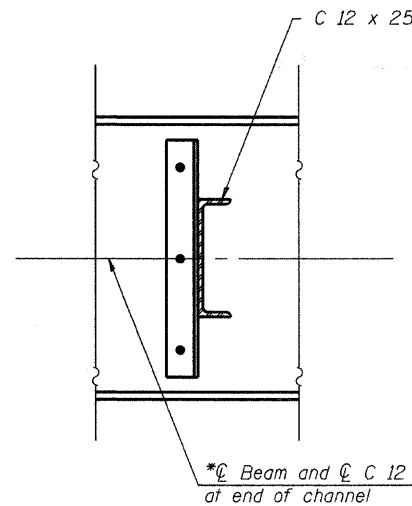
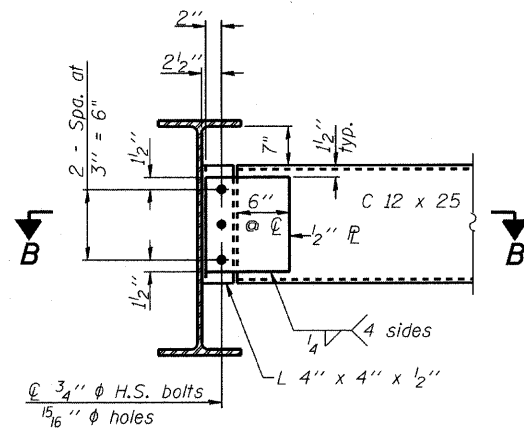


**INTERIOR DIAPHRAGM D**

Note:  
Two hardened washers required for each set of oversized holes.  
\*Alternate channels (C 12 x 30) are permitted to facilitate material acquisition. Calculated weight of structural steel is based on the lighter section. The alternate, if utilized, shall be provided at no additional cost to the Department.  
\*\*3/4"  $\phi$  HS bolts, 15/16"  $\phi$  holes

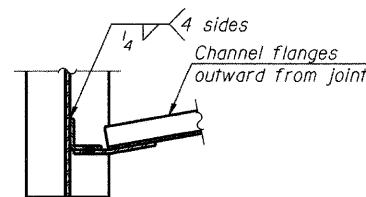


**SECTION A-A**



**END DIAPHRAGM D1**

Note:  
Two hardened washers required for each set of oversized holes.



**SECTION B-B**

INTERIOR GIRDER MOMENT TABLE		
0.5 Span		
$I_s$	(in <sup>4</sup> )	3,270
$I_c(n)$	(in <sup>4</sup> )	10,383
$I_c(3n)$	(in <sup>4</sup> )	7,688
$S_s$	(in <sup>3</sup> )	243
$S_c(n)$	(in <sup>3</sup> )	390
$S_c(3n)$	(in <sup>3</sup> )	352
DC1	(k/')	0.736
M <sub>DC1</sub>	('k)	257
DC2	(k/')	0.129
M <sub>DC2</sub>	('k)	45
DW	(k/')	0.286
M <sub>DW</sub>	('k)	100
$M_L + IM$	('k)	560
$M_u$ (Strength I)	('k)	1,506
$\phi_r M_n$	('k)	2,091
$f_s$ DC1	(ksi)	12.70
$f_s$ DC2	(ksi)	1.53
$f_s$ DW	(ksi)	3.41
$f_s$ ( $L + IM$ )	(ksi)	17.23
$f_s$ (Service II)	(ksi)	40.04
$0.95R_n F_y f$	(ksi)	47.50
$V_f$	(k)	23.75

INTERIOR GIRDER REACTION TABLE		
Abut.		
R <sub>DC1</sub>	(k)	20.1
R <sub>DC2</sub>	(k)	3.4
R <sub>DW</sub>	(k)	7.6
$R_L + IM$	(k)	79.4
R <sub>Total</sub>	(k)	110.5

All cross frames or diaphragms shall be installed as steel is erected and secured with erection pins and bolts except as otherwise noted. Individual cross frames or diaphragms at supports may be temporarily disconnected to install bearing anchor rods.

$I_s, S_s$ : Non-composite moment of inertia and section modulus of the steel section used for computing  $f_s$  (Total-Strength I, and Service II) due to non-composite dead loads (in<sup>4</sup> and in<sup>3</sup>).  
 $I_c(n), S_c(n)$ : Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing  $f_s$  (Total-Strength I, and Service II) in uncracked sections, due to short-term composite live loads (in<sup>4</sup> and in<sup>3</sup>).  
 $I_c(3n), S_c(3n)$ : Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing  $f_s$  (Total-Strength I, and Service II) in uncracked sections, due to long-term composite (superimposed) dead loads (in<sup>4</sup> and in<sup>3</sup>).  
DC1: Un-factored non-composite dead load (kips/ft.).  
M<sub>DC1</sub>: Un-factored moment due to non-composite dead load (kip-ft.).  
DC2: Un-factored long-term composite (superimposed excluding future wearing surface) dead load (kips/ft.).  
M<sub>DC2</sub>: Un-factored moment due to long-term composite (superimposed excluding future wearing surface) dead load (kip-ft.).  
DW: Un-factored long-term composite (superimposed future wearing surface only) dead load (kips/ft.).  
M<sub>DW</sub>: Un-factored moment due to long-term composite (superimposed future wearing surface only) dead load (kip-ft.).  
 $M_L + IM$ : Un-factored live load moment plus dynamic load allowance (impact) (kip-ft.).  
 $M_u$  (Strength I): Factored design moment (kip-ft.).  
 $1.25 (M_{DC1} + M_{DC2}) + 1.5 M_{DW} + 1.75 M_L + IM$   
 $\phi_r M_n$ : Compact composite positive moment capacity computed according to Article 6.10.7.1 (kip-ft.).  
 $f_s$  DC1: Un-factored stress at edge of flange for controlling steel flange due to vertical non-composite dead loads as calculated below (ksi).  
 $M_{DC1} / S_{nc}$   
 $f_s$  DC2: Un-factored stress at edge of flange for controlling steel flange due to vertical composite dead loads as calculated below (ksi).  
 $M_{DC2} / S_c(3n)$   
 $f_s$  DW: Un-factored stress at edge of flange for controlling steel flange due to vertical composite future wearing surface loads as calculated below (ksi).  
 $M_{DW} / S_c(3n)$   
 $f_s$  ( $L + IM$ ): Un-factored stress at edge of flange for controlling steel flange due to vertical composite live plus impact loads as calculated below (ksi).  
 $M_L + IM / S_c(n)$   
 $f_s$  (Service II): Sum of stresses as computed below (ksi).  
 $f_{sDC1} + f_{sDC2} + f_{sDW} + 1.3 f_s (L + IM)$   
 $0.95R_n F_y f$ : Composite stress capacity for Service II loading according to Article 6.10.4.2 (ksi).  
 $V_f$ : Maximum factored shear range in composite portion of span computed according to Article 6.10.10.