



Original Report Date: 1-12-18 **Proposed SN:** 046-0156/0157 **Route:** FAI-57 (I-57)
Revised Date: 6-22-18 **Existing SN:** 046-0008/0009 **Section:** [(139)VBJES
Geotechnical Engineer: Michael Haley, Lin Engineering, Ltd. **County:** Kankakee
Structural Engineer: Michael Haley, Lin Engineering, Ltd. **Contract:** 66F74

Indicate the proposed structure type, substructure types, and foundation locations (attach plan and elevation drawing): The proposed structures are dual 3-span bridges with 36" PPC IL beams supported on integral abutments and multi-column piers. Piers and slope walls are located to avoid existing foundations and to provide adequate railroad clearances. Abutments are located to intersect the slope walls at 1:2 (V:H) slope. The bridges will each have back-to-back abutment lengths of 200'-3", out-to-out widths of 51'-1" and a 10°-54'-30" right ahead skew. Each substructure unit will be constructed approximately 12 feet wider to the outside to accommodate future widening. A preliminary TSL drawing is attached.

Discuss the existing boring data, existing plans foundation information, new subsurface exploration and need for any additional exploration to be provided with SGR Technical Memo (attach all data and subsurface profile plot): The existing structures built in 1954 are 5-span dual bridges with spill thru abutments and multi-column piers. The original bridges utilize spread footing foundations founded on rock. Rock elevations shown in pile driving records from the 1990 widening are in line with the rock elevations shown in the design plans. Soil borings from 2016 and rock cores from 2017 are attached, along with a subsurface soil profile plot.

Provide the location and maximum height of any new soil fill or magnitude of footing bearing pressure. Estimate the amount and time of the expected settlement. Indicate if further testing, analysis, and/or ground improvement/treatment is necessary: The proposed abutments will be constructed on embankment approximately 13.3 ft higher than existing grade at the north abutment and 25.1 ft higher at the south abutment. The anticipated settlement at the north abutment is 0.07 inches, while the anticipated settlement at the south abutment is 0.43 inches. These settlements are not expected to create significant downdrag forces on the proposed piles. No soil remediation or settlement monitoring is required.

Identify any new cuts or fill slope angles and heights. Estimate the factor of safety against slope failure. Indicate if further testing, analysis or ground improvement/treatment is necessary: The proposed abutments and slopewalls will provide fill situations at each end of the structures. Preliminary stability analyses using Bishop's method were performed for each abutment. According to AASHTO LRFD 11.6.2.3, the required resistance factor for slope stability is 0.65 which is equivalent to a factor of safety of 1.5. The slope stability models for each abutment rendered factors of safety over 3.0.

Indicate at each substructure, the 100-year and 200-year total scour depths in the Hydraulics report, the non-granular scour depth reduction, the proposed ground surface, and the recommended foundation design scour elevations: Preliminary analysis shows that scour is not a concern at this location.

DESIGN SCOUR ELEVATION TABLE

Event / Limit	Design Scour Elevations (ft.)				Item 113	
	State	N. Abut.	Pier 1	Pier 2		S. Abut.
Q100		660.2	638.8	637.5	660.3	8
Q200		660.2	638.8	637.5	660.3	
Design		660.2	638.8	637.5	660.3	
Check		660.2	638.8	637.5	660.3	

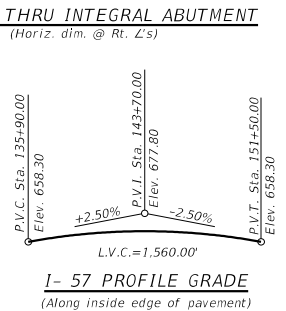
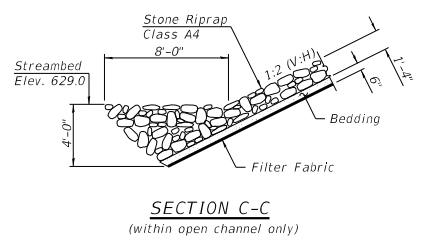
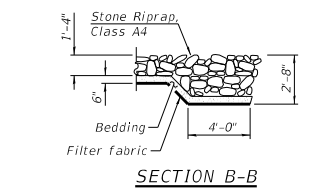
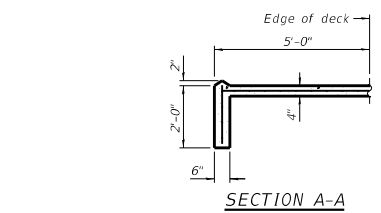
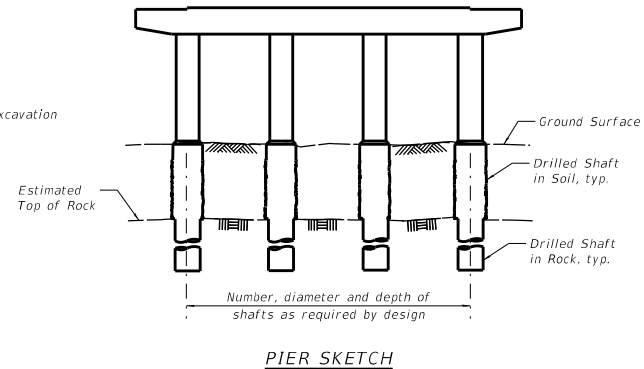
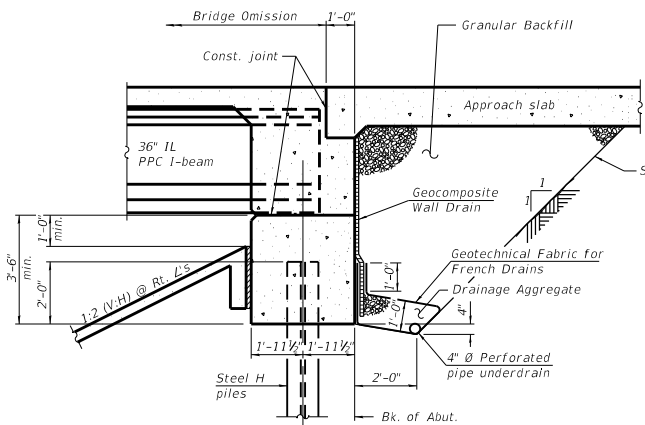
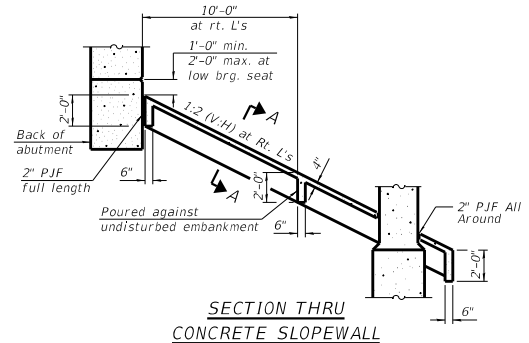
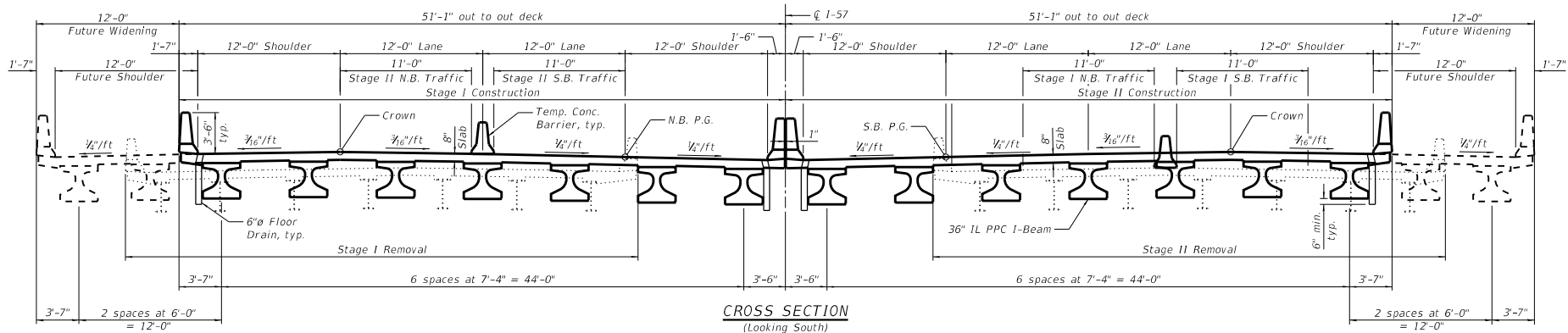
Determining the seismic soil site class, the seismic performance zone, the 0.2 and 1.0 second design spectral accelerations and indicate if that the soils are liquefiable: Based on IDOT Design Guide LRFD Soil Site Class Definition, Soil Site Class C controls. The Design Spectral Acceleration at 1.0 sec (SD1) is 0.072g and at 0.2 sec (SDS) is 0.125g. These values are based on a 1000 year design return period earthquake. According to AASHTO LRFD 3.10.6 the Seismic Performance Zone is 1. Liquefaction analysis is not required for SPZ 1.

Confirm feasibility of the proposed foundation or wall type and provide design parameters. Attach a pile design table indicating feasible pile types, various nominal required bearings, factored resistances available and corresponding estimated lengths at locations where piles will be used. Provide factored bearing resistance and unit sliding resistance at various elevations and confirm no ground improvement/treatment is necessary where spread footings are proposed. Estimated top of rock elevations as well as preliminary factored unit side and tip resistance values shall be indicated when drilled shafts are proposed: Due to IDOT's strong desire for a jointless structure, integral abutments will be provided. Per IDOT Integral Abutment Pile Selection Design Guide, all metal shell and H-pile types are permissible at this location. However, H-piles are preferred since these piles will likely be driven to rock. See attached spreadsheets for estimated pile lengths and

capacities. The estimated factored design loads are 1300 kips at the abutments and 5260 kips at the piers. Due to the shallow bedrock elevations, either spread footings or drilled shafts are preferred at the piers. Considering the excavation required for spread footings along with railroad horizontal clearance requirements, the spread footings are not recommended, leaving drilled shafts as the preferred choice at the piers. Per AGMU 12.0, a Geotechnical Design Memorandum will be required for the drilled shafts during the design phase. Preliminary analysis shows the limestone layers at elevation 616.0 will provide a nominal unit side resistance (q_s) of 32 ksf and a nominal unit tip resistance (q_p) of 3375 ksf. Per AASHTO 10.8.3.5.4b, the side resistance is controlled by the compressive strength of the concrete shaft. Resistance factors of 0.50 and 0.55 shall be used for the tip and side resistances respectively when calculating the factored resistances for Strength. Only side or tip resistance should be considered during design, not both simultaneously. Rock elevations will be approximately 626.3 at Pier 1 and 625.4 at Pier 2.

Calculate the estimated water surface elevation and determine the need for cofferdams (type 1 or 2), and seal coat: Construction of the substructure units can be performed using conventional methods without a need for water diversion or cofferdams.

Assess the need for sheeting or soil retention or temporary construction slope and provide recommendation for other construction concerns: Temporary soil retention will be required to retain soil between the two structures during construction. Preliminary design shows Temporary Sheet Piling is feasible and is recommended. However, if it is determined during design phase that the embedment is expected to be within a soil layer with Q_u larger than 4.5 tsf, a Temporary Soil Retention System would be required. Pile shoes are recommended for driving piles into limestone layers. Due to the consistent rock elevation data provided in the borings, no test piles are recommended. Rather, the proposed pile lengths shall be extended by two feet to accommodate any variations encountered in the field.



NORTH TRACK (MAIN)

Sta. 48+95	Elev. 640.61
Sta. 49+46	Elev. 640.69
Sta. 49+83	Elev. 640.71
Sta. 50+17	Elev. 640.66
Sta. 50+55	Elev. 640.59
Sta. 51+07	Elev. 640.49

SOUTH TRACK (SIDING)

Sta. 49+30	Elev. 638.99
Sta. 49+60	Elev. 639.16
Sta. 49+81	Elev. 639.28
Sta. 50+06	Elev. 639.35
Sta. 50+37	Elev. 639.29
Sta. 50+74	Elev. 639.35

GENERAL DATA

I-57 OVER NORFOLK SOUTHERN RAILWAY & DRAINAGE DITCH

F.A.I. RTE 57 - SEC. I(139)VB/ES

KANKAKEE COUNTY

STATION 143+61.89

STRUCTURE NO. 046-0156 (N.B.)

STRUCTURE NO. 046-0157 (S.B.)

<p>LIN ENGINEERING LTD. Consulting Engineers Soils & Rock</p>	USER NAME =	DESIGNED - MTH	REVISD -	<p>STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION</p>	<table border="1"> <tr><td>F.A.I. RTE</td><td>SECTION</td><td>COUNTY</td><td>TOTAL SHEETS</td></tr> <tr><td>57</td><td>I(139)VB/ES</td><td>KANKAKEE</td><td>NO.</td></tr> <tr><td colspan="4">CONTRACT NO. 66F74</td></tr> </table>	F.A.I. RTE	SECTION	COUNTY	TOTAL SHEETS	57	I(139)VB/ES	KANKAKEE	NO.	CONTRACT NO. 66F74			
	F.A.I. RTE	SECTION	COUNTY			TOTAL SHEETS											
57	I(139)VB/ES	KANKAKEE	NO.														
CONTRACT NO. 66F74																	
PLOT SCALE =	CHECKED - VPT	REVISD -	SHEET 2 OF 2 SHEETS														
PLOT DATE =	DRAWN - CGY	REVISD -	ILLINOIS FED. AID PROJECT														
	CHECKED - MTH	REVISD -															

MODEL: D:\P\011
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SOIL BORING LOG

ROUTE FAI-57 (I-57) DESCRIPTION I-57 over Con-Rail Corp. Railroad, 0.9 miles North of IL 17 LOGGED BY Larry Myers

SECTION 139VBR LOCATION NE 1/4, SEC. 33, TWP. 31N, RNG. 12E, 3rd PM, Latitude 41.131521, Longitude -87.836207

COUNTY Kankakee DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME Automatic

STRUCT. NO.	Station	BORING NO.	Station	Offset	Ground Surface Elev.	D E P T H (ft)	B L O W S (/6")	U C S (tsf)	M O I S T (%)	Surface Water Elev.	Stream Bed Elev.	D E P T H (ft)	B L O W S (/6")	U C S (tsf)	M O I S T (%)
046-0008/0009	143+72	02	145+27	10.0 ft Rt.	665.51										
Augered Black Silty Clay Loam Fill & Gray / Brown Silty Clay Loam Fill										Very Stiff to Hard Gray & Brown Sandy Clay Loam, Loam Fill & some Sand & Gravel Fill @ 20 Ft. (continued)					
						663.01									
Very Stiff to Hard Gray & Brown Silty Clay Loam Till Fill with some Black Silty Clay Loam Layers							2		15						
							4	3.5							
							4	P							
						-5	3								
							4	4.0	17						
							5	B							
						658.51				638.51					
Very Stiff to Hard Gray & Brown Sandy Clay Loam, Loam Fill & some Sand & Gravel Fill @ 20 Ft.							3		19	Hard to Very Stiff Black, Gray & Brown Silty Clay Loam & Sandy Clay Loam Fill					
							4	4.4							
							5	S							
						-10	3								
							4	3.4	16						
							6	B							
							4								
							5	3.8	17						
							6	S							
						-15	3			631.01					
							5	4.2	17	Very Stiff Gray & Black Silty Clay Loam					
							7	S							
							4								
							5	4.2	14						
							7	S							
										626.51					
						-20									

SOIL BORING 046-0008,0009.GPJ IL_DOT.GDT 1/24/17

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



SOIL BORING LOG

ROUTE FAI-57 (I-57) DESCRIPTION I-57 over Con-Rail Corp. Railroad, 0.9 miles North of IL 17 LOGGED BY Larry Myers

SECTION 139VBR LOCATION NE 1/4, SEC. 33, TWP. 31N, RNG. 12E, 3rd PM, Latitude 41.131782, Longitude -87.836172

COUNTY Kankakee DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME Automatic

STRUCT. NO. 046-0008/0009
Station 143+72

BORING NO. 04 (Pier)
Station 144+23
Offset 0.0 ft Centerline
Ground Surface Elev. 638.49 ft

DEPTH (ft)	BLOWS (/6")	UCS (tsf)	MOIST (%)
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Surface Water Elev. _____ ft
Stream Bed Elev. _____ ft

Groundwater Elev.:
First Encounter 626.5 ft ▼
Upon Completion 626.5 ft ▼
After _____ Hrs. _____ ft

Augered CA6, Black Silty Clay Loam / Silty Loam Fill with Heavy Gravel Pieces & Sand Layers - Fill			
633.49	-5		
Stiff Gray & Black Silt, Silty Clay Loam Fill with Gravel Pieces	2		
	3	1.5	15
631.49	3	P	
Soft Brown, Gray & Black Silty Loam, Silty Clay Loam with Sand Layers & Gravel Pieces - (Fill?)	WH		
	1	0.5	26
	2	P	
-10			
	WH		
	2	0.5	16
	2	P	
625.99			
Gray Limestone - Weathered Surface	625.57	100/5*	9
End of Boring			
-15			
-20			

SOIL BORING 046-0008,0009.GPJ IL_DOT.GDT 1/24/17

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



SOIL BORING LOG

ROUTE FAI-57 (I-57) DESCRIPTION I-57 over Con-Rail Corp. Railroad, 0.9 miles North of IL 17 LOGGED BY Larry Myers

SECTION 139VBR LOCATION NE 1/4, SEC. 33, TWP. 31N, RNG. 12E, 3rd PM, Latitude 41.131764, Longitude -87.836406

COUNTY Kankakee DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME Automatic

STRUCT. NO. 046-0008/0009
 Station 143+72

BORING NO. 05
 Station 144+29
 Offset 58.0 ft Rt.
 Ground Surface Elev. 638.70 ft

DEPTH (ft)	BLOWS (/6")	UCS (tsf)	MOIST (%)
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Surface Water Elev. _____ ft
 Stream Bed Elev. _____ ft

Groundwater Elev.:
 First Encounter 626.2 ft ▼
 Upon Completion 626.2 ft ▼
 After _____ Hrs. _____ ft

Augered Black & Brown Silty Clay Loam Fill with Large Gravel & Oversize Gravel Pieces			
633.70	-5		
Stiff Black & Brown Silty Clay Loam, Silty Loam Fill with Gravel & Debris	2 2 3	1.5 P	20
631.70			
Very Stiff Brown & Gray Silt, Silty Loam, Silty Clay with Limestone Gravel Pieces	3 5 7	3.0 P	17
629.20			
Medium Brown Fine to Coarse Loamy Sand with Layers of Brown Sandy Clay Loam / Sandy Loam	-10 4 5 9		17
626.20 ▼			
Gray Limestone - Weathered Surface	61		
625.53	100/2"		9
End of Boring			
-15			
-20			

SOIL BORING 046-0008,0009.GPJ IL_DOT.GDT 1/24/17

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
 The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



Illinois Department of Transportation

Division of Highways
Illinois Department of Transportation

ROCK CORE LOG

Date 11/24/17

ROUTE FAI-57 (I-57) DESCRIPTION I-57 over Con-Rail Corp. Railroad, 0.9 miles North of IL 17 LOGGED BY Larry Myers

SECTION 139VBR LOCATION NE 1/4, SEC. 33, TWP. 31N, RNG. 12E, 3rd PM, Latitude 41.13179, Longitude -87.836406

COUNTY Kankakee CORING METHOD Split Barrel Wire Line

STRUCT. NO. 046-0008/0009 CORING BARREL TYPE & SIZE N W/L 2
Station 143+72

BORING NO. RC 01
Station 144+23
Offset 61.0 ft Rt.
Ground Surface Elev. 638.78 ft

DEPTH (ft)	CORE (#)	RECOVERY (%)	R.Q.D. (%)	CORE TIME (min/ft)	STRENGTH (tsf)
625.78	1	90	20	5.6	
-15					697.3 692.7
	2	100	43	4.4	724.0 759.5 719.7
-20					723.7
	3	95	52	4.8	676.6
-25					713.6
					657.2
610.78					741.7
-30					

Dense Gray Limestone, Horizontally Fractured. Vertical Fracturing to 15 ft. Tight Joints

End of Boring

ROCK CORE 046-0008.0009.GPJ IL_DOT.GDT 3/6/18

Color pictures of the cores Yes

Cores will be stored for examination until Construction Complete

The "Strength" column represents the uniaxial compressive strength of the core sample (ASTM D-2938)

I-57 over R x R in Kankakee

SN 046-0008 / 0009 11-24-2017

Hole # 1

Depth 13 Ft to 23 Ft

Box 1 of 2

Start
13 Ft



12/11/2017



I-57 over R&R in Kankakee

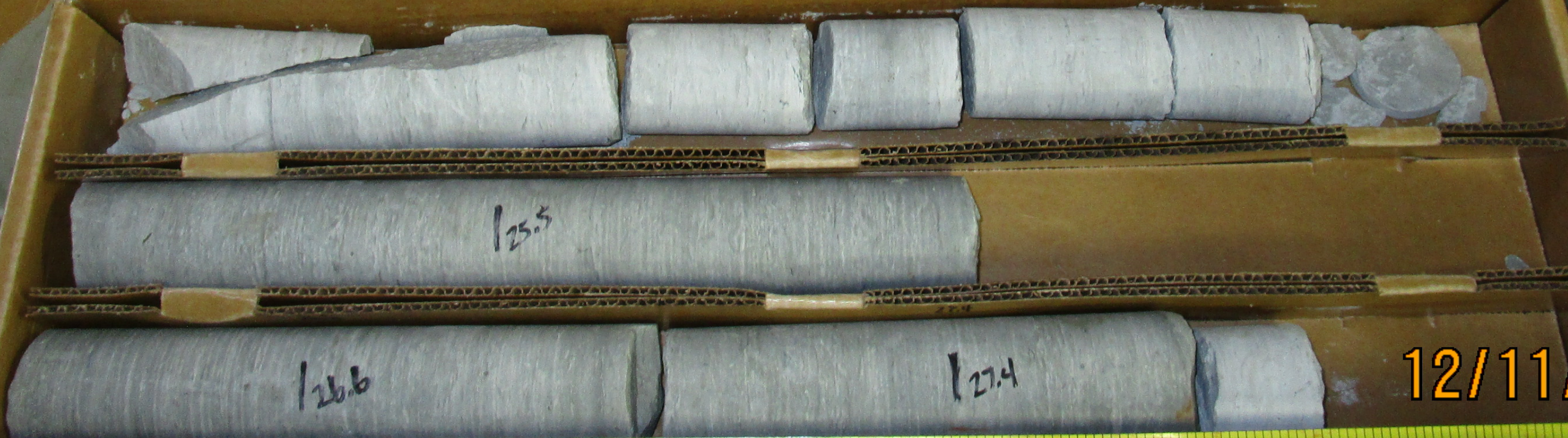
SN 046-0008 / 0009

Hole #1 11-24-2017

Depth 23 FT to 28 FT

Box 2 of 2

Sheet
#3



12/11/2017

I-57 over R x R in Kankakee

SN 046-0008 / 0009

Hole # 2 11-24-2017

Depth 14 Ft. to 23.5 Ft.

Box 1 of 2

Start
14 ft



12/11/2017

1-57 over R x R in Kankakee
SN 046-0008 / 0009

Hole #2 11-24-2017

Depth 23.5 FT to 29 FT

Box 2 of 2

Box 2
of 2
Cor 2-3



12/11/2017

Boring No.: 01 (N. Abut. NBL)
 Station: 142+12
 Offset: 47.0 ft Lt.
 Ground Surface Elev. 665.93

	N	Qu	w%
Augered Bitum. Shoulder 663.43			
Stiff to Very Stiff Black Silty Clay Loam / Silty Loam with minor gray & Brown Silty Clay Loam - All Fill	6	2.0P	19
	4	1.0P	20
	4	1.3P	22
	5	1.3P	22
Very Stiff Brown & Gray Silty Clay Fill with Some Layers of Black Silty Clay Loam Fill	6	2.1B	25
	6	2.0P	26
	9	3.8B	21
Very Stiff to Hard Gray, Black & Brown Sandy Clay Loam & Sandy Loam with Sand Seams - Fill	12	3.4S	14
	11	4.0P	16
	11	3.5P	17
	16	5.1S	16
Very Stiff Gray & Brown Sandy Clay Loam / Sandy Loam	12	3.9S	17
Medium Gray & Brown Fine to Coarse Sand - Minor Loam Layers	11		17
	23		21
Dense Gray Weathered Limestone	100/4"		12

Boring No.: 03 (Pier)
 Station: 144+20
 Offset: 55.0 ft Lt.
 Ground Surface Elev. 638.08

	N	Qu	w%
Augered Black & Brown Silty Clay Loam / Silty Loam Fill with Oversize Stone 0 - 3 Ft.	4	2.5P	16
Stiff to Very Stiff Black & Brown Silty Loam, Silty Clay Loam Fill with Gravel Pieces & Debris	10		13
	15	3.5P	16
Loose to Medium Brown Loamy Sand with Layers of Brown Sandy Clay Loam / Sandy Loam (Fill ?)	100/2"		13
Very Stiff Gray Silt / Silty Loam with Limestone Gravel Pieces and Sand & Gravel Pockets			
Dense Gray Limestone - Weathered Surface			

Boring No.: 04 (Pier)
 Station: 144+23
 Offset: 0.0 ft Centerline
 Ground Surface Elev. 638.49

	N	Qu	w%
Augered CA6, Black Silty Clay Loam / Silty Loam Fill with Heavy Gravel Pieces & Sand Layers - Fill	6	1.5P	15
Stiff Gray & Black Silt, Silty Clay Loam Fill with Gravel Pieces	3	0.5P	26
	4	0.5P	16
Soft Brown, Gray & Black Silty Loam, Silty Clay Loam with Sand Layers & Gravel Pieces	100/5"		9
Gray Limestone - Weathered Surface			

Boring No.: 05
 Station: 144+29
 Offset: 58.0 ft Rt.
 Ground Surface Elev. 638.70

	N	Qu	w%
Augered Black & Brown Silty Clay Loam Fill with Large Gravel & Oversize Gravel Pieces	5	1.5P	20
Stiff Black & Brown Silty Clay Loam, Silty Loam Fill with Gravel & Debris	12	3.0P	17
Very Stiff Brown & Gray Silty Loam, Silty Clay with Limestone Gravel Pieces	14		17
Medium Brown Fine to Coarse Loamy Sand with Layers of Brown Sandy Clay Loam / Sandy Loam	100/2"		9
Gray Limestone - Weathered Surface			

Boring No.: 02
 Station: 145+27
 Offset: 10.0 ft Rt.
 Ground Surface Elev. 665.51

	N	Qu	w%
Augered Black Silty Clay Loam Fill & Gray / Brown Silty Clay Loam Fill	8	3.5P	15
Very Stiff to Hard Gray & Brown Silty Clay Loam Till Fill with some Black Silty Clay Loam Layers	9	4.0B	17
Very Stiff to Hard Gray & Brown Sandy Clay Loam, Loam Fill & some Sand & Gravel Fill @ 20 Ft.	9	4.4S	19
	10	3.4B	16
	11	3.8S	17
	12	4.2S	17
	12	4.2S	14
	14	4.5P	13
	11	4.5P	18
	13	3.5P	15
Hard to Very Stiff Black, Gray & Brown Silty Clay Loam & Sandy Clay Loam Fill	11	4.0P	17
	12	4.0P	17
	11	4.0P	20
Very Stiff Gray & Black Silty Clay Loam	10	3.2B	24
	9	3.0B	19
Gray Limestone in Gray Silty Loam / Silty Clay Loam Matrix	12		9
Dense Gray Limestone	100/2"		

SUBSTRUCTURE=====North Abutment
 REFERENCE BORING =====B-01
 LRFD or ASD or SEISMIC =====LRFD
 PILE CUTOFF ELEV. =====662.31 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 660.31 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) =====None
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD =====ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) =====ft

TOTAL FACTORED SUBSTRUCTURE LOAD ===== 1300 kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 64.00 ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 1

Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 162.50 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 60.94 KIPS

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
418 KIPS	418 KIPS	230 KIPS	36 FT.

PILE TYPE AND SIZE ===== Steel HP 12 X 53
 Plugged Pile Perimeter===== 3.967 FT. Unplugged Pile Perimeter===== 5.800 FT.
 Plugged Pile End Bearing Area===== 0.983 SQFT. Unplugged Pile End Bearing Area===== 0.108 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL PLUGGED			NOMINAL UNPLUG'D			NOMINAL REQ'D BEARING (KIPS)	FACTORED LOSS FROM SCOUR or DD (KIPS)	FACTORED LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)	SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
659.43	0.88	1.00			2.5		16.3	3.6		5.1	5	0	0	3	3
656.93	2.50	1.00			7.0	13.8	23.3	10.3	1.5	15.4	15	0	0	8	5
654.43	2.50	1.00			7.0	13.8	45.5	10.3	1.5	27.4	27	0	0	15	8
651.93	2.50	2.10			11.9	28.9	56.0	17.4	3.2	44.7	45	0	0	25	10
649.43	2.50	2.00			11.5	27.6	92.4	16.9	3.0	64.2	64	0	0	35	13
646.43	3.00	3.80	9		21.7	52.4	108.6	31.7	5.7	95.4	95	0	0	52	16
643.93	2.50	3.40	12		16.6	46.9	133.5	24.3	5.1	120.6	121	0	0	66	18
641.43	2.50	4.00	11		18.8	55.1	145.4	27.5	6.0	147.3	145	0	0	80	21
638.93	2.50	3.50	11		17.0	48.2	184.4	24.8	5.3	174.6	175	0	0	96	23
636.43	2.50	5.10	16		20.6	70.3	188.5	30.1	7.7	202.9	188	0	0	104	26
633.93	2.50	3.90	12		18.4	53.7	180.1	27.0	5.9	226.9	180	0	0	99	28
631.43	2.50		11	Medium Sand	2.0	26.9	211.5	2.9	2.9	233.0	212	0	0	116	31
628.43	3.00		23	Medium Sand	5.0	56.3	405.1	7.3	6.2	261.0	261	0	0	144	34
627.43	1.00			Limestone	98.8	245.0	504.0	144.5	26.8	405.5	405	0	0	223	34.9
626.43	1.00			Limestone	98.8	245.0	602.8	144.5	26.8	550.0	550	0	0	302	35.9
625.43	1.00			Limestone	98.8	245.0	701.6	144.5	26.8	694.5	694	0	0	382	36.9
624.43	1.00			Limestone		245.0			26.8			0	0		

Pile Design Table for North Abutment utilizing Boring #B-01

Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)
Metal Shell 12"Φ w/.25" walls			Steel HP 10 X 42			Steel HP 12 X 84		
106	58	16	101	55	18	101	55	16
132	72	18	114	63	21	127	70	18
151	83	21	144	79	23	152	84	21
185	102	23	146	80	28	183	101	23
201	110	26	168	92	31	187	103	28
244	134	28	218	120	34	221	121	31
312	171	31	335	184	35	282	155	34
Metal Shell 14"Φ w/.25" walls			Steel HP 10 X 57			Steel HP 14 X 73		
102	56	13	103	57	18	78	43	13
129	71	16	117	64	21	116	64	16
160	88	18	147	81	23	146	80	18
182	100	21	149	82	28	178	98	21
225	124	23	172	95	31	211	116	23
241	132	26	226	124	34	219	121	28
296	163	28	454	250	36	263	145	31
386	212	31	Steel HP 12 X 53			319	175	34
Metal Shell 14"Φ w/.312" walls			95	52	16	578	318	36
102	56	13	121	66	18	Steel HP 14 X 89		
129	71	16	145	80	21	81	44	13
160	88	18	175	96	23	118	65	16
182	100	21	180	99	28	149	82	18
225	124	23	212	116	31	181	100	21
241	132	26	261	144	34	215	118	23
296	163	28	418	230	36	222	122	28
386	212	31	Steel HP 12 X 63			267	147	31
Metal Shell 16"Φ w/.312" walls			98	54	16	329	181	34
78	43	10	123	68	18	705	388	37
124	68	13	147	81	21	Steel HP 14 X 102		
154	85	16	178	98	23	82	45	13
191	105	18	182	100	28	120	66	16
214	118	21	214	118	31	151	83	18
267	147	23	269	148	34	183	101	21
282	155	26	497	273	36	218	120	23
350	192	28	Steel HP 12 X 74			225	124	28
466	256	31	99	55	16	270	149	31
Metal Shell 16"Φ w/.375" walls			125	69	18	337	185	34
78	43	10	149	82	21	810	445	37
124	68	13	181	99	23	Steel HP 14 X 117		
154	85	16	184	101	28	85	46	13
191	105	18	217	119	31	122	67	16
214	118	21	276	152	34	154	85	18
267	147	23	589	324	37	186	102	21
282	155	26	Steel HP 8 X 36			222	122	23
350	192	28	110	60	23	228	125	28
466	256	31	116	64	26	274	151	31
782	430	34	117	64	28	347	191	34
Steel HP 8 X 36			131	72	31	Precast 14"x 14"		
110	60	23	175	96	34	82	45	10
116	64	26	286	157	36	130	72	13
117	64	28				164	90	16
131	72	31				204	112	18
175	96	34				231	127	21
286	157	36						

SUBSTRUCTURE===== South Abutment
 REFERENCE BORING ===== B-02
 LRFD or ASD or SEISMIC ===== LRFD
 PILE CUTOFF ELEV. ===== 662.36 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 660.36 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== None
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft
 TOTAL FACTORED SUBSTRUCTURE LOAD ===== 1300 kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 64.00 ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 1
 Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 162.50 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 60.94 KIPS

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
418 KIPS	418 KIPS	230 KIPS	37 FT.

PILE TYPE AND SIZE ===== Steel HP 12 X 53
 Plugged Pile Perimeter===== 3.967 FT. Unplugged Pile Perimeter===== 5.800 FT.
 Plugged Pile End Bearing Area===== 0.983 SQFT. Unplugged Pile End Bearing Area===== 0.108 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL PLUGGED			NOMINAL UNPLUG'D			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)	SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
658.51	1.85	1.00			5.2		19.0	7.6		9.1	9	0	0	5	4
656.01	2.50	1.00			7.0	13.8	26.0	10.3	1.5	19.4	19	0	0	11	6
653.51	2.50	1.00			7.0	13.8	33.1	10.3	1.5	29.7	30	0	0	16	9
651.01	2.50	1.00			7.0	13.8	40.1	10.3	1.5	40.0	40	0	0	22	11
648.51	2.50	1.00			7.0	13.8	47.2	10.3	1.5	50.3	47	0	0	26	14
646.01	2.50	1.00			7.0	13.8	54.2	10.3	1.5	60.6	54	0	0	30	16
643.51	2.50	1.00			7.0	13.8	109.5	10.3	1.5	76.2	76	0	0	42	19
641.01	2.50	4.50	11		20.6	62.0	116.3	30.1	6.8	104.9	105	0	0	58	21
638.51	2.50	3.50	13		17.0	48.2	140.2	24.8	5.3	130.5	130	0	0	72	24
636.01	2.50	4.00	11		18.8	55.1	159.0	27.5	6.0	157.9	158	0	0	87	26
633.51	2.50	4.00	12		18.8	55.1	177.8	27.5	6.0	185.4	178	0	0	98	29
631.01	2.50	4.00	11		18.8	55.1	185.6	27.5	6.0	211.7	186	0	0	102	31
628.51	2.50	3.20	10		15.9	44.1	198.7	23.2	4.8	234.7	199	0	0	109	34
626.51	2.00	3.00			12.1	41.3	414.5	17.7	4.5	274.7	275	0	0	151	36
625.51	1.00			Limestone	98.8	245.0	513.3	144.5	26.8	419.2	419	0	0	234	36.9
624.51	1.00			Limestone	98.8	245.0	612.2	144.5	26.8	563.7	564	0	0	340	37.9
623.51	1.00			Limestone		245.0			26.8						

Pile Design Table for South Abutment utilizing Boring #B-02

Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)
Metal Shell 12"Φ w/.25" walls			Steel HP 10 X 42			Steel HP 12 X 84		
98	54	19	109	60	24	110	61	21
115	63	21	125	69	26	137	75	24
140	77	24	140	77	29	165	91	26
163	90	26	148	82	31	186	102	29
187	103	29	160	88	34	193	106	31
203	112	31	229	126	36	207	114	34
221	122	34	335	184	37	296	163	36
Metal Shell 14"Φ w/.25" walls			Steel HP 10 X 57			Steel HP 14 X 73		
70	39	16	90	49	21	93	51	19
121	67	19	111	61	24	127	70	21
140	77	21	128	70	26	158	87	24
170	93	24	144	79	29	191	105	26
197	108	26	152	83	31	223	122	29
224	123	29	163	90	34	229	126	31
242	133	31	238	131	36	244	134	34
263	145	34	454	250	38	335	184	36
Metal Shell 14"Φ w/.312" walls			Steel HP 12 X 53			Steel HP 14 X 89		
70	39	16	105	58	21	96	53	19
121	67	19	130	72	24	130	71	21
140	77	21	158	87	26	161	89	24
170	93	24	178	98	29	194	107	26
197	108	26	186	102	31	226	124	29
224	123	29	199	109	34	233	128	31
242	133	31	275	151	36	248	136	34
263	145	34	418	230	37	346	190	36
Metal Shell 16"Φ w/.312" walls			Steel HP 12 X 63			Steel HP 14 X 102		
82	45	16	107	59	21	98	54	19
147	81	19	133	73	24	131	72	21
166	91	21	161	88	26	163	90	24
202	111	24	180	99	29	197	108	26
233	128	26	188	103	31	229	126	29
264	145	29	201	110	34	236	130	31
283	156	31	283	156	36	251	138	34
306	168	34	497	273	38	354	194	36
Metal Shell 16"Φ w/.375" walls			Steel HP 12 X 74			Steel HP 14 X 117		
82	45	16	109	60	21	810	445	39
147	81	19	135	74	24	100	55	19
166	91	21	163	90	26	134	74	21
202	111	24	183	101	29	166	91	24
233	128	26	190	105	31	200	110	26
264	145	29	204	112	34	232	128	29
283	156	31	290	160	36	239	131	31
306	168	34	589	324	39	254	140	34
782	430	36				364	200	36
Steel HP 8 X 36						Precast 14"x 14"		
109	60	29				89	49	16
116	64	31				155	85	19
126	69	34				178	98	21
185	102	36				216	119	24
286	157	38				251	138	26