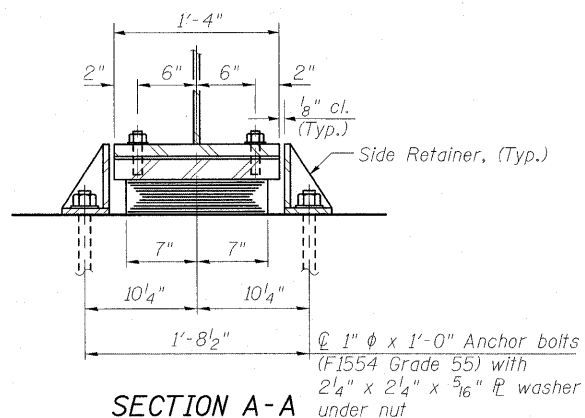
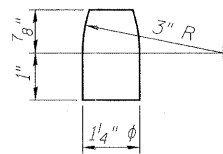


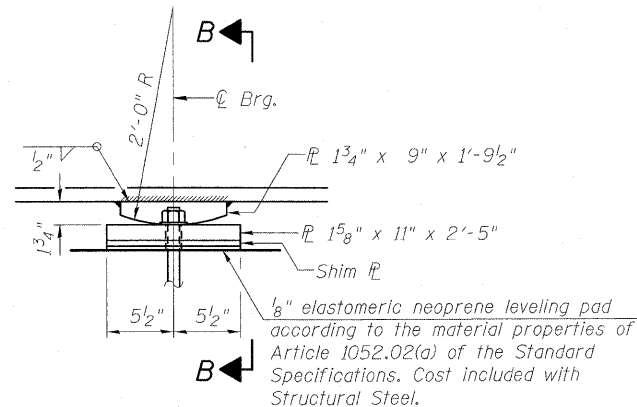
ELEVATION AT ABUT.



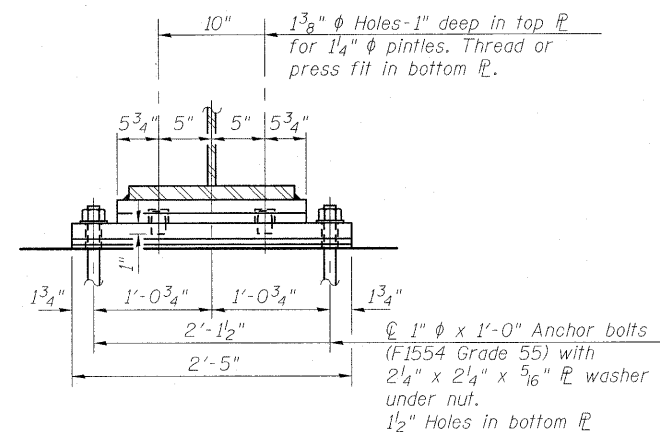
SECTION A-A



PINTLE



ELEVATION AT PIER



SECTION B-B

**TYPE I ELASTOMERIC EXP. BRG.**

(6 required)  
(3 at each Abut.)

**FIXED BEARING**

(3 required)

**Notes:**

Anchor bolts shall be ASTM F1554 all-thread (or an Engineer-approved alternate material) of the grade(s) and diameter(s) specified. The corresponding specified grade of AASHTO M314 anchor bolts may be used in lieu of ASTM F1554.

Anchor bolts at fixed bearings may be either cast in place or installed in holes drilled after the supported member is in place.

Anchor bolts for side retainers may be cast in place or installed in holes drilled before or after members are in place.

Drilled and set anchor bolts shall be installed according to Article 521.06 of the Standard Specifications.

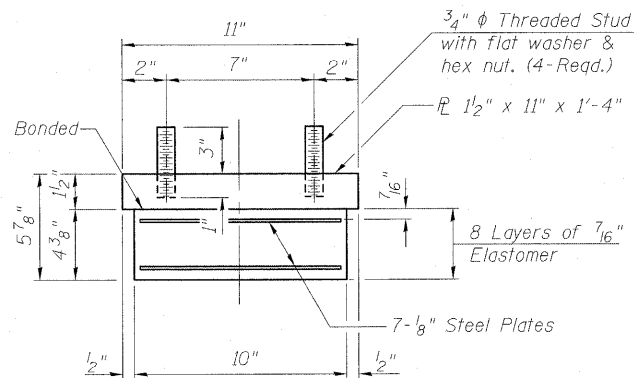
Side retainers and other steel members required for the elastomeric bearing assembly shall be included in the cost of Elastomeric Bearing Assembly, Type I.

See sheets 22 and 24 of 46 for Anchor Bolt Location Details.

Two 1/8" adjusting shims shall be provided for each bearing in addition to all other plates or shims and placed as shown in the bearing details.

All bearing plates shall be M270 Gr. 50.

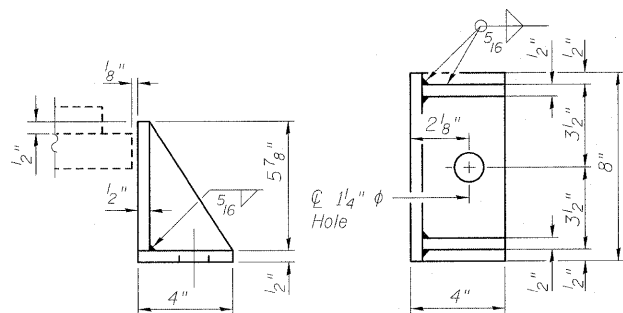
The anchor bolt sizes and grades shown constitute a calculated seismic structural fuse. Substitution of higher diameter and/or grade anchor bolts will not be allowed.



**BEARING ASSEMBLY**

**Note:**

Shim plates shall not be placed under Bearing Assembly.



**SIDE RETAINER**

Equivalent rolled angle with stiffeners will be allowed in lieu of welded plates.

INTERIOR GIRDER MOMENT TABLE			
		0.4 Sp. 1 or 0.6 Sp. 2	Pier
$I_s$	(in <sup>4</sup> )	15688	28512
$I_c(n)$	(in <sup>4</sup> )	38157	-
$I_c(3n)$	(in <sup>4</sup> )	27453	-
$S_s$	(in <sup>3</sup> )	869	1326
$S_c(n)$	(in <sup>3</sup> )	1108	-
$S_c(3n)$	(in <sup>3</sup> )	981	-
DC1	(k/')	0.75	0.85
M <sub>DC1</sub>	(k)	792	1951
DC2	(k/')	0.33	0.33
M <sub>DC2</sub>	(k)	387	689
DW	(k/')	0.14	0.14
M <sub>DW</sub>	(k)	161	286
M <sub>L</sub>	(k)	762	882
M <sub>u</sub> (Strength I)	(k)	3049	5272
* $\phi_r M_n$	(k)	5527	-
$f_s$ DC1	(ksi)	10.9	17.7
$f_s$ DC2	(ksi)	4.7	6.2
$f_s$ DW	(ksi)	2.0	2.6
$f_s$ 1.3(L)	(ksi)	10.7	10.4
$f_s$ (Service II)	(ksi)	28.4	36.9
** $f_s$ (Total)(Strength I)	(ksi)	-	47.7
V <sub>r</sub>	(k)	2.4	-

\* compact sections

\*\* non-compact and slender sections

INTERIOR GIRDER REACTION TABLE		
	Abut.	Pier
R <sub>DC1</sub>	(k)	35.7
R <sub>DC2</sub>	(k)	16.1
R <sub>DW</sub>	(k)	6.7
R <sub>L</sub>	(k)	26.7
R <sub>Total</sub>	(k)	85.2

$I_s, S_s$ : Non-composite moment of inertia and section modulus of the steel section used for computing  $f_s$  (Total-Strength I, and Service II) due to non-composite dead loads (in<sup>4</sup> and in<sup>3</sup>).

$I_c(n), S_c(n)$ : Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing  $f_s$  (Total-Strength I, and Service II) due to short-term composite live loads (in<sup>4</sup> and in<sup>3</sup>).

$I_c(3n), S_c(3n)$ : Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing  $f_s$  (Total-Strength I, and Service II) due to long-term composite (superimposed) dead loads (in<sup>4</sup> and in<sup>3</sup>).

DC1: Un-factored non-composite dead load (kips/ft.).

M<sub>DC1</sub>: Un-factored moment due to non-composite dead load (kip-ft.).

DC2: Un-factored long-term composite (superimposed excluding future wearing surface) dead load (kips/ft.).

M<sub>DC2</sub>: Un-factored moment due to long-term composite (superimposed excluding future wearing surface) dead load (kip-ft.).

DW: Un-factored long-term composite (superimposed future wearing surface only) dead load (kips/ft.).

M<sub>DW</sub>: Un-factored moment due to long-term composite (superimposed future wearing surface only) dead load (kip-ft.).

M<sub>L</sub>: Un-factored live load moment due to Pedestrian Load (kip-ft.).

M<sub>u</sub> (Strength I): Factored design moment (kip-ft.).

$1.25(M_{DC1} + M_{DC2}) + 1.5M_{DW} + 1.75M_L$

$\phi_r M_n$ : Compact composite positive moment capacity computed according to Article 6.10.7.1 (kip-ft.).

$f_s$  (Service II): Sum of stresses as computed from the moments below (ksi).

$M_{DC1} + M_{DC2} + M_{DW} + 1.3M_L$

$f_s$  (Total)(Strength I): Sum of stresses as computed from the moments below on non-compact section (ksi).

$1.25(M_{DC1} + M_{DC2}) + 1.5M_{DW} + 1.75M_L$

V<sub>r</sub>: Maximum factored shear range in composite portion of span computed according to Article 6.10.10.

**BILL OF MATERIAL**

Item	Unit	Total
Elastomeric Bearing Assembly Type I	Each	6
Anchor Bolts, 1"	Each	18