

Abbreviated Structure Geotechnical Report

Original Report Date:	2-22-2013	Proposed SN:	027-0103	Route:	IL 54 (FAP 71)	
Revised Date: 4-12	2-2013	Existing SN:	027-0077	Section:	(115BR) BR	
Geotechnical Engineer: Terry McCleary, McCleary Engineering					Ford	
Structural Engineer:	Joseph Lowrance	Farnsworth Gr	oup	Contract:	66943	

Indicate the proposed structure type, substructure types, and foundation locations (attach plan and elevation drawing): Single span structure, 91.6 ft. in total length from back to back of abutments. The superstructure will be supported by intergal abutments with no piers. Six piling are estimated for each abutment. Because of the differing soil strengths found in the two sets of borings a test pile is strongly recommended for each abutment. Abutment loadings are anticipated to be near 1600 kips and the foundation width near 35 ft.

Discuss the existing boring data, existing plans foundation information, new subsurface exploration and need for any additional exploration to be provided with SGR Technical Memo (attach all data and subsurface profile plot): Two borings were taken for the existing structure in 1980. Two new borings were taken for the proposed structure in 2009. Both sets of borings show stiff to hard cohesive soils however the 2009 borings show higher unconfined compressive strength. The existing structure is a single span with driven metal shell supported abutments. See the attached boring logs and test pile data.

Provide the location and maximum height of any new soil fill or magnitude of footing bearing pressure. Estimate the amount and time of the expected settlement. Indicate if further testing, analysis, and/or ground improvement/treatment is necessary: Approximately 2 ft. of fill is to be placed at the abutments. The estimated additional wt. of 240 psf from this fill is not expected to have an adverse effect on existing soils as they are of relatively high shear strength and moderate moisture content. Using a strength limit state analysis, the resulting factored footing pressures are approx. 6.0 tsf using a $\varphi = 0.5$. Should a spread footing be desired a more detailed analysis is recommended during the design phase of the project where the size of footing is known and a service limit analysis can be performed.

Identify any new cuts or fill slope angles and heights. Estimate the factor of safety against slope failure. Indicate if further testing, analysis or ground improvement/treatment is necessary. Two feet of new fill and pavement will be added to the current grade while maintaining a 2:1 (H:V) end slope on the stream side of the abutments. The factor of safety of the proposed end slope is 4.9 for short term undrained conditions. Long term, drained conditions resulted in a factor of safety of near 1.5. A small fraction of the undrained cohesion is required to obtain this value. The existing slopes are currently considered to be in a drained condition and show no signs of any problems.

Indicate at each substructure, the 100-year and 500-year total scour depths in the Hydraulics report, the non-granular scour depth reduction, the proposed ground surface, and the recommended foundation design scour elevations. No scour was accounted for at the abutments per policy. Scour depths are presumed to be at the bottom of the proposed abutments, 748.42 ft. Elev at the south abutment and 748.45 ft. Elev at the north abutment.

Determining the seismic soil site class, the seismic performance zone, the 0.2 and 1.0 second design spectral accelerations and indicate if that the soils are liquefiable. Using the 2009 borings the seismic site class is C with an SPZ=1, SDs=0.146 and SD1=0.084. Liquifaction is not a concern in a site performance zone, SPZ = 1.

Confirm feasibility of the proposed foundation or wall type and provide design parameters. Attach a pile design table indicating feasible pile types, various nominal required bearings, factored resistances available and corresponding estimated lengths at locations where piles will be used. Provide factored bearing resistance and unit sliding resistance at various elevations and confirm no ground improvement/treatment is necessary where spread footings are proposed. Estimated top of rock elevations as well as preliminary skin friction and end bearing values shall be indicated when drilled shafts are proposed. After discussing with BBS and reviewing the pile driving data of the existing structure, the author believes a metal shell pile may be the most appropriate pile type for this project. The high Qu values at relatively shallow depth were initially a concern but the N-values are relatively low and the existing structure is supported on driven metal shell piling. Because the pile driving records of the existing structure show the metal shells were driven safely, without damage to the pile, the author recommends a Metal Shell be used. See attached estimated pile length design table. Per ABD 12.3, the MS 14 and H-piling are allowed for integral abutments. Assumptions include: Bottom of Abutment elevation = 748.42 for the South Abutment and 748.45 for the North Abutment.; no geotechnical losses accounted for; and a 2.0 ft. pile embedment into the abutment is presumed.

Calculate the estimated water surface elevation and determine the need for cofferdam(s) and seal coat. There will be no need for a cofferdam as there will be no in stream pier work.

Assess the need for sheeting/soil retention versus using a temporary construction slope and provide recommendation for the most feasible option. At this time the author anticipates the structure to be constructed under closed road conditions therefore no sheet piling will be needed at a stage line. There will be no piers and therefore no in stream work is anticipated.



May 11, 2013

Mr. Paul Loete
Illinois Department of Transportation
Attn. Steve Ferguson
700 East Norris Drive
Ottawa, IL 61350

RE: Geotechnical Memorandum IL 54 (FAP 71)
Section (115BR)BR
Ford County
SN027-0103 (Proposed)

Mr. Ferguson:

Please find attached the revised Pile Length table resulting from the possible need to precore the piling at the north abutment to facilitate the use of an integral abutment at this structure. Using the 1980 boring logs and pile driving data this extra effort is not needed and was not included in the original approved SGR. However, using the 2009 boring logs the north abutment soils are characterized to be very stiff to hard with unconfined compressive strengths by RIMAC method between 3.0 tsf and 5.8 tsf.

We estimate the expansion of the bridge to be in the realm of 0.3 inch. The Bridge Office requested the SGR to recommend metal shell piles. With this recommendation the only metal shell pile that should be used is the 14 inch diameter. With this size of pile and the limited sizes of commonly available augers to drill the pre-core holes we recommend the pre-core hole to be 18 inch diameter. The depth of pre-core was presumed to be 10 ft. below the bottom of the abutment elevation. The resulting bottom of the pre-core elevation is 738.42 ft.

This pre-core is only required at the north abutment. At this time the Bureau of Bridges and Structures asks that the pre-core holes be filled with bentonite and not loose sand. This can occur prior to or after driving the piles. If this is done after the piles are driven the bentonite may be placed in flowable slurry or in dry form. If the dry form is chosen the benonite should be in a fine powder form.

With this change to the pile table we took the opportunity to modify the soil profile, shifting the logs down relating the elevations of the bottom of the abutment with the top of boring elevations.

If you have any questions please don't hesitate to contact me at (815) 780-8486 or via email at terry@mcclearyengineering.com. It has been a pleasure working with you on this work project.

Sincerely,

Terrence L. McCleary

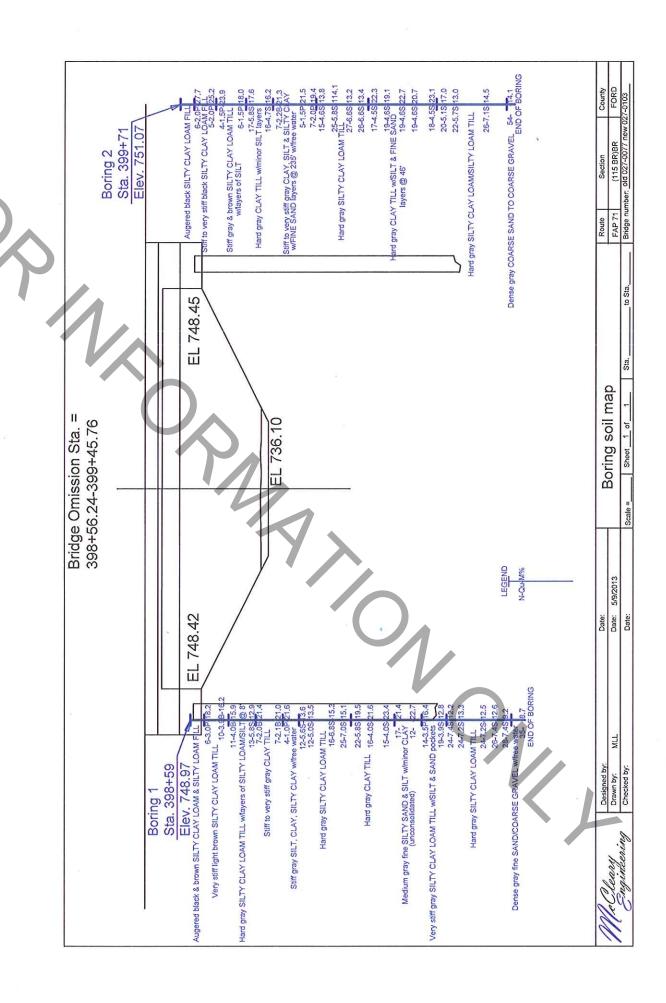
McCleary Engineering

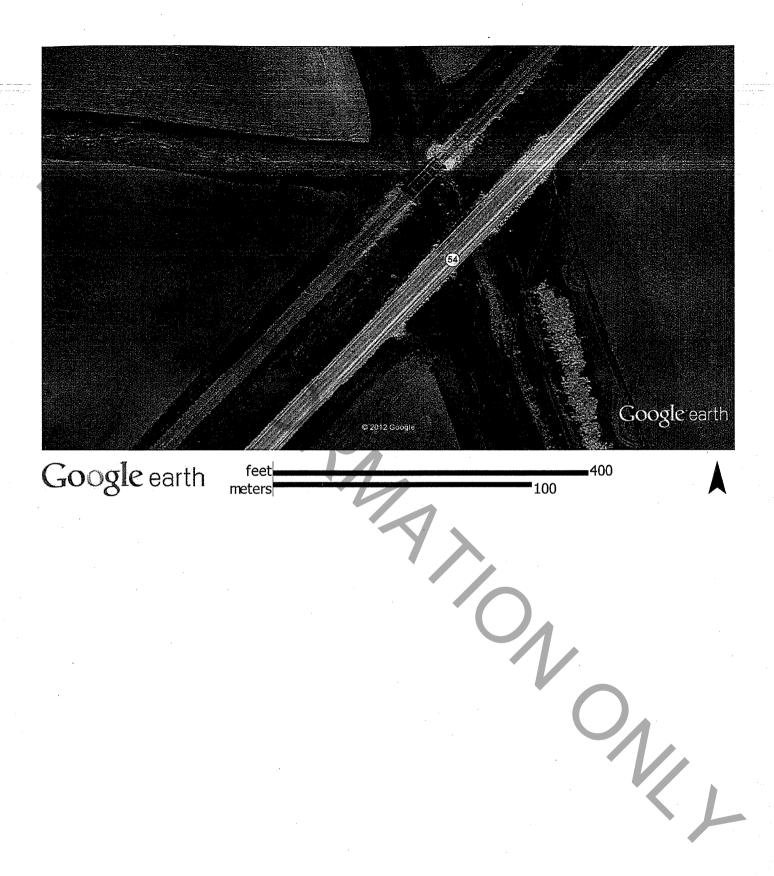
PILE LENGTH TABLE

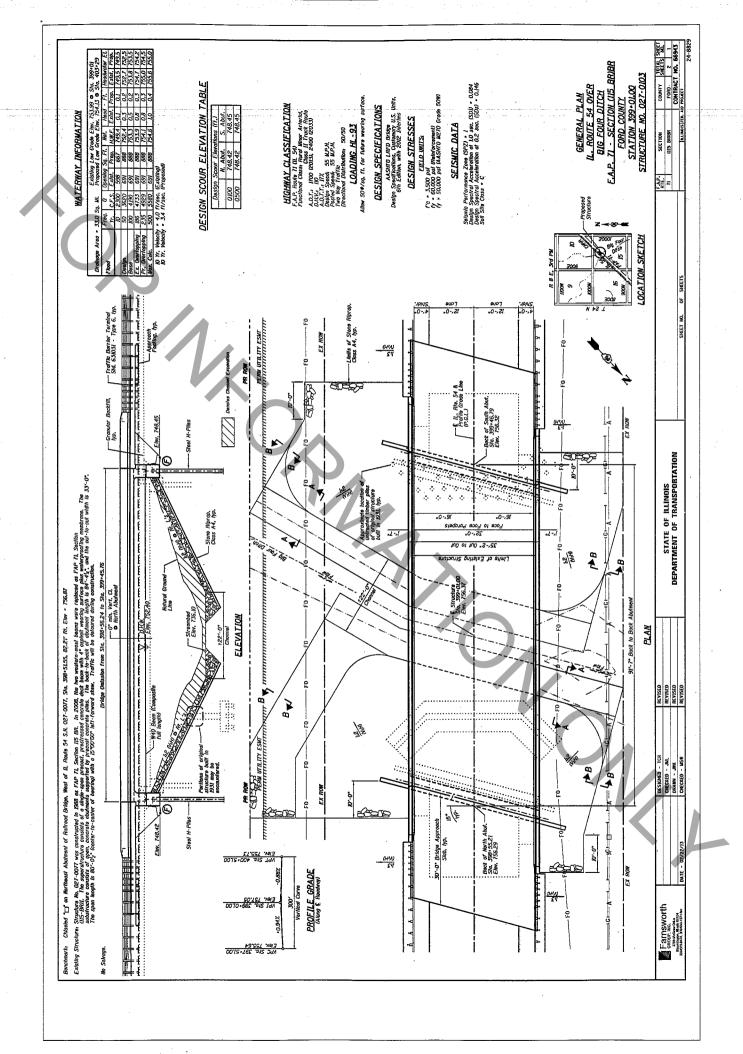
	outment, Using B			South Abutn	nent, Using Borin	g B-2 (2009)
(2009) Pre-core*	k				
Nominal	Factored	Estimated		Nominal	Factored	Estimated
Required	Resistance	Pile Length		Required	Resistance	Pile Length
Bearing (KIPS)	Available	(Ft.)		Bearing (KIPS)	Available	(Ft.)
	(KIPS)				(KIPS)	
100000	14 with 0.25" w				MS 14 with 0.25"	
233	128	28		222	122	24
258	142	33		305	168	29
385	212	39		334	184	33
413	227	48		413	227	39
MS	14 with 0.312" v	vall		MS	14 with 0.312" v	vall
364	200	41		329	181	31
364	200	46		365	201	36
454	250	51		425	234	41
513	282	56	**	513	283	47
	HP 10x42				HP 10x42	74
211	116	46		205	113	33
272	150	51		240	132	38
308	170	56		273	150	43
335	184	62		335	185	49
	HP 12x53				HP 12x53	
220	121	36		117	97	24
219	121	41		240	132	29
240	132	44		257	141	33
326	179	48		299	165	38
364	200	53		339	187	43
418	229	62		418	229	49
120	HP 12x63				HP 12x63	
368	202	53		323	178	41
413	227	58		372	204	46
461	253	65		430	237	51
497	273	71*		497	273	57
-157	HP 14x73	, -		13.	HP 14x73	
295	162	44		291	160	29
408	224	48		318	175	33
429	236	51		368	203	38
481	265	56		415	228	43
503	276	60		487	268	48
578	318	67		578	318	54
376	HP 14x89			370	HP 14x89	
435	239	51		457	251	46
509	280	60		530	292	51
606	334	70		595	328	56
		80*		705	387	60
705	387	80"	<u></u>	/05	30/	UU -

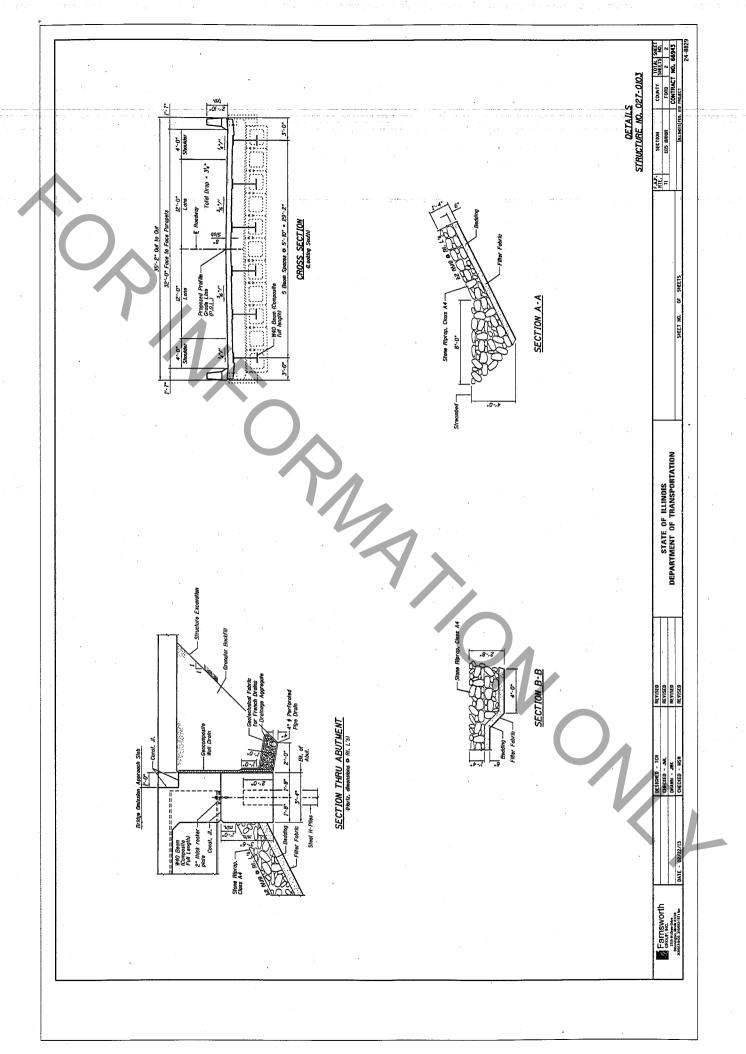
^{*}Beyond the end of the boring.

^{**}North Abutment is to be pre-cored to an elevation of 738.42 ft. The diameter of pre-core is 18 in.









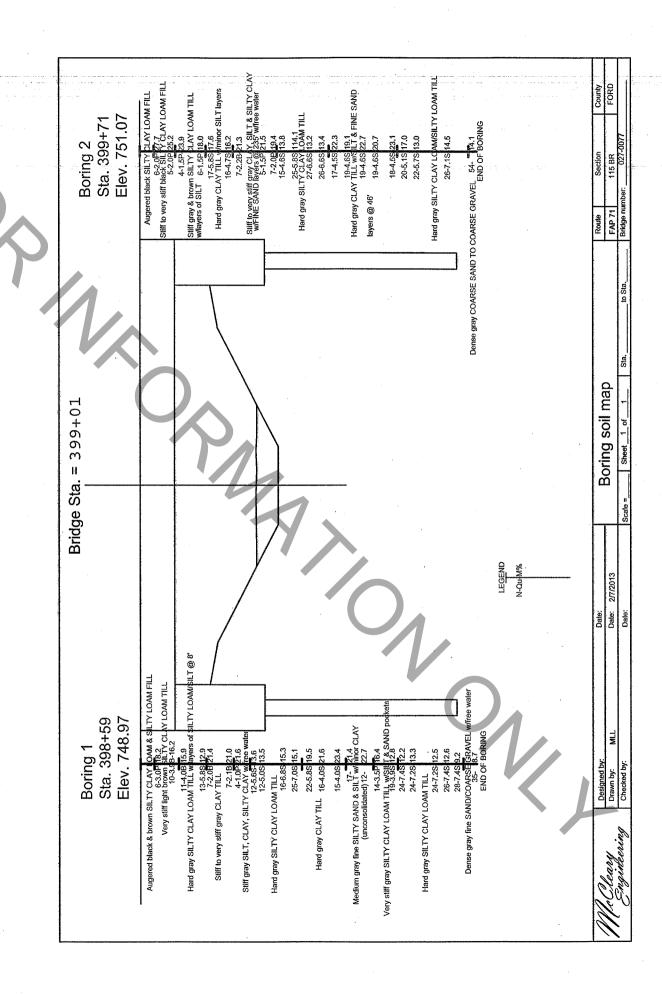
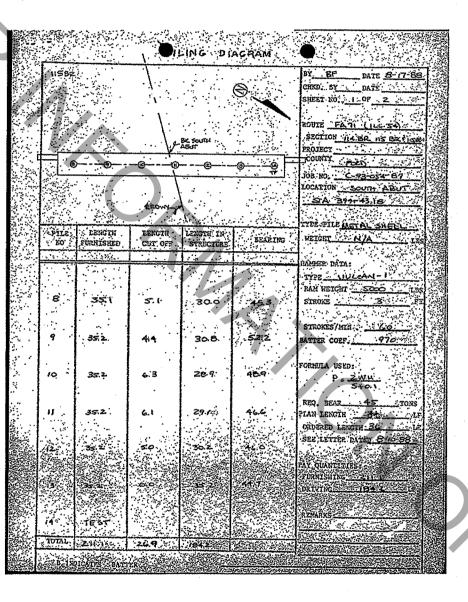


Table 1: PILE LENGTH TABLE 027-0103

North Abu	tment, Using (2009)	Boring B-1		South Abu	itment, Using (2009)	Boring B-2
Nominal	Factored	Estimated		Nominal	Factored	Estimated
Required	Resistance	Pile Length		Required	Resistance	Pile Length
Bearing	Available	(Ft.)		Bearing	Available	(Ft.)
(KIPS)	(KIPS)	(ГС.)		(KIPS)	(KIPS)	(1 6.)
	14 with 0.25" v				MS 14 with 0.25	
220	121	van 22		222	122	24
294	162	27	***************************************	305	168	29
342	188	32		334	184	33
413	227	38		413	227	39
	227 L4 with 0.312"				14 with 0.312"	
342	188	waii 32		329	181	31
378	208	37		365	201	36
458	252	42			234	
513	282			425		41 47
212	HP 10x42	48		513	283 HP 10x42	4/
228	126	37		205	T	33
232	127	42		203	113	
		42			132	38
264	145			273	150	43
335	184	53		335	185	49
227	HP 12x53	27		HP 12x53		
269	125	32		-	97	24
284	148 156	37		240	132	29 33
284	156	42		257 299	141 165	38
327	180	47		339	187	43
418	229	53		418	229	45 49
410	HP 12x63	33		410	HP 12x63	43
330	182	47	· .	323	178	41
412	227	52		372	204	46
456	251	57		430	237	51
497	274	62*		430	273	57
737	HP 14x73	02		437	HP 14x73	37
311	171	29		291	160	29
326	179	34		318	175	33
342	188	42		368	203	38
399	220	47	· · · · · · · · · · · · · · · · · · ·	415	203	43
505	278	52		413	268	48
578	318	58		578	318	54
5,0	HP 14x89	- 50		376	HP 14x89	
512	281	52		457	251	46
565	311	57		530	292	51
586	322	61		595	328	56
J00	J & L	0,1		رور ا	1 320	

^{*}Beyond the end of the boring.

LING DIAGRAM ĆHKO. BY .. DATE 127-00 77 (Mess) SHEST NO. Z OF ROUTE SECTION NA BE PROJECT COUNTY JOB NO. C-93-084-6 LOCATION N ABOT Recd Br. Off. Aug. 24, 1989 . Length Fernished COT OFF PILE NO LENGTH IN STRUCTURE BEARING RAN WEIGHT SOOS TEST STROKES/MIN DATTER COEF 970 40.1 88 FORMULA USED: 40.1 78 32:3. 47.1 REQ. BEAR 45 40.1 47.1 Plan Length 41 ORDERED LENGTH 40 SEE LETTER DATER PAY QUANTITIES 40.3 + 13.6 Furnishing 12.74 40,1 +18.1 HID WITE



ED-757 (Rev. 2-73)

STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION

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Test Pile Driving Record

was driven 398-64.66 15.06 Lt. C.L. (N. Ab Elev. from which pile was driven 193.9

		47 4			a salagae
Elev.	Feet. Below Cut Off	Blows Per Foot	Blows Per Minute	Bearing In Tons	Remarks
180.88	14	, . ૪ √		71	
179.88	. 15	6.		7.1-	Completely
178.88	16	*			* Stop for splice
177.88	. 17	9.		. 10.5	
176.88	18	10		11.5	P=2WH/S+0.1
475.88	19	12	56	13.6	
174.88	. 20	13		14.7	Zana da Barana da Ba
173.88	21	16	* '	17.6	Date Driven:
172.88	22	17		18.6	8-8-88
171.88	23	23	•	. 24.1	
170.88	24	30	60	30.0	Precored 5 ft.
169.88	25	44		40.2	Very little resistance
168.88 -	26	61	·	38.2	encountered 5° to 14°.
167.88	27 .	47	33	. 42-2	\
165.88	28 .	49	. 60,	43.5	, Witnessed by:
165.88	. 29	.49	1916	43.5	Mike Watterson, R.T. &
164.88.	.30	54: 34	1400 N	46.6	Bruce Fuoss
163.88	31	53	Sec. 3. 1	746.0	SECTION OF THE RESERVE
162:88	32	∴56₹	A 1988	22.47 VZ (25)	Valenta and an
161:88.	公公33 333	:360 X	487494	65010	
160.88	:34	61	-	7:30:6	
159.88	. 1:°∙35. >	- 67	60 :	53.7 %.*.	CONTRACTOR OF STREET
158.88	36	. 62	4.0	57.4	C 00080.20 NAME (0.0.1)
157.88	37	. 57 55	JAMAS	48:3	1923 S.
.156.88	·*.38 · .÷.:	259	(A) (A)	64 49 4 · ·	

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STATE OF ILLINOIS

DEPARTMENT OF TRANSPORTATION

Test Pile Driving Record

Project	Type & Weight of Hammer
Route	The state of the s
Section	Length of Fall
County	Type of Pile
Station of Structure	Required Bearing
	Elev. Top Pile
	Elev. Tip of Pile
	Elev. Cutoff
Station location at which pil-	
es driven	Grierad Tanoth

Elev.	Feet Below Cut Off	Blows Per Foot	Blows Per Minute	Bearing In Tons	Remarks
.155.88	39	64	3.5074	52.2	
.154.88	40	68		54.3 :-	
153.88	41	717.	17 17	.55.8	
152.68	42 -	78 ,		59.1	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
151.88	43	79		59.5	
150.88	44	61 😁	50	50.6	
149.88	45	52 .		45.3	/
146.88	46 .	49	-1	43.5	
147.88	47	57	60.	48.3	
146.88	48	66		53.2	1
145.88	. 49	57		48.3	
144.88	50 ·	63		51.6	
143.88	51	46 .		41.6	
142.88	52	58	-	48.9	A 10
141.88	53 :	93		65.5	
140.88	.54	78-		.59.1	
	34 - 34 - 3	7 727.	V 1831	The second second	
31.012	and the second	15.50	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	5. 127 1 3. 34 A	the state of the second second second second
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	W. T. & 30.44	47.50	19 19 19		The state of the s
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	100	7.3.3	5/2/	6 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	
		1.58	16-9122	Man visi	
	S-12 782	. 72	The street of		Control of the contro

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STATE OF ILLINOIS

DEPARTMENT OF TRANSPORTATION

Test Pile Driving Record

Project	ACERF-71(26).		Type & Weight of Hammer
Route	FA 71 (111:54)		Vulcan 1 (Air) - 5,000 lbs.
Section	1148R. (1158R) -1158R-1		Length of Fall 3 ft.
County	Ford	•	Type of Pile Metal Shell
Station	of Structure 399401	•	Required Bearing 45 Tons
			Blev. Top Pile 212.88
		•	Elev. Tip of Pile 138.08
			Elev. Cutoff 194.98
Station .	location at which pile	2.0	Estimated Plan Length 41
	200-27 7A 15 0CL LE C'L		

Station location at which pile Betimated Plan Length 4 was driven 399437.34 15.06 Lf.C.L. (S. Abut.) Ordered Length 36 Elev. from which pile was driven 194.0

Elev.	Feet Below Cut Off	Blows Fer Foot	Blows Per Minute	Bearing In Tons	Remarks
189.98	5	3	100	3.7	
185.98	6	. 2		-2.5 .	
187.98	7	3		3.7	P=2WH/S=0.1
186.98	8	^4		4.8	
185.98	'9	4		4.8	
184.98	10	4		4.8	Date Driven:
183.98	11	4		4.6	6-8-88
182.98	12	3		3.7	
181.98	13	4		4.8	Precored 5 ft.
180.98	14	4		4.8	
179.98	15	•		*	* Stopped to splice lengths
178.98	16	11		12.6	
177.98	17	32	a est alla	13.6	
176.98	18	14.	٠.	15.7	Witnessed by:
175.98	19	.14	56	15.7	Mike Watterson, R.T.
174.98	20	- 37	1	18,6	Bruce Fuoss
173.98	21	20		21.4	
172.98	- 22	- 26		.26.7	M. 数据数据。10.19 · 20.17 (20.5)
171.98	23	.43	1	39.6	· 电影響為不同。 如果 5人。
170.98	. 24	40	1 200	37/5/3	ASSESSED TO THE PARTY OF
169.98	: 25	43		39.6	TO COMPANY TO THE STATE OF THE
168,98	2.6	52	60	: 45,3	
167.98	27	49	100	43.5	
166.98	28	49		43.5	A Company of the Comp
165.98	29	- 51	1 : 1 : 1	44:7	PART STAR Same LARGE

BD-757 (Rev. 2-73)

STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION

Test Pile Driving Record

Project Route	Type & Weight of Hammer
Section County	Length of Fall
Station of Structure	Required Bearing Elev. Top Pile Elev. Tip of Pile
Station location at which pile	Elev. Cutoff Estimated Plan Length
was driven Elev. from which pile was driven	Ordered Length

Elev.	Feet Below Cut_Off	Blows Per- Foot	Blows Per Minute	Bearing In Tons	Remarks
164.98	30	- 53		46.0	
163.98	31	55	17.7	47.1	I was bringer to a least
162.98	32	58	47.17	48.9	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
161.98	33	54	. 60	46,6	
160.98	34.	53 .		46.0	
159.98	35	. 51		46.7	//
158.98	36	50		44.1	The state of the s
157.98	37	48		42.9	
156.98	38	47		42.2	
155.98	39	45		40.9	
154.98	40	42		38.9	
153.98	41	41	-60	38.2	
152.98	42	. 39		36.8	
151.98	43	38		· 36.1	
-150.98	44	39	3.	36.8.	
149.98	45	- 58	V/	36.1	
/148.98.	- 46	1:38 s	10 10	36.1	
147.98	-,- 47	35	7 A	33:9:	
146.98	48.	36	30.00	34.6	
145:98	-3. 49	35	34.00	در 33 وا 33 دري	
144.98	. 50	3A .	No. 34	0371	Stopped driving to aplica extra
143.98:	5 - 51	.35	3552	33.9	in the state of th
142.98	52	37	F4550	35.4.	7.3- 12.5
141.98	53:	.37	Section.	35.4	The Court of State State of the Court of the
140.98	5h :-	33 %	Contract	32.4	

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STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION

Test Pile Driving Record

Project	Type & Weight of Hammer_
Route	
Section	Length of Fall
County	Type of Pile
Station of Structure	Required Bearing
	Elev. Top Pile
	Elev. Tip of Pile
	Elev. Cutoff
Station location at which pile	Estimated Plan Longth
was driven	Ordered Length
Klay from which mile was driven	

Elev.	Feet Below Cut. Off	Blows Per Poot	Blows Per Minute	Bearing In Tous	Remarks
139.98	. 55	\$2		45.3	
138.98	56	. 64	27/	52.2	
137.98	57	168 🖫	7.77		Stopped driving.
			Y: //		
	3.00			7	7/0
		-			
				//	
				7	
					// // // · · · · · · · · · · · · · · ·
			*	Not the Attack	
			11 (2.3		
7 33				3	STOLEN THE
t National	6 Buch	ra kilinga		2 22%	
		2.3°2-13.	S. S	re a participa	
	44:36.1.5%	Contract		Service Service	
	200		Annual Control	2 / 1 / 1 / 1 / 2 / 2 / 2 / 2 / 2 / 2 /	
CONTRACTOR	n		14-201-26		
	** 1 '9.3				
4. A		**************************************	123-4754	er egany Alvey Calabara a Nash	
	erior Wasaa	er en en en en en	Super Super Super		



Page $\underline{1}$ of $\underline{2}$

Date 8/25/09

DESCRIPTION IL 54 over Big Four Ditch, 7.6 miles North of IL 9 LOGGED BY L. Myers FAP 71 (IL 54) SECTION LOCATION N 1/2, SEC. 15, TWP. 24N, RNG. 8E 115 BR COUNTY **DRILLING METHOD** HAMMER TYPE **CME Automatic** Hollow Stem Auger U U D В М D M Surface Water Elev. 736.81 ft STRUCT, NO. 027-0077 (Exist.) Ε С 0 E L C 0 L 399+10 Stream Bed Elev. Station 736.21 ft Р 0 S Ρ 0 S 1 ı W S T W S T BORING NO. Groundwater Elev .: 1 (N.E. Quad.) Т Qu S Qu Н S Т Н First Encounter <u>709.0</u> ft <u>▼</u> Station 398+59 **Upon Completion** 729.0 ft ∑ Offset 31.00ft Lt. (/6")(%) (ft) (/6") (tsf) (%) (ft) (tsf) Ground Surface Elev. 748.97 After Hrs. Augered Black & Brown Silty Clay Hard Gray Silty Clay Loam Till 2 Loam & Silty Loam Fill 5 5.6 13.6 7 S Very Stiff Light Brown Silty Clay Loam Till 5 5.0 13.5 3 18.2 3.0 3 P 7 S 3 5 7 6.8 15.3 4 3.9 16.2 6 В 9 S 741.97 Hard Gray Silty Clay Loam Till with Layers of Silty Loam/Silt @8' 9 15.1 5 4.0 15.9 11 7.0 14 S 6 В 719.47 Hard Gray Clay Till 5 5 9 5.8 19.5 6 5.8 12.9 13 S 7 S 736.97 Stiff to Very Stiff Gray Clay Till 5 2 4.0 21.6 21.4 3 2.0 9 4 В S 2 23.4 3 2.1 21.0 6 4.0 S 4 В Stiff Gray Silt, Clay, Silty Clay with free water Medium Gray Fine Silty Sand and 6 Silt with minor Clay 21.6 7 21.4 1 1.0 (unconsolidated) 10 3 Ρ **728.97**∇*-*20



Page <u>2</u> of <u>2</u>

Date 8/25/09

ROUTE FAP 71 (IL 54) DESCRIPTION IL 54 over Big Four Ditch, 7.6 miles North of IL 9 LOGGED BY L. Myers SECTION 115 BR LOCATION N 1/2, SEC. 15, TWP. 24N, RNG. 8E COUNTY **DRILLING METHOD CME Automatic** Hollow Stem Auger **HAMMER TYPE** U u M В D В STRUCT, NO. 027-0077 (Exist.) Surface Water Elev. 736.81 ft E С 0 E C L L 0 Station 399+10 Stream Bed Elev. 736.21 ft Р 0 S P 0 S 1 Т W S T W S BORING NO. 1 (N.E. Quad.) Groundwater Elev .: н S Qu T S Qu T Н Station 398+59 First Encounter 709.0 ft **▼** Offset 31.00ft Lt. 729.0 ft ∑ **Upon Completion** Ground Surface Elev. __ (ft) (/6")(tsf) (%) (/6")(%) (ft) (tsf) 748.97 After Hrs. ft Medium Gray Fine Silty Sand and 4 Dense Gray Fine Sand/Coarse 10 Silt with minor Clay Gravel with free water (continued) 5 22.7 17 8.7 (unconsolidated) (continued) 7 18 687.47 **End of Boring** Very Stiff Gray Silty Clay Loam Till with Silt & Sand pockets 3.5 16.4 6 8 P 6 8 3.9 12.8 11 S 701.97 Hard Gray Silty Clay Loam Till 6 9 7.4 12.2 15 S 6 9 7.2 13.3 15 S 8 12.5 10 7.2 14 S 9 11 7.4 12.6 15 S 10 11 7.4 9.2 17 S 689.97 Dense Gray Fine Sand/Coarse Gravel with free water



Page <u>1</u> of <u>2</u>

Date 8/31/09

ROUTE FAP 71 (IL 54) DESCRIPTION IL 54 over Big Four Ditch, 7.6 miles North of IL 9 LOGGED BY L. Myers SECTION 115 BR LOCATION N 1/2, SEC. 15, TWP. 24N, RNG. 8E COUNTY Ford **DRILLING METHOD** Hollow Stem Auger HAMMER TYPE CME Automatic U D В U М D М STRUCT, NO. 027-0077 (Exist.) Surface Water Elev. 736.81 ft Ε C 0 E L C 0 L 399+10 Station Stream Bed Elev. 735.61 ft P 0 Р 0 S S 1 W Т W S Т S BORING NO. 2 (S.E. Quad.) Groundwater Elev .: н S Qu Т Н S Qu Т Station 399+71 First Encounter <u>706.1</u> ft ▼ Offset 27.00ft Lt **Upon Completion** 733.1 ft ∑ Ground Surface Elev. (ft) (/6")(tsf) (%) (ft) (/6")(tsf) (%) 751.07 After Hrs. Stiff to Very Stiff Gray Clay, Silt & Augered Black Silty Clay Loam Fill wh Silty Clay with Fine Sand layers @ 2 1.5 21.5 23.5' with free water (continued) 3 Ρ Stiff to Very Stiff Black Silty Clay Loam Fill 2.0 27.7 3 2.0 19.4 3 3 P 4 Р 2 Hard Gray Silty Clay Loam Till 3 2 4.6 13.8 2.0 25.2 6 3 P 9 S 744.57 Stiff Gray & Brown Silty Clay Loam Till with layers of Silt 2 9 2 1.5 23.9 11 5.8 14.1 2 Ρ 14 S 10 2 1.5 18.0 12 6.6 13.2 4 P 15 S Hard Gray Clay Till with minor Silt layers 10 5 17.6 13.4 7 5.8 11 6.6 10 S 15 716.57 Hard Gray Clay Till with Silt & Fine Sand layers @ 46' 4 6 4.7 16.2 4.5 22.3 9 S 10 S Stiff to Very Stiff Gray Clay, Silt & Silty Clay with Fine Sand layers @ 3 6 23.5' with free water 3 2.2 21.3 8 4.6 19.1 4 В 11 S



Page $\underline{2}$ of $\underline{2}$

8/31/09

Date

ROUTE FAP 71 (IL 54) DESCRIPTION IL 54 over Big Four Ditch, 7.6 miles North of IL 9 LOGGED BY L. Myers SECTION 115 BR LOCATION N 1/2, SEC. 15, TWP. 24N, RNG. 8E COUNTY **DRILLING METHOD** Hollow Stem Auger HAMMER TYPE CME Automatic В u М D В М STRUCT. NO. 027-0077 (Exist.) Surface Water Elev. 736.81 ft E L С 0 E L C O 399+10 Stream Bed Elev. Station 735.61 ft P 0 0 S ı S 1 T W W S Т S BORING NO. 2 (S.E. Quad.) Groundwater Elev.: S Qu Т Т Н Н S Qu Station 399+71 First Encounter 706.1 ft **▼** Offset 27.00ft Lt **Upon Completion** 733.1 ft ∑ (ft) (/6")(tsf) (%) (ft) (/6")(tsf) (%) Ground Surface Elev. **751.07** Hrs. Hard Gray Clay Till with Silt & Fine Dense Gray Coarse Sand to 6 12 Sand layers @ 46' (continued) Coarse Gravel 9 4.6 22.7 21 14.1 10 S 33 689.57 End of Boring 8 4.6 20.7 11 S 6 4.5 23.1 9 9 S 704.07 Hard Gray Silty Clay Loam/Silty Loam Till 8 9 5.1 17.0 11 S 13.0 10 5.7 12 S 10 12 7.1 14.5 14

691.07 -60





Illinois Department of Transportation

Memorandum

To:

J. T. Rayburn

From:

R. H. Blasius

By: J. Jereb

Subject:

Foundation Boring Logs#

Date:

February 25, 1985

FA Route 71 Section 115BR Ford County P-93-048-79

We are transmitting the foundation boring logs for the proposed improvement.

This bridge is located on Illinois Route 54, 2.0 miles southwest of Melvin, Illinois.

WHB:si

cc: Barrientos & Assoc., Inc.

B. L. Hynd

Soils '

Attachment:

(2) Boring Logs

(1) Location Sketch

BRIDG	e i	FOL	INDA IL Ro	TIC otute	DN BORING	LCG Dato Ma	irch	6. 1	980	
OJECT FA 71					. Vermilion R.	Based By G.			200	200 Sept. 1
115BR	STA.		399+1			Chested By_	₩.	Beck		
Bering No. 1(N.Abut.) Station 398+40 Offset 14' Lt.	Elovation	Z	Qu 1/0.1.	(°2)	Surface Water El. Greundwater El. at Completion After — Hours	191.3	Elevation	2	Q 1/0.1.	(°,)
round Suries 200.2	0				LOOSE BR. CSE.	SAND _{177.2}		4	-	22
198.2					STIFF GR. SICL	176.2		2	1.3B	22
VERY STIFF Y. BR. TO B. S		13	2.5 P	28	HARD GR. SIC-T	ILL <u>173.7</u>	- <u>25</u>	28	5.4 B	74
STIFF Y. BR. TO BL. SICL	-5	12	1.2	24	VERY STIFF GR.	SIC-TILL		29	3.5 B	15
STIFF Y. BR. SANDY C			1.0		MEDIUM GR. SIC	171.2 -TILL ·	- 30		0.8	
191.2		3_	P	21	\checkmark	168.7		<u> 41 </u>	В	19_
VERY STIFF Y. BR. SIC-TI	LL <u>10</u>	1 14	2.5 B	17	HARD GR. SIC-T			40	4.5 P	16
	-				VERY STIFF GR.	166.2 SIC-TILL	- 35			
186.2		16	2.3 B	15	and the state of t		_	30	3.9 B	22
STIFF OL. GR. SIC-TILL	<u>-15</u>	20	1.7 S	15		167.0	-	22	2.1 8	24
VERY STIFF GR. SIC-TILL			2.7		STIFF GR. SIC-	161.2 TILL	- 40		11.7	
	_	14	B	21		158.7	- بیند ند	117 1	В	26
	- <u>20</u> -	16	2.3 B	21	STIFF GR. SILT		-	17	1.8 P	21
178.7						156.2	-4	5		

M-Standard Penetration Test-Blows por feet to drive 2" O.D. Split Spean Sampler 12" with 140# hammer falling 30".

Qu-Unconfined Compressive Strongth - t/sf

w - Water Content - percentage of oven dry weight - 5.

Typo failuro:

B-Bulge Failure

S - Shear Failure

eulaV batamite3 - 3

BRIDGE FOUNDATION B	DOLING LOG		
BORING #1 FA ROUTE 71 SECTION 115BR BORING #1 SECTION 115BR		Elevation 14	Qu 1/6.1.
VERY STIFF GR. SIC		1 1 1 1 1 1 1 1 1 1	(1 ng) (2n 1)

**	BRIDG	e i	FOL	INDA	1710	on Boring Log	
PQ () <u> </u> [DRIC	GE_	IL Rou	ite	54 Dato March 7, 1980	
7.5	UTEFA_71	<u> 0ve</u>	er Ti	rib. W	1. B	r. Vermilion R. Bored By J. Legan	
SEC		STA.		399+10)	Chested By W. Beck	
	Bering No. 2(S.Abut.) Station 399+90 Office 15' Lt.	Etovotion	Z	Qu 1/0.6.	(°°)	Surface Water El. 191.3 c c c c c c c c c c c c c c c c c c c	
Gn	ound Surism 200.2	O				2.3	
Mineral Principle	198.2					VERY STIFF GR. SICL 11 B 21	
	STIFF BL. SICL		13	1.5 P	30	HARD GR. SIC-TILL -25 4.1 25 B 14	
		<u>- 5</u>				VERY STIFF GR. SIC-TILL 3.5	
	193.7		8	В	30	171.2 25 B 14	
	STIFF YL. BR. TO B. SICL		4	1.5 P	29		
	191.2 MEDIUM YL. BR. SICL	- 10				HARD OL. GR. SIC-TILL 5.6	
	188.7		7	1.0 B	21	166.2 33 S 13	
***************************************	HARD GR. SIC-TILL 186.2	· · · · · · · · · · · · · · · · · · ·	22	5.0 S	16	STIFF GR. SIC-TILL -35 1.9 12 B 16 163.7	
-	STIFF GR. SIL	<u>=15</u>	14	1.9	15	HARD GR. SIC-TILL 38 4.5 38 P 13	
	183.7 VERY STIFF GR. SICL-TILL		15 15 15 15 15 15 15 15			VERY STIFF GR, SIC -40	
	181.2		15	2.2 S	13		
	VERY STIFF GR. SICL	- 20	i	3.1		23 2.9 05	
Table 17 Abbellow believes to the		-	18	B	21	156.2 B 25	

N-Standard Ponotration Test-Blows per feet to drive 2" O.D. Split Speen Sampler 12" with 140# hammer falling 30". Qu - Unconfined Compressive Strongth - t/sf

w - Water Content - percentage d oven dry weight - 7:

Typo failuro: 8 – Bulgo Failuro

S - Shoar Failuro

E-Estimated Value

4.5.0.0.0.0		BRIDGE	FO	יסאט	l Ti	ON_	Bor	ING	LOX	3				
F	ORING #2 .A. ROUTE 71 ECTION 115BR	Elevation		Qu 1/a.1.	(%) ^^						Elavation	1	Qu 1/6.1	V (%)
S S S S S S S S S S S S S S S S S S S	EDV STIFF OF S	- <u>L5</u>	13	1.0 B	22				and the second s					of the state of th
The second secon	ERY STIFF OL. G	R. SIC-IILL .	<u> 179</u>	2.9 B	15						- <i>1</i> 75			
***************************************		149.2	29	3.7 B]4	•						er de Gestrage - op troue cystypes (
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Consider Season Assets as a top of		-60							1	.	.B.5.	m my many de special personal state and general special special special special special special special special	STEP THE SEASON ASSESSMENT OF THE SEASON ASSES	man by the first field of the construction of the first construction o
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And the second s		-70		ti, da a da				•		•	28.1		Aug of Files. A civil-y-a management and a civil-y-a	

SEISMIC SITE CLASS DETERMINATION ID.O.T. BBS FOUNDATIONS AND GEOTECHNICAL UNIT

PROJECT TITLE=====|Selsmic:Site Class for Structure 027:0103 using 2009 Borlings

ft. inches	# #				
		inition:	(Blows/ft.) NA (Blows/ft.) NA (ksf) NA	_	(is)
Substructure 4 Base of Substruct. Elev. (or ground surf for bents) Pile or Shaft Dia. Boring Number	Top of Boring Elev. Approximate Fixity Elev.	Individual Site Class Definition:	N (bar): N _{ch} (bar): s _u (bar):	5	
surf for bents) It.	ני		NA NA		
Substructure 3 Base of Substruct. Elev. (or ground surf for bents) Pile or Shaft Dia. Boring Number	Top of Boring Elev, Approximate Fixtly Elev,	Individual Site Class Definition;	N (bar): (Blows/ft.) Na (bar): (Blows/ft.) su (bar): (Ksf)	Seismic Bot. Of Soil Golumn Sample Sample	Hevation
ft.					
or ground surf for bents) 748.45 ft. 12 ln 2 ln 2	742,45 ft.		ft.) Soil Site Class Dft.) NASoil Site Class C <controls< li=""></controls<>	Layer le Description	(187) (187)
		Definition:	23 (Blows/ft.) NA (Blows/ft.) 4.13 (ksf)	of Sample	
Substructure 2 Base of Substruct. Elev. Pile or Shaft Dia. Boring Number	Top of Boring Elev. Approximate Fixity Elev.	Individual Site Class Definition:	N (bar): Net (bar): s _u (bar):	Selsmic Bot. Of Soll Column Sample	
	- <	=			
142 ft.	742,42 ft.		<control< th=""><th>ptfon</th><th><u>k</u></th></control<>	ptfon	<u>k</u>
for bents) 748	742.42		Soil Site Class D NA Soil Site Class C	Layer Description	(167) (167)
r ground surf for bents) 748	742	oltion:	(Blows/ft.) Soil Site Class D (Blows/ft.) NA (ksf) Soil Site Class C <controls< th=""><th>Lay Sample Descri</th><th> N Qu (197)</th></controls<>	Lay Sample Descri	N Qu (197)
re 1 uct. Elev. (or ground surf for bents) 748 a.		Class Definition:	20 (Blows/ft.) Soil Site Class D NA (Blows/ft.) NA 4.48 (ksf) Soil Site Class C		(ft.) (eff.) (ef
Substructure 1 Base of Substruct. Elev. (or ground surf for bents) 74842 ft. Pile or Shaft Da. Borind Number 1	lev. diy Elev.	Individual Site Class Definition:		Sample	Haveling Check C

Soll Site Class D
) NA, H < 0.1*H (Total)
Soll Site Class C <---Controls Global Site Class Definition: Substructures 1 through 2 N (bar): 22 (Blows/ft.)
N_{ch} (bar): (Blows/ft.)
S_u (bar): 4.3 (ksf)

```
Conterminous 48 States
2007 AASHTO Bridge Design Guidelines
AASHTO Spectrum for 7% PE in 75 years
Latitude = 40.541695
Longitude = -088.281982
Site Class B
Data are based on a 0.05 deg grid spacing.
```

Period	Sa	
(sec)	(g)	
0.0	0.052	PGA - Site Class B
0.2	0.122	Ss - Site Class B
1.0	0.050	S1 - Site Class B

Conterminous 48 States

2007 AASHTO Bridge Design Guidelines

Spectral Response Accelerations SDs and SD1

Latitude = 40.541695

Longitude = -088.281982

As = FpgaPGA, SDs = FaSs, and SD1 = FvS1

Site Class C - Fpga = 1.20, Fa = 1.20, Fv = 1.70

Data are based on a 0.05 deg grid spacing.

Period	Sa	
(sec)	(g)	
0.0	0.062	As - Site Class C
0.2	0.146	SDs - Site Class C
1.0	0.084	SD1 - Site Class C