

| Original Report Date: Ap | oril 18, 2014 Propos | ed SN: 027-2019 | Route: | FAP 798 (IL 115) |
|---------------------------|------------------------|-----------------|----------|------------------|
| Revised Date: August 8, | 2014 Existing | g SN: 027-2506 | Section: | (107) CR-6 |
| Geotechnical Engineer: | Vichael Short; IDOT D | District 3 | County: | Ford |
| Structural Engineer: Marl | k Wylie; Farnsworth Gi | Contract: | 66C03 | |

Indicate the proposed structure type, substructure types, and foundation locations (attach plan and elevation drawing): The proposed structure is a double 8-feet by 6-feet precast concrete box culvert with a 40° right forward skew and an upstream cast in place drop structure.

Discuss the existing boring data, existing plans foundation information, new subsurface exploration and need for any additional exploration to be provided with SGR Technical Memo (attach all data and subsurface profile plot): The existing structure consists of a double 6-feet by 4-feet concrete box culvert with an upstream drop structure and no skew. Two soil borings were performed by IDOT in 2012. A copy of the soil borings is attached.

Provide the location and maximum height of any new soil fill or magnitude of footing bearing pressure. Estimate the amount and time of the expected settlement. Indicate if further testing, analysis, and/or ground improvement/treatment is necessary: The profile of the of the roadway is not expected to change, therefore there will not be any significant load applied to the soils. A site visit indicated no signs of settlement problems with the existing structure. No further settlement analysis is required.

Identify any new cuts or fill slope angles and heights. Estimate the factor of safety against slope failure. Indicate if further testing, analysis or ground improvement/treatment is necessary. *The proposed side slopes are expected to be flatter than existing. Proposed slopes range from 1:3 to 1:4 and will be a maximum of 9-feet high at culvert ends. A site visit indicated no stability problems with the existing structure. No further slope stability analysis is warranted.* Indicate at each substructure, the 100-year and 500-year total scour depths in the Hydraulics report, the non-granular scour depth reduction, the proposed ground surface, and the recommended foundation design scour elevations. *The design scour elevations at the upstream and downstream ends of culvert are 701.15 and 700.90, respectively. The elevations are based on a 3-feet deep cut-off wall below invert elevation. If the drop structure is constructed, then the scour elevation is only applicable to the downstream end of the culvert.*

Determining the seismic soil site class, the seismic performance zone, the 0.2 and 1.0 second design spectral accelerations and indicate if that the soils are liquefiable. *Not applicable to box culverts.*

Confirm feasibility of the proposed foundation or wall type and provide design parameters. Attach a pile design table indicating feasible pile types, various nominal required bearings, factored resistances available and corresponding estimated lengths at locations where piles will be used. Provide factored bearing resistance and unit sliding resistance at various elevations and confirm no ground improvement/treatment is necessary where spread footings are proposed. Estimated top of rock elevations as well as preliminary skin friction and end bearing values shall be indicated when drilled shafts are proposed. *Horizontal cantilever wingwalls are feasible on the downstream end of the box culvert. If the length of the wingwall exceeds the maximum allowable length for horizontal cantilever wingwalls, then L-type wingwalls or a horizontal cantilever wingwall with gabion extensions are feasible. If one of these options is selected, please contact the SGR author to provide the factored bearing resistance and unit sliding resistance values for the foundation soils under the wingwall. In addition, it may be possible to construct horizontal cantilever wingwalls that slightly exceed the 14 foot length limitation outlined in the Culvert Manual. The drop structure at the upstream end of the box culvert to precise any special geotechnical considerations. The only aggregate needed under the precast concrete box culvert is the 6 inches required by Article 540.06 of the Standard Specifications.*

Calculate the estimated water surface elevation and determine the need for cofferdam(s) and seal coat: The structure can be constructed using conventional methods for water diversion.

Assess the need for sheeting/soil retention versus using a temporary construction slope and provide recommendation for the most feasible option. The new structure will be constructed using stage construction. Soil strengths exceed 4.5 tsf, therefore the pay item "Temporary Soil Retention System" should be used.

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SOIL BORING LOG

Date 12/19/12

ROUTE IL 115 (FAP 798) DESCRIPTION IL 115 over a Stream, 4.1 miles South of US 24 LOGGED BY Larry Myers

Illinois Department of Transportation

Division of Highways

| | 107 & 107B LOCATION _ | | | | | NE 1/4, SEC. 33, TWP. 26N, RNG. 9E, | | | | | | | |
|---|--|--|-----------------------|-----------------------|-------------------|--|---|---|-----------------------|-----------------------|-------------------|-----------------------|--|
| COUNTY | Ford | DRILLING METHOD | | | | Hol | low Stem Auger | HAMMER TYPE | (| CME Automatic | | | |
| STRUCT. NO. Station BORING NO. Station Offset | 027-2506 (Exis 215+47 1 (N.W. Quad. 215+03 13.0 ft Rt. | <u>) </u> | D E P T H | B L O W S | U C S Qu | M O I S T | Surface Water Elev Stream Bed Elev Groundwater Elev.: First Encounter Upon Completion | <u>703.73</u> ft <u>706.51</u> ft <u>Dry</u> ft Dry ft | D E P T H | B L O W S | U C S Qu | M O I S T | |
| Ground Surfac | ce Elev. 711.8 | 2 ft | (ft) | (/6") | (tsf) | (%) | After Hrs. | ft | (ft) | (/6") | (tsf) | (%) | |
| Brown Silty Clay | y Loam Fill | S. | | | | | Loam Till (continued) | lity Clay | | 5 7 | 4.5 S | 19 | |
| Stiff to Very Stif Silty Clay Loam | f Black & Brown Fill | 709.32 | | 3 3 3 | 2.0 P | 28 | | | | 4 6 8 | 4.5 S | 18 | |
| Stiff to Very Stif Clay/Silty Clay I | f Black Silty ₋oam Topsoil | - | -5 | 3 3 3 | 2.0 P | 32 | | | 25 | 5 7 7 | 4.5 S | 19 | |
| Very Stiff Brown Loess | n & Gray Silty Cla | 704.32 y | | 3 3 3 | 2.0 P | 29 | | | | 6 7 8 | 4.4 S | 22 | |
| Stiff Brown & G Loam Till | ray Silty Clay | 702.32 | -10 | 1 2 2 | 1.5 P | 24 | 0 | 1 | -30 | 6 6 8 | 4.5 S | 23 | |
| Hard Brownish Loam Till | Gray Silty Clay | 699.82 | | 5 8 10 | 5.9 S | 16 | | 0 | | | | | |
| | | - | -15 | 7 | 59 | 17 | | | -35 | 7 | 47 | 23 | |
| | | | | 12 | S | | End of Boring | 675.3 | 2 | 9 | S | | |
| | | | | 5 6 7 | 4.5 S | 17 | | | | | | | |
| | | | -20 | | | | | | -40 | | | | |

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer) The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

| (The formation of Transportation | ne | nt | | SC | | | | Page | <u> 1 </u> | of <u>1</u> | | |
|---|-------------|-------------|-------------|-----------------|--|---|-------------|---------------|------------------|-------------|--|--|
| Division of Highways IDOT | | I | | | | | | Date | 12/ | 19/12 | | |
| ROUTE IL 115 (FAP 798) DE | SCR | IPTION | | 115 ov | er a Stream, 4.1 miles | South of US 24 | LOGG | ED BY | Larry | Myers | | |
| SECTION 107 & 107B | I | OCAT | | NW 1/ Latitu | 4, SEC. 34, TWP. 26N de 40.689037, Longit | , RNG. 9E, t ude -88.18011 | | | | | | |
| COUNTY Ford DRILLING | G ME | THOD | | Hol | low Stem Auger | HAMMER TYPE | | CME Automatic | | | | |
| STRUCT. NO. 027-2506 (Exist.) Station 215+47 | D E P | B L O | U C S | M O I | Surface Water Elev. Stream Bed Elev. | <u>703.73</u> ft 706.11 ft | D E P | B L O | U C S | M O I | | |
| BORING NO. 2 (S.E. Quad.) Station 215+87 Offset 13.0 ft Lt. | Т Н | W S | Qu | S T | Groundwater Elev.: First Encounter Upon Completion | Dryft Dryft | H T | W S | Qu | S T | | |
| Ground Surface Elev. 712.17 ft | (ft) | (/6") | (tsf) | (%) | After Hrs. | ft | (ft) | (/6") | (tsf) | (%) | | |
| Silty Clay Loam Fill | _ | - | | | (continued) | Loam Ini | | 7 8 | 5.7 S | 16 | | |
| 709.67 | | 3 | | | | | | 6 | | | | |
| Fill | | 2 3 | 2.5 P | 29 | | | | 6 9 | 5.3 S | 18 | | |
| | -5 | 3 | M | 1 | | | -25 | 5 | | | | |
| 705.67 | | 2 4 | 2.5 P | 30 | | | | 7 9 | 5.3 S | 17 | | |
| Very Stiff Brown & Gray Silty Clay Loess 704.67 | | | | | ∇ | | | | | | | |
| Very Stiff Brown & Gray Silty Clay Loam Till | | 3 3 5 | 2.5 P | 23 | | | | 5 7 9 | 5.1 S | 17 | | |
| 702.67 | | - | | | | | | - | | | | |
| Loam Till | | 7 | 7.1 | 19 | | 1. | | 5 7 7 | 5.1 | 17 | | |
| | | 14 | 5 | | | V | | | 5 | | | |
| | | 6 | 6.9 | 17 | | | | - | | | | |
| | | 14 | 0.0 S | | | | 4 | | | | | |
| | -15 | 6 | | | | • | -35 | 6 | | | | |
| | | 8 12 | 6.1 S | 16 | | 675.6 | 57 | 6 8 | 5.1 S | 17 | | |
| 695.17 Hard Gray Silty Clay Loam Till | | - | | | End of Boring | | | | | | | |
| , , , | | 6 8 | 6.2 | 16 | | | | | | | | |
| | | 12 | S | | | | | | | | | |
| | -20 | 1 | | | | | -40 | 1 | | | | |

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