

Original Report Date: <u>4/29/22</u>	Proposed SN: <u>062-0074</u>	Route: <u>FAP 318 (IL 29)</u>
Revised Date: <u>4/13/23</u>	Existing SN: <u>062-0008</u>	Section: <u>(3-B) BR</u>
Geotechnical Engineer: <u>Joe Olson - IDOT D4</u>		County: <u>Marshall</u>
Structural Engineer: <u>Hurst-Roche, Inc.</u>		Contract: <u>68E33</u>

Indicate the proposed structure type, substructure types, and foundation locations (attach plan and elevation drawing): The proposed structure will be a 57'-0" long, single span bridge on a 10-degree skew. The new bridge consists of IL27-1830 PPC beams with a concrete deck set on integral abutments. According to information provided by the structural designer, the estimated factored load at each abutment is 882 kips. The TSL general plan and elevation is attached.

The new structure will be approximately 18 feet longer than the existing structure. The integral abutments will be located behind the existing abutments to allow sufficient waterway opening and construction of riprap-lined endslopes.

Stage construction is planned to maintain traffic on IL 29.

Discuss the existing boring data, existing plans foundation information, new subsurface exploration and need for any additional exploration to be provided with SGR Technical Memo (attach all data and subsurface profile plot): Existing boring data is limited to one soil boring log included in the 1944 bridge plans. The plans show soil profile of 22 feet of sand and gravel over 6.5 feet of clay over hard shale at El. 427.4. The existing bridge was built in 1948 with closed abutments set on spread footing foundations at El. 450.2.

Two soil borings were drilled in September 2021 for the proposed structure. One boring was drilled near each abutment by Geo Services Inc. The borings were logged by Terracon. The soil profile generally consists of an average 15 inches of pavement overlying up to 5 feet of silty loam fill. Below the fill is 20 to 30 feet of cohesive soil consisting of layers of silt, clay, silty loam, and silty clay loam. Below the cohesive soil is 6 to 10 feet of more granular material consisting of layers of sandy loam and sand. Below this is a gray hard shale encountered at El. 426.4 on the north side of Barrville Creek and at El. 434.4 on the south side. All standard penetration tests on the shale resulted in $N > 100$ blows per foot. SB-1 was drilled for the proposed north abutment and terminated in 1.5 feet of coal at El. 412.4. SB-2 was drilled for the south abutment and terminated in the referenced shale at El. 422.4. The boring logs and a subsurface profile are attached.

Provide the location and maximum height of any new soil fill or magnitude of footing bearing pressure. Estimate the amount and time of the expected settlement. Indicate if further testing, analysis, and/or ground improvement/treatment is necessary: No additional soil fill height is planned for the project, so settlement should be minimal. No further settlement analysis or ground treatment is necessary.

Identify any new cuts or fill slope angles and heights. Estimate the factor of safety against slope failure. Indicate if further testing, analysis or ground improvement/treatment is necessary: New 1V:2H slopes will be established between the streambed and integral abutments. These cut slopes will be a maximum of 7 feet high and ultimately lined with Class A4 riprap. Due to the relatively low slope height, the factor of safety against slope failure can be assumed to exceed 1.5 without detailed analysis. No ground improvement or treatment is necessary.

Indicate at each substructure, the 100-year and 200-year total scour depths in the Hydraulics report, the non-granular scour depth reduction, the proposed ground surface, and the recommended foundation design scour elevations: The new integral abutments will be set back away from the channel and positioned behind 1V:2H slopes lined with Class A4 riprap. This is considered an adequate level of scour protection such that no scour is anticipated below the bottom of the abutments. The design scour elevations at the abutments are therefore set to El. 460.45.

Determining the seismic soil site class, the seismic performance zone, the 0.2 and 1.0 second design spectral accelerations and indicate if that the soils are liquefiable: Seismic soil site class = D, $SPZ = 1$, $SDS = 0.165g$ and $SD1 = 0.105g$. Liquefaction analysis is not required for sites in SPZ 1. The IDOT Seismic Site Class Determination spreadsheet is attached along with a screenshot from the AASHTO Guide Specifications for LRFD Seismic Bridge Design software, Version 2.1.

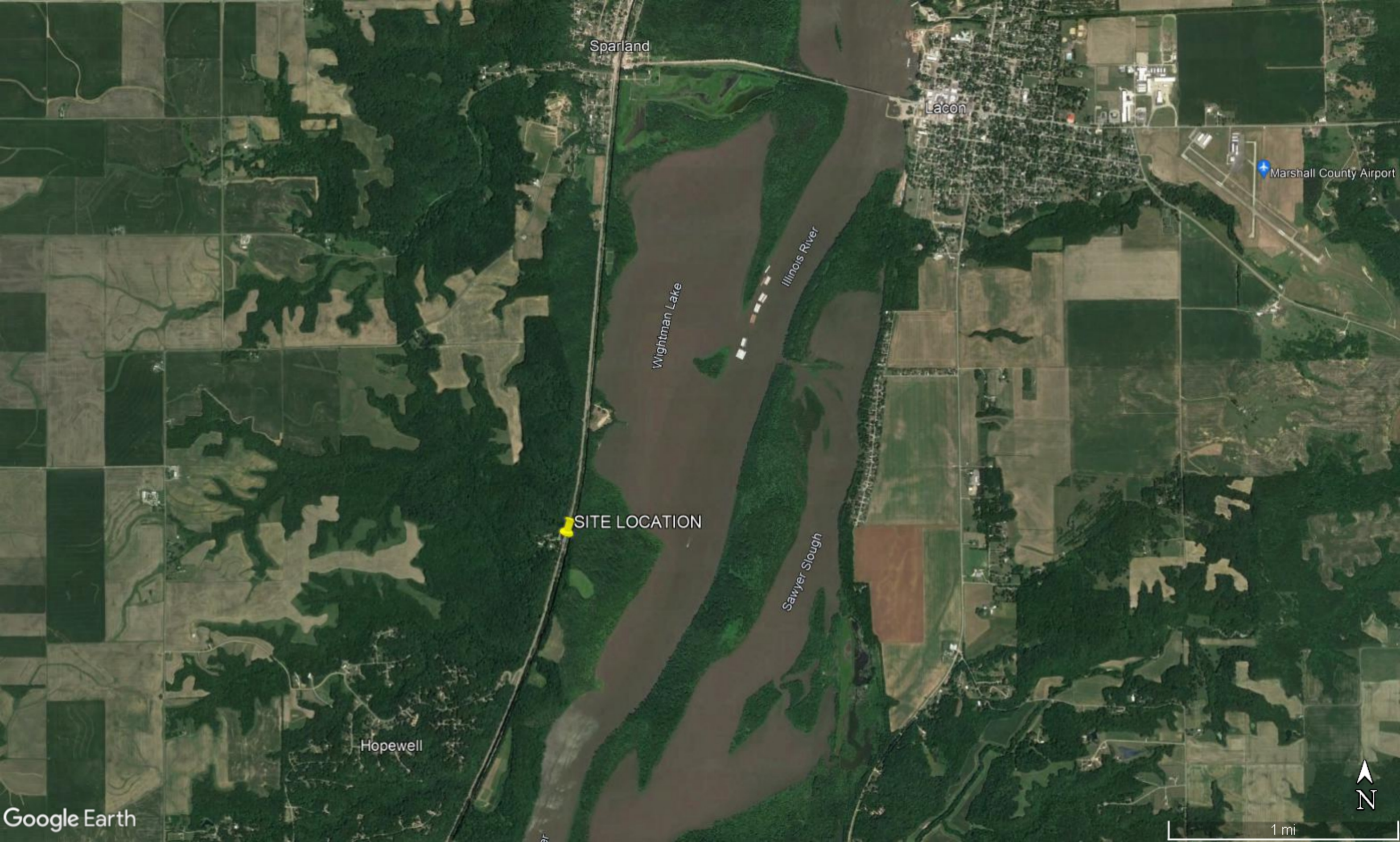
Confirm feasibility of the proposed foundation or wall type and provide design parameters. Attach a pile design table indicating feasible pile types, various nominal required bearings, factored resistances available and corresponding estimated lengths at locations where piles will be used. Provide factored bearing resistance and unit sliding resistance at various elevations and confirm no ground improvement/treatment is necessary where spread footings are proposed. Estimated top of rock elevations as well as preliminary factored unit side and tip resistance values shall be indicated when drilled shafts are proposed: It is recommended that H-piles be driven to their maximum nominal required bearing in shale. The attached Pile Design Tables provide the maximum bearing values for various sizes of H-pile. The tables also provide factored resistance values, estimated pile lengths, and pile cutoff elevations.

A test pile is recommended for the north abutment where the top of the shale is expected to be deepest.

The structure designer should evaluate the lateral resistance of the piles supporting the abutments considering both soil and structure properties. Soil parameters for generating P-y curves with the LPILE computer program are provided in the attached table.

Calculate the estimated water surface elevation and determine the need for cofferdams (type 1 or 2), and seal coat: The attached TSL shows EWSE = 459.3. The proposed structure is a single span bridge. Since there are no piers or other foundations to be constructed in the waterway, there should be no need for cofferdams.

Assess the need for sheeting or soil retention or temporary construction slope and provide recommendation for other construction concerns: Temporary soil retention will be needed since stage construction is planned. The TSL indicates the new abutments will be installed behind the existing abutments. The backfill placed behind the first stage of the new abutments will need to be retained for an estimated 7 foot height along the stage line to allow for construction of the second stage. This should be feasible with temporary sheet piling designed according to IDOT Bridge Manual Design Guide 3.13.1.



Sparland

Lacon

Marshall County Airport

Wightman Lake

Illinois River

SITE LOCATION

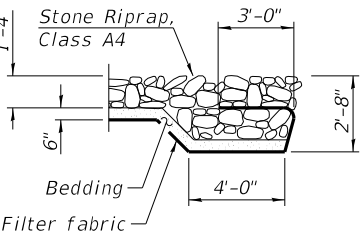
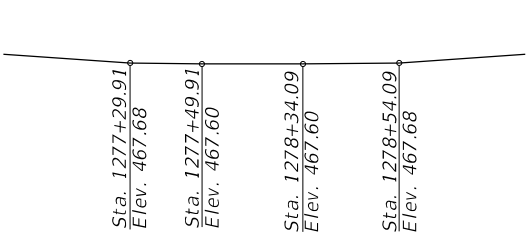
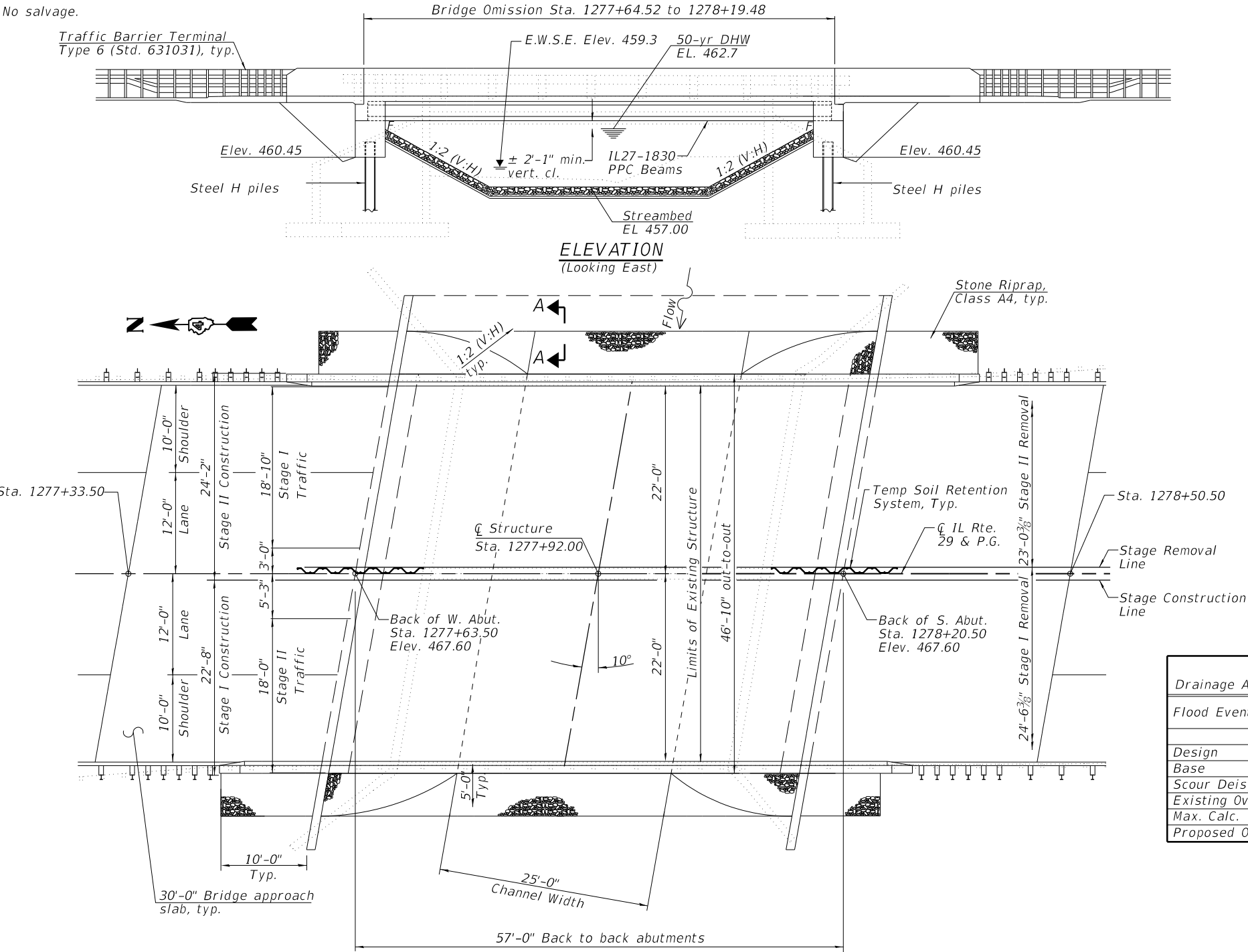
Sawyer Slough

Hopewell

Benchmark: M-233 USC & GS East end of South Abutment Sta. 1262+16, 25' Rt, Elev. 468.06

Existing Structure: SN 062-0008 originally built in 1948 as Section 3-B. The existing single span, cast in place reinforced concrete T-beam superstructure is supported by closed abutments on spread footings. The back to back abutment length is 39'-0" with no skew and out-to-out width of 45'. Traffic to be maintained using stage construction.

No salvage.



PROFILE GRADE
Along Centerline Roadway

SECTION A-A

DESIGN SCOUR ELEVATION TABLE

Event / Limit State	N. Abut.	S. Abut.	Item 113
Q100	460.45	460.45	8
Q500	460.45	460.45	
Design	460.45	460.45	
Check	460.45	460.45	

WATERWAY INFORMATION

Drainage Area = 2.0 sq. mi.					Existing Overtopping Elev.	=467.60	at Sta. 1277+92		
					Proposed Overtopping Elev.	=467.60	at Sta. 1277+92		
Flood Event	Freq. Yr.	Discharge Ft ³ /s	Waterway Opening Ft ²		Natural H.W.E. ft.	Head - Ft.		Headwater El. Ft.	
			Exist.	Prop.		Exist.	Prop.	Exist.	Prop.
	10	1020	164	194	462.4	1.5	0.5	464.0	463.0
Design	50	1720	176	208	462.7	2.5	1.1	465.2	463.9
Base	100	2050	178	212	462.8	3.9	1.2	466.7	464.0
Scour Deisgn Check	200	2250	178	214	462.8	4.8	2.8	467.6	465.6
Existing Overtopping	200	2250	178	NA	462.8	3.9	NA	466.7	NA
Max. Calc.	500	2870	203	244	463.5	4.4	3.8	467.8	467.2
Proposed Overtopping	500	2870	NA	244	463.5	NA	3.8	NA	467.2

DESIGN SPECIFICATIONS

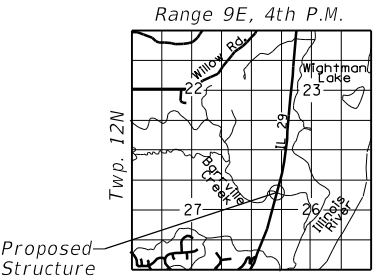
2020 AASHTO LRFD Bridge Design Specifications, 9th Edition

LOADING HL-93

Allow 50#/sq. ft. for future wearing surface.

SEISMIC DATA

Seismic Performance Zone (SPZ) = 1
Design Spectral Acceleration at 1.0 sec. (SD1) = 0.105
Design Spectral Acceleration at 0.2 sec. (SDS) = 0.165
Soil Site Class = D



LOCATION SKETCH

HIGHWAY CLASSIFICATION

FAP 318 IL Rte. 29
Functional Class: Other Principal Arterial
ADT: 6600 (2021): 8132 (2032)
ADTT: 726 (2021): 895 (2032)
DHV: 813
Design Speed: 55 m.p.h.
Posted Speed: 55 m.p.h.
Two Way Traffic
Directional Distribution: 50:50

DESIGN STRESSES

FIELD UNITS

f'c = 3,500 psi
f'c = 4,000 psi (Superstructure)
f'y = 60,000 psi (Reinforcement)

PRECAST PRESTRESSED UNITS

f'c = 8,500 psi
f'ci = 6,500 psi
fpu = 270,000 psi (0.6" \odot Low Relaxation Strands)
fpbt = 202,300 psi (0.6" \odot Low Relaxation Strands)

STATE OF ILLINOIS
DEPARTMENT OF TRANSPORTATION

GENERAL PLAN AND ELEVATION
STRUCTURE NO. 062-0074

SHEET 1 OF 2

GENERAL PLAN
IL 29 OVER BARRVILLE CREEK
F.A.P. RTE. 318 - SEC. (3-B) BR
MARSHALL COUNTY
STATION 1277+92.00
STRUCTURE NO. 062-0074

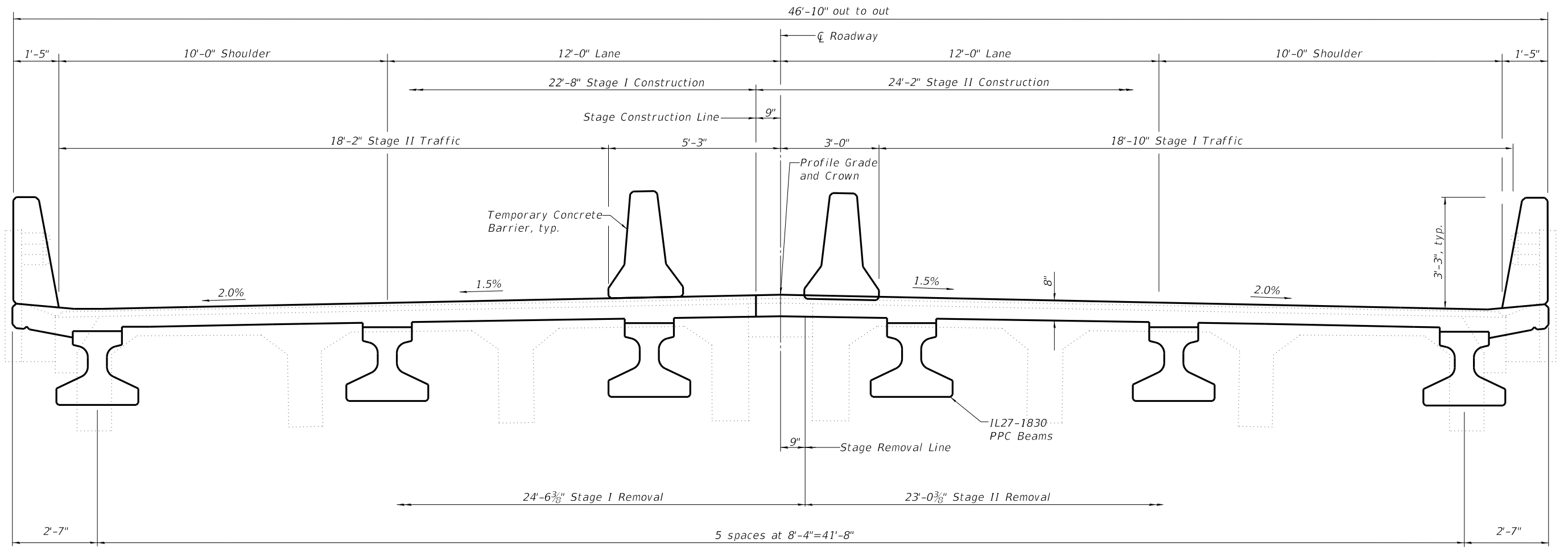
F.A. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
318	(3-B) BR	MARSHALL	2	1
CONTRACT NO. 68E33				
ILLINOIS FED. AID PROJECT				



Hurst-Rosche, Inc.
1400 E. TREMONT ST.
HILLSBORO, IL
PH: 217.532.3959
JOB NO. 192-3091

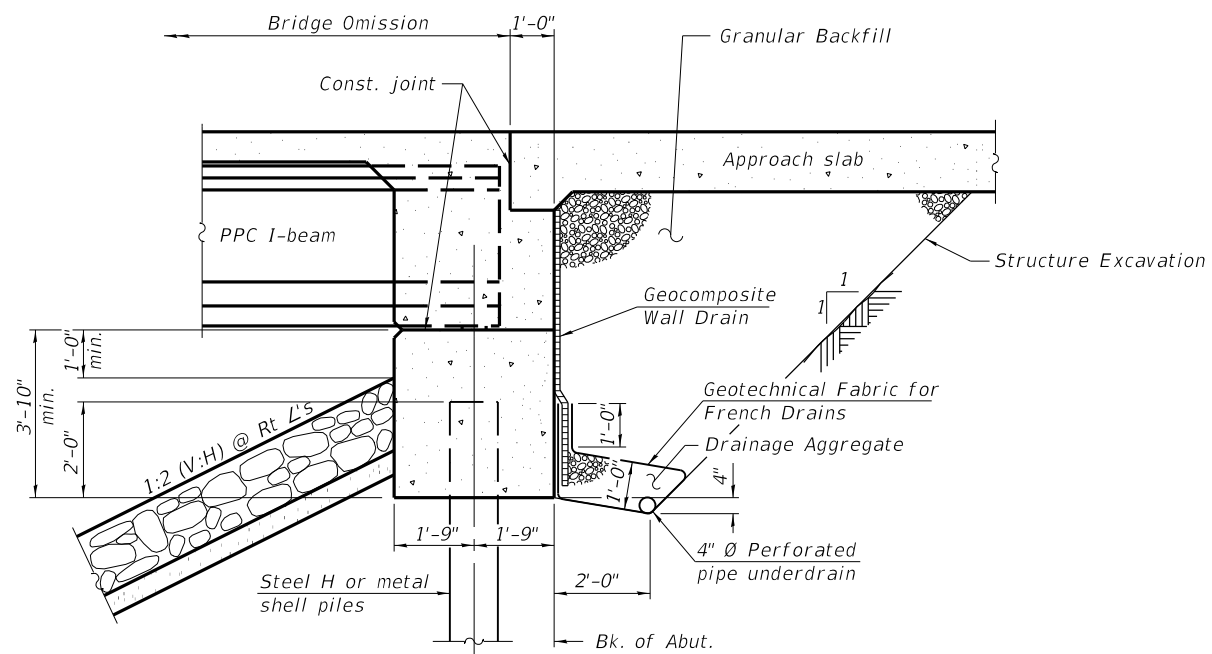
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	CJC	
PLOT SCALE	CHECKED -	REVISD -
	CJC	
PLOT DATE	DRAWN -	REVISD -
1/20/2022	BP	
	CHECKED -	REVISD -
	CJC	

MODEL: \$MODELNAME\$
FILE NAME: X:\Projects\Current\192-3091 IDOT D4 WO11 IL 29 over Barrville Creek (TSL-Hyd Rep)\Dgn\068E33-001-GP&E.dgn



CROSS SECTION

(Looking North)



SECTION THRU INTEGRAL ABUTMENT
(Horiz. dim. @ Rt. L's)

GENERAL PLAN & ELEVATION
IL 29 OVER BARRVILLE CREEK
SECTION (3-B) BR
MARSHALL COUNTY
STATION 1277+92.00
STRUCTURE NO. 062-0074

STATE OF ILLINOIS
DEPARTMENT OF TRANSPORTATION

TYPICAL SECTION AND DETAILS
STRUCTURE NO. 062-0074

SHEET 2 OF 2 SHEETS

F.A.S. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
318	(3-B) BR	MARSHALL	2	2
CONTRACT NO. 68E33				
ILLINOIS FED. AID PROJECT				

USER NAME =	DESIGNED - CJC	REVISED -
PLOT SCALE =	CHECKED - CJC	REVISED -
PLOT DATE = 1/20/2022	DRAWN - BP	REVISED -
	CHECKED - CJC	REVISED -



SOIL BORING LOG

ROUTE FAP 318 (IL 29) DESCRIPTION Structure boring for north abutment LOGGED BY JS (Terracon)

SECTION (3-B) BR LOCATION IL-29 over Barrville Creek, SEC. 26, TWP. 12 N, RNG. 9, 4th PM,
Latitude 40.9973, Longitude -89.4432

COUNTY Marshall County DRILLING METHOD Mud Rotary HAMMER TYPE Automatic

STRUCT. NO. 062-0008 (EX)
Station 1277+92

BORING NO. SB-1
Station 1277+67
Offset 18.0 ft RT
Ground Surface Elev. 467.40 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)	Surface Water Elev. _____ ft	D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
				Stream Bed Elev. _____ ft				
				Groundwater Elev.: _____ ft				
				First Encounter <u>458.9</u> ft ▼				
				Upon Completion <u>456.9</u> ft ▼				
				After _____ Hrs. _____ ft				
Asphalt, approximate thickness of 2"	467.20			Silt Loam, with gravel and cobbles, brown, medium stiff to stiff, very moist		5		
Concrete, approximate thickness of 16"	465.90	5				6		14
FILL: Silty Loam, trace gravel, brown, very moist		4	17			8		
		4						
	463.40	4				3		
Clay, brown, stiff		4	1.2			3		15
	-5	4	B			4		
		3				4		
		3	1.1		440.40	3		26
		3	B	Silty Clay Loam, brown, stiff, wet to very moist		2		
		3				3		
		3	1.6			5		16
	-10	3	B			6		
	456.40							
Silt Loam, brown, medium stiff, moist to very moist		3						
		5	17					
		5						
		2				1		
		2	13		432.90	3		12
	-15	3		Sandy Clay Loam, with gravel and coal, brown to black, loose, moist	-35	6		
		5						
No Recovery from 16.5 to 19.5		3	-					
		1						
					429.40			
		1		Sand, brown, medium dense, moist		12		
		3	15			8		12
	447.40	4			-40	11		

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

Page 2 of 2

Date 9/23/21

Surface Water Elev.	_____	ft
Stream Bed Elev.	_____	ft
Groundwater Elev.:		
First Encounter	458.9	ft ▼
Upon Completion	456.9	ft ▼
After _____ Hrs.	_____	ft

Sand, brown, medium dense, moist (<i>continued</i>)	426.40			
Shale, highly weathered, gray, hard, very moist to wet				
		50/3"	14	
	-45			
		50/2"	20	
	-50			
	413.90			
Coal Seam, black, hard, wet		50/3"	24	
	412.40			
End of Boring	-55			
	-60			

BBS, form 137 (Rev. 8-99)



SOIL BORING LOG

ROUTE FAP 318 (IL 29) DESCRIPTION Structure boring for south abutment LOGGED BY JS (Terracon)

SECTION (3-B) BR LOCATION IL-29 over Barrville Creek, SEC. 26, TWP. 12 N, RNG. 9, 4th PM,
Latitude 40.9972, Longitude -89.4431

COUNTY Marshall County DRILLING METHOD Mud Rotary HAMMER TYPE Automatic

STRUCT. NO. 062-0008 (EX)
062-0074 (PR)
Station 1277+92

BORING NO. SB-2
Station 1278+28
Offset 16.0 ft LT
Ground Surface Elev. 467.40 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)	Surface Water Elev. _____ ft	D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
				Stream Bed Elev. _____ ft				
				Groundwater Elev.: _____ ft				
				First Encounter <u>459.9</u> ft ▼				
				Upon Completion <u>457.4</u> ft ▼				
				After _____ Hrs. _____ ft				
Asphalt, approximate thickness of 13" _____ 466.30				Clay, trace gravel, medium stiff to soft (<i>continued</i>) _____		0		
FILL: Silt Loam, trace gravel, brown and orange _____	1					0	dist.	22
	4		16			2		
	2							
				443.90				
	1			Sandy Loam, brown, loose to medium dense, wet _____		4		
	1		24			3		23
	2					4		
	-5					-25		
461.40								
Silt Loam, trace gravel, brown, medium stiff, very moist to wet _____	4					8		
	4		16			6		18
	4					8		
	4					10		
	3		22			8		13
	3					6		
	-10					-30		
456.90								
Silt, brown, very soft, wet _____								
	0							
	0		30					
	0							
	0							
	0		25			50		
	1					50/2"		19
	-15					-35		
450.90								
Silt Loam, trace gravel, brown, wet, medium stiff _____	1							
	2		20					
	3							
448.40						50/4"		16
	0							
Clay, trace gravel, medium stiff to soft _____	2	1.0	26					
	2	B						
	-20					-40		

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



SOIL BORING LOG

ROUTE FAP 318 (IL 29) DESCRIPTION Structure boring for south abutment LOGGED BY JS (Terracon)

SECTION (3-B) BR LOCATION IL-29 over Barrville Creek, SEC. 26, TWP. 12 N, RNG. 9, 4th PM,
Latitude 40.9972, Longitude -89.4431

COUNTY Marshall County DRILLING METHOD Mud Rotary HAMMER TYPE Automatic

STRUCT. NO. 062-0008 (EX)
Station 062-0074 (PR)
1277+92

BORING NO. SB-2
Station 1278+28
Offset 16.0 ft LT
Ground Surface Elev. 467.40 ft

D E P T H	B L O W S	U C S Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

Surface Water Elev.	_____	ft
Stream Bed Elev.	_____	ft
Groundwater Elev.:		
First Encounter	<u>459.9</u>	ft ▼
Upon Completion	<u>457.4</u>	ft ▽
After _____ Hrs.	_____	ft

Shale, slightly weathered, gray,
hard, wet (*continued*)

422.40 -45

End of Boring

-50

-55

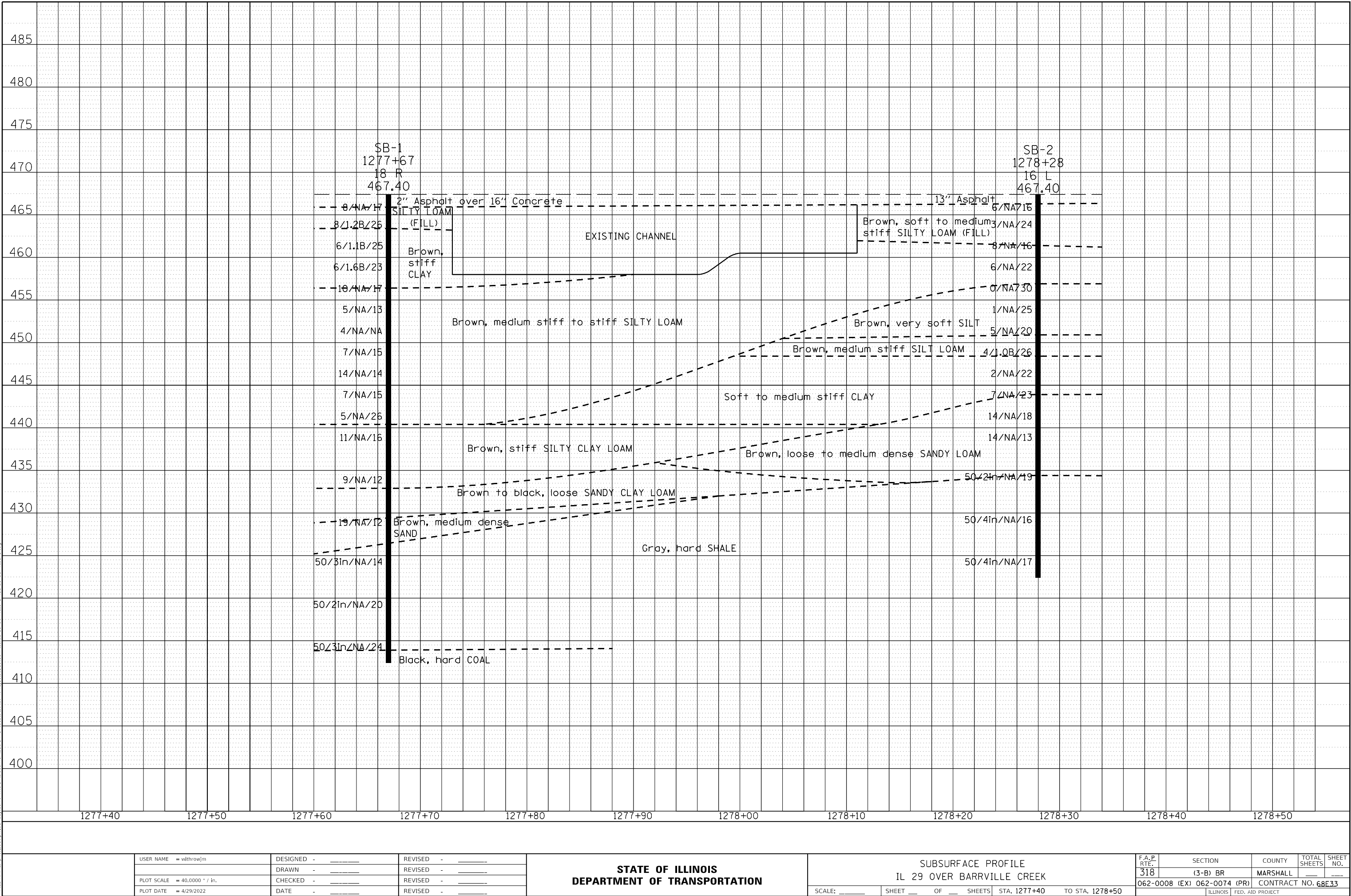
-60

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

PLAN	SURVEYED	BY	DATE
	PLOTTED		
	ALIGNMENT CHECKED		
NOTE BOOK NO.	CADD FILE NAME		

PROFILE	SURVEYED	BY	DATE
	PLOTTED		
	GRADES CHECKED		
NOTE BOOK NO.	STRUCTURE NOTATION CHNG		

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SEISMIC SITE CLASS DETERMINATION

PROJECT TITLE=====

Substructure 1

Base of Substruct. Elev. (or ground surf for bents)460.45ft.

Pile or Shaft Dia.12inches

Boring NumberSB-1

Top of Boring Elev.467.4ft.

Approximate Fixity Elev.454.45 ft.

Individual Site Class Definition:

N (bar):25 (Blows/ft.) Soil Site Class D <----Controls

N_{ch} (bar):25 (Blows/ft.) Soil Site Class D

s_u (bar):(ksf) NA, H < 0.1*H (Soil)

Seismic Soil Column	Bot. Of Sample	Sample	Layer Description
Depth	Elevation	Thick. N Qu	Boundary
(ft)		(ft.) (tsf)	
	464.9	2.50 8	
	463.4	1.50 8	B
	460.9	2.50 8 1.20	
	458.4	2.50 6 1.10	
	456.4	2.00 6 1.60	B
0.6	453.9	2.50 10	
3.1	451.4	2.50 5	
5.6	448.9	2.50 4	
8.1	446.4	2.50 7	
10.6	443.9	2.50 14	
13.1	441.4	2.50 7	
14.6	439.9	1.50 5	B
17.1	437.4	2.50 11	
19.6	434.9	2.50 11	
22.1	432.4	2.50 9	B
24.1	430.4	2.00 9	
25.1	429.4	1.00 9	B
27.1	427.4	2.00 19	
28.1	426.4	1.00 19	B
100.0	354.5	71.90 100 5.00	R

Substructure 2

Base of Substruct. Elev. (or ground surf for bents)460.45ft.

Pile or Shaft Dia.12inches

Boring NumberSB-2

Top of Boring Elev.467.4ft.

Approximate Fixity Elev.454.45 ft.

Individual Site Class Definition:

N (bar):14 (Blows/ft.) Soil Site Class E

N_{ch} (bar):17 (Blows/ft.) Soil Site Class D <----Controls

s_u (bar):4.12 (ksf) Soil Site Class C

Seismic Soil Column	Bot. Of Sample	Sample	Layer Description
Depth	Elevation	Thick. N Qu	Boundary
(ft)		(ft.) (tsf)	
	464.9	2.50 6	
	463.9	1.00 6	
	461.4	2.50 3	B
	458.9	2.50 8	
	456.9	2.00 6	B
0.1	454.4	2.50 1	
2.1	452.4	2.00 1	
3.6	450.9	1.50 1	B
6.1	448.4	2.50 5	B
8.6	445.9	2.50 4 1.00	
10.6	443.9	2.00 2	B
13.1	441.4	2.50 7	
15.6	438.9	2.50 14	
18.1	436.4	2.50 14	
20.1	434.4	2.00 14	B
100.0	354.5	79.90 100 5.00	R

Substructure 3

Base of Substruct. Elev. (or ground surf for bents)ft.

Pile or Shaft Dia.inches

Boring Number

Top of Boring Elev.ft.

Approximate Fixity Elev.ft.

Individual Site Class Definition:

N (bar):(Blows/ft.) NA

N_{ch} (bar):(Blows/ft.) NA

s_u (bar):(ksf) NA

Seismic Soil Column	Bot. Of Sample	Sample	Layer Description
Depth	Elevation	Thick. N Qu	Boundary
(ft)		(ft.) (tsf)	

Substructure 4

Base of Substruct. Elev. (or ground surf for bents)ft.

Pile or Shaft Dia.inches

Boring Number

Top of Boring Elev.ft.

Approximate Fixity Elev.ft.

Individual Site Class Definition:

N (bar):(Blows/ft.) NA

N_{ch} (bar):(Blows/ft.) NA

s_u (bar):(ksf) NA

Seismic Soil Column	Bot. Of Sample	Sample	Layer Description
Depth	Elevation	Thick. N Qu	Boundary
(ft)		(ft.) (tsf)	

Global Site Class Definition: Substructures 1 through 2

N (bar):20 (Blows/ft.) Soil Site Class D
N_{ch} (bar):21 (Blows/ft.) Soil Site Class D <----Controls
s_u (bar):(ksf) NA, H < 0.1*H (Total)

AASHTO Guide Specifications for LRFD Seismic Bridge Design

This program allows the user to obtain seismic design parameters for sites in the 50 states of the United States, Puerto Rico and the U.S. Virgin Islands. Ground motion maps are also included in PDF format.

Click on Okay to begin calculation

Correct application of the data obtained is the responsibility of the user. This software is for design and/or analysis.



ANALYSIS - Map Parameters, Design Parameters, and Response Spectra

File Project Name Help

Input Data and Parameter Calculations

Select Geographic Region

Conterminous 48 States

Guidelines Edition

2007 AASHTO Bridge Design Guidelines

Specify Site Location by Latitude-Longitude or Zip Code

☒ Latitude-Longitude : Recommended ☐ Zip Code

40.99647

-89.4434

Latitude (50.0 to 24.6)

Longitude (-125.0 to -65.0)

Calculate Basic Design Parameters

Probability of Exceedance

7% PE in 75 years

Calculate
PGA, S_s, and S₁

Calculate
A_s, S_{Ds}, and S_{D1}

Calculate Response Spectra

Map Spectrum

Design Spectrum

View Spectra

Output Calculations and Ground Motion Maps

2007 AASHTO Bridge Design Guidelines
AASHTO Spectrum for 7% PE in 75 years

Latitude = 40.996470

Longitude = -89.443400

Site Class B

Data are based on a 0.05 deg grid spacing.

Period (sec)	S _a (g)	
0.0	0.045	PGA - Site Class B
0.2	0.103	S _s - Site Class B
1.0	0.044	S ₁ - Site Class B

Conterminous 48 States

2007 AASHTO Bridge Design Guidelines

Spectral Response Accelerations S_{Ds} and S_{D1}

Latitude = 40.996470

Longitude = -89.443400

A_s = F_{pga}PGA, S_{Ds} = F_aS_s, and S_{D1} = F_vS₁

Site Class D - F_{pga} = 1.60, F_a = 1.60, F_v = 2.40

Data are based on a 0.05 deg grid spacing.

Period (sec)	S _a (g)	
0.0	0.071	A _s - Site Class D
0.2	0.165	S _{Ds} - Site Class D
1.0	0.105	S _{D1} - Site Class D

Clear Output

View Maps

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Pile Design Tables

North Abutment - Boring SB-1

Pile Type & Size	Nominal Required Bearing (kips)	Factored Resistance Available (kips)	Estimated Length (feet)	Pile Cutoff Elevation
HP 10 x 57	454	250	44	462.5
HP 12 x 53	418	230	42	462.5
HP 12 x 63	497	273	43	462.5
HP 12 x 74	589	324	45	462.5
HP 12 x 84	664	365	46	462.5
HP 14 x 73	578	318	43	462.5
HP 14 x 89	705	388	45	462.5
HP 14 x 102	810	445	46	462.5
HP 14 x 117	929	511	48	462.5

South Abutment - Boring SB-2

Pile Type & Size	Nominal Required Bearing (kips)	Factored Resistance Available (kips)	Estimated Length (feet)	Pile Cutoff Elevation
HP 10 x 57	454	250	37	462.5
HP 12 x 53	418	230	34	462.5
HP 12 x 63	497	273	36	462.5
HP 12 x 74	589	324	38	462.5
HP 12 x 84	664	365	39	462.5
HP 14 x 73	578	318	35	462.5
HP 14 x 89	705	388	37	462.5
HP 14 x 102	810	445	39	462.5
HP 14 x 117	929	511	41	462.5

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Soil Parameters for Lateral Pile Analysis

Location	Expected Groundwater Elevation (ft)	Elevation (ft)	Unit Weight (pcf)	Cohesion (psf)	Phi (degrees)	K (pci)	E ₅₀
North Abutment SB-1	457	460 to 456	120	1300	--	393	0.008
		456 to 440	115	1000	--	233	0.009
		440 to 429	118	1500	--	500	0.007
		429 to 426	115	--	34	--	--
		426 to 412	130	>4500	--	1500	0.005
South Abutment SB-2	457	460 to 457	115	1000	--	233	0.009
		457 to 451	112	250	--	<30	>0.02
		451 to 448	115	750	--	100	0.010
		448 to 444	120	1000	--	233	0.009
		444 to 434	112	--	33	--	--
		434 to 422	130	>4500	--	1500	0.005