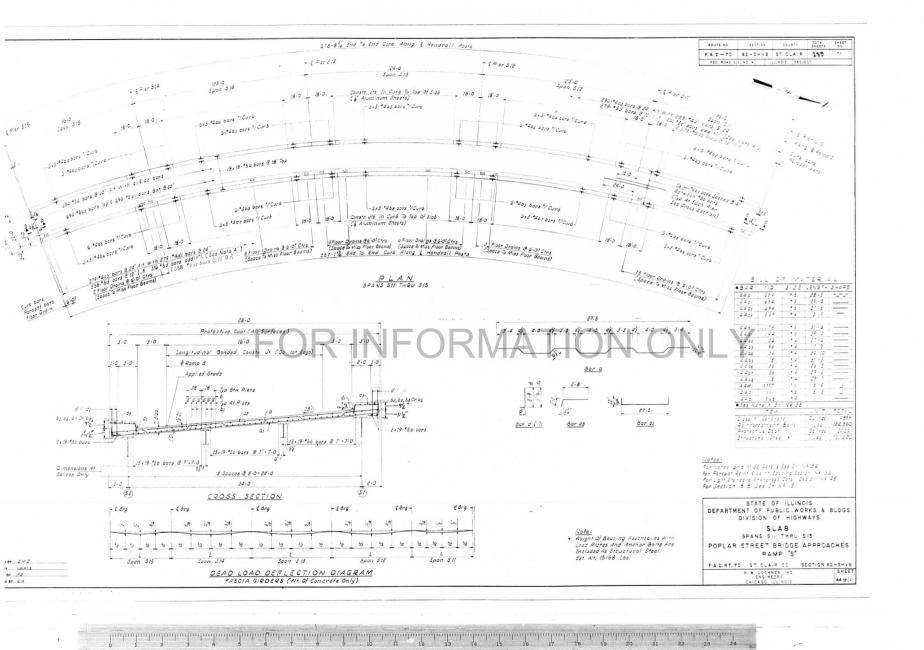


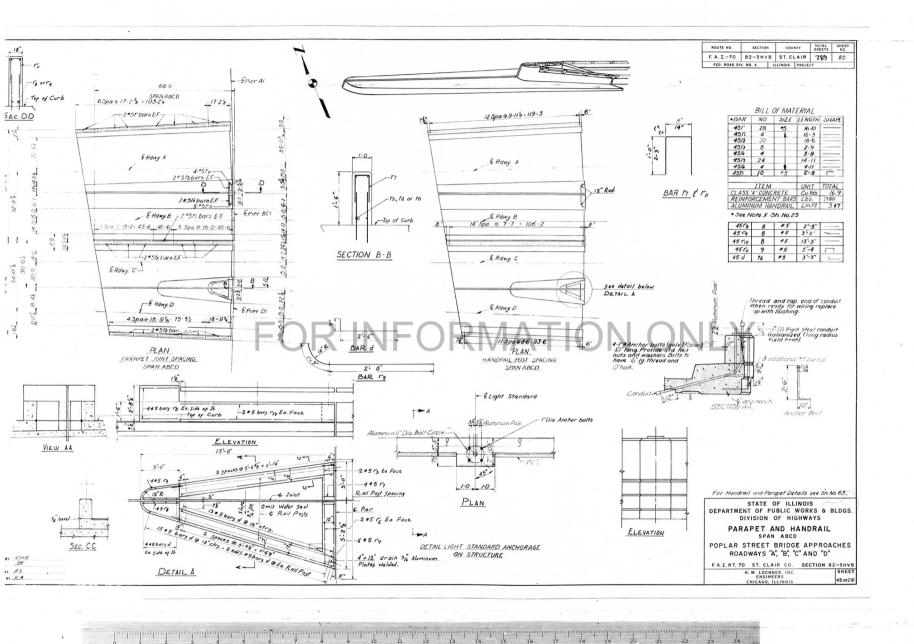


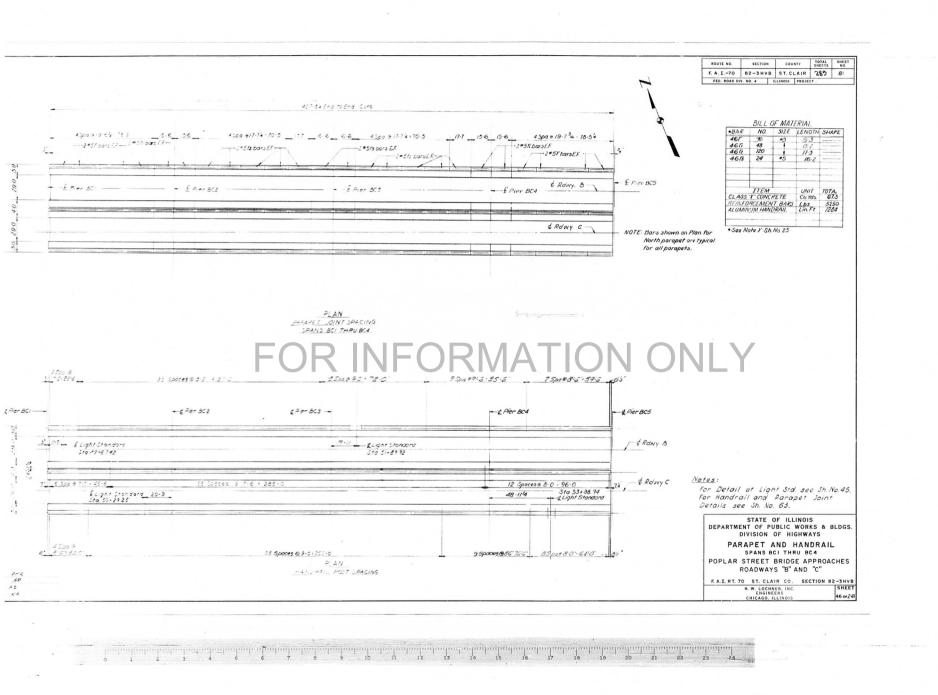


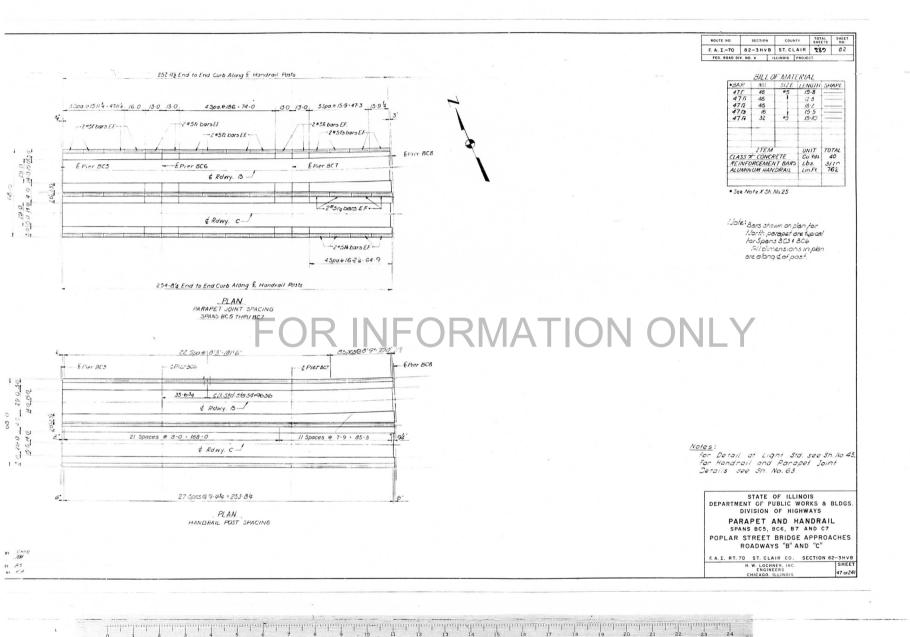


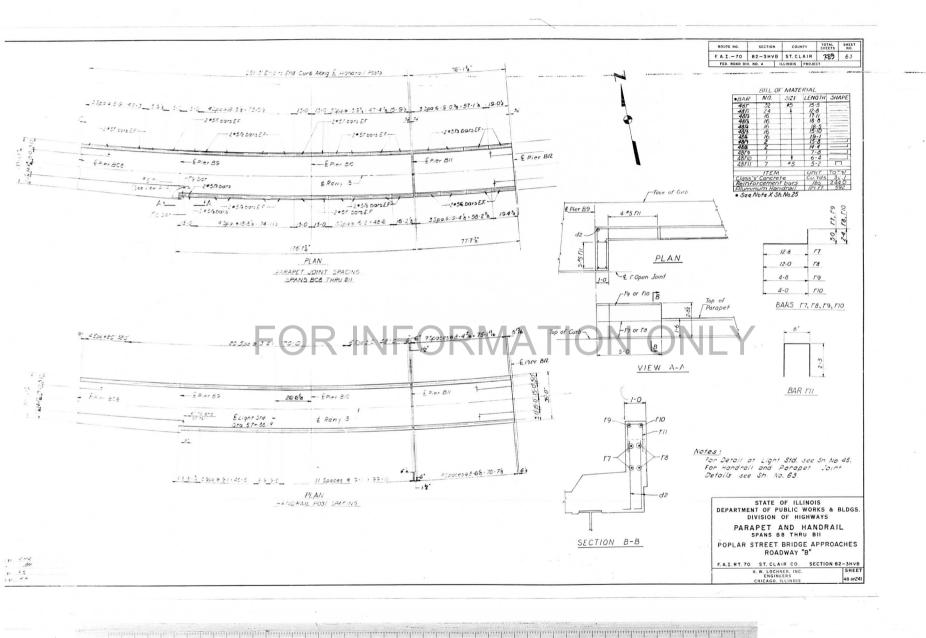


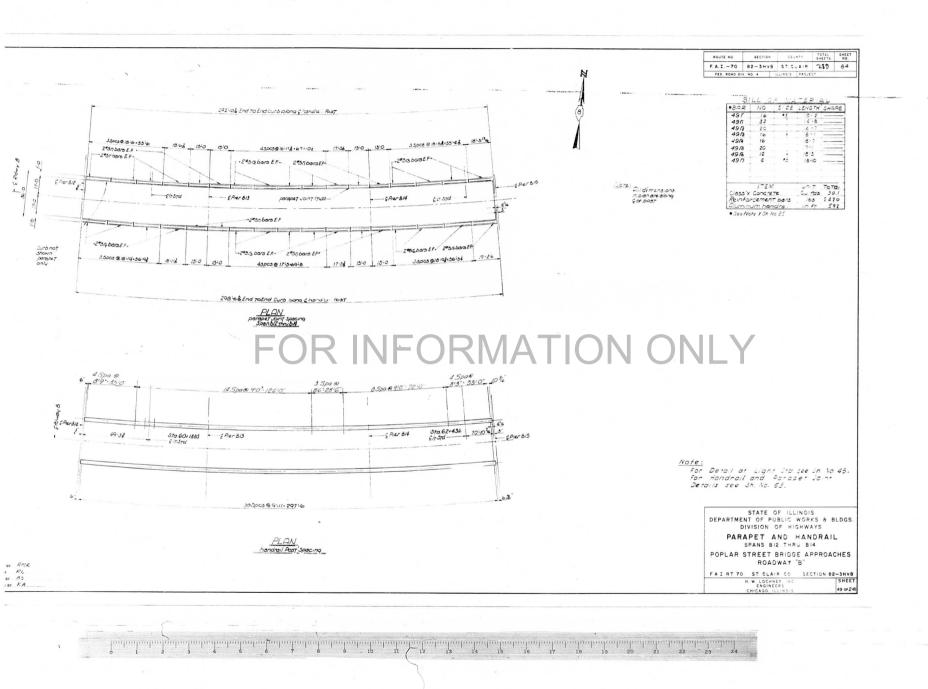




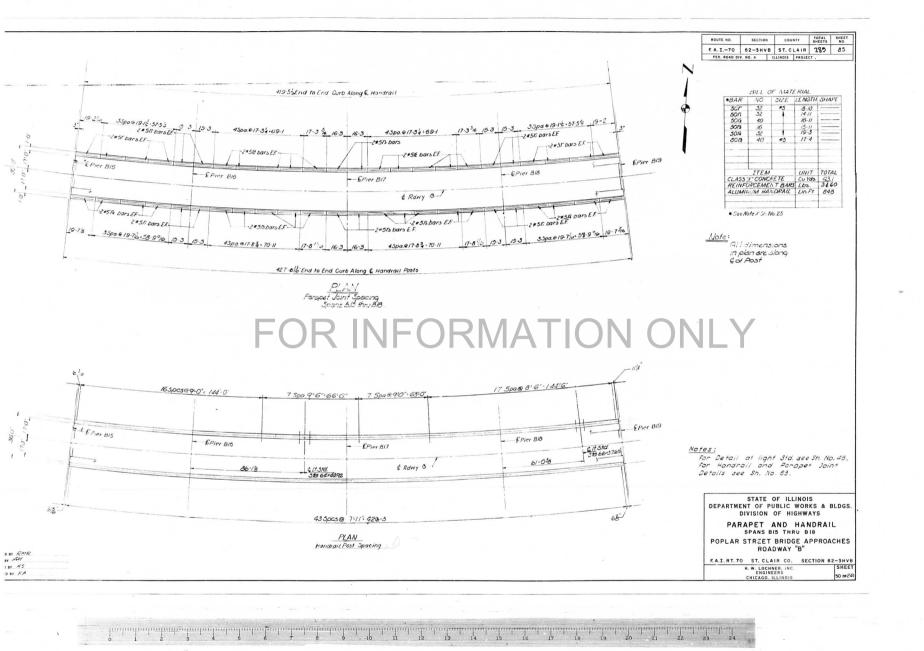


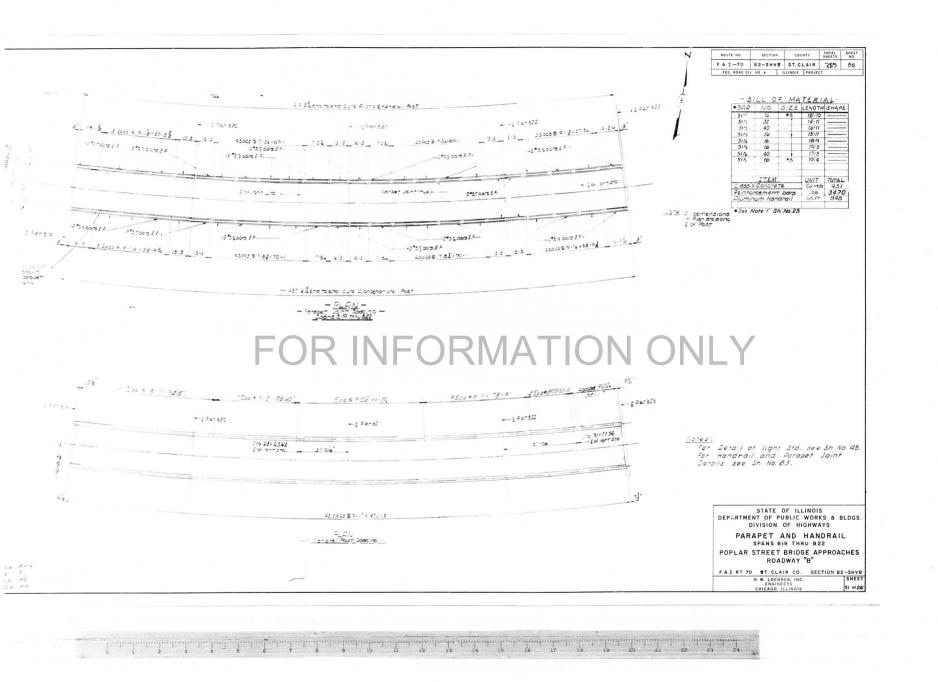


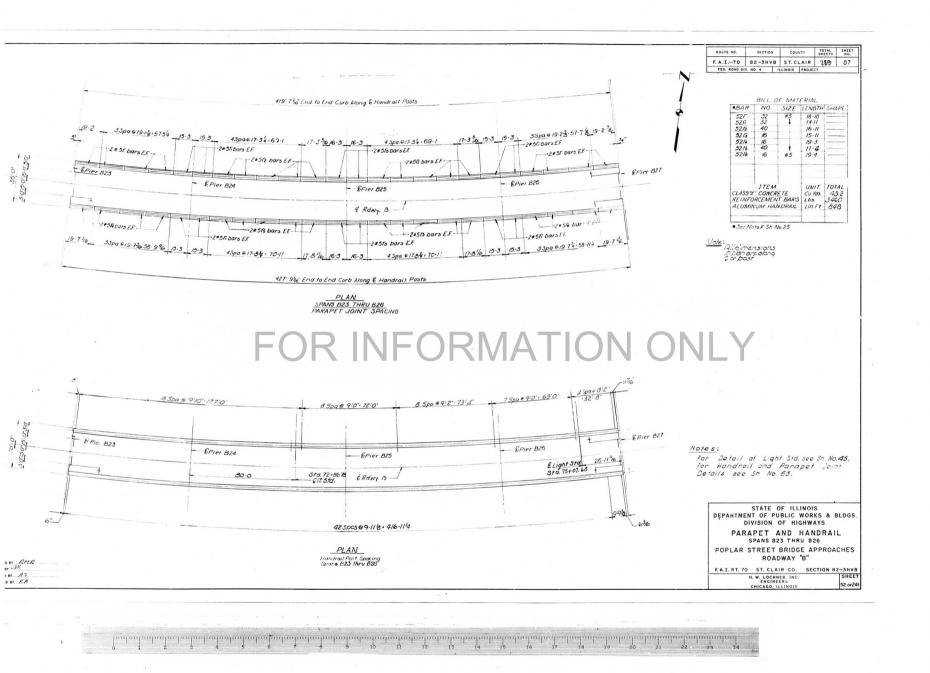


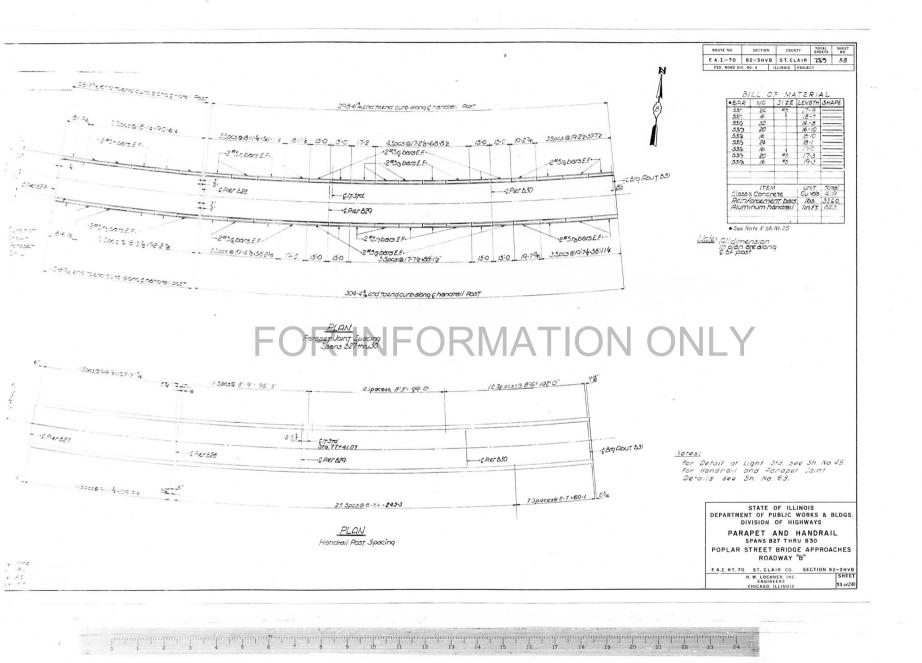


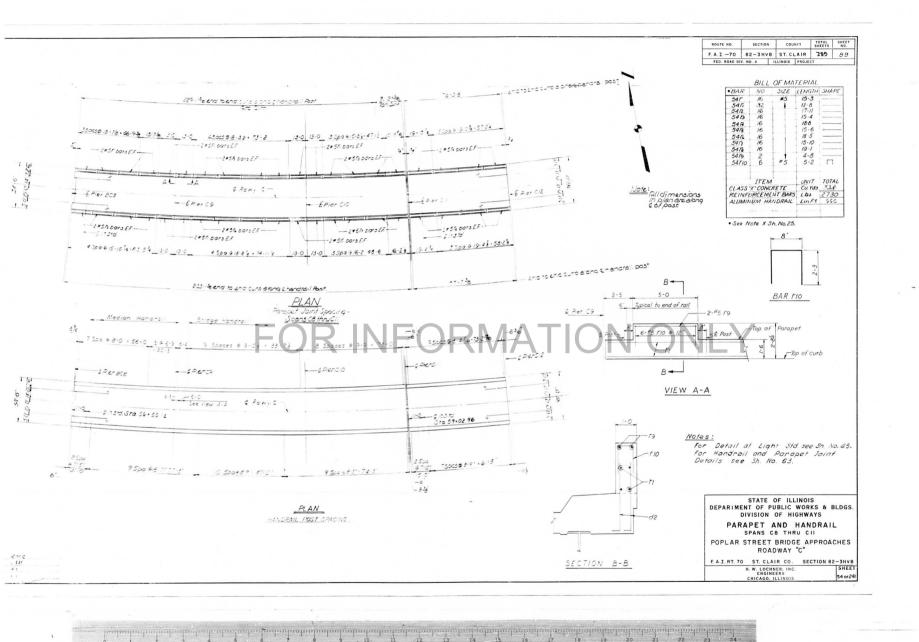
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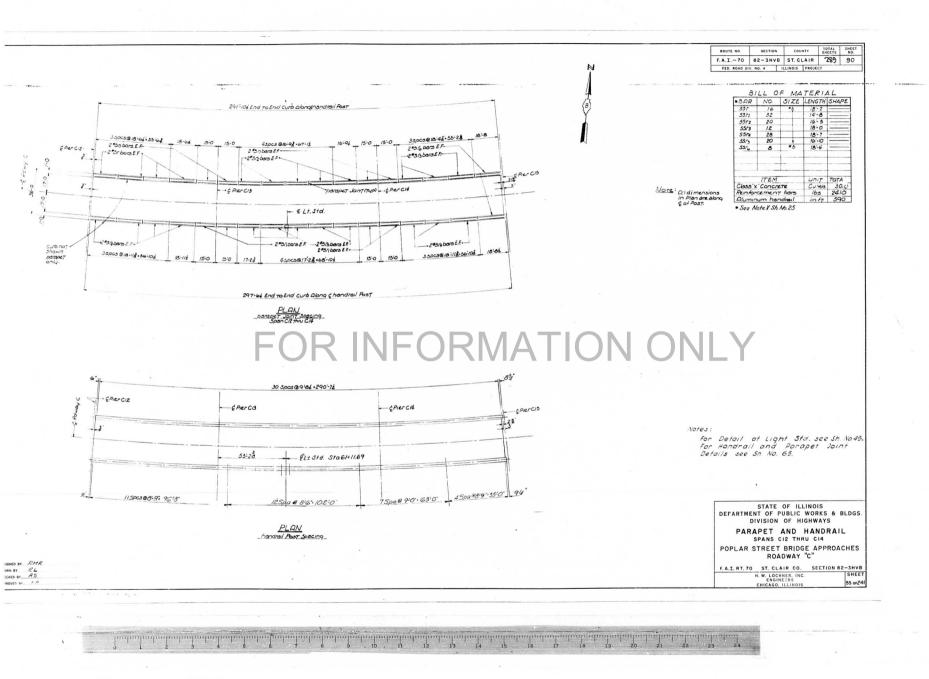


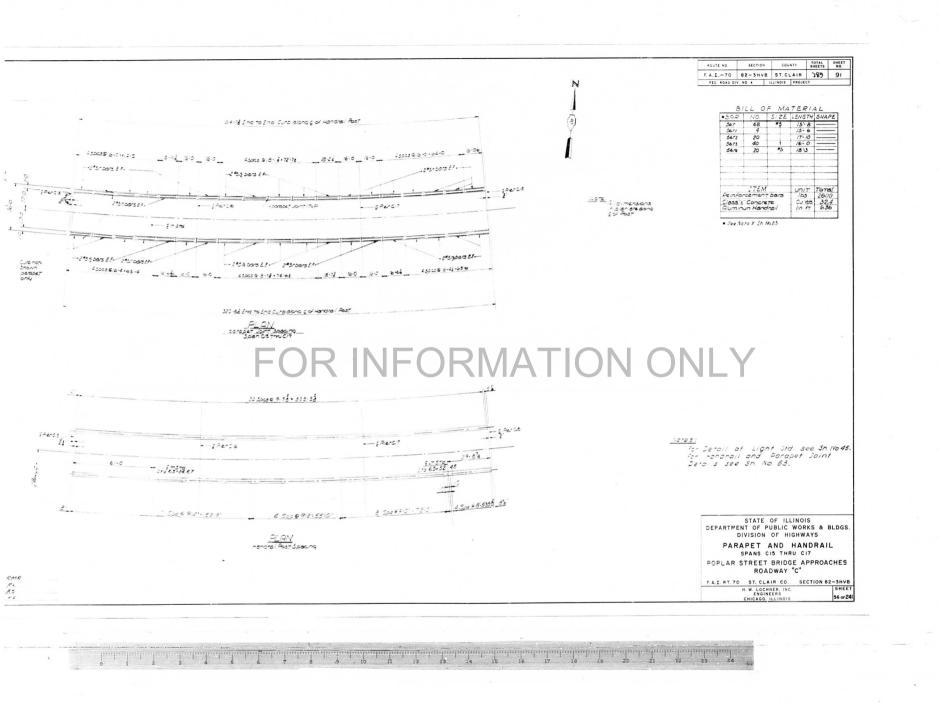


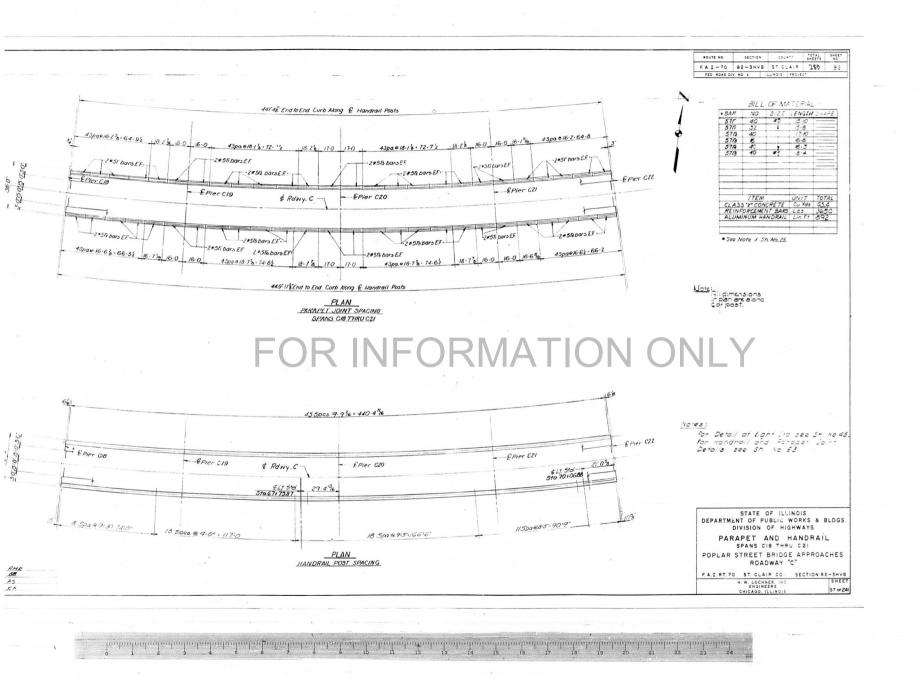


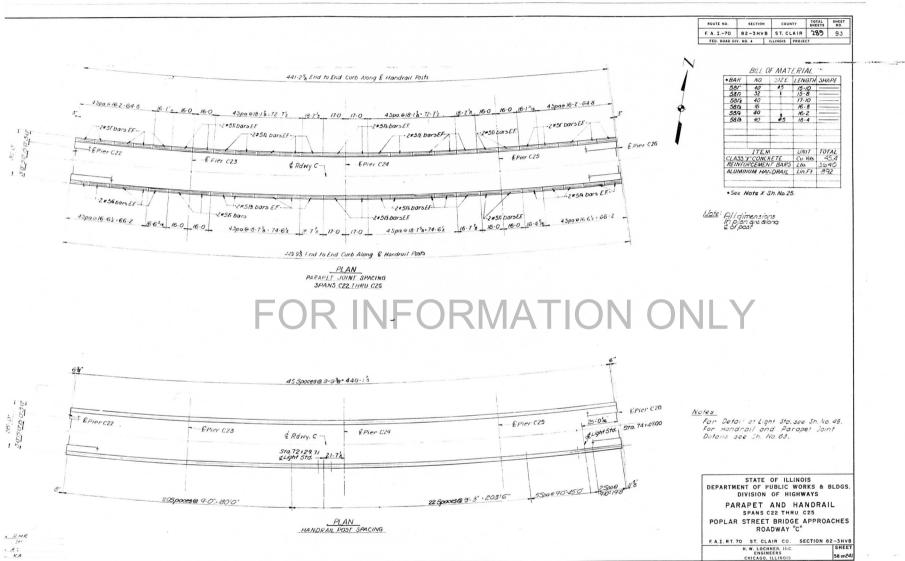


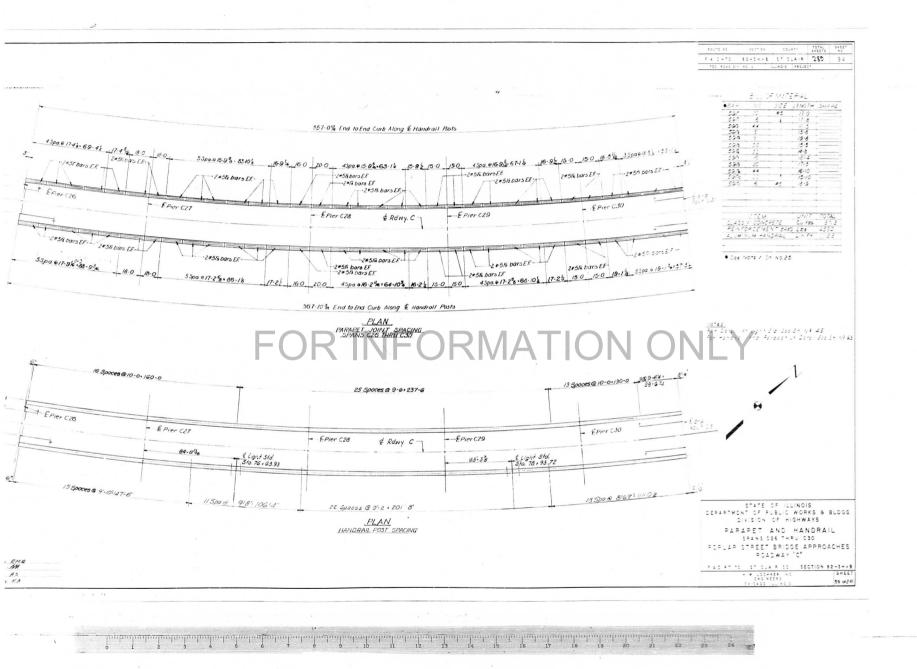


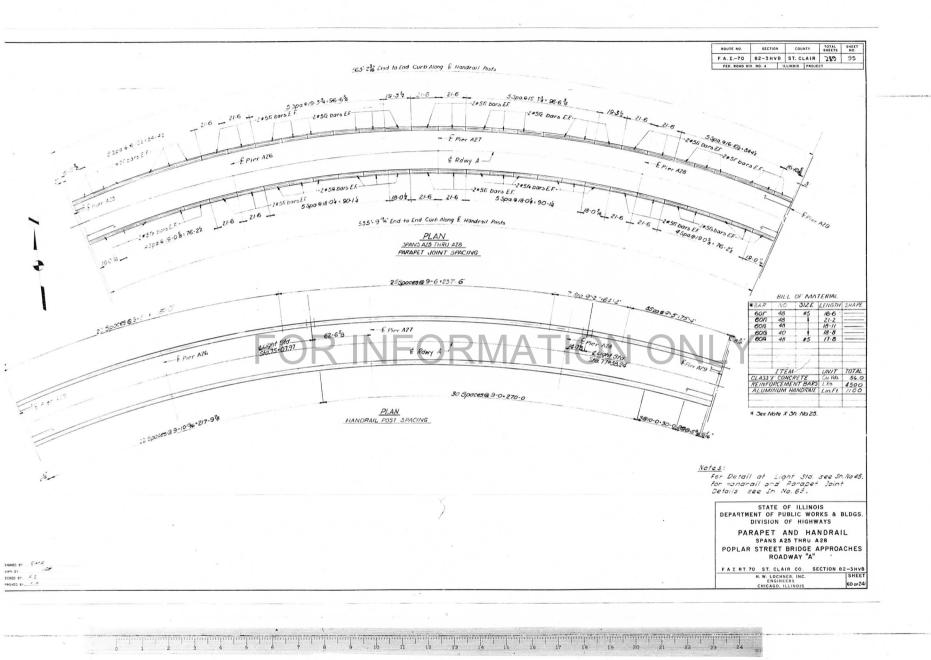


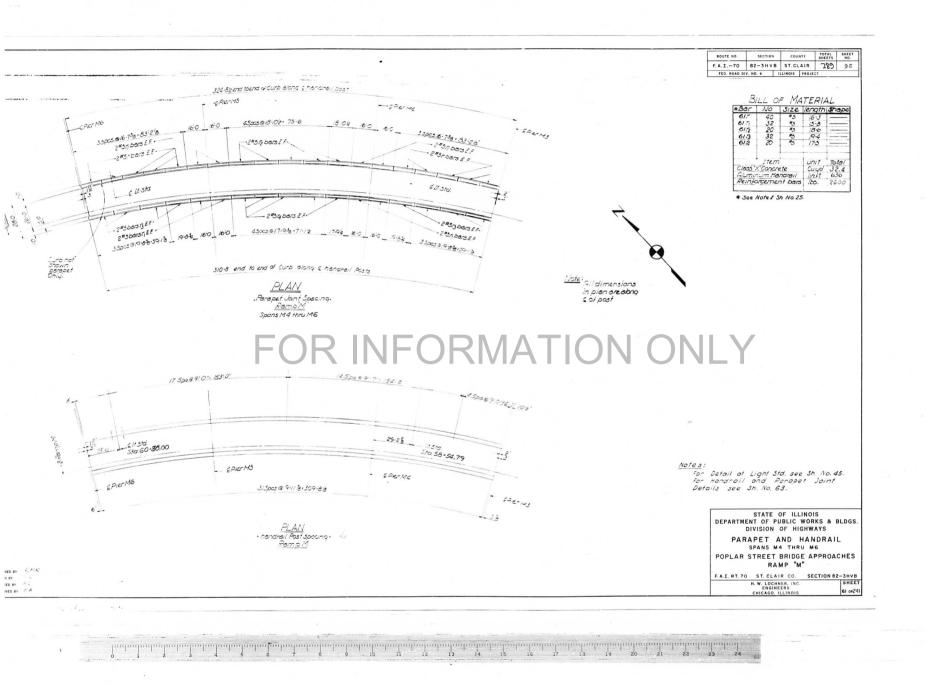


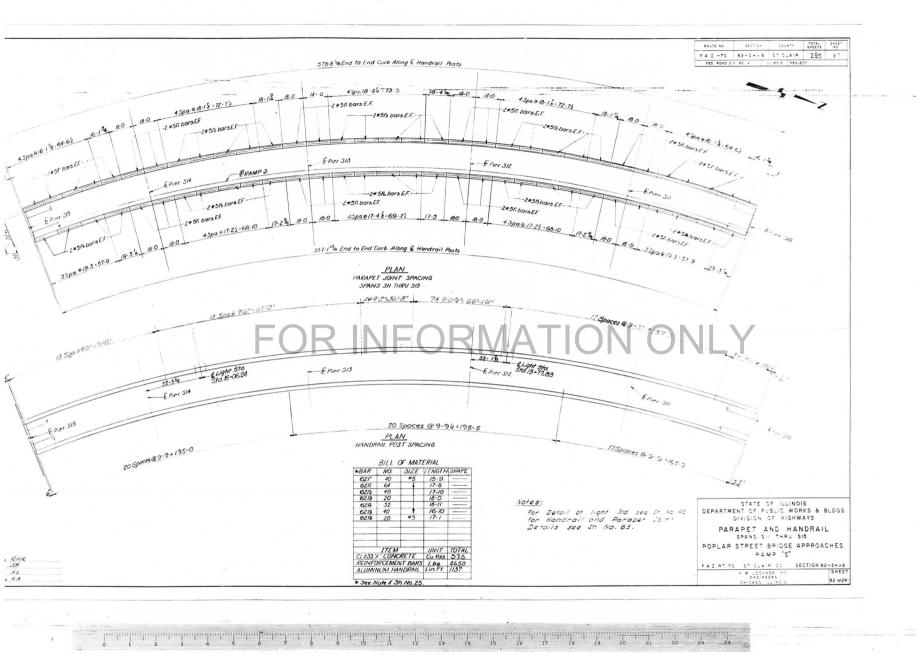


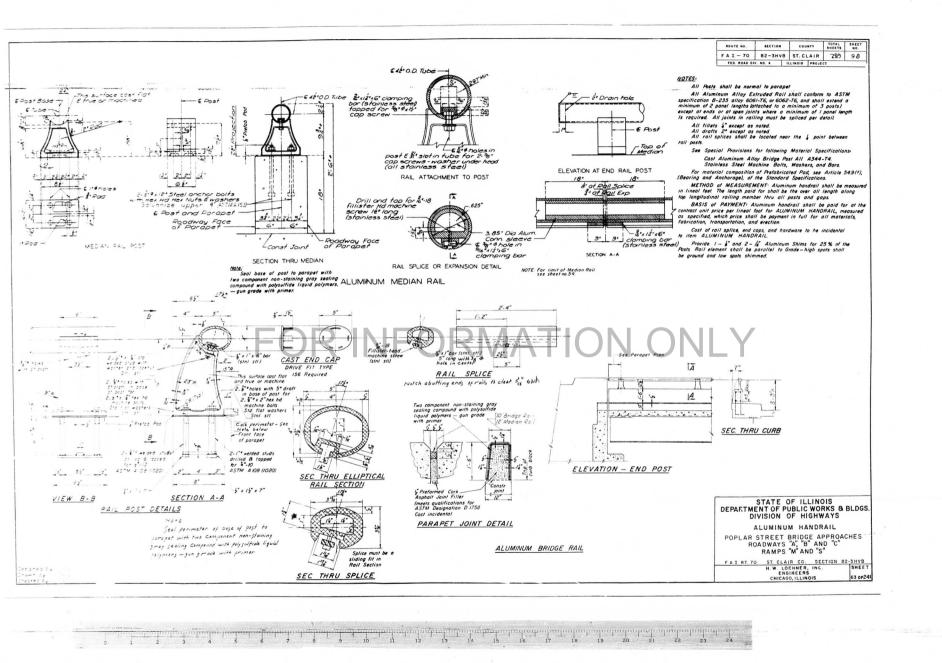


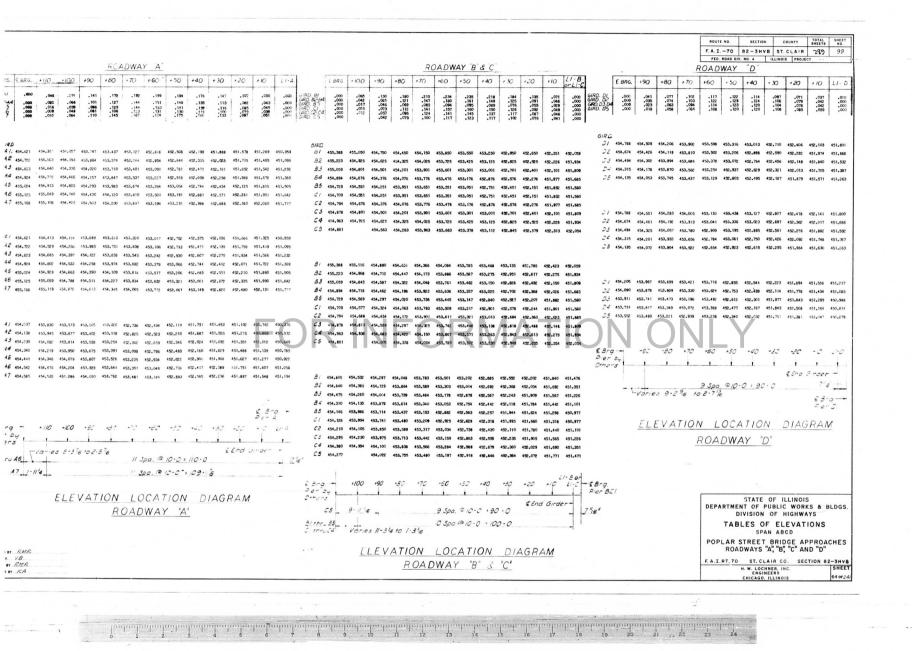












D.L. DEFLECTION (FT.) SPAN BC 2 2 2.5 4 4.5 5.5 7.5 8 8.5 3 3.5 6.5 9 9.5 10 .011 .003 .000 .000 .099 .041 .034 .090 .019 .008 .001 .022 .021 .031 THEORETICAL ELEVATION TOP OF CONCRETE S PO. 81 451,950 451,771 451,596 451,596 451,596 451,596 451,596 451,596 451,596 451,596 451,596 450,571 450,337 450,112 440,895 440,888 440,489 440,299 440,118 448,546 440,783 444,629 440,483 440,546 440,783 579. 451.633 451.654 451.479 451.279 450,199 450,199 450,197 450,454 450,250 440,195 449,571 449,571 449,572 449,100 448,666 444,512 448,506 444,229 448,101 447,882 447,872 \$7.9. 451,716 451,527 451,532 451,002 451,002 451,002 450,007 450,100 450,100 445,878 449,861 449,861 449,856 449,005 449,005 449,006 449,009 444,009 57 451,599 451,450 451,245 450,975 450,715 450,463 450,220 449,986 449,781 449,584 449,387 449,188 449,787 449,586 449,787 449,788 447,688 5 80. 82 451,482 451,393 451,188 450,588 450,588 450,584 450,584 450,598 450,594 450,693 445,685 449,427 449,220 449,021 448,831 448,655 448,478 444,315 444,161 448,015 447,678 447,750 447,691 447,621 THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION 9 7 3 3 451,995 451,776 451,677 451,567 451,567 451,104 451,657 451,060 451,104 451,652 450,503 450,503 450,503 450,999 449,688 449,492 449,510 449,510 449,510 449,578 448,670 449,578 448,670 449,578 451,678 451,678 \$1.6.3 451.659 451.650 451.650 451.650 451.650 451.650 445.650 445.650 445.650 445.650 445.650 446.651 445.650 446.650 451,716 451,546 451,363 451,126 450,870 450,616 450,369 450,125 449,889 449,855 449,855 449,258 449,258 448,566 448,566 448,566 448,287 448,136 448,287 448,143 448,004 447,757 451,599 451,465 451,009 450,753 450,551 450,565 457,009 450,755 450,008 449,775 449,548 445,337 449,141 448,959 448,789 448,627 448,471 444,319 444,175 448,056 447,887 447,640 FL CZ 451.488 451.398 451.149 450.688 450,688 450,584 450,785 449,881 449,855 449,655 449,004 449,672 448,580 448,550

ROUTE NO.	SECTION	COUNTY	TOTAL	NO.
F. A. I -70	82 - 3 H V B	ST. CLAIR	289	100

	0. L.	SEFLECTION (FT.)	INIEC	DIMATIA	ONI ONII V
SPAN	BC 3			5 F A N BC 4	
To the state of th	4 /4.5 /5 /5	5.5 16 16.5 17	/7.5 /8 /8.5 mi	9.5 3.0 20.5 21 21.5 1.3	
. 900, 000, 910, 900, 100, 000.	041 .039 .031 .	.020 .010 .002 .000	.003 .011 .021 .0	.000, 600, 520, 660, 860, 860, 100,	

#### THEORETICAL ELEVATION TOP OF CONCRETE

\*\*\* HT-06\*\* HT

THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION

THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION - SLAB THICKNESS (7')

\$\frac{1}{2}\$ \quad \text{4.17}\$ \quad \text{4.17}\$ \quad \text{4.17}\$ \quad \text{4.17}\$ \quad \text{4.18}\$ \quad \quad \text{4.18}\$ \quad \text{

Note A:

floor Baom 15 nations a line had may between floor Beam / and floor Beam 2. The times of elevations for Stringers are identified by nein relative position to the Girden indicated in the Tables.

STATE OF ILLINOIS
DEPARTMENT OF PUBLIC WORKS & BLDGS.
DIVISION OF HIGHWAYS
TABLES OF ELEVATIONS

SPANS BCI THRU BC4
POPLAR STREET BRIDGE APPROACHES
ROADWAY "B"

F.A.I.RT.70 ST. CLAIR CO. SECTION 82-3HVB
H. W. LOCHNER, INC.
ENGINEERS
CHICAGO, ILLINOIS
SHEET

D.I	DEFI	ECTION	(FT)

				SPA	N BC	5							SP	AN BC	6							5/	PAN B	7			
FLOOR BEAMS	L4	L4.5	22	22.5	23	23.5	24	24,5	25	25.5	26	26.5	27	27.5	28	28.5	29	29.5	30	30.5	31	31.5	32	32.5	33	33.5	L5
	.000	.007	.017	.021	.021	.016	.008	9000	.000	,006	.016	.027	.095	,038	.095	.027	.016	,004	.000	.002	,009	.016	.021	.021	.016	,007	.000

# THEORETICAL ELEVATION TOP OF CONCRETE

GIRD.	3/ 447.75	3 447.712	447.670	27,619	447.568	447.516	447,465	447.414	447,363	447.311	447.260	441.200	447,136	447.100	447.000	447.004	440, 753	****		440.720	440.747	440.033	440.045	440.332	*****	440.201	440.402
STR	447.63	447.620	447,601	447.578	447,555	447.532	447,509	447,486	447,463	447.440	447.417	447,393	447.370	447.347	47.24	447.301	447,278	47.25	47.22	447,207	447, 183	447,161	447,144	447,126	447,107	447,097	447,089
STR	447.50	4 447.528	447,532	447,537	447,542	447.547	447,552	447.558	447.563	447.568	447.573	447.578	447,583	447,588	447.594	447,599	447,604	447,609	447.614	447,619	447,624	447.634	447.648	447,663	447,679	447.695	447.715
STR	447.40	9 447.436	447,463	447.496	447.530	447,563	447,596	447,629	447.663	447,696	447.729	447.763	447.796	47.821	47.863	447.896	47.229	47.963	47.99	448,030	448,066	448.107	448.152	448,200	448.252	448,295	448.341
6100	0 2 447 26	447 344	447. 394	447.455	447-517	447.578	447-640	447,701	447.763	447.824	447,886	447.947	448,009	448.070	44.12	448.194	448.255	448.317	44.378	448,441	448.508	448.579	448.655	448.736	448.823	448,893	448.967

### THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION

GIRD. BI	447.753	447.719	447.687	447.641	447.589	447.533	447.474	447.416	447,363	447.318	447.277	447.236	447, 193	447,145	447.090	447.031	446,969	446,908	44.850	446,801	446,756	446.712	446,665	446,613	446.557	445,508	446,462
STR.	447.638	447.627	447.618	447.600	447.576	447.548	447,518	447.488	447.463	447.446	447.453	447.421	447.406	447,386	447,359	47.28	447,295	47.262	47.22	447,210	447,192	447.178	447,166	447,148	447.124	447.104	447,089
STR.	447.524	447,535	447.549	447,559	447,564	447,564	447,561	447.560	447,563	447.574	447.590	447.605	447,618	447,627	47,629	447,626	447.620	447,615	47,614	447,621	447.634	447.651	447,669	447,685	447,696	447,703	447.715
STR.	447,409	447.444	447.480	447.518	447.551	447.579	447.605	447,632	447,643	447.703	447.746	447.790	447.831	447,864	447,250	47,123	447,946	447,969	47.9%	448.033	448.075	448.123	448.173	448.222	448.268	448.302	448.341
GIAN AS	447 204	447 252	447 411	447 477	447.538	447.595	447 649	447.704	447 763	447 831	447.903	447.975	448.044	448.109	44.167	448,221	448.272	44.23	44.378	448,444	448,517	448.596	448.676	448,758	448.840	448,900	448.967

### THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION - SLAB THICKNESS (7")

GIRD. BI	447.170	447.136	447.104	447.057	447,006	446,949	446.891	446.833	446.779	446.734	446.693	446,653	446,609	44.541	444,507	446,448	444,386	44.25	441.267	446,218	446.172	446.128	446.081	446.030	445.973	445.925	445.879
STR.	447.055	447.044	447.035	447.017	446.993	446.965	446.934	446,905	446.879	446.863	446.850	446.837	446,822	446.802	446.776	446.745	446.711	446,678	44.649	446.626	446.608	446.595	446,582	446,564	445,540	445.520	446,505
STR.	446.940	446.952	446,966	446.976	446,980	446.960	446.978	446.977	446,979	446.991	447.006	447,022	447,035	447,043	47.045	447,043	447,037	47,02	447.031	447.038	447,050	447.067	447.086	447.101	447.113	447.119	447.12
STR.	446,825	446.860	446.897	446.935	446.968	446.996	447.022	447.049	447.079	447.119	447,163	447,207	447,248	447.284	447,315	447.340	447,363	47.34	47,413	447,449	447,492	447.540	447.590	447,638	447,685	447.718	447,758
	*** 710	446 760	446 997	445 004	446 958	447 011	447 065	447 191	447 100	447.248	447.319	447.301	447.461	47.95	447.584	47.627	447.688	447,740	41.795	447.861	47.934	448.012	448.093	448, 175	448,257	448,317	449.364

## 

### THEORETICAL ELEVATION TOP OF CONCRETE

GIRD	BI	446,459	446.5:2	446.544	446,598	446,652	446.706	446.760	446.814	446.858	446,922	446.976	447,030	447,084	447,138	417.192	447.246	447,300	447,354	47.40	447,462	447.516	447.570	447.524	447.678	447.732	447,776	447.820
57	R.	447.092	447,130	447,176	447,227	447,278	447,333	447,392	447,445	447,496	447,550	447,610	447.663	447.713	447.768	447.827	447.880	447.931	447,365	448,544	448.097	448.147	448,202	448.261	448.315	448.366	448.412	448.450
57	R.	447,724	447,765	447,809	447,861	447,912	447,967	448,027	448,081	448.131	448.187	448.247	448,300	448.351	448,404	444,465	448,519	448,569	448.524	441,481	448.736	448.787	448.841	448,901	448.955	449.006	449,052	449,100
ST	R.	448,357	448,398	448,442	448,494	448,546	448,502	448,562	448,717	448,757	448.823	448.884	448,937	448,988	449,044	449,104	449.157	449,208	449,253	417.32	449.376	449.427	449,481	449,541	449.595	449.646	449,692	449,740
GIRD																											450,336	

### THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION

GIRD. BI	446.459	446.509	446.561	446.620	446,673	- 446.722	446.769	446.817	445,868	445.929	446,993	447.057	447,119	447.176	447.227	447.273	447, 317	447,361	4.42	447.465	447.525	447.586	447.645	447.700	447.749	447.784	447.82
STR.	447.092	447.140	447, 192	447,249	447,299	447,349	447,401	447,448	447,495	447.557	447,626	447.690	447.748	447,806	447.862	447,907	447,947	447.991	445,544	448,099	448.156	448,218	448,282	448,337	448,383	448,419	448,450
STR.	447.724	447.772	447,826	447,883	447,933	447,984	448,036	448.083	448,131	448,193	448.263	448.327	448.386	448,444	448.501	418,546	448,586	44,5%	444,643	448,739	448.796	448.858	448.922	448.977	449,023	449,059	449,100
STR.	448.357	448.405	448.459	448.516	448.567	448.618	448,671	448.719	448.757	448,830	448,900	448.965	449,023	449.082	449,139	449.184	449,225	449,259	41,32	449.378	449,435	449,498	449.562	449.617	449.663	449,699	449.74
GIPD B2	A40 000	449 040	440.000	*** ***	440 011	440.000	*** 210	*** ***	*** ***	440 496	*** ***	440 407	449 559	110 700	445 751	449 958	449.870	449.515	415.941	450,000	450,083	450,146	450,205	450,260	450,309	450.344	450.360

### THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION - SLAB THICKNESS (7")

	GIAD. DI	445.876	445,925	445.977	446.036	446.090	446.139	446.186	446.233	446.265	446.343	440.403	440.4/4	440.530	440.793		****	440.130	****		440.001	440.542	441,000	44.1000				
	STR.	446,509	446.556	446,609	446.666	446.716	446.766	446.818	446.864	445,912	446.974	447,043	447,107	447,165	447,223	447.279	447.224	447.364	447,408	417,450	447.516	447,573	447,635	447,599	447,753	447.800	447,836	447.876
	STR.	447,141	447, 189	447.242	447,299	447,350	447.400	447.453	447,500	447,548	447.610	447.680	447.744	447.803	447.861	447.917	447.963	448,003	448,047	441.100	448.155	448.213	448.275	448,339	448.393	448.440	448,476	448.516
GNED BY 2 MA	STR.	447,773	447.822	447.876	447,933	447,984	448,035	448,088	448.136	448.184	448.247	448.317	448.381	448,439	448,499	448,556	448.601	448.641	448.585	441,739	448.795	448.852	448.914	448,979	449.033	449,080	449.116	449.156
IN BY V3 IXED BY RMR HOVED BY KA	31RD. 82	448,405	448,456	448,510	448,572	448,628	448,679	448,727	448,776	448,830	448.892	448.957	449,024	449,086	449,145	449,197	449.744	449,289	449,334	117,38	449,439	449,500	449,562	449,521	449,676	449.726	449.760	449.796

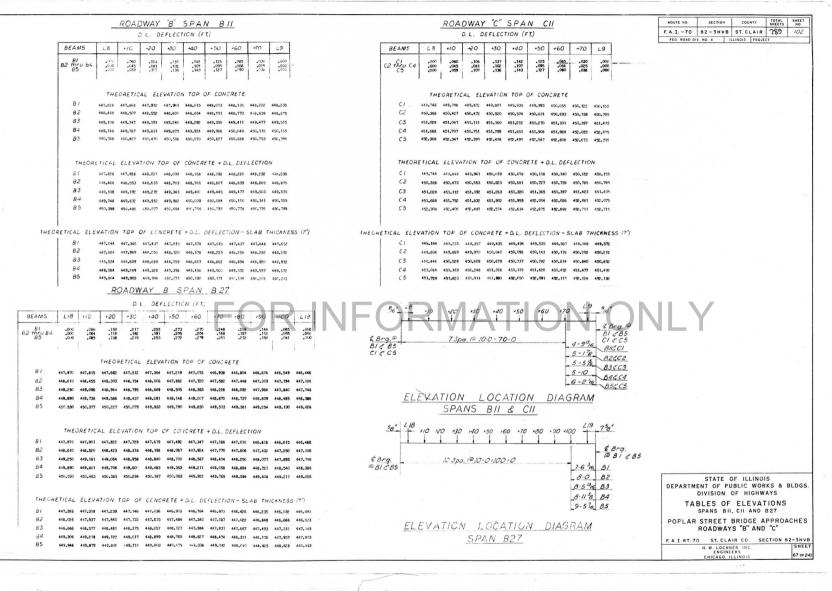
See Note A - Sn. No. 65 .

STATE OF ILLINOIS
DEPARTMENT OF PUBLIC WORKS & BLDGS
DIVISION OF HIGHWAYS

TABLES OF ELEVATIONS

POPLAR STREET BRIDGE APPROACHES
ROADWAY "B"

F. A.I.RT. 70 ST. CLAIR CO. SECTION 82-3HVB
H. W. LOCHNER. IN.C.
ENGINEERS CHICAGO. ILLINOIS 6607241



ROUTE NO.	SECTIO	N	cou	NTY	TOTAL SHEETS	SHEET NO.
F. A. I70	82-3H	VВ	ST. C	LAIR	289	103
FED. ROAD D	V. NO. 4	1	LLINOIS	PROJE	CT	

D. L. DEFLECTION (FT.)

		_				5 0.	AN B	12									SPA	N B	13									SPA	N B	14				
FLOOR	L10	L	10.5	46	46.5	47	47.5	48	48.5	49	49.5	50	50.5	5/	5/.5	52	52.5	53	53.5	54	54.5	55	55.5	56	56.5	57	57.5	58 -	58.5	59	59.5	60	60.5	LII
DEAMS	, 500		,003	.019	,030	.05	,735	.029	.080	,516	,378	.000	.005	.015	.027	,039	.047	.090	,047	,039	.027	.015	.005	.000	.002	.010	.090	.090	.035	.035	.030	.018	.00?	.000

### THEORETICAL ELEVATION TOP OF CONCRETE

G190. 81	114,544	448.976	448,308	448,360	148.17	44.455	448.517	448,569	44.421	448,673	448.726	448.778	442,830	44.80	448.934	448.987	449,039	449,091	449,143	449, 195	449.248	449.300	449, 352	449,404	449,456	449,509	449, 561	449,613	449.665	449.717	449.770	449.800	449.831
57 A.	112.384	649.515	449.545	448.394	449,049	443,105	449,149	449,901	449.258	449, 309	449.358	449,410	449,457	445.518	449,566	449,619	449.575	49.727	449.775	449.828	449.884	449, 336	449.984	450.037	450,093	450, 145	450, 193	450,245	450, 302	450, 355	450,406	450,438	450,471
579.	113 154	445 195	449.589	449.634	449.589	445.740	449,799	449.841	449, 299	449,545	49,998	450,050	450, 107	450, 158	450,206	450.259	450,315	450,367	450,415	450,468	450,524	450,576	450,624	450,677	450,733	450,785	450,833	450,885	450,942	450,995	451,046	451.078	451,111
579.	197.114	417 199	450 999	450 274	450, 393	450,560	450, 429	450,481	450,538	450,589	450,638	450,690	450,747	450,798	450,846	450,899	450,955	451,007	451,055	451,108	451.164	451.216	451,264	451,317	451,373	451.425	451.473	451.525	451,582	451,635	451,686	451,718	451,751
G/RD, R2	150,304	490 494	450.868	450.300	450,379	451.195	451,077	451,129	451,181	451,830	451,286	451,338	451.390	451,442	451,494	451.547	451.599	451.651	451,703	451.755	451,808	451.860	451.912	451,964	452,016	452,069	452.121	452.173	452.225	452.277	452.330	452.360	452.391

# THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION

G/AC. 8 /	643,744	441,900	448.327	448,391	449,449	44,52	448,547	448,590	44,12	448,676	448,775	448,783	44,845	44,910	448,974	449,034	449,089	449, 138	449,183	449,223	449.263	41,35	449.352	449,407	449,467	449,529	449,591	449,648	449.701	449.748	449.788	449,803	449.831
STA.	443, 184	648,916	448,961	449,024	145,085	445,136	449,179	443,222	449,258	449.312	449,356	449,415	419.42	41.54	449,606	449,566	449.725	449,774	449.815	449,856	449,900	415,541	449,984	450,039	450, 104	450, 165	450,223	450,281	450, 338	450, 385	450,425	450,440	450,471
STR.	445.524	449,056	449,601	449,564	449,725	449,775	449,819	449,862	449,308	41.92	449,998	450,055	490,122	450, 186	450,246	450,306	450,300	450,414	450,455	450,496	450,540	450.581	450,624	450,679	450,744	450,805	450,863	450, 921	450.978	451.025	451.065	451,080	451, 111
578.	107 114	455 156	450.941	450, 304	410.365	150, 616	450.459	450.500	450.548	450.590	450,638	450,695	450,752	450.85	450,886	450,946	451,006	451,054	451,095	451.136	451,180	451.221	451.264	451.319	451.384	451.445	451,503	451.561	451.618	451.665	451.705	451.720	451.751
5.00.02	100 304	177 147	450 687	450, 951	451.704	411.146	451,107	451,150	451.199	451,236	451,286	451,343	451,405	451,470	451,534	451,594	451.649	451,698	451,743	451,783	451.823	451.865	451,912	451,967	452.027	452.089	452, 151	452.208	452.261	452,308	452.348	452, 363	452, 391

### THEORETICAL ELEVATION TOP OF CONCRETE + QL. DEFLECTION - SLAB THICKNESS (7')

GIRD 81	147,160	447,595	447,744	447,807	447,865	447,515	447,963	448,07.5	41.41	448,090	448, 142	448,200	443.252	41.27	448,390	448.451	448,506	44.92	44.599	448,640	448,580	44.72	448,749	448,824	448,884	448.946	449.008	449,065	449.118	449, 164	449.205	449.220	449.247
578	448,97	448,300	448.378	448,441	43,50	44,92	448,595	44,639	44.585	44.73	448.774	443.82	44.299	44.80	449,022	449,083	449.142	449, 191	449,231	449.272	449.315	419.354	449,401	449.456	449,521	449.58?	449,640	449, 697	449.754	449,802	449,841	449,857	449.887
57A.	143.541	445 975	449 019	449 (81	449.149	41 18	449.535	449,279	49.25	41,30	449,414	449.472	449,539	449,500	41.662	449.723	49.78	449.831	449,871	449.912	49.86	449.998	450,041	450,096	450, 161	450.222	450,280	450, 337	450, 394	450,442	450,481	450, 497	450.527
579.							*** ***	145 515	445 567	100.000	450.054	450, 112	450, 179	450.743	450,302	450,363	450,422	450,471	450,511	450.552	450.596	450,436	450,681	450.736	450,801	450,862	450,920	450,977	451.034	451.082	451.121	451, 137	451, 167
5 00 B3	155 005	10.00	15. 30	100.000	102 101	150 121	150 500	450,544	450.408	A50.053	450,70	450,760	150,822	450, 887	450,950	451,011	451,086	450,115	451, 159	451,200	451,240	A\$1.282	451.329	451.384	451,444	451,506	451.568	451.625	451.678	451.724	451,765	451,780	451.807
5 / AD. 62	* 3	17.12	.,.,.	19.00	* >1.1-2.						11111	A.L			7.0			- 1		1/	/ /						- 1	1				V	
G/RD. 82											V	1 Г		- 1	LV			- / 1		111	/   /			11.					7   1	VI I			
																				. II V										4 1			

See Note A.Sh. No. 65.

STATE OF ILLINOIS
DEPARTMENT OF PUBLIC WORKS & BLDGS.
DIVISION OF HIGHWAYS
TABLES OF ELEVATIONS

SPANS BIZ THRU BI4

POPLAR STREET BRIDGE APPROACHES ROADWAY "B"

F. A.I.RT.70 ST. CLAIR CO. SECTION 82-3HVB
H. W. LOCHNER. INC.
ENGINEERS
CHICAGO, ILLINOIS 68 07241

	FOTION	

					SP	AN B	/5						NA SER MARS IN TO			PAN	9. 16					
FLOOR BEAMS	L 12	L 12.5	61	61.5	62	62,5	63	63.5	64	64.5	65	65.5	66	66.5	6.7	67.5	68	68.5	69	69.5	70	70.5
	.000	.004	. 020	. 032	. 038	.038	.032	.022	.011	.008	. 990	,000	.010	.021	. 031	. 039	.041	.038	.030	.019	.008	.001

## THEORETICAL ELEVATION TOP OF CONCRETE

GIRD. BI	449.845	449.878	449,912	449.965	450,019	450,072	450, 126	450, 179	450.233	450, 287	450, 340	450, 394	450,447	450,501	450.554	450,606	450,662	450, 115	450,769	450.822	450,876	450,929
STR.	450, 485	450, 514	450,545	450, 598	450,656	450,708	450,758	450,811	450,870	450, 300	450, 877	451,096	451,084	451,137	451,186	451,240	451.298	451.351	451,400	451,454	451.513	451,565
STR.	451.125	451.154	451, 185	451.238	451.296	451,348	451, 398	451,451	451,510	451.562	451.612	451,666	451,724	451,777	451,896	451,880	451,938	451,991	452,040	452.094	452.153	452.205
STR.	451.765	451.794	451.825	451.678	451.936	451.988	452.038	452.091	452.150	152.52	452.752	452.306	452,364	452,417	412.466	452,520	452,578	459.631	450,680	452,734	452.793	452.845
GIRD. B2	452,405	452.438	452.472	452.525	452.579	452.522	452.686	452,739	452,793	4级,44	12,900	452.954	453,007	453,061	455, 114	453,168	453.222	453.275	453, 399	453.362	453, 436	453,489

### THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION

(	GIRD. BI	449.845	449,883	449,933	449,998	450.057	450,110	450,158	450.202	450,245	450,290	450,340	450,396	450,458	450,522	450,584	450.647	450,703	450,754	450, 799	450,842	450,885	450, 931
	STR.	450,485	450,519	450,566	450,631	450,695	450,746	450,790	450,834	450,881	450, 994	451, 877	451.028	451,094	451,158	451,218	451,279	451,340	451,389	451,421	451,474	451, 521	451.567
	STR.	451.125	451, 159	451.206	451.271	451,335	451,386	451,430	451,474	451.521	451,564	451,412	451,668	451.734	451,798	451,858	451,919	451,980	452.029	450.071	459.114	452.161	452.207
	STR.	451.765	451,799	451.846	451,911	451,975	452,026	452,070	452,114	452, 161	452.806	412.252	452.308	452,374	452,438	450,496	452.559	452,620	452.669	450.711	452.754	452, 901	452.847
	SIRD. RZ	450, 405	459 443	459 499	150 550	452 617	110 500	150 718	(50.760	455 906	450 190	415 ST	155 954	452 514	153 200	122 115	452 202	463 563	453 314	781.566	453 400	453 445	450 401

## THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION - SLAB THICKNESS (7')

									0.00													
GIRD. BI	449.262	449.299	449, 349	449,415	449,474	449.527	449,575	449.618	449, 561	449,707	445,757	449.813	449.874	449.929	450,000	450,064	450,120	450,170	450.216	450,259	450, 301	450.348
STR.	449, 902	449.935	449.983	450,048	450, 111	450,163	450,206	450.250	450.298	450, 343	450,389	450, 445	450,511	450,575	450,635	450,696	450,757	450,806	450 848	450,891	450,938	450.984
STR.	450,540	450, 575	450,623	450.688	450,751	450,803	450,846	450,890	450,938	450,160	451.029	451,085	451,151	451.215	451.275	451.336	451.397	451,446	451,488	451.531	451,578	451.624
STR.	451,162	451.215	451.263	451,328	451, 391	451,443	451,486	451,530	451,578	451,422	451,669	451,725	451,791	451,855	451,915	451.976	452,037	450,086	459,128	452, 171	452.218	452.264
GIRD. 62																						

							_		-	L. D	4-41	ON (F	7.)		VE.		N /		_			71	N I
51,000	1	,		,		SPAN	8 /	,			ш	X			JΕ		S	PANE	/8				
FLOOR BEAMS	7/ .	71.5	72	72.5	73	73.5	74	74.5	75	Z5.5	76	76.5	77	77.5	7.8	78.5	79	7.8.5	90	80.5	81	81,5	L/3
	.000	.001	.008	. 019	.030	.038	, 041	.039	.031	. 35.	.010	.002	. 000	.001	.511	. 22	. 032	. 038	. 036	.032	.020	.004	.000

### THEORETICAL ELEVATION TOP OF CONCRETE

GIRD. BI	450,983	451.03	451,090	451,143	451, 197	451.250	451,304	451,358	451,411	451,465	eth.the	451.572	451.625	451,471	451,729	451,776	451.822	451.86*	451,909	451,950	451.989	452.012	452,034
STR.	451,614	451.668	451.726	451.779	451.828	411.882	451,941	451,993	452,043	450.09*	414.155	452.207	452.257	452, 310	452,364	452,412	452,454	452,499	459.546	452,587	452.625	452.649	452.674
STR.	452.254	452,308	402.366	452,419	452,469	452,522	452,581	452.633	452, 683	472, ***	400.790	452.847	452,897	452, 950	455,004	453,052	453,094	453,139	453, 185	453,227	453.265	453.289	453.314
STR.	402,894	452.948	453,006	453.059	453,108	453,162	453,221	453.273	453.323	453.7	115.19	453,487	453,537	453,590	453,644	453,692	453,734	453,779	450, 104	453,867	453,905	453.929	453,954
GIRD. B2	453.543	453,596	453,650	453,703	453,757	453,810	453,864	453.917	453,971	454, 355	454,075	454, 132	454, 185	454,227	454,258	454,336	454,382	454,427	454,449	454,510	454,549	454,572	454,594

## THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION

GIRD. BI	450,983	451,038	451,099	451,163	451,227	451,289	451,346	451.397	451,443	451,486	411.521	451,574	451,625	451,681	451,799	451,798	451,855	451,905	451,948	451,983	452,010	452,016	451,034
STR.	451.614	451,670	451.735	451,799	451,859	451.921	451.982	452.032	452,075	450,113	150.165	450.010	452.257	452.313	452.274	152.434	452,486	455, 537	155.585	452.420	452,645	452.653	452.674
STR.	450.254	452,310	452.375	452,439	452,499	412,561	452,622	412.672	452,715	410.79	401, 801	450.850	452,897	452,953	453,016	455,074	453,126	455, 177	453,775	455,240	453,285	453.293	453, 314
STR.	452.894	452,950	453.015	453,079	453, 139	453, 201	453.252	453.312	453, 355	413, 399	(1), 445	453,490	453,537	453,593	455, 456	452,714	453,766	455, 817	455, 145	453,900	453,925	453, 933	453,954
GIRD, R2	453 543	452 500	459 659	452 703	453 747	452.240	112 204	152 957	454 203	100.000	V24 765	151.154	454 155	251.347	111 165	454 555	154 115	eternit.	111 505	101.015	154 570	454 576	454 554

# THEORETICAL ELEVATION TOP OF CONCRETE - D.L. DEFLECTION - SLAB THICKNESS (7')

GIRD. BI	450, 399	450,455	450,515	450,580	450,644	450,705	450,762	450.813	450,860	450, 900	450,945	450,991	451.042	451,098	651,156	451.215	451.271	451, 200	411.565	451,400	451,426	451,433	451,451
STR.	451,031	451,087	451,152	451.215	451,276	451,337	451.399	451,449	451, 491	451,525	411.581	451.62	451.674	451,730	451,793	451,851	451,903	451,954	450,001	452,037	452.062	452,070	452,091
STR.	451,671	451.727	451.792	451.855	451,916	451,977	452,039	452,089	452, 131	452.175	452.222	451.267	452.314	452.770	450,433	455.491	452,543	452,594	450,641	450,677	452.702	452,710	452,731
STR.	452.311	452.367	452,432	452.495	452,556	452, 617	452.679	452.729	452,771	452.315	452,862	452.907	452.954	453,010	455,075	453, 131	453,193	453.234	412.281	452, 217	453.342	453,350	453, 371
GIRD. 82	452,959	453,015	453,075	453,139	453,204	453.265	453, 322	453, 373	453, 420	453, 460	453,505	413.551	452,602	453, 658	455,716	455,775	453, 837	453,882	451,926	453, 960	453.986	453,993	454,011

F.A.I.-70 82-3HVB ST.CLAIR 289 104

See Note A - Sh. No. 65

STATE OF ILLINOIS
DEPARTMENT OF PUBLIC WORKS & BLDGS. DIVISION OF HIGHWAYS

TABLES OF ELEVATIONS SPANS BIS THRU BIS

POPLAR STREET BRIDGE APPROACHES
ROADWAY "B" F 4 I RT. 70 ST. CLAIR CO. SECTION 82-3HVB

H. W. LOCHNER. INC. ENGINEERS CHICAGO. ILLINOIS

SHEET

1 BY 2 M 2 Y 7 B BY 2 M R .

D. L. DEFLECTION (FT.)

					SPAI	V B I	9									SPAN	V B 2	0				
FLOOR	L 14	L 14.5	82	82,5	83	83.5	84	84.5	85	85.5	86	86.5	87	87.5	88	88.5	89	89.5	90	90.5	91	91.5
	.000	. 204	,090	.032	, 038	036	.032	.022	.011	.003	.000	.002	.010	.021	.031	.039	.041	.038	.030	.019	.008	.001

## THEORETICAL ELEVATION TOP OF CONCRETE

GIRD. BI	452.043	452,065	452.085	452,116	452,146	452, 173	452, 199	452.223	452.245	452.264	452.282	452.298	452.312	452.324	452.335	452.343	452.349	452.354	452.356	452.357	452.355	452.352
STR.	452.683	452,700	452.718	452.749	452.783	452,809	452,831	452.855	452.881	452.900	452.914	452.930	452,949	452.960	452.966	452.975	452.986	452.989	452,988	452.989	452.992	452.988
STR.	453, 223	453, 340	453.358	453, 389	453,423	453,449	453.471	453,495	453,521	453,540	453, 554	453,570	453,589	453,600	453,606	453.615	453, 626	453, 629	453.628	453, 629	453,632	453,628
STR.	453, €3	453,980	453.998	454,029	454,063	454,089	454,111	454, 135	454.161	454,180	454, 194	454.210	454.229	454.240	454.246	454.255	454.266	454.269	454.268	454.269	454.272	454.268
GIRD. B 2	454,603	454.625	454.645	454.676	454,706	454.733	454.759	454.783	454,805	454.824	454.842	454.858	454.872	454.884	454,895	454,903	454,909	454,914	454,916	454,916	454,915	454,912

### THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION

GIRD. BI	452,043	452,069	452.106	452.149	452.185	452.212	452.231	452.245	452.256	452.268	452.282	452,301	452.323	452.346	452.367	452.382	452.391	452.392	452.386	452.376	452.364	452.354
																						452.989
STR.	453.323	453.345	453, 379	453,422	453,462	453, 487	453,503	453,517	453,533	453,544	453,554	453, 573	453,599	453,621	453,638	453, 654	453, 667	453,668	453, 658	453,548	453, 541	453.629
STR.	453,963	453.985	454,019	454.062	454, 102	454, 127	454, 143	454, 157	454,173	454, 184	454.194	454.213	454,239	454.261	454.278	454.294	454.307	454,308	454,298	454.288	454,281	454.269
GIRD. BZ	454.603	454.629	454,666	454,709	454,745	454,772	454.791	454.805	454.816	454.828	454, 542	454.861	454.883	454,906	454.927	454.942	454,951	454,952	454,946	454.936	454.924	454, 914

#### THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION - SLAB THICKNESS (7")

GIRD BI	451,460	451,486	451.523	451.566	451,601	451.628	451.648	451.662	451.673	451.685	451.699	451,717	451,739	451.762	451.783	451.799	451.807	451.809	451,803	451.793	451,781	451.770
STR.	452,100	452, 122	452,156	452, 199	452.238	452.264	452.280	452.294	452,309	452.320	452.331	452.349	452.376	452.398	452,415	452.431	452.444	452.444	452,435	452.425	452.417	452.406
STR.	452,740	452.762	452.796	452.839	452,878	452,904	452.920	452.934	452.949	452,960	452.971	452.989	453.015	453,038	453,055	453,071	453,084	453,084	453.075	453.065	453,057	453.046
STR.	453.380	453,402	453,436	453,479	453.518	453.544	453,560	453.574	453,589	453,600	453,611	453,629	453,656	453,678	453, 695	453,711	453,724	453,724	453, 715	453, 705	453, 697	453,686
GIRD. 82																						

									1	D. L. DE	EFLECTI	ON (FT.	)	- /			- III	//	Λ	-	٠,		
						SP	AN B	21	М								S	PAN B	22				
FLOOR	92	92.5	93	93.5	94	94.5	95	95.5	96	96.5	97	97.5	98	98.5	99	99.5	100	100.5	101	101.5	102	102.5	L 15
	.000	.001	.oos	.019	.030	.038	,041	.039	,031	.021	.010	.002	.000	.003	.011	.022	.032	.038	.038	.032	. 020	.004	.000

### THEORETICAL ELEVATION TOP OF CONCRETE

GIRD. BI	452.347	452.339	452.330	452.319	452.306	452,291	452.275	452.256	452.235	452.212	452.188	452.161	452.133	452, 103	452.070	452.036	452,000	451,962	451,922	451.880	451.836	451.808	451.779	
STR.	452.978	452.972	452.967	452,955	452,938	452,923	452,911	452,891	452.867	452.844	452.825	452.797	452.765	452.735	452.707	452.672	452.632	452,594	452,559	452.517	452.472	452.445	452,419	
STR.	453,618	453,612	453,607	453,595	453,578	453,563	453,551	453,531	453,507	453,484	453,465	453.437	453,405	453, 375	453.347	453.312	453.272	453.234	453, 199	453.157	453.112	453,085	453.059	
																						453.725		
GIRD. B2	454,907	454,899	454,890	454.879	454.866	454,851	454.835	454.816	454.795	454.772	454.748	454.721	454.693	454,663	454,630	454.596	454,560	454,522	454,482	454,440	454,396	454,368	454.339	

## THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION

GIRD. BI	452.347	452,341	452.339	452.339	452.337	452,330	452.316	452.295	452.267	452.234	452.198	452,164	452.133	452,106	452,082	452,058	452.032	452,000	451,961	451,913	451,857	451,812	451,779
STR.	452.978	452,973	452.976	452.975	452.968	452,962	452,953	452.931	452.899	452.866	452.835	452.800	452.765	452,738	452.719	452.694	452.664	452.632	452,597	452.550	452,493	452.449	452,419
STR.	453.618	453,613	453,616	453,615	453,608	453.602	453.593	453.571	453.539	453,506	453,475	453,440	453,405	453, 378	453, 359	453.334	453.304	453.272	453.237	453, 190	453, 133	453.089	453.059
STR.	454,258	454.253	454.256	454.255	454.248	454,242	454,233	454,211	454.179	454.146	454.115	454.080	454,045	454,018	453,999	453.974	453,944	453,912	453.877	453, 830	453,773	453,729	453.699
GIRD R2	454 mm	454 001	454 900	454 000	454 997	454 800	454 070	454 056	454 507	454 704	454 750	454 704	454 400	454 666	454.640		*** ***						

### THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION - SLAB THICKNESS (7")

GIRD. BI	451,763	451,758	451.756	451.756	451.753	451,747	451.733	451.712	451.684	451,650	451,615	451.581	451,550	451.523	451,499	451,475	451.449	451,417	451.377	451, 330	451.274	451.229	451, 196
STR.	452.395	452,390	452,393	452,391	452,385	452.379	452.369	452.347	452,315	452.282	452.252	452.216	452,181	452, 155	452, 135	452, 111	452,081	457,049	452.014	451.967	451,910	451.866	451.835
STR	453,035	453,030	453,033	453,031	453,025	453,019	453,009	452.987	452.955	452.922	452.892	452.856	452.821	452.795	452.775	452.751	452.721	452,689	452,654	452,607	452,550	452,506	452,476
STR.	453,675	453,670	453,673	453,671	453,665	453,659	453,649	453,627	453,595	453,562	453,532	453,496	453.461	453,435	453,415	453, 391	453, 361	453, 329	453, 294	453.247	453, 190	453, 146	453, 116
GIRD, B2																							

COUNTY TOTAL SHEET NO. ROUTE NO. SECTION F. A. I. -70 82 - 3 HVB ST. CLAIR 289 105 FED. ROAD DIV. NO. 4 | ILLINOIS | PROJECT

See Note 4-Sn No. 65 .

STATE OF ILLINOIS DEPARTMENT OF PUBLIC WORKS & BLDGS. DIVISION OF HIGHWAYS

TABLES OF ELEVATIONS
SPANS BI9 THRU B22

POPLAR STREET BRIDGE APPROACHES ROADWAY "B"

F. A.I.RT. 70 ST. CLAIR CO. SECTION 82-3HVB

H. W. LOCHNER. INC. ENGINEERS CHICAGO. ILLINOIS

70 of 24

ED BY ZMZ IBY VB ED BY ZMZ IED BY KA

#### DEFLECTION (FT.)

					5 P A	N 8 2	23								5 P	AN S	24					
FLOOR	L 16	L 16.5	103	103.5	104	/04.5	105	/05.5	04	06.5	107	107.5	/08	/08.5	109	109.5	110	110.5	111	111.5	112	112.5
DEP. III	.000	.004	.050	, c3g	STREET, SQUARE, THE	COMMISSION OF	OF SHAPE OF	. 299		-		-	-	.021					.090	.019	, toe	.001

#### THEGRET CAL ELEVATION TOP OF CONCRETE

GRD\_BI 69.7%

# THEORETICAL ELEVATION TOP OF CONCRETE + O.L. DEFLECTION

\$\text{GIRD. 81} \text{ 451.765} \text{ 451.765} \text{ 451.765} \text{ 451.665} \text{ 451.66

## THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION - SLAB THICKNESS (7')

GRRD 81 491.59 491.19 4

# 

### THEGRET ILL ELEVATION TOP OF CONCRETE

\$\text{GIR. BI}\$ \$\text{colored}{\pi\_1}\$ \$\text{colored}{\pi\_2}\$ \$\text{colore

### THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION

GRRD, BT 407,377 407,99 497,145 457,79 457,7

### THEORETICAL ELEVATION TOP OF CONCRETE + QL. DEFLECTION - SLAB THICKNESS (7')

6/RD 8/I 49,739 49,449 49,579 49,479 49,579

See 10 % A . Sr 110 65

STATE OF ILLINOIS
DEPARTMENT OF PUBLIC WORKS & BLDGS.
DIVISION OF HIGHWAYS
TABLES OF ELEVATIONS

F.A.I.-70 82-3HVB ST. CLAIR 289 /06

FED ROAD DIV NO. 4 ILLINOIS PROJECT

SPANS B23 THRU B26
POPLAR STREET BRIDGE APPROACHES

ROADWAY "B"

FALIST.70 ST. CLAIR CO. SECTION 82-3HVB

H W LOCHNER, INC.
ENGINEERS
CHICAGO, ILLINOIS
71 0# 24

TY RMR YB Y RMR BY KA

0 1 1 12 13 14 15 16 17 18 19 20 21 22 23 24

ROUTE NO.	SECTION	•	cou	NTY	TOTAL	SHEET NO.
F. A. I70	82-3HV	В	ST. C	LAIR	289	107
FED. ROAD DI	V. NO. 4	11	LINOIS	PROJE	T	

					SPAN	1 8 2	8										AN B										-	SPAN	R 30	-			
BEAMS	L20	20.5	124	124.5	125	/25.5	126	126.5	127	127.5	128	128.5	129	129.5	130	/30.5	131	131.5	132	132.5	133	133.5	134	134.5	135	/35.5	136	/36.5	137	137.5	/38	138.5	La
	.000	.006	021	. 031	.035	. 034	.079	.020	.010	,002	,000	.005	.015		.039	.047	.050			.027	.015	.005	.000	.002	.010	.019	.029	.034	.035	.031	.022	.007	

### THEORETICAL ELEVATION TOP OF CONCRETE

GIRD.	BI	446.428	446.338	446.248	446.110	445, 971	445.832	445.693	445,555	445,416	445.277	445, 139	445,000	444.861	444.723	444,584	444,445	444.307	444, 168	444.029	443, 891	443.752	443, 613	443,475	443, 336	443, 198	443.059	442,920	442.782	442 643	449 504	449 366	440 000	442, 167
STA	₹.	447,068	446.974	446.882	446.743	446.608	446.468	446.326	446.187	446.053	445.913	445.771	445, 632	445,498	445.359	445, 216	445.078	444.943	444.804	444,661	444,523	444, 389	444.249	444 107	447 060	442 024	112 605	442 550	442 414	442 000	40.111	****	442.200	442.807
STA	₹.	447.708	447,614	447.522	447.353	447.248	447,108	446.966	446.827	446.693	446,553	446.411	446, 272	446,138	445,999	445,856	445,718	445.583	445,444	445, 301	445, 163	445,029	444,889	444 747	444 600	*** ***	444 025	444 100	444.054	442.000	440.701	443.001	442.903	442,807
STA	۹.	448, 348	448.254	448.162	448,023	447.888	447,748	447,606	447,467	447.333	447, 193	447,051	446,912	446,778	446,639	446,496	446,358	446.223	446,084	445, 941	445, 803	445, 669	445.529	445 207	445.040		444.333	444.172	444.004	443,920	443, 781	443,641	443,543	444,087
GIRD.	B2	448.988	448.898	448,608	449,670	448.531	448.392	448.253	448.115	447.976	447.837	447,699	447.560	447.421	447.283	447, 144	447,005	446.867	446,728	446, 589	446, 451	446, 312	446, 173	446.025	445.096	445 750	445 610	445,400	445 242	445 000	445.024	444.281	444, 183	444,087

# THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION

GIRD. B	446.428	446, 345	446.270	445, 141	446,007	445.867	445,723	445,575	445,426	445,280	445, 139	445,005	444.877	444,750	444,523	444,493	444.357	444.215	444,069	443, 918	443,767	443.619	443,475	443, 339	443, 208	443, 079	442.950	449 017	442 679	440.530	440 200	440.073	400 117
STR.	447.068	446.981	446.903	446,774	446.644	446,503	446.355	446.207	446,063	445,916	445.771	445,638	445,513	445.386	445,255	445, 125	444,993	444,851	444, 701	444,551	444.404	444 955	444, 107	443 971	442 044	442 715	442 500	440.440	****	442.13	442,300	446.513	442.167
STR.	447.708	447, 621	447.543	447,414	447.284	447, 143	446, 995	446,847	446,703	446,556	446,411	446,278	446, 153	446,026	445, 895	445, 765	445, 633	445 491	445 241	445 101	445.044	****	*** ***		443,044	443,713	443.307	443,449	443, 315	449,173	443.023	442.910	442.807
STR.	448, 348	448, 251	448, 183	448.054	447 994	447 783	447 696	447 407	447 343	447 106	447 051	445 910	446 703	*** ***	446 636	446 406	445 070	*** ***	*******	140.191	445,144	444.895	****	444.011	444.484	444,355	444, 222	444.089	443,955	443.813	443,663	443,550	443, 447 444, 087
6100 0	2						447.033	447,407	447.343	447.190		440.910	440.733	440.000	440. 333	440,403	440,213	440.131	445, 981	445.831	445, 684	445.535	445.387	445.251	445, 124	444,995	444.862	444.729	444,595	444,453	444, 303	444.190	444.087
GIRD. B.	448.988	448.905	448,830	448, 701	448.567	448.427	448.283	448, 135	447, 986	447.840	447.699	447.565	447, 437	447.310	447.183	447,053	446, 917	446,775	446, 529	445.478	445 227	445 170	446 036	*** ***		*** ***	*** ***			140000000000000000000000000000000000000	0.0000000000000000000000000000000000000		

# THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION - SLAB THICKNESS (7')

GIRD. B	445.8	45 44	5.761	445.686	445,558	445,423	445, 284	445, 139	444.992	444,843	444.697	444, 555	444,422	444.293	444, 167	444,040	443,909	443,773	443.632	443, 485	443, 335	443, 184	443.035	442, 892	442.756	442.524	442,496	442, 366	442, 233	442.096	441.953	441 004	441 (00)	441.500
STR.	446.4	85 44	6. 297	446, 320	446, 191	445, 060	445, 920	446 770		445 400	44E 000	445 100	*** ***	*** 000	444 909	444 679	444 540	*** ***	*** ***		1000000													
STR.	447.7	65 44	7. 677	447,600	447, 471	447,340	447.200	447,052	445.904	446,760	446,613	446,468	446, 334	446,210	446,083	445, 952	445,822	445, 690	445, 548	445 397	445 247	445 101		******	***.	3,901	11.11	*******	443.506	4432372	443.730	443,000	4421967	442.863
GIRD. B	2 448.4	05 44	6. 321	448.246	448.118	447.983	447.844	447,699	447.552	447.403	447,257	447, 115	446.982	446.853	446.727	446,600	445.469	446, 333	446, 192	446,045	445,895	445 744	445 595	45 450	445 216	444,541		****	444 700	******	4435.075	443,720	443.607	443,503

See Note A. Sn. No. 65.

STATE OF ILLINOIS DEPARTMENT OF PUBLIC WORKS & BLDGS. DIVISION OF HIGHWAYS

TABLES OF ELEVATIONS SPANS B28 THRU B30

POPLAR STREET BRIDGE APPROACHES ROADWAY "B"

F. A.I.RT. 70 ST. CLAIR CO. SECTION 82-3HVB
H. W. LOCKNER: INC.
ENGINEERS
CHICAGO, ILLINOIS
72 08/24|

BY 2MR
Y V8
BY RM2
DBY KA

		NOI	

						SPAN	BC I									SPAN	BC 2					
FLOOR- BEAMS	12	L2.5	I	1.5	2	2.5	3	3.5	4	4.5	5	5,5	6	6.5	7	7.5	8	8.5	9	9.5	10	10.5
	.000	.005	.022	.033	.038	.038	.031	.021	.011	.003	.000	.007	.010	.021	.031	.039	.041	.038	.030	.019	.008	.001

### THEORETICAL ELEVATION TOP OF CONCRETE

GIRD. CI	451.48	451,303	451,128	450.858	450,598	450,346	450.103	449,869	449.644	449,427	449.220	449.021	448.831	448.650	448.478	448.315	448.161	448.015	447.878	447.750	447.631	447.521
STA.	451,599	451,420	451.245	450.975	450,715	450.463	450,220	449.986	449.761	449.544	449.337	449,138	448.948	448.767	448.595	448.432	448.278	448.132	447,995	447.867	447.748	447.638
STR.	451,715	451.537	451.362	451,092	450,832	450,580	450,337	450,103	449.878	449.661	449,454	449,255	449,065	448.834	448.712	448,549	448.395	448,249	448.112	447.984	447.865	447.755
57 A.	451.832	451,654	451.479	451,209	450.949	450.697	450,454	450,220	449.995	449.778	449.571	449.372	449.182	449,001	448.829	448.666	448.512	448.366	448.229	448.101	447.982	447.872
G/AD. C2	451,950	451,771	451,596	451.326	451,066	450.814	450,571	450.337	450.112	449,895	449,688	449.489	449,299	449,118	448.946	448.783	448,629	448,483	448.346	448.218	448.099	447.989

### THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION

GIRD, CI	451,482	451,309	451,150	450,892	450,637	450,384	450,135	449.891	449.655	449,431	449,220	449.029	448.842	448.672	448.510	448,354	448,202	448.053	447.909	447.770	447.640	447.523
STA.	451.599	451,426	451,267	451,009	450.754	450,501	450,252	450,008	449.772	449,548	449,337	449,146	448,959	448.789	448.627	448.471	448.319	448,170	448.026	447.887	447.757	447,640
STA.	451,716	451.543	451.384	451.126	450.871	450,618	450.369	450.125	449.889	449,665	449,454	449.263	449.076	448.906	448.744	448,588	448.436	448.287	448.143	448,004	447.874	447.757
57A.	451.832	451,660	451.501	451.243	450.988	450.735	450,486	450.242	450,006	449.782	449.571	449,380	449.193	449.023	448.861	448.705	448.553	448.404	448.260	448,121	447,991	447.874
GIAD CZ	451,950	451,777	451,618	451.360	451,105	450,852	450,603	450.359	450.123	449,899	449,688	449.497	449,310	449,140	448.978	448.822	448.670	448,521	448,377	448,238	448,108	447.991

### THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION - SLAB THICKNESS (7°)

G/90, C/	450.899	450.726	450.567	450,309	450.053	449.801	449.552	449.308	449.072	448.847	448.637	448.446	448.258	448,088	447.927	447.771	447.619	447.470	447.325	447.187	447,057	446.940
57A.	451.016	450.843	450.684	450.426	450,170	449.918	449.669	449,425	449.189	448.964	448.754	448,563	448.375	448,205	448,044	447.888	447.736	447.587	447.442	447,304	447.174	447,057
STR.	451,132	450,960	450,801	450,543	450.287	450,035	449.786	449.542	449.306	449.081	448.871	448,680	448.492	448.322	448,161	448,005	447.853	447.704	447.559	447,421	447,291	447.174
STR.	451,250	451,077	450.918	450,660	450,404	450, 152	449.903	449,659	449,423	449.198	448,988	448.797	448,609	448.439	448,278	448.122	447.970	447,821	447,676	447.538	447,408	447,291
G/RD, C2	451.367	451.194	451.035	450.777	450.521	450.269	450,020	449.776	449.540	449,315	449,105	448.914	448.726	448.556	448,395	448.239	448.087	447.938	447.793	447.655	447.525	447.408

SPAN BC 8										D.L.	DEFL	ECTIO	V (F T	1	1.0				5.10							N I	N IN I	
							S	PAN B	C 3							-			SPAN	BC 4	- A							
00, 20, 29, (60, 80, 80, 10, 10, 10, 10, 10, 00, 70, 10, 10, 10, 10, 10, 10, 10, 10, 10, 1	FLOOR	17	11,5	12	12.5	/3	13,5	14	14,5	15	15.5	16	16,5	17	17.5	/8	18.5	19	19,5	20	20.5	21	21.5	L3	V	LV		ш
		.000	.001	.008	.019	.030	.038	,041	.039	.031	.021	.010	.007	.000	.003	.011	.021	.031	.038	.038	.033	.055	.005	.000				

### THEORETICAL ELEVATION TOP OF CONCRETE

GIRD. C	44",420	447.327	447.244	447.169	447.103	447.046	446,998	446.959	446.928	446,906	446.894	446.890	446.894	446.908	446,931	446.962	447,002	447.052	447.106	447.160	447.214	447,249	447.285
575.	44".53"	447.444	447,361	447,286	447,220	447.163	447,115	447,076	447,045	447,023	447,011	447,007	447,011	447.025	447,048	447.079	447,119	447,169	447.223	447.277	447.331	447.366	447,402
574.	447,654	447.561	447,478	447.403	447.337	447.280	447,232	447.193	447,162	447,140	447,128	447,124	447.128	447,142	447,165	447,196	447,236	447.286	447.340	447.394	447,448	447.483	447,519
570.	417,77	147.678	447.595	447.520	447.454	447,397	447.349	447,310	447,279	447.257	447.245	447.241	447,245	447.259	447.282	447,313	447.353	447,403	447.457	447.511	447.565	447,600	447.636
G/90. C2	417,188	447,795	447.712	447.637	447.571	447.514	447.466	447,427	447.396	447.374	447,362	447.358	447.362	447.376	447,399	447,430	447.470	447.520	447.574	447.628	447.682	447.717	447.753

### THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION

G/90. C/	44",420	417.29	447.253	447.189	447,134	447,085	447,039	446.998	446,960	446.928	446.904	446.897	446.894	446,912	446,942	446.984	447.034	447.090	447.144	447.193	447.236	447.255	447.285
STP.	447.537	447,446	447.370	447.306	447.251	447.202	447.156	447.115	447.077	447,045	447,021	447.014	447,011	447,029	447,059	447,101	447,151	447.207	447.261	447,310	447,353	447.372	447.402
STA.	447,454	447,563	447,487	447.423	447.368	447,319	447.273	447.232	447, 194	447,162	447,138	447.131	447,128	447,146	447.176	447.218	447.268	447.324	447.378	447.427	447.470	447.489	447.519
STA.	447,777	447,580	447,604	447.540	447,485	447,436	447,390	447,349	447.311	447.279	447.255	447.248	447,245	447,263	447.293	447.335	447.385	447.441	447.495	447.544	447.587	447,606	447.636
G/80 C2	447,188	447,797	447.721	447.657	447,602	447,553	447.507	447,466	447,428	447,396	447, 372	447,365	447.362	447,380	447,410	447,452	447,502	447,558	447.612	447,661	447,704	447,723	447,753

### THEORETICAL ELEVATION TOP OF CONCRETE + D.I. DEFLECTION - SLAB THICKNESS (7.)

1445 1 2 4 2 144 17 3 3 1545 17 4 4 4 4045 17 4 4

					INE	UNETTE	ML ELE	VALIO	VIOP	Ur CU	NCHEIL	+ D.L.	DELLEC	.11014 -	JLAD !	HICKINE	33 1/-/						
G190, C1	444.83*	445.745	446.669	446,605	446.550	446,501	446.456	446.414	446.377	446.344	446.320	446,314	446,311	446.328	446.359	446,401	446,451	446.506	446.561	446,610	446.652	446.672	446.702
5 T R.	448.954	445.860	446.786	446.772	446.667	446,618	446.573	446.531	446,494	446,461	446.437	446,431	446.428	446.445	446.476	446.518	446.568	446.623	446.678	445,727	446.769	446.789	446.819
STR.																							
57 B.	447, 38	447.097	447.020	446.956	446.901	446.852	446,807	446.765	446.728	446.695	446.671	446,665	446,662	446,679	446.710	446.752	446.802	446.857	446,912	446.961	447,003	447,023	447.053
GIRD. C2	441,305	447,214	447,137	447,073	447,018	446,969	446,924	446.882	440.845	446.812	446.788	446,782	446.779	446.796	446.827	446,869	446.919	446.974	447,029	447,078	447,120	447,140	447,170

See Note A . Sn 10 65

STATE OF ILLINOIS
DEPARTMENT OF PUBLIC WORKS & BLDGS.
DIVISION OF HIGHWAYS

TABLES OF ELEVATIONS
SPANS BCI THRU BC4
PLAR STREET BRIDGE APPROACHE

POPLAR STREET BRIDGE APPROACHES
ROADWAY "C"

F. A.I.RT. 70 ST. CLAIR CO. SECTION 82-3HV8
H. W. LOCHNER INC.
ENGINEERS
CHICAGO. ILLINOIS 73 or 241

ROUTE NO. SECTION COUNTY STORAL SHEET SHEE

																														ROUTE NO	14.0	1104	COUNTY	101 SHE	TAL SP
												C	L. DE	FLECTI	ON (F	Z)															82 - 3		NOIS P		89 /
				S	PAN B	C 5				,				AN B	_								PAN	6.7		_		-							
LOOR	L4	L4.5	22	22.5	23	23.5	24	24.5	25	25,5	26	-	-	27.5	28	28.5		29.5		30.5	31	31.5	32	32.5	33	33.5	_								
	.000	.007	.017	.021	.021	.016	.008	.002	.000	.006	.016	.027	.035	.038	.095	.027	.016	.006	,000	.000	,000	.016	,081	.00	.017	.006	,500								
														VATION																					
D. CI	447.293	447.337	447.381	447.435	447,489	447.543	447.597	447.651	447.705	447.759	447,813	447.867	447,921	447.975	448,029	448,083	448,131	448.177	44.22	MAT 201	448.574	448, 359	448,132	ANIL-NOS	44.186	448,950	449,014								
TR. TR.	447,410	447,454	447.498	447.552	447,506	447.777	447.714	447.885	447.822	447,993	418,047	448.101	448.155	448.209	44,263	448.317	448.410	448.518	44.87	44.72	44,443	448,951	449,059	41.10	449.276	449,366	449,456								
TP	447,644	447,688	447.739	447.786	447.840	447,894	447.948	448.002	448.056	448.110	448.164	448.218	448.272	448.326	448,380	41.434	448.550	448.589	44.23			449.247													
D. C2	447,761	447.805	447.849	447.903	447,957	448.011	448.065	448,119	448,173	448,227	448.281	448,335	448.389	448,443	445,497	44.55	448,690	448,860	449,025	m1_975	41.37	449,543	449,714	F142-1914	450,055	450.197	450,339								
																	L. DEFL																		
D. CI	447.293	447.345	447,398	447.457	447.510	447.559	447,606	447.654	447.705	447,765	447,830	447.894	447.956	448.013	448,064	44.110	41.141	448,183	44,22	44LET.	44.32	44.575	44,757	MLC.	448.574	448,542	449.014								
TR. TR.	447,410	447,462	447.515	447,574	447.627	447.676	447.723	447.771	447.822	447,882	441,547	448,128	448.190	448.247	44.29	44.34	448,287	44.25	44.627	44.77	44.15	44,967	449,081	41, 1H	445.293	449.374	449.456								
TO		*** ***	*** 7**	447 808	447 061	447 910	447-957	448,005	448.056	448,116	448,181	448,245	448.307	448.364	448.415	44.461	448.567	448.595	441.323	44.1	445.117	449.253													
D C2	447.761	447.813	447.866	447.925	447.978	448.027	448.074	448,122	448.173	448,233	418,798	448,362	448,424	448,481	41,52	44.571	41,76	448,857	449,000	145,258	41.31	449,559	49,72	wi)_\$X	450,072	450,205	450,339								
								THEO	RETICAL	LELEV	ATION	TOP C	F CON	RETE +	aL. D	<b>EF</b> LECT	10N - SL	AB TH	ICKNES	(2)															
	446,710	446.762	446.815	446.874	446.927	446.976	447.023	447,070	447.122	47.182	447.245	447.311	447.373	447,430	447,481	47.27	417,564	447.60	47,639	41.91	41,73	47,72	447,843	MT 885	41,890	447,950	448,431								
R.	446.827	446.879	446,932	446,991	447,044	447.093	447.140	447, 187	447.239	447.299	447,363	47,428	447,490	447.547	447,715	47,761	417.704 417.844	47.171	448,043	641. 154	448.259	441.384	441,417	WH_HER	448.710	448.791	448.873								
R.	447,061	447,113	447,166	447.108	447,278	447.327	447.374	447.421	447.473	447.533	47,597	47,662	447.724	447.781	47.12	47,878	447.983	448,113	449,244	wi. X	44.52	448,580	44,85				449,314								
	447,178	447.230	447.283	447.342	447.395	447,444	447,491	447,530	447,590	447,650	447,714	447,779	447,841	447,896	447,949	41,995	44,123	448.284	44,44	₩1.Q1	44.79	w.rs	41. 2	M1.27	445,485	449.622	449,756								
000					SPAN	C 8				447,690	447,714	447,779	447.841 2. L. D. 5.P.A	FLECTV	47.541 ON (FT	47,990	44, 123	41.294		) A		4.5	949,7 <del>2</del>	2 0	245,485	11			N	ı	Y	,			
000		447.230 LG.5	34		SPAN			36.5	447,590	447,650	447,714	447,779	47,61 0. L. D. 5 P.A 39	#7.86 E F L E C T // N C S	0N (FT.	40.5	44,123	41.5	42	42.5	43	43.5	PAN 44	1 C 44.5	45	45.5	5 47	0	Ν	IL	Y	7			
200				34.5	35	C 8				447,690	447,714	447,779	447.841 2. L. D. 5.P.A	FLECTV	47.541 ON (FT	47,990	44,123	41.294		) A	43	43.5	PAN 44	2 C 44.5	245,485	45.5	5 47	0	Ν	IL	Y	,			
OOR AMS	.000	L6.5	.016	34.5	35 .021	C 8 35.5	36	36.5	37	37, 5	38 .016	38.5 .027	47,41 2 L. D. 5 P.A 39 .035	VATION	0N (FT.	40.5 .007	44.123 4/ .016	41,5	42	42.5	43	43.5 43.5	PAN 44	2 C 44.5	45	45.5	5 4.7	0	N		Y	,			
OCR AMS	L6 .000	LG.5	34 .016	34.5	35 .021	C 8 35.5	36	36.5 .oog	37	37.5	38 .016 THE	38.5 .027 ORETIC	47,641  2. L. D. 5 P.A. 39  .035  AL ELE	447.890  EFLECT/ N C : 39.5  .008	47,349 ON (FT. 9) 40 .036	40.5 .027	44,123 41 ,016 CRETE 449,243	41,5	42,343	42.5	43 .014	43,495	649,142	C C 44.5	45	45.5	5 L 7 .000	0	N	L	Y	7			
D. CI	448,583 449,034 449,484	448.610 449.084	34 .016 448.636 449.135 449.635	34.5 .021 448.670 449.201 449.735	35 .021 448.704 449.205	C 8 35.5 .016 448.737 449.332 449.935	36 .009 448.777 449.390 450,005	36.5 .00g 448.821 449.435 450.053	37 .000 448,866 449,479 450,099	37.5 .006	3.6 .016 THE 443,958 443,579	36.5 .087 ORETIC 449,004 449,626 450,853	447,841  2. L. D. S.P.A.  3.9  .035  AL ELE 449,051 449,672 450,299	### ATTION 449,098 449,721 450,350	0N (FT. 9) 40 .035 .035 .035 .035 .035 .035	40.5 .027 OF CON 449.194 449.823 450.456	44,123 .016 CRETE 449,243 449,870 490,504	41,5	449,343 449,343 450,632	42.5 .728 .41.301 .41.301	43 .004	449,495 450,785	#49,547 #49,547 #30,184 #30,184	C C 44.5	45, 652 45, 652 450, 287 450, 827	45.5	5 L7 .000	0	N		Y	/			
D. CI	448.583 449.034 449.484 449.935	448.610 449.084 449.559 450.034	3.4 ,016 448,636 449,135 449,635 450,135	34.5 .021 448.670 449.201 449.735	35 .021 448.704 449.205 449.833 450.401	C 8 35.5 .016 448.737 449.332 449.935 450.537	36 .009 448.777 449.390 450.005	36.5 .00g 448.621 449.435 450.053 450.671	37 .000 448,856 449,479 450,099 450,719	37.5 ,006 448,912 449,527- 490,149 450,771	3 &	447,779  38.5 .087  ORETIC  449,004  449,626  450,853  450,879	447,841  2. L. D.  5. P.A.  3.9  .035  AL ELE  449,051  449,672  450,299  450,997	### ATTION 449,098 449,721 450,350 450,980	47,949  ON (FT.  9  40  .035  TOP ( 49,146 49,175 450,406 451,037	40.5 .087 .087 .087 .087 .089.194 .49.182 .49.182 .49.182	44, 123  4/ .016  CRETE 449,243 449,870 450,504 451,137	445,294 445,293 449,293 449,293 450,996 451,191	449,343 449,343 450,812 451,244	42.5 .728 .41.301 .65.26 .65.361	445, 444 450, 574 450, 712 451, 345	449,495 450,127 450,785 450,785 451,403	#49,547 430,781 430,784 430,784 431,481	# 1 0   44.5   221   44.5   221   44.5   221   45.5   221   45.5   221   45.5   221   45.5   231   231   45.5   231	445, 455 .017 445, 652 450, 287 450, 597 451, 556	45.5 , , , , , , , , , , , , , , , , , , ,	5 L7 .000	0	N	L	Y				
D. CI	448.583 449.034 449.484 449.935	448.610 449.084 449.559 450.034	34 ,016 448,636 449,135 449,635 450,135	34.5 .021 448.670 449.201 449.735	35 .021 448.704 449.205 449.833 450.401	C 8 35.5 .016 448.737 449.332 449.935 450.537	36 .009 448.777 449.390 450.005	36.5 .00g 448.621 449.435 450.053 450.671	37 .000 448,856 449,479 450,099 450,719	37.5 ,006 448,912 449,527- 490,149 450,771	3 &	447,779  38.5 .087  ORETIC  449,004  449,626  450,853  450,879	447,841  2. L. D.  5. P.A.  3.9  .035  AL ELE  449,051  449,672  450,299  450,997	### ATTION 449,098 449,721 450,350 450,980	47,949  ON (FT.  9  40  .035  TOP ( 49,146 49,175 450,406 451,037	40.5 .087 .087 .087 .087 .089.194 .49.182 .49.182 .49.182	44,123 .016 CRETE 449,243 449,870 490,504	445,294 445,293 449,293 449,293 450,996 451,191	449,343 449,343 450,812 451,244	42.5 .728 .41.301 .65.26 .65.361	445, 444 450, 574 450, 712 451, 345	443,495 443,495 450,127 450,755 451,403	#49,547 430,781 430,784 430,784 431,481	# 1 0   44.5   221   44.5   221   44.5   221   45.5   221   45.5   221   45.5   221   45.5   231   231   45.5   231	445, 455 .017 445, 652 450, 287 450, 597 451, 556	45.5 , , , , , , , , , , , , , , , , , , ,	5 L7 .000	0	N	IL	Y				
OOR EAMS	448.583 449.034 449.484 449.935	448.610 449.084 449.559 450.034	34 ,016 448,636 449,135 449,635 450,135	34.5 .021 448.670 449.201 449.735	35 .021 448.704 449.205 449.833 450.401	C 8 35.5 .016 448.737 449.332 449.935 450.537	36 .009 448.777 449.390 450.005	36.5 .00g 448.621 449.435 450.053 450.671	37 .000 448,856 449,479 450,099 450,719 451,348	37.5 .006 448,912 449,527 420,149 450,771 451,402	3.6 .016 .016 .016 .016 .016 .019 .019 .019 .019 .019 .019 .019 .019	38.5 .027 ORETIC 449.004 449.626 450.253 450.879 451.510	447,641  2 L. D.  5 P.A  39  .036  AL ELE  449,051  449,672  450,299  450,997  451,564	### ##################################	0N (FT. 9) 40 .095  TOP (6) 449,146 449,775 450,406 451,677	40.5 .007 .007 .007 .007 .007 .007 .007	44, 123 47 .016 CRETE 449,243 449,870 450,700 451,737 451,780	449.293 449.293 449.293 449.293 450.956 451.191 451.834	449, 340 449, 340 449, 375 450, 810 451, 244 451, 488	42.5 .728 .41.301 .65.26 .65.361	445, 444 450, 574 450, 712 451, 345	443,495 443,495 450,127 450,755 451,403	#49,547 430,781 430,784 430,784 431,481	# 1 0   44.5   221   44.5   221   44.5   221   45.5   221   45.5   221   45.5   221   45.5   231   231   45.5   231	445, 455 .017 445, 652 450, 287 450, 597 451, 556	45.5 , , , , , , , , , , , , , , , , , , ,	5 L7 .000	0	N	IL	Y				
OGR EAMS PD. CI TR. TR. TR.	448,583 449,034 449,484 449,935 450,385	448,610 449,084 449,559 450,034 450,510	3.4 .016 446.636 449.135 449.635 450.636	34.5 .021 448.670 449.201 449.735 450.866	35 .021 448.704 449.265 449.830 450,401 450,977	C 8 35.5 .016 448.737 449.332 449.935 450.537 451.146	36 .009 448.777 449.390 450.005 450.621 451.240	36.5 .002 448.821 449.435 450.653 450.671 451,294	448,856 449,479 450,099 450,719 451,348	37.5 .008 448,912 449,927- 490,149 490,771 451,472	38 .016 THE 449,998 449,579 450,898 451,498	36.5 .027 ORETIC 449.004 449.026 450.253 450.879 451.510	447,641  2 L. D.  5 P.A  39  .036  AL ELE  449,051  449,672  450,299  450,299  710N T	### A 10 - 10 - 10 - 10 - 10 - 10 - 10 - 10	ON (FT. 9) 40 40 40,145 449,175 450,406 451,037 451,672	40.5 .087 .087 .087 .089 .49.823 .451.089 .451.726	44, 123  47  .016  CRETE  449,243  449,870  451,137  451,780	449,290 449,290 449,290 450,596 451,191 451,894	449,340 449,340 449,379 450,410 451,244 451,1888	42.5 .008 46.30 65.36 65.46 65.46 65.46	445, 444 450, 474 450, 474 450, 773 451, 349	449,495 449,495 450,127 450,785 451,403 452,050	#49,547 #49,547 #50,884 #50,883 #51,#45	48.50 44.5 48.50 48.50 48.50 48.50 48.50 48.50	45,485 .017 45,652 450,287 450,566 450,566	45.5 ,,,,,,,,	5 449,740 66 449,740 62 450,380 72 451,000 11 451,660 6 452,300	0	N	IL	Y				
OOR CITTR. TR. TR. RD. C2	448.583 449.034 449.484 449.935 450.385	448,610 449,084 449,559 450,034 450,510	3.4 .016 448.636 449.135 449.635 450.135 450.636	34.5 .021 448.670 449.201 449.735 450.806	35 .021 448.704 449.265 449.833 450,401 450,977	C 8 35.5 .016 448.737 449.332 449.935 450.537 451.146	448,777 449,390 450,005 450,621 451,240	36.5 .002 448.821 449.435 450.053 450.671 451,294	448,856 449,479 450,099 450,719 451,348	448,912 449,927 450,149 450,771 451,472 THEO RE 448,918	36 .016 THE 449,929 490,920 490,828 451,439 451,439	447,779  36.5  .007  ORETIC  449,024  450,253  450,879  451,510  ELEVA  449,031	447,641  2. L. D.  S.P.A.  3.9  .036  AL ELE  449,051  449,057  450,299  450,997  451,564	417.896  EFLECTV  N C 3  39.5  .098  EVATION  449.098  449.721  450.396  451.618  CP CF  449.136	0N (F7. 9 40 .035 109 6 49,145 49,175 450,405 451,037 451,672	40,5 .027	449,243 449,243 449,870 450,564 451,137 451,780	449,293 449,293 449,293 449,293 451,193 451,834 451,834	449,343 449,375 450,812 451,244 451,288	42.5 .708 46.30 65.36 65.36 65.36	445, 444 450, 574 450, 574 450, 712 451, 996	449,495 450,127 450,785 450,785 451,400 452,790	#49,547 449,547 490,784 490,820 451,441 452,704	48.45 48.45 48.47 48.47 48.47 48.47 48.47	445,485 .017 445,652 450,287 450,566 450,566	45.5 , , , , , , , , , , , , , , , , , , ,	5 49,740 6 49,740 6 451,960 7 451,660 6 452,900	0	N	IL	Y				
OGR CITR. TR. TR. CRD. C2 CTR. TR. CTR. CTR. CTR. CTR. CTR. CTR.	448.583 449.034 449.484 449.935 450.385	448.610 449.084 449.539 450.034 450.510	3.4 .016 449.135 449.635 450.636 448.652 449.151	34,5 .021 448,670 449,201 449,730 450,806	35 .021 448,704 449,265 449,833 450,401 450,977 448,725 449,286	C 8 35.5 .016 448.737 449.332 449.935 450.537 451.146	36 .009 448.777 449.390 450.005 450.621 451.240	36.5 .00g 448.821 449.435 450.653 450.671 451.294 448.824 449.438 450.056	448,856 449,479 450,099 450,719 451,348 448,856 449,479 450,099	448,912 449,927 490,149 490,711 451,472 THEORE 449,533 490,156	3.6 .016 THE 443,908 449,179 450,803 450,803 450,803 450,408 450,408 450,408 450,803 450,803 450,803 450,803 450,803	447,779  36.5 .087  ORETIC 449,004 449,626 450,859 451,510  ELEVA 449,031 449,654 450,280	447,641  2 L. D.  S P A  39  .035  AL ELE  449.051  449.057  450.927  451.964  TION T  449.066  449.070  450.305	417.896  EFLECTV  N C 3  39.5  .098  EVATION  449.098  449.721  450.980  CP CF  449.136  449.759  449.759	447,569 ON (FT)  109 140 .099 450,144 449,175 450,405 449,167 449,161 449,161 449,161	40.5 .007 .007 .007 .007 .007 .007 .007	444,123  47  .016  CRETE  449,243  449,870  450,504  451,137  451,780  D. L. DEF6  449,880  450,580	449.293 449.293 449.293 449.293 450.396 451.191 451.834 451.299 449.297 449.299	449,343 449,375 450,812 451,244 451,248 451,248 451,488	42.5 .508 46.301 46.361 46.361 46.361 46.361	445, 454 450, 074 450, 074 451, 349 451, 349 450, 583 450, 583 450, 781	449,495 449,495 450,127 450,785 451,403 452,090	#49,547 #40,547 #50,184 #50,184 #50,184 #51,441 #51,441 #51,441 #51,441 #51,441	44.50 44.5 46.50 4	445, 655 450, 951 450, 951 450, 951 451, 566 452, 212 445, 665 450, 364	449,69 480,39 480,39 451,61 482,25	5 L7 .000  5 449.740  2 450.386  4 450.366  4 450.366  4 450.366  4 450.366  4 450.366	0	N		Y				
OCR SEAMS  PD. CI TR. TR. PD. C2  PD. C1 TR. TR. TR. TR. TR. TR.	448.583 449.034 449.034 449.385 450.385	448,610 449,084 449,084 450,530 450,510 448,616 449,089 450,650	34 .016 448,636 449,135 449,635 450,636 448,632 449,551 449,551	34.5 .021 448.670 449.201 449.735 450.269 450.806 449.692 449.757 450.291	35 .021 448,704 449,265 449,833 450,401 450,977 448,725 449,886 449,886 449,886	C 8 35.5 .016 448.737 449.332 449.935 450.537 451.146 448.754 449.939 449.939 449.939	36 .009 448,777 449,390 450,005 450,621 451,240 448,786 449,015 450,630	36.5 .00g 448.621 449.435 450.653 450.671 451.294 449.438 450.656 450.674	448,856 449,479 450,099 450,719 451,348 448,856 449,479 450,099 450,719	448,912 449,527- 490,149 490,771 451,472 THECRE 449,153 490,153 490,178	36 .006 THE 449,929 450,920 450,920 450,920 450,920 450,920 450,920 450,920 450,920 450,920 450,920	447,779  36.5 .027  0 RETIC 449,026 450,253 450,253 451,510  ELEVA 449,031 449,654 450,906	447,641  2 L. D.  SPA  39  .036  AL ELE 449,051 449,672 450,299 450,927 451,564  TION T 449,086 449,707 450,335 450,362	447, 898  EFLECT/ N C 3  39,5  .098  EVAT/ON  449,098  450,390  451,618  CP CF  449,136  449,759  450,389	447, 348  ON (F7.7)  40  .095  40, 146  449, 146  451, 077  449, 141  449, 141  449, 141  449, 141  449, 141	40.5 .087 .087 .087 .087 .087 .087 .087 .087	449,243 490,504 491,137 451,780 0.L. DEFE 449,280 449,887 451,154	449,293 449,293 449,293 451,191 451,1294 451,299 449,299 449,297 451,197	449,343 449,375 450,813 451,244 451,488 449,343 449,343 451,244	42.5 , 02: 45.30 45.24 45.60 45.30 45.30 45.30 45.30 45.30	445, 444 450,074 450,712 451,349 451,990 445,452 450,083 450,751 451,358	449,495 450,127 450,765 451,403 452,090 449,518 450,143 450,143	#49,567 #49,567 #49,567 #49,663 #49,563 #49,563 #49,563 #49,563 #49,563	40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6	465, 022 - 007 - 0	45.55 .00 449.69 450.33 450.47 450.47 450.47 450.47 450.47 450.47 450.47	5 2.7 ,000 66 449,746 62 451,020 71 451,660 72 451,060 73 451,660 74 449,746 74 449,746 74 451,660 74 451,660 75 451,660 76 451,660 77 451,660 77 451,660	0	N	ee No	Υ				
D. CI FR. D. CZ	448.583 449.034 449.034 449.385 450.385	448,610 449,084 449,084 450,530 450,510 448,616 449,089 450,650	34 .016 448,636 449,135 449,635 450,636 448,632 449,551 449,551	34.5 .021 448.670 449.201 449.735 450.269 450.806 449.692 449.757 450.291	35 .021 448,704 449,265 449,833 450,401 450,977 448,725 449,886 449,886 449,886	C 8 35.5 .016 448.737 449.332 449.935 450.537 451.146 448.754 449.939 449.939 449.939	36 .009 448,777 449,390 450,005 450,621 451,240 448,786 449,015 450,630	36,5 .002 449,621 449,435 450,631 450,631 451,294 449,438 450,056 450,674 451,296	37 .000 448,856 449,479 450,099 450,719 451,348 448,866 449,479 450,099 450,719 451,348	37, 5 ,004 448,912 449,527 450,771 451,402 449,533 449,533 449,533 450,154 451,402	36 .296 .296 .485,599 .495,893 .495,893 .495,893 .495,893 .495,893 .495,893 .495,893 .495,893 .495,893 .495,893 .495,893	36.5 .007 .007 .007 .007 .007 .007 .007 .0	39 .095 AL ELEE 449,091 449,097 450,299 450,997 451,564 449,707 449,085 449,707 451,599	VATION 449,096 449,791 449,096 441,611 449,199 441,196 449,196 449,196 449,196 449,196 449,196 449,196 449,196 449,196 449,196 449,196 449,196 449,196	447, 548  ON (FT)  ON	40.5007  40.5007  40.507  40.408  40.408  40.408  40.408  40.408  40.408  40.408  40.408  40.408	44,123  27  .016  43,243  431,275  451,786  451,776  451,776  451,776	449,293 449,293 449,293 449,293 451,193 451,193 451,294 451,294 451,340	449,343 449,343 449,343 451,244 451,244 451,244 451,244 451,244 451,244 451,244 451,244 451,244 451,244	42.5 (41.30) 42.5 (41.30) 45.50 45.50 45.50 45.50 45.50 45.50 45.50 45.50 45.50 45.50 45.50	445, 444 450,074 450,712 451,349 451,990 445,452 450,083 450,751 451,358	449,495 450,127 450,765 451,403 452,090 449,518 450,143 450,143	#49,567 #49,567 #49,567 #49,663 #49,563 #49,563 #49,563 #49,563 #49,563	40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6000 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.600 40.6	465, 022 - 007 - 0	45.55 .00 449.69 450.33 450.47 450.47 450.47 450.47 450.47 450.47 450.47	5 2.7 ,000 66 449,746 62 451,020 71 451,660 72 451,060 73 451,660 74 449,746 74 449,746 74 451,660 74 451,660 75 451,660 76 451,660 77 451,660 77 451,660	0				TE OF	ILLI BLIC W	VORKS	å BL
D. CI FR. D. CZ D. CI FR. TR. D. CZ	L6 .000 448,583 449,034 449,484 449,935 450,385 448,583 449,583 450,385	449,610 449,04 449,084 450,034 450,030 449,089 449,089 449,055 450,040 450,516	3.4 .016 449,636 449,135 450,636 449,636 449,631 449,631 449,631	448,6726 449,201 449,201 450,269 450,866 449,735 449,737 449,737 450,828	448,704 449,265 449,265 449,833 450,401 449,285 449,285 449,285 449,285 449,285 449,285 449,285	C 8 35.5 .016 448,737 449,332 449,935 450,537 451,146 449,734 449,734 449,734 449,734 449,734 449,734 449,734 449,734	36 .009 448,777 449,390 449,390 440,493 441,399 440,015 440,015 450,620 451,240	36.5 5 .00g 448,821 449,435 450,631 450,631 450,631 450,631 450,631 450,631 450,631 450,631 450,631 450,631 450,631 450,631 450,631 450,631 450,631 450,631	37 .000 448,806 449,479 450,719 451,348 448,866 449,479 450,719 451,348	37,5 ,006 448,912 449,527 450,771 451,402 469,533 449,533 449,533 450,176 451,402	38	36.5 .007 .007 .007 .007 .007 .007 .007 .0	30 .036 .036 .036 .036 .036 .036 .036 .0	447,888  N C 39,5  .098  449,791  450,390  451,616  451,616  451,616  451,656  CRETE 1	447, 569  ON (FT)  ON	40,50 .007 .007 .007 .007 .007 .007 .007 .0	44, 123  47  .016  492,435  451,137  451,786  451,876  451,876  451,876  451,876  451,876  751,076  751,076  751,076  751,076  751,076	449,293 449,293 449,293 449,293 451,193 451,193 451,193 449,299 449,297 441,197 451,197 451,197	449,343 449,343 449,343 451,888 451,888 451,888 449,343 449,343 449,343 441,348 441,348 441,348 441,348 441,348 441,348	42.5 .002 45.30 45.26 45.60 45.30 45.30 45.30 45.30 45.30 45.30 45.30 45.30 45.30 45.30 45.30 45.30	46,450 46,450 46,070 46,070 46,450 46,450 46,450 46,450 46,450 46,450 46,450 46,450 46,450	23.5 .016 45.495 45.00 45.405 45.405 45.405 45.405 45.405 45.405 45.405	#49,192 #49,597 #49,597 #49,597 #49,598 #49	#8.800 #8.800 #8.100 #8.100 #8.100 #8.100 #8.100 #8.100 #8.100 #8.100 #8.100 #8.100 #8.100 #8.100	45,489  45,121  45,121  45,121  45,121  45,156  45,111  45,166  45,166  45,166  45,166  45,166	45.5 .00 .49,69 .450,33 .450,97 .451,61 .452,25 .450,34 .450,37 .451,61 .452,25	17 .000 16 449,741 .000 17 .000 18 449,741 .000 18 449,741 .000 18 449,741 .000 18 449,741 .000 18 449,741 .000 18 449,741 .000	0		DEPART	STA MENT O DIVISI	TE OF	F ILLI BLIC W F HIG	VORKS HWAYS VATIO	S
D. CI D. CI TR. D. C2 TR. TR. TR. TR. TR. TR. TR.	L6 .000 446,593 449,034 449,935 449,036 449,935 449,933 449,933 449,934 449,934	LG.5 5 .005 .446.610 .449.084 .449.529 .450.034 .450.510 .449.661 .449.089 .449.565 .450.040 .450.516 .449.089	3.4 .016 448,636 449,135 450,135 450,636 448,632 449,151 449,651 449,653 449,653	448,670 449,705 449,705 450,769 440,755 440,222 449,757 450,229 440,222 440,757 450,291 450,628	35 PAN 35 .001 448,704 449,265 449,833 450,401 450,977 448,725 449,286 449,854 450,492 449,854 450,978 448,142 450,998	C 8  35.5  .016  448,737 449,335 450,537 451,146  448,754 449,349 449,952 450,537 451,146	36 ,009 448,777 449,390 450,005 450,621 451,240 449,399 450,015 450,630 451,249	36.5 .00g 449,421 449,423 540,033 450,031 451,234 451,234 451,236 451,	37 .000 448,856 449,479 450,099 450,779 451,348 448,856 449,479 450,099 450,779 451,348 451,348 451,348 451,478 451,348	37, 5 .004 440,912 440,527 450,149 450,771 451,402 450,752 450,156 450,772 450,156 450,772 451,402	36 .096 .096 .096 .491,079 .491,479 .491,479 .491,479 .491,479 .491,479 .491,479 .491,479	461,779  36.5 .087  CRETIC  449,026 450,289 450,879 451,510  ELEVA 450,280 450,280 450,280 450,280 450,280	2 L. 0 SPA 39 .035	447,888  EFLECTIVATION  39,5  .008  490,099  440,099  440,104  440,709  441,018  CP CF  441,018  CRETE + 448,553	447, 548  ON (FT)  100  .095  400  .095  449, 144  449, 775  450, 407  451,	40,5 ,007 40,5 ,007 40,134 401,203 401,009 401,009 401,009 401,009 401,009 401,009 401,009 401,009 401,009 401,009 401,009 401,000 401	44, 123  47  .016  49, 243  49, 243  49, 150  40, 150  40	449,293 449,293 449,293 449,293 450,193 451,193 451,193 451,193 451,193 451,193 451,194 451 451 451 451 451 451 451 451 451 45	443, 243 443, 273 443, 274 451, 284 451, 284 451, 284 451, 284 451, 284 461, 284 471, 288	42.5 , 722 451,352 451,454 451	48,450 45,178 46	48,495 45,195 45	#49,547 #49,547 #49,547 #49,548 #49	#1.50 #1.50 #1.50 #1.50 #1.50 #1.50 #1.50 #1.50 #1.50	445,485  445,485  445,485  445,485  450,287  450,287  450,356  450,356  450,356  450,356  450,356  450,356	45.5 45.5 45.33 450.33 450.43 451.61 450.34 450.34 450.34 450.34 450.34	5 L7 7 .000  6 449,747  7 .000  6 449,747  6 450,366  6 450,367  6 450,366  6 450,366  6 450,366  6 450,366  6 450,366	0		DEPART T.	STA MENT O DIVISI A B L E S SPA	TE OF	F ILLI BLIC W F HIG ELEV 5 THRU	VORKS HWAYS VATIO	s NS
OCR EAMS  OCC TR.  TR.  TR.  TR.  TR.  TR.  TR.  TR.	L6 .000 448,583 449,034 449,484 449,935 449,034 449,935 449,034 449,935 449,034 449,935	449,610 449,084 450,034 450,034 450,036 449,089 449,089 449,089 449,089 449,089 449,089 449,089 449,089	3.4 ,016 440,636 449,135 449,635 450,636 448,637 449,631 449,631 449,631 449,631 449,631	448,672,701 449,705 450,709 450,709 450,806 440,602 440,707 450,209 450,806 440,602 440,400 440,400 440,400 440,400	35 PAN 35 .001 .001 .001 .001 .001 .001 .001 .00	26 8 35.5 .016 448,737 449,325 449,935 4451,164 451,170 448,170 448,170 448,170 448,170 448,170 648,17	36 .009 448,777 449,200 50,621 451,240 448,786 449,399 450,620 451,240 451,240	36,5 ,00g 449,435 449,435 450,631 451,234 451,234 451,236 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	37 .000 448,856 449,479 450,099 450,719 451,348 448,856 451,713 451,348 448,856 451,713 451,348	37, 5 .006 444,912 449,527 450,149 450,771 451,422 7HECR2 449,535 450,156 449,535 450,156 450,	38	467,779  36.5 .007  49,704  49,704  49,004  490,009  491,010  70P  449,007  449,007  449,007	39 .036 .036 .036 .036 .036 .036 .036 .036	447,986  FLECT TO S  33,5  .098  449,096  449,096  449,196  449,196  441,018  650,080  660,08	447, 548  ON (F7)  ON	40.5 .007 .007 .007 .007 .007 .007 .007	44, 123  47  .016  CRETE 493,243 493,195 493,196 493,197 493,196 493,197 493,196 493,197 493,196 493,197 493,197 493,197 493,197 493,197 493,197 493,197	449,291 449,291 449,291 450,595 451,191 451,193 451,197 450,592 451,197 451,197 451,197 451,194 451,197 451,490 451,497 451	443,343 449,375 451,244 451,244 451,244 451,244 451,244 451,244 451,244 451,244 451,244 451,244 451,244 451,244	42.5 .000 40.300	48,450 194 48,450 194 450,194 450,196 450,196 450,196 450,196 450,196 450,196 450,196	449,495 449,495 450,197 450,197 450,197 451,403 450,197 450,197 450,198 450,19	#46,572  #46,572  #46,573  #46,573  #46,573  #46,573  #47,473  #47,473  #47,473  #48,583  #48,583  #48,583  #48,583  #48,583	#1.80 #1.60 #1.00	445,485 445,485 445,485 450,287 450,287 450,287 450,256 450	449,09 449,09 450,37 451,61 450,37 451,61 450,37 451,61 450,26 449,75 449,75	5 L7 7 .000  6 449,747  7 .000  6 449,747  6 450,366  6 450,367  6 450,366  6 450,366  6 450,366  6 450,366  6 450,366	0		DEPART T.	STA MENT O DIVISI A BLES SPAN	TE OF	F ILLI BLIC W F HIG ELEV 5 THRU	VORKS HWAYS VATIO U CIO	s NS
RD. CI STR. RD. CZ	L6 .000 445,503 449,035 449,035 450,385 469,385 469,484 449,335 469,484 449,335 449,484 449,335	449,610 449,094 449,093 450,034 450,036 449,565 450,040 449,065 450,040 449,065 449,065	34 ,016 449,135 449,035 450,135 450,135 449,631 449,631 449,632 449,063 449,063	448,670 449,751 449,752 449,752 449,752 449,752 449,757 450,258 448,632 449,757 448,632 449,757 449,757	35 PAN 35 .021 449,704 449,205 449,834	C 8 35.5 .016 446,737 449,335 450,537 451,146 446,754 445,499 450,557 446,766 449,767	36 .009 448,777 449,390 450,005 450,025 449,399 450,015 450,620 448,203 448,203 448,203 448,203 448,203 448,203 448,203	36,5 ,00g 449,821 449,435 450,033 450,671 451,294 451,294 451,296 451,296 451,296 451,494 451,296 451,494 451,496 451,	37 .000 449,479 450,099 450,719 451,348 449,479 450,099 450,099 450,719 451,248 449,251 448,251 448,251 449,516 450,516	444,312 449,527 450,149 446,318 446,318 446,318 446,318 446,318 446,318 446,318 446,318 446,318 446,318 446,318	3 8	36.5 .027 .027 .027 .027 .027 .027 .027 .027	447,841  3. L. D. S. P. A. 3.9  .036  AL ELLE 449,051 449,672 451,564 450,395 469,385 469,385 469,385 469,385 469,385 469,385 469,385	447,886  FLECT N C S  39.5  .098  449.098  449.178  449.178  449.178  449.178  449.178  449.178	447, 348  ON (F7.7)  10  40  400  400  400  400  400  400	40,5 COA 40,196  40,5 F COA 40,194  40,195  40,195  40,195  40,195  40,195  40,195  40,195  40,196  40,196  40,196  40,196  40,196  40,196  40,196  40,196  40,196  40,196  40,196  40,196  40,196  40,196  40,196  40,196	44, 123  47  .016  49, 243  49, 243  49, 150  40, 150  40	444,294 449,293 450,556 451,191 450,295 449,297 440,299 441,197 451,184 451,184 451,184 461	449,343 490,375 490,375 491,244 491,243 491,244 491,244 491,243 491,244 491,244 491,244 491,244 491,245	42.5 .002 45.303 45.204 45.303 45.304 45.305 45.304 45.305 45.304	443,444 450,174 450,174 450,174 450,179 451,199 451,199 451,199 451,199 451,199 451,199 451,500	443,492 450,191 443,492 450,192 443,493 450,193 443,493 450,193 443,59	#49,547  490,519  490,519  490,620  490,620  490,620  490,620  490,620  490,620  490,620  490,620	#1.00 #1.00 #1.00 #1.00 #1.00 #1.00 #1.00 #1.00 #1.00 #1.00 #1.00	445,489  45,100  460,100  460,100  460,100  460,100  460,100  460,100  460,100  460,100  460,100  460,100  460,100  460,100  460,100  460,100  460,100	449,19 450,33 450,37 450,47 450,47 450,25 450,27 450,27 450,27 450,27 450,27 450,27 450,27 450,27 450,27	2 L7 7 .000  449,740	0	E	DEPART T.	STA MENT O DIVISI A BLES SPAN	TE OF	F ILLI BLIC W F HIG ELEV 5 THRU RIDGE AY "C	YORKS HWAYS ZATIO U CIO E APP	S NS ROAC

RMR ST

ROUTE NO.	SECTION	•	cou	NTY	TOTAL	SHEET NO.
F. A. I70	82-3HV	В	ST. C	LAIR	289	110
FED. ROAD DE	V. NO. 4	- 11	LLINOIS	PROJEC	T	-

					SPA	N CI	2									S P	AN	: 13					T	-			SP	AN C	14				
FLOOR BEAMS	L 10	L 10.5	46	46.5	47	47.5	48	48.5	49	49.5	50	50.5	51	51.5	52	52.5	53	53.5	54	54.5	55	55.5	56	56.5	57	57.5	58	58.5	59	59.5	60	60.5	LII
	.000	.005	.020	.031	.035	.035	.029	.020	.010	.002	.000	.005	.015	.027	.039	.047	.050	.047	.039	.027	.015	.005	.000	.002	.010	.020	.029	.035	.035	.030	.019	.004	.000

### THEORETICAL ELEVATION TOP OF CONCRETE

### THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION

## THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION - SLAB THICKNESS (7)

See Note A - Sh No. 65.

STATE OF ILLINOIS
DEPARTMENT OF PUBLIC WORKS & BLDGS.
DIVISION OF HIGHWAYS

TABLES OF ELEVATIONS
SPANS CIZ THRU CI4
POPLAR STREET BRIDGE APPROACHES

ROADWAY "C"
F. A. I. RT. 70 ST. CLAIR CO. SECTION 82-3HVB

H. W. LOCHNER, INC.
ENGINEERS
CHICAGO, ILLINOIS
SECTION 82-SIVE
SHEET
FOR STREET
FOR STR

2 2 M R 7 E 2 M R

 $\frac{1}{1} + \frac{1}{2} + \frac{1}{10} +$ 

	00	11	04.3	SECTION	COUNTY	SHEETS	SHEET NO.
F.	4	:	-70	82-3HV8	ST. CLAIR	789	///
	7.7	•		V. NO. 4	ILLINOIS PROJE	**	

					SPAN	C 15		,								SPAN	C 16										5.4	AN C	17				
FLOOR BEAMS	L 12	L12.5	6/	61.5	62	62.5	63	63.5	64	64.5	65	65.5	66	66.5	67	67.5	68	68.5	69	69.5	70	70.5	7/	71.5	72	72.5	73	73.5	74	74.5	75	75.5	L /3
	.0.0	.004	.021	.034	.041	.040	.034	.023	.011	•00	•GOO	.005	.017	.032	.046	.055	.059	.055	.046	.032	.017	.005	,000	•00.5	.011-	.025	,094	.040	.041	.035	.001	.0.5	.00

# THEORETICAL ELEVATION TOP OF CONCRETE

GIRD. CI	451.759	451.794	451.829	451,885	451.941	451.997	452.053	452,108	452.164	452.220	452.276	452.332	452,387	452,443	452,499	452,555	452,611	452,666	452.722	452.778	452.834	452,890	49.95	455,001	450,067	455,111	453, 148	453.204	453.200	452 226	455 305	155 155	153 155
STR.	452.399	452.430	452.462	452.518	452,578	452.632	452.683	452.740	452.80	452.855	452.907	452.963	453,024	453,079	453,130	453,186	453,247	453.302	453,353	453,409	453.470	453 855	455.5%	453.633	455.693	452 744	10.70	185 188	453 014	183 000	******		*53,465
STR.	453,039	453,070	453,102	453,158	453,218	453,272	453,323	453,380	453,440	453,495	453,547	453,603	453,664	453,719	453.770	453.026	453 007	452 942	452 002	454.040	454 110	****	464 514	484 575	454.000			*50,000	453,916	453.973	*3*	454,065	454,105
STR.	453,670	453,710	453,742	453,798	453.858	453,912	453,963	454.020	454.080	454 195	454 107	454 242	454 304	454 250	450.110	455,626	455,667	453,942	453,993	454,049	454.110	454,165	*34.216	*94.273	454,333	454,388	132,135	454,496	454.556	454.613	154.65	454.75	454.745
STR.	454 219	454 354	154 300		454.501	154 557	******	454,020	454.060	134.133	434.187	454,243	434,304	454.359	454.410	454,466	454.527	454.582	454.633	454.689	454,750	454,805	494,898	454.913	454,973	42.03	44	455, 136	455, 196	455,250	425.X*	12.345	455, 91
-GIRD. C2		40.03.4		*37,445	131,501	131.557	454,613	454.668	454.724	454.780	454.836	454.892	454.947	455.003	455,059	455,115	455,171	455,226	455,282	455.338	455,394	455.45	455,505	455,561	455,517	455, 573	455, 775	455,754	455,840	455.006	A 100 Sec.	4 FF 50 5	152 755

## THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION

GIRD. CI	451.759	451.799	451.851	451.920	451.982	452.038	452,087	452,132	452.176	452.223	452.276	452,337	452,405	452.476	452.545	452.611	452.670	452.722	452.768	452.811	452,851	452.895	42.345	453.004	453,068	453,136	455,505	455.565	453.301	452 271	153 114	152 154	152 111
STR.	452.399	452.434	452,484	452,552	452.619	452.673	452.718	452.764	452,812	452.858	452.907	452.969	453,C41	453,111	453,176	453,242	453,306	453,358	453,399	453,442	453,488	453,531	450,576	453,635	453.75	453.77	455 PM	453, 197	457 954	154 0.4	154 145	484.000	160.000
STR.	45009	453,074	453,124	453,192	453,259	453,313	453,358	453,404	453,452	453,498	453,547	453,609	453,681	453,751	453.816	453,882	453,946	453,998	454,039	454.000	454, 128	454.171	454.214	454.275	454.345	454.422	154 674	104 596	154 500	101 011	111 110	464.50	454.705
STR.	450.679	453.714	453.764	453,832	453.899	453.953	453,998	454.044	454.092	454.138	454,187	454,249	454.321	454.391	454.456	454.522	454.586	454.638	454.679	454.722	454,768	454.811	454.856	454.915	454.905	495.000	455-114	458.176	495.134	498 144	101 703	455.761	454, 445
GIRD C2	454.319	454.359	454,411	454,480	454.542	454.598	454,647	454.692	454.736	454.783	454.836	454.897	454,965	455.036	455.105	455.171	455,230	455,282	455.328	455.371	455,411	455.42	455,575	455.564	455,628	455,696	425.751	425.825	455.881	455,931	455.374	455, 954	49.00

											THEORE	ETICAL	ELEVA	TION 1	OP OF	CONCE	PETE + D	L. DEF	LECTIO	N - SLA	B THIC	KNESS	(75	- 1		N 10.			S 1	A 10		W	
GIRD. CI	451.176	451.216	451.268	451,336	451.399	451.454	451.504	451,549	451.592	451,639	451,692	451.754	451.822	451.892	451,962	452.027	452,086	452.139	452.185	452.227	452,268	452,012	42,362	45,48	472,485	12.2	12.00	40,00	12.73	19.71	150 . 121	100 000	450.000
STR.	451.816	451.851	451.901	451,969	452.035	452,090	452,135	452,180	452.229	452.275	452.323	452.386	452.458	452,528	452,593	452,659	452,723	452,774	452,816	452,859	459,904	10.317	10.90	455.045	485.151	45.00	And the con-	483 813	100 001				
STR.	452.456	452,491	452.541	452,609	452.675	452.730	452.775	452,820	452.869	452.915	452.963	453,025	453,098	453,168	453,233	453,299	453,363	453,414	453,456	453,499	453,544	\$50,587	453,430	452,690	451,761	455.85	452.75	455.965	124 124	484 -48	174 574	111 111	
STR.	453.096	453.131	453,181	453,249	453,315	453,370	453,415	453,460	453,509	453,555	453,603	453,665	453,738	453.808	453,873	453,939	454.003	454,054	454,096	454.139	454,184	454.227	454.273	454,332	454,401	454.458	454.50	654.593	454.654	454.74	101.00	100 707	154, 600
GIRD. C2	453,736	453,778	453,828	453,8%	450.959	454,014	454.064	454.109	454.152	454.199	454.252	454.314	454.382	454.452	454,522	454.587	454.646	454.699	454.745	454.787	454.828	454,873	454.80	454,380	455,045	455,113	455, 180	42.141	42.00	455,348	194,90	407,773	455.45

18Y RMR
Y VB
8Y RMR
D8Y KA

See Note A - Sr. No. 65.

STATE OF ILLINOIS
DEPARTMENT OF PUBLIC WORKS & BLDGS.
DIVISION OF HIGHWAYS

TABLES OF ELEVATIONS SPANS CIS THRU CI7

POPLAR STREET BRIDGE APPROACHES
ROADWAY "C"

F.A.I.RT.70 ST. CLAIR CO. SECTION 82-3HVB H. W. LOCHNER, INC. SHEET H. W. LOCHNER, INC. ENGINEERS CHICAGO, ILLINOIS 76 of 24/

		*001E	NO SECTION	COUNTY	SHEETS	SHEE
LECTION (FT.)		F. A. I.	-70 82-3HVB	ST. CLAIR	289	112
220		160 1	POAD DIV. NO. 4	ILLINOIS PROJE	CT	
	0.0411.0.00					

																											F. A. I70	82-3HV	B ST C	LAIR	289
									D	. L. DE	FLECTI	ON (FT.	!														FED ROAD DIV				-05
					5 P A	ANCI	8								5 /	PAN	C 19														
FLOOR BEAMS	L 14	L 14.5	76	76.5	77	77.5	78	78.5	79	79.5	80	80.5	81	81.5	82	82.5	83	83.5	84	84.5	85	85.5									
The second second	.000	.006	.028	.035	.040	.039	.033	.022	.010	.002	.000	.000	.008	.021	.033	.041	.044	.041	.032	.020	.009	,001									
																				1											
								THE	ORETIC	AL ELE	VATION	TOP O	CONC	RETE																	
RD. CI	452.473	453.511	453.548	453,602	453,654	453.704	453.751	453.797	453,841	453,883	453,922	453.960	453,996	454,029	454,061 4	54.090	454.118	454.143	454.166	454,187	454.207	454.224									
STR.															454.692 4																
STR.		454.786													455.332 4					455,459											
		455.426					455,662 456,311	455,708 456,357							455.972 4 456.621 4					456,099											
. U.	450.035	430.071	450.136	400.102	45.214	430.204	430.511	4.804.337	434,401	130.443	1.0.40.	430.32	430,300	430,307	430,621	x	430.010	430.703	450.720	430.747	430.767	456.784									
								ETICAL																							
TR.															454.094 4 454.725 4																
TR.		454,790					455,055		455.128	455,160	455, 193		455.281				455,439	455,460	455.470												
TR.	455,393	455,470	455,483	455.549	455.611	455.659	455.695	455,731	453.768	455.800	455,833	455.872	455.901	455,966	456.005 4	56.043	456.079	456,100	456,110	456,120	456,132	456.141									
SD CS	456,033	456,077	456.131	456.197	456,255	456,303	456.345	456.379	456.412	456.445	456.482	456,521	456,565	456,611	456,654 4	56.692	456.722	456.744	456.759	456.768	456.776	456.785									
																				6											
					THE	ORFTICA	L ELE	VATION	TOP	OF CON	CRETE	+ D. L. D	EFLECT	ION - S	LAB THIC	KNESS	5 (7")														
D. CI	452.000	450.034	452,988	453,054											453,511 4			453,601	453,616	453,625	453.633	453,642									
TR.	450,500	453,509	450,620	453,686	453.748	453.795	453,632	453.867	453.905	453,937	453,970	454,009	454.058	454.102	454.142 4	54.180	454,215	454.236	454.247	454,256	454.269	454.277									
TR.															454.782 4																
TR.															455,422 4																
4D. C2	455.450	455.494	455.548	455,614	455.671	455.720	455.761	455.796	455.828	455.862	455.899	455,938	455.981	456.027	456.071 4	56.109	456.139	456.161	456.176	456.185	456,193	456.202									
													- 1																		
										D. L. D	EFLECT	ION (F	<i>''</i>												1	11					
													1	- 1	- 1		SPA	N C 2	1// 1/4	_	- 11 /			- //							
LOOR		-	-		-	SPA	N C 20	0			-	-		-		-	714	/ -	_						-1117	NI.	1 1				
EAMS	86	86.5	87	87.5	88	88.5	1	-	90	90.5	91	91,5	92	92.5	93 9	93.5	94	94.5	95	95.5	96	96.5	L 15		ハ	V	L 1				
EAMS	.000	86.5	.009	87.5	.032	1	1	-	90	90.5	9/	91.5	92	92.5 .œ2		93.5	-13	94.5		95.5	96	96.5	L 15		川	V	L ì				
AMS		*****	E-1		-	88.5	89	.041	.633	.021	.008	.000	,cce	.002		-	94	4	95	A					<i>ا</i> ار	V	Lì				
EAMS		*****	E-1		-	88.5	89	.041	.633	.021	.008		,cce	.002		-	94	4	95	A					ハ	V	Lì				
	,ccc	.(0)	.009	.021	.032	88.5	.044	89.5 .041	.COS	.021	.008	.000	F CON	.002 CRETE		•055	.033	.039	95	.035	.022	.005	.000		ハ	V	Lì				
D. C1	454,239	.001 454.252	,009 454,263	.21 454.272	454.279	88.5 .041	.044	69.5 ,041 THE	.033 EORETIC 454,286	.021 CAL ELI 454.283	.008 EVATION 454.278	.000 TOP (	.cce OF CON 454.261	.002 CRETE 454.249	.010	.022	.033	.039 454.183	.040	.035	.022	454,094	.000		<i>י</i> וע	N	Lì				
D. CI TR. TR.	454.239 454.870 456.610	.001 454,252 454,883 455,523	.009 454,263 454,699 455,539	454.272 454.907 455.547	.032 454.279 454.910 455.550	88.5 .(41 454.284 454.915 456.555	.044 454,287 454,003 456,563	69.5 .041 THE 454.287 454.203 455.963	.033 EORETIC 454.286 454.917 455.567	.021 CAL ELI 454.283 454.914 455.554	.008 EVAT/ON 454.278 454.914 455.954	.000 TOP 0 454,270 454,905 455,545	.000 OF CON 454,261 454,892 455,532	.002 CRETE 454.249 454.881 455.520	.010 454.236 45 454.672 45 455.512 45	.022 4.220 4.855 5.495	94 .033 154,203 154,833 155,473	.039 454.183 454.814 455.454	95 .040 454.161 454.797 455.437	.035	.022 454.112 454.747 455.387	454,094 4 454,731 4 455,371	.000 454.076 454.716 155.356		יו <i>ר</i>	N	Lì				
D. CI TR. TR.	454,239 454,870 455,510 456,150	454,252 454,883 455,523 496,163	,009 454,263 454,899 455,539 456,179	454.272 454.967 455.547 456.187	.032 454.279 454.910 495.650 456.190	88.5 .641 454.284 454.915 456.555 456.195	454,287 454,003 456,563 456,203	69.5 .041 THE 454.287 454.903 496.963 496.203	.033 EORETIO 454,286 454,917 455,567 456,197	.021 CAL ELS 454.283 454.914 455.554 456.194	.008 EVAT/CM 454.278 454.914 455.954 456.194	.000 TOP 0 454.270 454.905 455.545 456.185	.600 OF CON 454.261 454.892 456.532 456.172	.002 CRETE 454.249 454.881 455.520 456.160	.010 454.236 45 454.672 45 455.512 45 456.152 45	.022 4.220 4.855 5.495 6.135	94 .033 454,203 454,833 455,473 456,113	.039 454.183 454.814 455,454 456.094	95 .040 454.161 454.797 455.437 456.677	.035 454.137 454.774 455.414 456.054	.022 454.112 454.747 455.387 456.027	454,094 4 454,731 4 456,011 4	.000 454.076 454.716 455.356 455.996		יוכ	N	Lì				
D. CI TR. TR.	454,239 454,870 455,510 456,150	454,252 454,883 455,523 496,163	,009 454,263 454,899 455,539 456,179	454.272 454.967 455.547 456.187	.032 454.279 454.910 495.650 456.190	88.5 .641 454.284 454.915 456.555 456.195	454,287 454,003 456,563 456,203	69.5 .041 THE 454.287 454.903 496.963 496.203	.033 EORETIO 454,286 454,917 455,567 456,197	.021 CAL ELS 454.283 454.914 455.554 456.194	.008 EVAT/CM 454.278 454.914 455.954 456.194	.000 TOP 0 454.270 454.905 455.545 456.185	.600 OF CON 454.261 454.892 456.532 456.172	.002 CRETE 454.249 454.881 455.520 456.160	.010 454.236 45 454.672 45 455.512 45	.022 4.220 4.855 5.495 6.135	94 .033 454,203 454,833 455,473 456,113	.039 454.183 454.814 455,454 456.094	95 .040 454.161 454.797 455.437 456.677	.035 454.137 454.774 455.414 456.054	.022 454.112 454.747 455.387 456.027	454,094 4 454,731 4 456,011 4	.000 454.076 454.716 455.356 455.996		יוכ	V					
D. CI TR. TR.	454,239 454,870 455,510 456,150	454,252 454,883 455,523 496,163	,009 454,263 454,899 455,539 456,179	454.272 454.967 455.547 456.187	.032 454.279 454.910 495.650 456.190	454.284 454.284 454.915 456.555 456.195 456.844	454,287 454,287 454,033 416,563 456,203	454,287 454,283 456,903 456,543 456,547	.633 EORETIC 454,286 454,917 455,567 456,197 456,846	.021 CAL ELI 454.283 454.914 455.554 456.194 456.843	.008 EVATION 454.278 454.914 455.554 456.194 456.838	.000 I TOP 0 454,270 454,905 455,545 456,185 456,185	.000 0F CON 454.261 454.892 456.532 456.172	.002 CRETE 454.249 454.881 455.520 456.160 456.809	.010 454.236 45 454.672 45 456.512 45 456.796 45	.022 4.220 4.855 5.495 6.135	94 .033 454,203 454,833 455,473 456,113	.039 454.183 454.814 455,454 456.094	95 .040 454.161 454.797 455.437 456.677	.035 454.137 454.774 455.414 456.054	.022 454.112 454.747 455.387 456.027	454,094 4 454,731 4 456,011 4	.000 454.076 454.716 455.356 455.996		יו <i>ר</i>	V					
ID. CI TR. TR. TR. TR.	454.239 454.870 455.510 456.150 456.799	454,252 454,883 455,523 456,812	.009 454.263 454.099 455.539 456.179 456.823	454.272 454.907 455.547 456.187 456.832	.032 454.279 454.910 455.550 456.190 456.839	88.5 .641 454,284 454,915 456,555 456,195	59 .044 454,287 454,003 415,563 456,203 456,947 THEOR	89,5 .041 THE 454,287 454,993 495,993 496,203 456,847	.033 EORETIC 454,286 454,917 455,567 456,197 456,846	.021  CAL ELI 454.283 454.914 455.554 456.134 456.843	.008 EVAT/CN 454.278 454.914 455.954 456.194 456.838 OP OF	.000 454,270 454,905 455,545 456,185 CONCRE	.000 0F CON 454,261 454,892 456,532 456,172 156,821	.002 CRETE 454.249 454.881 455.520 456.160 456.809	.010 454.236 45 454.672 45 456.512 45 456.796 45 LECTION	.022 4.220 4.855 5.495 6.135	94 .633 .654,203 .654,833 .655,473 .656,763	.039 454.183 454.814 455.454 456.094 456.743	95 .040 454.161 454.797 455.437 456.077 456.721	.035 454.137 454.774 455.414 456.054 456.697	.022 454.112 454.747 455.387 456.027 456.672	.005	,000 454,076 454,716 455,356 455,996 456,434		יוע						
RD. CI TR. TR. TR. RD. C2	454.239 454.870 456.510 456.150 456.799	454,252 454,883 455,523 456,812	.009 454.263 454.099 455.539 456.179 456.823	454,272 454,907 455,547 456,832 454,093	454,279 454,910 455,550 456,839 454,312	88.5 .641 454,284 454,915 456,555 456,195 456,844	59 .044 454,287 454,003 476,563 456,203 156,847 THEOR	89,5 .041 THE 454,287 454,993 495,993 496,203 456,847	.633 EORETIC 454,286 454,917 455,567 456,197 456,846 ELEVA 494,380	.021 CAL ELL 454.283 454.914 455.954 456.124 456.843	.008 EVATION 454.278 454.914 455.954 456.194 456.838 OP OF 454.286	.000 1 TOP C 454,270 454,905 455,545 456,185 456,830 CONCRE 454,271	.000 OF CON 454.261 454.892 456.532 456.172 176.821 TE + C 454.261	.002 CRETE 454.249 454.881 455.520 456.160 456.809 L. DEF 454.252	.010 454.236 45 454.677 45 456.512 45 456.796 45 LECTION 454.246 45	.022 4.220 4.855 5.495 6.135 6.780	94 .633 454,203 454,833 456,473 456,113 456,763	.039 454.183 454.814 455.454 456.094 456.743	95 .040 454.161 454.797 455.437 456.077 456.721	.035 454,137 454,774 455,414 456,054 456,697	.022 454.112 454.747 455.387 456.027 456.672	.005 454,094 454,731 455,371 456,011 456,654 454,099	,000 454,076 654,716 455,356 455,996 456,634		יוע		Lĭ				
RD. CI TR. TR. TR. RD. CZ	454.239 454.870 456.610 456.799	494,252 454,853 455,923 496,163 456,612 454,254 454,255	.009 454.263 454.099 455.539 456.179 456.823	454,272 454,967 455,547 456,187 456,832 454,793	454,279 454,910 455,550 456,190 456,839 454,312 454,943	88.5 .641 454,284 454,915 456,555 456,195 456,844 454,325 454,927	59 .044 454,287 454,003 476,563 456,203 456,847 THEOR 454,331 454,968	59,5 .041 THE 454,287 454,903 456,903 456,847 ETICAL 454,329 454,964	.033 EORETIC 454,286 454,917 455,957 456,846 ELEVA 454,320 454,930	.021 CAL ELL 454.283 454.914 455.954 456.124 456.843 TION T 454.304 454.935	.008 EVATION 454.278 454.914 455.954 456.194 456.838 OP OF 454.226 454.226	.000 1 TOP C 454,270 454,905 455,545 456,185 456,830 CONCRE 454,271 454,206	.000 OF CON 454.261 454.892 456.172 156.821 TE + C 454.261 454.261	.002 CRETE 454.249 454.881 455.520 456.160 456.809 L. DEF 454.252 454.883	.010 454,236 45 454,672 45 456,152 45 456,152 45 456,152 45 456,796 45 456,246 45 454,246 45	.022 4.220 4.855 6.135 6.760 4.243	94 .033 154,203 154,833 155,473 156,763 154,236 154,236	.039 454.183 454.814 455.454 456.094 456.743	95 .040 454.161 454.797 455.437 456.077 456.721	.035 454,137 454,774 455,414 456,054 456,697	.022 454.112 454.747 455.387 456.027 456.672 454.134 454.769	454,094 4 454,731 4 456,071 4 456,654 4 454,099 4 454,736 4	,000 454,076 454,716 455,556 455,998 454,678 454,678		יונ		Lĭ				
RD. CI TR. TR. TR. RD. C2 RD. CI STR.	454.239 454.870 456.510 456.799 454.239 454.239	454,252 454,803 455,503 456,610 456,610 454,054 454,055 454,055	.009 454,263 454,099 455,539 456,179 456,823 454,272 454,948 455,548	454,272 454,967 455,547 456,832 454,793 454,796 455,568	454,279 454,910 455,550 456,839 454,312 454,943 455,583	454,284 454,284 454,915 456,555 456,195 456,844 454,325 454,957 455,596	454,287 454,287 454,003 456,563 456,203 456,847 THEOR 454,331 454,968 455,668	59,5 .041 THE 454,287 455,963 455,963 456,847 ETICAL 454,329 454,964 455,664	.033 EORETIO 454.286 454.917 455.967 456.846 ELEVA 491.380 454.990 455.900	.021 CAL ELI 454.283 454.914 455.954 456.194 456.843 TION T 454.935 465.975	.008  EVAT/ON  454.278  454.214  455.554  456.194  456.838  OP OF  454.226  454.923  456.563	.000 (TOP C) 454,270 454,905 455,545 456,185 456,830 CONCRE 454,271 454,306 455,546	.000 OF CON 454.261 454.892 456.532 456.172 176.821 TTE + C 454.261 454.261 454.261 454.263	.002 CRETE 454.249 454.881 455.520 456.160 456.809 L. DEF 454.252 454.883 455.523	.010 454.236 45 454.677 45 456.512 45 456.796 45 LECTION 454.246 45	.022 4.220 4.855 6.135 6.760 4.243 4.878 6.518	9.4 .033 .033 .033 .054,203 .054,833 .055,473 .056,763 .056,763	.039 454.183 454.814 455.454 456.094 456.743 454.223 454.223 454.854 455.494	95 .040 454.161 454.797 455.437 456.077 456.721 454.202 454.838 455.478	.035 454,137 454,774 495,414 495,054 456,697 454,879 454,879 455,449	.022 454.112 454.747 455.387 456.627 496.672 494.134 454.769 455.409	.005 454,094 4 454,731 4 456,011 4 456,654 4 454,099 4 454,736 4 455,376 4	154,076 154,776 155,756 155,756 155,996 155,996 155,096 155,776		יונ			4-50	W 65		
RD. CI TR. TR. RD. CZ RD. CI TR. TR.	454.239 454.870 455.510 456.799 454.239 454.870 456.150	454,252 454,883 455,523 454,163 456,812 454,254 454,254 454,355 456,515	.009 454.263 454.092 455.539 456.179 456.823 454.272 454.278 455.548 456.188	454,272 454,967 456,547 456,187 456,832 454,293 454,298 455,568 456,208	454,279 454,910 455,550 456,190 456,839 454,312 454,943 455,583 456,223	454,284 454,284 454,915 456,555 456,195 456,844 454,325 454,957 455,996 456,236	454,287 454,287 454,013 416,563 456,203 456,203 454,331 454,968 455,668 456,248	454,287 454,287 454,287 456,543 456,543 456,543 456,544 454,329 454,364 456,604	.033 EORETIO 454,286 454,917 455,967 456,846 ELEVA 494,380 494,990 496,590 496,230	.021  CAL ELI  454.283 454.914 455.954 456.194 456.843  TION T  454.304 454.935 475.975 456.215	.008  EVAT/ON  454.278  454.914  455.954  456.194  456.838  OP OF  454.286  454.923  455.563  456.203	.000  TOP 0  454,270  454,905  455,545  456,830  CONCRE 454,271  454,906  455,546  456,186	.000 0F CON 454.261 454.892 455.532 456.172 17E + C 454.261 454.261 454.261 454.261 454.261 454.261 454.261 454.261	.002 CRETE 454.249 455.520 456.160 456.809 L. DEF 454.252 454.883 455.523 456.163	.010 454.236 45 455.672 45 456.152 45 456.152 45 456.796 45 456.796 45 456.246 45 456.523 45	.022 4.220 4.855 5.495 6.135 6.780 4.243 4.876 6.518 6.158	9.4 .033 .033 .034,203 .034,203 .035,473 .036,113 .036,763 .036,763	.039 454.183 454.814 455.454 456.094 456.743 454.223 454.854 455.494 456.134	95 .040 454.161 454.797 455.437 456.077 456.721 454.202 454.838 455.478 456.118	.035 454,137 454,774 455,414 456,054 456,697 454,173 454,879 455,449 456,089	.022 454.112 454.747 455.387 456.627 454.672 454.769 455.409	454,094 4 454,731 4 455,371 4 456,011 4 456,654 4 454,099 4 454,736 4 455,376 4 456,016 4	.000 654.076 654.716 655.356 655.998 656.434 654.076 654.716 655.356		JI'		ee Note				
RD. CI TR. TR. RD. CZ RD. CI TR. TR.	454.239 454.870 455.510 456.799 454.239 454.870 456.150	454,252 454,883 455,523 454,163 456,812 454,254 454,254 454,355 456,515	.009 454.263 454.092 455.539 456.179 456.823 454.272 454.278 455.548 456.188	454,272 454,967 456,547 456,187 456,832 454,293 454,298 455,568 456,208	454,279 454,310 456,650 456,839 454,312 454,343 459,583 456,223 456,872	454,284 454,915 456,555 456,195 456,844 454,325 454,957 455,596 456,236 456,885	454,287 454,287 454,263 476,563 476,203 456,203 454,331 454,968 455,608 456,248 456,891	454,287 454,287 454,983 456,963 456,847 456,847 454,329 454,364 455,664 456,244 456,889	454,286 454,917 455,567 456,197 456,846 ELEVA 454,950 454,950 456,550 456,680	.021 CAL ELI 454.283 454.914 455.554 456.194 456.843 ATION T 454.305 456.215 456.864	.008 EVATION 454.278 454.914 456.194 456.838 OP OF 454.226 454.223 456.233 456.233	.000 (TOP C) 454,270 (454,270 (455,545 (456,830 CONCRE 454,271 (454,906 456,546 (456,831 )	.000 OF CON 454.261 454.892 456.532 456.172 454.261 454.261 454.261 454.261 454.261 454.261 454.261 456.172 456.172	.002 CRETE 454.249 454.881 455.520 456.160 456.809 L. DEF 454.252 454.883 455.523 456.163 456.812	.010  454.236 45 454.677 45 455.512 45 456.192 45 456.736 45  LECTION  454.246 45 456.633 45 456.633 45	44.220 44.855 55.495 6.135 6.780 44.243 44.243 44.243 6.5518 6.5518 6.658	94 .c33 .654.203 .654.833 .655.473 .656.113 .656.763 .654.236 .654.236 .654.236 .654.236 .654.236 .654.236	.039 454.183 454.814 455.454 456.094 456.743 454.223 454.854 455.494 456.134	95 .040 454.161 454.797 455.437 456.077 456.721 454.202 454.838 455.478 456.118	.035 454,137 454,774 455,414 456,054 456,697 454,173 454,879 455,449 456,089	.022 454.112 454.747 455.387 456.627 454.672 454.769 455.409	454,094 4 454,731 4 455,371 4 456,011 4 456,654 4 454,099 4 454,736 4 455,376 4 456,016 4	.000 654.076 654.716 655.356 655.998 656.434 654.076 654.716 655.356		JI'		DEPARTME	STATE	OF IL	WORKS	
RD. CI TR. TR. TR. RD. CZ RD. CZ TR. TR. TR. TR. RD. CZ	454.239 454.870 456.610 456.150 456.239 454.239 454.870 456.150 456.799	454.252 454.003 455.523 456.163 456.212 454.254 454.254 454.255 454.255 454.255 454.255 454.255 454.255	.009 454.093 454.093 455.539 456.179 456.823 454.272 454.272 454.278 456.188 456.188	454,272 454,907 455,547 456,187 456,832 454,793 454,793 456,208 456,208 456,208 456,208	454,279 454,910 456,550 456,190 456,839 454,943 456,833 456,833 456,833	494,284 494,915 495,955 496,195 496,844 494,325 494,325 496,844 494,325 496,846 496,846 496,846 496,846 496,846	59 .044 .287 .494,287 .495,093 .495,293 .495,293 .495,293 .495,698 .495,608 .405,608	454,287 454,287 454,293 456,203 456,203 456,847 454,329 454,364 455,604 456,244 456,889	454,286 454,917 456,4917 456,197 456,846 ELEVA 454,320 454,950 456,230 456,230 456,230 456,230 456,230	.021 CAL ELG 454.283 454.914 455.554 456.194 456.843 TION T 454.305 456.215 456.215 456.216	.008  EVATION  454.278  454.214  456.194  456.838  OP OF  454.226  454.226  454.223  456.203  456.203  456.203	.000  TOP 0  454,270  454,265  456,165  456,830  CONCRE 454,271  454,306  455,546  456,186  456,831	200 CON 454.261 454.892 456.532 456.261 454.692 456.261 456.821 456.821 456.821 456.821 456.821	.002  CRETE  454.249  454.881  455.500  456.160  456.809  L. DEF  454.252  454.883  456.163  456.812	.010  454,236 45 454,672 45 455,512 45 456,192 45 456,736 45  LECTION  454,246 34 456,163 45 456,163 45 456,163 45 456,163 45		94 .033 .634,203 .654,203 .655,473 .656,763 .656,763 .656,763 .656,764 .656,766 .756,766	.039 454.183 454.814 455.454 456.094 456.743 454.223 454.824 455.494 456.134 456.783	95 .040 454,161 454,177 455,437 456,077 456,077 456,771 456,772 456,772 456,772	.035 454,137 454,774 455,654 456,657 454,173 454,819 455,449 456,069 456,733	.022 454.112 454.747 455.387 456.427 456.427 454.134 454.134 454.69 456.649 456.694	454,094 456,011 456,654 4456,016 456,016 456,019 4	.000 854,776 854,776 855,996 855,996 854,076 854,776 854,776 854,776 854,776 854,576		) I'	N	DEPARTME	STATE NT OF	OF IL PUBLIC OF H	WORKS	S
RD. CI TR. TR. TR. RD. CZ RD. CI TTR. TTR. TTR. TTR. TTR. TTR. TTR. TTR	454.239 454.670 456.150 456.799 454.239 454.670 456.799 454.799	454,252 454,803 455,523 454,163 456,812 454,255 454,255 459,165 459,165 459,165	.009 454.263 454.093 456.179 456.823 454.272 454.988 456.188 456.188 456.4832	454,272 454,967 455,947 456,187 456,832 454,928 455,568 456,208 456,853	454,279 454,910 455,050 456,190 456,839 454,312 454,943 455,283 456,223 456,272 THE	454,284 454,284 454,915 456,555 456,195 456,844 454,325 454,957 456,236 456,885 ORETICA	59	456,267  456,267  456,263  456,563  456,563  456,564  456,264  456,264  456,264  456,264	.033 EORETIC 454.286 454.917 455.507 456.197 456.846 ELEVA 454.320 454.320 455.500 456.230 456.230 456.230 456.230 456.230 456.230	.021 CAL ELI 454.283 454.914 456.554 456.194 456.843 TION T 494.304 456.215 456.215 456.864 OF CON 453.721	.008  EVATION 454.276 455.954 456.958 456.194 456.838  OP OF 454.923 456.563 456.203 456.846	.000   100	2600 264 261 264 264 265 262 265 265 265 265 265 265 265 265	.002  CRETE  454.249  454.881  455.250  456.160  456.160  456.809  L. DEF  454.883  456.812  456.817	.010  454,236 45 454,677 45 456,172 45 456,736 45 456,736 45 456,246 45 456,833 45 456,836 45 456,836 45 456,836 45		94 ,033 ,033 ,033 ,035 ,035 ,035 ,035 ,035	. C39 454,103 454,814 455,454 456,094 456,743 454,223	95 .040 .040 .040 .040 .040 .040 .040 .04	.035 464.137 494.774 495.414 496.094 496.697 494.173 494.819 495.449 496.089 496.733	. 922 454,112 454,147 456,127 456,127 456,172 456,172 456,173 456,173 456,173 456,173 456,173 456,173 456,173 456,173	454,094 4 454,731 4 456,011 4 456,654 4 456,654 4 456,659 4 456,016 4 456,659 4	,000 155,00		<i>)</i>		DEPARTME (	STATE NT OF DIVISION	OF IL PUBLIC OF H	WORKS IGHWAY VATI	s ONS
RD. CI TR.	454,239 454,670 456,610 456,190 456,799 454,279 456,799 454,799 454,799	454,252 454,803 455,523 454,163 456,812 454,255 454,255 459,165 459,165 459,165	454,263 454,093 456,073 456,023 456,023 456,023 456,023 456,023 456,038 456,038 456,038	, c21 454,272 454,977 456,547 456,632 454,293 455,568 456,208 456,633	454,273 454,910 456,520 456,190 456,633 456,633 456,633 456,633 456,633 456,633 456,633 456,633 456,633	454,284 454,915 456,555 456,195 456,844 454,325 454,957 455,966 456,625 ORETICA 453,742 454,373	59 .044 .454,267 .454,263 .416,563 .456,263 .456,263 .456,667 .456,668 .456,669 .456	E9.5  .041  THE 454.287 454.293 455.933 455.934 456.204 456.204 456.204 456.206 456.206 456.206 456.206 456.206 456.206 456.206 456.206 456.206 456.206 456.206 456.206 456.206 456.206 456.206 456.206 456.206 456.206	454,286 454,917 455,567 456,197 456,846 ELEVA 454,380 454,380 456,530 456,530 456,530 456,530 456,530	.021  CAL ELI 454.283 454.914 455.554 456.134 456.843  TION T 454.356 456.215 456.864  OF CON 453.721 454.352	.008  EVATION  454.278  454.914  455.554  456.194  456.838  OP OF  454.286  454.286  456.203  456.203  456.203  456.203  456.203  456.203	.000   454,270   454,205   455,545   456,830   CONCRE 456,830   45	,000 ,000 ,000 ,000 ,000 ,000 ,000 ,00	.002  CRETE 454.249 454.881 455.300 456.160 456.809  L. DEF 454.232 456.163 456.817	.010  454,236 45 454,672 45 455,512 45 456,192 45 456,736 45  LECTION  454,246 34 456,163 45 456,163 45 456,163 45 456,163 45	4.220 4.220 4.255 5.495 6.135 6.135 4.243 4.243 4.243 6.518 6.518 6.518 6.583	94 ,033 155,473 155,473 155,473 155,473 155,473 155,473 155,763 155,277 155,50	.C09 454.103 454.814 455.454 456.743 456.743 456.743 456.783 456.783	95 .040 .040 .040 .040 .040 .040 .040 .04	.035 454.137 454.774 455.414 456.054 456.057 454.173 454.819 455.449 456.069 456.733	. 022 454.112 454.747 455.367 456.672 456.672 456.672 456.694 456.694 456.694	454,094 4 454,731 4 456,011 4 456,654 4 456,654 4 456,659 4 456,016 4 456,659 4	1,000 154,076 154,776 155,256 1556,158 1556,158 1556,158 1554,076 1554,176 1554,186		) I'		DEPARTME (	STATE NT OF DIVISION LES O SPANS STREET	OF IL PUBLIC OF H OF EL! CIB TH	WORKS IGHWAY EVATION RU C21 GE API	SNS
RD. CI STR. STR. STR. STR. STR. STR. STR. STR.	454,239 454,870 455,510 456,793 454,870 456,793 454,870 456,793 454,870 456,793 454,870 454,870 454,870 454,870 454,870 454,870 454,870	454,252 454,803 455,523 456,163 456,212 454,254 456,254 456,25	454,263 454,093 455,539 456,179 456,223 454,277 455,346 455,188 455,188 455,188 455,188 455,188 455,188	454,272 454,927 455,547 456,632 454,033 454,033 455,036 455,033 455,036 455,035 455,035 455,035	454,279 454,910 455,000 456,190 456,039 456,039 456,039 456,039 456,039 456,039 456,039 456,039 456,039 456,039 456,039	494.284 494.915 496.195 496.195 496.195 496.236 494.325 494.325 494.325 494.325 494.325 494.325 494.325 494.325 494.325 494.325 494.325	59 .044 454,287 454,293 410,549 450,549 450,549 450,549 450,549 450,549 450,549 450,640,649 450,640 450,640 450,640 450,640 450,640 450,640 450,640 45	E9.5 .041 THE 454.287 454.973 455.973	454,286 454,287 456,197 456,197 456,198 456,197 456,198 456,197 456,198	.621  ASAL ELI 454,283 454,314 450,564 456,184 456,184 456,184 456,185 456,185 456,185 456,185 456,185 456,185 456,185 456,185 456,185 456,185 456,185 456,185 456,185	.008  EVATION 454.276 454.276 456.254 456.194 456.194 456.256 456.256 456.266 456.266 456.266 456.266 456.266 456.266 456.266 456.266 456.266 456.266 456.266	1 TOP C 454,270 454,270 454,270 455,265 456,16	,000 ,000 ,000 ,000 ,000 ,000 ,000 ,00	.002  CRETE 454.249 454.881 455.300 456.160 456.160 456.160 456.603 456.603 456.603 456.603 456.603 456.603 456.603 456.603 456.603 456.603 456.603 456.603	454,236 45 454,636 45 456,239 45 456,239 45 456,239 45 456,162 45 456,163 456,163 45 456,163 45 456,163 45 456,163 45 456,163 45 456,163 456,163 45 456,163 45 456,163 45 456,163 45 456,163 45 456,163 45 456,163 45 456,163 45 456,163 45 456,163 45 456,163 45 456,163 456,163 45 456,163 45 456,163 45 456,163 45 456,163 45 456,163 456,163 45 456,163 45 456,163 45 456,163 45 456,163 45 456,163 45 456,163 45 456,163 45 456,163 45 456,163 45 456,163 45 456,163 456,163 45 456,163 45 456,163 45 456,163 45 456,163 45 456,163 456	4.220 4.855 5.495 6.135 6.135 6.136 6.518 6.518 6.518 6.518 6.586	94 .033 454,203 454,433 456,433 456,113 456,236 454,236 454,236 454,236 454,236 454,236 454,236 454,236 454,236 454,238	.C39 454,103 454,814 456,644 456,044 456,743 454,222 454,223 454,223 454,223 454,223 454,223 454,223 454,223 454,223 454,223 454,223 454,223 454,223 454,223	95 .040 .040 .040 .045,161 .045,797 .0456,791 .0454,202 .0454,838 .0454,782 .0454,782 .0454,782 .0454,782 .0454,783	.035 454.137 454.774 455.414 456.054 456.697 454.809 456.099 456.733 453.589 454.866	. 322 454,112 454,747 456,127 456,127 456,134 454,134 454,136 454,136 456,149 456,149 456,149 456,149 456,149	454,094 454,731 456,011 456,054 455,376 455,01	1,000 1554,776 1554,776 1555,996 1556,698 1554,678 1554,078 1554,776 1554,796 1554,796 1554,796 1554,796 1554,193 1554,193 1554,193		) I'		DEPARTME TAE	STATE NT OF DIVISION LES O SPANS STREET ROA	OF IL PUBLIC OF H OF EL! CIB TH CBRID DWAY	WORKS	S ONS PROACH
STR. STR. STR. STR. RD. CI STR. STR. STR. STR. STR. STR. STR. STR.	454,239 454,870 456,610 456,150 456,170 456,170 456,170 456,170 456,170 456,170 456,170 456,170 456,170 456,170 456,170	454.752 454.883 459.763 459.163 454.754 454.785 454.785 456.781 456.781 456.781 456.781 456.781 456.781 456.781 456.781	454,263 454,073 455,523 456,173 456,423 454,277 451,346 455,623 451,425 451,426 451,425 451,42	.01 454,272 454,967 455,567 455,187 456,187 45	494,273 494,910 495,020 496,190 496,030 496,030 496,030 496,232 THE 490,730 494,640 494,640 494,640 494,640 494,640 494,640 494,640 494,640 494,640	88.5	69 .044 .494,287 .494,293 .495,493 .495,493 .495,493 .495,493 .495,493 .495,493 .495,494 .495 .495 .495 .405 .405 .405 .405 .405 .405 .405 .40	#9,60 FP, 746	454,286 454,917 455,067 456,197 456,196 644,390 456,593 456,193	.021  CAL ELLI 454,293 454,914 455,945 456,134 456,134 456,043 456,043 456,043 456,043 456,043 456,043 456,054 456,054 456,054 456,054 456,054 456,054 456,054 456,054 456,054	.008  EVATION 454,278 455,954 456,194 455,838  OP OF 456,223 456,563 456,234 456,846  LORETE 453,733 455,563 456,739 455,619	1 TOP C 454,270 455,055 456,05	,5006  454,261  454,261  454,892  456,172  454,261  454,261  454,261  454,261  454,261  454,262  456,372  456,372  456,372  456,372  456,372  456,372  456,372  456,372	.002  CRETE 454.249 456.160 456.160 456.009  L. DEF 454.282 456.163 456.163 456.017  ION - 5	.010  454.236 45 454.672 45 455.512 45 455.796 45 456.796 45 456.796 45 456.163 45	.022 44,000 44,855 6,780	94 .033 454,203 554,833 555,473 556,763 556,763 656,763 656,765 656,766 656,766 656,766 656,766 656,766 656,766	.039 454.183 454.814 456.454 456.094 456.743 454.223 454.854 456.134 456.134 456.783 456.854 456.874 456.874 456.874	95 .040 .040 .040 .040 .040 .040 .040 .04	.035 454,137 456,174 456,414 456,554 456,67 456,67 456,67 456,67 456,67 456,67 456,67 456,67 456,67 456,67 456,67 456,67 456,67 456,67 456,67 456,67	. 322 454, 112 454, 147 456, 147 456, 167 456, 167 456, 167 456, 168 456, 169 456, 169 456, 169 456, 169 456, 169	454,098 4 456,731 456,654 4 456,654 4 455,376	,000 155,000 155,106 155,10		) I'		DEPARTME (	STATE NT OF DIVISION LES O SPANS STREET ROA	OF IL PUBLIC OF H OF ELI CIB TH F BRID DWAY	WORKS IGHWAY EVATION RU C21 GE API "C" SECT	S ONS PROACH

ED BY RMR
BY RMR
RD BY KA

SECTION COUNTY TOTAL SHEETS F. A. I. -70 82 - 3HVB ST. CLAIR 289 D. L. DEFLECTION .FT.) FED. ROAD DIV. NO. 4 ILLINOIS PROJECT 99.5 100 100.5 101 101.5 102 102.5 103 103.5 104 104.5 105 105.5 106 106.5 //65 37 97.5 QB QB 5 QQ 116 .005 .002 .000 .041 THEORETICAL ELEVATION TOP OF CONCRETE G/RD, C/ 454,008 454,009 454,299 453,299 453,299 453,209 453,209 453,200 453,2 \$7.A. 494,700 494,684 494,801 494,601 494,601 494,001 455,386 455,324 455,321 455,567 455,267 455,258 455,197 455,153 455,111 455,073 455,056 454,571 454,571 454,677 454,677 454,673 454,664 454,575 454,685 454,575 454,677 454,677 STA. 455,086 485,064 455,041 4 G/AD. C2 456,609 456,509 456,509 456,509 456,509 456,509 456,509 456,600 456,600 456,600 456,600 456,600 456,600 456,600 456,600 456,600 456,600 456,600 456,600 456,600 456,600 456,600 456,600 456,6 THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION GIRD, CI 494,000 494,094 494,094 494,094 494,094 494,094 494,094 494,094 494,094 495,091 495,091 495,091 495,091 495,091 495,091 495,091 495,091 495,091 495,091 495,091 495,091 495,091 495,091 STR. 454,700 454,600 164,600 454,600 454,600 454,600 454,600 454,600 454,000
454,000 4 STR. 455,301 455,301 455,301 455,301 455,301 455,301 455,301 455,501 4 57A. 455.086 455.083 455.084 4 GARD C2 456.688 456.611 456.501 456.501 456.500 456.50 THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION - SLAB THICKNESS (7") G/RD, C/ 400,465 500,471 400,405 400,401 400,4 STR. 454,105 454,116 454,105 454,105 454,105 454,105 454,105 454,105 454,105 455,105
455,105 4 454,795 254,741 254,743 454,743 454,454 454,453 154,653 454,655 454,555 455.45 455.56 455.50 455 G/MC. C2 454,045 454,051 456,052 456,057 456,057 456,058 456,057 456,058 456,057 456,058 456,0 FLOOR 107 107.5 108 (08.5 109 109 5 .033 . 341 .:44 .000 .000 .022 .033 .039 .040 .022 .005 THEORETICAL ELEVATION TOP OF CONCRETE 6/AD. C/ 109.500 105.5 \$7.8. 450,559 450,551 450,455 450,551 450,455
450,455 \$78. 454,757 454,155 454,555 455,557 455,457 455,757 455,457 455,757 455,457 4 57 A. 494.879 494.866 454.776 494.465 454.577 454.465 454.577 454.465 454.577 454.465 454.277 454.465 454.277 454.187 454.465 454.277 454.187 454.465 454.277 454.467 454.277 454.467 454.277 454.467 454.277 454.467 454.277 454.467 454.277 454.467 454.277 454.467 454.277 454.467 454.277 454.467 454.277 454.467 454.277 454.467 454.277 454.467 454.277 454.467 454.277 454.467 454.277 454.467 454.277 454.477 G/AD, C2 495,509 005,404 005,109 005,109 005,109 005,109 005,109 005,109 005,109 005,109 005,100 005,1 THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION 6/AD.C1 400.000 400.00 57A, 455,599 803,007 403,484 403,008 403,003 403,007 403,007 403,008 403,008 403,008 403,008 403,008
403,008 4 STR. 484.000 694.001 494.004 494.004 495.001 4 \$7.R. 450,879 454,877 454,476 455,479 454,476 See Nois A.Sn No 65. 6/D1 F2 200.000 200.00 STATE OF ILLINOIS DEPARTMENT OF PUBLIC WORKS & BLDGS THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION - SLAB THICKNESS (7') DIVISION OF HIGHWAYS TABLES OF ELEVATIONS 6/90.6/ 40,000 400,000
400,000 SPANS C22 THRU C25 57R. 453,006 423,944 423,451 423,451 423,452 423,453 4 POPLAR STREET BRIDGE APPROACHES \$7.R. 438,450 453,551 ROADWAY "C" \$7.R. 454.296 454.201 454.101 454.003 454.011 455.004 455.004 455.004 455.007 455.004 455.007 455.004 455.007 455.004 455.007 455.004 455.007 455.004 GIRD, C2 484,545 454,771 454,684 454,737 454,685 454,537 454,685 454,537 454,685 454,537 454,681 454,737 454,681 454,737 454,681 454,737 454,681 455,533 455,235 455,235 455,235 455,235 F. A. I. RT. 70 ST. CLAIR CO. SECTION 82-3HVB SHEET H. W. LOCHNER. INC. ENGINEERS 78 of 24/ CHICAGO. ILLINOIS

18 2MR

																		D.	L. DE	FLECTI	ON (F1	)											70					114
						-	SPAN	C 26											s	PAN	C 27									-			v C 28		ILLING	)   PRO	rec i	
+	1.8	L18.5	118	118.5	119	119.5	120	120.5	121	121.5	122	122.5	123	123.5	124	124.5	125	125.5		126.5	127	127.5	128	128.5	129	129.5	130	130.5	131	131.5	132	132.5			134	134.5	135	/35.5
+	.000	,008	.21	•13e	.350	.056	.055		.037	.023	,011	.002		.009	.024	.043	.061	.078	,089	.094	.091	.082	.066	.047	.077	.011	.000		.002	.004	.013	.020	.024	.024	.019	.011	.003	,000
	.000													1		1						İ						1	1		1		1		1		1	
																	THEO	RETICA	L ELEV	ATION	TOP OF	CONCR	RETE															
. 41	.913	450,842	490.770	450,681	450,590	450,476	450,360	45.043	450.124	450,003	449.880	449.756	449.630	449,500	449.368	449.237	449.106	448.975	448.844	448.713	448.582	448.451	448,320	448.189	448.058	447.930	447.803	447.674	447,545	447.416	447.287	447.159	447,030	446.901	446.772	446.643	446.515	446.386
								450.875																														
45	2.193	452, 119	452.045	451.955	451,866	451.752	451.632	451.515 452.155	451.401	451.279	451.152	451,658	451,547	450,775	450,641	450,510	450,383	450,251	450,116	449.985	449.859	449.727	449,592	449,461	449,334	449,206	449.715	448,947	448.822	449,332	449,200	449,071	448.947	448.817	448.684	448.556	448.432	448.302
2 45	3.473	453, 402	453,390	453,241	453.150	453.036	452.920	452.803	452.684	452.563	452.440	452.316	452.190	452.050	451.928	451.797	451,666	451.535	451.404	451.273	451.142	451.011	450,880	450,749	450.618	450,490	450,363	450,234	450,105	449.976	449.847	449.719	449,590	449,461	449.332	449,203	449,075	448.946
																			ION TO																			
								450,292		450,027	449,891	449.758	449.630	449.509	449.393	449.281	449.168	449.053	448.934	448.808	448.674	448.533	448.386	448.236	448,086	447,941	447,803	447.670	447.543	447.421	447.301	447.180	447.055	446.925	446.792	446.655	446.518	446.385
8.00								450,924 451,564		450,663	450,523	450,391	450.267 450.907	450.785	450,665	449.913 450.553	449.805	449,689	450,206	449,440	449.311	449.169	449.659	449,509	449,362	448.578	449.075	448,942	448.820	448.697	448.573	448,452	448.332	448,201	448.064	447.928	447.795	447.661
45	2.833	452.767	410.707	452.634	452,558	452.448	452,328	452.204	452.078	451.943	451,803	451.671	451.547	451.425	451.305	451.193	451.085	450,969	450,846	450.720	450.591	450.449	450,299	450.149	450,002	449.858	449.715	449,582	449.460	449.337	449,213	449.092	448,972	448.841	448.704	448,568	448.435	448,301
2 4	3,473	453,410	453,352	453,260	453,201	453,092	452.976	452.852	452.721	452.587	452,451	452.318	452.190	452,069	451,953	451.841	451.728	451.613	451,494	451.368	451.234	451.093	450.946	450.796	450.646	450,501	450.363	450.230	450,103	449,981	449.861	449.740	449,615	449.485	449.352	449,215	449,078	448.945
																			F CONC											*** ***	446 710	115 506	416 471	116 242	445 200	446.670	445 035	175.60
27 4	K.330	450,267	450,209	450,136	450,057	449,949	449.833	449,706 450,341	449.578	449,443	449.338	449.175	449,683	449,976	449.442	448.697	448.585	449,106	448.953	448.225	448.091	448,586	448.435	448.285	448.139	447.934	447.852	447.719	447.597	447,474	447.350	447.229	447,108	446.978	446.841	446.705	446.572	446.438
45	1.510	451,543	451.483	451.411	451.335	451,225	451,105	450,981	450.855	450.719	450,580	450.447	450,323	450,202	450,082	449,970	449,862	449.746	449,623	449,497	449.367	449.226	449.075	448.925	448.779	448.634	448.492	448,359	448.237	448.114	447.990	447.869	447.748	447,618	447.481	447.345	447.212	447.07
4	2.250	452, 183	450.123	452.051	451.975	451.865	451.745	451.621	451.495	451,359	451,200	451.067	450,963	450.842	450.722	450.610	450.502	450,385	450,263	450.137	450,007	449.866	449.715	449.565	449.419	449.274	449.132	448.999	448.877	448.754	448.630	448.509	448.388	448.258	448.121	447.985	447.852	447.71
5 +	32.995	452.827	450.769	452,676	452.617	452.509	452,393	452.268	452.138	452.003	451.868	451.735	451.606	451.486	451.370	451.257	451.145	451.030	450,911	450.795	450.651	450,510	450,363	450,213	450,062	449.918	449.779	449.040	447.50	****	447.273	145.150	443.03.	443.20.	*****	44	10,110	*******
															D. L.	DEFLE	CTION	(FT.)																				
						-				-	PAN	C 29	7	-			-				7	SP	AN C	30	_		7					ш		/				
				Ī	FLCCR	/36	/36.5	/37	/37.5		1	-	/39.5	140	140.5	141	141.5	142	142.5	143	143.5	B // I	1	*	145.5	146	146.5	L 19				н.						
					g E A M S	.000	.005	.016	.030	.043	.051	.054	051	.042	.029	.016	.005	.000	,0C4	.012	.023	.033	.039	.039	.034	.023	.007	.000					- 1					
																			F CONC																			
								446.000																														
								446.637					445.932 446.632																									
								447,917				447.401	447.272	447.139	447.011	446,886	446.756	446,624	446.495	446.371	446,241	446,108	445,980	445.856	445.727	445.596	445,508	445,422										
					GIAD. C	448.817	448.688	448.560	448.431	449,302	448.173	448.044	447.916	447.787	447.658	447,529	447,400	447.272	447.143	447,014	446.885	446.756	446.627	446.499	446.370	446.241	446,151	446.062										
													ORETICA										107	140.000	413.545	1/2 704	442 500	443.600										
								446.017 446.654																														
					STR.	447.529	447.407	447.294	447.178	447.058	446.938	446.816	446.683	446.541	446,400	446,263	446.122	445.984	445.859	445.744	445.624	445,502	445,379	445,256	445.122	444,980	444.875	444.782										
								447.934 448.577																								See	Vore	4 - 3	er. No	65		
					GIRD C	449.617	448.694	448.577	448,462	448.345	449.225	448.099	447.967	447,829	447.688	447.545	447,405	441.212	447.147	447.026	446.308	440.703	440.007	440,530	446,403	440.204	440.155	440.002							TE OF			
										_			LEVATI					255	COT/ON	- 61 40	TILLER	VECE (7	-									DE	PARTM		F PUBL ON OF			BLDG
					GIPD C	145.676	445-551	445,433	445,318															443.395	443.261	443.121	443,015	442,910							OF E			s
						445.326			445.954	445,834	445.715	445,593	445.460	445.318	445.177	445,039	444.899	444,760	444,636	444.520	444.401	444.278	444.156	444.032	443.898	443,756	443,652	443,559							S C26			
								446.710					446.100																			PC	PLAR		DADWA		APPRO	ACHI
								447.350																								F. A	I.RT. 70	o st	. CLAIR	co. s	SECTION	82-3
2					GIAD. C	440.254																												H. W. 1	OCHNER.	INC.		5H
21	12																																		NGINEER!	5		

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													0	055	i ECTIO	ON (FT.)														F. A. I7	0 82-31	VB ST	CLAIR	Z89	115
																					-	PAN	A 26							FED. ROA	D DIV. NO. 4	ILLINO	IS PROJEC	1.	
			-		-	_	PAN A					Τ.				7	1	8	8.5	9	9.5	10	10.	5 11	11.5	12	12.5	13	/3,5						
WS.	LI	L 1.5	1	7.5	2	2,	5 3		3.5	4	4.5	5	5,5	6	6.5		7,5	-	_	-	-	-	-		-			-							
	.000	.015	.039	.758	,069	,:	.0	268	.057	.241	. 224	.009	,001	.000	.003	.011	.024	.040	056	.069	.078	•082	.07	,067	.054	.038	.022	.010	.002						
																TOP OF																			
4)	415.7%	47.,167	477.294	470.0	17.54	471.	09 471,	457 47	71.593	471,318	472.131	472.332	472,521	472,699	472.856	473,002	473.138	473.263	473.378	473.483	473,577	473.661	473.73	4 473.797	473.850	473.892	473.924	473,945	473.956						
	449,230	469,521	469.75	470,02	470,300	47.	564 470.	813 41	71,048	477.274	471,486	471,688	471.876	472,055	472,21	472.358	472.493	472,620	472.734	472.839	472,933	473.017	473.09	0 473,154	473,205	473,248	473,279	473,301	473.311						
	468,652	468,881	469.110	469,300	443,640	469.	24 470.	173 4	70,408	170,534	47.,846	471.048	471.237	471.415	471.57	471.719	471.854	471,360	472.094	471.560	471.653	471.737	471.81	0 472.514	471.926	471.969	471.999	472.002	472.032						
	468.012	458.241	458.47	468.70	469.3	469.	284 469.	533 44	69,768	169,994	470,206	410.408	440.061	47. 120	470.00	470.442	470.570	470,703	470.818	470.923	471.017	471.101	471.17	4 471.237	471,290	471.332	471,364	471.385	471.396						
2	457,577	45.60	467.834	458.	468,38	468.	147 468.	87 4	69.133	449,500	403.00	402.712	******	*****	* // **	410.44	410.370	410.100	4.010																
										TH	EORET	ICAL E	LEVATI	ON TOP	OF C	ONCRET	+ D.L.	DEFLEC	ATLAN	479.660	473.655	473.74	3 473.81	2 473,865	473,904	473,930	473,946	473.955	473.958						
41	449,933	477.185	47.,43	47.79	271.01	5 471.	282 471.	.26 4	(7), (7)	471,253	477, 150	471 697	472,522	470.065	479.91	5 479.370	472.518	472,660	472.790	472.909	473,011	473,099	9 473.16	7 473,222	473.260	473,286	473,301	473,311	473.314						
	469,290	469.534	109.79	45,09	0 455.77	e 250.	991 47.	.242 4	17.444	47.475	47.47	471.057	471,23	471,415	471.57	5 471.730	471.878	472.020	472.150	472.269	472.371	472.460	472.52	7 472.582	472.620	472.647	472.662	472.672	472.674						
	448.77	458,254	458,51	458.81	469,09	4 455.	357 469.	.602 4	169.25	17.73	470,230	470,418	470,59	470,775	470.93	5 471,090	471.238	471,380	471.511	471.629	471.731	471.820	471.88	8 471.942	471.980	472.007	472,022	472.032	472.034						
2	467.37	467,623	467,67	453.17	5 455,45	9 468.	72 468	.966	459.191	455,400	459,595	469.782	469,96	470,139	470.29	9 470.454	470,602	470.744	470,875	470,993	471,095	471.18	3 471.25	2 471,305	471.344	471.370	471.386	471,395	471.398						
								7+	HECRE	TICAL	ELEV.	ATION	TOP C	CONC	RETE +	AL. DE	FLECTI	ON - SL	AB THI	CKNES5	(7")								-						
	455.34	100.00	469.85	17.0	2 17.1	25 470	490 470	.942	471,167	171,275	471.57	471.758	471,93	472,116	472.27	6 472.431	472.579	472.720	472.852	472.969	473.072	473.16	473.22	8 473,282	473.321	473.347	473,363	473.372	473.375						
	444.70	444.00	445,50	445.5	. 419.7	470	.054 470	.298	47.50	17.72	470.92	471.114	471.29	471.472	471.63	1 471.787	471.935	472.077	472.207	472.326	472.428	472.51	6 472.58	472.638	472.676	472.703	472.718	472.728	472.731						
	468,06	458.31	461.56	6 244,86	459.1	1 469	414 469	.658	469,883	17,090	470,28	470.474	47.,65	470,830	470.99	1 471.147	471.295	471.437	471.567	471.686	471.788	471.67	6 471.94	471.998	472.037	472.063	472.078	472.088	472.091						
2.	46",49	447.67	117.70	468.00	* 444.5	11 408	.774 469	.:18	469,242	489.42	469,64	469.834	470,01	4 470,192	470,35	2 470,507	470.655	470,797	470,927	471.046	471.148	471.23	6 471.30	4 471,358	471.397	471,423	471.438	471.448	471.451						
42	466.78	467.03	467.29	0 457,59	K 41".1	7 466	.139 468	.×.	+68.50*	468.816	469.01	469.196	469.37	9 469,556	469.71	6 469,871	470.019	470,161	470.292	470,409	470.512	470,60	0 470,00	58 470,722	470,761	470.787	470,803	410.812	470.815						
													0	DE	LECTI	ON (FT.)													-						
_	-					_		5.2	DAN.	4 27				. 527		311,					/		5	PAN A	28	17			71	7					
9		14.5	15	12.5	16	16.5	1.7	17	7,5	/ê	8.5	19	19.5	20	20.5	21	21.5	22	22.5	23	23.5	24	24.5	25	25.5	26	26.5	27 2	7.5 L2		Y				
S		-	-		-		-	-	-	_	-	-	.056	_	.024	- 10	.003	.000	.001	.009	.024	/01	.057	_	.073	.069	.056	.039	.015 .0	·					
1	,000	.002	.010	.022	, 238	.754	. 4			. 40		.009	.000		.02.														1	1					
											B1 484	THEOR	ETICAL	ELEVA	73.612	TOP OF	CONCH 17.710 4	E/E 172.544 4	72.356 4	72.156 4	71.945 4	71.722	471.487	471.240 4	70.982 4	70.712 4	70.430 4	70.136 46	9.901 469.6	62					
-	-7.8%	173,546	173.905	473,895	473,853	475.801	475.739	475.	100	7.583 4	77,490	470.740	73.272	179.503	72.367	477.223 4	72.06€ 4	71.900 4	71.711 4	71.512 4	71,300 4	71.078	470.842	470,596	70.337 4	70.068 4	69.785 4	69.493 46	9,259 469.0	22					
						V = 112	17. 152	17	100 17	7. Y. 6	70.954	477,103 4	71.987	71.864	71.728	471.583 4	71.426 4	71.260 4	71.071 4	70.872 4	70.660 4	70.438	470,202	469.956	69.697 4	69,428 4	69,145 4	68,853 46	8.619 468.3	82					
		· * ***	× 44	121 52	477.33	471.177	471,816	471.	742 17	1,660 4	77,566	471,463	71.347	171.224	71.088	470.943 4	70.786 4	70,620 4	70.431 4	70.233 4	70.020 4	69.798	469.562	469.316	69,057 4	68.788 4	68,505 4	68,213 46	7.979 467.7	42	,				
:	17,196	471,385	471,366	471,335	477,293	471.241	471,173	471.	106 47	1,021 4	7.,930	47.826	70.712	170,587	170,452	470.306	70.150 4	69.984 4	69.796 4	69,597 4	69,385 4	69,162	468,927	468.680	68,422 4	68.152 4	67.870 4	67.576 46	7.341 467.1	02					
																ONCRET																			
	175,356	475.345	173,336	4"1.51"	477.89	173,198	477,807	473,		5.66	72.568	173.455	73,328	473.187	73,036	472.878	472.714 4	172.544 4	72.357 4	72.166 4	71.969 4	71.763	471,544	471.309	71.055 4	70.781 4	70.488 4	70.176 46	9.916 469.6	62					
			. 00 . 00		175 573	,	100 164	475	194 17	4. 50 1	7.94	477.812	172.684	472.544	172.392	472,235	472.069	471,900 4	71.712 4	71.522 4	71.324 4	71.119	470.899	470.665	70,410 4	70.137 4	69.843 4	69.533 46	9.274 469.0	22					
				796 776	(** 163	15.15	17.51		.46. 47	7.381 4	72.284	472.172	172.044	471,904	471.752	471.595	471.429	471.260 4	71.072 4	70.882 4	70.684 4	70.479	470.259	470.025	69.770 4	69.497 4	69.203 4	68.893 46	8.634 468.3	82					
	472.000	47.74	477.012	4*1,933	1***,963	4"1,930	471,884	471.	.85		121.544	471,532	471,404	471,264	471.112	470.955	470.789	470.620 4	7.432 4	70.242 4	70,044 4	69,839	469,619	469,385	69.130 4	60.857 4	67.000 4		7.994 467.7		Note A -	Sh. No.	65.		
43	271,396	471.389	471,376	471,357	4"1,35"	471,096	471.24	7 471.	. 154 4	1,104	471,009	47895	470.768	470,627	470.476	470.318	4 10.154	469.984 A	69.797 4	67,606 4	03,403 4	67.203	400,304	468.749	00.133 4	ovecci 4	w., 200 A	U., UIU 40	7.356 467.1	~		TE OF			

THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION - SLAB THICKNESS (7')

SIPA AI (2015) 470.00

\$7.8. 47.75 47.75 47.75 47.55

\$7.70 x71.00 x71.01 x71.00 x71.01 x71.00 x71

\$72 miles critical cr

2 3 4 5 6 7 8 8 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24

STATE OF ILLINOIS
DEPARTMENT OF FUBLIC WORKS & BLDGS.
DIVISION OF HIGHWAYS
TABLES OF ELEVATIONS

SPANS A25 THRU A28
POPLAR STREET BRIDGE APPROACHES

POPLAR STREET BRIDGE APPROACHE
ROADWAY "A"

F.A.I.RT.70 ST. CLAIR CO. SECTION 82-3HVB

H. W. LOCHNER. INC. SHEET
ENGINEERS CHICAGO. ILLINOIS BO 0424/

ROUTE NO.	SECTIO	ON.	cou	NTY	TOTAL	SHEET NO.
F. A. I70	82-3H	v B	ST. C	LAIR	285	//6
FED. ROAD DI	V. NO. 4	- 11	LINOIS	PROJE	CT	

						5	PAN	м 6									SP.	AN M	5										PAN					
LOOR EAMS	L2	15.5	15	5 1	4.5	14	/3.5	/3	12.5	12	11.5	11	10.5	10	9.5	9	8.5	8	7.5	7	6.5	6	5.5	5	4.5	4	3.5	3	2.5	M 4	45	,	, , , ,	Τ.
	.000	.004	.0	25	.039	.046	.045	.037	.025	.012	.002	.000	.004	.014	.028	.042	.052	.095	.052	.042	.028	.014	.004	.000	,000	,012	.025	.037	,045	.046	.039	.025	.006	-

#### THEORETICAL ELEVATION TOP OF CONCRETE

GIRD.MI 477,802 477,912 476,016 476,116 476,116 476,116 476,115 476,015 476,016 476,01 \$1.8. 477,100 477,000 STR. 476.502 476.602 476.602 476.602 476.602 476.602 476.602 4776. GIRD.M 2 475.002 475.002 475.002 475.003 475.0

### THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION

GIRD.MI 471.002 471.010 471.001 471.00 \$\frac{1}{2}\$\$FR. 477,005 477, GIRD, M2 475,482 475,193 475,1

# THEORETICAL ELEVATION TOP OF CONCRETE + Q.L. DEFLECTION - SLAB THICKNESS (7")

GIRD WI 477,219 477,515 477,416 477,11 \$\'7.87 4\'7.69 4\'7.6 57R. 478,999 476,695 478,175 476,197 476,997 476,097 476,097 476,097 476,097 476,097 477,097 4

See Note 4- Sn No.65

STATE OF ILLINOIS DEPARTMENT OF PUBLIC WORKS & BLDGS. DIVISION OF HIGHWAYS TABLES OF ELEVATIONS SPANS M4 THRU M6 POPLAR STREET BRIDGE APPROACHES

RAMP "M"

F. A.I.RT. 70 ST. CLAIR CO. SECTION 82-3HVB SHEET

H. W. LOCHNER, INC 81 of 241

BY VB
DBY RMR
ED BY KA

7 + 10 10 11 12 13 14 15 16 17 18 19 20 21

ROUTE NO.	SECTION	4	cou	NTY	TOTAL	SHEET NO.
F. A. I70	82-3HV	В	ST. C	LAIR	289	//7
FED. ROAD D	IV. NO. 4	11	LLINOIS	PROJE	CT	

[	-				SPA	N 513						$\top$		-			5PA	N 512										S	PAN SII					
FLOOR	16.5	16	15.5	15	14.5	14	13.5	13	12.5	12	11.5	11	10.5	10	9.5	9	8.5	8	7.5	7	6.5	6	5.5	5	4.5	4	3.5	3	2.5	2	1.5	ı	LI.5	LI
	\$000	.011	.025	.036	.048	.051	.048	.038	.025	.011	•005	.000	.003	.013	.027	.041	.051	.055	.052	.042	.028	.014	.003	.000	.003	.013	*058	.038	.045	.045	.036	.024	.004	.000

### THEORETICAL ELEVATION TOP OF CONCRETE

GIRD, SI 494,892 494,891 494,497 494,295 494,091 497,794 487,694 485,2 57.7. 494,247 494,647 493,634 493,611 493,274 (493,634 493,611 493,274 (493,634 493,611 493,274 493,614 493,274 493,614 493,274 493,414 493,274 493,414 493,274 493,414 493,274 493,414 493,274 493,414 493,274 493,414 37.8, 493,467 493,467 493,467 493,467 493,467 493,467 493,467 492,497 492,497 492,497 492,497 492,497 492,497 492,497 492,497 493,497 492,497 4

### THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION

\$\text{G}\$\text{L}\$\text{S}\$\text{1}\text{484,894}\$\text{494,793}\$\text{494,595}\$\text{494,697}\$\text{494,697}\$\text{495,697}\$ \$7.7. 494,249 494,059 493,859 493,859 493,452 493,179 425,155 STR. 483,609 493,419 493,219 493,010 420,782 492,500 492,519 493,010 420,782 492,500 482,517 491,999 491,697 491,799 491,697 491,799 490,751 490,425 480,406 489,784 489,410 489,644 480,466 480,468 480,484 4 GFR, 5.2 482,478 482,783 482,585 482,574 482,785 482,585 482,585 482,585 482,585 482,585 485,5

### THEORETICAL ELEVATION TOP OF CONCRETE + D.L. DEFLECTION - SLAB THICKNESS (7")

G/RD S/ 494,311 494,120 493,921 49,710 493,484 493,239 492,976 492,695 492,398 492,092 491,773 491,452 431,127 45,577 457,579 481,719 481,444 482,472 481,140 482,471 578. 493,666 493,476 493,276 493,066 492,839 492,595 422,331 492,051 401,753 491,445 491,128 430,807 490,481 470,153 487,815 STR. 493,006 492,836 492,636 470,426 492,199 491,955 421,691 491,411 491,113 490,006 490,488 400,168 499,487 489,513 489,175 488,461 488.079 GIRD. 52 492,391 492,200 492,001 491,791 491,564 491,320 491,056 490,775 490,470 490,170 489,853 489,530 488,207 488,877

See Note A - Sh. No. 65.

STATE OF ILLINOIS DEPARTMENT OF PUBLIC WORKS & BLDGS. DIVISION OF HIGHWAYS

TABLES OF ELEVATIONS SPANS SII THRU SI3

POPLAR STREET BRIDGE APPROACHES RAMP "S"

F. A. I. RT. 70 ST. CLAIR CO. SECTION 82-3HVB SHEET

H. W. LOCHNER. INC. ENGINEERS 82 of 241

VB RMR KA

ROUTE NO. SECTION COUNTY TOTAL SHEET NO. F. A. I. -70 82 - 3 HVB ST. CLAIR 289 1/8 FED ROAD DIV. NO. 4 | ILLINOIS | PROJECT

					5 8	AN S	/5									SPA	N 514							
LOOR	L2	27.5	27	26.5	26	25.5	25	24.5	24	23.5	23	22.5	22	21.5	21	20.5	20	19.5	/9	/8.5	/8	/7.5	17	
the state of	,000	.004	.224	,038	.045	.045	.038	.025	.013	.003	.000	.003	.014	.028	.042	.062	.055	,051	.041	.027	.013	.003	.000	
40. S /	496,295	496,334	496.368	456,415	436,445	4%,473	496.484	436,484	49.47	4%,449	4%,413	496,396	496.308	496,238	4%,1%	496,063	495,957	495,840	495,711	495,571	495,419	495,256	495,060	
																495,417								
																494,777				134,286	494,135	493.971		
10. S2	454,375	494,414	454.448	194,175	494,929	494,553	494,564	494,564	494.552	434,529	494,493	134,446	494,388	494,318	194,236	494,149	494,037	493,920	493,791	493.65	492,499	493.336	493,160	
DO 51	496.355	290.000a	496. Ye	496,450	496.496	496,518	496,522	496,510	49.46	4%,4%	496,413	49.17	496.322	496.266	494,196	496.115	496.013	495,692	495,753	495,599	495,430	495,259	495,080	
57 R.	495,655	495,695	495,742	495,808	495,851	495,873	495.878	495,865	475.841	495,807	495,759	435,725	495.678	495.621	495,554	195,475	495,369	495,247	495,109	434,3%	454,785	454.614	494.436	
																494,830								
																494,195								
															.~	156.151	495-429	191, 909	495,170	495,516	454.645	69.07	191.197	
											495,430	495,757	175,735	490.583	Max and	495,511 494,686	454,715	494,584	196.25	m.494.378s	494,205	450,630	490.653 = =	_
							- 10	42.22		495.224						494.246						493,390	49742,73	
			493,889	-					W. III	493,949						490,611							492,577	

See Note A - Sh. No. 65.

STATE OF ILLINOIS
DEPARTMENT OF PUBLIC WORKS & BLDGS.
DIVISION OF HIGHWAYS

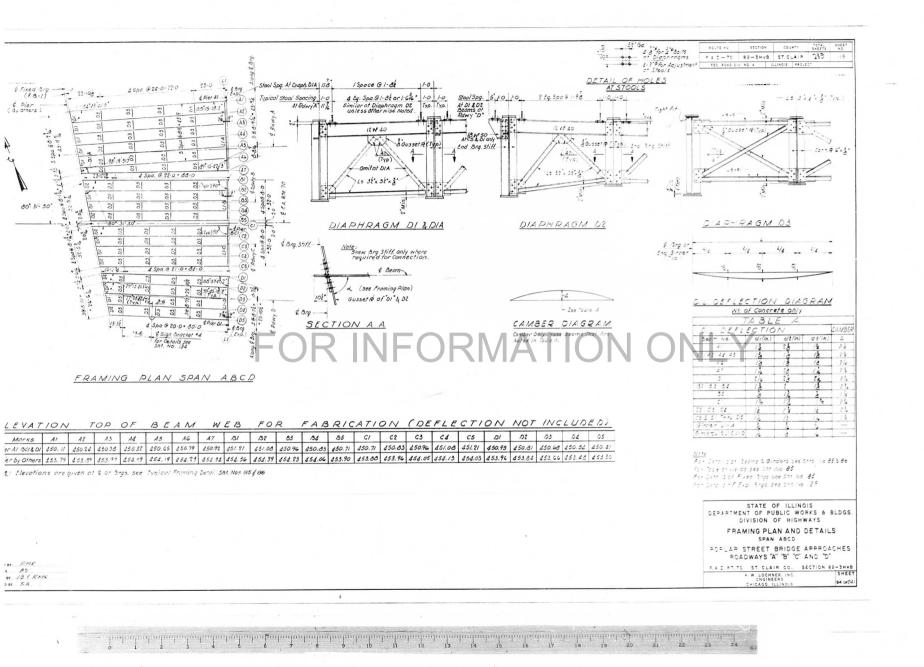
TABLES OF ELEVATIONS SPANS SI4 AND SI5

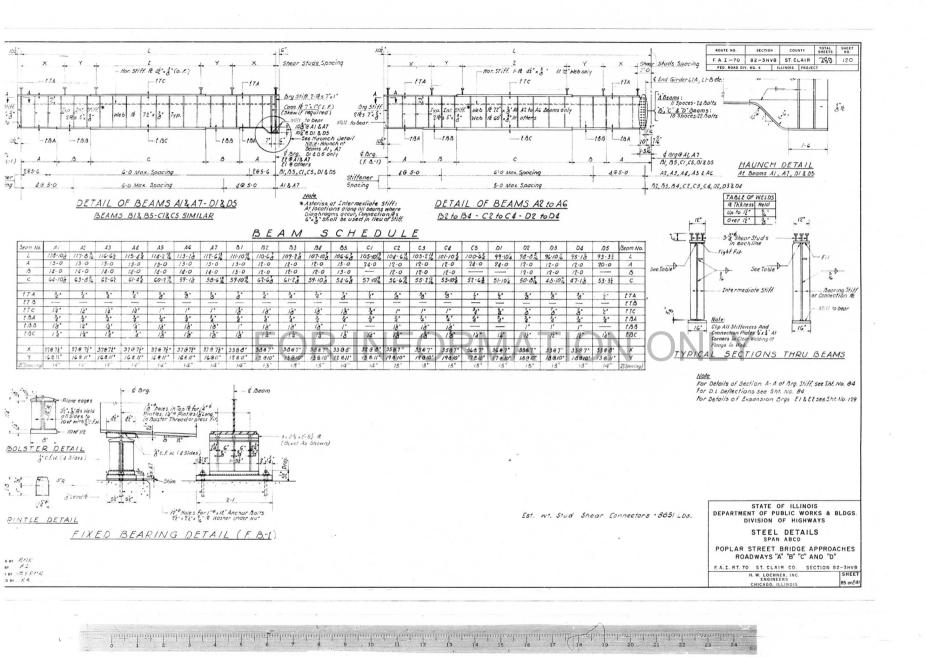
POPLAR STREET BRIDGE APPROACHES RAMP "S"

F. A. I. RT. 70 ST. CLAIR CO. SECTION 82-3HVB H. W. LOCHNER. INC. SHEET

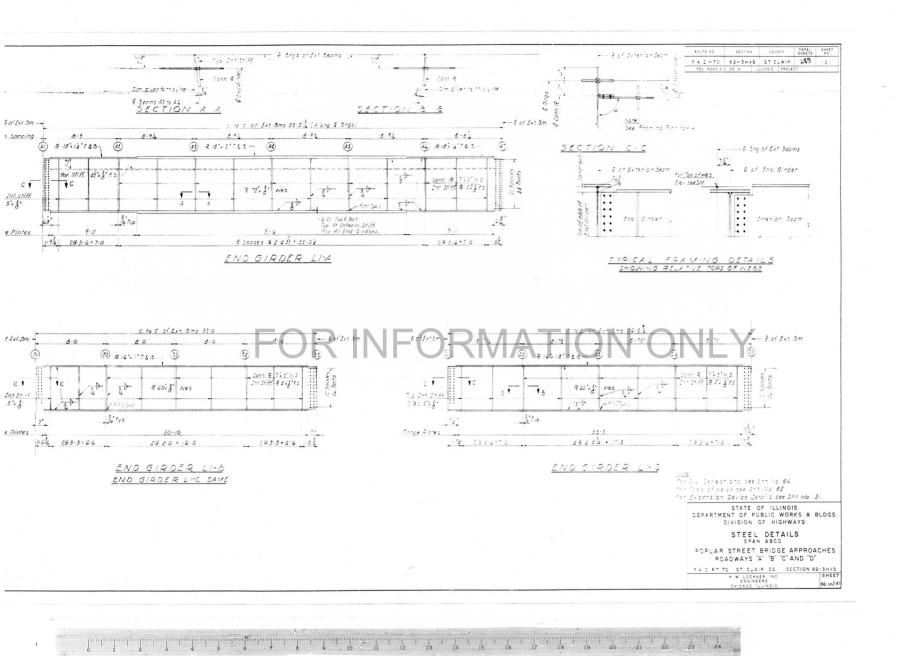
H. W. LOCHNER. INC. ENGINEERS CHICAGO. ILLINOIS

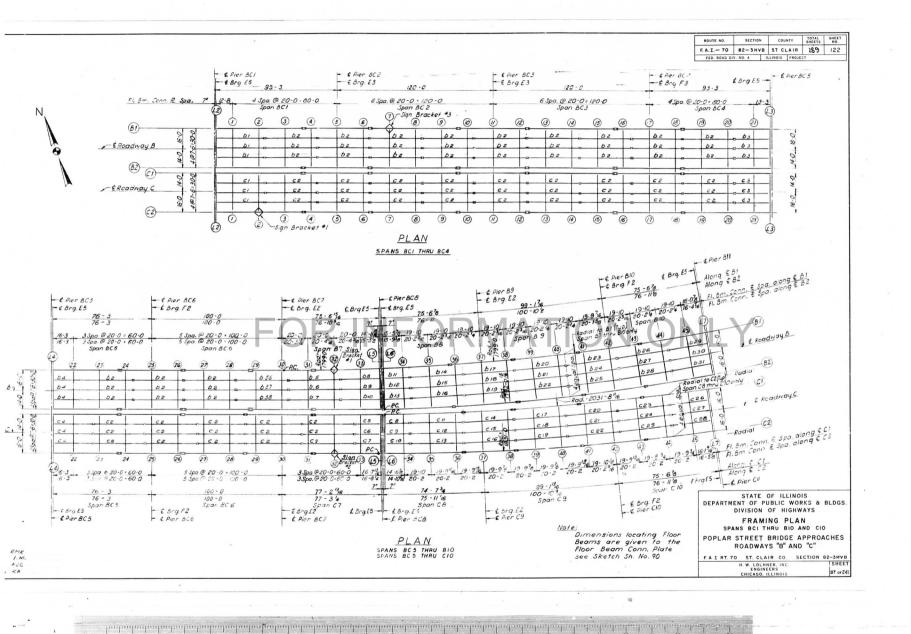
ED BY RMR
BY VB
ID BY RMR
IED BY KA

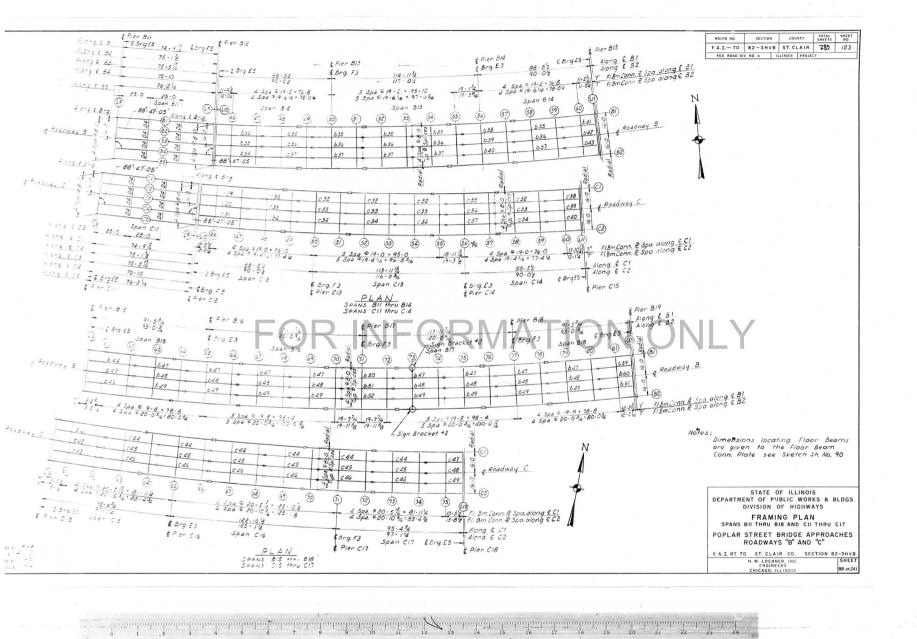


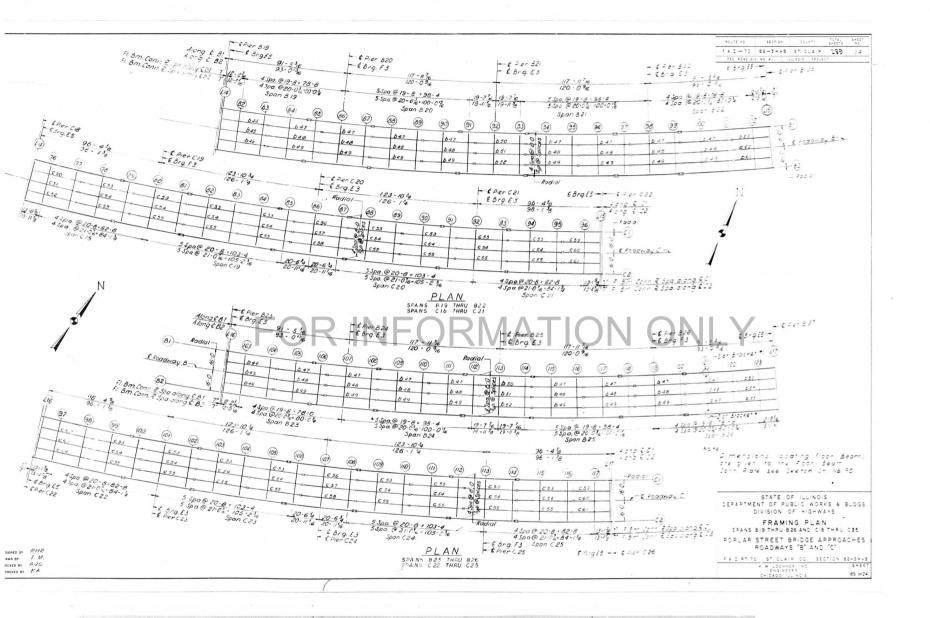


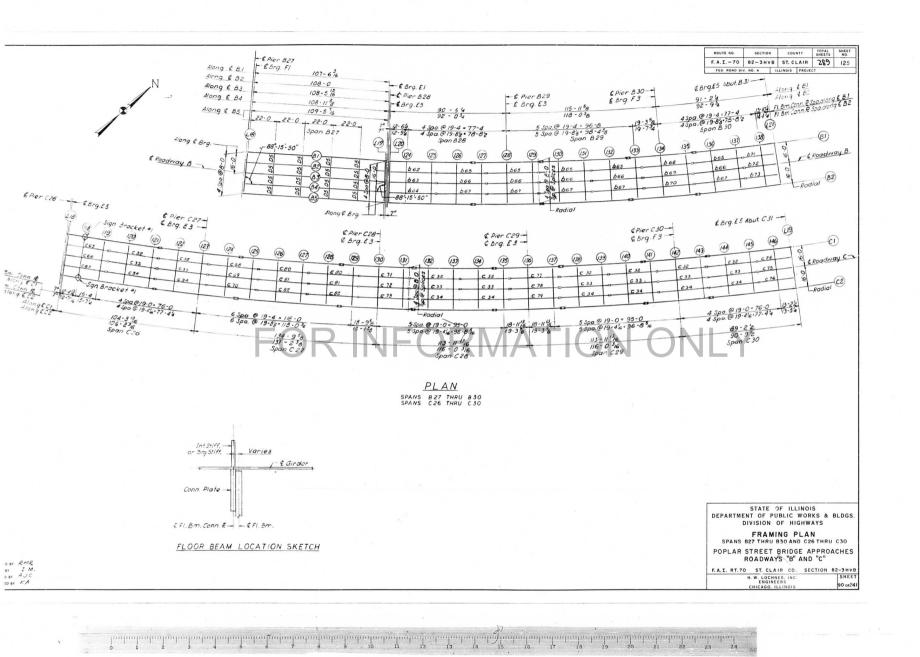
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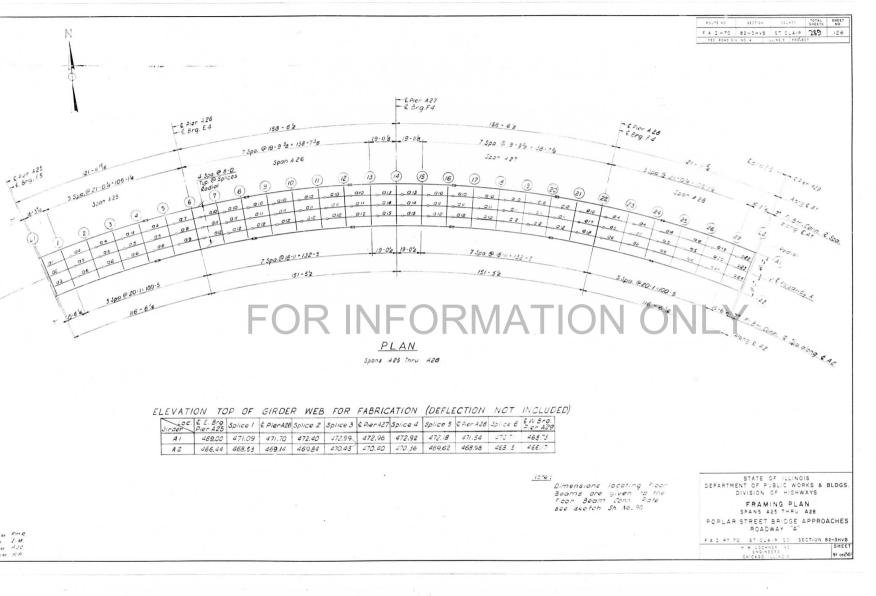








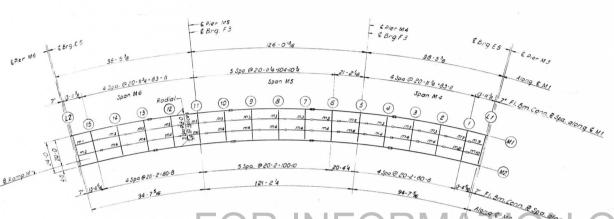




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ripringradiu

SECTION COUNTY TOTAL SHEET NO. ROUTE NO. F. A. I. - 70 82-3HVB ST. CLAIR 389 127 FED ROAD DIV NO 4 LILLINGIS PROJECT



Span M4 Thru M6

ELEVATION TOP OF GIRDER WEB FOR FABRICATION (DEFLECTION NOT INCLUDED)

Girder	€ E. Brg. Pier M6	Splice 4	É PierM5	Splice 3	Splice 2	€ Pier M4	Splice 1	£W.Brg PierM3
MI	476.66	477.64	477.82	477.94	477.76	477.35	477.07	475.67
M2	474.9€	475.72	475.90	476.02	475.84	475.43	475./5	473.75

Note:

Dimensions locating Floor Beams are given to the Floor Beam Conn. Plate see sketch Sh. No. 90

STATE OF ILLINOIS
DEPARTMENT OF PUBLIC WORKS & BLDGS. DIVISION OF HIGHWAYS

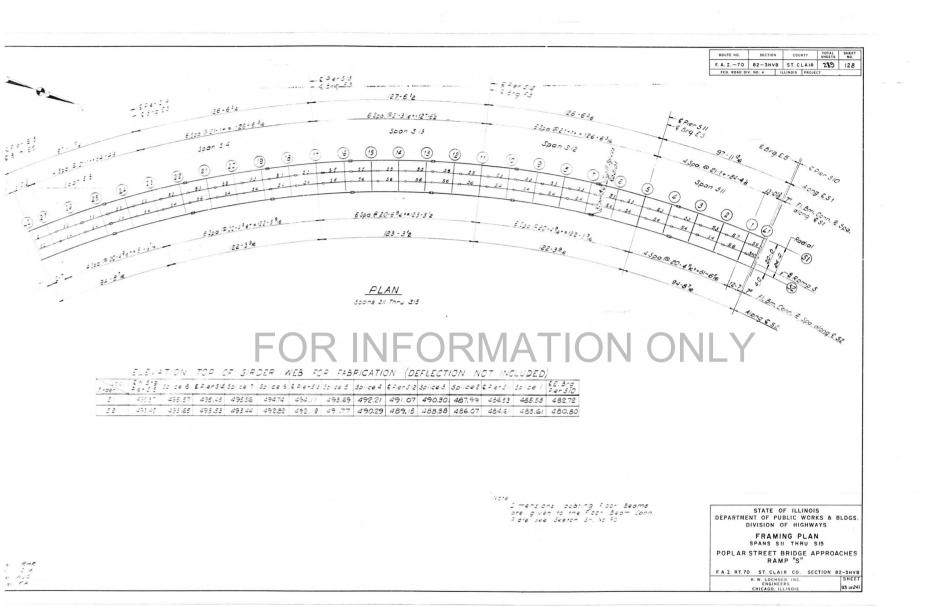
> FRAMING PLAN SPANS M4 THRU M6

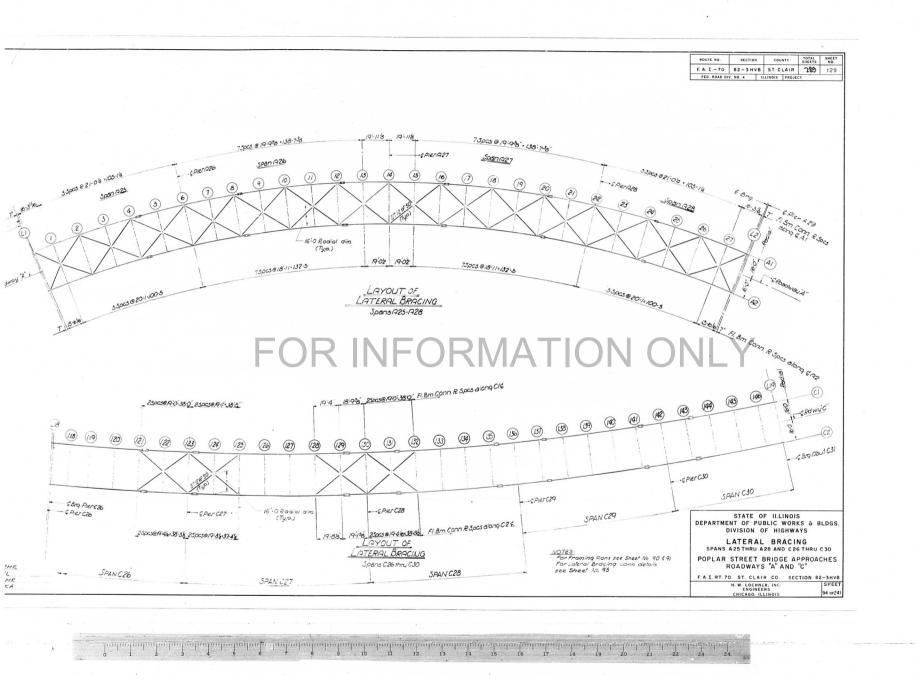
POPLAR STREET BRIDGE APPROACHES RAMP "M"

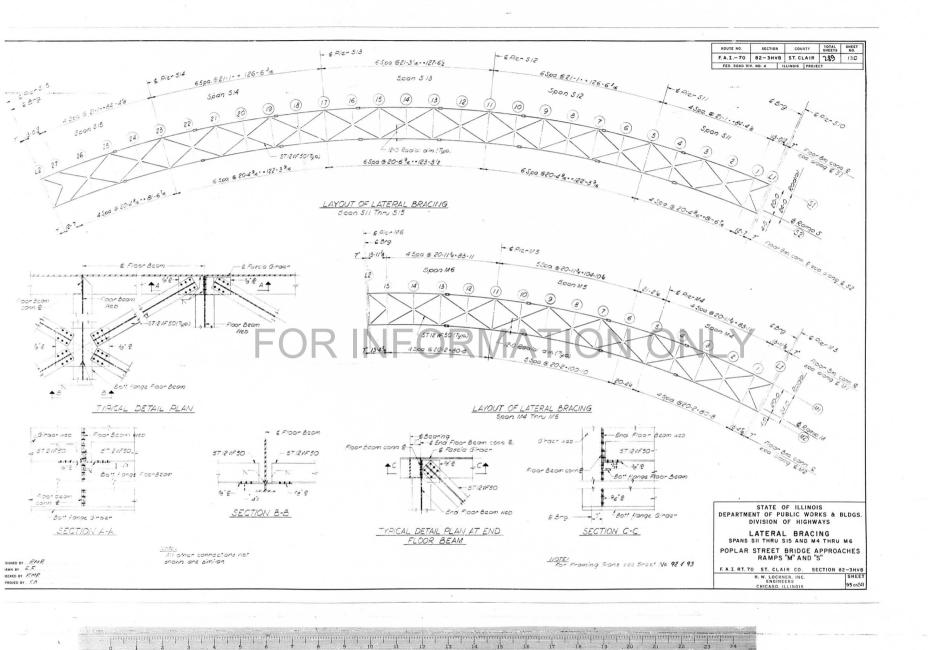
F. A. I. RT. 70' ST. CLAIR CO. SECTION 82-3HVB SHEET H. W. LOCHNER, INC. ENGINEERS CHICAGO, ILLINOIS

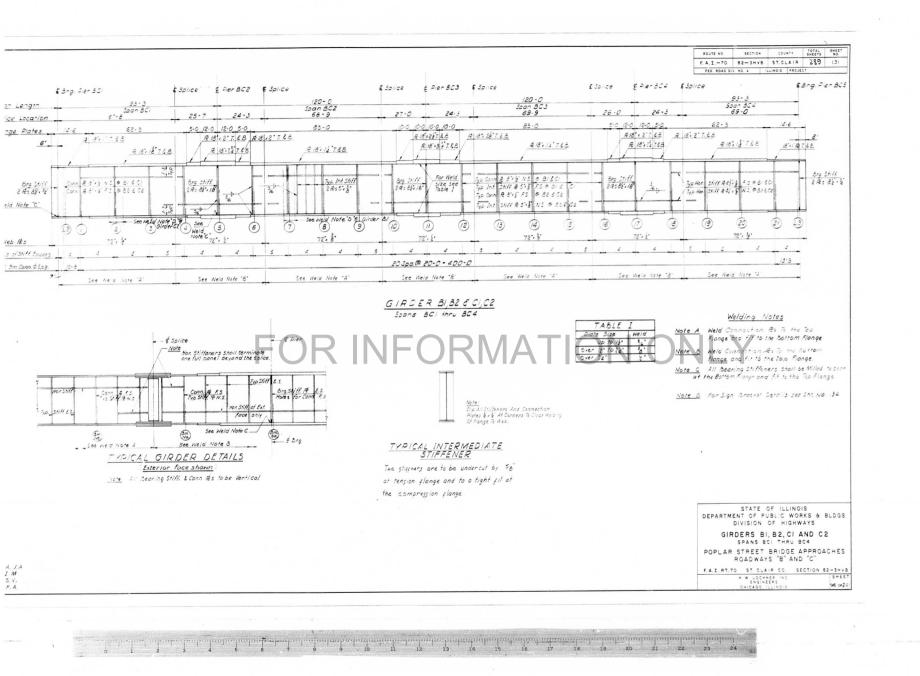
92 of 241

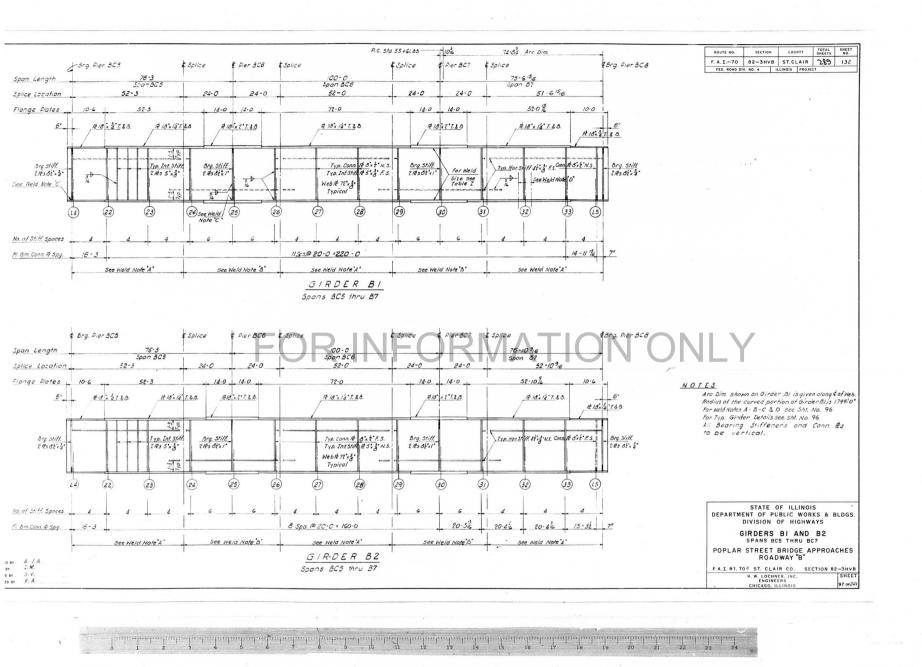
I.M. Y AJC BY KA

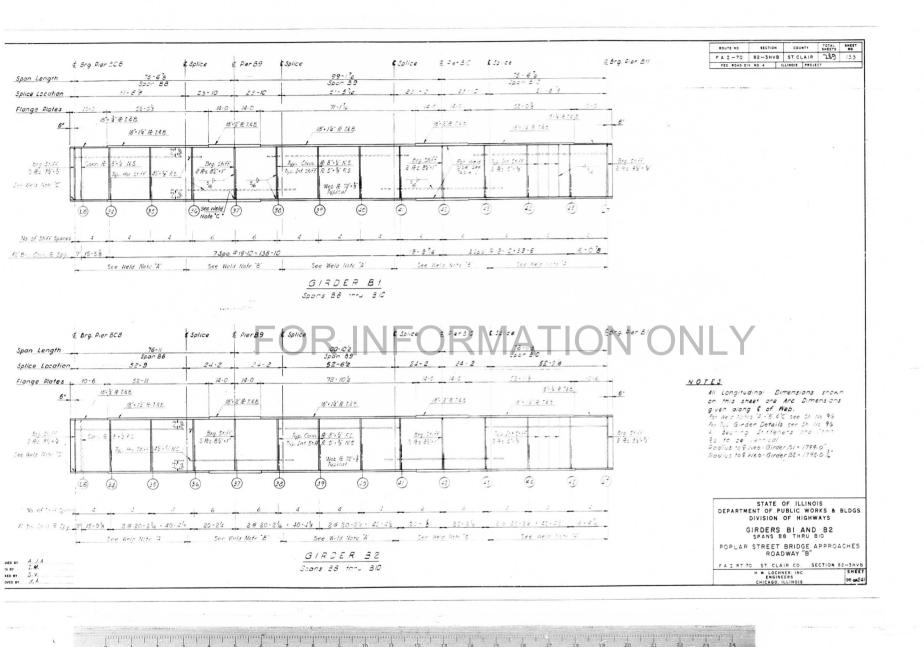


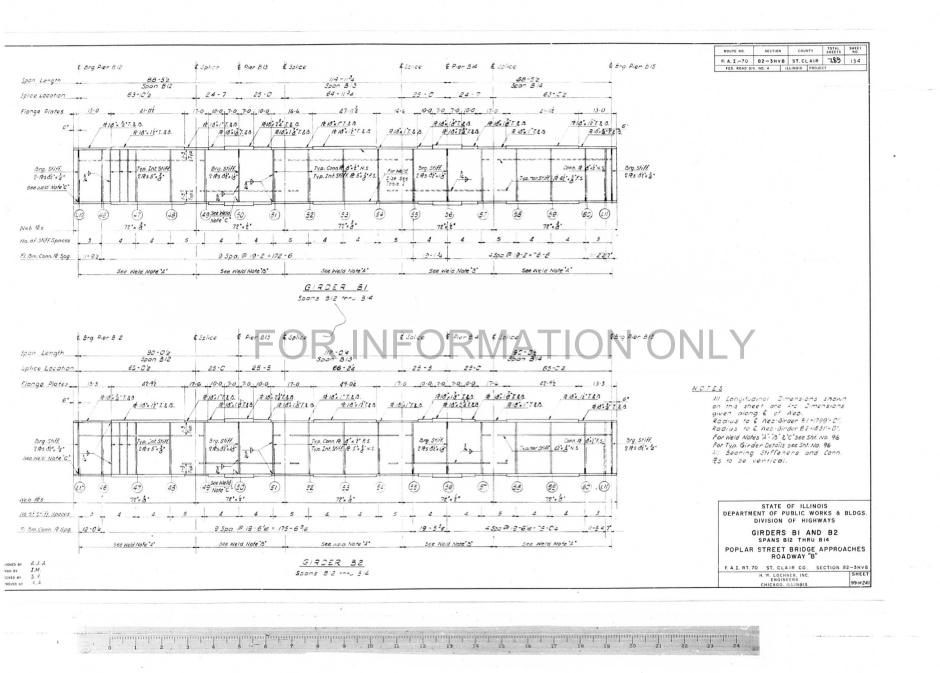


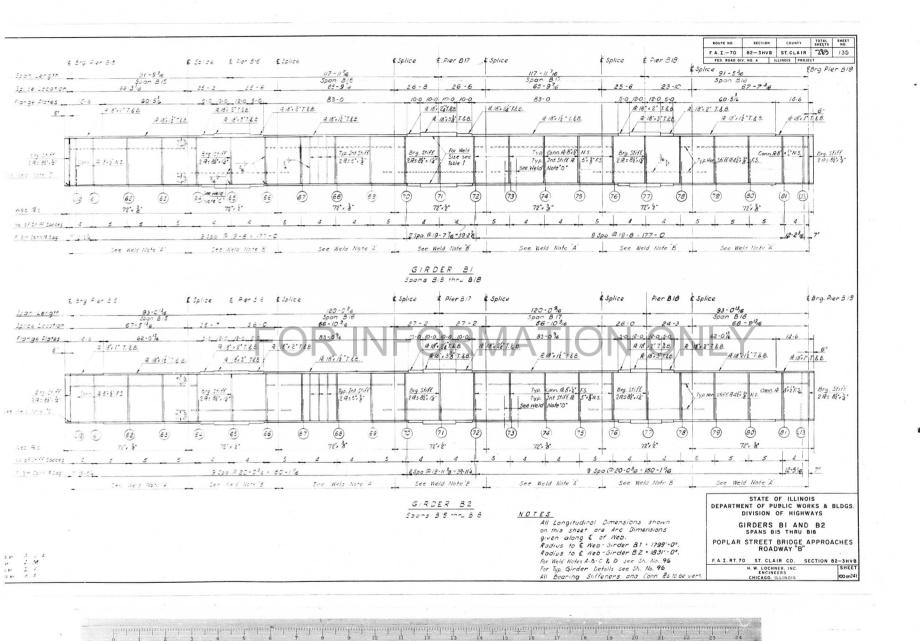


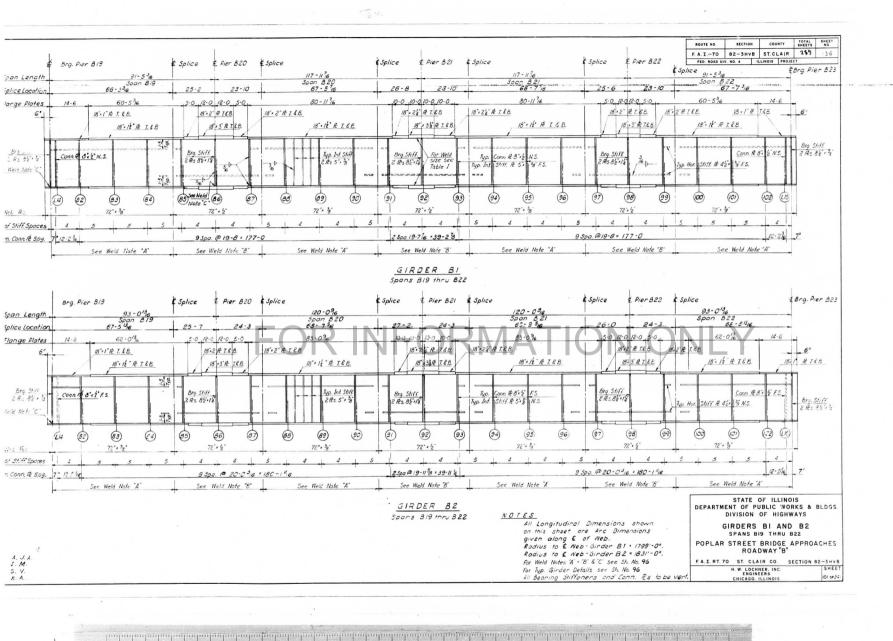


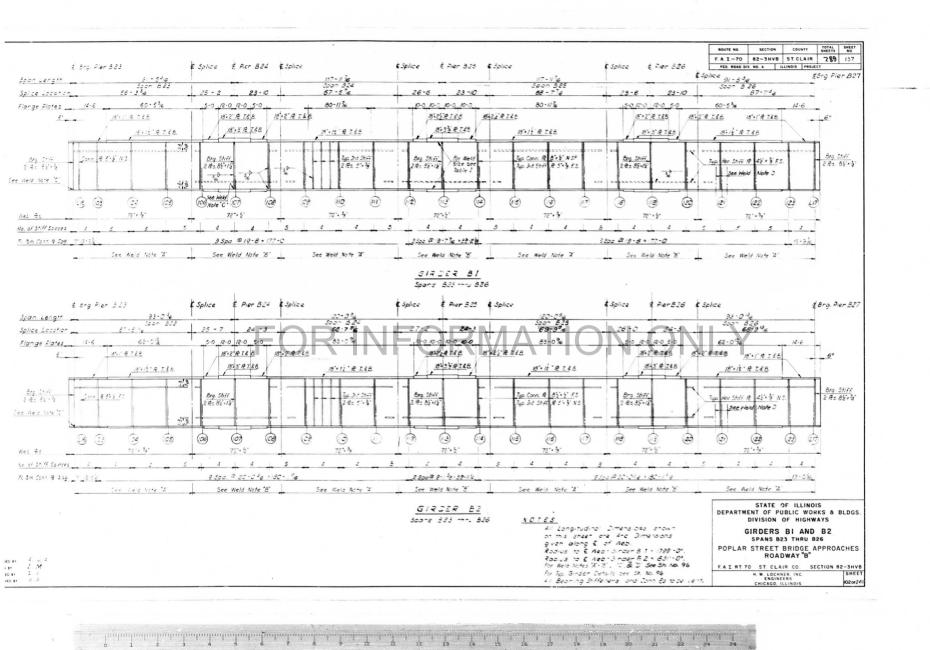


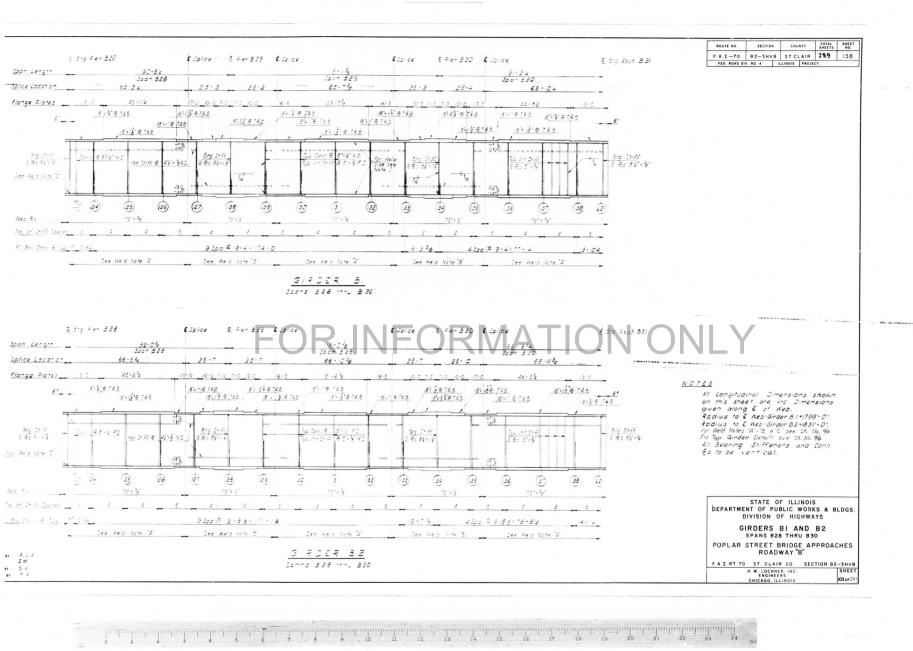


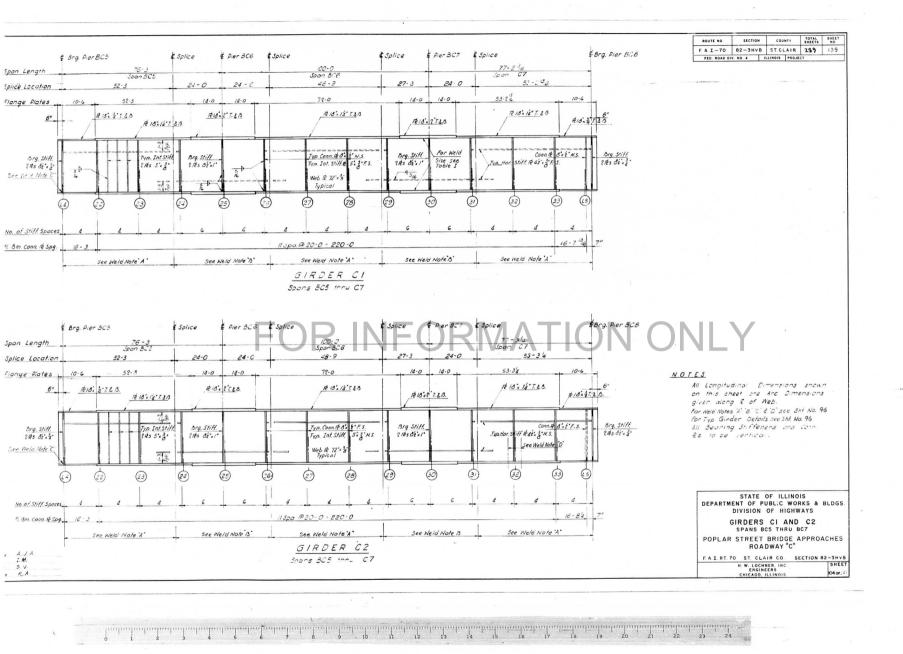


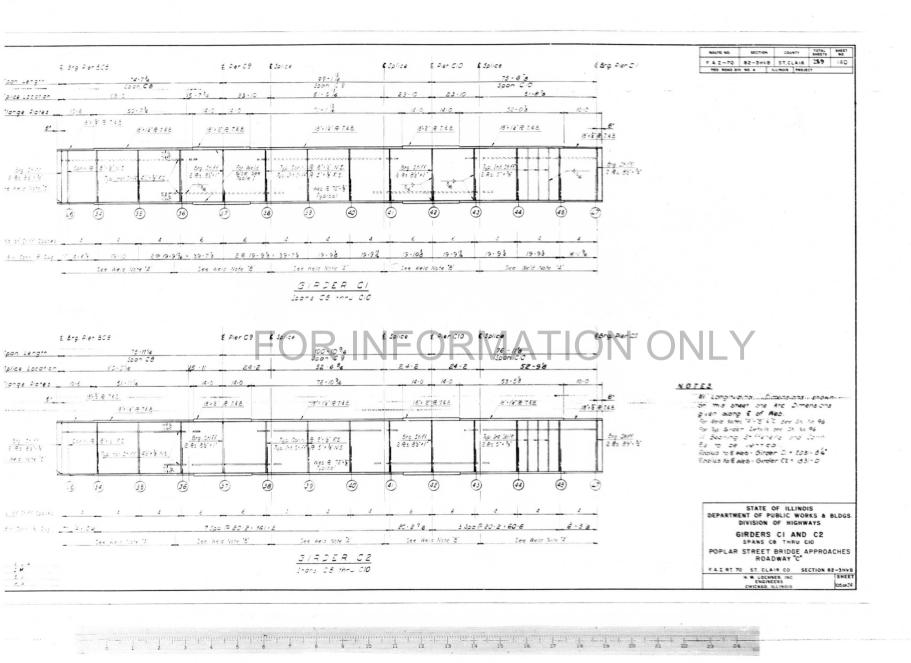


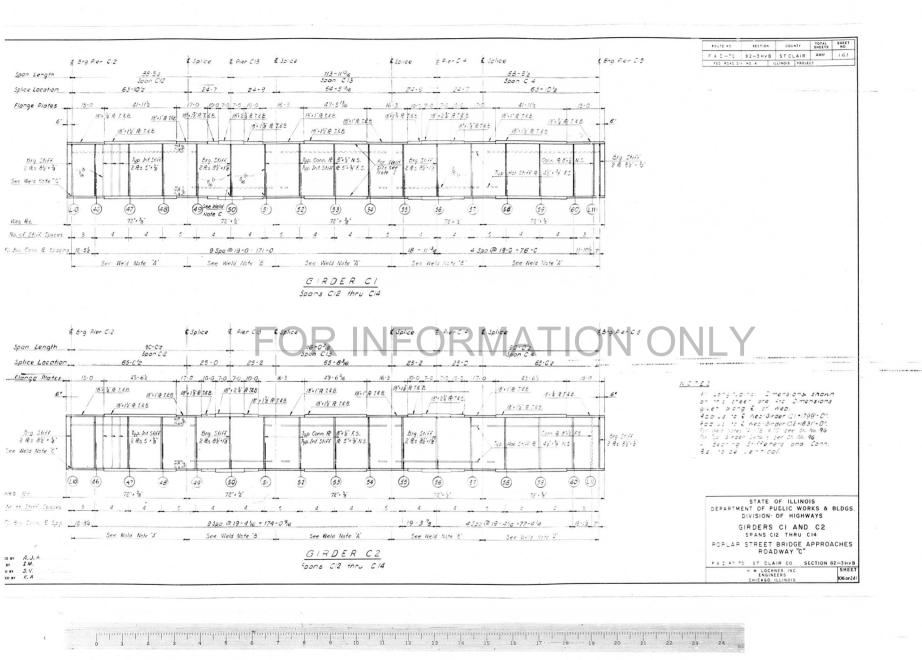


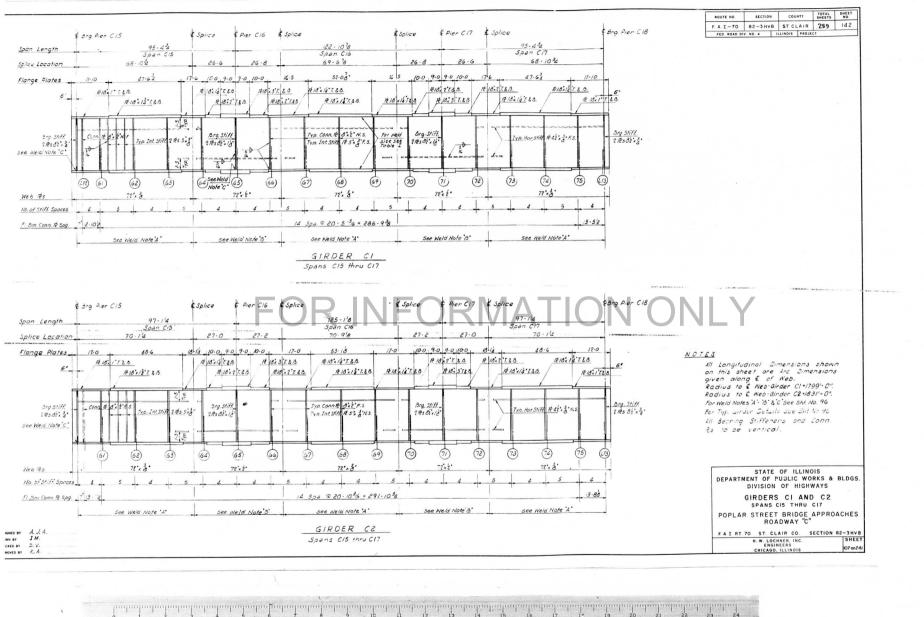


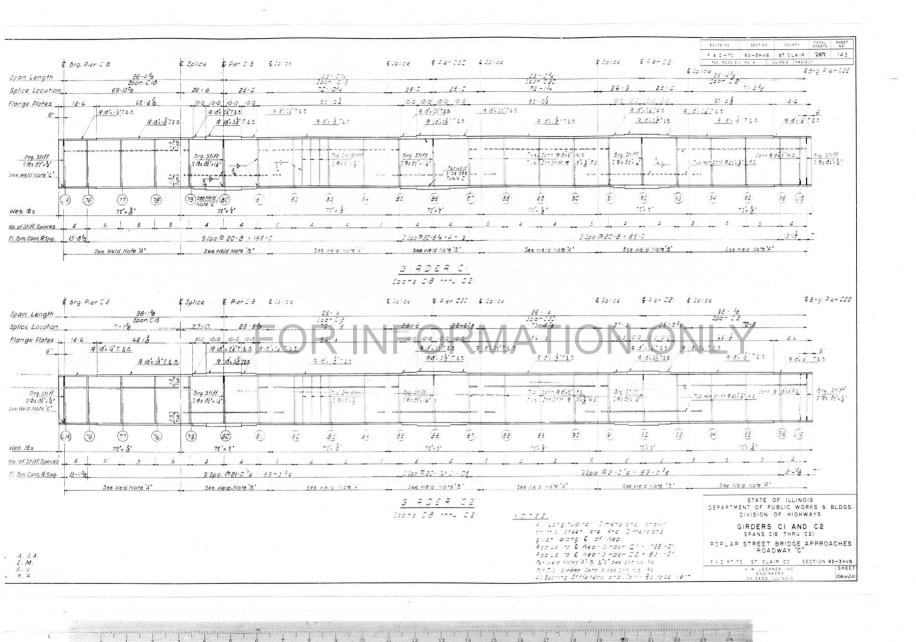


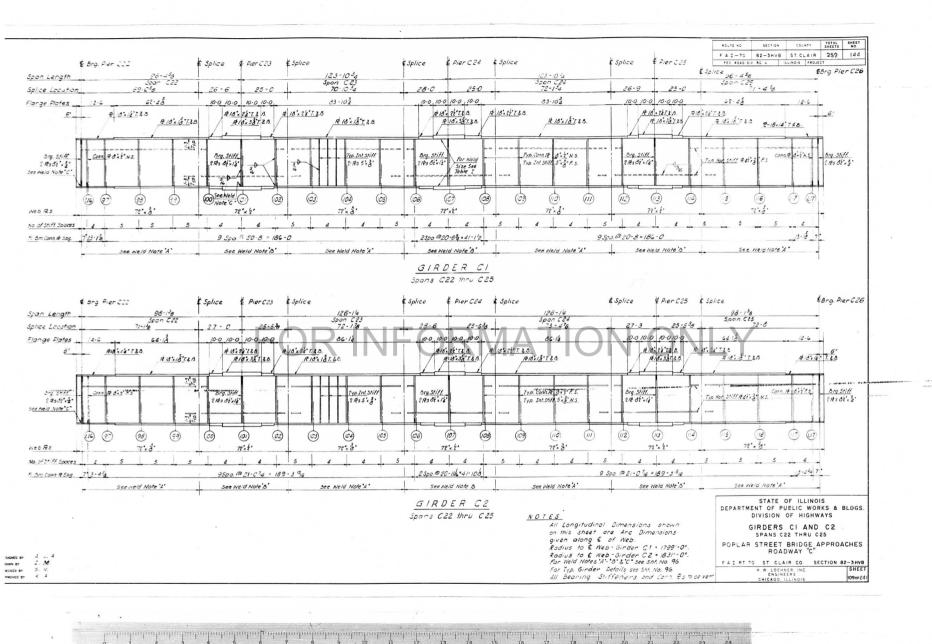


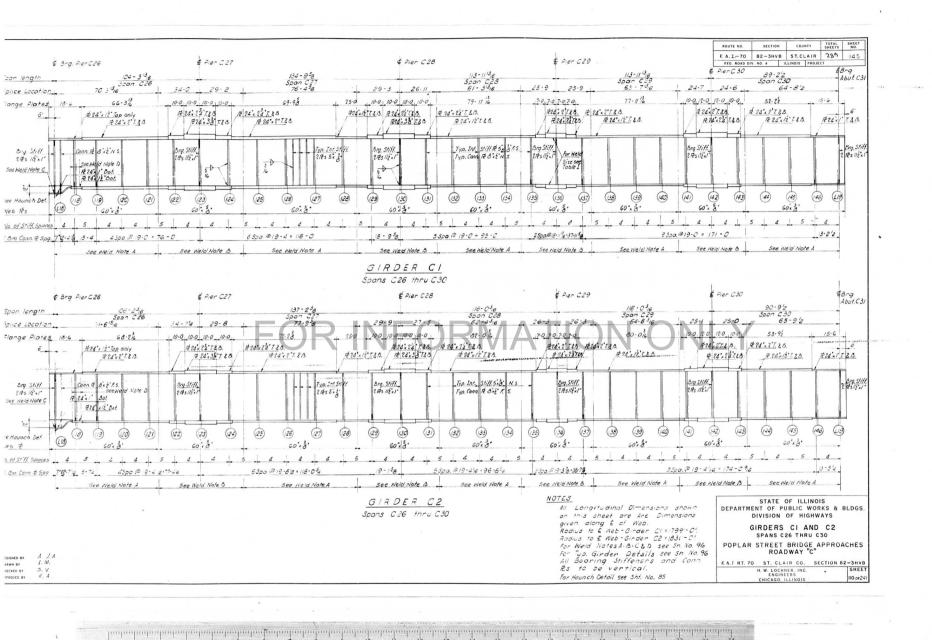


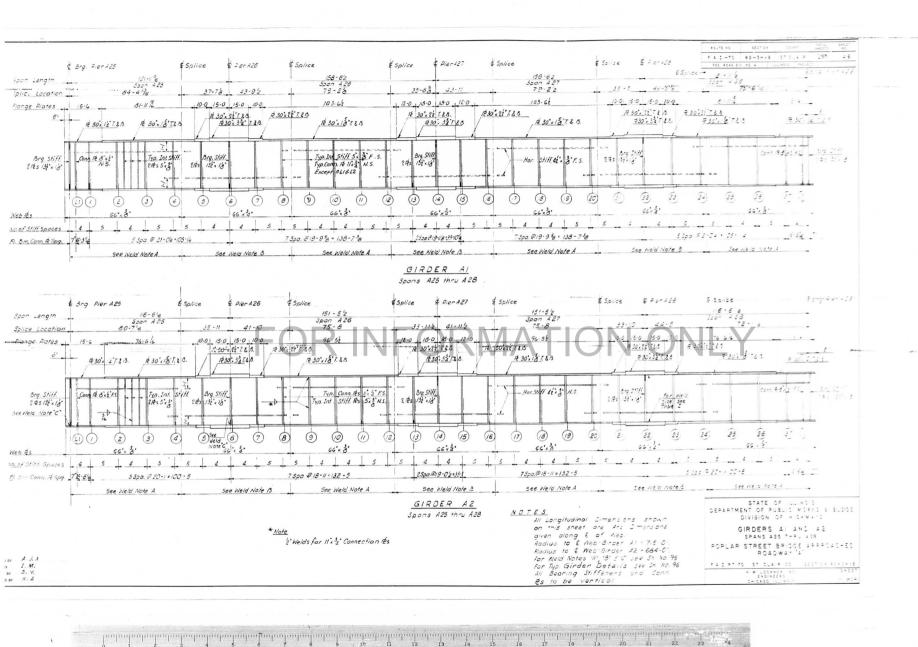


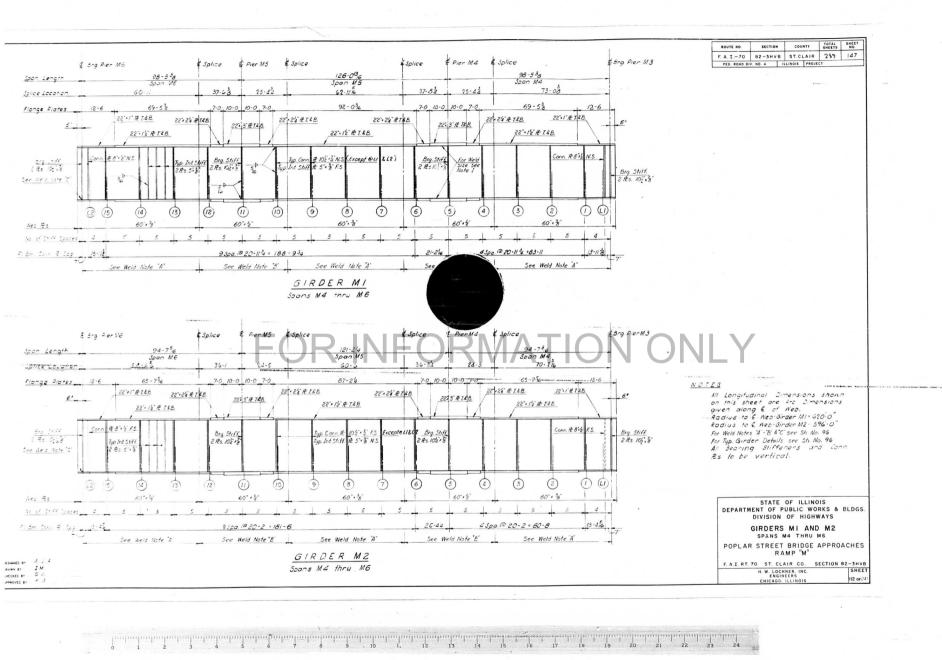


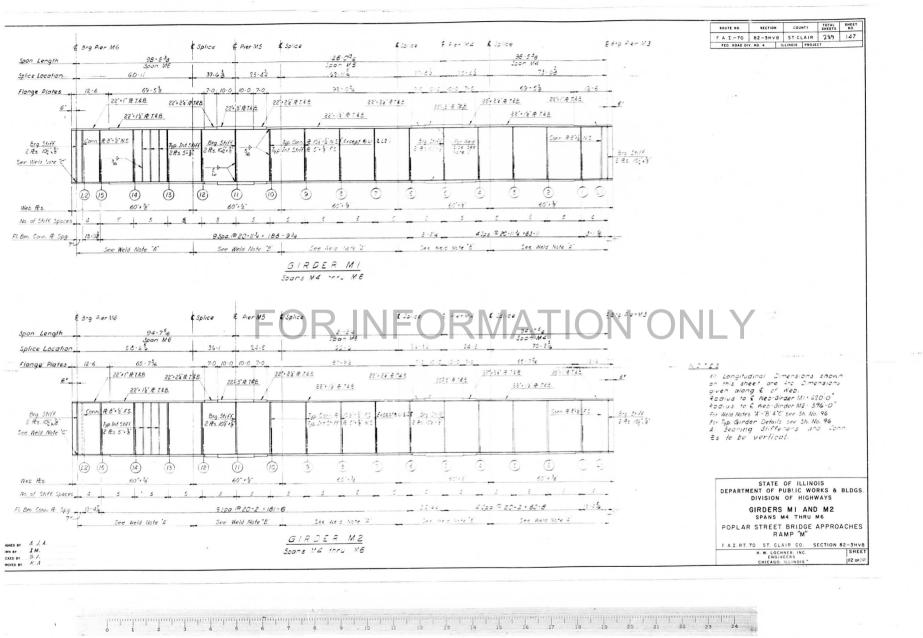


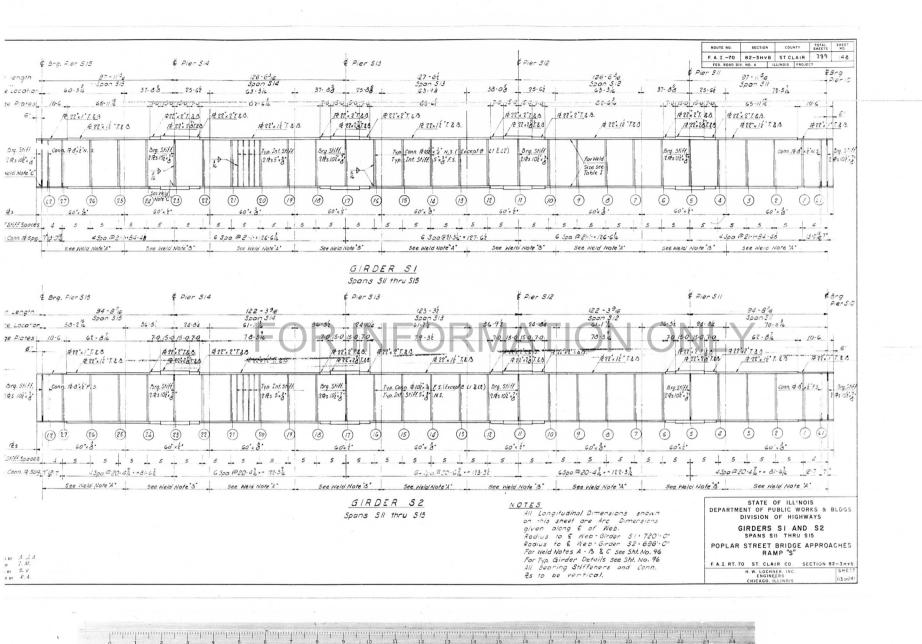












ROUTE NO. SECTION COUNTY TOTAL SHEET NO. FAI-70 82-3HVB ST. CLAIR 289 149 ELEVATION TOP OF GIRDER WEB FOR FABRICATION (DEFLECTION NOT INCLUDED) FED. ROAD DIV. NO. 4 | ILLINOIS | PROJECT \$\frac{\chi\_{1}}{\chi\_{1}}\$\frac{\chi\_{1}}{\chi\_{2}}\$\frac{\chi\_{2}}{\ 5P2 5P3 Per 817 504 505 Pier 818 506 Pier 819 Pier 819 5P1 Pier 820 5P2 5 P 3 Pier 821 5P5 Pier 822 5P 4 450.22 450.57 450.7/ 450,63 451.28 451.34 451.40 451.41 451.41 451.41 451.25 451.19 451.14 450.86 15/13 453 39 453 68 453 69 453 84 453 90 453.96 453.97 \$ Brg. Abut. 331 S rote 7 Pier 8 27 Pier 8 28 Girde No Pier 8 28 50 Pier 329 5P2 5P3 Pier 830 5P4 445 52 444 58 444 22 445 85 442 91 442 56 442 21 441 25 446 58 444 14 444 17 445 18 445 47 445 47 445 17 443 81 450 65 450 46 450 3 450 6 449 60 449 38 449 48 444 17 441 92 447 61 450 48 449 48 449 48 449 47 449 63 449 445.62 ROADWAY B \*449.00 \*449.41 5P3 Pier C20 5P4 595 Pier C21 596 Pier C22 5P3 Pier Cit 504 En. Brg FE. Brg DIR C19 301 502 453.09 453.24 453.30 453.35 453.33 453.32 453.31 453.76 451-08 452 03 452 17 452 55 452 56 452.87 452 98

En. 59 25.509. SP) Profess 501 503 500 520 104 505 Profess 506 SP7 Profess 500 500 Abuncas Sec. 038, 207 CR2 509 Profess 501 503 500 620 104 505 Profess 506 SP7 Profess 500 Abuncas Sec. 038, 207 CR2 500 Abuncas Sec \*Asterisks indicates elevation to top of Flonge of W.

455.72 455.43 455.54 455.65 455.60 455.86 455.9/ 455.09 455.88 455.87 455.72

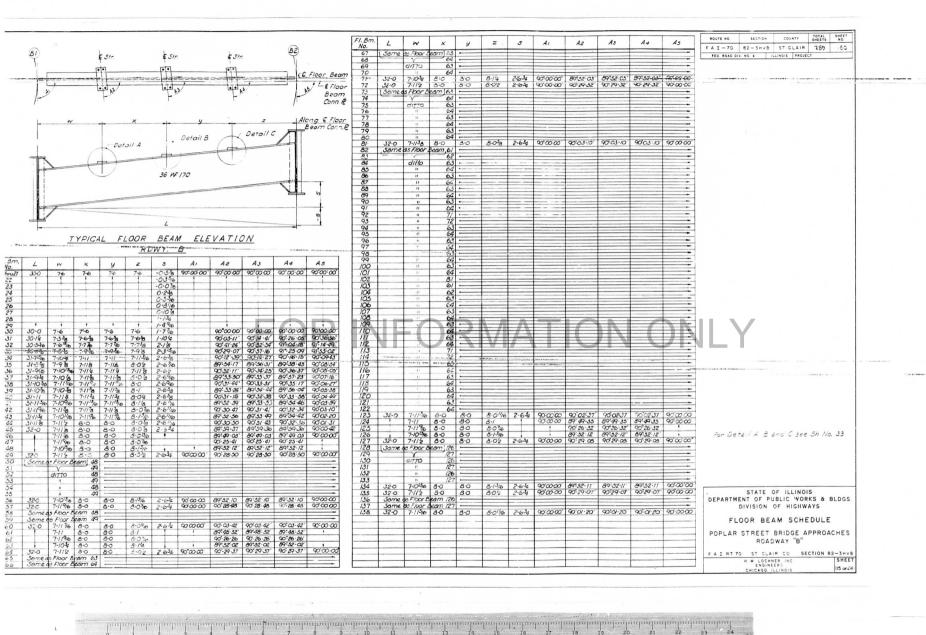
STATE OF ILLINOIS DEPARTMENT OF PUBLIC WORKS & BLDGS. DIVISION OF HIGHWAYS

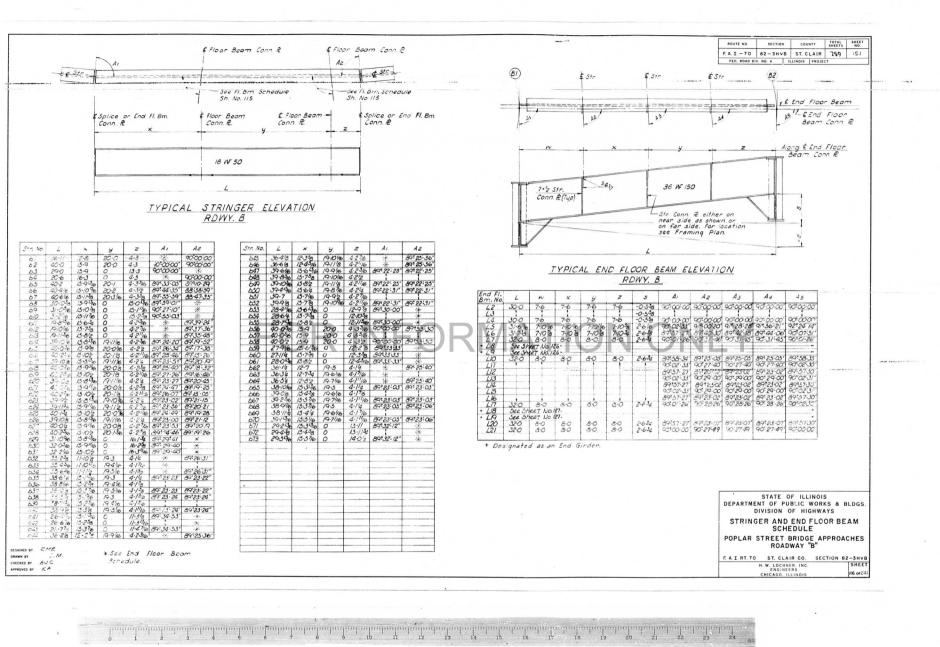
ELEVATIONS - TOP OF GIRDER WEB

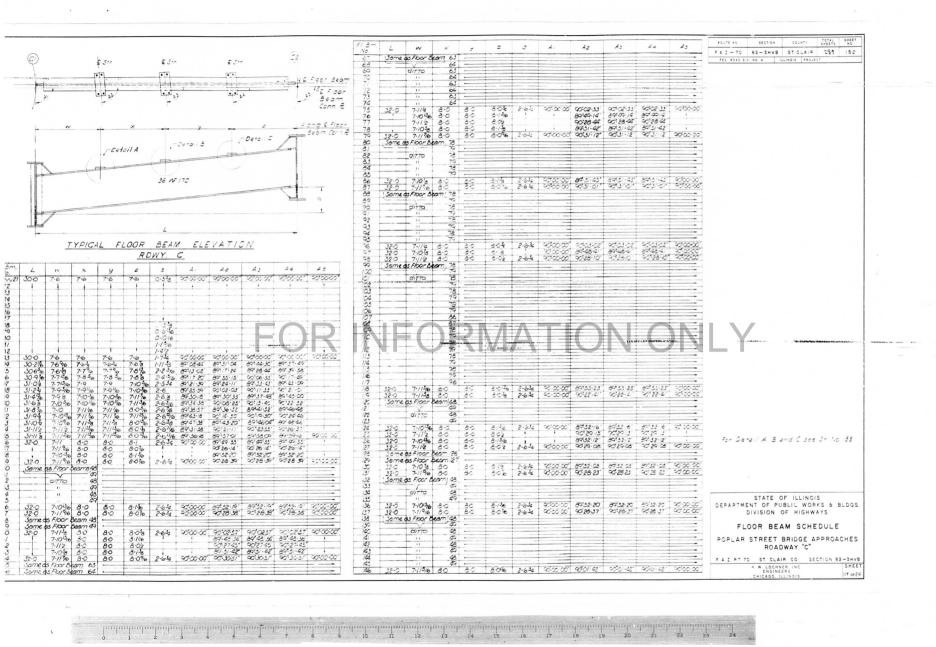
POPLAR STREET BRIDGE APPROACHES ROADWAYS "B" AND "C"

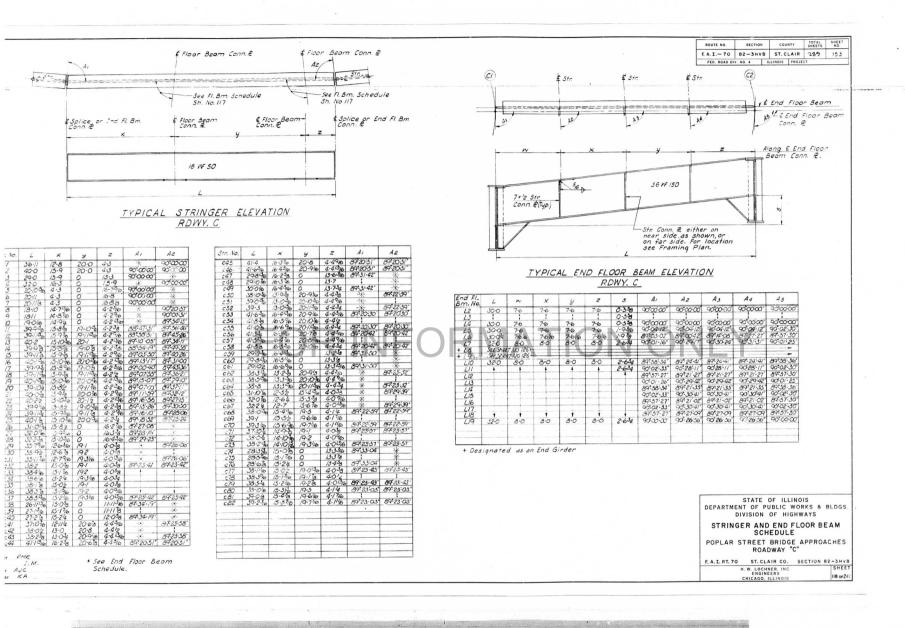
F. A. I. RT. 70 ST. CLAIR CO. SECTION 82-3HVB SHEET H. W. LOCHNER, INC. ENGINEERS CHICAGO, ILLINOIS 114 of 24

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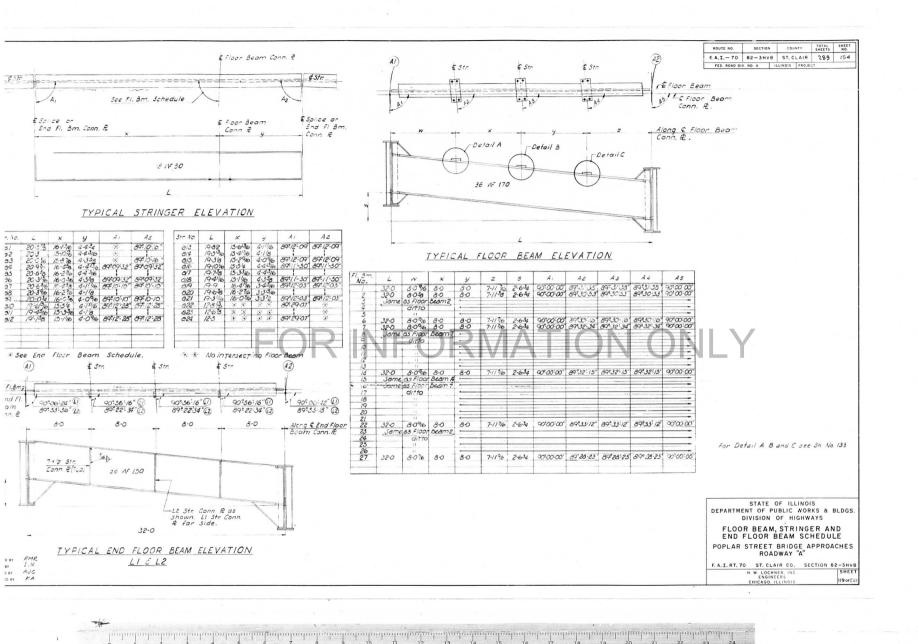


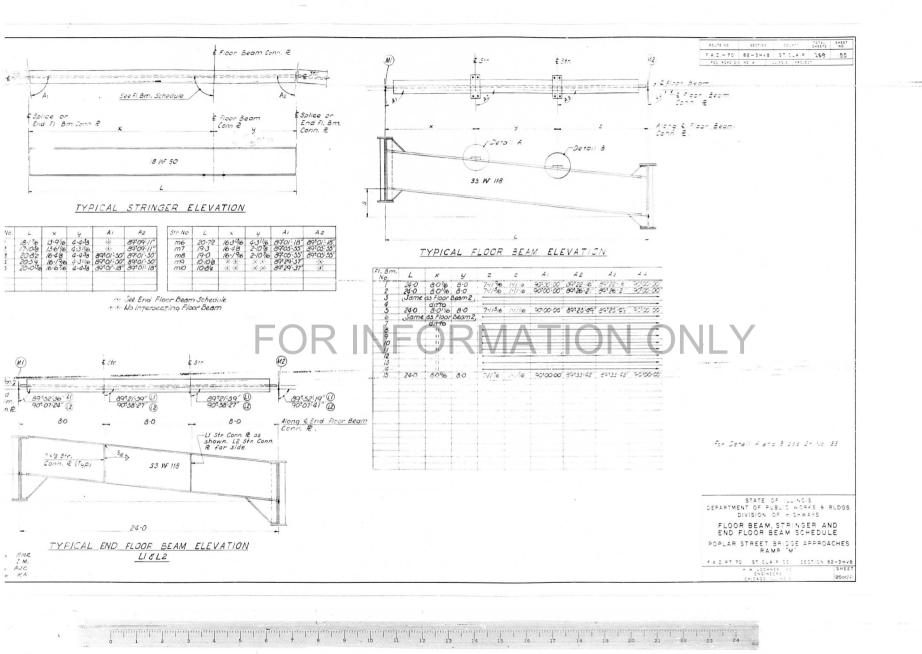


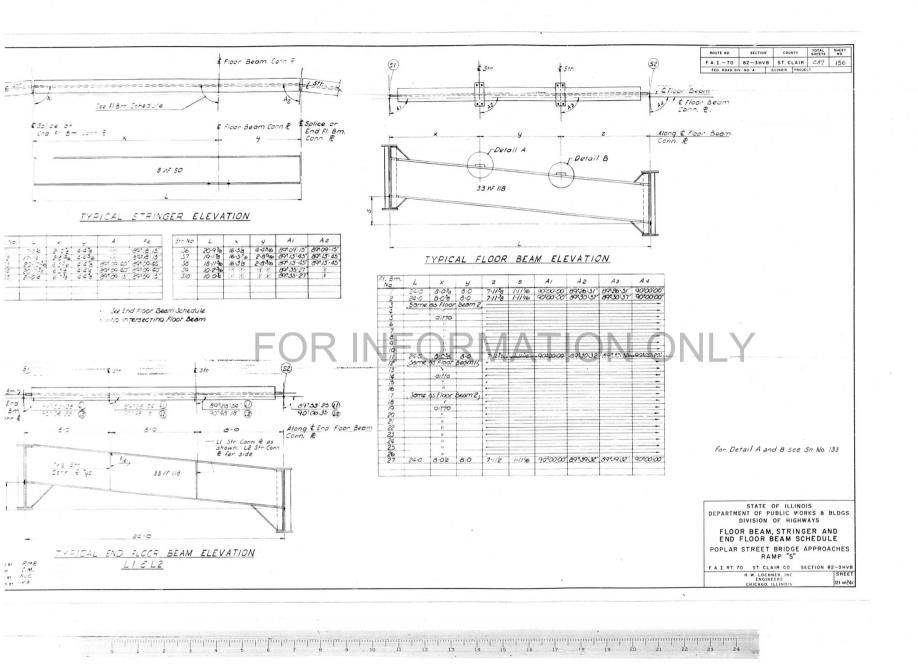




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*1.10 *1	section	SSUNTE	S-EETS	SHEET	
F 4 I - 70	82-3HVB	STOLAIR	289	15.7	

3-Span	Continuous

		Spans	309	89 8	10 *		
			omen		_	a c t i	on
Loca	100	. 4 Soon BC 8	.53pan B9	Pier 39	Pier BC8	Pier B9	
Cea	Primary	1160	1300	2680	85 312		
Loo	Secondary	23	26	53	2	6	
Live	Primary	1030	1080	1080	71	105	
Loos	Secondary	21	22	20	/	2	
Im,	post	26	243	241	13	26	
Cent	rifugal Force	57	39	37	2	Ĵ	
Tota	7/	2532	270	4043	130	454	
Sect	ion Modulus	1930	930	2910	-	_	
П	Dead Load	4.7	5.2	8.8	* Dos	ign app	lies
00	Live Load	4.1	4.5	3.4		to Spa	
	Impact	1.0	1.3	0.8		367	
200	Total	9.8	10 5	3.0	Spa	ns BC8,	C9, C1
- 1	Section	67.5	67.5	108.0	1		

3-Span Continuous

		Spans	828	thru	B30 *				
		М	omen	+	Re	acti	on		
Loc	ation	.4 Span 828	.55pan 829	Pier 829	Pier 829	Pier 829			
Dea	d Primary	1650	16 90	3740	104	360			
200	d Secondary	33	34	75	2	7			
Live	Primary	1290	1430	1460	72	123			
100	Secondary	24	29	29	1	2			
Ιm	poct	302	301	323	14	14 27			
Cent	ritugal Force	47	52	53	2	4			
Tota	a/	3346	3536	5680	195	523			
Seci	ion Modulus	2410	2410	3970		_			
	Dead Load	6.6	6.8	12.4	* Casis	n appli	ine also		
00	Live Load	5.2	5.7	5.0		ons BIZ			
2.0	Impact	1.0	1.2	1.3		Spans Cla			
00	Total	12.8	13.7	18.7	1				
7	Section	87.75	87.75	148.5	1				

4 -3pan Contin ซื่อบร

		30	005 5	161 10	-0 30	4					
			Mem	ent		seaction					
	ation	.450an 801	.5 Spor 3 C 2	2/er 302	363	2 g - 33	2 g r 8 0 8	2 e n 803			
Dead	2-mary	690	1510	4100	4400	€ 3	332	388			
Lood	Secondary	_		-	_		-				
e	Primary	1250	270	630	1830	13	2.9	33			
Lood	Secondary							-			
:-00	et	288	260	356	373	-	28	27			
Centr	fugal force	-	-		-	_	_				
Total		3228	30 40	6086	6603	9.5	339	543			
502110	n Modulus	2090	930	3970	4460	_					

Moments in Foot-Kias Reactions in Kias Section Modulus - Ind

4-Span Continuous

				315 th	-				
			Mom	ent		Re	acti	on	
Loca	ation	.4 Span B/5	.5 Span B16	3/er 8/6	21er 317	Pier 8/5	Pier BIG	Pier B17	
Dead	Primary	660	1490	4060	4340	103	378	384	
Logo	Secondary	33	30	41	44	2	8	8	
Live	Primary	230	260	640	1930	73	29	134	
Load	Secondary	25	25	16	13	1	2	3	
ITO	act	300	262	357	378	17	28	29	
Cent	fugal force	46	46	60	67	3	5 4		
Total		3344	33	6174	6677	199	550	562	
Sec.	on Modulus	2 260	2260	4300	4300	_	-	-	
2	ead Load	6.6	6.0	3.4	14.3		gn opp		
00.	ive Load	5./	5.0	5.4	6.0		775 B19		
00:	mpact	1.2	1.0	1.2	1.2	270	350 13 5		
00	Total	.2.9	12.0	20.0	21.5	]			
''	Section	31.0	31.0	162.0	9225				

DESIGNED BY AJA
CRAWN BY IM
CHECKED BY AJA

SPEROVED BY < A

		50	ans C			eact	, , , , ,	
_			Mcm	ent	MINISTER STATE	Re	acti	on
Loca	ation	.4Span CIB	.5 Span C 19	Pier C19	Pier C20	Pier CIB	Pier C19	CZO
Dead	Primary	1860	1650	4500	4800	///	398	402
Load	Secondary	37	33	45	48	2	_	-
Lve	Primary	1360	1360	1790	2000	74	134	139
Load	Secondary	27	27	18	20	2		-
Imp	act	310	277	382	404	17	29	28
Cent	rifugal force	49	49	65	72	3	5	5
Tota	1	3643	3396	6800	7344	209	565	574
Secti	on Modulus	2420	2420	4800	5/20	-	_	-
1	Dead Load	7.5	6.6	14.8	15.8	* Des	ign a	oplie.
000	live Load	5.4	5.4	5.9	6.6	0/50		Spons
00	mpoct	1.2	1.1	1.2	1.3	C22	thru	625.
00	Total	14.1	13.1	21.9	23.7	1		
7	Section Modulus	87.6	87.6	132	196	1		

	30	0,05	425 1	א טיאא	26					
		W.c.m	e nata	-	<i>5</i> e	sesction.				
Location	.3 Span 4 25	.5 3200 2 26	2.26	2187	2 8 5	2/€.	427			
Dead Frimar	2695	2466	7236	7488	33	497	499			
Load Seconda	y 157	19	246	2.0	é	_				
e Primar	1730	240	2750	3810	74	6	167			
Load Secondar	4 100	5 6	93	84	3		_			
: - 2021	370	3.7	338	546	3	35	35			
Senta (ugal for	ce 66	63	257	230	-	5	ć			
Total	5216	452	11,122	11616	23.	753	7.7			
Sestion Module	15 3480	2480	7920	7920	-	_	_			
Jean Load	34	3	72	75						
0 - 1 ve 1000	22	22	27	30			TATE C			
: impost	£		5	5	DEPA		OF PU			
- C Total	6/	57	153	110		DIV	1510N			

6/ 57 /54 //0 204 244 560 560

STATE OF ILLINOIS
DEPARTMENT OF PUBLIC WORKS & BLDGS.
- DIVISION OF HIGHWAYS

STRESS TABLES

POPLAR STREET BRIDGE APPROACHES ROADWAYS "A", "B" AND "C"

FAIRT 70 ST CLAIR CO SECTION 82-3HVB
- W. LOCHNER ING SHEET
(NO. NO. 25 S. 10) - 241 122 c r 241

ROUTE NO.	SECTIO	N	cou	NTY	SHEETS	SHEET	
F. A. I70	82-3HV	В	ST. CLAIR		289	158	
FED ROAD DE	V. NO. 4	11	LINOIS	PROJE	C1		

## 5-Span Continuous

					Table	of M	omen	its a	and	Reac	tions					
						Spai	ns C	26 th	ru C	30						
					Mc	men	+				Reaction					
Loc	ation	.4 Span C 26	.5 Span C 27	.55pan _C28	.5 Span C 29	.6Span C 30	Pier C21	Pier C28	Pier C29	Pie-	Pier C26	Pier C27	Pier C28	Pier C29	Pier C30	Abut C31
Dead	Primary	2250	23 77	1151	1591	1554	5124	4594	3450	3714	120	435	388	335	370	97
Load	Secondary	43	50	24	32	30	105	92	69	74	2	9	8	7	7	2
Live	Primary	1520	1560	1250	1260	1220	1920	1710	1640	1532	74	141	140	131	128	61
Load	Secondary	30	31	25	25	24	38	34	33	30	2	3	3	3	3	1
Im,	pact	335	306	267	268	291	398	350	348	344	/6	29	29	28	29	13
cent	rifuga Force	55	57	45	46	44	70	62	59	54	3	5	5	5	5	2
Tota	0/	1233	4381	2762	3222	3163	7655	6842	5599	5748	217	622	573	509	542	176
Sect	ion Modulus	3100	3100	2370	2370	2370	5210	5210	4320	4320	_	_	_	_	-	_
1	Dead Load	10.2	12.0	5.5	8.4	7.2	18.3	15.4	11.1	/3.5		-				-
000	ive Load	7.5	7.5	6.0	6.0	5.9	6.7	6.5	5.7	5.2	1					
001	mpact	1.6	1.5	1.3	1.3	1.4	1.4	1.3	1.2	1.1	1					
00	Total	19.3	21.0	12.8	15.7	14.5	26.4	23.2	18.0	19.8	1					
3	Modulus	192	192	144	144	144	324	324	264	264	1					

	50	ons C	15 th	ru c	/7	
		М	omei	n f	Reac	tion
Loc	ation	.45pan C 15	.5Span C16	Pier C16	Pier C15	Piei CI6
Deaa	Primary	1850	1900	4200	110	390
Load	Secondary	37	38	84	2	8
Live	Primary	1400	1430	1630	75	131
Load	Secondary	28	28	32	1	3
Impo	ict	320	294	346	17	28
Centri	fugal Force	5/	52	59	2	4
Total		3686	3742	6351	207	562
Section	n Modulus	2590	2590	4280	_	-
0	ead Load	7.4	7.6	13		
300	ive Load	5.6	5.7	5		
	mpact	7.3	1.2	2		
		14.3	14.5	20		
35	odulus	94.5	94.5	162		

## 5: Some Court DIN A

						5-5	pan	Conti	חטסט.	5				_11		$\Lambda I$
					Table	of M	omen	15 0	and	Reac	tions					
						5,	oons	511 TH	ru 51	5						
					Мо	men	+				Reaction					
-		.4 Soon 8 11	.5Span 5/2		.5 Spon	.6 Span		Der 314	Pier SI3		Pier	Sil	Pier Si2	Pier Si3	Pier	Pier SIS
Dead	Primary	670	1490	1440	1490	1670	3920	3960	3960	3920	93	34/	343	343	341	93
Load	Secondary	110	25	121	125	.10	39	40	40	39	5	-	-	-	-	5
Live	Primary	875	890	975	890	875	1165	1290	1290	1165	48	88	92	92	88	48
Load	Secondary	58	75	92	7.5	58	. 2	13	13	12	2	-	-	-		2
Im	pact	210	193	212	193	210	243	260	260	248	10	19	18	18	19	10
Cent	rifugal force	79	80	33	80	79	105	//6	116	105	4	3	8	8	8	4
Tota	0/	3 002	2853	2918	2953	3 002	5489	5679	5679	5489	162	456	461	461	456	162
Sect	ion Modulus	2190	2190	2190	2190	2190	4070	4070	4070	4070	-	-	-	_		
1	Dead Load	202	18.0	17.4	19.0	20.2	3 9.0	40.0	40.0	39.0				-	-	
0 6	ive Load	10.6	10.8	11.8	10.8	.0.6	2.0	13.0	13.0	12.0	1					
00	mpact	2.5	2.3	2.6	2.3	2.5	2.5	2.6	2.6	2.5	1					
00	010/	33.3	3/./	3.8	31.1	33.3	53.5	55,6	55.6	53.5	l					
1	Modulus	121	121	121	121	121	232	232	232	232	ĺ					

> Moments in Foor-Kips Reactions in Kips Section Nogulus - In.

0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24

## Table of Mamanta and Reactions

lab.			nts o	_	React	1005
	39		ome			rion
Loca	ation	4Spon	.5Span M5	Pier	Pier M3	Pier M4
Dead	Primary	582	1430	3890	94	342
Logo	Secondary	95	37	127	5	-
Live	Primary	998	980	1/20	43	35
Load	Secondary	54	22	37	3	-
Impact		2/4	180	244	11	18
Centr	ifugal force	106	104	132	6	10
"otal	/	2949	2703	5558	167	455
Section	on Modulus	2200	2200	4240		_
. 0	eaa Load	22.5	220	420		
200-	ive Logo	13.5	13.3	13.6	1	
	mpact	3.0	2.7	29	1	
	otal	39.0	38.0	5 <b>8</b> .5		
5	ection lodulus	121	121	242		

STATE OF ILLINOIS DEPARTMENT OF PUBLIC WORKS & BLDGS DIVISION OF HIGHWAYS

## STRESS TABLES

POPLAR STREET BRIDGE APPROACHES ROADWAY "C" AND RAMPS "M" & "S"

FA.I. RT. 70 ST. CLAIR CO. SECTION 82-3HVB

H. W. LOCHNER, INC ENGINEERS CHICAGO, ILLINOIS SHEET 123 or 24

DESIGNED BY AJA
DRAWN BY
CHECKED BY AJA
APPROVED BY KA

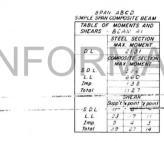
ROUTE NO	SECTION	cou	NTY	SHEETS	SHEE
F. A. I 70	82-3HVE	ST. C	AIR	289	159
FED ROAD D	V NO 4	ILLINOIS	PROIL	CT	-

				Toble o	f Mom	ents a	nd Rea	ctions				
			ind Girde	rs - Span	s ABCD	, BII, CII	and Bi	7 (Simple	Spans)			
	500	n 48CD	Span	4300	Span	ABCO	Spar	ABCD	Spans L	311 & C11	300	n B27
.0005	Girde	r L/- A	3100	e - 11.3	Gird	er LI-C	Gird	er 11.0	Girders	L8 and L9	Girders	L 18 and L19
	Vomen	Reaction	Noment	Reaction	Moment	Reaction	Moment	Reaction	Moment	Reaction	Moment	Reaction
2000.000	29 O	/98	0/7	ð.	363	92	1034	9/	740	10	1082	103
#	457	93	728	66	722	66	798	65	7/7	63	745	73
:-:::	337	28	2.9	20	2.6	20	239	20	2/5	/9	224	22
Ta 1a	4304	311	1964	33	.907	178	207	176	1672	152	2051	199
Sector Yourus	290/	-	1-8	-	1178	-	297		1070	-	1290	_

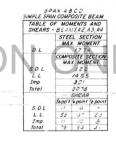
	Moment	Reaction
Dead Load	325	30
Live Load	490	47
Inpact Total Section Modulus	145	14
Total	953	91
Section Modulus	379	-
Dead Load	160	15
Live Lood	457	43
Impact	133	13
Total	753	71
Section Modulus	503	-
Section Modulus Dead Load Live Load Impact Total Section Modulus Dead Load Live Load Impact Total Total	139	24
Live Lood	283	35
Impact	85	- 11
	357	70
Section Modulus	355	
18 W 50 ·	Stringer	
	Mon	nent
Dead Load		7
Live Load	9	4
Impact	2	3
Total	13	9

324N			
TABLE OF SHEARS	- WO	MENTS	4.40
	STEE	L SEC	TION
2.4	WA.	x McA	ENT
		S TE S	ECTION
306		63	
ine		808	-
Tore		56	
	5,000	SHEAR Appint	2 20 01
3.26	6		-
:-:	-0.		-
73.12/	65	4.3	20





2 2 3 4 5 6 7 6 9 16 11 12 19 14 15 16 17 18 19 20 21 22 23 24











Moments are in F1 - Kips Reactions and Shears are in Kips D t. Poed load S D L. To Poed load S D L. Superimposed dead load colon to the load L. L. Live load Imp. 2 Impeat Imp. 2 Ic = Moment of inertia comp. sec. Stc = Sec. Mod. top. comp. sec. Sec = Sec. Mod. bott. comp. sec.

STATE OF ILLINOIS DEPARTMENT OF PUBLIC WORKS & BLDGS. DIVISION OF HIGHWAYS

STRESS TABLES SPANS ABCD, BII, CII AND B27 POPLAR STREET BRIDGE APPROACHES ROADWAYS "A", "B" AND "C"

F. A. I. RT. 70 ST. CLAIR CO. SECTION 82-3HVB H. W. LOCHNER INC.

SHEE 124 of 241

ROUTE NO.	SECTIO	N COL	INTY	SHEETS	SHEET
F. A. I70	82-3HV	B ST. C	LAIR	289	160
FED. ROAD DI	V. NO. 4	ILLINOIS	PROJE	CT.	

	OF MOI		
	STE	EL SEC	TION
	MA.	X. MON	IENT
DL		1664	1
		SITE S	
SDL		305	
LL		14/2	
Imp		295	
Total		2012	
		SHEAR	,
	Supp't	4 point	2 point
SDL	11	3	-
L.L.	53	37	24
Imp.	13	10	7
Total	7.5	52	3/

	ROPERTIES
51	teel Section
Is	58746
575	1306
SBS	1932
Con	nposite Section
Ic	135450
STC	6399
Sec	2534

TABLE	OF MOI	MENTS	AND
SHEARS	· BE	AM A	7
	STE	EL SEC	TION
	MA.	X. MON	<b>IENT</b>
D. L.		1711	
	COMP	SITE S	ECTION
	MA	X. MON	IENT
S.D.L.		266	
L.L		609	
Imp		128	
Total		1003	3
		SHEAR	?
	Supp't	a point	2 point
SDL	10	5	
L.L.	23	16	10
Imp.	5	5	3
Total	3.8	26	13

- 5	teel Section
Is	58746
575	1306
SBS	1992
Co	mposite Section
Ic	164000
STC	10950
Sec	2750

TABLE SHEARS			AND
SHEARS		L SEC	TION
		K. MOM	
D. L.		239	5
		SITE S	
S. D. L.		169	
L.L		430	
Imp		91	
Total		690	
		SHEAR	
	Supp't.	a point	2 poin
S. D. L.	6	3	-
L.L.	17	11	8
Imp.	4	4	2
Total	27	18	10

S	teel Section
Is	62868
575	1554
Sas	1833
Co	mposite Section
Ic	171088
STC	20450
Sac	2580

TABLE SHEARS				
	STEE	L SEC	TION	
	MA.	X. MON	ENT	
D. L.		1442		
S.D. L.		SITE S	ECTION	
		242		
		239		
Imp	264			
Total		745		
		SHEAR	,	
	Supp't.	4 point	2 point	
S.D.L.	9	4	-	
	48	33	21	
Imp.	10	10	7	
Total	67	17	20	

5	teel Section
Is	42869
575	1123
SBS	1736
Cor	mposite Section
Ic	99538
STC	5693
Sec	2193

TABLE SHEARS				
		L SEC		
	MA.	X. MON	IENT	
D. L.		1550		
S D. L.			ECTION	
	MA	MAX. MOMENT		
		154		
		6/2		
Imp		132		
Total		898		
		SHEAR	,	
	Supp't.	4 point	2 point	
S.D.L. L.L. Imp.	6	3	-	
	25	17	11	
	5	5	3	
Total	36	25	14	



SIMPLE	SPAN	COMP	20517	Έ	BEA	M

		EL SEC		
D. L.	/569			
		SITE S	ECTION	
SDL	220			
L.L	605			
Imp				
Total	957			
		SHEAR	?	
	Supp't	4 point	'a point	
SDL	6	-	-	
LL	25	18	17	
Imp	5	4	3	
Total	38	26	14	



TABLE O				
		L SEC		
	MAZ	K. MON	IENT	
D. L.		1302		
	COMPO	SITE S	ECTION	
	MA.	X. MOM	ENT	
SDL	2/6			
LL				
Imp	261			
Total		674		
		SHEAR	•	
	Supp't.	4 point	2 poin	
SDL	ô	4	~	
L.L.	19	35	31	
Imp.	17	10	7	
Total	68	49	28	



	STE	L SEC	TION	
		X. MON		
D. L.		1302		
S D L	COMPO	SITE S	ECTION	
	MA	X. MOM	ENT	
		216		
		1197		
Imp		261		
Total		674		
		SHEAR	,	
	Supp't	4 point	2 point	
SDL	ô	4	-	
L.L.	19	35	31	
Imp.	17	10	7	
Total	68	149	28	



SIMPL	F SPA	N COME	OSITE	REAM		SIMPLE SPA	N COMP	OSITE	BEAM
TAB	LE C	BEAN	IENTS	AND	$\Lambda \Lambda \Lambda$	TABLE O			
		STEE	L SEC	TION				L SEC	ENT
D.	D.L. 1026		D. L.	-		******			
			SITE S	ECTION				X. MOM	
SD	S.D.L. 549 L.L 1/4.3	-	549			S. D. L.		228	1
			L.L.	1161					
Imp			254		1	Imp		260	,
Tota		-	1946			Total		1645	9
1010	,,	+	SHEAR					SHEAR	?
				2 point			Supp't.	4 point	's point
5.1	0.	22	+ point	z point		SDL	9	4	-
		49	77			L. L.	5/	36	22
L.		49	34	55		Imp.	177	10	7
Im		11	10	6		Total	7/	50	29
Tota	a/	82	55	28		10101	1.77	30	69

5	teel Section
Is	36105
575	945
SBS	1494
Col	mposite Section
Ic	89669
STC	55/3
Sac	1945

SHEARS				
		L SEC		
	MA.	K. MON	IENT	
D.L.		12.72	2	
			ECTION	
S. D. L.	MA	X. MOM	ENT	
	209			
	5/0			
Imp	//6			
Total	835			
	-	SHEAR	,	
	Supp't	4 point	'a point	
S.D.L.	9	5	-	
L.L.	23	17	11.	
Imp.	6	5	2	
Total	38	27	13	

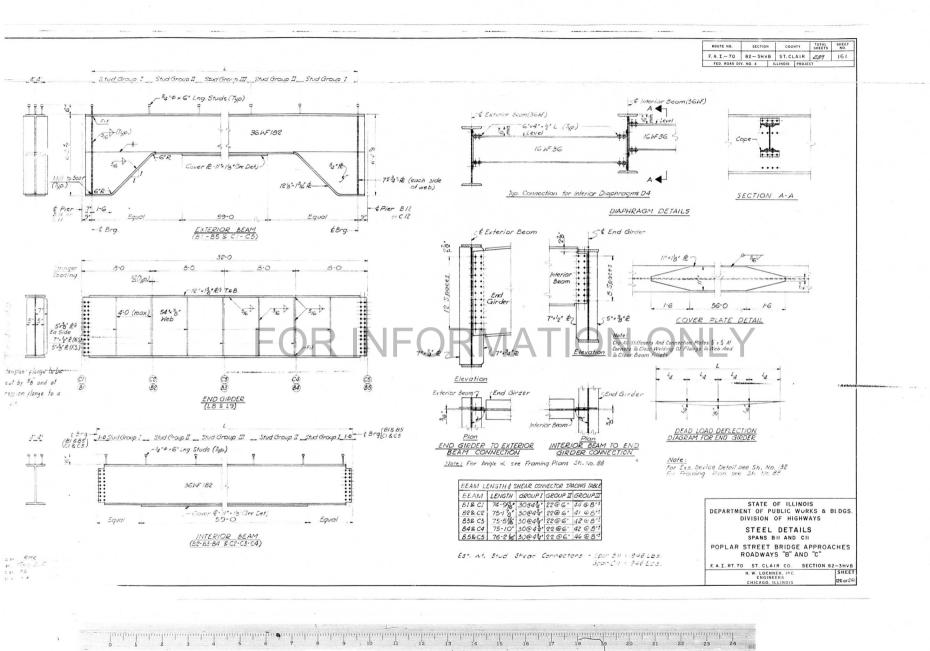
S	teel Section
Is	41374
STS	895
Sas	1503
Cor	mposite Section
Ic	135807
STC	9830
Sec	2270

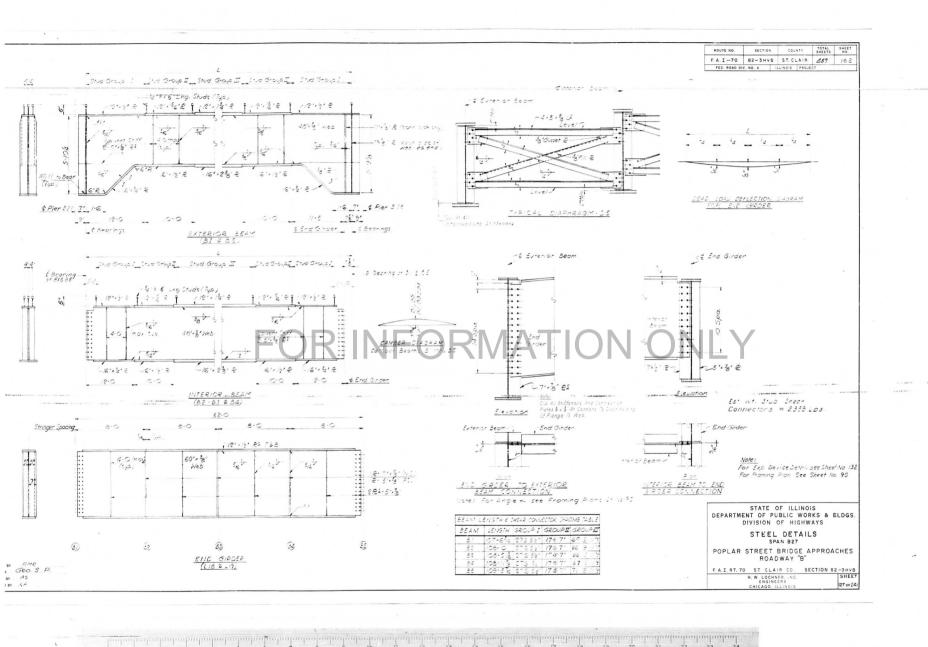
STATE OF ILLINOIS DEPARTMENT OF PUBLIC WORKS & BLOGS DIVISION OF HIGHWAYS

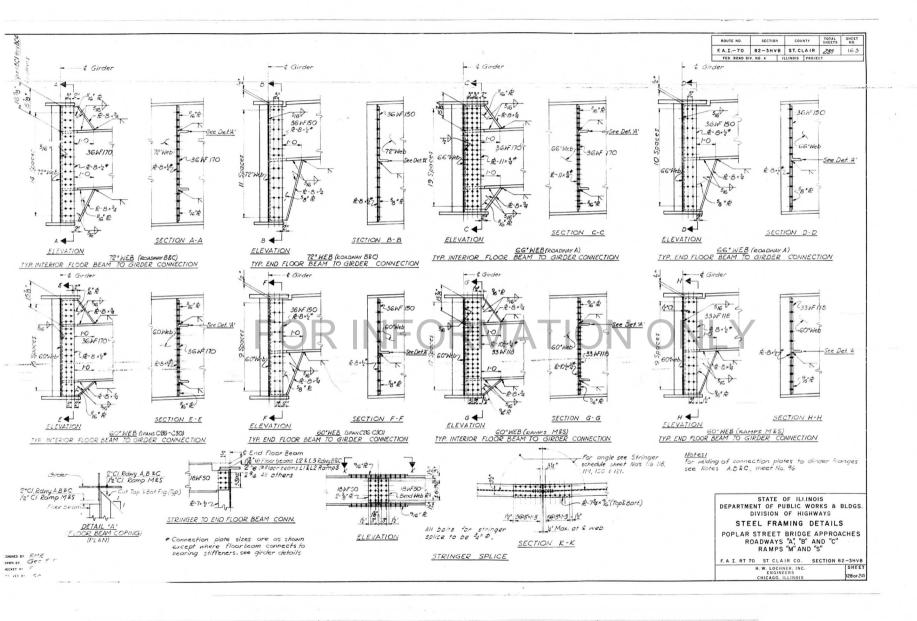
STRESS TABLES

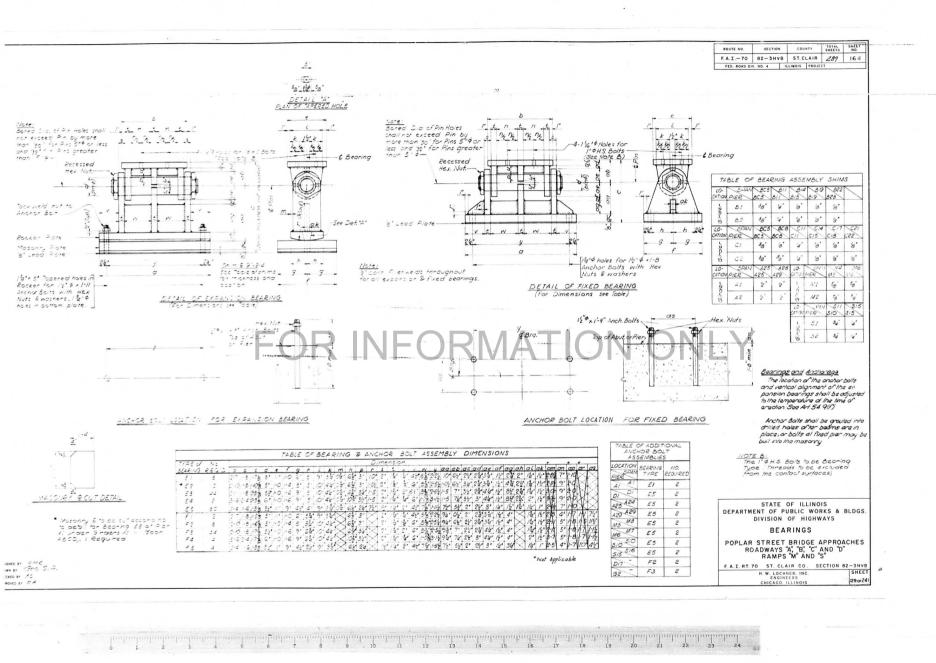
POPLAR STREET BRIDGE APPROACHES ROADWAYS "A", "B", "C" AND "D"

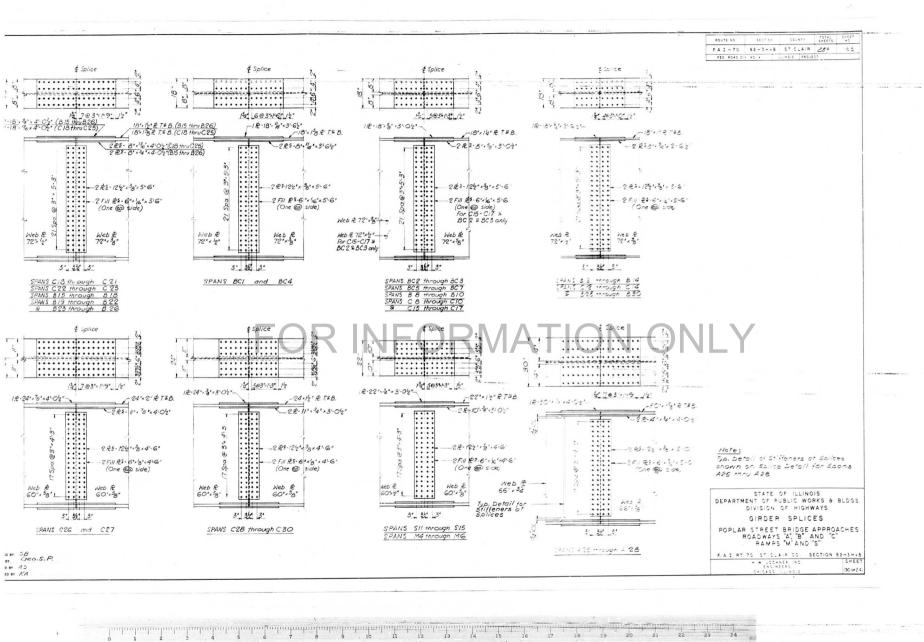
FAIRT 70 ST. CLA	IR CO. SECTION 82-3HVB
H. W. LOCH	
CHICAGO	

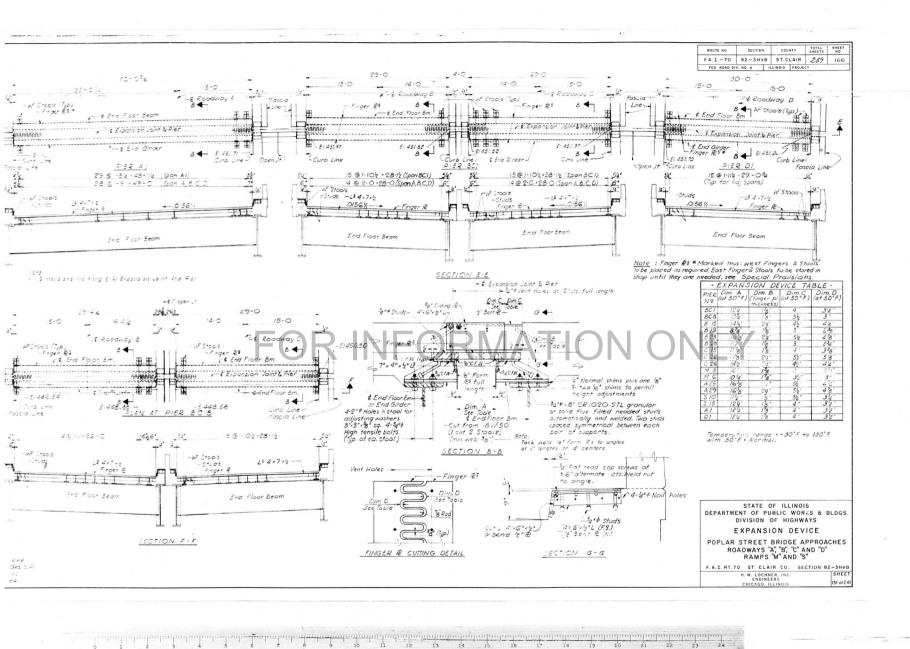


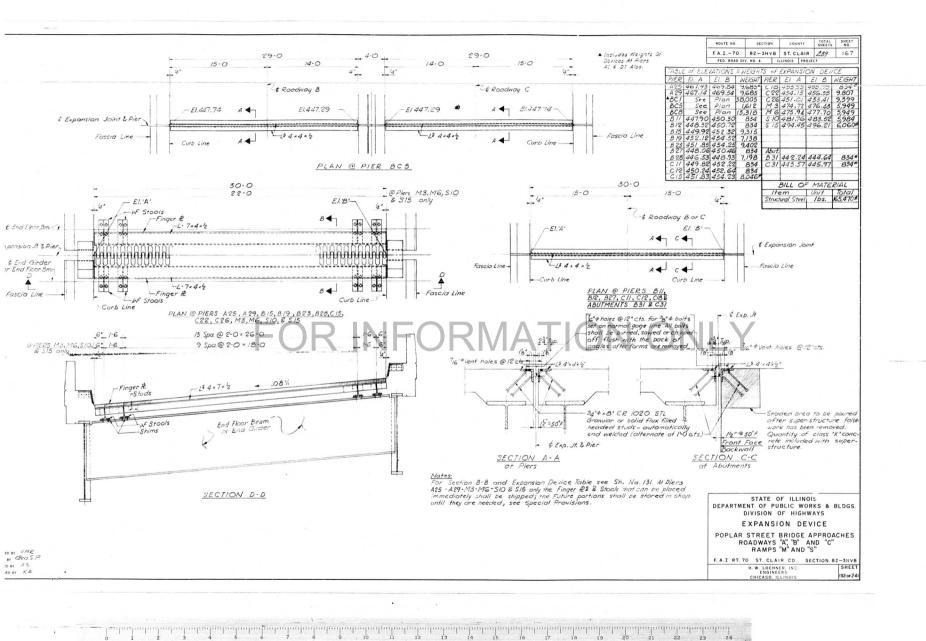












	3m. No.		Deta	il A			Deta	oil E	3		Deta	il C	
		11	12	13	14			13			12		
,	Thru 4	30	13,6	13/6	1/2	501	חפ סי	deta	1/ A	Sen	e as	deta	1/ 4
3	- 0 - 0 8	16	1/16	13/6	116								
9	Tn-U 12	9,6	18	34	156								
3	Toru 16	58	14	58	114								
7	-nru 20	34	15/6	12	1'8								
2/	Thr_ 24	13/6	176	7/6	11/6								
5	7000 27	15/6	19/6	5/6	5,6		•				*		
_			-										
_			-	-	-			-		-	-	-	-

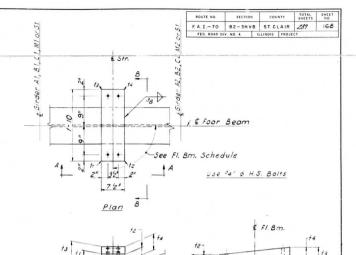
1. 3m. No.	1 4	Deta	il A		1 4	Deta	il B		1 4	eta	11 C	
7. DITI. NO.	++	12	t3	14	tt	t2	13	14	11	te	13	14
Tanu 6	1/8	14	58	34			letail	A	Sam		detail	
7 Thruiz	1	18	34	78						1		
3 Thrul8	78	1	'8	1								
9 Thru 21	13/6	1516	1516	16		1				1		
32	15/6	1	78	15/6	78	15/6	15/6	1	78	15/6	15/6	1
32 13 34	15/6	15/6	15/6	15/6	15/6	15/6	15/6	15/6	38	<sup>7</sup> 8	1	1
24	1	15/6	15/6	3	15/6	<sup>7</sup> 8	1	15/6	15/6	78	1	15/6
?5	1	15/6	15,6	8	1	8	1	78	15/6	13/6	146	15/6
16	146	78	1	13/6	1	<sup>7</sup> 8	1	78	1	13/6	1/16	78
27	16	18	1	13/6	116	13/6	146	13/6	/	13/6	116	78
28	1'8	13/6	146	34	116	13/6	146	13/6	1/16	34	1/8	13,6
29	1'8	13/6	11/6	34	118	34	18	34	116	34	118	13/6
30	13/6	34	118	1/16	118	34	18	34	1'8	11/6	1316	34
	13/6	34	18	1/16	1316	"16	1316	11/6	18	1/16	13/6	4
32	1316	1/16	136	58	13/6	"16	13/6	1/16	18	58	16	34
33	14	"16	1316	8	1316	58	14	116	1316	58	14	"16
14 Thru 78	13/6	9/6	1516	1/16	Same	2 05 0	ietail	Α	Same	05	detail	A
19Thru 81	1316	9/6	15/6	1/16		- 1				1		
32Thru 87	/3/6	58	14	"16								
38 Thru 93	14	5 <sub>B</sub>	14	58								
94 Thru 99	14	1/16	136	58								
00 Thru 102	196	"16	13/6	9,6								
03 Thru 108	15/6	"16	1316	9,6								
09 Thru 114	15/6	34	18	916								
15 Taru 120	138	34	1'8	12								
21 Thru 123	138	34	16	'2								
24 Thru 138	/38	13/6	146	2		,				1		

FI. Bm. No.	1 4	Deta	11 A			Deta	ril E	,	1 4	Deta	il C	•
	11	12	13	14	+1	te	13	+4	+1	12	13	14
I Thru 6	14	118	3	5 <sub>A</sub>	Same	2.05.0	totail	4	Same	05.0	etail.	4
7 Thru 12	18	1	8	34								
13 Thru 18	1	8	1	78								
19 Thru 21	15/6	13/6	146	15/6								
22 Thru 28	15/6	13/6	146	156		•				•		
29	15/6	13/6	146	15/6	3	34	1/8	1	78	1/16	1316	1
30	15/6	3/	1/8	15/6	15/6	1/6	13/6	15/6	78	"16	13/6	1
31	1	1/16	13/6	78	15/6	"16	1316	15/6	15/6	58	14	15/6
32	1	1/16	136	8	1	58	14	3	15/6	58	14	1516
33	1/16	58	14	13/6	1	58	14	3	1	%	1516	78
34	1'8	58	14	34	1/16	9/6	14	13/6	146	9,6	1516	13K3
35	18	58	14	34	18	9/6	15/6	34	146	916	15/6	13/6
36	1316	96	15/6	16	18	96	156	34	1'8	1/2	13	34
37 Thru 15	1316	9,6	15/6	16	Same	as	ietail	A	Same	asc	ietai	A
76 Thru81	13/6	9/6	15/6	1/6		1				-1		
82 Thru87	1316	5 <sub>B</sub>	14	1/16								
88 Thru 93	14	58	14	58								
94 Thru 96	14	1/16	13/6	5€								
97 Thru 102	15/6	"16	13/6	9/6								
103Thru108	15/6	"16	1316	9/6								
109Thru114	1516	34	18	96								
115 Thrui17	138	34	18	2								
118 Thru 121	138	34	18	2								
122 Thru 146	138	13/6	146	2						+		

3 m. No.	1 4	Deta	11 A			Deta	ril E	3	1	Deta	il c	•
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	11	12	13	14	+1	te	13	14	+1	12	13	14
hru 6	14	118	3,	5 <sub>A</sub>	Same	2.05.0	totail	4	Same	05.0	etail	4
hru 12	18	1	8	34								
Thru 18	1	<sup>7</sup> 8 <sup>13</sup> /6	1	78								
hru 21	15/6	13/6	146	15/6								
hru 28	15/6	13/6	146	15/6		•						
	15/6	13/6	146	15/6	3	34	18	1	78	1/16	1316	1
	15/6	3	1/8	15/6	15/6	1/6	13/6	15/6	78	"/6	13/6	1
	1	1/16	13/6	78	15/6	1/16	1316	15/6	15/16	58	14	15/6
	1	1/16	136	<i>'8</i>	1	58	14	3	15/6	58	14	1516
	1/16	58	14	13/6	1	58	14	78	1	%	1516	78
	1'8	58	14	34	1/16	9,6	14	13/6	146	9,6	1516	13/6
	18	58	14	34	18	9/6	15/6	34	146	9/6	15/6	13/6
	1316	96	15/6	16	1'8	96	156	34	1/8	1/2	13	34
Thru 15	1316	916	15/6	16	Same	as	ietail	A	Same	asc	ietai	
hru81	13/6	9,6	15/6	1/6		1						
Thru87	1316	5 <sub>B</sub>	14	1/16								
hru93	14	58	14	58								
hru 96	14	1/16	13/6	5€								
hru 102	15/6	1/16	13/6	9/6								
Thru/08	15/6	116	1316	9/6								
Thru 114	15/6	34	18	96								
Thruil7	138	34	18	2								
hru 121	138	34	18	2								
Thru 146	138	13/6	116	2		1				+		

FI. 8m. No.		Deta	// A			Deta	il B	
71. bm. Vo.	+,	12	13	14	11	12	13	14
1 Thru 3	78	176	7/6	1	San	e as	dela	il A
4 Thru 6	34	138	12	13		1		
7 Thru 9	11/6	14	53	13,6				
10 Thru 12	9/6	1316	1/16	15,6				
13 Thru 15	1/2	118	34	138				

Fl. Bm. No.		Deta	11/ 4			Deta	ril B	1
ri. Biii. No.	+1	12	13	14	11	te	13	14
1 Thru 3	13/6	13/6	516	15/6	Sam	e as	detai	/ A
4 Thru 6	13,6	136	5/6	1516				
7 Thru 9	1316	134	38	15/6				
10 Thru 12	1'8	1116	38	1				
13 Thru 15	1/	158	12	1'8				
16 Thru 13	15/6	196	916	13/6				
19 Thru 21	78	1/2	58	14				
22 Thru 24	3,6	138	34	15/6				
25 Thru 27	34	1516	13,6	138		+	- 6	





DETAIL A, B, or C Shim shown at Floor Beam 37 thru 75 Other shims are similar

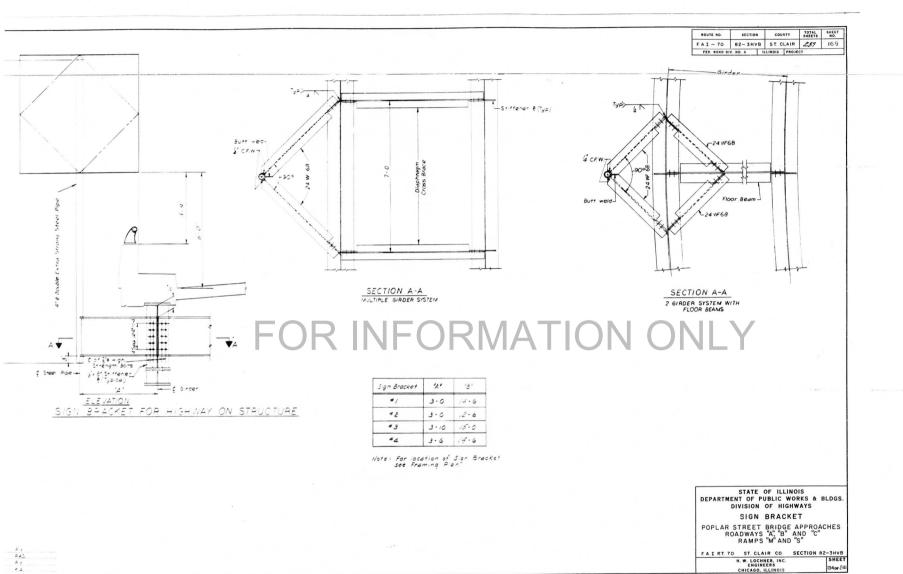
Note: If additional Shims are required, the cost of these shims is to be incidental to Structural Steel.

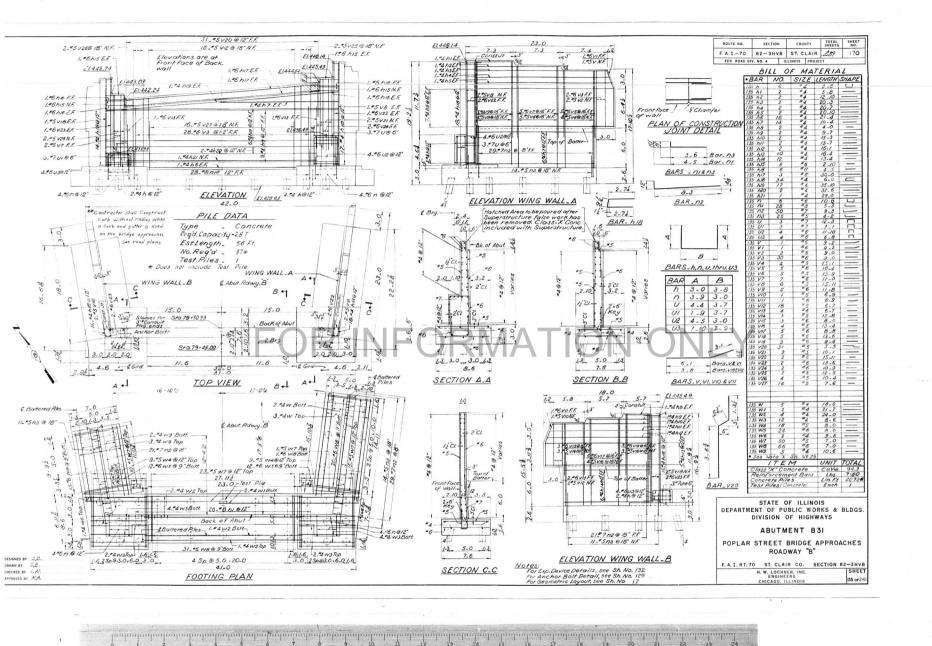
NOTE For location of Detail A. B or C see Floor Beam Schedule.

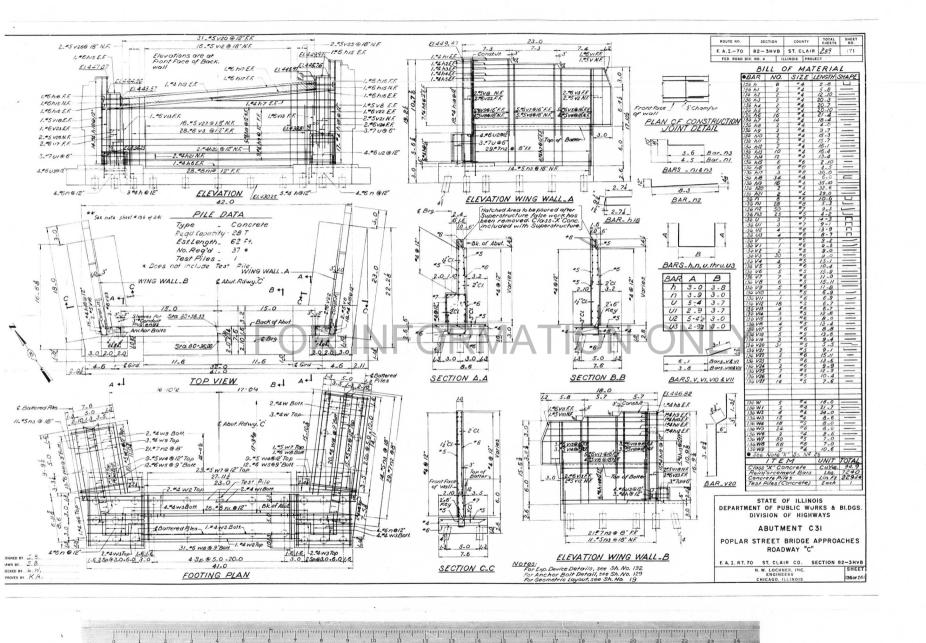
STATE OF ILLINOIS DEPARTMENT OF PUBLIC WORKS & BLDGS. DIVISION OF HIGHWAYS

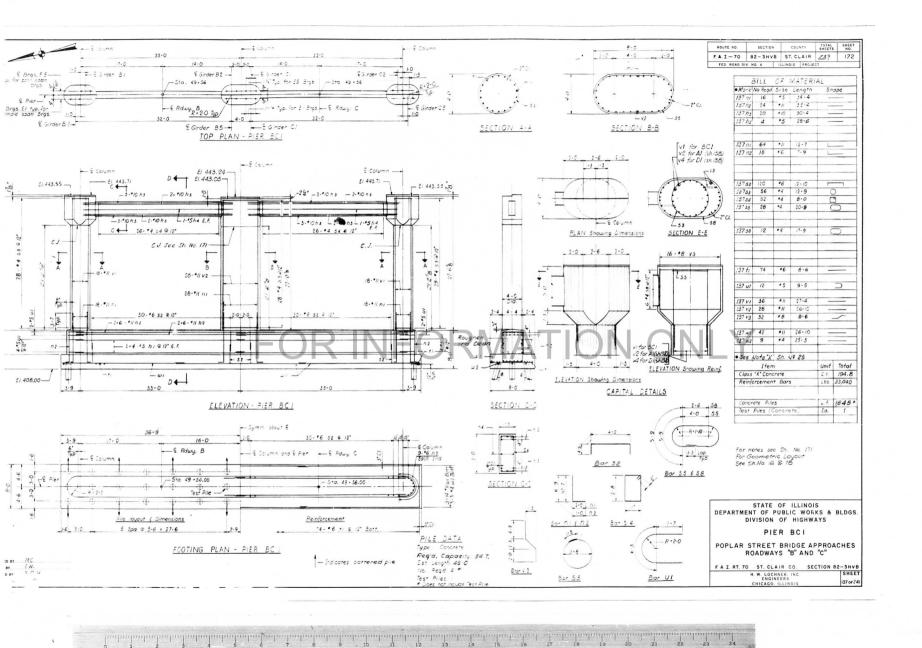
STRINGER SHIMS POPLAR STREET BRIDGE APPROACHES
ROADWAYS "A" "B" AND "C"
RAMPS "M" AND "S"

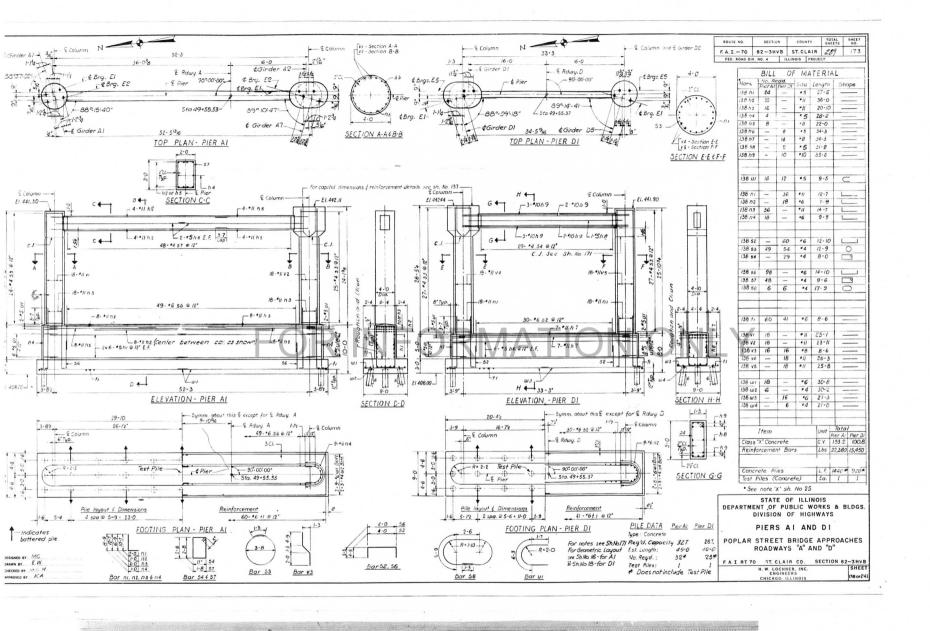
F. A. I. RT. 70 ST. CLAIR CO. SECTION 82-3HVB H. W. LOCHNER, INC. ENGINEERS CHICAGO, ILLINOIS

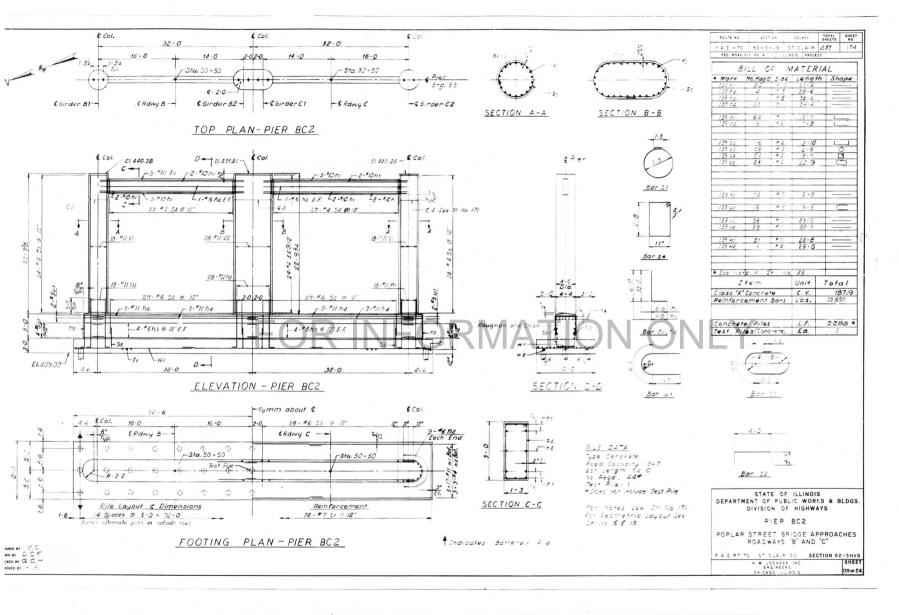


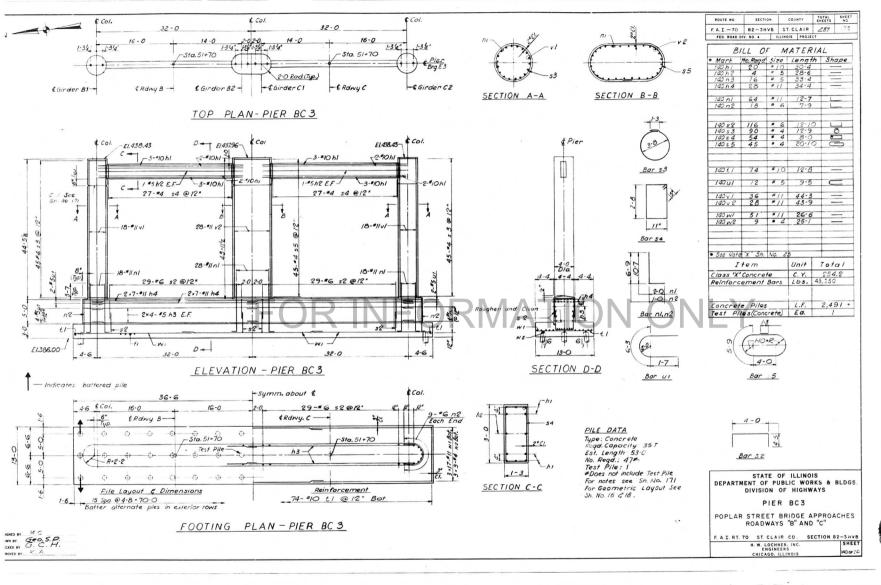












STATE OF ILLINOIS
DEPARTMENT OF PUBLIC WORKS & BUILDINGS
DIVISION OF HIGHWAYS

-	-	-	-	==
To	82-	st. Clair	289	175A

SHEET NO.

FOR INFORMATION ONLY

FOOTING FLAN

LEGEND

WETHE FOR

PILE DATA

TYPE: CONCRETE
CAPACITY: 35 TOOS

EST LENGTH: 46'
NO REQUIRED: 18

ADDITIONAL MATERIAL
CLASS I CONCRETE 2.6 C. YAS
CONCRETE PIRES 1932 LIN FI

AS BUILT

PIER BC 3
POPULAR STREET BRIDGE APPROACHES
FAT BY TO SEC 82-34VB
ST CLARE COUNTY
PROJECT \$150-74-116910

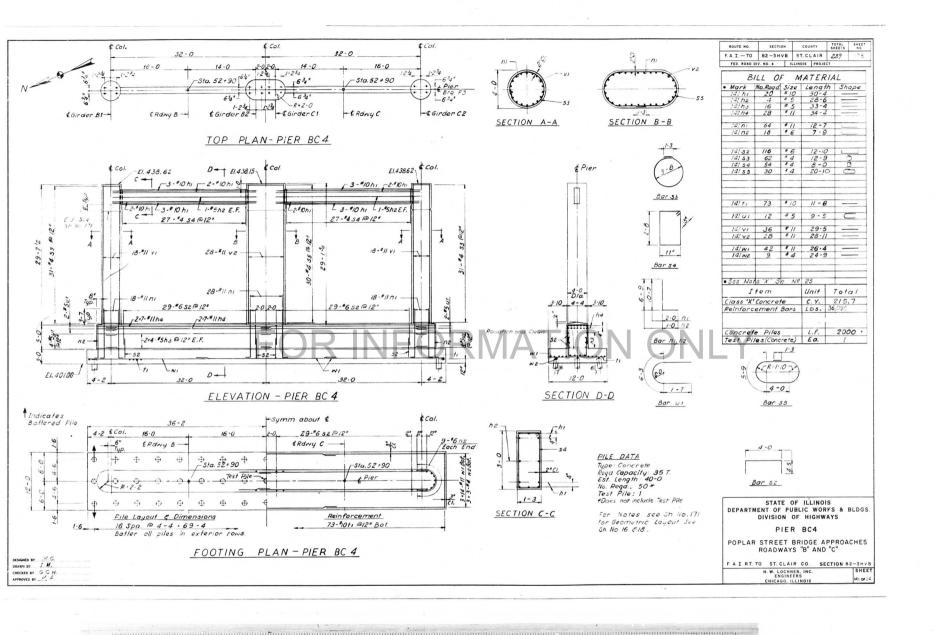
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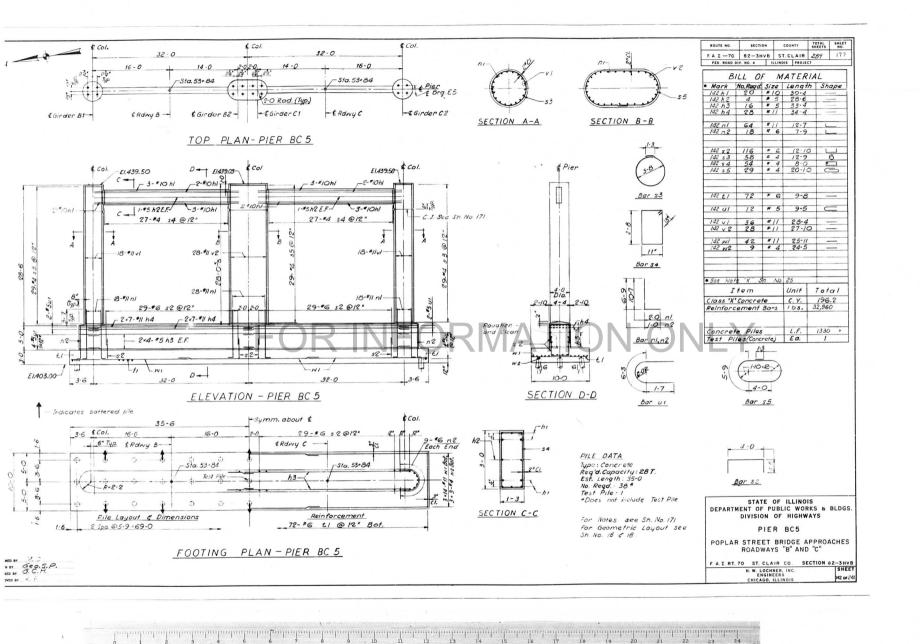
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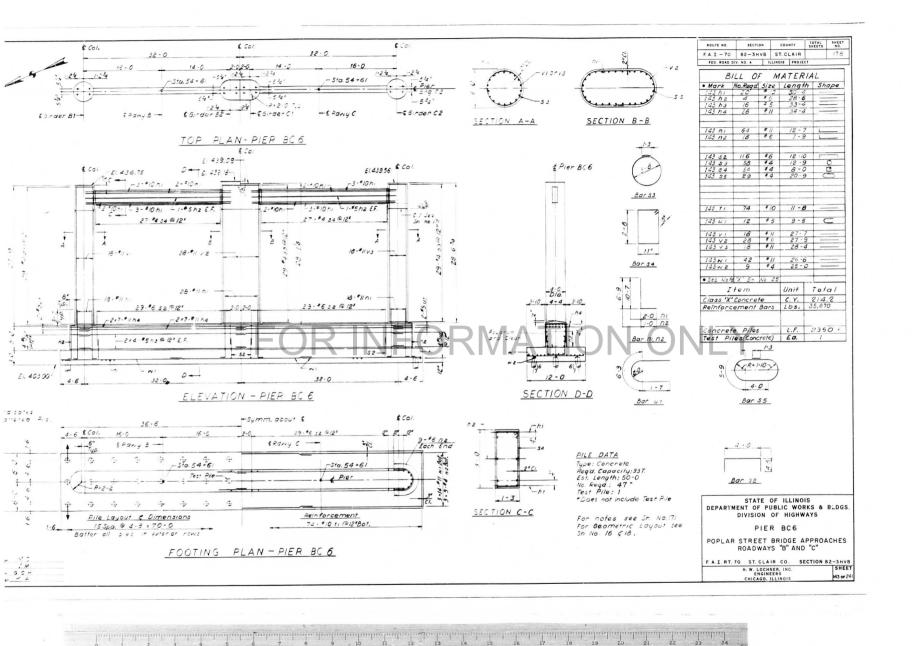
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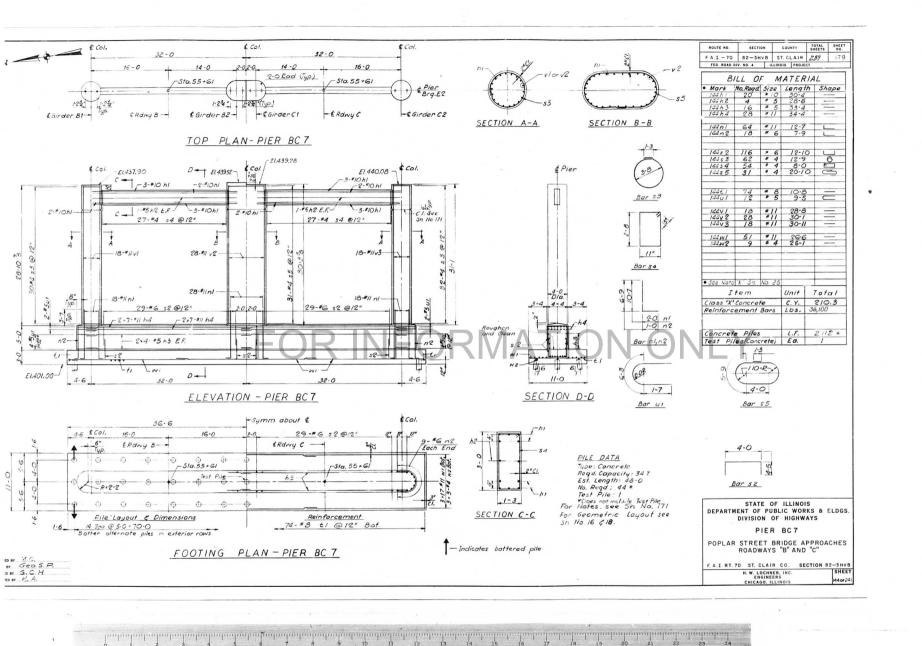
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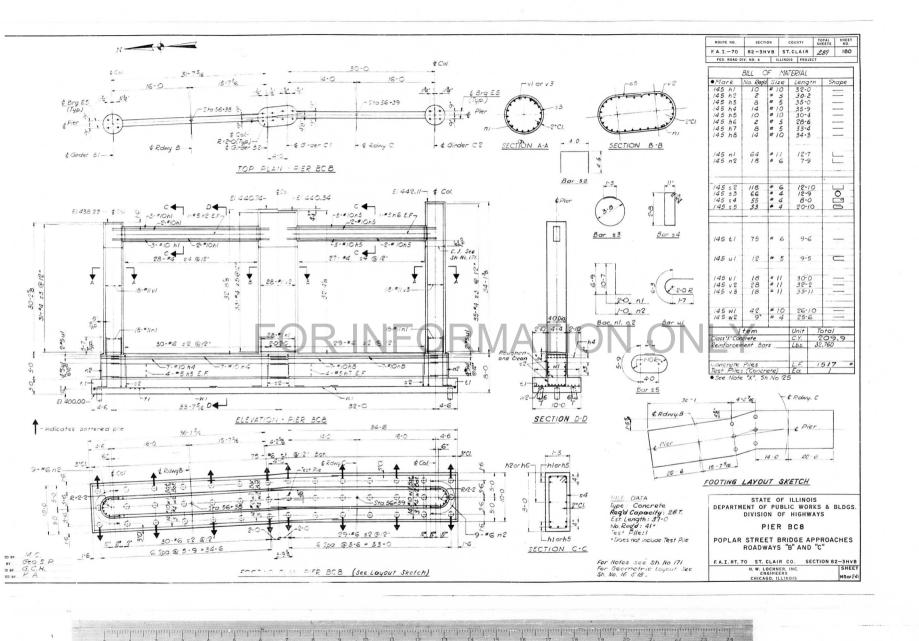
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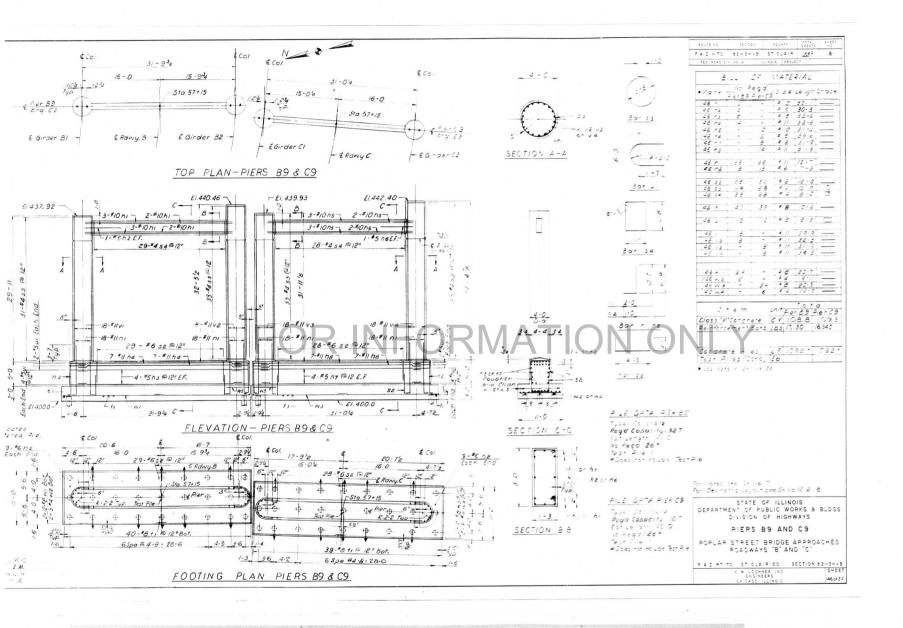


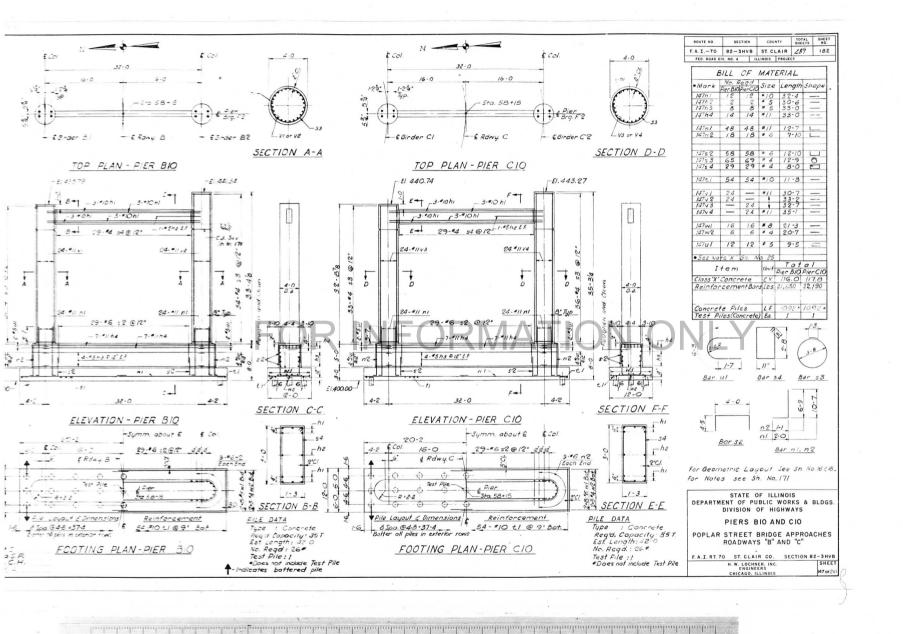


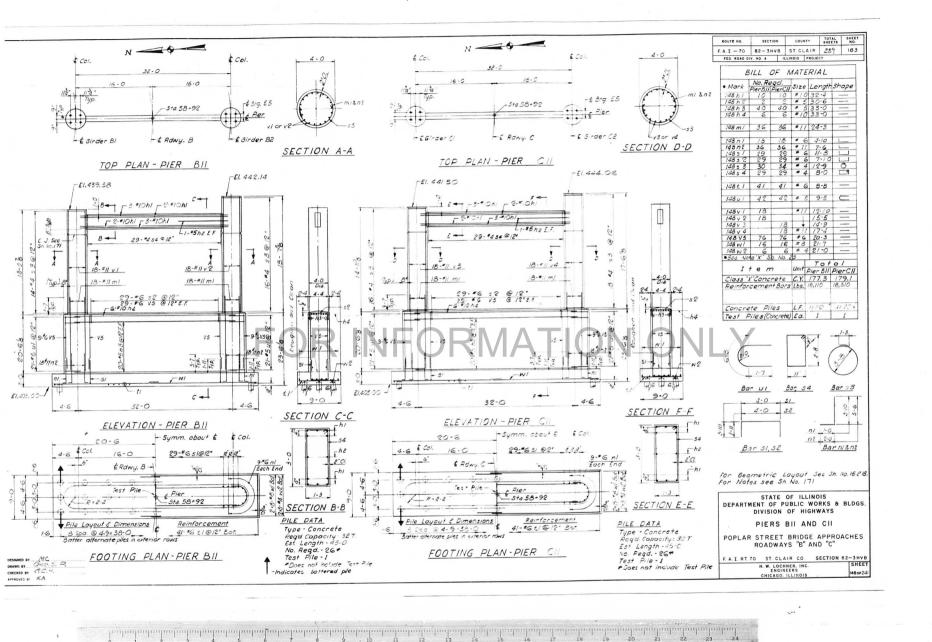


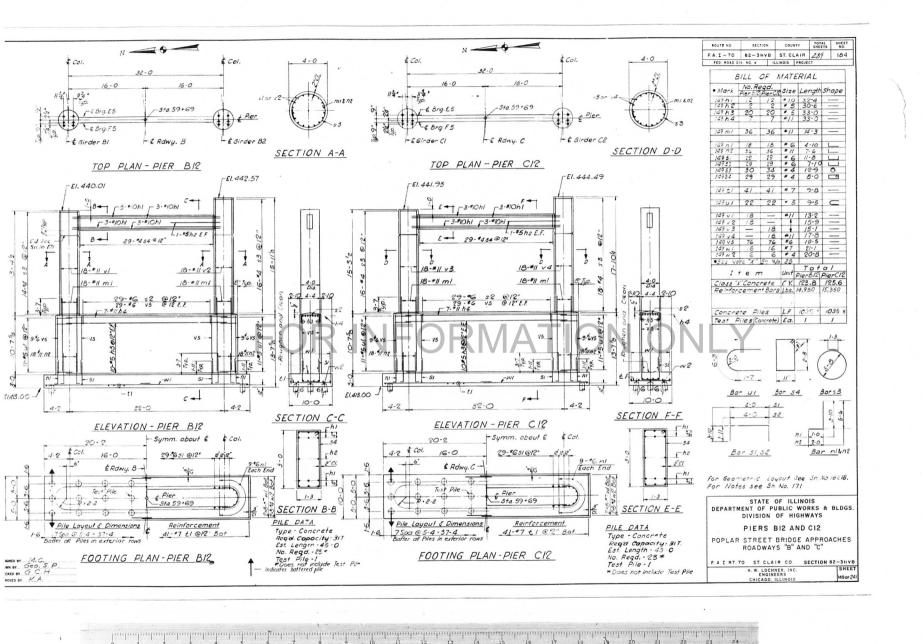


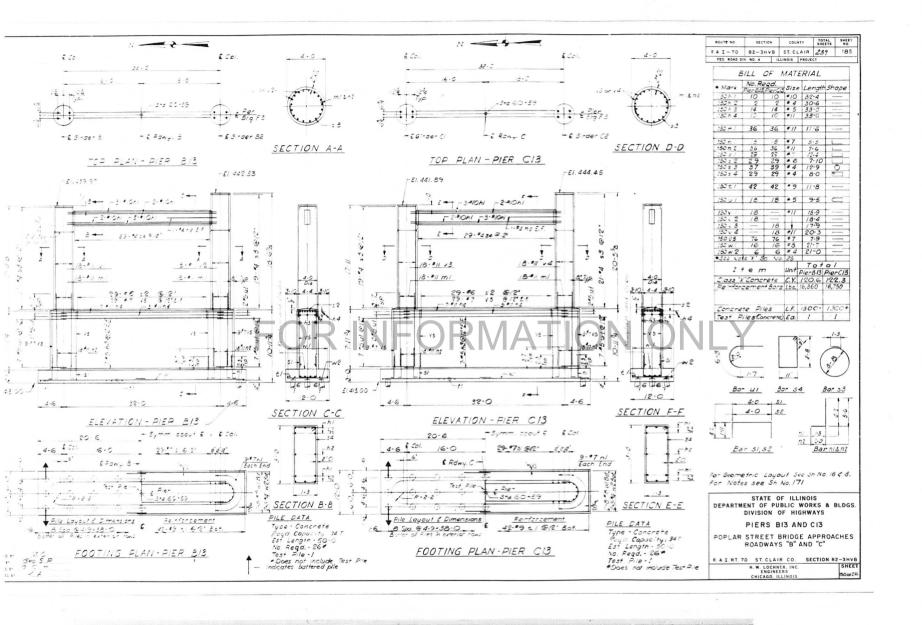


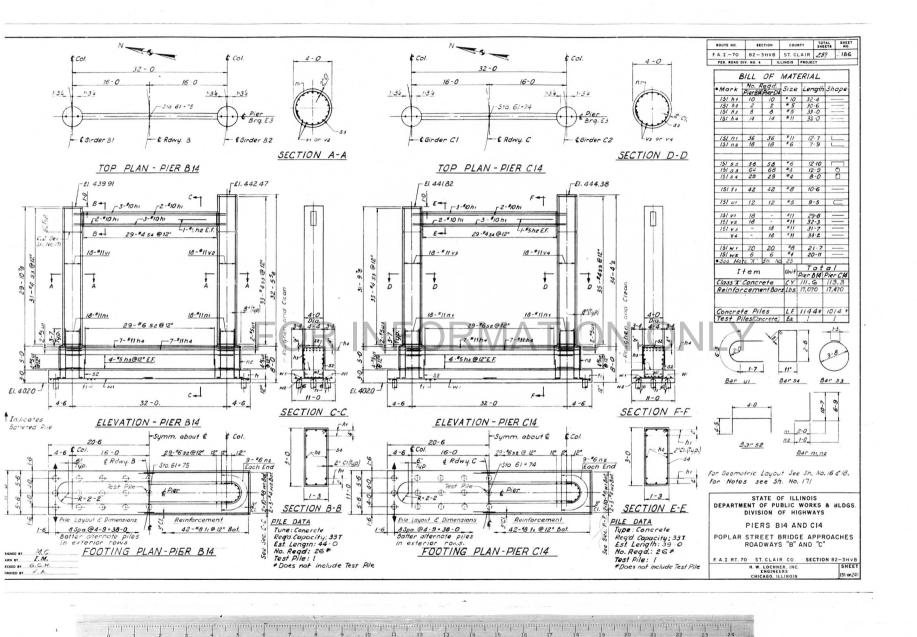


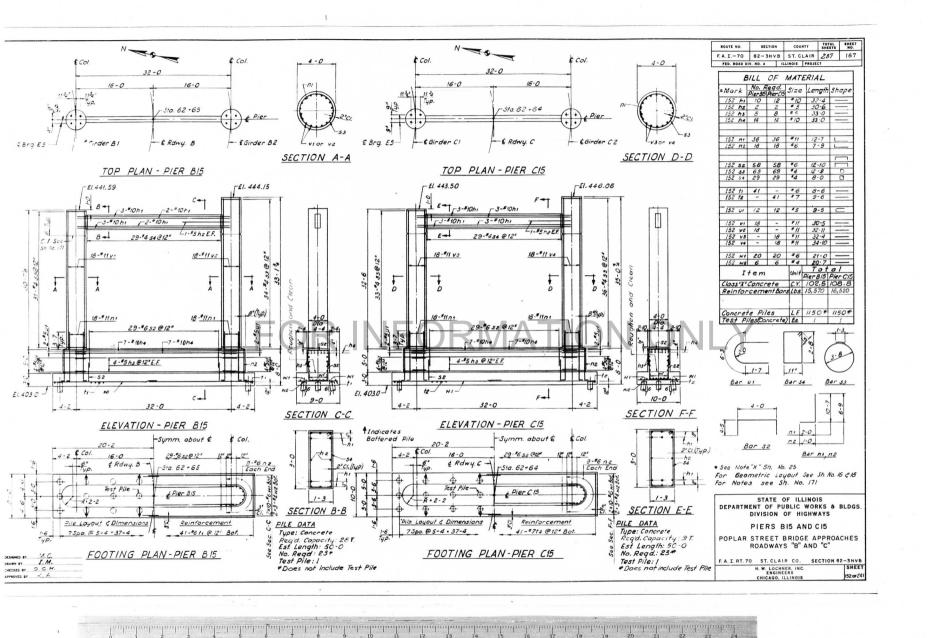


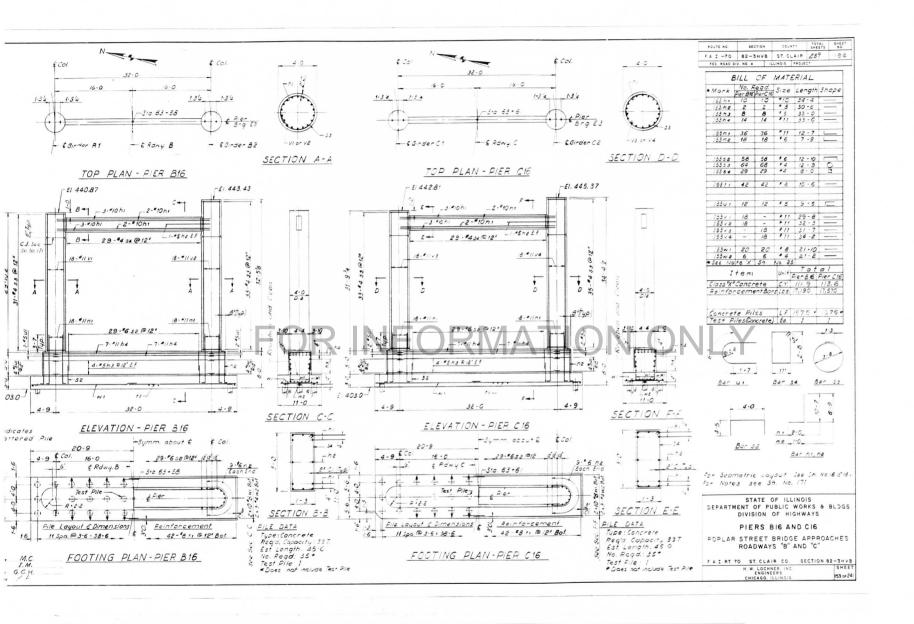


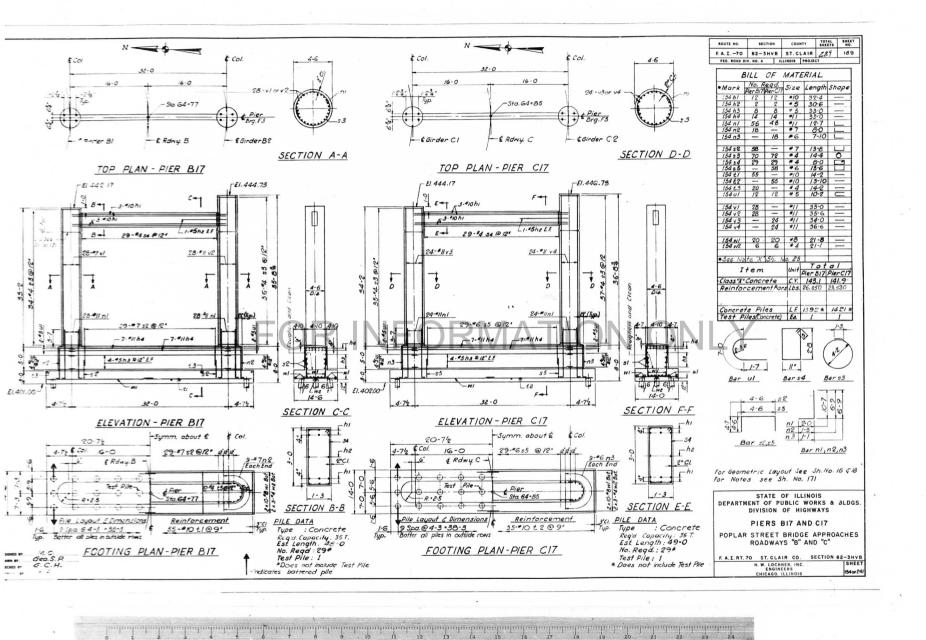


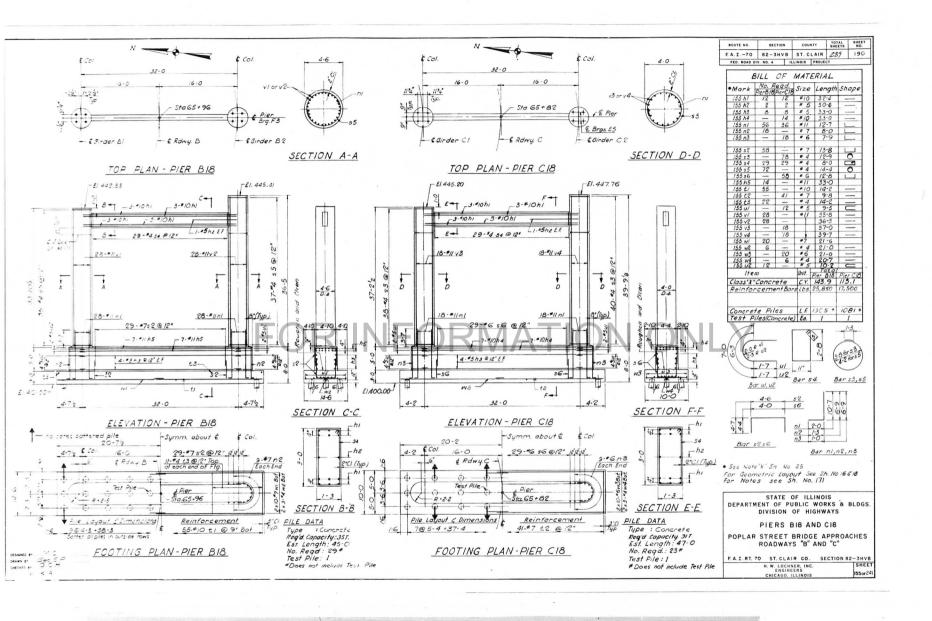


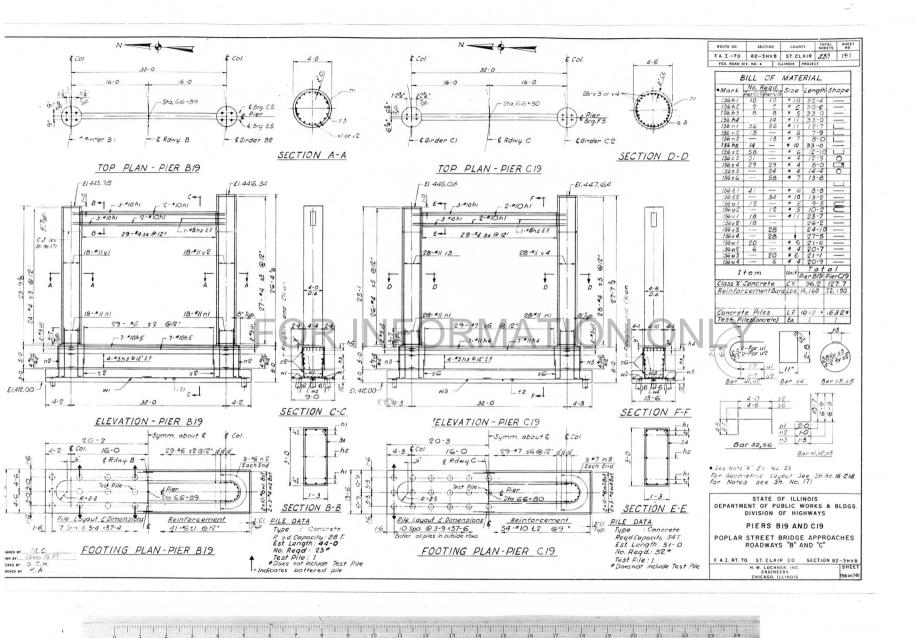


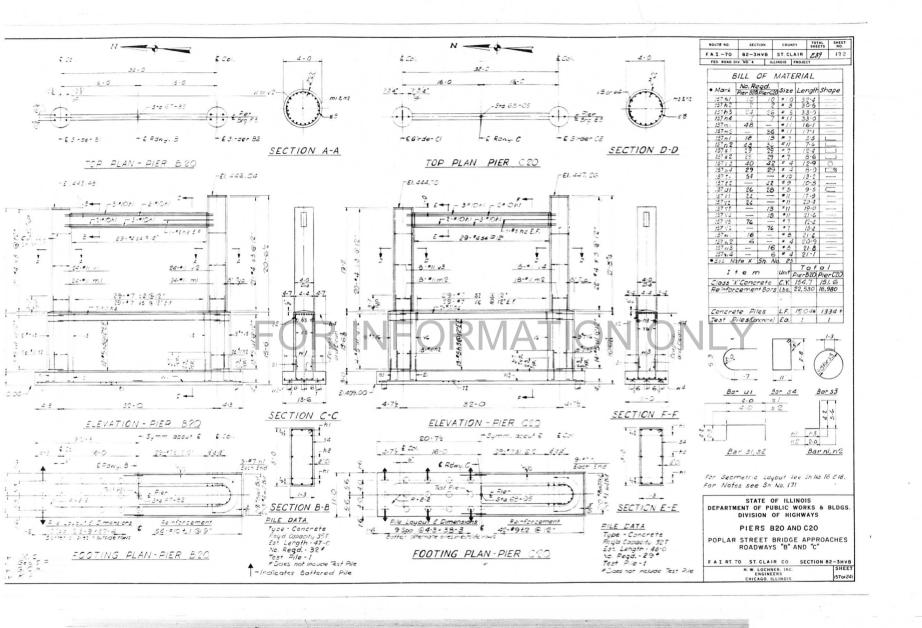


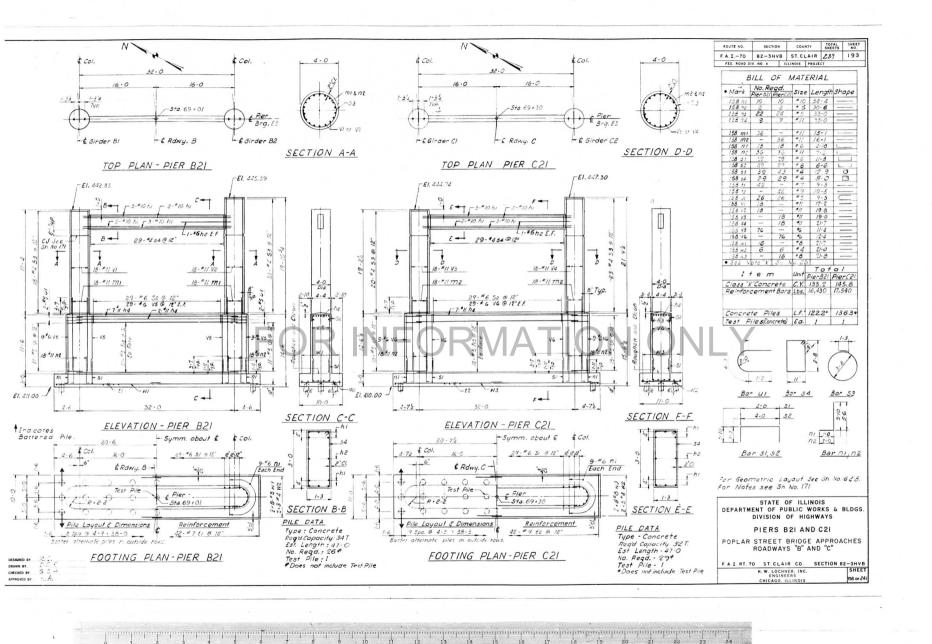


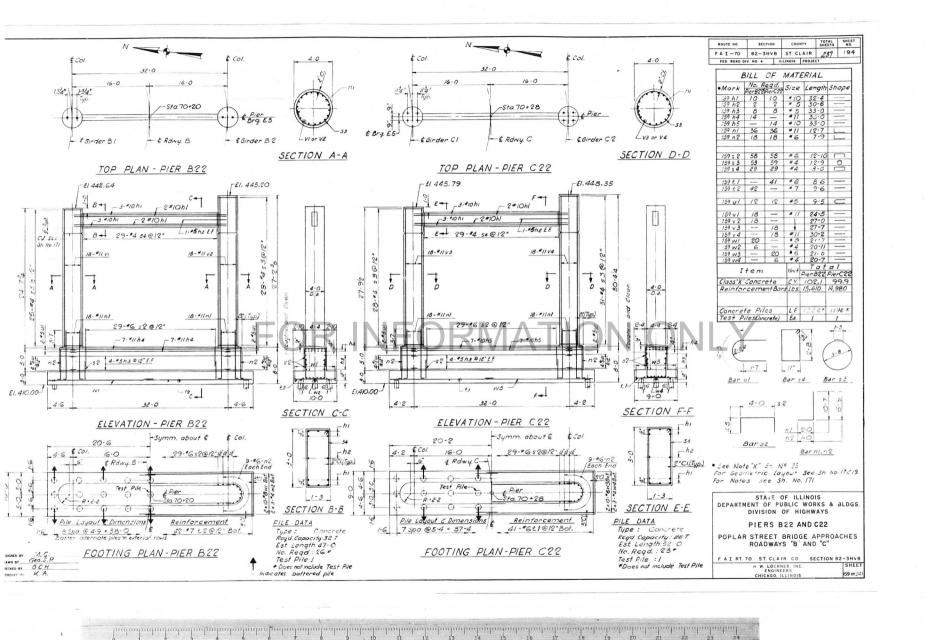


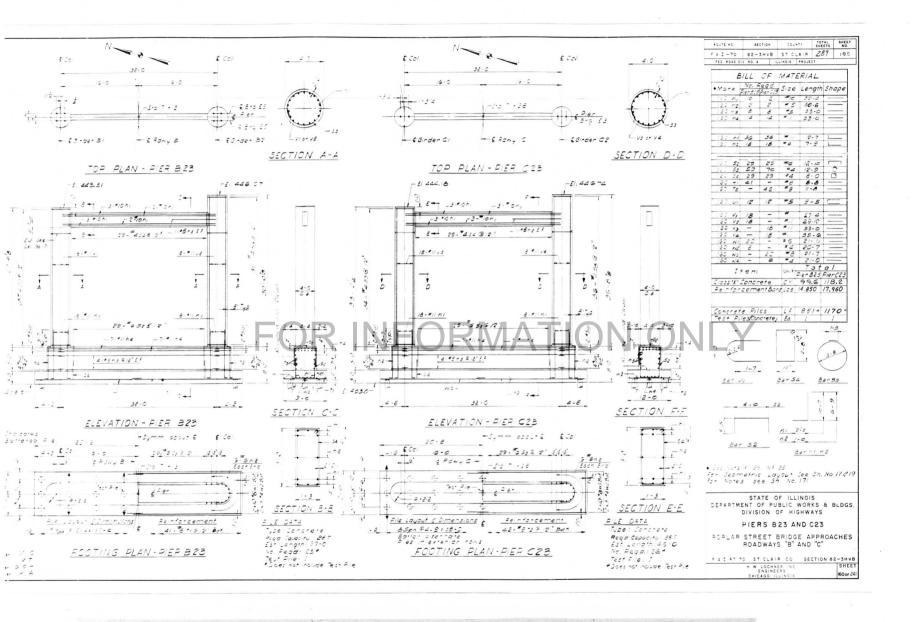




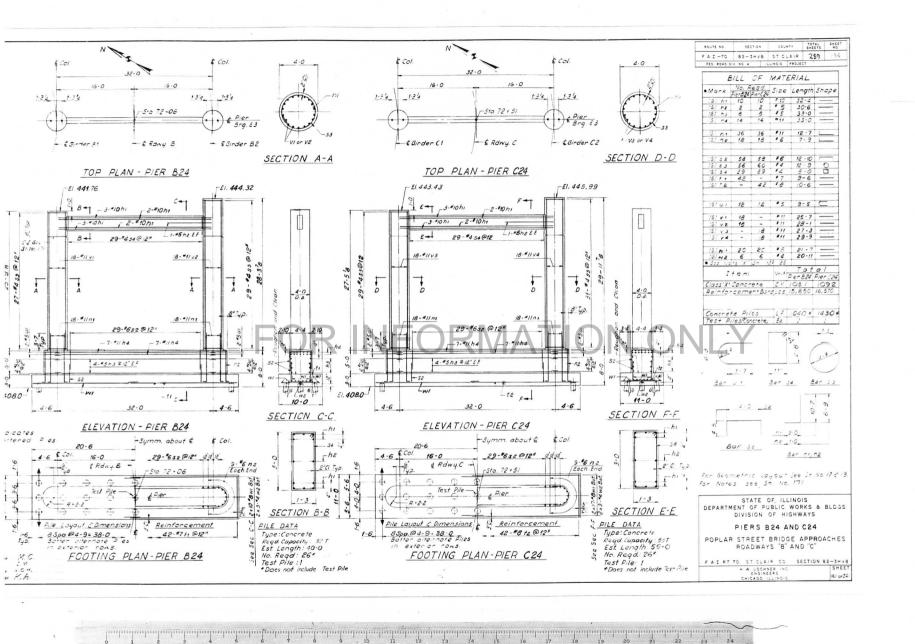


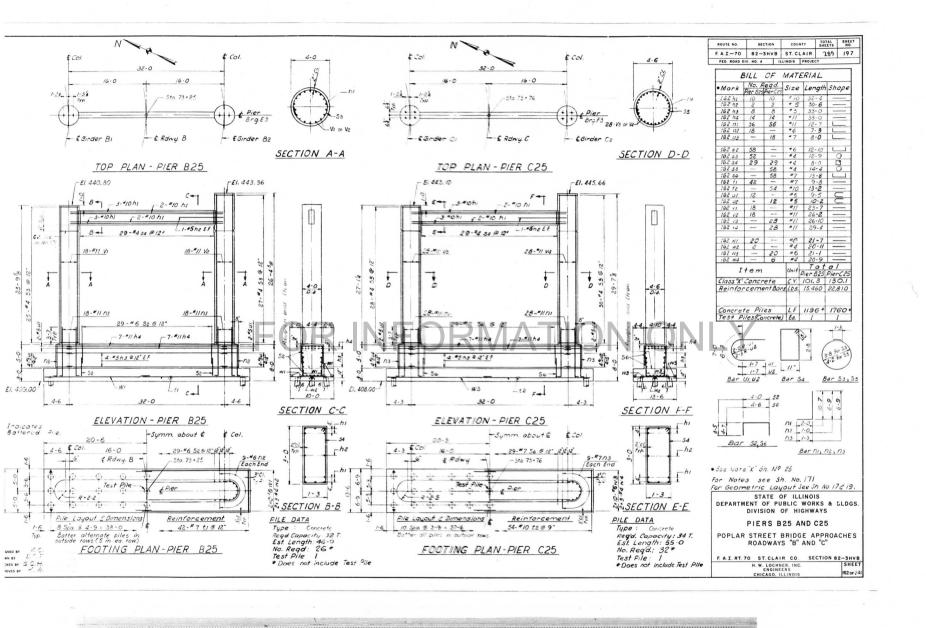


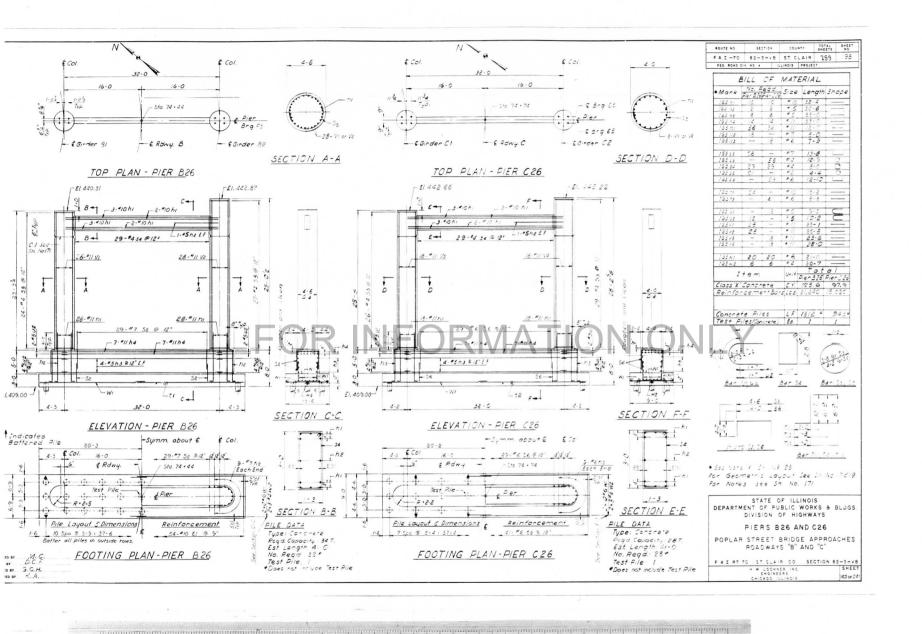


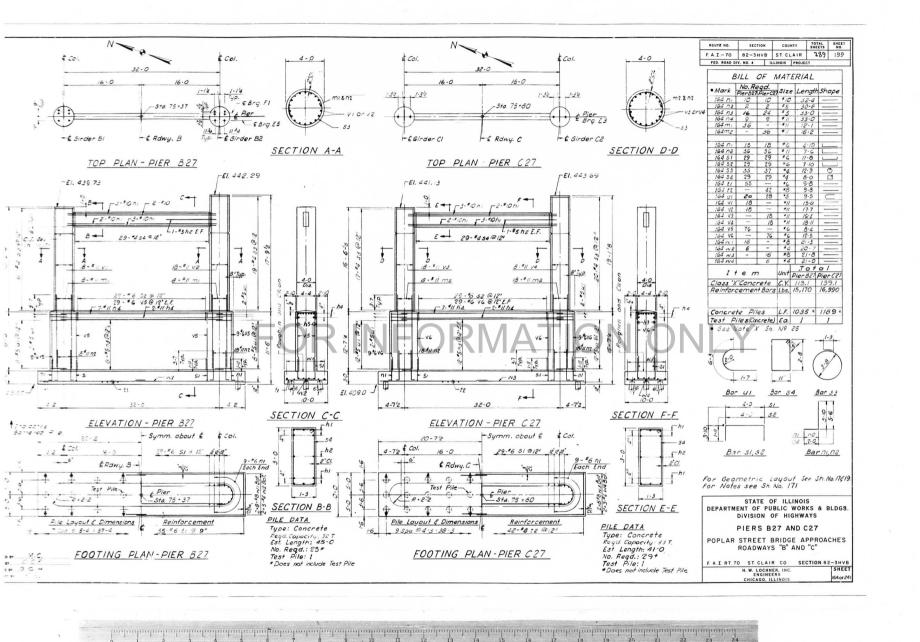


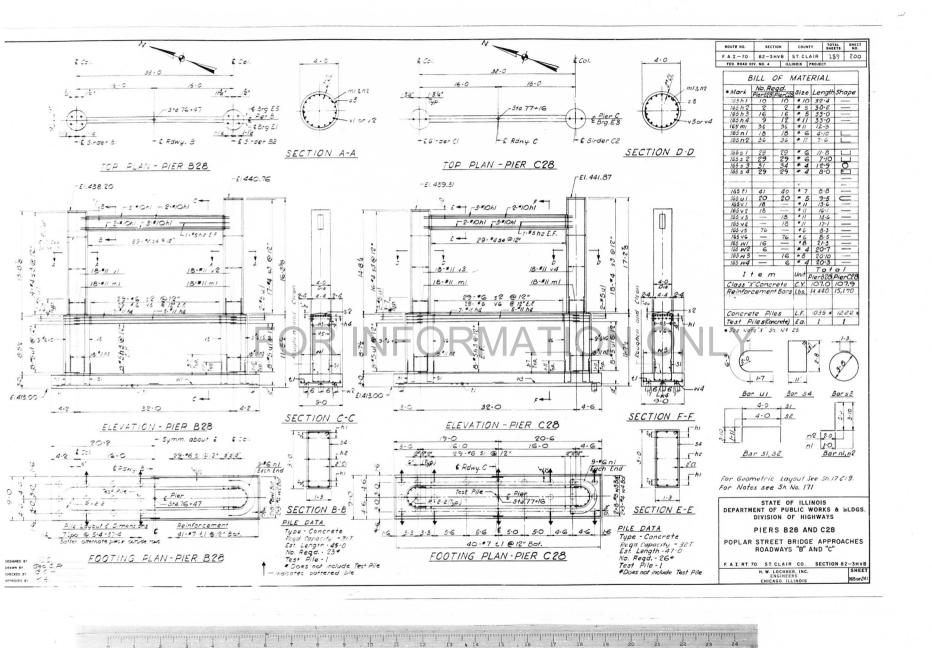
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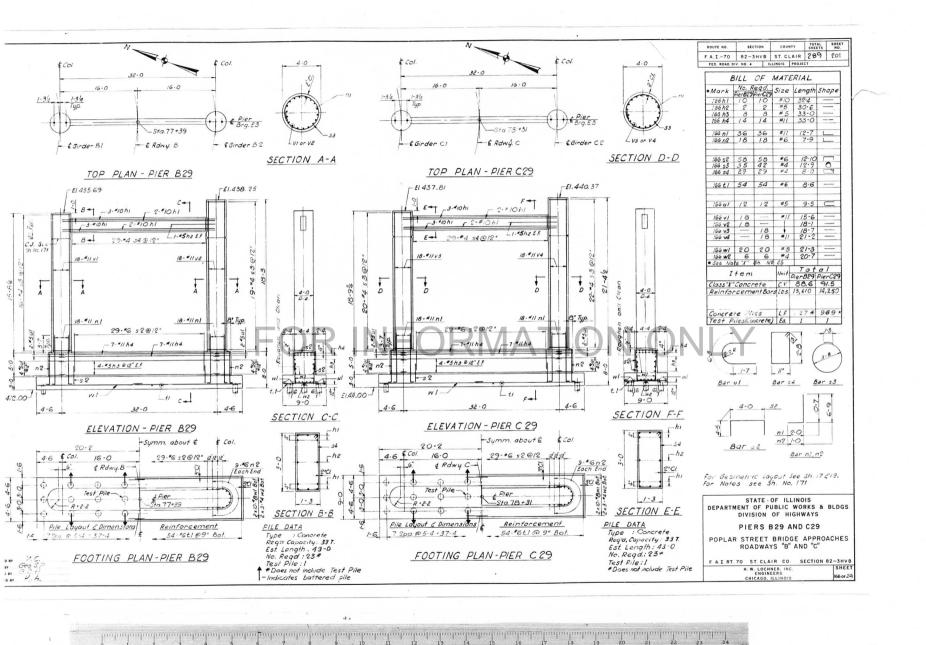


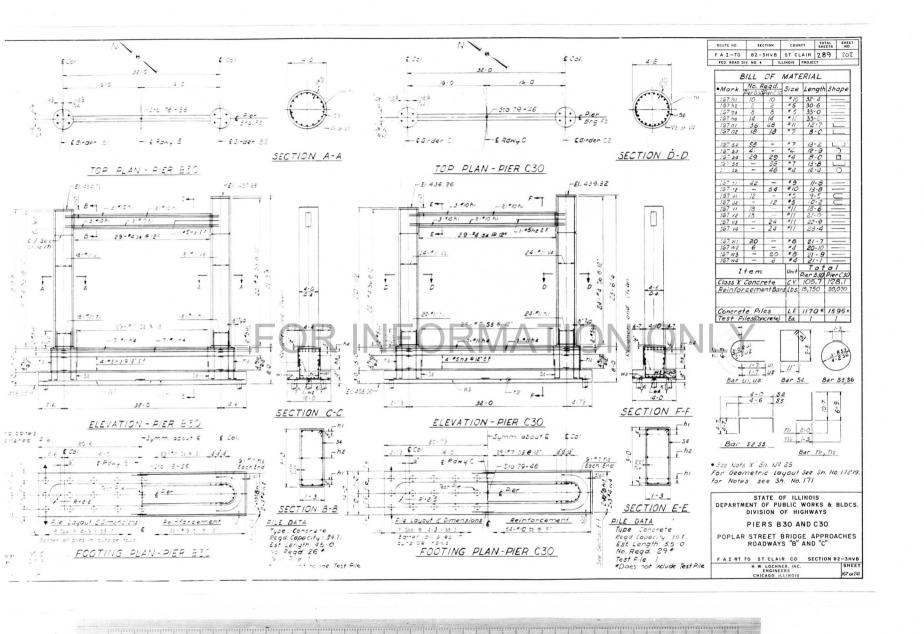


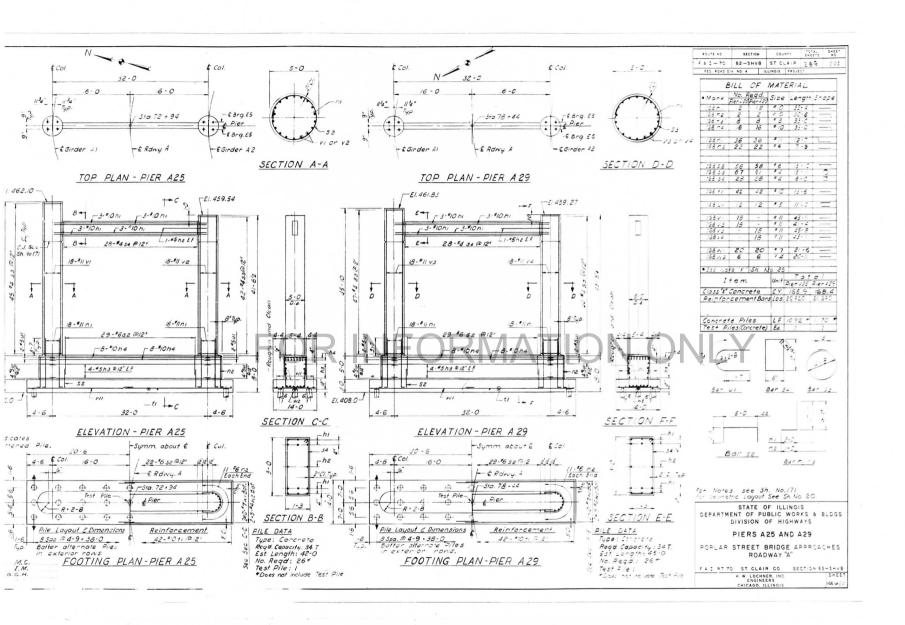


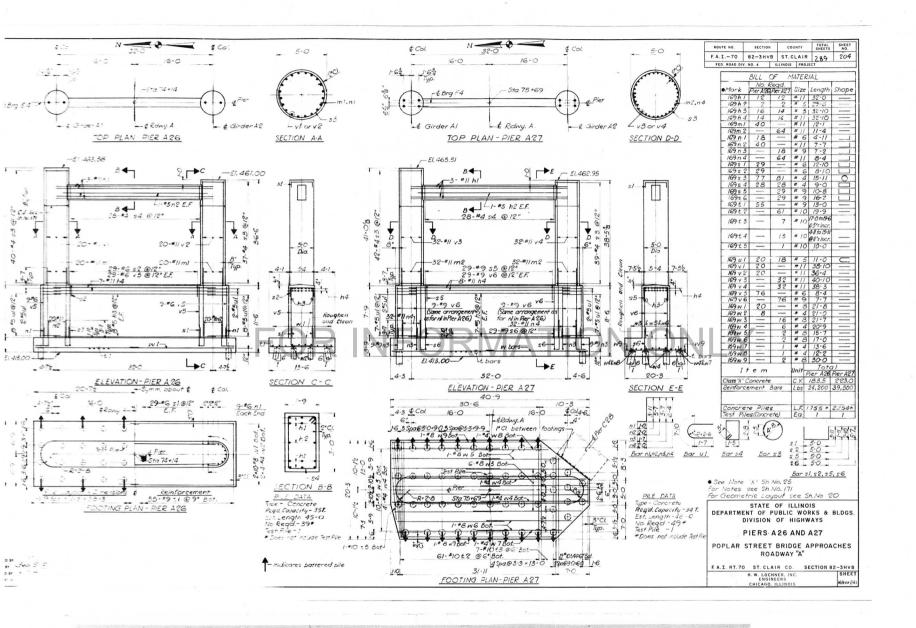




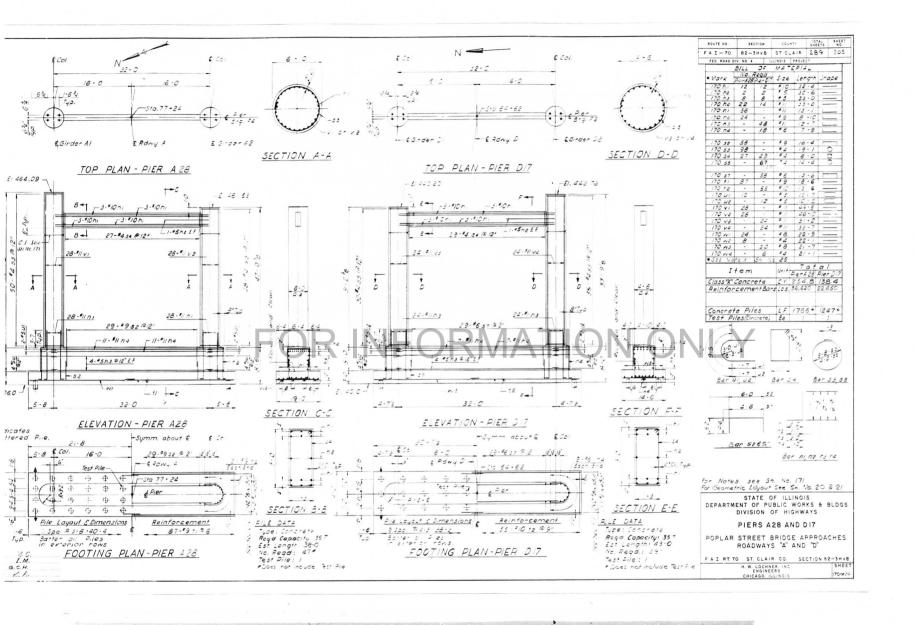


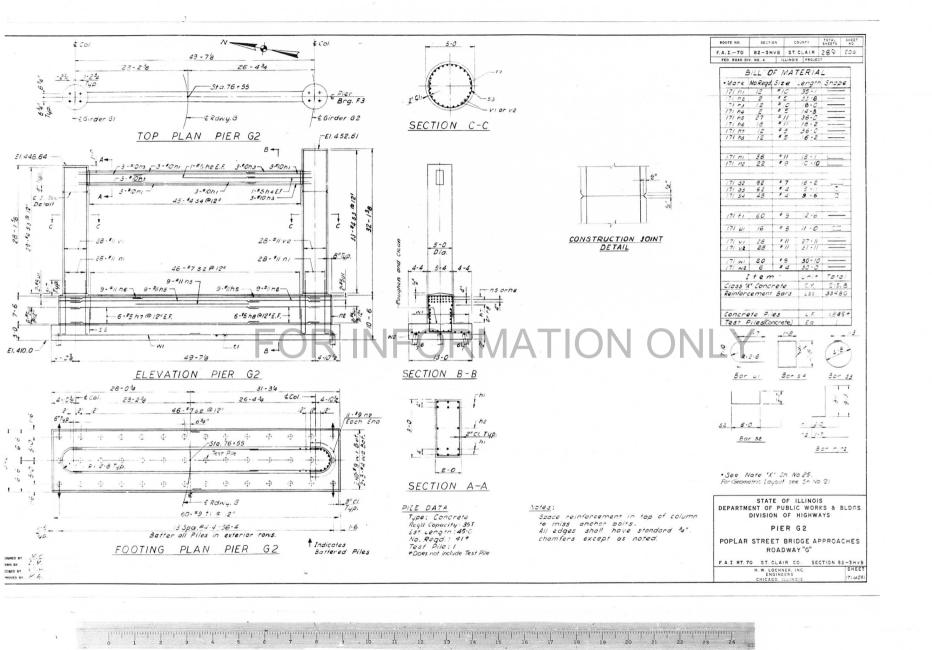


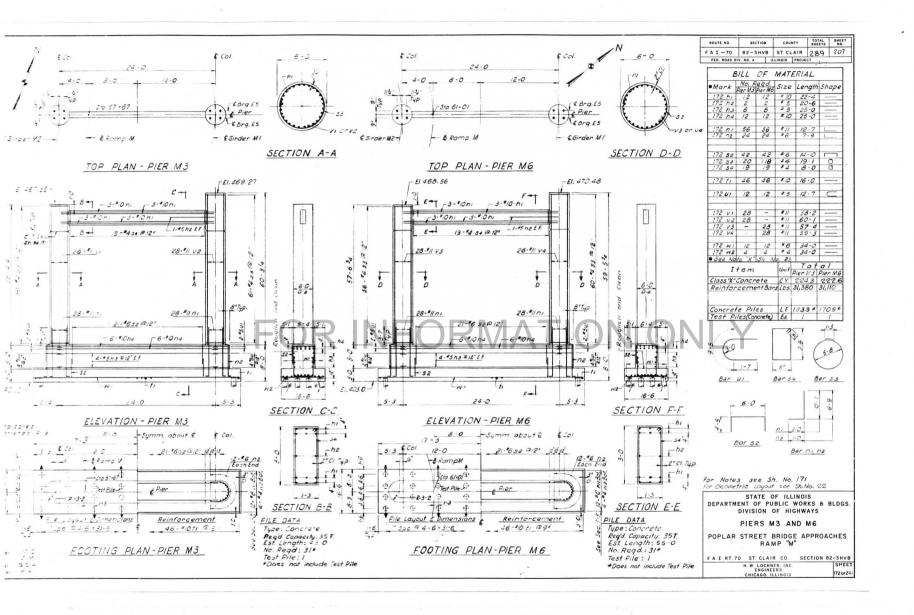




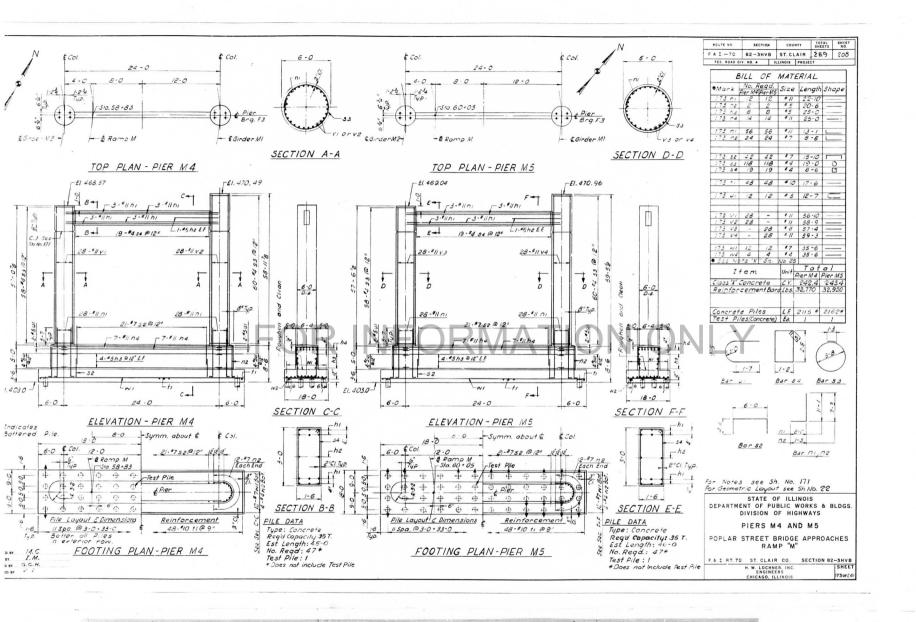
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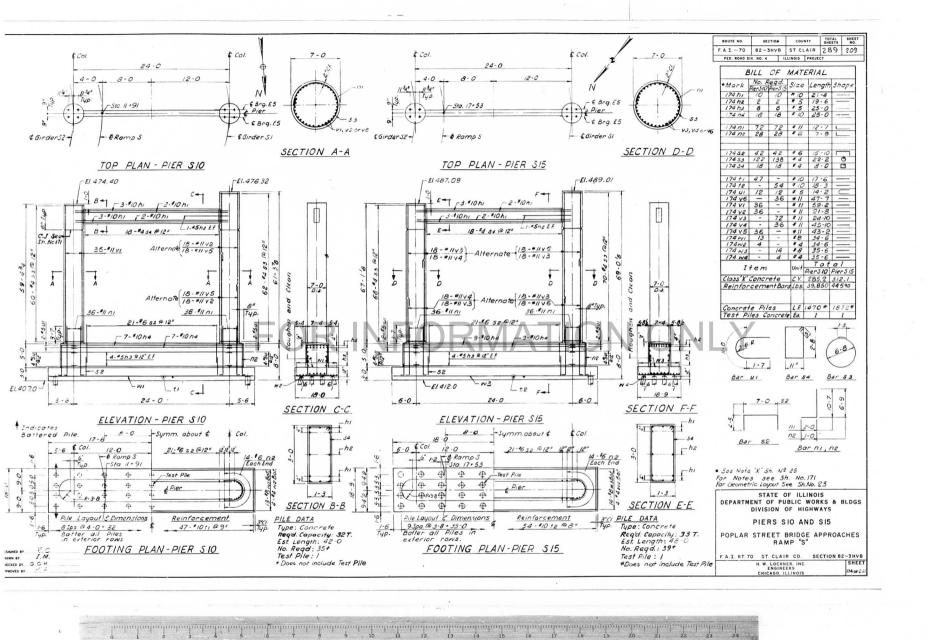


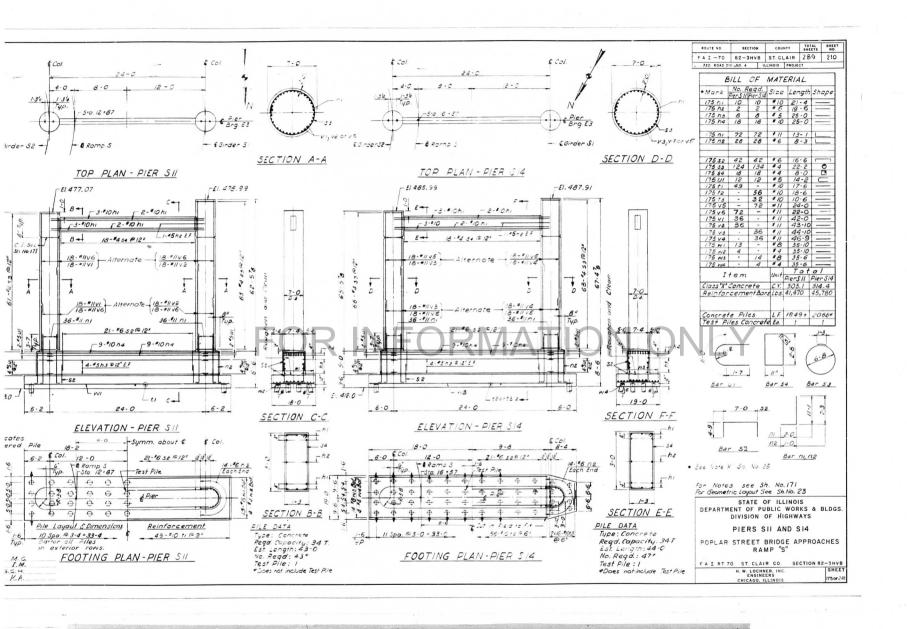


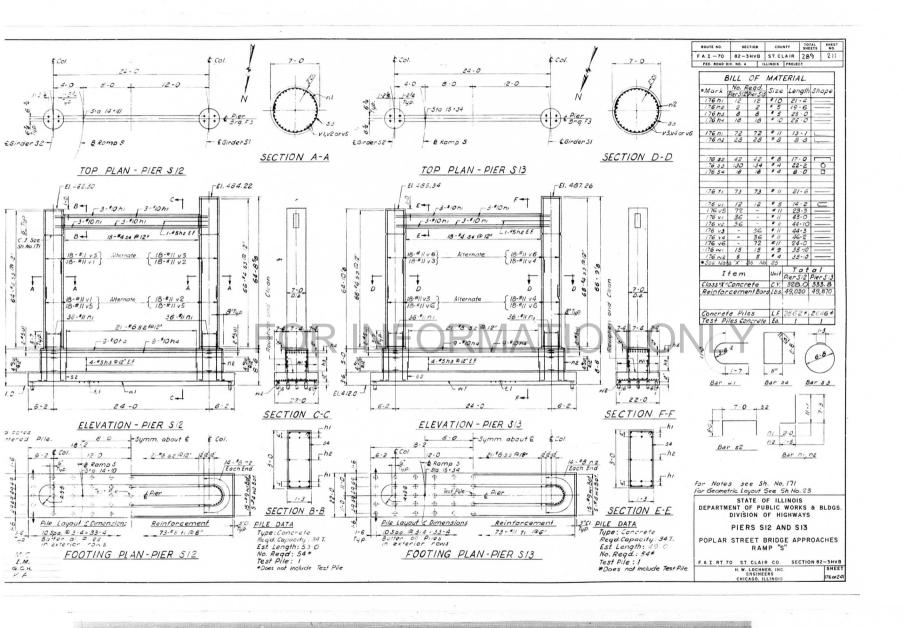


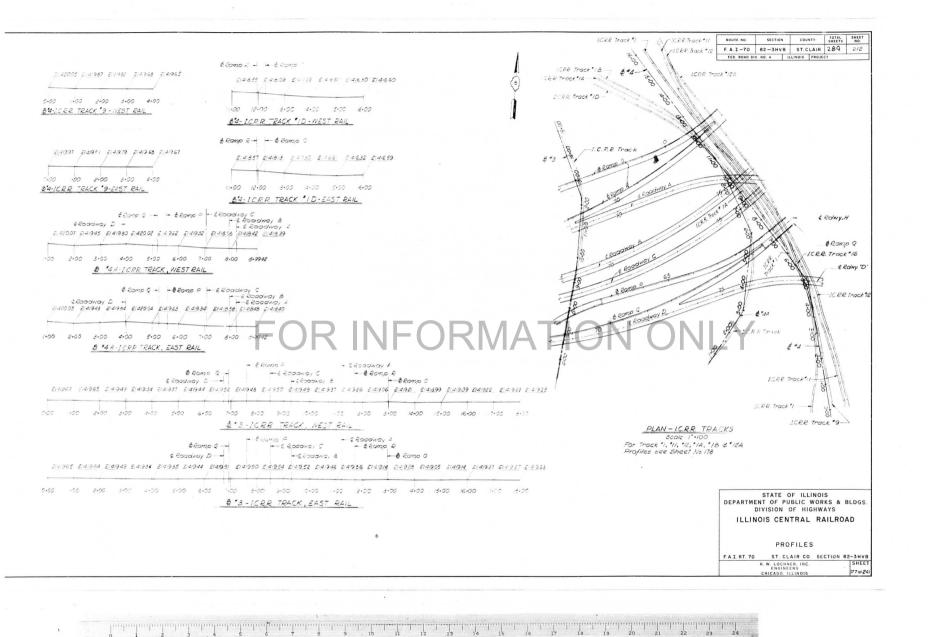
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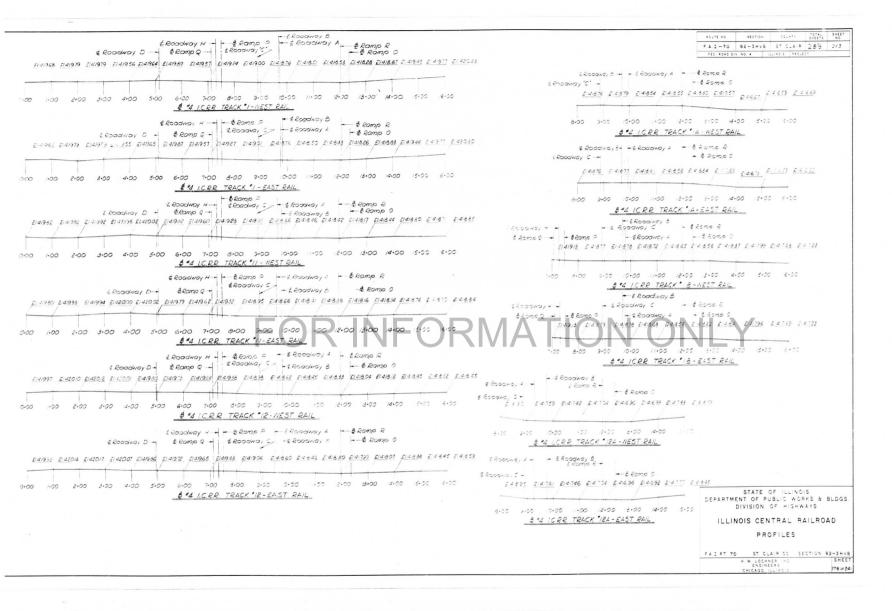




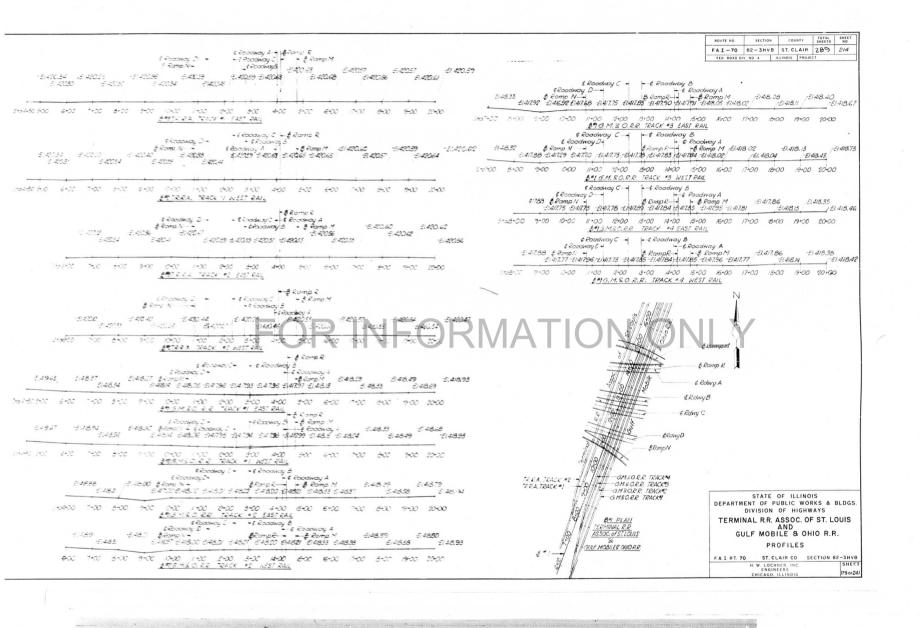


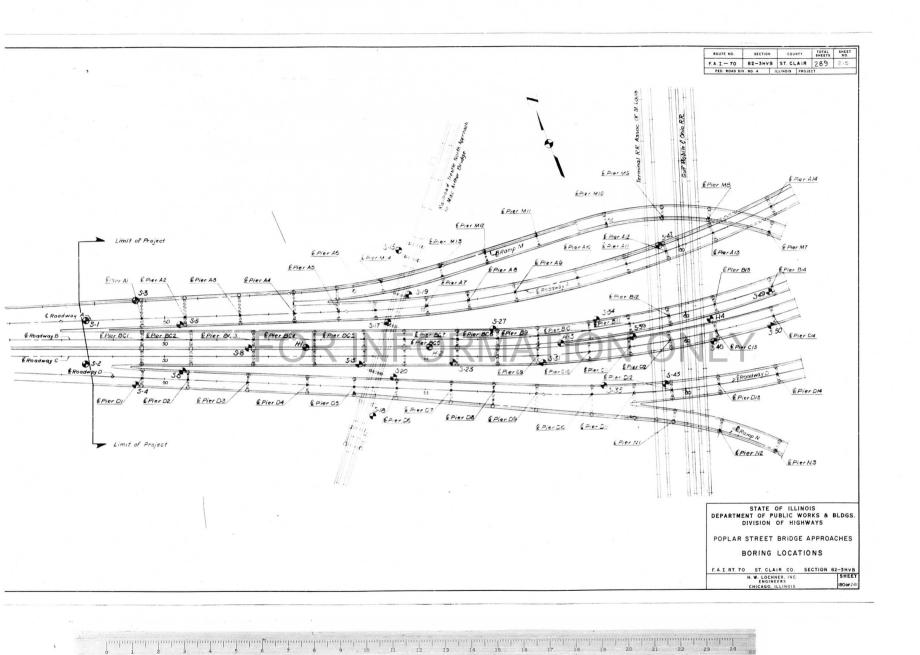


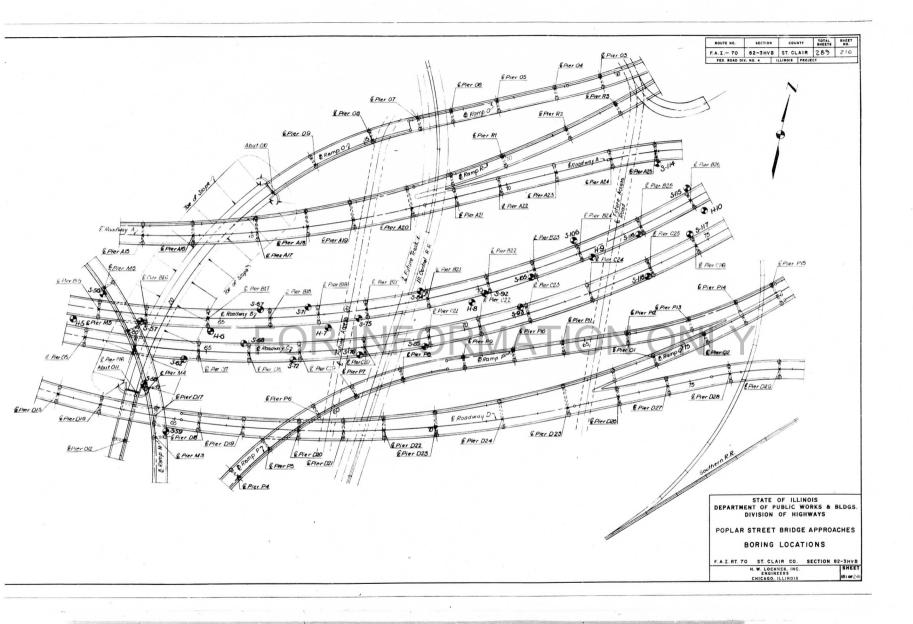


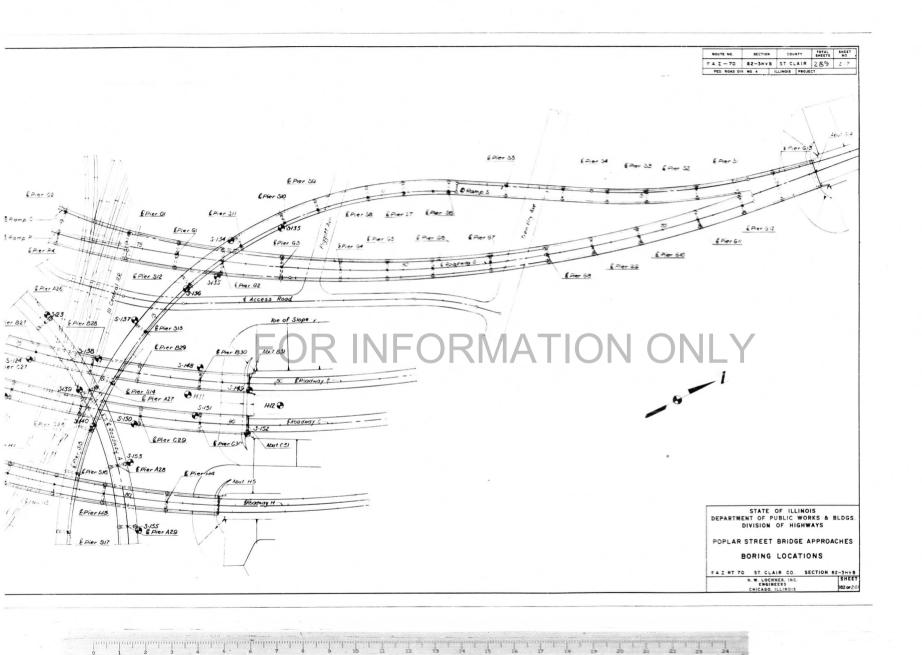


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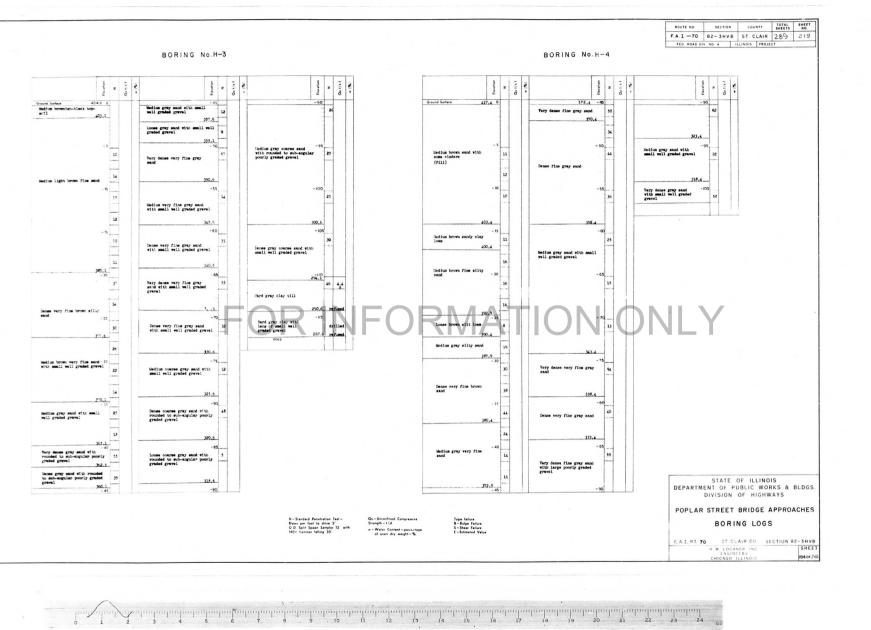


SECTION COUNTY TOTAL SHEET NO. F.A.I.-70 82-3HVB ST. CLAIR 289 218 BORING No. H-1 BORING No. H-2 Ground Surface Topeoil Very sell gray-mottled sandy clay 12 Dense fine gray sand Medium fine gray eard with small well graded gravel Medium gray sand with small well graded gravel Medium gray fatty 387.1 22 37/.1 Very dense gray rotten limestone Dense very fine gray silty sand Loose gray fine sand with pieces of rotten wood Dense fine gray sand Dense very fine gray silty sand with rounded to sub-sug poorly graded gravel Medium gray fine sand Medium fire gray sand 277.7 refused Delge fire gray sand Dense fine gray silty sand Loose coarse gray sand with small well graded gravel Medium fine gray sand STATE OF ILLINOIS 317.6 362.1 - 45 DEPARTMENT OF PUBLIC WORKS & BLDGS. DIVISION OF HIGHWAYS POPLAR STREET BRIDGE APPROACHES Qu - Unconfined Compressive Strength - 1/st w - Water Content - percentage of even dry weight - % BORING LOGS Type failure

B - Bulge Failure

S - Shear Failure

E - Estimated Value N - Standard Penetration Test -Blows per foot to drive 2" O D. Split Spoon Sampler 12" with 140" hammer falling 30". F. A.I RT 70 ST. CLAIR CO. SECTION 82-3HVB H. W. LOCHNER, INC. ENGINEERS CHICAGO, ILLINOIS 183 of 241



SECTION COUNTY TOTAL SHEET NO FA I -70 82-3HVB ST. CLAIR 289 220 BORING No.H-6 BORING No. H-5 z i Ground Surface 405.5 5 Medica black topent! Fround Surface 407.2 0 Medium black topeoil 406.2 tion pro fin and medica gray very firm 19 Medium very fine gray sand with large poorly graded gravel Hedium brown very fine Loose gray stity loss Medium gray coarse sand with rounded to sub-angular 12 poorly graded gravel Very loose gray silty clay loss toose gray coarse sand -105 with rounded to sub-angular moorly graded gravel -15 Medium light brown fire sand Dense gray coarse sand with small well graded gravel 12 drilled Very dense rotten limestone 290.2 drilled 25 - 75 21.2 -60 later very five one land letius gray min-angular poorly gradet gravel 'edium very fire year eard with small well graded gravel 19 Loose gray fine sand with containous graves 13 STATE OF ILLINOIS
DEPARTMENT OF PUBLIC WORKS & BLDGS.
DIVISION OF HIGHWAYS POPLAR STREET BRIDGE APPROACHES BORING LOGS Type fature

8 - Burge Fature

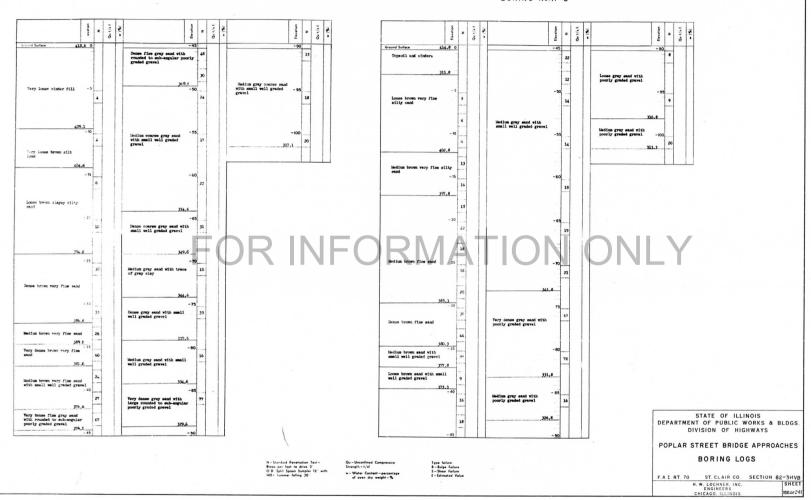
5 - Shew Fature

1 - Internet Fature will Migher Content - percentage of siven bry weight - % FAIRT 70 ST CLAIR CO SECTION 82-3HVB M W LOCHNER INC. ENGINEERS CHICAGO, ILLINOIS

0 1 2 3 4 5 5 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 55

BORING No. H-7

BORING No. H- 8



ROUTE NO. SECTION COUNTY TOTAL SHEET NO.

F.A.I.-70 82-3HVB ST. CLAIR 289 222 FED. ROAD DIV. NO. 4 ILLINOIS PROJECT

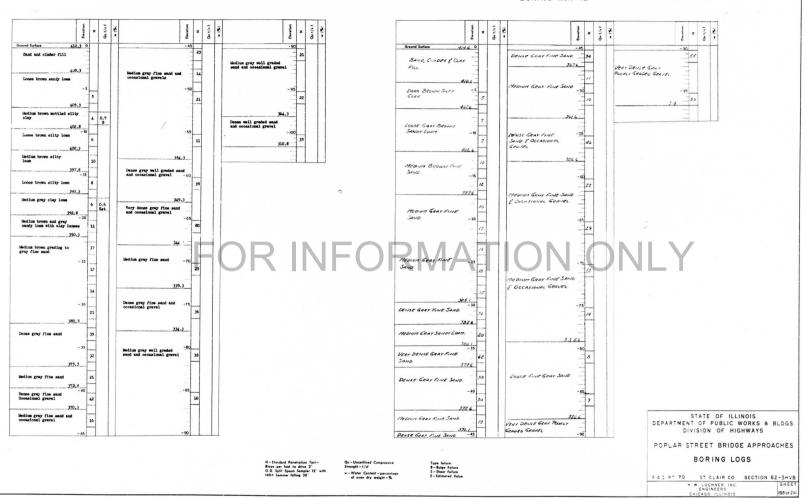
BORING No. H-10 BORING No. H-9 Ground Surface Send and cinder fill Very noft elightly silty clay Medium gray sand with small well graded gravel Medium gray clay Loose gray fine sandy Dense gray very fine sand STATE OF ILLINOIS
DEPARTMENT OF PUBLIC WORKS & BLDGS.
DIVISION OF HIGHWAYS POPLAR STREET BRIDGE APPROACHES BORING LOGS Type failure: B - Bulge Failure S - Shear Failure E - Estimated Value F. A. I. RT. 70 ST. CLAIR CO. SECTION 82-3HVB w - Water Content - percentage of oven dry weight - % H. W. LOCHNER, INC. ENGINEERS CHICAGO, ILLINOIS

1 2 3 4 5 7 8 9 15 11 12 13 14 15 16 17 18 19 20 21 22 23 24-

ROUTE NO	SECTION	cou	NTY	SHEETS-	NO
F A I - 70	82-3HV	B ST. C	LAIR	289	223
FED. ROAD DIV	NO. 4	ILLINOIS	PROJE	CT	

BORING No. H-II

BORING No. H-12



FAI-70 BZ-3MVB ST CLAIR 289 FER BOAR DIN NO 4 | ELINOIS | PROJECT BORING No. S-I BORING No. S-2 BORING No. S-3 BLEV. H AU V 1.17. . DU V DEPTH BLOWS T/S.F. S IDENTIFICATION DESTRUCTION (continued) Some Silt Trace clay Ground Surface .18.3 J Ground Surface Ground Surface (continued Loose Cinder and Brick Fill Fine to Medium Dense Ginder, Brick & Misc. Fill Sand Stiff Brown Silty Clay Some Brick & Cinder \_ 12 Gray Trace Medium Greyish-Brown Silt Fill Silt 5 12 1.858 13 Soft Tellow Brown Clayer Silt, trace fine and fill LU7.1 347 Fine 365.3 Medium Dense Dinder, prick with bloy will 55 28 55,37 55 30 Dense To Black Cinder Fill Medium Salt Soft Cinter, Coal, Gravel and Brown Silty Clay 10 10 5 1.315 22 Silt. ∃" Medium Coal 62 52 Course 60 m 60 36 Cinder Send Gran Sand 36 3 Trace Miscellaneous Silt, F111 65 65 45 33 Soft Very Loose Grey Fine Sand with 3" Pocket Decomposed good Dark .445 39 orey Sand 70 100 Compact Grey Loose gray fine to medianni, tr. silt-medianni, tr. silt-medianni, tr. silt-medianni, tr. silt-trace fine to Medium Sand, some silt, trace clay 168.6 ine to 25 eilt 187.0 Fine Sand .53 .875a8 3 .ley Very Dense Gray Fine to Medium Sand, Trace Silt \_ . .548 36 3388 75 92 rine Cleyey Soft 363.6 -3ù PATER LEVEL 16 Gray Medium Clayey 3 .618 40 - 3 Light
Gray
Fine to
Medium
Sand
Some
Silt
Trace
Clay send .45B 32 Silt 35 7 15 3 .748 34 Silt Vurved Loose Grey Fine Send Trace Silk 85 76 Trace Small Very Loose Fine Sand Loose Grey Fine Med Silty Sand Redium Cense poring Stopped by Inspector. Grey Fine Gray 45 42 45 51 MATER LEVEL 16 continued (continued) STATE OF ILLIMONS DEPARTMENT OF PUBLIC WORKS & BLDGS DIVISION OF HIGHWAYS POPLAR STREET BRIDGE APPROACHES TYPE FAILURE

B - BULGE

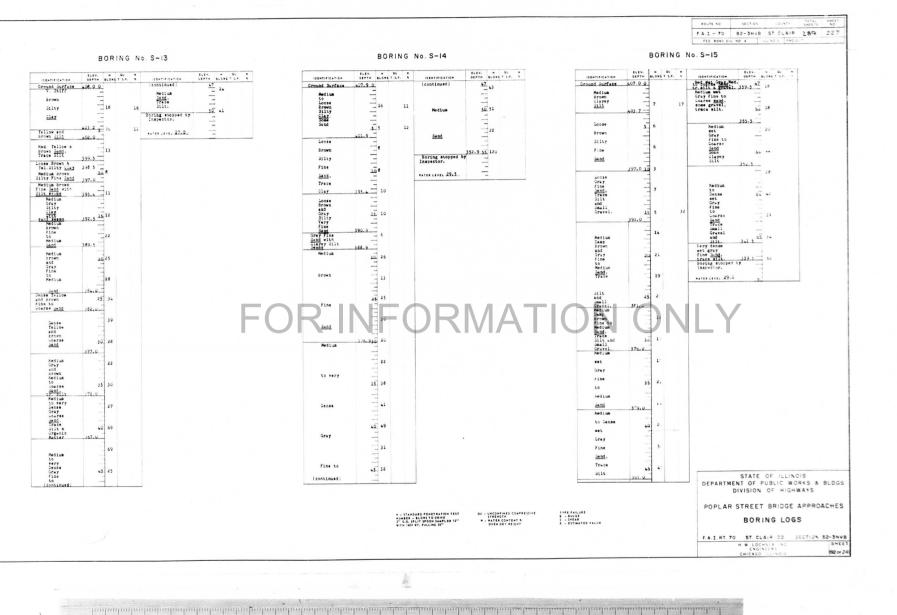
S - SHEAR

E - ESTIMATED VALUE QU - UNCONFINED COMPRISTRENGTH
W - WATER CONTENT %
OVEN DRY WEIGHT BORING LOGS FAIRT TO ST. CLAIR CO. SECTION 82-3HV9 \* W LOCHMER INC ENGINEERS CHICAGO ILLINGIS

F. A. I. - 70 82-3HVB ST. CLAIR 289 225 FED ROAD DIV. NO. 4 | ILLINOIS' PROJECT BORING No. S-4 BORING No. S-5 BORING No. S-6 ELEV. N QU V ELEV. N QU V ELEV. H QU ... IDENTIFICATION IDENTIFICATION IDENTIFICATION Ground Surface 412.6 0 (continued (continued) 1111111111 Medium Send to To hrown Medium 65 Cinders, 362.5 Sand Sand Medium Cinder Medium Miscellaneous Cinder F111 5546 F111 Stiff Brown Silty Clay 365.1 \_\_38 17 Dense Wet Gray Sand Some Gravel 401.6 Medium Yellow Brown Silty Glay Redium Brown Silty Clay Fine Sand Fill Fine to Stiff Yellow 7 1.225 21 F111 Sand Soft Dense to 15 WATER LEVEL 3700 Brown Very Medium To Gray 4 .655 Very Silty 65 60 Dark Silty Dense Clay Gray Clay 20 2 .485 42 Clayey Gray Gray Loose Gray Clayey Silt silt Fine Fine Sand. Trace 2 .578 29 To 20 23 Trace
Very
Fine
Sand
Joft
Gray
Silty
Ulay
Trace
Fine Sand
Medium Dry
Fine to
Medium Sand
Worker
Sand
Sand
Wellin Sand rine 71 Medius Moiat Brown Fine Sand. Trace Trace Silt, -nd Small 80 Brown 335.1 51 doring stopped by Inspector. Γo Medium Dry Gray Fine Sand and Silt Sand 44 380.1 11 WATER LEVEL 39.5 Loose to Very 35 18 15 12 ... Loose wet gray silt some fine sand, trace clay. Gray Send Dense Medium wet gray sandy silt Silt 40 30 Dense wet 38 Kedius to gray fine Dense 45 54 rine Set STATE OF ILLINOIS (continued Gray (continued) DEPARTMENT OF PUBLIC WORKS & BLDGS. DIVISION OF HIGHWAYS POPLAR STREET BRIDGE APPROACHES TYPE FAILURE B - MULGE S - SHEAR E - ESTIMATED VALUE BORING LOGS F.A.I.RT. 70 ST. CLAIR CO. SECTION 82-3HVB SHEET H. W. LOCHNER, INC. ENGINEERS CHICAGO, ILLINOIS

ROUTE NO. SECTION COUNTY SHEETS NO.

ROUTE NO. SECTION COUNTY SHEETS NO. F.A. I. - 70 82-3HVB ST. CLAIR 289 226 FED. ROAD DIV. NO. 4 | ILLINOIS | PROJECT BORING No. S-7 BORING No. S-8 BORING No. S-9 BLEV. H QU W BLEY. H QU V ELEV. H QU W ELEV. H QU W IDENTIFICATION Ground Surface
Stiff
Brown
Silty
Clay & Fill Ground Surface Ground Surface 47 29 t Small Gravel 147.2 47 24 Small Sand. Trace Brown Silty 3ma 11 50 50 38 Stiff Brown Silty Clay and Fine Sand Silty Gravel 50 48 Clay 1 5 Gravel Clay 7 6 with Brown Silty Sand To للللللله 387.4 V. Dense Miscella Very Dense det Gray Fine to Medium Sand, Trace Silt Wet Grey F111 Brown Medium Trace Medium Browsilty Clay Trace Fine Sand. Very 55. 83 Clayey Send, Fine 363 7 10 3 Trace Sand 84.7 10 8 \_ 32 Gravel 80.2 Dense to 72 Silty Sand 60 27 379.9 Moist 60 65 15 11 Medium Dense det Gray Fine to Medium Sand 15 21 V. Dense Moist 49 Medium 39 Gray Moist Gray Very Dense Wet Gray Fine Silty Sand, Trace Clay 115 Gray 177.2 18 65 34 65 Sand Fine to Medium to 20 22 Send, 323.7 71 Boring stopped by Inspector. Silt Fine Sand Dense Trace 17 Silt Boring stopped by Inspector. Boring stopped by Inspector. 324.770 Gray 25 30 brown WATER LEVEL 19.5 Fine & Gray Medium to 24 Sand Coarse Sand 30 15 164 7 10 46 Dense to Medium Gray Coarse Sand and Small Gravel Gray Nedium 17 - l11 62.2 16 Very Dense det Gray Sand Coarse Medium 25 7 Send, Trace Small 15 Gravel
Loose
met
Gray
Send,
Some
Fieces
of acod
and
Small
Gravel 157.2 8 154.9 Coarse 40 12 Gray Sand. Fine to 13 149.4 Gray 45 19 45 30 Fine to 45 17 Sand STATE OF ILLINOIS (continued) DEPARTMENT OF PUBLIC WORKS & BLDGS DIVISION OF HIGHWAYS POPLAR STREET BRIDGE APPROACHES QU - UNCONPINED COMPRESSIVE STRENGTH W - WATER CONTENT S OVEN DRY WEIGHT TYPE FAILURE
B - BULGE
S - SNEAR
E - ESTIMATED VALUE BORING LOGS F.A.I.RT. 70 ST. CLAIR CO. SECTION 82-3HVB H. W. LOCHNER, INC ENGINEERS CHICAGO, ILLINOIS SHEET



FA.I.-70 82-3HV8 ST CLAIR 289 228 BORING No. S-18 BORING No. S-17 BORING No. S-16 BLEV. H QU V #LEY. . D. . BLEV. H GU W ELEV. N QU V IDENTIFICATION IDENTIFICATION IDENTIFICATION IDENTIFICATION IDENTIFICATION Ground Surface 407.6 0
Stiff
Dark
Brown
Silty
Clay 32 Ground Surface 408.1 0 159.847 20 Ground Surface Loose Brown Silty (con'd) Silt. Trace
Silt

Medium Wet
Gray Fine to
Coarse Sand,
Trace Silt. Miscellaneous trace F111 Boring stopped by Inspector. 71 eilt. 50. 22 23 50 12 with Medius Medium 5 6 WATER LEVEL -1 to Silty 15 Clay Loose Loose Gray Damp 55 33 fine Henry Brown sand, Clayey 36 Silty Fine 10 6 concrete Silt Very Loose Damp Brown Send Trace Clay Fine limestone 60 35 Sand. fregments Trace Very Silt. Clay Dense 15 15 18 Coerse 24 Loose Brown silty sand Medium Damp Gray Sand, Some Silt 26 Grev Medium Sand, 65 30 Brown Coarse 20 22 Kedium 25 Fine 23 Send, to Send. Trace 27 Dense Gravel 32 Silt Fine 70 35 Damp trace drown 25. 31 25 38 25 21 silt. 36 Sand, Organic Trace Silt Medium dump to moist fine to course brown Sand, trace gravel and silt. V. Dense v. Dense
wat
Gray
Find
Medium
sat Gray
Fine
Fine
Sand
Trace
Sand
Trace
Small to
Medium
Heart
Hea Very dense wet Gray fine sand Boring stopped by Inspector. fine to 10. 35 30 22 10 17 8414 29.5 25 coarse 76.0 75.6 23 Medium set Gruy Fine to Course Sand, trace gravel and silt. trace silt. WATER LEVEL 31.0 Medium Met Gray Fine Sand, Trace Silt. 80 27 15 20 35 29 34.5 51 370.0 Medium to Dense det Gray Fine to Course Send, Trace Silt. 27 very WATER LEVEL 29.5 Medium to 40 42 Very Dense Gray gray 6 33 35 65 Fine fine Send, 45 68 45 10 45 70 Trace STATE OF ILLINOIS
DEPARTMENT OF PUBLIC WORKS & BLDGS. (continued) DIVISION OF HIGHWAYS POPLAR STREET BRIDGE APPROACHES M - STANDARD PENETRATION TEST HUMBER - BLOWS TO DRIVE 3" O.D. SPLIT SPOOM SAMPLER 12" WITH 140F WT. PALLING 30" BORING LOGS F.A.I.RT. 70 ST. CLAIR CO. SECTION 82-3HVB SHEET H W LOCHNER INC ENGINEERS CHICAGO, ILLINOIS 193 of 24

BORING No. S-19	BORING No. S-20	ROUTE NO   SECTION   COUNTY   STOCKE   SHEET   NO
	*	
Openinication		
	N - TRANSAR FRENT RATION TEST OF - SECRETARIS CONFRESIVE THE RATIO TEST OF THE RATIO	POPLAR STREET BRIDGE APPROACHES BORING LOGS
		F.A.I.RT. 70 ST. CLAIR CO. SECTION 82-34-VA H. M. LOGHNER IN. SHEET ENGINEERS CHICAGO ILLINOIS 1994-07241

2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 cc

FA 1 - 70 82-3HVB ST. CLAIR 289 230 3434 10. 75 1:::10 grave) trace silt. Grey coarse Pone Slay 60. 32 Casse to \_37 medius 65. 45 ETS. fine to 20. 27 STATE OF ILLINOIS DEPARTMENT OF PUBLIC WORKS & BLDGS DIVISION OF HIGHWAYS

BORING No. S-24 BORING No. S-22 BORING No. S-23 BLEV. H QU V #LEV. . 50 . IDENTIFICATION IDENTIFICATION Ground Surface a05.5 0

Kadium brown silty sols. 0

Brown clays silt, trabs 100.5 356.2 33 50 24 Ground Surface Ground Surface 405.7 0 Dense wet gray fine Sand, trace silt. Stiff fine to Brown coarse Silty Medium wet gray medium Sand, trace silt and gravel. Sand, Loose Clay trace Loose brown very fine Sand, some silt. Damp Brown 29 152.7 - 20 silt. Tery brown 7104 very fine Loose ome 11 55 22 3434 Brown 55 41 atltv gravel. Very Fine 10 20 silt. Sand. - 59 Very Medium 15.20 Dense 93.7 -Damp 60 62 moist Silt. dense brown Medium 15 19 gray Medium wet fine to fine Sand. 1.61.11.11.1 medium 3 48 trese salt. Sand, Boring stopped by inspector. fine fine trace brows silt. VATER LEVEL 29.5 Sand. fine to 15 medium \*\*\*\*\* 20.3 20 25 silt. 48 m4114 Sand, 337.7 Dense wet gray
fine to coarse
Sand, trace
sanil graval.
Boring,stopped by
Inspector. 23 brown 335.7. 70 43 25 22 25 25 18 Trace WATER LEVEL 32.0 fine to Silt. 373.7 Dense brown fine to coarse Sand, trace gravel & silt. 30 31 374.3 silt. 369.7 Kedium \_\_ 39 Medium. dense Medium wet gray 15 29 35 19 35 24 gray fine to 20 medium. fine to Sand.
Hedium
dense
wet
gray
fine to
coarse
Sand,
trace 23 medium Send. 40. 24 40 25 40 37 \_ 36 36 silt and Medium 45 . 27 45 37 Wet 45 23 gravel. Gray POPLAR STREET BRIDGE APPROACHES TYPE FAILURE B - BULGE S - SHEAR E - ESTIMATED YALUE BORING LOGS FAIRT TO ST. CLAIR CO SECTION 82-3HVB 195 or 24

F.A.I.- 70 82-3HVB ST. CLAIR 289 . 231 FED ROAD DIV NO 4 | ILLINOIS PROJEC BORING No. S-25 BORING No. S-26 BORING No. S-27 ELEV. H QU V ELEV. N QU W ELEV. H QU DEPTH BLOWS T'S.F. IDENTIFICATION

ISONAL | JOHN Ground Surface
Stiff
Brown
Clayey
Silt
trace
fine
sand. 47 23 Ground Surface 357.9 47 Ground Surface (continued) = 12 Medium moist Stiff brown Sandy Silty Clay Loose dans Loose damp
brown
very fine
Sand,
some
silt.
Loose damp
brown
very fine
Sand,
some 5 6 Loose to medium brown fine Sand, and Silt. 5 11 5 7 fine 38 398.9 Nedium scist brown very fine Send and Silt 12 55. 28 55 29 #11t 10 16 Medium damp brown fine to medium 1016 10 17 23 Medium Boring stopped by inspector. 17 trace silt. 392.9 Boring stopped by Inspector. WATER LEVEL 29.0 Nedium dann fine prown brown 15 16 trace MATER LEVEL 29.0 fine to 21 nectua fine 10 -15 Send. LTace. to gravel and silt. stit. 2011 20 17 Medium gray clayey Silt 20 10 383.9 nedius Redium damp yellow & brown fine to medium dams. Very dense moist 16 Sand Ary fine to med.

Send, trace silt

Medium
wet
gray
fine to
coarse
Sand,
trace
clayer
silt
sens. 340.3 333.9 trace silt. Nectual noist yellow brown line to commune wand, trace a.lt and gravel. 25 15 trace silt. Medium wet gray fine to medium Sand, trace silt and small gravel Medium Aprilia est sroy line to nectua mand. truce sitt wet gray fine to coarse bend 17 23 Send, trace gravel and silt. gravel and silt. read. Nedlus ett erey fine to 368.9 321.9 368.6 Medium wet gray course Sand, some gravel, trace silt. Medium to very dense wet gray fine to coarse 22 course send; trace gravel and silt. hery sense moist gray twey fine Sand. trace silt Medium 318.9 Hed ium 363.9\_ Sand, trace small to nedium gravel EFRY 15 27 fine to 90 27 ense wet gray fine to course Sand, trace small gravel. CONTRE 45 25 38 wet (continued) DEPARTMENT OF PUBLIC WORKS & BLDGS DIVISION OF HIGHWAYS gravel, POPLAR STREET BRIDGE APPROACHES QU - UNCONFINED COMPRESSIVE STRENGTH W - WATER CONTENT % OVEN DRY WEIGHT trace silt. BORING LOGS

> Boring stopped by Inspector.

3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 2

SECTION COUNTY TOTAL SHEET NO.

F. A. I. RT. 70 ST. CLAIR CO. SECTION 82-3HVB

SHEET 1960# 241

	BORING	No. S-31		BORI	NG No. S-32			BORING N	5. S-33	
#11F(C#1)G#	#LEV. # 90 *		ISENTIFICATION	ELEV. H C	OU T	1.17 Do	IDENTIFICATION	#LEY. # 80 *	GENTIFICATION	ELEY 00 -
	LOL. 5 0	continued) 32 20	Ground Surface 40 Loose moist	4.2 0	(continued)	<u>47</u> 2)	Ground Surface	404.60	(continued)	<u>*7</u> 16
Hedium damp brown very fine Sand, some silt.	=	tan 22	ailty Clay 40	2.2	fine to	3 1 1 1	Innacil	403.6		_
rown		_	ailty Clay 40:	2.2	Sand.	-	Medium brown silty clay	402.1 6 1,29 24	eilt.	149.6
ine		gravel. SG at	Loose	7	silt.	5 <u>0</u> 39		- 'a "		\$0 44
some		353.5 - -	Loose damp brown silty very fine Send 396	5 10	Gray fine Sand	333:3	Loose		Dense to very dense set gray fine to coarse Sand. Truce all and sell and	_
	199.5 5 13	747 = 34	Yery fine	5 10	21 Medium to	- 17		1 10	****	3.0
00.84 50		77 47 1104 5400	34nd 396	6.2	Medium to Dense wet gray fine to coarse Sand, trace small gravel and eilt.	=	prows		wet	
		17808	Loose	7	to coarse Sand,		1.542	∃,	fine to	4
		#:11. 349.5 55 a)	to	3.	gravel and	<u>sī</u> 36	****	4	Send.	54. 34
edium	Ξ	21514 est gray	medium.	-3	TAPE	344.2	,	3	ailt and	=
	9 -	find 10 — 11	damp	10 15	dense	= 57	fine	10 10	gravel.	58
42;	=	594784 5454	brown	-7	Fine	-		4		
0.05	∃.	Gray - 41 Constant - 41 Constant - 41 Constant - 41 Constant - 41 Constant - 41 Constant - 41	Y017	17	dense est gray fine Send, trace		Send.	- 1°		4
		477	fine	-3 "	Soring stopped by	144.2 6 <u>0</u> 63		-3	Borine stooms by	144.6 60 111
15 #5		graini. 343.5	Sand,	-3	Inspector.	-	10 Me	4	boring stopped by inspector.	
	13. 10		BOB6	15. 9	***** . **** 27.5			15 12	***** LT-91, 27.3	-
: 50		Secure	silt.	15 9			1116.		with their start.	
	∃.	_		∃。			Xedius	367.6		
		es: 6 <u>5</u> . 16						- 3,		
155,	4		36:				brown ailty Send,	-		
	20. 31	= 1.		20 24			Sand. VIII Moft	20 12 21		
	=		Medium	16		7	0147 ******	4		
• • • •	15	71ne 10	brown	∃,,			Medium damp yells t brown fine to	11 20		
		.201 35	fine to	3.0			t brown fine to	181.1		
		1 4					Medium Medium vellow &			
111.	25 19	##51 UM	aediua .	25. 20			yellow a brown fine	25 20		_
		14.2.	3m.	1.		$\Gamma \Lambda \Lambda \Box$		, A		
	15		uria (	19	-( )	11/1/41			II Y	
	276.5	25 **	ilit.	25.2			#115# Course Mand #157 Amil grows		-	
	-	17111	Kedium 37				-	109.0		
411.48	30 10	57	wet	30 20				10 21		
		126.0 14	gray				Xed1um	4		
	19	soring stopped by	fine	16				- 20		
47.84			to				**:	-		
4:		6-0-11-0	coarse	-				-		
	35 34		Sand	35 22			fine to	15 20		
rey			Medium	8.2				-		
154 10	- 28		fine to	22			104794	- 20		
			trace Lignite	55.2			97.7			
4784			Grey fine to	40 28			34.05 ·	크		,
end .	40 39		Gray fine to coarse Sand, trace small gravel & silt. 16					40 22		(
			Very dense	23.2			trace	-		
• 0 •	31		fine a medium	63				-30		
::			_ 3aod, trace milt. 36	-			small	=		
	1		Medium	45 18				4		
1.6	45 10		to dense	45 18			grevel	45 22	_	
stinued)			gray (continued)				(continued)		DEPARTMENT	TATE OF ILLINOIS OF PUBLIC WORKS & BLDG
									DIV	ISION OF HIGHWAYS
					H - STANDARD PENETRATION TEST		TYPE FAILURE		POPLAR ST	REET BRIDGE APPROACHE
					HUMBER - BLOWS TO DRIVE 2" O.B. SPLIT SPOON SAMPLER 12" WITH 1467 WT. FALLING 36"	DU - UMCOMPINED COMPRESSIVE STREMETH T - MATER COMPENT & OVER DRY WEIGHT	TYPE FAILURE B - BUIGE S - BREAR E - ESTIMATED VALUE			BORING LOGS
									FA 1 RT 70	ST CLAIR CO SECTION 82-3H
										W LOCHNER INC SHI
										NICAGO ILLINOIS 1970

Particular de la facta de de la facta de l

				ROUTE NO.	SECTI	ON	COUNTY	SHEETS	SHEET
				F. A. I 70	82-3H		ST. CLAIR	289	233
				FED ROAD DI			LINOIS PROJ	CT	
			G	No. S-36					
EV.	BLOWS	QU T/3.F.	:	IDENTIFICATION		N LOWS	QU		
0 0				Medium	47	16			
.0				to	-				
=	10	2.4EP	23	dense	50	12			
5				wet	54	**			
_	11			gray	_				
5_	"			fine to		30			
.5	1			coarse	=				
-	8			Sand	55	29			
-	1			trage	-				
,:	10			smell	-				
10				gravel	-	33			
-	-			and	-				
-	5			silt.	60	32			
-	-				344.0 -				
15	10				-				
-				Very	-	121			
.5	-			dense	-				
	32			gray	65	80			
.0				fine silty	-				
20	8			silty		62			
-	1				_	04	2		
-	١								
_	17				70	14			
-	1			Sand	1 -	1			
2.	12			×	332.5	60			
-	7			Boring stopped b	у				
8.0	18	1	III.	VATER LEVEL 29.0		_			
6.5	Н		117						
- 4	H	v							
3	32			4					
-	-								
-	22								
-	5 29								
-	-								
1	5 29								
-									
	17								
-	١,.								
4	0 17								
7	-								
	21								
2.0	7								
4	5 33								

BORING No. S-34 IDENTIFICATION

BLEV. N QU V 47 24 50 45 Ground Surface 404.6 0 Medium Stiff 14 1,55 15 silty 400.6 clay dense Loose damp brown silt Medium brown sandy Silt, trace clay 399.1 5 9 38 gray 95.6 10 fine to 55 31 course 10 7 Sand, 29 Loose to medium damp silty very fine brown send. trace small gravel 15 11 37 388.6 and Silty Clay with fine sand. - 9 1.hz 33 Boring stopped by Inspector. 99 385.6 VATER LEVEL 29.0 Very dense to medium damp brown

26

15

25 27

369.1 36

365.6

163.6

361.6

158.6

378.6

very

fine
Sand.
Loose
brown
x gray
medium to
coarse
truce
gravel
and
silt.

dense wet gray fine to coarse Sand, truce small gravel and silt.

wed silt.

Dense
wet gray
fine to
medium
trice
trice
ingray course
sand, truce

BORING No. S-35

BLEV. H QU T IDENTIFICATION 57 30 356.0 30 50 29 Ground Surface 404.50 (continued) and alt. Marian was gray fine to coerse fand and sea silling, 0 and to coerse fand and sea silling, 0 and to coerse fand and to coerse f Medium damp brown Silt, trace clay some very fine sand. 2,1E 23 398,5 damp yellow & brown very fine WATER LEVEL 28.5 Sand, trace

88.5

385.5

20

35 37

31

17

45 18

15

Medium moist brown fine Sand, trace silt.

trace

Dense wet gray fine Sand, trace silt.

Medium wet gray coarse Sand. trace small gravel

25 22 silt. Medium dense gray medium Sand, trace silt. Medium dense wet gray fine to coarse Sand, trace small gravel and silt.

0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24

QU - UNCONFINED COMPRESSIVE STRENGTH W - WATER CONTENT % OVEN DRY WEIGHT

TYPE FAILURE

B - BULGE

S - SHEAR

E - ESTIMATED VALUE

Ground Surface

topsoil stiff brown clayey Silt.

Medium dry yellow and brown silty fine Sand

yellow &

fine

Sand

Medium

Sand,

wet fine to

course gray

Sand,

trace

gravel and

silt.

Dense wet gray fine Sand, trace silt.

milt. 378.0

Hed.molst Br.fine to
co.Sand & milgravel,
tr.silt(5\*seam chart)76.5
red wood & debrie)

yellow & brown fine

DIVISION OF HIGHWAYS

POPLAR STREET BRIDGE APPROACHES BORING LOGS

F.A.I.RT. 70 ST. CLAIR CO. SECTION 82-3HVB H. W. LOCHNER. INC. ENGINEERS CHICAGO. ILLINOIS

F.A.I.- 70 82-3HVB ST. CLAIR 289 234 FED. ROAD DIV. NO. 4 ILLINOIS PROJECT BORING No. S-37 BORING No. S-38 BORING No. S-39 ELEV. 4 GU \* BLEV. H QU W ELEN. . . . . . . ELEY. H QU W BLEV. H QU W SE-1 F C+1 S+ IDENTIFICATION IDENTIFICATION Ground Surface 405.0 0 (continued) 47 22 419.40 Ground Surface 419.1 0 47 20 (continued) to trace small gravel and silt. 5 11 12 19 9 Ξ, Cinders, 50 28 Loose Camp brown silty very fine wet 50 27 bricks. 57 cinders, gray dense Dense fine congrete, 5 12 7411-2 wet gray concrete 38 28 .... fine to silt & COAFSE /4115w secius and mincellaneous 55 47 455 55 48 55 34 gray Sand, trace f111. 10 6 trace miscellaneous Loose to medium yellow brown clayey Silt. trace fine sand. 1114 silt. - 41 gravel \_30 1111 424 347.0 F111, 12 ..... Kedium 60 29 1.... trace 358.4 Doose feed brown fine Send; brack sint wet coarse Medium wet gray coarse <u>Sand</u>, some clayey silt with small gravel. 15 9 15 3 26 25 grav sand. 10 Brown Sand. 7411.2 1.25 (747.1 11141 11141 11141 11141 silty very 10 Clay. 65 60 05 19 65 22 fine fine Send, 20 5 20 5 29 Trans. send. to trace King a version 397.6 medium 12 Medium silt. scring stopped by inspector. 335.020 53 vellow 20 46 and 25 11 45 15 brown 25 16 \*\*\*\*\* . EVEL \_28.5 yellow and fine 10 Sand. 3441 75 44 Very dense wet gray fine fine 30 5 30 18 Silt. Sand, WATER LEVEL 41.8 trace 44 Loose silty Sand. 23 milt. to 119.4 62 49 Boring stopped by Inspector. 545; at dense 384.8 Dense yellow and brown fine Sand. 15 7 very 382.6 Dense yellow a brown fine Sand, trace silt with organic matter seams. 1.54 fine 49 44.75 Sand, 25424 trace silt. 3 (5 . 44 0 1 ) 40 32 378.4 3 27.3 ... Medium wet brown 39 15.7 coarse Sand, trace small gravel asilt. 373.9 45.51 \*\*\*\*\* -5 18 3742 45 32 Medium 2.55 Medium (continued) STATE OF ILLINOIS (continued) DEPARTMENT OF PUBLIC WORKS & BLDGS DIVISION OF HIGHWAYS POPLAR STREET BRIDGE APPROACHES TYPE FAILURE B - BULGE S - SHEAR E - ESTIMATED VALUE H - STANDARD PENETRATION TEST HUMBER - BLOWS TO DRIVE 2" O.D. SPLIT SPOON SAMPLER 12" WITH 1808 WT. FALLING 30" QU - UNCONFINED COMPS STRENGTH \* - NATER CONTENT S GNEW 281 MEGAT BORING LOGS F.A.I.RT. 70 ST. CLAIR CO. SECTION 82-3HVB H. W LOCHNER INC. ENGINEERS CHICAGO ILLINOIS

0 1 2 3 4 5 6 7 8 9 10 13 12 13 14 15 16 17 18 19 20 21 22 23 24

SECTION COUNTY TOTAL SHEET NO.

	BORING N	lo. S-40				BORI	NG No. S-41				BORIA	G No.	S-42		
	BLEV. H QU W		ELEV. H QU W	Г		ELEY. H QU DEPTH BLOWS T/S.		ELEY 50 .		IDENTIFICATION	#LE+ 00 00075 8L0957 L	. :	SENTIFICATION	ELEV D	
ntification		(continued)	47		Ground Surface	415.4 0 -	(continued)			round Surface	419.0 0		(continued)	52 ()	
		fine to medium	34		Black		trace	<u>-</u> 29			=		Sand.	= "	
		Sand, trace silt &			cinders,	7,	smell			Cinders.	= ,		trace	_	
Cinders.	∃′	gravel.	369.5 50 35		clayey	1 -1 1	grevel	<u>50</u> 51		Silt.	= -		small	دد قع	
bricks,		Medium to	1 4 1		eilt, &	1 3.1	and	-			<u></u> 13		gravel	-	
DITCES!	5 14	to dense wet	23		miscellaneous	5 6	silt.	- 15		Gypsus ,	-	4.0	d silt.	= 25	
Stone,	14	gray fine	3		<u>F111</u> .			361.9		limestone,	Ξ.			365.5	
	14	to coarse	J.,		medium loose	10 9	Medium	<u>5</u> € 17		silt, and	_ 1.			32 32	
silt and	1 3 1 1	Send, some small	55 21		loose brown fine Sand, with	F	wet	= .,							
	10 10	gravel, trace	1 7 1 1		with	10 9	gray	-		miscellaneo	us		Dense	3	
miscellaneou	• =	silt.	32		clayey	E 4.004	fine to	= 17		7111 coose moist rellow and	408.0		Wet EFAT	∃"	
	9 18	Dense wet gray f	361.0 T	L		403.4	coarse		1,3	rellow and	∃ 10		fine	4	
111.	406.5 - 9 18	Dense wet gray f Sand, trace sile Gray coarse sand	t.359.7 60 32		Medium	10	Sand.	6Q. 28	fi	ne Sand		16	to	6€ 16	
dium ist llow d own ne lty, ayey nd	= = = = = = = = = = = = = = = = = = = =	Gray coarse sand w/sml.gravel,tr.	01336.5			三	small		-		405.0		CO4780	=	
104	15 13 24	gray fine			damp	15 19	gravel,				15 +	*2	Send.	- is	
	4	Sand, trace silt.	356.0			3		351.9					8084	3	
e y	LO1.5 = 8	Medius				15	gray fine Sand,			Brown	= ,	37	11	55 2.	
	401.5	to	65 23		yellow	3 1	trace silt.  Very dense wet gray fine Sand, trace silt.  Boring stopped t Inspector.	359-4-65 61		silty			gravel.	52 **	
n y		dense				-	VATER LEVEL 38.5			81109	3	36	trace		
y	20 4 .81-5 37	wet	34		and	20 27	WATER LEVEL JOIN			clay	20 10 398.0	E 2.7	silt.	251 5 7 15	
		gray	1 7 1			1 1				Loose to medium	-	Ins	pector.	3	
	7 30	fine to	20 56		brown	24				medium yellow		21	to Level 41.0		
Send	396.0		74 16			= -				end	=				
st	23 31 .9.	coarse			fine	25 19				fine silty Sand. ose Woist by fine lty Sand.	₹5. 12			_	
ist llow d		Send,	88		rige			$\Lambda$	-	Sand.	393.0				
own ne	17	with	=	- ( )	K	a -	+( )  -	$< 1 \setminus / \mid \triangle $	gr al	by fine	F.		1	Y	
nd. ace lt.	-: 1/	small.	75. 41		Send,				tr		311.0				
	190.5	gravel, trace				1 - 3 - 1				Kedius					
itum	١٤ ايو	silt.	342.0 50		trace	30 30				to	15. 18				
dense		poring stopped by	,						1	dense demp					
st	- 38	WATER LEVEL 41.0				33				yellow	1.				
llow					eilt.	-				and					
orown ne	35 28					35 30				brown	25 3-				
ie id,	33 40					179.4				fine					
h					Medium moist gra	378.4 28				silty	·				
t.	36					28				Send.	381.0				
	561.0				Medium	-				Dense					
brown d, trace enic oted.	40 21				wet	40 24					40. 5G				
oted.	378.5				gray					fine to moist Sand.					
et	30					26				dend, trace silt.	38				
brown coarse					fine to				-		376.0				
wce wel	.2. 2				medium	1 3				Dense wet					
180	274.7 45 14					45 30				fine to	45. 48			STATE OF ILLINOIS	
y nued)				L	(continued)					(continued)			DEPARTM	ENT OF PUBLIC WORK DIVISION OF HIGHWA	KS &
							- STANDARD PENETRATION TEST	S L-COMPRESS COMPRESS	TYPE FAILURE B - BULGE				POPLAR	STREET BRIDGE AF	PRO
							I - STANDARD PEMETRATION TEST UMBER - BLOWS TO DRIVE " O.D. SPLIT SPOON SAMPLER 12" ITM 1405 WT. PALLING 30"	o peccentues competes interests * * * * * * * * * * * * * * * * * * *	B - BULGE 5 - IMEAR E - ESTIMATE	D VALUE				BORING LOGS	
						774							F. A. I. RT. 7	O STICLARICO SEC	TION
														H W LOCHNER HS ENGINEERS CHICAGO L. NS S	
														CHICAGO 45 5	

2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 63

ROUTE NO. SECTION COUNTY SHEETS NO. F.A. I. - 70 82-3HVB ST. CLAIR 289 236 FED. ROAD DIV. NO. 4 ILLINOIS PROJECT BORING No. S-43 BORING No. S-44 BORING No.S-45 ELEN. . 30 . ELEY. H QU Y DEPTH BLOWS T/S.F. % ELEV. H QU W BLEN. N BL W GENTIFICATIO INTERTIFICATION 56 - 34 - 60 43 224.0.0 \$7 16 50 29 Ground Surface BDack = 2 wet gray Sand. cipathors. Very trace and 50 27 fire to course SCHOOL STREET loose ----11 silt. Sand, trace gravel, 5 7 5 9 MUZZ. black 32 Medium wet gray fine to coarse Send, some small \_20 trece small gravel \_\_ n cinders, silt. adjace-Character and milt. 2122 55 25 eilt. 35.2 55.42 boring stopped by 65, 30 brick 35 5 10 2 \*\*\*\*\* LEVEL 39. \_\_ 68 Medius fragments. Denne 60 31 & F111. wet Time Sunt. 20 46 ..... 35 · 15 5 27900 NG 32. .9E 30 gray ="" Sand. 14 SHE'S fine Medium 1740 352.8 65 52 V.dense V.dense wet gray fine to medium Sand. trace damp Sand. 75 43 1 20 5 .52 23 20 11 yellow truce **STATE** 29 349.3 355.8 silt. Mexico the second secon and 337.9 80 8 Gray clayey Silt. brown 25 14 32 BUTTONE 32 sand 335.4 very Summer Streets Streets Medium fine 85 26 34 38 30 15 fine Sand, \*\*\*\*\* LEVEL 41.0 Sand, trace 22 - 28 23 silt. 328.4 1964. 4 90 64 silt. Dense to 35 31 Sec. 26. 35 22 very dense Modern Street St wet gray 19 fine to 384.4 Brown 95 45 COAFSE 378.0 27 fine to 40 13 Sand, medium Some - 55 Sand, small 12 374.9 24 gravel. Boring stopped by Inspector. 334\_ Hedium 45 28 45 18 WATER LEVEL 42.0 dense STATE OF ILLINOIS 35 50 26 DEPARTMENT OF PUBLIC WORKS & BLDGS wet DIVISION OF HIGHWAYS POPLAR STREET BRIDGE APPROACHES gray

TYPE FAILURE

B - BULGE

S - SHEAR

E - ESTIMATED VALUE

39

fine to

medium

BORING LOGS

F.A.I.RT. 70 ST. CLAIR CO. SECTION 82-3HVB

SHEET

H. W. LOCHNER. INC. ENGINEERS CHICAGO. ILLINOIS

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#001E NO SECTION COUNTY TOTAL SMEET
#001E NO SECTION COUNTY TOTAL SMEET
#0 FA I - 70 82 - 3 M/48 ST CLAIR 285 237
#00 KOND DIV NO A | LUMBON SMEARS

BORING No. S-46

BORING No. S-47

BORING No. S-48

DENTIFICATION	ELEV. N QU DEPTH BLOWS T S.F.		FICATION	DEPTH BLOWS T 3.1			IDENTIFICATION	DEPTH BLOWS TISSE.		51874 BLOWS 7 5.8. 5		IDENTIFICATION	DEPTH BLOW	1 5.7.	IDENTIFICATION	25 PT - 8L245 T SA. 4	
ound surface	417.3 0	(cont	inued)	269 3 29		-	Ground Surface	<b>417.2</b> 0	(continued)	±7 _ 47		Ground Surface	417.2 0		Dense	<u>47</u> 31	
Loose to	4	De	nse	369.3			Charcosl,		grey	=		Black,	-		coarse Sand		
very	= ,		t eray	1 4			Black	<u> </u>	67			Cinder,	=,		small gravel	68.2	
loose		Sa	ne nd.	50 37			Cinters, &		fine	52 49		Brick.	= -	i	Dease	20 31	
black	4		11	366.3	- 1		Miscellaneou	•				Coal,			Erey		
cinders,	5 7	No.	dium	38	1.1		F111	11. 7 5 10	to			and	5 5		fine		
red		we	t				Loose		coarse	- "					Sand, truce silt.		
brick.	3	gr	ay	3			demp yellow &					Miscellaneous	-	-	ense wet gray med.	05.2	
Coal,	2	fi	ne	55 33			fine Sand,	- 7	Send.	S\$ 30		Fill. Medium	409.2	1 5	o coarse Sant.tr. ml.gvl.aOrg.mat.	63-755 32	
and	=	to					trace silt.	408.2	trace	=		damp red and		-	ar.ger.aurg.auc.	_	
Sand	10 2	co	arse	- 1			Medium	10 12		-		brown	106 7 10 17	26			
	406.3		nd.	19			damp		small	= 19		silty Clay Very loose	106.7		gray fine	_ 23	
n Silt. some	-	30		3			yellow x	-	gravel	3		& brown	- ∃,		to	=	
fine Sand.	404.3 - 2		all	60,25			brown	∃.	29	<u>50</u> 28		Silt,	e 3		Sand, trace	62.31	
Loose			avel,	3			fine		and	=		wand.	L03.2 -		small		
to	77.		ace	-			Sand,	15 12	29 silt.	-		Loose to	15 6		small gravel and silt.	-	
medium	15 6		15.	354.3			some.	_	Boring stopped t	250.7 = 19		medium	Ë		silt.	- 22	
damp	7	Ye.	dium.				silt.	400.2	inspector.	-		damp	-				
	11	fin	t gray	65 18		-	*110.	- 8	PATER LEVEL \$1.0			yellow &	- 6		3	52.2 <sub>65</sub> 18	
yellow			rse <u>Sand</u> ,					-				brown	7	T.	Boring stopped by		
and			ll gravel.	,,				1 7				Y0.77	201.0			7	
brown	20 6	1	nse	29			Medium	20 10				fine	20 9		MATER LEVEL 41.0	=	
very	- 1		t gray										7				-
fine	10	1	ne to				to	1e				Sand,	14				
Sand,	3		arse	70,48				∃."									
trace			and									and	25 16				
silt.	25 16		race	87			dense	25 15				silt.	-				
te molet	391.3		mall								T-1/	Loose	191.2			7	
low & brown t, some y fine Sand.	- 6	30 8	ravel.			( )	yellow	16		' I\ /I /\	1 1/	irace clay.	189.2 9				
fine Sand.	3*9.3	boring	stopped by	342.3 75 34				A			1 1/	trace clay.	709.2	/   "U			
Medium		Inspec	tor.				and			v . /		Pedium	27.1				
damp	10. 20	FATER L	EVEL 41.0					30 17				yellow	10. 19				
yellow							brown	=					=				
and	16						010411	- 25				fine Sand. trace	14				
brown	-10						fine					trace					
							line					Very	383.2				
fine	35 16						04	15. 24				dense	35 95				
Sand,							Sand,					fine					
trace								Ξ.,				Send, truce	- 74				
silt.	- "	İ				1	trace	33					379.2				
a dama	378.3											Dense, damp gray fine to coarse Sand, trace small	-				
fine to m Sand, silt.	40 9						silt.	40 41				trace small					
sIlt.	376.3											Medium	376.2				
								376.2				wet gray	- 22				
to coarse trace small l and silt.	374.3											fine Sand, trace allt.	374.2				
							Medium	1 1				gray fine	1 4				
fine to	45 23						dense	45. 23				Send, trace	45 40				
fine to m Sand.								-				Sand, trace small gravel and silt.	171.2			STATE OF ILLI	
ntinued)						L	wet (continue	4								NT OF PUBLIC W	
																IVISION OF HIG	HWAYS .
								w - 57	HOARD PEHETRATION TEST		(200	***			POPLAR	STREET BRIDGE	APPROAC
								2" 0.0 WITH 14	R - BLOWS TO DRIVE SPLIT SPOOM SAMPLER 12" 105 WT. FALLING 30"	DU - UNCOMPINED COMPRESSIV STRENGTH V - VATER CONTENT N DVEN DRY MEIGHT	1 - 1014	TED VALUE				BORING LO	GS
															F.A. I. RT. 70		SECTION 82-
																H W LECHNER INC ENGINEERS	
																ENGINEERS	b

F.A.I. - 70 82-3HVB ST. CLAIR 289 238 FED ROAD DIV. NO. 4 | ILLINOIS | PROJECT BORING No. S-51 BORING No. S-49 BORING No. S-50 ELEV. H QU V ELEV. H QU W ELEV. H QU W ELEY. H QU W BLOWS T/S.F. N IDENTIFICATION IDENTIFICATION. 57.6 - 44 IDENTIFICATION IDENTIFICATION (continued) 47 23 round Surface 407.5 0 50 79 Ground Surface Ground Surface
Loose brown
silty
clay
little 407.0 0 5 11 Topsoil trace Topsoil COATES 50 104 5 6 atlt. clayey dry dense wet gray fine Silt 5 yellow 352.6 38 gray fine fine
Sand.
Dense wet
gray fine
to coarse
Sand, trace
black organic
matter. brown Medium damp yellow and brown very fine Sand, trace silt. Dense
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ve very coarse Sand, trace small gravel. medius fine 55 36 49.6 Sand, 10 8 Medium 10 7 trace 347.6 = 16 sitt. 199.0 |
Di. rery k br. Clayy |
Di. rery k br. Clayy |
Di. rery k br. Clayy |
Di. rery k br. Clayy |
Di. rery k br. Clay |
Di. .... Dense, wet gray fine to medium Sand, trace 60,43 15 60 24 345.6 60 26 fine Gray Sand. 346.0 silty sand. dense wet gray fine to medium Sand, trace small gravel. WATER LEVEL 27.3 15 11 - 83 damp yellow & brown fine sand. Medium moist gray silty v.f. Sand. 390.5 187.6 - 16 Medium 65 33 Boring stopped by Inspector. damp Medium damp yellow and brown very fine silty yellow 6 Medium demp yellow end brown very fine (continued) Boring stopped by 339.5 48 20 20 WATER LEVEL 30.0 brown fine MATER LEVEL 31.0 Sand, 23 12 382.1 Sand. trace 25 20 25 35 25 27 Loose moist dark gray very fine Sand. 381.5 Madium wet gray very fine Sand, trace Bilt. 379.5 fine 30 16 30 12 Medium 376.0 Sand. Medium Medium to 16 gray dense fine to 35 17 35 22 gray wet - 26 18 10 fine to -to dense 40 40 40 25 Sand. fine 36 39 Dense wet gray fine Sand, truce silt. fine to coarse to 45 31 STATE OF ILLINOIS [continued] DEPARTMENT OF PUBLIC WORKS & BLDGS DIVISION OF HIGHWAYS POPLAR STREET BRIDGE APPROACHES QU - UNCOMPINED COMPRESSIVE STRENGTH W - WATER CONTENT % OVEN DRY WEIGHT TYPE FAILURE
B - BULGE
S - SHEAR
E - ESTIMATED VALUE BORING LOGS F.A.I.RT. 70 ST. CLAIR CO. SECTION 82-3HVB SHEET H. W. LOCHNER, INC.

ROUTE NO. SECTION COUNTY TOTAL SHEET NO.

203or241

CHICAGO ILLINOIS

COUNTY TOTAL SHEET NO. F.A. I. - 70 82-3HVB ST. CLAIR 289 239 FED. ROAD DIV. NO. 4 | ILLINOIS | PROJEC BORING No. S-56 BORING No. S-57 BORING No. S-55 ELEY. H QU V BLEV. H QU V \*\*\*\* # 60 . IDENTIFICATION IDENTIFICATION IDENTIFICATION (comt'd) tr.silt. 360.8 47 Ground Surface
Brown
clayey
Silt. 407.0 0 47 45 wet Ground Surface 405.9 0 .04.0 Topsoil
Loose damp yelabra.
v.f. Sand, clay, some G2.9 fine some very fine Sand. Loose dry yellow & brown very fine Sand, trace silt. - 32 wet 50. 18 50 17 gray 5 6 medius fine 353.9 24 Sand. 147.0 60 21 damo Medium to dense wet gray fine to coarse land, trace 50 to 01.0 yellow temp yellow and temp temp Com lend, sine still. Loose COATS 108 brown Sand . 22 - 6 tani gravel 55. 25 very fine 350.955 44 brown Decade wet gray fine Dand, trace Sand. fine very 142.5 30 a Grey medium to coarse Sand, some small grave) Sand - 35 fine Medium 80ae Sendy Silt. 345.960 45 60 22 very Brown dense fine Medium 5747 1154 15 11 Frey 20 25 15 9 Sand 37 to coarse land trace small gravel trace wet gray very fine fine silt. 23 Sand, 65 42 65 40 coarse Sand, trace ---20 11 silt. Send. 75 68 186.9 20 5 small Sortagitopped by 338.4 29 31 20 331.0 dense Hedium wet gray fine gravel, some coarse sand, trace silt. desc \*\*\*\*\* . t \* t. \_ 31.0 20 39 Silty 25 7 grey 80 22 25 5 25 30 fine Send. -31 Medium 23 trace wet silt 375.9 30 34 35, 27 MATER LEVEL \_12\_ 85 20 grav gray Medium fine to coarse 30 32 Sand, dense some 90 25 27 trace smell. ... 15 15 silt 370,5
Loose v.est gray v.f.
sand, little silt.tr.
yood a light e j09.0
Refine wat
gray fine
to medium
Send, trace 40
gravel. j06.0 gravel, gray Dense wet gray fine to medium Sand, 15.0 - 22 some small gravel, trace silt. to 17 40 18 40 17 312.0 COATSE Boring stopped by Inspector. 15 21 Sand . WATER LEVEL 30.5 LF+C+ 45 38 3. 45 47 STATE OF ILLINOIS DEPARTMENT OF PUBLIC WORKS & BLDGS. DIVISION OF HIGHWAYS Sand. 50 35 trace POPLAR STREET BRIDGE APPROACHES TYPE FAILURE B - BULGE 5 - SHEAR E - ESTIMATED VALUE DU - UNCONFINED COMPRESSIVE STRENGTH W - WATER CONTENT % DVEN DRY WESCHT silt BORING LOGS 20 F.A.I.RT. 70 ST. CLAIR CO. SECTION 82-3HVB H. W LOCHNER, INC. ENGINEERS CHICAGO, ILLINOIS SHEET

		5 NO	SECTION	COUNTY	1-11-1	NO	
F	4 :	- 70	82-3HVB	ST CLAIR	287	240	
	11:	9545 SI	NO 4	LL 14015   **515	61		

## BORING No. S-58

IDENTIFICATION	ELEY. DEPTH	BLOWS	QU T/3.F.	:	IDENTIFICATION	ELEV. DEPTH		QU T/LF.	:
Ground Surface	406.9 0				(continued) Sand, trace	47	26		
damp yellow	-				pilt.	358.4	1		
SINE"	403.9	8		20	gray fine to coarse Sand,	50	43		
silty Clay	602.6			1	gravel & silt.	55.9			
Loose dry yellow and brown fine Sand, trace silt.	400.9	8		17	Dense wet	-	67		
Sand, trace sitt.	400.9				gray fine Sand,	1 3			
Loose yellow		5		30	trace silt.	5.5	43		
end brown	-				Med.wet gray fine	350.9	7		
Silt. trace fine	10	9			coarse Sand, tr. sm		28		
sand.	395.4				Boring stopped by	ted -			l
Loose wet bross	-	5		34	Inspector.	60	=		
silty clay	392.9				WATER LEVEL 31.0	61	4		
Nedium loose	15	12							
yellow and		-							
brown wery fine Sand.	1 -	18							
some	388.4	i°.							
V-00-2-02	-	1							

Loose

very fine

Sand,

silt.

gray

fine

trace

silt

and

Medium wet gray fine Sand, trace will and small grays).

Medium wet gray fine Sand, trace silt.

Medium wet gray medium

Shell gravel, 373,4 Med. wet gray fine to course send, trace small gravel 15 2" charred coal.

25 9

10 29

360.9

## BORING No. S-59

IDENTIFICATION	ELEV. DEPTH	BLOWS	QU T/S.F.	:	IDENTIFICATION	ELEV. DEPTH	SLOWS 1	1/1.7.
Ground Surface	405.9 0				(continued)	47	24	
Loose damp	-	1			trace		24	
yellow &	_	1				357.9	4 1	
brown silty	1	1			Dense	-	4 1	
sand, trace	_	1			gray	-	4	
clay.	402.9 -	7			coarse	10	34	
Loose	1.02.9				Sand,	20		
damp	1 -	4			800.0	1 -	1	
yellow t	_	1			smell			
brown		1 5			gravel.	1 .	7 1	
silty	2.	1 2			trace	1	13u	
Sand.	399.9	1			silt.			
		1				352.4	-	
Loose					V.Dense wet gray fine to medium Sa trace silt.	J	4	
to		7			fine to medium 34	Tin our	54	
to	_	-			Boring stopped by	370.755	- >•	
medius	-	+			inspector.	4	-	
	-	4			Inspector	-		
wet	10	7		37	WATER LEVEL 29.0	1 -	3 1	
brown	1	7			7	_	_	
and		i i						
		3			1			
gray		] ^			l .			
		4			I			
clay.		4						
CIOY.	391.4	4		29	ı			
Medium	15	12		29	I			
fine brown	1.	1			I			
Sand,	-	+			!			
	1	1			1			
some	1	1 16						
silt.		1 10			I			
		1			I			
Fedium	386.9	4			1			
gray fine	1	1			1			
Sand,	20	15	1		1			
some silt.	984.9	1						
Gray	104.7	1		į.	i			
very fine		1			1			
Sand,		1 12			1			
trace		1 "		1				
	201 0	1		1	i			

## BORING No. S-6

IDENTIFICATION	BLEY. DEPTH	8L045	90	;	istatificatioa	ELEV. N 25 DEPTH BLOWS T L.F.
Ground Surface	409.5 0			-	(continue)	
Topsoil.	-					<u>\$7</u> 31
lopsoil.	408.0					=
Loose	_	7			114734	<u>50</u> 34
damp yellow						
and brown	_					
sand v	5	9		17	1401	= 45
Silt.	-					_
	403.0					_=
Stiff brown		9 1	.8 6	24	27424	45.34
little very	400.5	- 1				\$ <del>\$</del> 34
Stiff brown silty Clay, little very fine Sand. Loose						-
	10	8 2			11.11.	352.0 = 44
yellow	_	- 1			Boring Stopped by Inspector.	_
	_	١. ١				
and	-	,		27	**************************************	ಕ್ಷದ
brown		1				
	17	9				
very	-	1				
**	-	5				
fine	-	10				
Sand,	-					
		1				
trace		4				
	_	-				
silt.	387.5					
Loose		10				
		-				
to	23	7				
dense	_ 3					
gray	-			k I		
	9	-188		١I		V
fine				//		
		3/4				
Sand.	N 3			'	N L	
Send. trace	2	.9			AL	
Sand.	N 3	.9			N L	I
Send. trace	- 2i	.9			NL.	I
Send. trace	2	.9			NL.	I
Send. trace	- 2i	.9			NL.	I
Send. trace	377.0	32			NL.	I
Sand, trace sit.	377.0	.9				I
Send. trace	377.0	32			N L	I
Sand, trace sit.	377.9	32			INL	I
Sand, trace sit.	377.9	32			INL	I
Send. trace silt. Medium	377.9	32			INL	I
Sand, trace sit.	377.0 = 3177.0 = -	32			NL	I
Send. trace silt. Medium	377.0 = 3177.0 = -	32				I
Send. trace silt. Medium	377.0 = 3177.0 = -	32 35 20 28			NL	I
Sends trace slit Medium	377.0 = 3177.0 = -	32			NL	I
Send. trace silt. Medium	377.0 = 3177.0 = -	32 35 20 28			N L	I

silt. Medium very dense gray 30 36 medium Sand, trace 60 silt & smell gravel. 15 57 28 Kedium wet 40 25

25

45 27

gray

fine

(continued)

H - STANDARD PENETRATION TEST HUMBER - BLOWS TO DRIVE "O.D. SPLIT SPOON SAMPLER 12" WITH 1402 WT. FALLING 10"

0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24

QU - UNCONFINED COMPRESSIVE STRENGTH W - WATER CONTENT % OVEN DRY WEIGHT TYPE FAILURE B - BULGE S - SHEAR E - ESTIMATED VALUE STATE OF ILLINOIS DEPARTMENT OF PUBLIC WORKS & BLOGS DIVISION OF HIGHWAYS

POPLAR STREET BRIDGE APPROACHES

BORING LOGS

# W LOCKER N: SHEET ENGINEE SHEET ENGINEERS ENGINEERS ENGINEERS ENGINEERS ENGINEERS ENGINEERS

ROUTE NO SECTION COUNTY NOTAL SMEET NO. F.A.I. - 70 82-3NVB ST. CLAIR 289 241

BORING No. S-61

BORING No. S-62

BORING No. S-63

IDENTIFICATION	ELEV. N DEPTH BLOW	00 ·	IDENTIFICATION	ELEV. N DEPTH BLOWS	QU .	40.00	ELEV.	N QU BLOWS T S.F.	• 1	-	ELEY. N QU TO DEPTH BLOWS TOS.F.	7		ELEV. H	QU W	1		ELEV. H	QU V	
Ground Surface Topsoil	408.4 0		(continued)	47 26	77.1.	Ground Surfac	406.8 0		`	(continued)	47 26	+	Ground Surface	406.5 Q	173.7.		continued)	47 41	1	
1093011	407.2		trace	= 1		Very loose	405.8				1 = 1		Ground Surface Black clayey Silt, and Cinder Topsoil	404.5			eilt.	1 4"		
hedium damp yellow and	_ 11	- teb 13	silt.	50 27		to stiff		4		silt.	50 33		V. loose damp silty very fine Sand.	403.5			f - c Sand.	156.8 50 25		
brown				357.4		fine Send.		-			4			5 5		Gray	Medium	356.0		
sandy Silt.	\$ 3 9 \$02.4	17	Dense to very	- 43		Sand, some sil			15		353.8 39		Loose brown wery fine Sand,				to	] 19		
itiff brown	-		dense wet	3		Loose				Medium dense			some silt.	=======================================			dense	E		
silty	100	1.45 25	fine	55_ 44		Loose yellow and brown	=	8		wet gray fine to coarse Sand, truce small gravel, some silt.	55 29			7	17		gray	55 16		
Locae	1 <u>.</u> *	26	nedium Sand.	7 1		brown very fine Sand.				small gravel, some silt.	1 = 1		Very	397.0	30		fine	1 =		
rrayish-			Sand. trace silt and	60		Sand, some silt.	-		-	Boring stopped by Inspector.	349.3 - 47		loose moist brown	= '			Send, trace	∃"		
very fine	-∃ .	1:	SE-11	7484 (0 7 100		Loose	394.8	7	34	WATER LEVEL 31.0			Very loose moist brown Silt, some very fin- sand.	10 7			silt.	J		
Sent.			Boring stopped Inspector.	Бу		brown Sandy			-	WATER CEVEL J.	60		sand.	393,0		Borin	ng stopped by pector.	146.5 60 43		
1000	15.		*ATER LEVEL 33.0			Loose	192.1	E 4					loose wet	15. 3		WATER	R LEVEL 29.0			
V0050	398					Loose wet gray fine Sand, some silt.	140 4						Very loose wet gray silty very fine	1						
2769 211t.	190.4.	•0				Medium damp brown	389.8	16					fine Sand.	= 3						
soft aray	184.3					fine Sand.	184.3						Loose damp brown fine	387.5						
fortun tang erey very file and, troce silt.	22,11	•3				Hed turn	20	14					Sand, trace silt. Loose	20 10						
troce	110					damp gray very fine							Loose moist gray very	1 7,						
	185.4					fine	-	1°					fine	-3						
	22 11					Sand Tittle silt.	25	17					fine Sand, some silt.	25 5						
silt and very fine						511t.	377.8	-				T-1/	Kadtum	380.5		i.	- N	7		
Send. Sedium damp gray fine	321				$\vdash$ ( )	$\mathbb{H}^{\prime}$				$\mathbb{R}^{1}$	$\Lambda / \Lambda / \Delta$	11(	damp gray fine Sand.	13		Ш				
Sandy Silt, an organic matter Dense damp gra	V V					Medium	IN	1	4			1 1/		377.5		L	_ !			
fine Sand, truce Silt.	377.9 30 -3						30	86					Medium wet gray fine to	30 23						
fine sand, truce silt. dense moist gray fine						dense							medium Sand, trace silt.	374.5						
Nedius	375.4							25						22						
rine to nedium Sand, trace silt.	25 22					gray	-	39					Medium	15 24						
	372.9						13	]"					to							
Redium	29					fine		31					dense	23						
dense							1 5						to			1				
	44.4						40	28					fine	40 40						
wet gray						Sand,	-						grey							
fine	37							38					100.000	41						
1.44						trace							very							
<u>Sond</u> ,	45, 41						45	27					fine	45 50				CTATE	OF ILLING	N.E.
(continued)						(continue	d)						(continued)		1 1	4		ENT OF P	OF HIGH	RKS & BLDGS.
																	POPLAR	STREFT	BRIDGE	APPROACHES
								H - ST. HUMBE 2" 0.0 WITH 1	R - BLC , SPLIT 405 WT.	PENETRATION TEST DVS TO DRIVE SPOON SAMPLER 12" FALLING 30"	QU - UNCONFINED COMPRE STRENGTH W - WATER CONTENT S OVEN DRY WEIGHT	SSIVE TYPE F B - BU S - SHI E - ES'	AILURE LGE EAR TIMATED VALUE				OTEAN		NG LOG	
																	FAIRT 7	o st. ci.	AIR CO. S	ECTION 82-3HVB
																		H. W. LOCH ENGIN	NER. INC.	SHEET
																		CHICAGO	ILLINOIS	206o#24

F.A.I.- 70 82-3HVB ST. CLAIR 289 242 FED ROAD DIV NO 4 ILLINOIS PROJEC BORING No. S-69 BORING No. S-68 BORING No. S-67 BEFTH BLOWS T/LF. 4 ELEY. - 60 . DEPTH BLOWS T'S.F. ELEV. N OU T IDENTIFICATION ---IDENTIFICATION INDUSTRICATION IDENTIFICATION (continued)
wet gray
coarse
Send,
trace
small
gravel
and
silt.
Very dense (continued wet gray fine to coarse Sant, small gravel, trace silt. Sround Surface 614.7 0 fround Surface 404.5 0 47 29 <u>57</u> 27 47 49 Ground Surface 405.4 0 (continued Topsoil Topsoil Topsoil
lery loose moist
prove silty very
fine Sand
Loose
ext gray
and brown
tlayey Silt,
trate very
fine Aand. dense 404.1 brown fine silty Sand. Stiff brown wet Loose 50 16 50 26 402.6 50 27 gray to Stiff brown
silty
Clay
trace
fine
aund
J99.4
Loss damp
brown Silt
trace Clay
\*\*use fine eand. 397.4 fine Very dame
wet gray
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trace
joi.2

Uense wet
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S sectus to 352.0 -35 \_ 53 CARD coarse . CATE Sand. Decayed wood. Medium moist trown very fine hand trace \*\*\* prove <u>-</u> 350.6 55 24 gray sinders brown fire Sand, trace silt and clay. fine to \*000 11112 wet medium 400 -46 organic matter, 356.2 gray Sand. brick wet gray fine to coarse Sand. trece F111 fine Loose est gray tery fine sandy bill 192.4 60 45 Very loose wet gray fine band, trace silt. silt Sand, Medden stiff damp gray silty clay trace organic matter. trace and 15 ) .)la )6 ..... silt. Wedium damp yellow a brown (ine Sand, trace silt. Very dense

we gray vo
sense gray vo
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Send trace Dense gray fine to coarse Sand, trace silt. Areve. 386.0 = , 388.4 Dense Very soft grey clavey Silt. 65 43 190.2 -\*\*: 3117111 Very loose wet yellow and brown fine Sand. Loose wet gray very fine brown Locate vel (Ter (Lot (Lot (Lot) 22. 8 and 337.9 - 29 Loose
wet gray
silty
fine
Sand
Loose
wet
gray
silt,
trace
clay
and
fine
sand 384.9 ... Medium coerse 111118 1111 wet 20 23 24 27 eray 380.0 T Very fine to Sapt. 25 2 Kedium wet gray medium Sand, trace silt and smell gravel coarse 21 send, trace silt. . 7 75 oring stopped by 377.4 330.4 75 23 Medium wet gray fine Sand little silt, trace black Boring stopped by Inspector. trace MATER LEVEL 40.5 .258 41 MATER LEVEL -- 22 ... fine sand Loose wet grey bill trace clay Boring stopped by Inspector. ETOY fine \*ATER LEVEL 29.0 .315 31 405 372.4 Soft gray clayey Silt. trece 15 -silt. \*\*: 309.4 Medium dark gray very fine Sand. little silt, trace organic satter. Soft ETAT Rectum wet gray fine hear trace fill and organic matter. 1150 2455 20 20 27.50 orgenic Hedium loose wet gray fine hend, trace silt; roots gray clayey silt. some sand, trece organic matter. matter 369.245 11 359.5 45 17 Kedium |continued| STATE OF ILLINOIS Medium DEPARTMENT OF PUBLIC WORKS & BLDGS Medium (continued) DIVISION OF HIGHWAYS POPLAR STREET BRIDGE APPROACHES TYPE FAILURE 8 - BULGE 1 - DEEAR 5 - ESTERATES TALVE . . STANDARD PENETRATION TEST HUMBER . BLOWS TO DRIVE 2" O.D. SPLIT SPOON SAMPLER 12" HITM HER WT. FALLING 30" OU - UHCONFINED COMPRESSIVE STRENGTH V - MATER CONTENT N OVEN DRY WEIGHT BORING LOGS F. A. I. RT. 70 ST. CLAIR CO. SECTION 82-3HVB SHEE H W LOCHNER INC ENGINEERS CHICAGO ILLINOIS

Indiahadaakadaalaadaahadaakadaakadaalaadaalaadaakadaataakadaadaakadaahadaadaa

SECTION COUNTY TOTAL SHEETS NO

BOUTE NO

		ROUTE NO
BORING No. S-70	BORING No.S-71	BORING No.S-72
	Series   Continued   Series	

0 1 2 3 4 5 6 7 9 9 . 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 81

							F.A.I 70 82-3HVB ST. CLAIR 269 244	
	Continue	BORING N	o. S-74		BORING No.	. S-75		
	N QU			IDENTIFICATION DEPTH BLOWS T'S.F. %	RENTALLTON	DEPTH BLOWS TISE. 4	identification depth slows Ti.F. T	
-	Dense est		Cround Surface 117.6 0	(continued) 17 24 24	Cluber.	-	22	
loose	ine to		and 7	course Sand So 43	- Book		and 50_ 22	
black			7411 413.1 5 14	3020	Grait Fill	110.1 5 14	silt.	
Cinders.	smell gra	vel 364.6 38		soan small gravel. truce sitt. \$25 Verling gray	Serve		soring stopped by aspector.	
brick.	6		yellow 10	silt. 55 25	Build		ATER LEVEL 46.0 ·	
gravel.		J59.6	brown =	Nedlum gray	atiley	١٠٠٠		
send,	545.5+		51n· 10 5	irac alli see 6	clay Loose	404.1		
and	1			ordina gray free dark. free dark. frey coarse dark trace saint gravel, a silt. 358.6 coarse darkin silt377.6 coarse darkin silt377.6 String toggray by	to	9		
silt	1	4   1	Soft br. wifty clay 403.1	Inspector.	aethur.	- 15_9		
Medium acist	12010	= 67			5etc	]		
Gray clayey allt 198.6	11 12	_	Nettun - 17		yell-	===		
Locae Loist or on					4/mit	20 14		
onity .	1 1	3-47	ati1 2d 14		berner.			
Retius		20 26	1 7.4		222m	18		
			<u>-</u>		sent.	25 25		
gr-y	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	342.6			1762			
fine	in tende	75 85		URIVIA	eller	3.5	VIL Y	
Seni.		-	30 29		organic	20,33		
truce 30	WORLDS ADDITE	338.1 44			motes.	3		
Selit. 383.1		2.5	20			382.1 25		
*-ap			35 37		Verry Deture Design grasy Ture	35 63		
tine 35			8116		Sent.	279.2		
truce	23		379.6		been yellow and brown medium lend, length meals grace.	60		
376.6	-		end brown Cin- to		leane dusp grwy fine to medium Sant, truce mail gravel.	40.49		
gray line to	0 31					374.1		
organicacter.	20		Jense 2/2.0		Section Cense	43		
Medium dense wet gruy medium to			truce		furm to course Sent, truce	45.20		
(continued)	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		Med lut.		fewery flame	1 1 1	STATE OF ILLINOIS DEPARTMENT OF PUBLIC WORKS & BLDGS DIVISION OF HIGHWAYS	
				H - STANDARD PENETRATION TEST HUMBER - BLOWS TO DRIVE 2" O.D. SPLIT SPOON SAMPLER 12" WITH 160 WT. PALLING 30"	20 - UNCOMPINED COMPRESSIME TYPE FM. STRENGTH B - SOLI W - NATER COMPRESS S - SHOE OVER DAY WIGHT E - EST	ILURE GE UR MAYED VALUE	POPLAR STREET BRIDGE APPROACHES	
				WITH 1409 WT. FALLING 30"	QVEH DRY MEIGHT T - ESTA	MATED VALUE	BORING LOGS	
							F. A. I. RT. 70 ST. CLAIR CO. SECTION 82-3HVB H. W. LOCHNER INC. SHEET ENGINEERS	

Institutional and a factor of the factor of

BO BORING No. S-77 BORING No.S-76 ELEV. H QU V BLEV. H QU T IDENTIFICATION IDENTIFICATION IDENTIFICATION IDENTIFICATION IDENTIFICATION 47 - 34 - 50 50 23 Ground Surface 415.6 O Ground Surface 414.1 0 (continued) 416.8 0 Ground Surface Topset1 413.1 Sand, Sand, Black cinders and brick fragments Fill. trace trace Brick. small small Coal .60.1 gravel gravel and 5 5 Brick 5 13 and silt. 36... 34 Miscellaneous silt. Boring stopped by Inspector. 11 12 13 13 14 15 18 Medium Sand, trace cla Loose damp yellow and brown very fine Sand, trace silt. dense 10 10 wet 35 60 16 Loose damp gray Sand, 55 yellow trace 15 9 silt. 15. 6 Very dense gray fine to coarse Sand truce small gravel. dense and Loose Boring stopped by Inspector. to yellow 29 25 23 23 22 20 15 dense brown 25 16 fine 16 fine 25 17 Sand, trace 28 silt 30 21 30 26 with orgenic 24 silt. 26 Sand, matter 35 37 noted. 35 38 35 28 25 375.6 wet gray 40. 52 Medium fine dense to wet \_ 23 Dense COATSO gray wet Sand, fine 45 37 gray 8000 45 34 45 42 STATE OF ILLINOIS DEPARTMENT OF PUBLIC WORKS & BLDGS fine to emall Continu DIVISION OF HIGHWAYS POPLAR STREET BRIDGE APPROACHES QU - UNCONFINED COMPRESSIVE STRENGTH W - WATER CONTENT S OVEN DRY WEIGHT TYPE FAILURE
B - BULGE
S - SHEAR
E - ESTIMATED VALUE BORING LOGS F.A.I.RT. 70 ST. CLAIR CO. SECTION 82-3HVB H. W. LOCHNER INC ENGINEERS CHICAGO ILLINGIS

ROUTE NO	SECTION	cou	NTY	TOTAL	SHEET	
F. A. I 70	82-3HVE	ST. CI	ST. CLAIR		246	
FED. ROAD DI	V. NO. 4	ILLINOIS	PROJE	C1		

BORING No. S-82



## BORING No.S-84

28411.04104	tate - 20 *	DENTIFICATION	ELEV 00 .
Ground Surface	413.3 Q	(continued)	47 20
winder.	-	redium	_ **
	_		-
2243		Sand.	
rati.		trace	50 27
Loose famp	_	silt	-
yellow and prown yery		5110	_
fine work	5.3	and	
trace that.	1.2.2 -	10.211	7 2 34
20014 20151	10/12	55.2 * 1	-
t own very line		rr.vel	
state are.	• . 5 . 8 3		
Soft SetS			
2000			
tieyey			-
1111	.10 -		21
1400	10.11		355.3
		Tery tesse	-
.::::	,	***	_
-0011		CTRI	60 93
		fire	_
5.7		STW.	_
	3 12	1111.	
2010.42	-2.0	-	350.3 92
		Borin' stopped by	
5450		to a grand .	
	- i e	18.0.	
		* It that your	
74			

20 25

1172

184.1 185.2 18

\*\*::::

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6747

:88 tinues

384.3

-5 25

GENTIFICATION	24979	81,040	7 3.5.	;	IDENTIFICATION	DEPTH	8LOWS T 1.F	
Ground Surface	413.2 0				(cont'd) Sand	366.2 4	30	
700				- 1	Grey		30	
2011	412.2				fine Send	165.2	-	
Stiff damp	-			- 1	hedium	-	-	
brown clayey	_	2		- 1	dense		+	
5111, some		10	4.275		wit	2.5	ī 19	
very fine sund.	416.2	-			gray	- 21	1 . ,	
				- 1	fine		-	
L009*				- 1	to	-	-	
1480				- 1	coarse		-	
b.rown.	5	7			Sand.		37	
1+17					trace		- 37	
fine				1	small	-	-	
silty				- 1	gravel		-	
Send.					and	-	4	
Sand.				1	silt:		5 20	
clay.	405.2			1	organic	5	5 20	
				1	matter	357.2	-	
25155					noted.	377.2	-	
1452					or. Clayey Silt	350.9	_	
2500	1	3 4	1 15	37	Dense wet	-		
Bandy	_	_		1			30	
511t.					cray fine	_	-	
1.545*				- 1			-	
clay	.01.0	2			Sand. trace silt.	_	-	
		3 -		6 1	trace alic.	353.2 6	0 42	
		2.0			Borite stopped t	377.4 6	0 42	
-7734					inspector.	,	-	
				1	inspector.	-	-	
					PATER LEVEL 37.5		-	
207145	1	5 10			SATES LEVEL JILY			_
		_						

33 27

IDENTIFICATION	ELEV.		QU T S.F.	:	IDENTIFICATION	ELEV. DEPTH	BL 0 V S	QU 1 5.7.	;
	L18.2 0	,			(continued)  Sand,  trace enall gr-vel and silt.	365.7	,,		
Fincellaneous Fill	-	14			Boring stopped by inspector.				

382.2 sedium sols landy Sills. Dense desp relicus x brown fine Seed, Ursce small crawn Nerium dende ent grwy fine Jani, trace all, organic matter untel. hedium wet gray fine to coarse (continue

end

25740

1110 Send. trace Dense gray fine .0 coarse [continued]

15

silty

Lley

Ketius

dense

QU - UNCONFINED COMPRESSIVE STRENGTH W - WATER CONTENT % OVEN DRY WEIGHT

TYPE FAILURE B - BULGE S - SHEAR E - ESTIMATED VALUE

STATE OF ILLINOIS
DEPARTMENT OF PUBLIC WORKS & BLDGS DIVISION OF HIGHWAYS

POPLAR STREET BRIDGE APPROACHES

BORING LOGS

F.A.I.RT. 70 ST. CLAIR CO. SECTION 82-3HVB H. W. LOCHNER. INC. ENGINEERS CHICAGO. ILLINOIS SHEET 211 of 241

	BORING	No.S-85			BORING	No. S-86				BORING	110.0 01		
TIFICATION	ELEV. # 50 DEFTH BLOSS 7 LF.	IDENTIFICATION	1144	IGENTIFICATION	ELEV DE DEPTH BLOWS T. L.F.		DEPTH BLOWS T'LF. S		-	DEPTH BLOWS T/S.F. S	(continued)	BLEY. BLOUG TELL.	
	414.5 0	& silfontinued)	er) 67.0 4.7 15	Oround Sufface	414.5 0	(continued) Sand, trace and 11 Frival A silt. Redium	15 25 166.5	-9	round Surface	414.5 0		25	
148	=	gray medium to coarse	3		11, 21, 21,	Medium gray fine	3		Cloders.	3.,	Hedium gray fine to medium Sand, trace small gravel and silt.	1311	
nd	7 18	coarse Sand	169.5 55 26	Black	- 7	fine to	50 17			= 16	and silt.	50 17	
inder	1 2	Sease	=	2.4tk	-	to coerse Sem	363,2				Patrice.	103.2	
11	109.7 5 3	KF+7	-5 47		<u>5</u> 7		- 31			5 6	Medium grey	726	
гу	=	fine	-	2,000	-	Dona's grey line	3		<u> </u>		fine to	326	
own	1 11.	30 to	 2)		∃ •	38.60	359.545 57			•	coarse	55 29	
	404.5 10 :	coarse	=		3	soring stopped by Inspector.				E	Send Redium	158.5	
11.	404.5 10 s	Sand.	_ se	<u>r111</u>	1 <u>5</u> 49	14711 LEVEL 38.0			brick	দ্রু +	fice Send	144 = 39	
35¢	Ē,	large		Medium brown	421.1					3   1		3	
	<b>3</b> 7	gravel	195.3.5 .0		L02.0 - 15					3,	Hedium gray fine	60_35	
		Boring stopsed by Inspector.	=						<u> </u>		to medium Sand, trace	1 - 1	
11 uz	141	earth styte 200	٠	re:: a	15 10					1 <u>5</u> 8	trece	- <u>-</u> 21	
: <b>-</b> 1.	4				=			-		198.0	Gray	151.0	
	- 11				∃•					] 1°	fine Send Boring stopped by Inspector	149.5 65 90	
nd.				brows.	3				Medius	4	Inspector	4	
	2 15				111111111111111111111111111111111111111					20 17	PATER LEVEL _39.5		
	-1				3				trown.	3.			
11.	392.0			1677	2.					- 28			
	=				3 1 1				fine				
Medius	25 25				13 21					<u>52</u> 57			
brown	-3						V V V	TIC	7 / 1				
	=======================================			-()K	4.2		$IV/I\Delta$	1 1 (	34KE.	3"			
fine	A 3				7		IVI/\		I		N L		
Send.	3 <b>3</b> 17			<u> 247.4</u> .	10 قد				trace	72 55			
race	4									7			
silt. Jense	362.5			12000 01	2.					25			
1r.e	1 1				361.0				eilt.	=			
iand,	379.5 15 5,			Sesse	15					15 35			
y dense y medium	1			6747	=======================================			-	Dense brown	)78.0 —			
y medium id, trace ii revel	377.0 52			fire	3.				fine Sand, trace	176.5			
Nedium				3•sd.	3				Dense	4			
fine to	-J. 2			trace organic	ەدققى				6747	AU 50			
Sand,				Mitter.	4				fine to	7			
truce small gravel	2.8				371.5				Send,	-= ,5			
end silt.				Medium					trece	3			
at gray fine	369.7 45 2.			Medium dense gray fine	±3 +2				see 11	(د قد			1010
small grave	. 1			to medium  consisuad	4				[continued]	168.5	DEPART	STATE OF ILLI MENT OF PUBLIC W DIVISION OF HIG	ORKS & BLD
											POPL	AR STREET BRIDGE	APPROACH
					•	ANDARD PENETRATION TEST - BLOWS TO DRIVE LIVELT MODE SAMPLES 12" dit WT. FALLING 30"	by - Unconfined Confeess	YE TYPE PAILUE B - SULGE S - SIMEAE E - ESTMEAT				BORING LO	6S

0 15 25 35 4 5 5 7 16 17 18 19 20 21 22 23 24 <u>8</u> 9 10 11 12 13 14 15 15 15 15 20 21 22 23 24 <u>8</u>

ROUTE NO. SECTION COUNTY SHEETS NO. F.A.I.- 70 82-3HV8 ST. CLAIR 289 247

F.A.I.RT, 70 ST. CLAIR CO. SECTION 82-3HVB
H. W. LOCHNER, INC. SHEET
ENGINEERS
CHICAGO, ILLINOIS DR 00241

F. A. I. - 70 82-3HVB ST. CLAIR 289 FED ROAD DIV NO 4 | ILLINOIS | PROJECT BORING No. S-91 BORING No. S-92 BORING No. S-93 IDENTIFICATION BLEV. H OU V (continued)
Sand, trace silt with
J\* wood seems. IDENTIFICATION IDENTIFICATION Ground Surface 413.5 U 47 34 (continued) Ground Surface Ground ourface brown very fine 3and. 47 39 47 15 Brick. Cinters 111111111111111 fine ama 1 1 Cimters 50 16 50. 20 coarse he flux 5 2 Sand, F111 trace yellow smell miscellaneous gray Very soft brown silty Clay gravel 55 57 medium ailt. F111 10 25 10 13 37 Stiff brown silty clay organic 64 37 Sand. 1.1 Sand. 'trace Medium 15 14 15 10 Keilun Boring stopped by Inspector. amal! loose yellow dense brown and gray very fine sand, trace silt brown fine trace
silt 333.8

very dense gray
coarse sand, vitt
smil gravel. 332.3 75 86
Boring stopped by
Inspector. Sand, TATER LEVEL 24.5 Dense yellow . Grey fine Sand.trace silt & organic mat. 373.8 prown silt. fine 35 63 Send 78.6 Medium dense fine gray dense fine to gray coarse fine med tue Sand, Sand. 17 trace trace silt. 371.6 coarse sas 11 Send. gravel. Med1um trace dense silt STATE OF ILLINOIS Medium gray fine DEPARTMENT OF PUBLIC WORKS & BLDGS DIVISION OF HIGHWAYS POPLAR STREET BRIDGE APPROACHES BORING LOGS TYPE FAILURE B - BULGE 1 - SHEAR F - ESTIMATED VALUE F. A. I. RT. 70 ST. CLAIR CO. SECTION 82-3HVB H. W. LOCHNER, INC. ENGINEERS SHEET CHICAGO, ILLINOIS

SECTION COUNTY TOTAL SHEET NO.

		ROUTE NO. SECTION COUNTY TOTAL SHEET NO.
		ROUTE NO. SECTION COUNTY SHEETS NO.  F.A.I 70 82-3HVB ST. CLAIR 289 249
		FED: ROAD DIV. NO. 4 ILLINOIS PROJECT
BORING No. S-103	BORING No. S-104	BORING No. S-105
Tity   x   00   v	CONSTITUTE   CALV. N 60 T   CONSTITUTE   CALV. N 60 T   CONSTITUTE   CALV. N 60 T   CONSTITUTE   CALV. N 60 T	CLEY. N GO U GLEY N GO U GLEY. N GO U THOU BAPTIN BLOWG TAR. N GREYTPICATION OFFTH BLOWG TAR. N
		riace \$12.4.0 Cat log 47 257
Ground suffice the 2 (continued) 17 35 10 10 10 10 10 10 10 10 10 10 10 10 10		partially decayed. 164. 4
and - 13	Topsoil 26 silt 10 35 Fill 127	
brick Sand,		·   =
	Till	to = 46
5 16 5 16	Loose gray 5 Sand Trace	
The yellow and tryati some SN 16 strain of the yellow strain of the yell	fine Sand. trace Silt 102.1 gray Stiff	
10 5 .9 30 Organia		101.4 3 46
siley	3071	
brish very fine 200.7		sit 53.4 of 62
>+diur 25 8 1.9x 27 351.7 118		
boring stopped by		- ATTO LEVY, 26.0.
212t	gray 50 sattle Live 33.0.	= "
nry 20 9 1.1x 34	clayer 20 6 .72 30	20 21
fine =	<u>511t</u>	=
9 1,38 34	- ).	7 Fine
Said 389.7   15 30	and 35,	
very fine sand	Sand Joseph A T   And organ	ie meres
17 see 386.7 13	Signal 155,11 FORMATI Signal 156,12 FORMATI	34ct 364.4 3
heffus -	may —	10 17
grey 20 15	fine	30, 17
very 17	silty = 22	1 30
fine -	sand. 377.6	3
Sand . 35 29	JE 17 to	15 x
5.11 376.7 4.	gray Coard C	· 🗐 🖟 📗
5.11 376.7 84	Aedium Jo	3 11
40 53	371.6 10 20 ett.	26
Recium	Dents	371.4
dense 26	gray - 25 fam. coarse - 25 coa	. = 29
grey	Sand 43 55 sand	u 10
fine special formation (continued)	(continue)	STATE OF ILLINOIS DEPARTMENT OF PUBLIC WORKS & BLDGS. DIVISION OF HIGHWAYS
		POPLAR STREET BRIDGE APPROACHES
		BORING LOGS
	# . I AMBRAD PROFE DATION TEXT	
	THE STATE OF	F.A.I.RT. 70 ST. CLAIR CO. SECTION 82-3HVB H. W. LOCHNER, INC. SHEET ENGINEERS SHEET
		CHICAGO, ILLINOIS 2140F241

- 20

POPLAR STREET BRIDGE APPROACHES	BORING No. S-106    Str.	BORING No. S-107	BORING No. S-ID8  BORING No. S-ID8  BORING No. S-ID8  BORING No. S-ID8  BORING No. S-ID8  BORING No. S-ID8  BORING No. S-ID8  BORING No. S-ID8  BORING No. S-ID8  BORING No. S-ID8  BORING No. S-ID8  Grand Sartis, AUG., 10  Grand Sartis, AUG., 10  Borice Solve Service Sartis, AUG., 10  Borice Solve So
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Sentendende de la companya del companya de la companya de la companya del companya de la company

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SECTION COUNTY TOTAL SHEET NO. EA. I. - 70 82-3HVB ST. CLAIR 289 251 FED. ROAD DIV. NO. 4 | ILLINOIS | PROJECT BORING No.S-II4 BORING No. S-II3 BORING No. S-II2 ELEY. H QU T DEFTH BLOWS T/5.F. % ----DEPTH BLOWS T/LF. S IDENTIFICATION IDENTIFICATION (continue DENTIFICATION (continued) Ground Surface . 417.5 O 50 67 iround Jurface Stack grey بالباليا الخياباليالية the Lilian coarse trace gravel fine Sand, silt. 50 32 20 trace Boring stopped Inspector. coarse -4-1. Medium VATER LEVEL 41.0 . Cinters silt.
Very loose
gray
silty,
clayey,
Sand
Very loose
gray
fine
Sand,
trace
ailt.
Very
loose
gray
fine
sand,
some
silt. dense small Miscellaneous \$5. 46 128 60. 12 gravel 55 19 · see llane via and very silt. 959.0 - 16 Boring stopped Inspector. fine 1 , 0.5 Vegt us \*ATER LEVEL 41.5 Sand. F ... re: 100 4 F111 33 65 8 20 6 Medium gray very Sens dense Medium gray silty medium to fine 20 13 29 29 46 46 51 FFAY 15 Soft fine .... 25 2 25 18 Medium 11 95 16 Hed: un 30 20 30 25 yellow .... 27 Send ama 11 24 prown with trace gray 35 20 35 24 very 15 20 silt. 21 large fine Medium Sand, A5 25 19 gravel trace dense 17200 23 silt. and 40 20 40 29 2112 coarse silt. 19 Sand dense gray fine Sand. Urace to TOLY Dense 45 39 dense 45 14 17 gray gray fine (continued STATE OF ILLINOIS 95 34 DEPARTMENT OF PUBLIC WORKS & BLDGS. DIVISION OF HIGHWAYS POPLAR STREET BRIDGE APPROACHES BORING LOGS TYPE PAILURE B - BULGE L - SHEAR E - ESTMATED VALUE Boring stopped by Inspector. F.A.I.RT. 70 ST. CLAIR CO. SECTION 82-3HVB SHEET H. W. LOCHNER. INC. ENGINEERS CHICAGO. ILLINOIS

BOUTE NO.

BORING No. S-115	BORING No. S-116	BORING No. S-117
DENTIFICATION OFF BLOWS TARE & IDENTIFICATION OFF BLOWS TARE.	IDENTIFICATION DEFIN SLOWS TILF. S IDENTIFICATION DEFIN SLOWS TILF. S CONSTITUTED TO SERVE SLOWS TILF. S	SENTIFICATION OFFTH SLOWETISF. N SOUTH SLOWETISF. N SOUTH SLOWETISF. N SOUTH SLOWETISF. N
Ground Surface 41).) 0 (continued) 47 56	Silt 365.7 47 23	
		Miscellaneous 22 fine so 120
	Brick, and	locae atit.
yellow	### ##################################	2   2   2   2   2   2   2   2   2   2
brown trace 7		terminal topics of the control of th
silt. 404.1 Boring stopped by		Very
gray Clay 403.5 10 6 1.5 27 WATER LEVEL 16.0	Medium	loose 10: > grey and
selty from Sold (02.)	500.6 == ,	treen - 3 , or 27
brown 3 1.0 37	Longe co	fine and
Silt. truce 15 5 1.0 30	grey 11 4 27 toerse 1 12	3000 27
fine		boss gray
send. 195.3 - 8	1740	District Service Control Servi
Redus yellow and 20 11	clay 22 5 and 3 41	erey very fise 20 12 Sand and
trown 19 11 fine eilty Sand	and	1166 and 201.7
199.0 :	10   10   10   10   10   10   10   10	Lacese 15
	fine 23 t 5 34 saturates 36.0 -	10 34
yellow and brown		
Partium 55, 27 graph yellow and prom 19 graph structure silt.	TELLINE	Cry To NLY
383.) 10 21		jīj₂1 \
Aedius	181 5 "	andium
gray 29		some 51
fine	1916 1916 1917 1917 1917 1917	eile. JE 7
377.2		=   =
Medium 46	Petiting group first of the course and cours	37h.7 -
andium 40 21	Dense gray fine to coarse Sand. trace 4D	Medium
Sand.		responses All to to to coarse and trace and tr
silt. J2	dence gray 50 floe	•iit
369.3		Denae gray medium AS 4.9
(confitting)	Band, AS Trace — (continued) —	Dense 169.4 To 169.4 To 169.5
		POPLAR STREET BRIDGE APPROACHES
		200110 1000
	- 17-03-03 PERTEATION TEST ON UNCONFRESSIVE TO  VARIABLE - 6-107-01 TO DISTRICT TEST TO 0.5 DEST PROFES SEAPLES 12" # WITE CONTENT \$ 1 VINE SEAT F. ASALINED TO THE CONTENT SEAPLES 12" OVER DESTRUCTION \$ 1	PORTAGUES - SUCRE - SUCR - SUCRE - SUCRE - SUC
		H LOCHNER INC. SHEET  H LOCHNER INC. SHEET  ENGINEERS  CHICAGO ILLINOIS  ZITOZGI

Light half the first that the first of the f

	ROUTE NO.	SECTION	COUN	TY	SHEETS	253	
F	A.I 70	82-3HVB	ST. CL	AIR	289		

	BORING	No. S-118			BORING	No. S-119			BORI	NG No. S	6-120		
	ELEV. N QU .		ELEV. N QU W		ELEY. H QU W		ELEY. H QU .	IDENTIFICAT	ELEV. N	QU .	IDENTIFICATION	ELEV. H QU DEPTH BLOWS T/S	. :
Ground Surface	DEPTH BLOWS T/S.F. 5	(continued)		Ground Sur- Cinde		(continued)	4.7	Ground Surf		10200	(continued) trace silt.	47 25	
Ground Surface	_	(concludes)	122	Brick	F*	trace	I - " I I	Cindere			eilt.	363.3	
Sleg	3	silt.	3	Sand Pill and		silt	3	bricks,	1 4		Dense		
plack	409.8		361.8 50 33	Coner	rte	and	50 22	clay	1 -3			50 45	
cinders,		Medium		Slag from	3.2' 406.1 own 5 7	wood	1 - 1 1 1	and	5 51		medium	1 7 1	1
and aiscellane	1406.8 5 5	Rray	27	Loose br very fin	Sand, LOL 6	chips.	357.6 7 16	sleg <u>Fill</u>	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2			42	1/1
brownfine Sand		fine	3 1	Soft grey		Loose	-		404.8		gray	=	1/
Soft	_ 6	coarse	55 17	brown	_6	fine	55. 9	Stiff	9	1.0 27	fine	55 25	
derk	= 1	Sand,		Clay	402.1	to coarse	3	gray and brown silty Clay	1 -3			1 -3	
brown	10 8 .7 27	some	_ 27	mediu	10 5	Sand, trace	10	Clay	10 5	.5 27	Sand,	21	
silty		small		grey	and	V.Loose	352.1	Medium	406.8			1 3 1	
truce	5 .6 31	gravel,	6u 11	brown	6 1.5 30	gray	60. 2	clayey Silt.	∃4	.5 34	trace	60. 45	
fine	-1	silt.	351.3	very	3	gravel,	3	brown clayey Silt. some fine sand.	1 3		silt.		
sand.	397.8		-	fine	15 9 2.0 2	fine to	3	sand.	396.8 15 11			149.3 - 26	
tine	E	Medium gray fine to coarse Sand, and Small gravel,	= 22	Sand,	4	Sand, 1/8 to 2" wood seams,	347.1	Medium	1 -1		Boringstopped by Inspector.		
trace stit	395.3 7	trace silt.	347.8	silt	- 12	wood seams.  Very loose gruy medium Sand, tr.si 1'8 - 2" wood seam	at =	gray	-11		WATER LEVEL 41.0		
brown dendy	3.	Dense	05- 45	Seuns		1/8 - 2" wood seam	345.6 65 12	and	1 3			•	
Silt	392.8	gr-y			391.1	gray fine	7	brown	20 32				
Kedium yellow and	20 23	fine	34		3 1	to medium Sand, trace	= 7	fine silty	1 4				
brown.	1	Sand,	343.3	Mediu	10	trace		Sand.	7				
fine	1*	Dense	29 40		"		70 33 339.6 -		388.8				
bend. trace silt.	25 13	to	7 1	gray	25 9	Dense	339.6	Medium	25 14				
alit.	386.3	dense gray fine	45	+00		Fine	3.0						
Medium		to		fine		to medium Sand, trace	Z; 68	dense.	21		II \		
gray sandy Silt.	14	Sand, trace	75 37			trace sit:	25 68	gray	A G	7 113			
	383.3	silt and		Sand	10 14	Very dense fine to medium	334.6		10 2				
fine Sand, trace silt.	30 15	gravel.	33	trac		gray Sand, trace silt &	104	fine	3				
Loose	381.3		333.3		3.1	small gravel.	331.6						
Silt,	. 8	Sense gray fine to coarse Sand, with small to large	80 41	silt	377.6	Kedium	<u>80</u> 22	to	1 4"				
very fine	378.3	small to large gravel, trace		Dens		dense	-]	sedium	1				
Dense to	35 47	311t.	330.3	gray			28		35 3				
very		Kedium to		medi Send		gray		Sand,	1 3				
1,	33	v.dense gray fine	85 45	trac	4.)	fine	85 30		3	'			
dense		fine to coarse	-	silt	. 371.6	to		trace	-				
	40 33	With	43		40 18	coarse	80	silt.	40 3	'			
Kray		gravel, trace		riedi	us .				-				
fine	40	silt,	90 27	gray	17	Sand.	94 45		- 2	9			
1		limestone fragments.		medi	us _	trace	"E		367.8				
wend.	45 54		319.8 50	to	45 13	silt	55	Medium gray medium	45 2	1			
trace		noring stopped b	y	Cour		and	-  "	medium Sand.	-		DEPARTA	STATE OF	ILLINOIS LIC WORKS & BLDGS.
(continued)	1 1 1	MATER LEVEL 35.0		i conti	nued)	-	95 19		mey.		DELANT	DIVISION OF	
						to	25 47				POPLA	STREET BI	RIDGE APPROACHES
			N - STANDARD PENETRATION TO NUMBER - BLOWS TO DRIVE 2" O.D. SPLIT SPOON SAMPLER I WITH 1405 WT. FALLING 30"	ST QU - UNCONFINED COMPRESSIVE STRENGTH " - WATER CONTENT S OVEN DRY WEIGHT	TYPE FAILURE B - BULGE S - SHEAR E - ESTIMATED VALUE	medium gravel.	3,5					BORING	
			WITH 1405 WT. PALLING 50"	VILL 255.271									
						Boring stopped by	21				F. A. I. RT.	H. W. LOCHNER	
						Immpector.	1 3 1					H. W. LOCHNER ENGINEER CHICAGO. ILL	5

SECTION COUNTY TOTAL SHEET NO. FAI - 70 B2-3HVB ST. CLAIR 289 254 WED WOMED DIN NO 4 ILLINOIS PROJECT BORING No. S-123 BORING No. S-122 BORING No. S-121 1.1+. . SU . IDENTIFICATION Dround Surface 417.6 Q <u>47</u> 28 (continued) gravel. 369.7 113 IDENTIFICATION Ground Surface ound purface grey fine Sand Cinders. SE 53 2747 367.2 50 34 12 2) Very .... brick grushed dense gray rock, 27400 very 7111 35. 43 fine 55 88 Short. 45.15 to medium fine Sand Sand. Medical graph Cuse to constructe Sandi. sous medical to 405.6 tery loose troom Silt with very fire sand. Very dense gray fine to charse Sant trace small gravel 3052 357.2 60 30 Loose Gray coarse Sand 15 = 25 15 11 cleyer Gravel Redium brown Silt and wery fine Send trace clay. Sand, & very dense gray fine Sand, trace silt. 65 25 .... 45)8 ametica Sandi fine fire Sand, ..... Very 111514 fine. dense Redlus 20 54 Medius 400 gray 25 11 25.00 25 21 fine to sand, \_ 18) 55el vellow medium gravel. Sand, trece very dense arey fine and Military, 335-075 to lose of the county of the 339.7 85 \*\*\*\*\* . \*\*\* . 37 Very dense to medium gray fine to coarse Sand, trace small gravel and silt. Kedium grey silty very fine send fine 23 €ÿ 19 376.0 15 26 Reditu gray fine Sand, truce silt. trace Medium dense trace silt, Medium grey yery fine Sand, with decayed wood organic gray organic matter noted. 85 34 fine to coarse \_ 27 Sand . gray trace 374.7 28 Redium gray fine smallto very nedium Jand, truce silt. Very dense gray fine Sand, trace silt and coarse fine gravel STATE OF ILLINOIS DEPARTMENT OF PUBLIC WORKS & BLDGS. hedium organic. 222.2 95 25 Boring stopped by DIVISION OF HIGHWAYS WATER LEVEL POPLAR STREET BRIDGE APPROACHES TYPE FAILURE 8 - BULSE 5 - SHEAR 8 - BYTHATED VALUE BORING LOGS FAIRT TO ST. CLAIR CO. SECTION 82-3HVB SHEET H W LOCHNER INC CHICAGO TELINOIS

BONITE WO

ROUTE NO.	SECTION		COUNTY		TOTAL	SHEET NO.		
F. A. I 70	82-3HVE	3	ST. CL	AIR	289	255		
FED. ROAD DI	V. NO. 4	ILL	INOIS	PROJE	CT.			

		No. S-124					No. S-125				В	ORING	No.S-12	26		
IDENTIFICATION	DEFTH BLOWS T/S.F. %		BLEY H QU V	IDENTIFICATION	DEPTH BLOWS T	90 V	IDENTIFICATION	DEPTH BLOWS T/S.F. S		IDENTIFICATION	DEPTH BL	H QU V	IDENTIFIE	CATION	BLEV. H QU .	
	417.8 0	(dontinued)	57 17 368.8 -	Ground Surface	413.6 0		(continued)	47 9		Ground Surface	413.9 0		(contin	ued)	47 - 37  50 27	
	1 -3	silt	[]	Cinders,	1 -3		to medium	1 -1 1 1		Cinders.	1 4		medi	un	3	
Black	= ,		50 20	Brick,	5 31		medium Sand, trace small gravel.	50 33		Slag &	l 3.	90			7,1	
	1 3 1	Dense gray fine to coarse		Rock	4.		gravel.	362.6		Brick	-		Sand		50, 27	
		fine	44	fragments	3	-	Dense	362.6		FILL	409.9				37	
cinders		coarse	= 44	F111	5 31		gray	65		Loose	5	7			37	
	1 - 1   1	Sand. small gravel.			1 4 1		fine			grey			trac		=	
	2	8.2.01.	17 10		405.6 22		Send	55 35		medium	1 7	5				
and	3		361.8	Gray	-			357.6		silty	404.9		silt		3	
	10 9	Very		Gray Clay, trace silt,	10 3 .	6 32	Medium			3400						
	- Y	dense gray very fine	215		402.6	." 32	dense	21		Loose to medium	10	7 1.20 30	1	3	55.9 7 46	
miscellaneou	14 -	Sand, trace	3	Brown	-		gray	3		gray	1 7					
	3	trace		and	3.	7 27	fine	60 57		gray silty very fine sand, some clay.	1 7	.70 37	Dene gray fine		60 47	
	3   1	Boring stopped by Inspector.	1 3 1 1	gray	3		to	1 3 1 1		sand,	-		fine		3	
F111	15			fine	15 10		coarse	3 1		clay.	200 , 15	7 1.10 37	medi Sand	un	3	
	LO1.3	WATER LEVEL 41.0	4 1 1	Sandy 311t	397.6		Sand,	333		Medium	398.4		silt	•	128	
Loose	T = , , ,			Brown	1 4.		trace			gray	3		to medi Sand trac silt with smal grav	h,	4	
Loose gray layey Silt Loose gray Silty very fine Sand	399.8 - 5 34			fine Sand, trace	313		silt.	348.1 65 36		brown fine Sand, trace	1 4	10	grav		65 34	
gray Silty	1 - 1			trace	1 -1					trace	4		Grav mad	ium to	47.9	
very fine	20 8			silt & black organic	20 26		Medium	] ,,		and clay.		14	coarse S	and & emal	16.4 - 30	
Sand	396.3			organic matter noted, Medium	392.1			] ] [ ]		Medium	392.9		Boring at Inspector	ium to and k emal race silts opped by	3"	
Medium	22				10			]			1 -	37		LEVEL _35.0		
brown	3"			fine	3.0			20 31		brown	1 -1.		*ATER		70	
fine	25 16			to	25 11		dense			fine	23 2		l	_	_	
Sand, trace silt.	4			nedium	14 11					Sand,						
*****	391.3			Silty				V/HZ111	1 1 (		<b>[</b> ],		N. I	$-\mathbf{v}$		
Kedium	18				)85.6	W	gray.	25, 25	I I '	trace	1 47	6	NL	- 1		
	3			Redium	3			1 3 1 1		silt.	-			_		
dense	30 40			gray	30 13			1 4			384.4	0				
					1 -1		Sand Fine to coarse	335.6		Medium gray	3					
gray	34			silty	17		Sand, trace sil	t _		fine Sand, some silt.	Э.					
	∃"			Send	380.1	B	fragments. oring stopped by napector.	333.6 80 26		silt.	1 1	.8				
fine	1 1			Medium	-	Ĭ	nspector.	1 4 1 1			379.9					
	35 24			gray very fine	35 20		WATER LEVEL .	27.0		Loose gray fine <u>Sand</u> , silt lenses	35 9	27				
Sand,	1 1 1			Sand Hedium gray yery fine	377.6	1 -				silt lenses	377.9					
				Sand, trace	21					Medium	1 -1,					
trace				afte & clay.	375.6						3					
	I			Dense	=					dense	-					
silt.	40 17			fine	40 26	1.1					40 2	6				
Gray Silt	376.8			Sand, trace silt.	3 1						-					
Medium	20			•116.	370.6 - 30					gray	1	6				
gray	1 F				7						1 7					
fine	45.24			Loose	45 9					fine	45 3		_			
Sand,	1 4 1 1			to dense	=						~3,	-			STATE OF ILLI	
(continued)	1 - 1 1			fine (continued)	1 7 1	1				to (continued)	1 -	1 1	D		ENT OF PUBLIC V	
															DIVISION OF HIG	HHAIS
														POPLAR	STREET BRIDGE	APPROAC
						H - STANDARD HUNBER - BLO	PENETRATION TEST OWS TO DRIVE SPOON SAMPLER 12"	QU - UNCONFINED COMPRESS STRENGTH W - WATER CONTENT %	IIVE .	TYPE PAILURE - BULGE - SHEAR - ESTIMATED VALUE					BORING LO	GS
						WITH 1405 WT.	FALLING 30"	OVEN DRY WEIGHT	;	- ESTIMATED VALUE						
													F.	A.I.RT. 7	ST. CLAIR CO.	SECTION 82
															H. W. LOCHNER. INC. INGINEERS	
															CHICAGO, ILLINOIS	
					789	-			->						INGINEERS CHICAGO, ILLINOI	15

COUNTY TOTAL SHEET NO. ROUTE NO. SECTION EA.I.- 70 82-3HVB ST. CLAIR 289 256 FED. ROAD DIV. NO. 4 | ILLINOIS | PROJECT BORING No.S-133 BORING No.S-134 BORING No. S-135 ELEY. H QU V ELEV. N QU T IDENTIFICATION DEPTH BLOWS T/S.F. S ELEV. H QU W IDENTIFICATION IDENTIFICATION 133 (continued) Ground Surface 11.0 0 61 50 50 silt 111 08.5 Cinters. gray Cinders
and
Sand.
Loose yellow
and brown
very fine
silty Sand. 2) broken 50 84 Horing stopped by Inspector. limestone. and fine 62 VATER LEVEL 38.0 5 16 27 miscellane Loose yellow and brown silty Sand. trace Clay. Stiff gray abrown Clay Stiff brown silty fine Sand, trace clay. organic Loose matter to trace 39 o1.c 10 3 .7 10 11 gray 29 noted. 7 1,25 24 fine silt. Sand, Medium little grav Loose
yellow &
brown
trace
fine mand
Medium
yellow
and
brown
fine
Sand
Loose gray
and brown
fore
fine sand
brown
fine
Sand
Loose gray
and brown
fine
Sand
some
Sand
Loose gray
and brown
fine
Sand
some
Sand
s 15 11 fine to 15 8 15 4 .5 27 18 Boring stopped by Inspector. Very CORTSE Send, 10 trace smell gravel 20 11 20 11 gray and WATER LEVEL 37.0 silt. clavey Very loose gray Silt, trace clay and fine sand. Very Boring stopped by 25 9 25 3 10 WATER LEVEL 36.0 some 381.4 30 4 JQ 4 .18 34 very fine fine 18 Medium dense brown very fine Sand, trace silt. 35 12 35 3 379.1 Medium dense brown fine Silty Sand, trace organic matter. \_\_\_ 22 28 10 Medium 40 13 40 31 28 \_ 33 Hedium brown silty fine Ser 26 45 49 45 53 STATE OF ILLINOIS dense コ Very dense brown continue DEPARTMENT OF PUBLIC WORKS & BLDGS DIVISION OF HIGHWAYS POPLAR STREET BRIDGE APPROACHES TYPE FAILURE
B - BULGE
S - SHEAR
E - ESTIMATED VALUE BORING LOGS

F. A. I. RT. 70 ST. CLAIR CO. SECTION 82-3HVB

H. W. LOCHNER. INC. ENGINEERS CHICAGO. ILLINOIS

SHEET

Ground Surface

silt,

and

F111

Loose brown very fine Sand

Very loose brown Silt, trace very Fine gravel.

to

medium

brown

very

fine

Sand,

BORE

...

Loose

gray

fine

Sand.

trace

silt.

Medium

very

fine

Sand.

trace continue

cinders,

miscellaneous

411.4 0

405.9

		F.A.I70 82-3HVB ST. CLAIR 285 257
BORING No. S-136	BORING No. S-137	BORING No. S-138
10   10   10   10   10   10   10   10	### ### #### #########################	10   10   10   10   10   10   10   10

ROUTE NO. SECTION COUNTY SHEETS NO.

H. W. LOCHNER. INC. ENGINEERS CHICAGO. ILLINOIS

2220F241

F.A.I.- 70 82-3HVB ST. CLAIR 289 258 FED. ROAD DIV. NO. 4 ILLINOIS PROJECT BORING No. S-141 BORING No. S-139 BORING No.S-140 Science 417.3 0 Medium yellow & 57 to 57 ELEY. H QU V DEPTH BLOWS T/LF. N DEPTH BLOTS TILF. & DEPTH BLOWS T/S.F. S round Surface IDENTIFICATION 416,8 0 47 47 47 70 50 22 Ground Surface Cinder, to 1 and limestone. coarse Medium to very dense gray fine to coarse Sand, trace slat, clay and small gravel. silt, Miscellaneous brick. fine Sand, 50 25 F111 sand & trace. Loose miscellaneou اظيليايانا limestonsilt. 27 yellow F111 goerse and Cragrents brown .8z 30 Sand, 55 511e. trace дгау 10 4 = 23 clay silt. miscellanen and fine to 60 63 Medium gray fine to coarse Sand, with small gravel and silt. F111 \*\*\*\* 1,1 60 22 gray fine to coerse Sand. trace very Brown very fine fine coarse 15 9 15 5 Loose to sedium gray fine to coarse Sand, trace shell gravel and silt. Boring stopped by 31 Sand, fine Dense gray fine Sate trace organic matte 65 301 WATER LEVEL \_13.0 trace Silty Very loose to stiff yellow trows gray clayer Silt. small 20 yellow 70 45 Sand and crave) TATY brown 20 and decse Dense yellow and brown fine Sand, some silty clay.
Dense to medium brown fine to trace fige Send. Redium brown very fine send, some silt. 392.6 gray fire silt. 25 40 25 13 jand, fine to 25 65 Medium 388.8 coarse silt. Send. 27.4 V medium
Sand,
trace
silt
und
organic
natter
noted.
Kedium
dense
brown
and
gray
fine
to
coarse
Sand,
trace
silt,
some
small
to
large
grayela
Medium 10 14 30 : 59 trace fine 385.3 An. 1: fine Sond. Some 21 80 28 Send. gravel 15 12 381.3 35 trece silt dark gray Silt, trace very fine sand. elit. 32.0.85 41 inring stopped by 375.3 fine to coarse Sand, truce small Ledium dense gray 45 dense 45 lc fine STATE OF ILLINOIS gray DEPARTMENT OF PUBLIC WORKS & BLDGS. (continued DIVISION OF HIGHWAYS POPLAR STREET BRIDGE APPROACHES BORING LOGS TYPE FAILURE

B - BULGE

S - SHEAR

E - ESTIMATED VALUE F.A.I.RT. 70 ST. CLAIR CO. SECTION 82-3HVB H. W. LOCHNER, INC. ENGINEERS CHICAGO, ILLINOIS SHEET

0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24

COUNTY TOTAL SHEET NO.

SECTION

SECTION COUNTY TOTAL SHEET NO. ROUTE NO. F. A. I. - 70 82-3HVB ST. CLAIR 289 259 FED. ROAD DIV. NO. 4 | ILLINOIS | PROJECT IDENTIFICATION 17 (continued) gravel and silt. 364.9 55 57 Dense brown fine to medium Sand, trace small gravel, cmatter noted. 356.460 40 Boring stopped by Inspectorl WATER LEVEL 39.5 21 STATE OF ILLINOIS

CHICAGO. ILLINOIS

224or24

BORING No. S-148 BORING No. S-149 BORING No. S-150 ELEV. H QU V ELEV. H QU V DEPTH BLOWS T/S.F. S ELEV. N QU V IDENTIFICATION (continued) Ground Surface 413.8 0 47 26 50 42 Ground Surface 12 Ground Surface (continued) 11.0 -\$09.5 - 4 \$ 4 Cinders. Crushed limestone Fill dense Labolin Malabalan Sand, Cley, and miscellaneous Fill brick. CO4 784 50. 34 clay. .ine Sand, Very loose brown very fine Sand, some silt. Medium brown very fine silty Sand \_5\_11 37 55 37 sand, to ..... - 11 concrete medium silt, Medium brown very fine Sand and Silt 55. 32 Sand, 10 5 10 13 27 miscellaneous 10 24 organic Medium gray Fill mtter Boring stopped by 153.8 60 58 fine to coarse \*\*\*\*\* LEVEL 38.0 Sand. Medium 15 16 Medium 15 6 \_ 28 trace brown silt. 14 fine **=** 10 Dense brown Sand gray 394.9 and 2012 fine to gray Silt fine coarse Sand, 25 16 25 12 dense brown and gray fine Sand, some silt, trace organic matter seams. 5000 to \_ 28 75 30 gravel, 30 25 30 26 30 32 coarse trace 27 trace silt. 39 \_\_ 22 organic matter 532,5 80 41 soring stopped by Inspector. 23 Send, Ned1um 35 26 35 33 35 31 dense VATER LEVEL 36.0 6797 fine ) — 22 — 22 trace \_\_ 26 Dense brown fine to coerse Sand, trace silt. Sand, trace 40 23 ₫ 36 40 40 silt. silt. 18 ] 31 Medium brown fine to coarse Sand, truce small (continue 16 Dense gray 45 17 45. 21 15 20 Hedium fine DEPARTMENT OF PUBLIC WORKS & BLDGS. (continued) (continued) DIVISION OF HIGHWAYS POPLAR STREET BRIDGE APPROACHES BORING LOGS TYPE PAILURE B - BULGE S - SHEAR E - ESTIMATED VALUE QU - UNCONFINED COMPR STRENGTH W - WATER CONTENT % OVEN DRY WEIGHT F.A.I.RT. 70 ST. CLAIR CO. SECTION 82-3HVB SHEET H. W. LOCHNER, INC. ENGINEERS

F.A.I.- 70 82-3HVB ST. CLAIR 289 FED. ROAD DIV. NO. 4 ILLINOIS PROJECT BORING No. S-153 BORING No. S-152 BORING No. S-151 DEPTH BLOWS T/S.F. S PLEY. N QU . -IDENTIFICATION round Surface 411.6 0 Ground Surface
Cindere,
brick,
stone,
send Loose gray fine to coarse <u>Sand</u>, some silt, organic matter with decayed wood. 47 21 dense Ground Surface Medium Miscellaneous gray Topsoil and
miscellance
fill
Very
losse
brown
clayey
Silt
Stiff
brown
clayey
Silt
trace
fine
sand F111 r.dense gray fine to coarse Sand, Jme silt, trace esall gravel. 50. 21 Medium gray fine to coarse Sand, trace silt and smell gravel. 60 22 TA088 5, 5 6 6 5 9 5 2) - 62 - 62 brown 65 coarse 55 33 clavey 55 22 Sand Fill edlum Silt, 10 9 brown 11 10 12 Kedium gray, silty clay, trace very fine Sand. Loose brown very fine Sand, smell clay & send, ₫, gravel, 62 50 Dense gray fine 70 silt. trace Medium brown fine Sand, trace silt, organic matte noted. 15 Loose silt. coarse Sand, trace small gravel and silt. 15 10 Dense gray fine 29 brown prown Medium very Medium brown very fine milty Sand Medium brow very fine Sand some milt. Redium gray silty fine 65 38 65 fine trace fine end, 20 dense Sand 803. 31 fine to medium clay wa Medium dense gray fine - Note-Boulses :11: 20 26 edius. fine to coarse Sand, some troce silt and clay. Loose gray very fine sand, some silt, organic matter noted. 25 14 atlt. 389.125 9 25 20 35 385.6 sone small gravel, trace silt and organic matter noted. 339.2 hedium dense gray medium to coarse sand, trace salt and scall gravel 22 75 Jend. 336.3 7 22 23 Very dense gray fine to coarse Sand, and small Send. and ..... trace 43 gray 80 22 80 silt. milt 331.7 35 31 Very dense gray coarse sand, trace silt, some small graye small 35 55 331.1 70 silt. Boring stopped by Inspector. 375.6 Send, Dense brown fine to coarse Sand, trace small gravel, trace 329.2 Vadtus 33 gravel. trace brown 85 Medium dense gray medium to coarse band, trace silt and small gravel. 25 19 fine silt. 40 45 22 Dense gray fine Sand, trace silt, and organic silt. 26 Send organic matter noted .... Medium 91 40 gray silt, Hedium brown fin to course <u>Sand</u>, some small gravel, trace silt. Boring stopped by Inspector. and trace silt. 45 25 WATER LEVEL 34 since gravel. 20.2 52.6 oring stopped by STATE OF ILLINOIS
DEPARTMENT OF PUBLIC WORKS & BLDGS Medium gray fine Sand, trace silt. WATER LEVEL -DIVISION OF HIGHWAYS Very dense gray fine to coarse 50 97 Dense gray fine to coarse <u>Sand</u>, small grave, trace silt and organic mattar noted. POPLAR STREET BRIDGE APPROACHES H - STANDARD PENETRATION TEST HUMBER - BLOWS TO DRIVE 2" O.D. SPLIT SPOON SAMPLER 12" WITH 1407 WT. FALLING 30" BORING LOGS F.A.I.RT. 70 ST. CLAIR CO. SECTION 82-3HVB 55 26 SHEET H. W. LOCHNER, INC 225or241 CHICAGO. ILLINOIS

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24

COUNTY TOTAL SHEET NO.

SECTION

COUNTY TOTAL SHEET NO. SECTION F. A. I. - 70 82-3HVB ST. CLAIR 489 261 FED. ROAD DIV. NO. 4 | ILLINOIS | PROJECT BORING No. S-154 BORING No. S-155 BORING No. S-156 ELEY. H QU W BEPTH BLOWS TOLF. & DEPTH BLOWS T/S.F. S Ground Surface (continued) IDENTIFICATION 4Z 24 Ground Surface 413.2 0 47 412.9 0 47 9 gravel. trace Topsoil. Sand. 4.2 miscellaneous Fill Sadt um miscellaneous Fill gray 50 25 Madtum 50 20 Medium brown Clay, some gray to coarse Sand, some small gfevel trace silt. 5 15 2.5 18 5 fine to - ay. 28 359.5 - 26 Sand, 2.0 11 ense gray Fine Medium gray coarse Sand little Madtum medium hand little edit. trace clay. Kedtum 410 10 26 20 29 50 25 60. 24 1. silt. gray brown Medium gray fine to medium 60 38 fine 15 11 15 10 very = 23 fine Sant. - " - " gray medium dine Sedien 65 to er-y 20 15 20 10 Sand. 20 = 29 17 Sand, Sand, trace nedium 70 Sand. 11 silt. trice 25 13 25 19 smell. 24 small\_ gravel. 24 75 18 75 54 gray fine to 10. 11 Medium gray medium Sand. 30 13 29 Kedium 31 28 gr.vel medium silt. dense Sand, very tense gray fine to - 13 Very dense gray medium sand, and some gravel with trace silt. trace silt. 80 105 379.5 80 63 gray Boring stopped by Inspector. Dense brown medium Send, trace silt. Sand, PATER LEVEL \_28.5 fine and: 35 33 35 25 Sand. soring stopped by Dense -44 36 trace gray 85 52 medium Sand, silt. Sand. 372.40 37 54 trace Medium fine to coarse Sand, trace silt, some small 25 90 48 Medium gray fine to coarse gravel, -5. 11 45 13 45 14 trece STATE OF ILLINOIS DEPARTMENT OF PUBLIC WORKS & BLDGS. DIVISION OF HIGHWAYS 18.3 95 25 Boring stopped by Inspector. POPLAR STREET BRIDGE APPROACHES PATER LEVEL 36.0 QU - UNCONFINED COMPRESSIVE STRENGTH W - WATER CONTENT S OVEN DRY WTIGHT TYPE FAILURE

B - BULGE

S - SHEAR

E - ESTIMATED VALUE BORING LOGS F.A.I.RT. 70 ST. CLAIR CO. SECTION 82-3HVB SHEET H. W. LOCHNER, INC. CHICAGO. ILLINOIS

