

TOP OF BEAM ELEVATIONS

	Beam 1	Beam 2	Beam 3	Beam 4	Beam 5
⊕ Brg. W. Abut.	797.23	797.71	798.34	798.95	799.54
⊕ Pier 1	800.21	800.64	801.21	801.75	802.26
Splice 1 (W36x210)	800.92	801.33	801.89	802.41	802.90
Splice 1 (W36x170)	800.90	801.31	801.87	802.38	802.88
Splice 2 (W36x170)	804.42	804.72	805.16	805.57	805.95
⊕ Pier 2	804.69	804.98	805.41	805.81	806.18
⊕ Pier 3	806.45	806.66	807.01	807.33	807.62
Splice 3 (W36x170)	806.66	806.86	807.21	807.51	807.80
Splice 4 (W36x170)	808.03	808.14	808.38	808.59	808.77
Splice 4 (W36x280)	808.04	808.15	808.39	808.60	808.78
⊕ Pier 4	808.23	808.30	808.52	808.70	808.85
Splice 5 (W36x280)	808.39	808.44	808.63	808.78	808.91
Splice 5 (W36x210)	808.40	808.44	808.63	808.78	808.91
⊕ Brg. E. Abut.	808.45	808.39	808.48	808.52	808.55

Top of Beam Elevations are given for fabrication only.
Elevations have been adjusted up to account for
Dead Load Deflection.

INTERIOR GIRDER MOMENT TABLE

	0.4 Sp. 1	Pier 1	0.5 Sp. 2	Pier 2	0.5 Sp. 3***	Pier 3	0.5 Sp. 4	Pier 4	0.6 Sp. 5
<i>I_s</i> (in ⁴)	13,200	13,200	10,500	10,500	10,500	10,500	10,500	18,900	13,200
<i>I_c</i> (n) (in ⁴)	31,087	-----	26,380	-----	-----	-----	26,380	-----	31,087
<i>I_c</i> (3n) (in ⁴)	22,554	-----	19,276	-----	-----	-----	19,276	-----	22,554
<i>S_s</i> (in ³)	720	720	581	581	581	581	581	1035	720
<i>S_c</i> (n) (in ³)	1008	-----	831	-----	-----	-----	831	-----	1008
<i>S_c</i> (3n) (in ³)	905	-----	750	-----	-----	-----	750	-----	905
<i>ψ</i> (K/ft.)	0.98	1.51	0.94	1.49	1.48	1.50	0.96	1.53	1.00
<i>M_ℓ</i> (K)	37	1191	544	902	167	678	410	1830	609
<i>sℓ</i> (K/ft.)	0.55	-----	0.55	-----	-----	-----	0.55	-----	0.55
<i>Msℓ</i> (K)	42	-----	382	-----	-----	-----	300	-----	368
<i>M_ℓ</i> (K)	413	453	752	417	198	410	736	652	832
<i>M</i> (Imp) (K)	115	113	164	103	54	101	162	146	188
<i>5₃(M_ℓ+I)</i> (K)	880	943	1527	867	420	852	1497	1330	1700
<i>Ma</i> (K)	1247	2774	3189	2300	764	1989	2869	4108	3480
<i>* Mu</i> (K)	4290	-----	3580	-----	-----	-----	3892	-----	4485
<i>fsℓ non-comp(k.s.i.)</i>	0.6	19.9	11.2	18.7	3.4	14.0	8.5	21.2	10.2
<i>fsℓ (comp) (k.s.i.)</i>	0.6	-----	6.1	-----	-----	-----	4.8	-----	4.9
<i>fs₅(ℓ+I) (k.s.i.)</i>	10.5	15.7	22.1	17.9	8.7	17.6	21.6	15.4	20.3
<i>fs (Overload) (k.s.i.)</i>	11.7	35.6	39.4	36.6	12.1	31.6	34.9	36.6	35.4
<i>** fs (Total) (k.s.i.)</i>	-----	46.3	-----	47.6	15.7	41.1	-----	47.6	-----
<i>VR</i> (K)	65	-----	65	-----	-----	-----	67	-----	64

* Compact, Braced Section
** Non-compact Section
*** Entire Span treated as negative moment region as total negative moments are larger than total positive moments.

INTERIOR GIRDER REACTION TABLE

	W. Abut.	Pier 1	Pier 2	Pier 3	Pier 4	E. Abut.
<i>R_ℓ</i> (K)	20.4	143.1	120.6	104.8	181.6	55.2
<i>R_ℓ</i> (K)	44.3	59.4	58.7	57.6	69.2	48.3
<i>Imp.</i> (K)	12.3	14.8	14.4	14.2	15.5	11.0
<i>R (Total) (K)</i>	77.0	217.3	193.7	176.6	266.3	114.5

I_s and *S_s* are the moment of inertia and section modulus of the steel section used in computing *fs* (Total & Overload).
I_c (n) and *S_c* (n) are the moment of inertia and section modulus of the composite section used in computing stresses due to Live Load.
I_c (3n) and *S_c* (3n) are the moment of inertia and section modulus of the composite section used in computing stresses due to superimposed Dead Loads. (See AASHTO 10.38)
VR is the maximum Live Load + Impact shear range in span.
Ma (Applied Moment) = 1.3(*M_ℓ* + *Msℓ* + *5₃(M_ℓ + *M* (Imp)))).
The Plastic Moment capacity (*Mu*) is computed according to AASHTO 10.48.1 and 10.50.1.1.
fs (Overload) is the sum of the stresses due to *M_ℓ* + *Msℓ* + *5₃(M_ℓ + *M* (Imp)))).
fs (Total) is the sum of the stresses due to 1.3(*M_ℓ* + *Msℓ* + *5₃(M_ℓ + *M* (Imp)))).***

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STRUCTURAL STEEL DETAILS

WESTBOUND HARRISON AVENUE
OVER UP & CC&P RAILROAD
F.A.P. ROUTE 0525
SECTION 02-00518-00-BR
ROCKFORD, ILLINOIS
STATION 95+25.35
STRUCTURE NO. 101-6109

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JOB NO. 03R1751

DATE 12/14/06

12/30/06 12:35 PM
12/14/06 12:35 PM
12/14/06 12:35 PM
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LAYOUT	SLG	12/14/06
DRAWN	MEM/JKR	07/13/06
REVIEWED	FIN	09/02/06