

76C44

ST. CLAIR

I&R

# 115

7-30-10 LETTING ITEM 115

STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION  
DIVISION OF HIGHWAYS

F.A.P. RTE. 998	SECTION 82-2-1HVB	COUNTY ST. CLAIR	TOTAL SHEETS 2.85	SHEET NO. 1
FED. ROAD DIST. NO.	ILLINOIS	CONTRACT NO. 76C44		

D-98-059-08



LOCATION OF SECTION INDICATED THIS: -

# PROPOSED HIGHWAY PLANS

FAP ROUTE 998 (I-70) <sup>RELOCATED</sup>  
SECTION 82-2-1HVB  
PROJECT: PNR5-0998(001)  
ST. CLAIR COUNTY  
C-98-022-10

PROPOSED I-70 CURVED BRIDGE OVER NS, TRRA, MCT & INDUSTRIAL DRIVE AND PROPOSED MSE RETAINING WALL

FOR INDEX OF SHEETS, SEE SHEET NO. 2

LIST OF STRUCTURAL WORK

I-70 OVER NS, TRRA, MCT, AND INDUSTRIAL DRIVE  
STATION 134+22.00  
STRUCTURE NO. 082-0318 (EB) PROPOSED I-70 BRIDGE  
STRUCTURE NO. 082-0319 (WB) PROPOSED I-70 BRIDGE  
LENGTH 1,285'  
STRUCTURE NO. 082-W234 PROPOSED MSE WALL  
CONSTRUCTED IN THIS CONTRACT

INDUSTRIAL DRIVE  
ADT = 25 (2008)  
DESIGN SPEED = 25 MPH  
POSTED SPEED = 20 MPH

EXCHANGE AVENUE  
ADT = 16,940 (2030)  
DESIGN SPEED = 30 MPH  
POSTED SPEED = 25 MPH

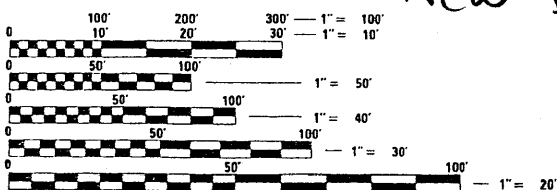
INTERSTATE 70  
DESIGN DESIGNATION - 6,594(30) INTERSTATE FREEWAY 48.96 (PCC-20)  
ADT = 59,940 (2030)  
DESIGN SPEED = 60 MPH  
POSTED SPEED = 55 MPH

IL ROUTE 3 (ST. CLAIR AVE.)  
ADT = 6,400 (2008), 7,900 (2030)  
DESIGN SPEED = 40 MPH (S. OF PACKERS AVE.)  
DESIGN SPEED = 45 MPH (N. OF PACKERS AVE.)  
POSTED SPEED = 35 MPH (S. OF PACKERS AVE.)  
POSTED SPEED = 45 MPH (N. OF PACKERS AVE.)

1ST STREET  
ADT = 1,350 (2008), 1,700 (2030)  
DESIGN SPEED = 35 MPH  
POSTED SPEED = 30 MPH

PROJECT LOCATED IN: FAIRMONT CITY, ILLINOIS

PLANS 1" = 50'  
PROFILES 1" = 5'  
X-SECTIONS 1" = 10' H  
1" = 5' V

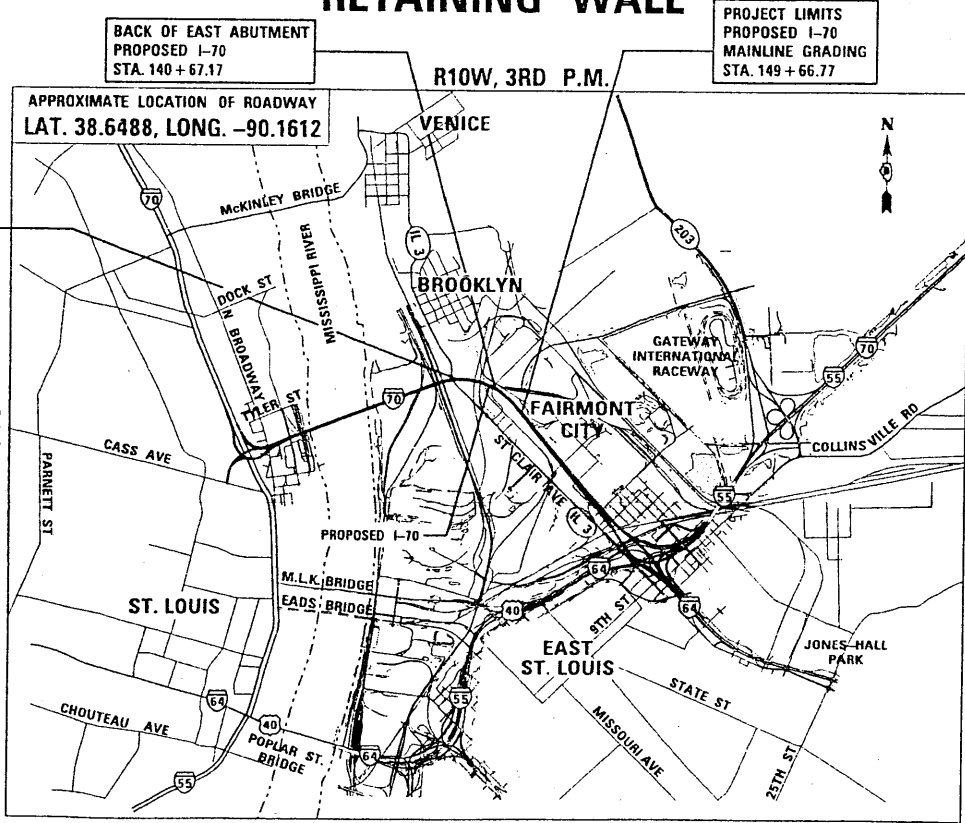


FULL SIZE PLANS HAVE BEEN PREPARED USING STANDARD ENGINEERING SCALES. REDUCED SIZED PLANS WILL NOT CONFORM TO STANDARD SCALES. IN MAKING MEASUREMENTS ON REDUCED PLANS, THE ABOVE SCALES MAY BE USED.

J.U.L.I.E.  
JOINT UTILITY LOCATION INFORMATION FOR EXCAVATION  
1-800-892-0123  
OR 811

100%  
10-10-2013

PROJECT LIMITS PROPOSED I-70 STA. 127+81.00 (SEE STRUCTURAL WORK DESCRIPTION IN UPPER LEFT CORNER)

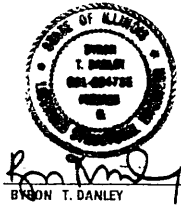


BACK OF EAST ABUTMENT PROPOSED I-70 STA. 140+67.17

PROJECT LIMITS PROPOSED I-70 MAINLINE GRADING STA. 149+66.77

APPROXIMATE LOCATION OF ROADWAY LAT. 38.6488, LONG. -90.1612

R10W, 3RD P.M.



EXPIRES: 11/30/2010

DATE: 3/11/10

FOR SHEETS: 76, 111-235



EXPIRES: 11/30/11

DATE: 3/10/10

FOR SHEETS: 1-77, 79-80

100-110, 236-285

STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION  
DIVISION OF HIGHWAYS

SUBMITTED: March 18 2010  
My [Signature]  
DEPUTY DIRECTOR OF HIGHWAYS, REGION ENGINEER

June 25 2010  
Scott E. Stitt, PE  
ENGINEER OF DESIGN AND ENVIRONMENT

June 25 2010  
Christine M. Reed  
DIRECTOR OF HIGHWAYS, CHIEF ENGINEER

PROJECT ENGINEER: MICHAEL D. PRITCHETT (618) 346-3180  
PROJECT MANAGER: JANE CHASTAIN MERCER (618) 346-3206

CONTRACT NO. 76C44 **082-0318(EB), 0319(WB)**



SCALE  
CANTEEN TOWNSHIP

GROSS LENGTH OF PROJECT: 0.244 MI (1,286.17')

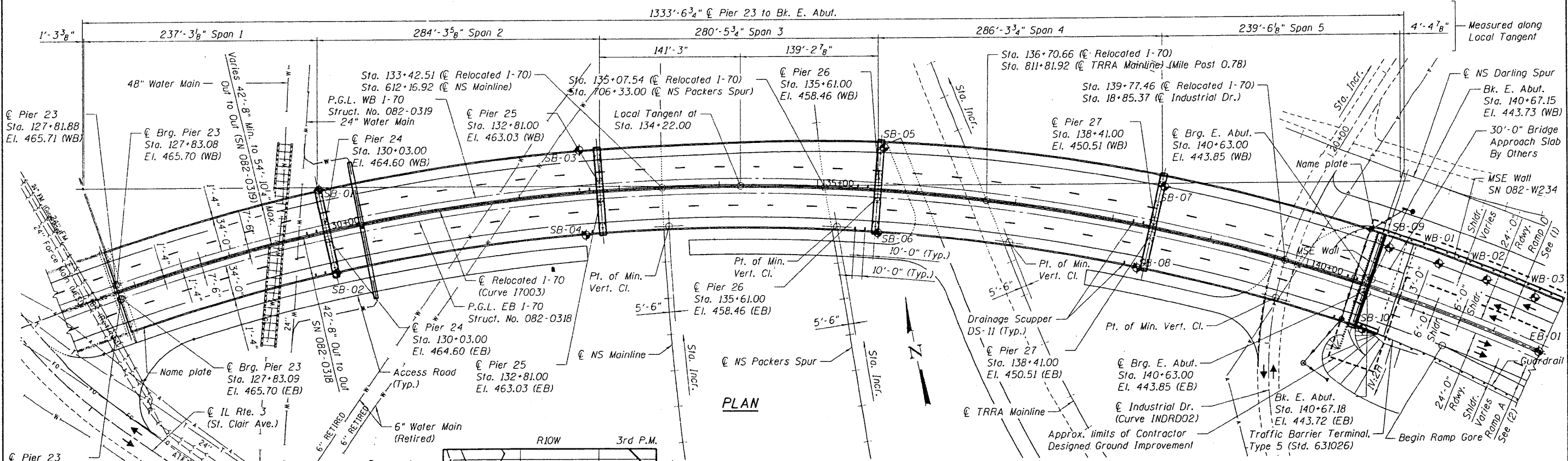
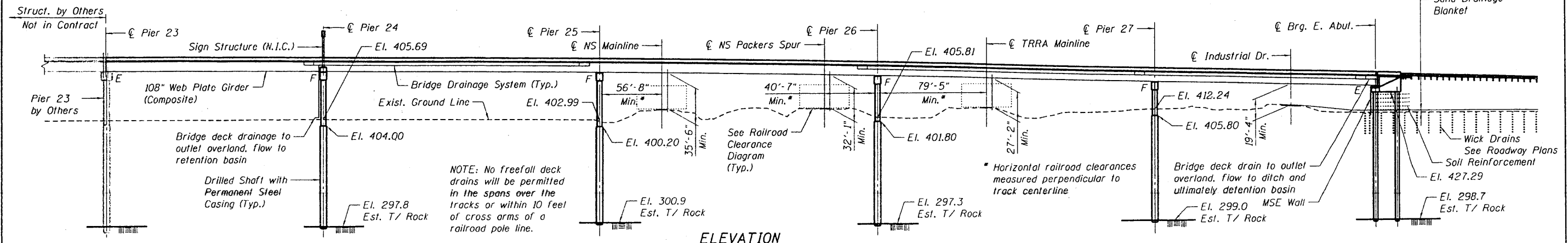
NET LENGTH OF PROJECT: 0.244 MI (1,286.17')

TENG

TENG & ASSOCIATES, INC.  
ENGINEERS/ARCHITECTS/PLANNERS  
205 N. MICHIGAN AVE. CHICAGO, IL 60601  
TELEPHONE: 312-616-0006

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BENCH MARK: Monument No. 11: Aluminum disk set in the back of a 4.5' concrete walk (end of walk), located on the west side of Illinois Route 3 approximately 0.3 miles south of Canal Street (Brooklyn). El. 414.02  
 EXISTING STRUCTURE: None



**DESIGN SPECIFICATIONS**  
 2007 AASHTO LRFD Bridge Design Specifications with 2008 & 2009 Interim Revisions

**DESIGN LOADING**  
 Vehicular Live Load: HL-93  
 Future Wearing Surface: 50 psf

**DESIGN STRESSES**  
 $f_c' = 3,500$  psi  
 $f_y = 60,000$  psi (reinforcement)  
 $f_y = 50,000$  psi (AASHTO M 270 Grade 50W)

**SEISMIC DATA**  
 (See Sheet S-3)

**LOCATION SKETCH**

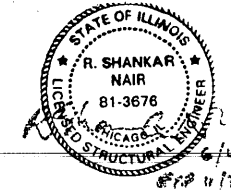
**RELOCATED I-70 CURVE I7003**  
 PI Sta. = 138+29.72  
 $\Delta = 74^\circ 40' 52''$  (RT)  
 $D = 2^\circ 56' 04''$   
 $R = 1,952.50'$   
 $T = 1,489.60'$   
 $L = 2,544.95'$   
 $E = 503.34'$   
 $SE = 5.40\%$   
 PC Sta. = 123+40.13  
 PT Sta. = 148+85.08

**INDUSTRIAL DR. CURVE INDRD02**  
 PI Sta. = 17+68.75  
 $\Delta = 87^\circ 47' 02''$  (RT)  
 $D = 15^\circ 03' 19''$   
 $R = 380.57'$   
 $T = 366.13'$   
 $L = 583.08'$   
 $E = 147.52'$   
 $SE = n/a$   
 PC Sta. = 14+02.62  
 PT Sta. = 19+85.70

(1) Ramp D (Auxiliary Lane) Drop Taper begins at Sta. 139+90.69, Offset 43.5' LT and ends at Sta. 133+42.43, Offset 31.5 LT.  
 (2) Ramp A Taper begins at Sta. 141+51.57, Offset 31.50' RT and ends at Sta. 144+42.57, Offset 43.5' RT.

**APPROVED**  
 FOR STRUCTURAL ADEQUACY ONLY

*Rajiv E. Anderson (TJD)*  
 ENGINEER OF BRIDGES AND STRUCTURES



FILE NAME =	USER NAME = #USER#	DESIGNED - KK	REVISED -	STATE OF ILLINOIS	GENERAL PLAN & ELEVATION	F.A.P. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
		DRAWN - KK	REVISED -	DEPARTMENT OF TRANSPORTATION	SCALE: SHEET NO. S-1 OF S-111	998	82-2-IHVB	ST. CLAIR	285	111
		CHECKED - TCU	REVISED -	1-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR.	STA. 134+22.00 TO STA.	SN 082-0318 (EB) & 0319 (WB) CONTRACT NO. 76C44				
		DATE - 06/04/10	REVISED -			FED. ROAD DIST. NO. ILLINOIS FED. AID PROJECT				

**GENERAL NOTES**

- Fasteners shall be AASHTO M164 Type 1, mechanically galvanized bolts in painted areas and M164 Type 3 in unpainted areas. Bolts  $\frac{7}{8}$  in.  $\phi$ , holes  $\frac{13}{16}$  in.  $\phi$ , unless otherwise noted.
- Calculated weight of Structural Steel = 7,894,000 lbs.
- All structural steel shall be AASHTO M 270 Grade 50W except expansion joints which shall be AASHTO M 270 Grade 50.
- No field welding is permitted except as specified in the contract documents.
- Reinforcement bars shall conform to the requirements of ASTM A 706 Gr 60. See Special Provisions.
- Reinforcement bars designated (E) shall be epoxy coated.
- If the Contractor elects to use cantilever forming brackets on the exterior beams or girders, the brackets shall be placed at the same locations as required for the hardwood blocks in Article 503.06(b) of the Standard Specifications. If additional cantilever forming brackets are required, hardwood blocking shall be wedged between the exterior and first interior beam at each of these additional bracket locations.
- Bearing seat surfaces shall be constructed or adjusted to their designated elevations within a tolerance of  $\frac{1}{8}$  in. (0.01 ft.). Adjustment shall be made either by grinding the surface or by shimming the bearings.
- Concrete Sealer shall be applied to the designated areas of the abutment.
- Structural steel shall only be painted for a distance of 10 ft. each way from the deck joints and piers. All structural steel shall be cleaned as specified in the Special Provision for "Surface Preparation and Painting Requirements for Weathering Steel".
- All exposed structural steel of the bearings shall be cleaned and shop painted as specified in the Special Provision for "Surface Preparation and Painting Requirements for Weathering Steel".
- Slipforming of the parapets is not allowed.
- The Contractor is alerted that camber and dead load deflection values shown on the girder detail drawings were developed based on the deck pouring sequence shown in the Contract Drawings. Any deviation from this pouring sequence will result in changes to camber and elevations that reflect dead load deflections. If the Contractor wishes to change the sequence, then the proposed plan revisions and design calculations shall be submitted to the Engineer for review and approval. The calculations shall be prepared and sealed by a Licensed Structural Engineer in Illinois.
- Abbreviations:  
 NS - Norfolk Southern  
 TRRA - Terminal Railroad Association  
 MCT - Metro County Transit

**BILL OF MATERIAL**

Item	Unit	Total
Structure Excavation	Cu Yd	462
Concrete Structures	Cu Yd	1,452.3
Concrete Superstructure	Cu Yd	4,076.2
Bridge Deck Grooving	Sq Yd	11,530
Protective Coat	Sq Yd	14,509
Furnishing And Erecting Structural Steel	L Sum	1
Furnishing and Erecting Structural Steel	Pound	1,150
Stud Shear Connectors	Each	31,625
Reinforcement Bars	Pound	680,740
Reinforcement Bars, Epoxy Coated	Pound	1,475,060
Bar Splicers	Each	97
Name Plates	Each	2
Permanent Casing	Foot	2,447
Drilled Shaft In Soil	Cu Yd	2,579
Drilled Shaft In Rock	Cu Yd	57
Anchor Bolts, 1"	Each	88
Anchor Bolts, 1 1/4"	Each	264
Concrete Sealer	Sq Ft	1,727
Drainage Scuppers, DS-11	Each	20
High Load Multi-Rotation Bearings, Fixed - 900 K	Each	33
High Load Multi-Rotation Bearings, Fixed - 1000 K	Each	11
High Load Multi-Rotation Bearings, Guided Expansion, 300 K	Each	22
Mechanical Splicers	Each	896
Drainage System	L Sum	1
Modular Expansion Joint-Swivel 9"	Foot	93.5
Modular Expansion Joint-Swivel 24"	Foot	80.0
Crosshole Sonic Logging	Each	5

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 06/04/10 10:30:07  
 TENG & ASSOCIATES, INC.  
 ENGINEERS/ARCHITECTS/PLANNERS  
 CHICAGO, ILLINOIS

FILE NAME :	USER NAME : #USER#	DESIGNED - KK	REVISED -	STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION I-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR.	GENERAL NOTES, BILL OF MATERIAL & INDEX OF SHEETS	F.A.P. RTE. 998	SECTION 82-2-JHVB	COUNTY ST. CLAIR	TOTAL SHEETS 285	SHEET NO. 112
PLOT SCALE : #SCALE#	CHECKED - TCU	REVISIONS -	DATE - 06/04/10			SCALE:	SHEET NO. S-2 OF S-111	STA. 134+22.00 TO STA.	SN 082-0318 (EB) & 0319 (WB) CONTRACT NO. 76C44 FED. ROAD DIST. NO. ILLINOIS FED. AID PROJECT	

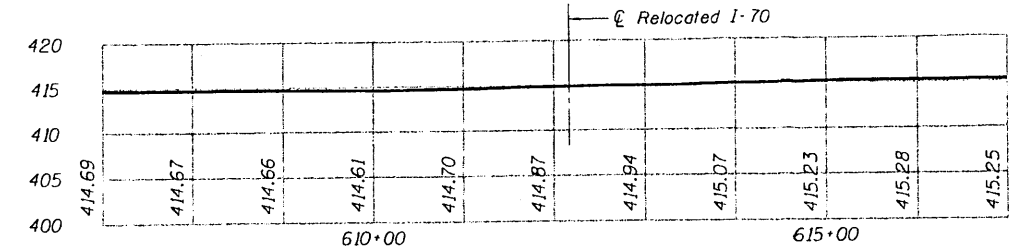
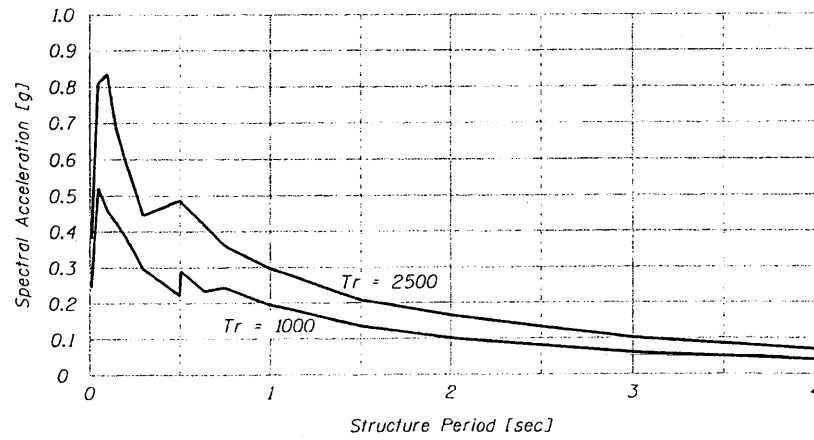
**SEISMIC DATA\***

Soil Site Class = D

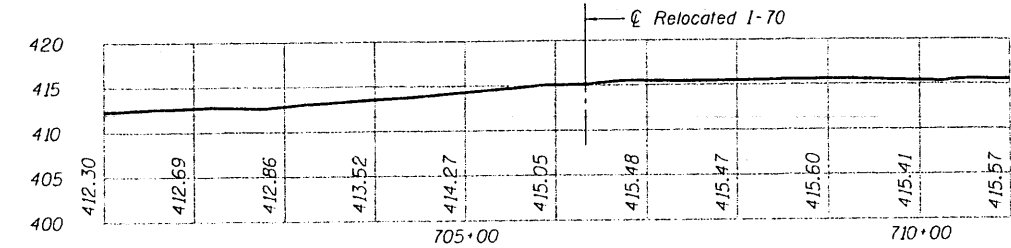
Return Period, $T_r$ [yrs]	1000	2500
Design Spectral Acceleration at 1.0 sec, $SD1$ [g]	0.20	0.30
Design Spectral Acceleration at 0.2 sec, $SDS$ [g]	0.39	0.60
Importance Category	Critical	Essential
Seismic Performance Zone	2	2

\* Seismic Data based on site-specific analysis.

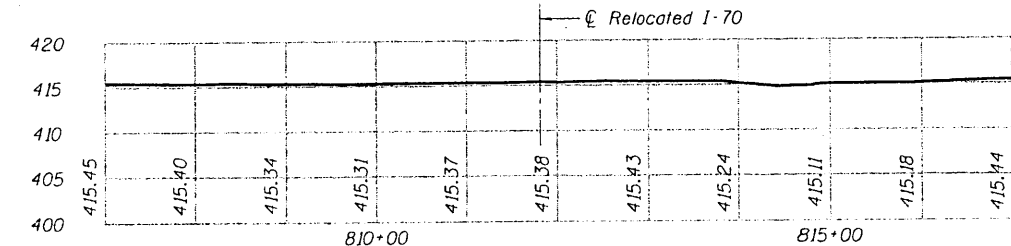
**SITE-SPECIFIC UNIFORM HAZARD SPECTRA**



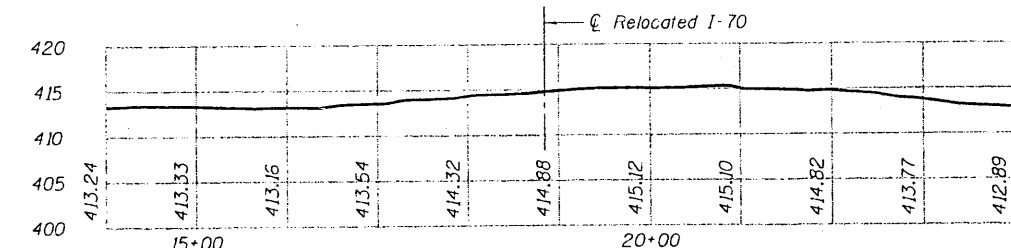
**NS MAINLINE PROFILE**



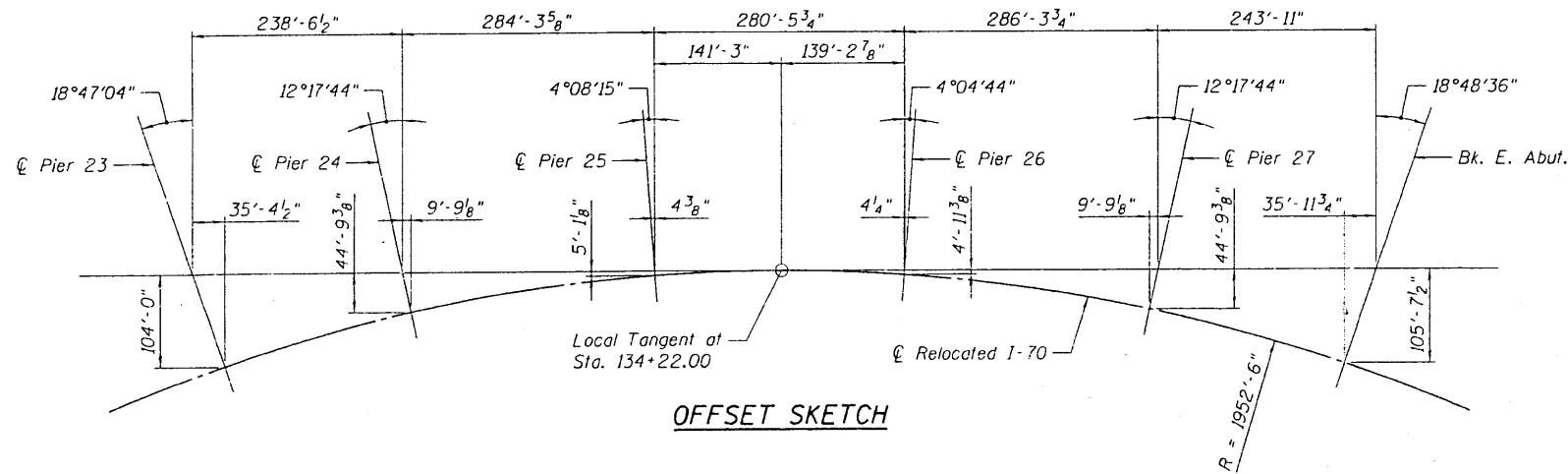
**NS PACKERS SPUR PROFILE**



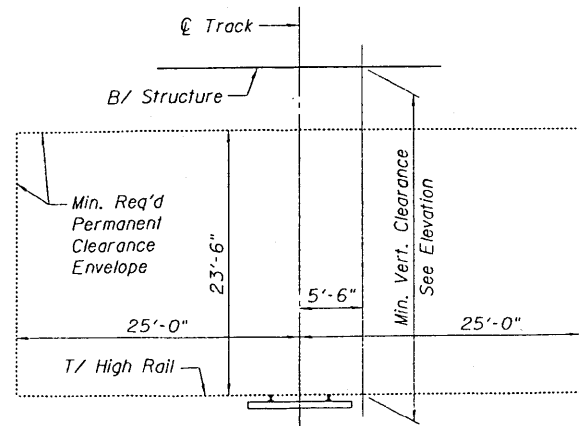
**TRRA MAINLINE PROFILE**



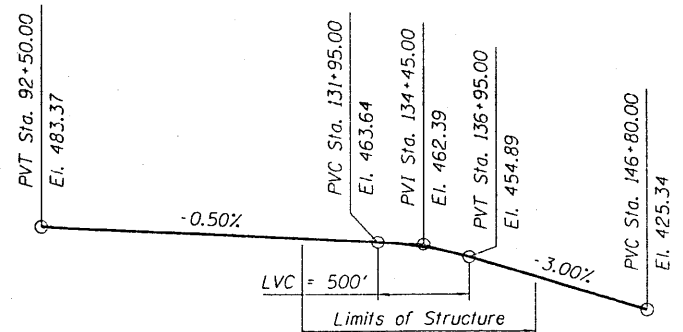
**INDUSTRIAL DR. PROFILE**



**OFFSET SKETCH**



**RAILROAD CLEARANCE DIAGRAM**



**PROFILE GRADE F.A.P. RTE 998 (RELOCATED I-70)**

STATION 134+22  
BUILT 2011 BY  
STATE OF ILLINOIS  
F.A.P. RT. 998 SEC. B2-2-IHVB  
LOADING HL - 93  
STRUCTURE NO. 082-0318

**NAME PLATE (EB)**  
See Std. 515001

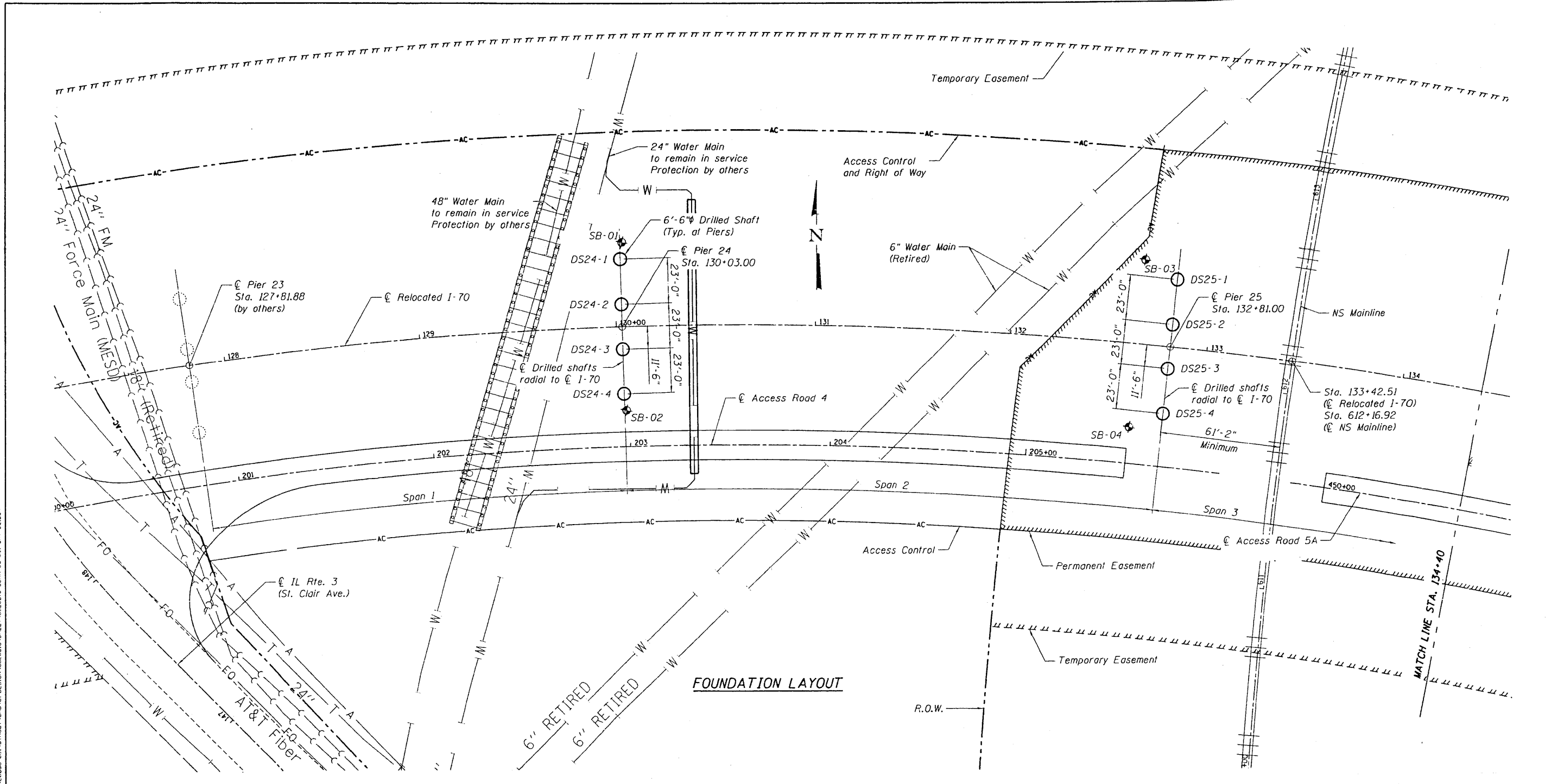
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BUILT 2011 BY  
STATE OF ILLINOIS  
F.A.P. RT. 998 SEC. B2-2-IHVB  
LOADING HL - 93  
STRUCTURE NO. 082-0319

**NAME PLATE (WB)**  
See Std. 515001

FILE NAME: \\FS10044\WORK\PROJECTS\10-PAVMS\872262\20868\081\STRUCT\1\JOB\01 DESIGN\0820318\01 SHEET\0820318-CONN-05-002-SHT-PLC.DGN  
 USER: BONDHILL  
 DESIGNED: KK  
 DRAWN: KK  
 CHECKED: TCU  
 DATE: 06/04/10  
 TENG & ASSOCIATES, INC.  
 ENGINEERS/ARCHITECTS/P.L.L.C.  
 CHICAGO, ILLINOIS

FILE NAME: \\FS10044\WORK\PROJECTS\10-PAVMS\872262\20868\081\STRUCT\1\JOB\01 DESIGN\0820318\01 SHEET\0820318-CONN-05-002-SHT-PLC.DGN	USER NAME: BONDHILL	DESIGNED: KK	REVISED:	STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION I-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR.	VERTICAL PROFILES & SEISMIC DATA		F.A.P. RTE: 998	SECTION: B2-2-IHVB	COUNTY: ST. CLAIR	TOTAL SHEETS: 285	SHEET NO.: 113
DESIGNED: KK	DRAWN: KK	CHECKED: TCU	DATE: 06/04/10		SCALE:	SHEET NO. S-3	OF S-111	STA. 134+22.00 TO STA.	CONTRACT NO. 76C44	FED. ROAD DIST. NO.	ILLINOIS FED. AID PROJECT
PLG1 SCALE: #SCALE#	PLG2 SCALE: #SCALE#	PLG3 SCALE: #SCALE#	PLG4 SCALE: #SCALE#								
PLG5 SCALE: #SCALE#	PLG6 SCALE: #SCALE#	PLG7 SCALE: #SCALE#	PLG8 SCALE: #SCALE#								

\P020218-CON-05-002-SL.DWG, \DRC\CON-05-ALIGNMENT2.DWG, \DRC\CON-05-RR-RM2.DWG, \DRC\CON-05-UTL.DWG, \AB220318-CON-05-RR-RI-BD.DWG  
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**FOUNDATION LAYOUT**

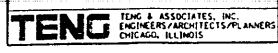
**LEGEND:**

Right of Way (R.O.W.)	-----
Access Control	-----AC-----
R.O.W. and Access Control	-----AC-----
Permanent Easement	
Temporary Easement	

- NOTES:**
1. Work this sheet with Sheet S-5.
  2. See Civil Plans for permanent access road details.

FILE NAME :	USER NAME : #USER#	DESIGNED - JLR	REVISED -	<b>STATE OF ILLINOIS</b> <b>DEPARTMENT OF TRANSPORTATION</b> I-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR.	<b>FOUNDATION LAYOUT</b> <b>1 OF 2</b>		F.A.P. RTE. 998	SECTION 62-2-1HVB	COUNTY ST. CLAIR	TOTAL SHEETS 285	SHEET NO. 114	
#FILE#	PLT SCALE = #SCALE#	DRAWN - JLR	REVISED -		SCALE:	SHEET NO. S-4 OF S-111	STA. 134+22.00 TO STA.	SN 082-0318 (EB) & 0319 (WB)	CONTRACT NO. 76C44			
TENG	PLT DATE = #DATE#	CHECKED - TCU	REVISED -		DATE - 06/04/10	REVISED -	FED. ROAD DIST. NO. [ILLINOIS] FED. AID PROJECT					
<b>TENG</b> TENG & ASSOCIATES, INC. ENGINEERS, ARCHITECTS & PLANNERS CHICAGO, ILLINOIS												

FILE NAME : USER NAME : #USER# DESIGNED - JLR REVISIONS -  
 DRAWN - JLR REVISIONS -  
 CHECKED - TCU REVISIONS -  
 DATE - 06/04/10 REVISIONS -  
 PLOT SCALE : #SCALE#  
 PLOT DATE : #DATE#



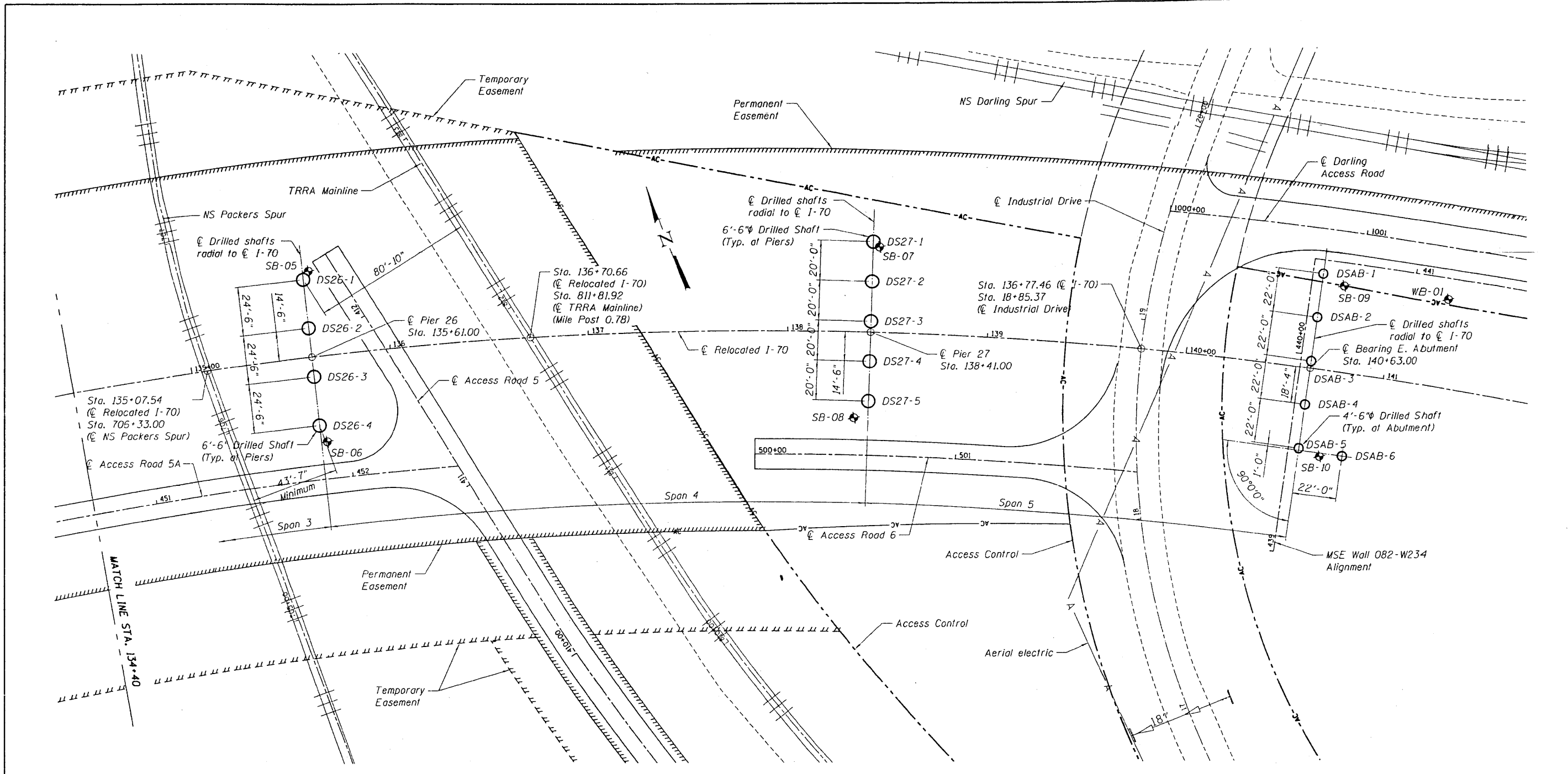
FILE NAME :	USER NAME : #USER#	DESIGNED - JLR	REVISIONS -
SCALE :		DRAWN - JLR	REVISIONS -
		CHECKED - TCU	REVISIONS -
		DATE - 06/04/10	REVISIONS -

**STATE OF ILLINOIS**  
**DEPARTMENT OF TRANSPORTATION**  
 I-70 CONNECTION OVER  
 NS, TRRA, MCT AND INDUSTRIAL DR.

**FOUNDATION LAYOUT**  
**2 OF 2**

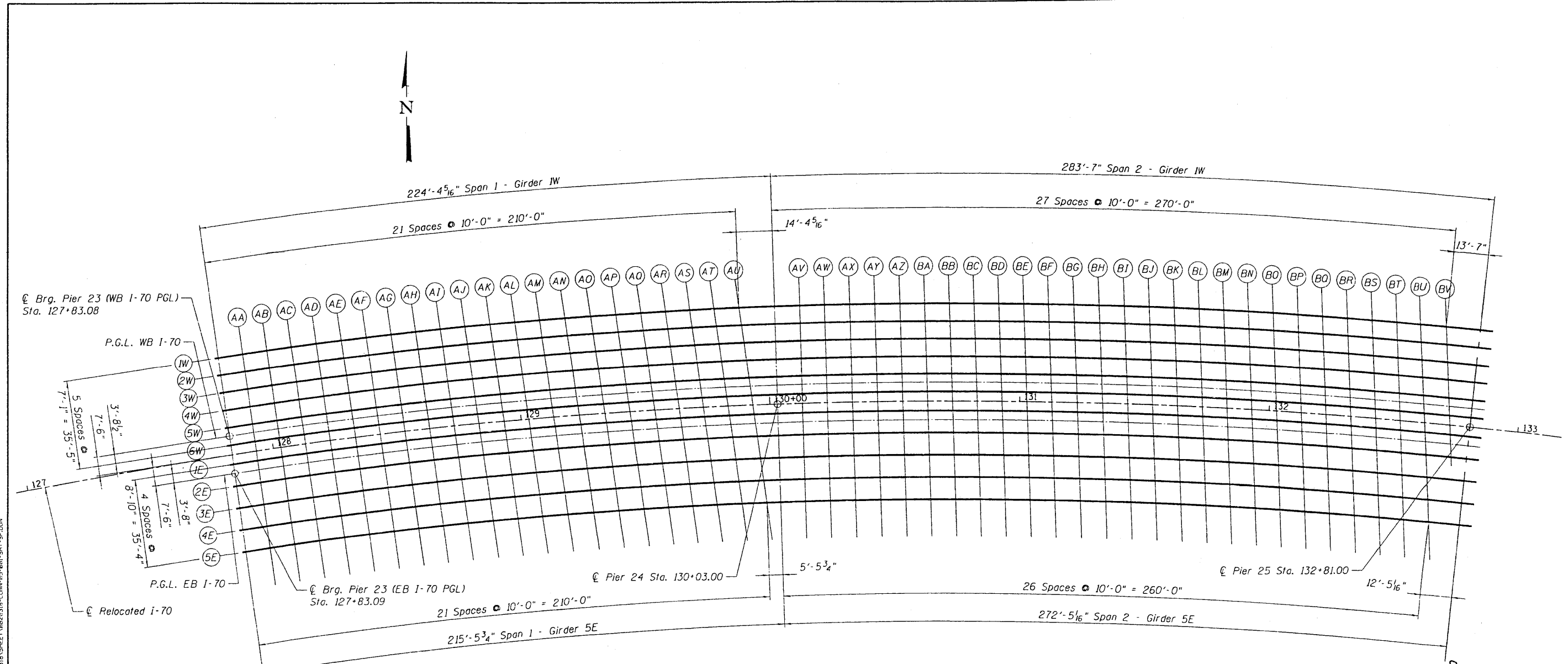
SCALE: SHEET NO. S-5 OF S-111 STA. 134+22.00 TO STA.

F.A.P. RTE. 998	SECTION 82-2-IHVB	COUNTY ST. CLAIR	TOTAL SHEETS 285	SHEET NO. 115
SM 082-0318 (EB) & 0319 (WB)		CONTRACT NO. 76C44		
FED. ROAD DIST. NO. [ILLINOIS] FED. AID PROJECT				

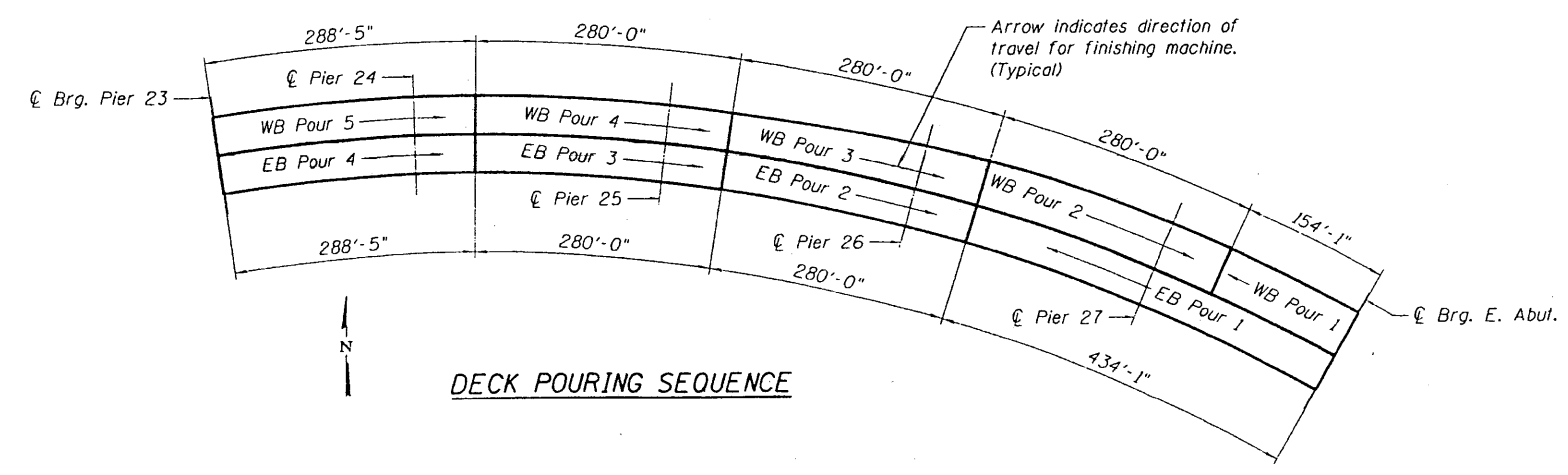


**FOUNDATION LAYOUT**

**NOTE:**  
 Work this sheet with Sheet S-4.



PLAN - SPANS 1 & 2



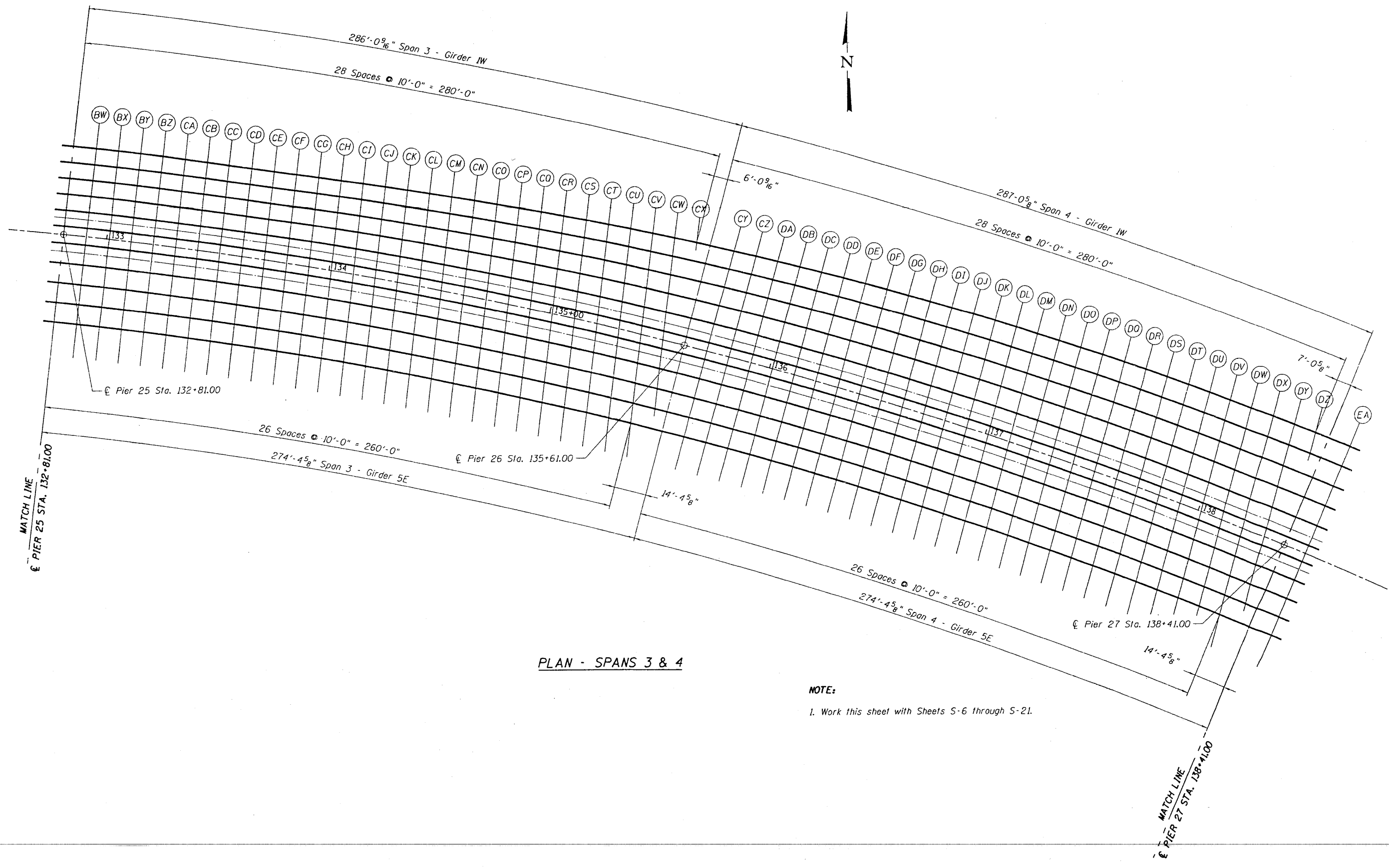
NOTES:

1. Work this sheet with Sheets S-7 through S-21.
2. The Contractor is alerted that camber and dead load deflection values shown on the plans were developed based on the deck pouring sequence shown on this sheet. Any deviation from this pouring sequence will result in changes to camber and elevations that reflect dead load deflections. If the Contractor wishes to change the sequence, then the proposed plan revisions and design calculations shall be submitted to the Engineer for review and approval. The calculations shall be prepared and sealed by a Licensed Structural Engineer in Illinois.
3. When the deck pour is stopped for the day at one or more of the transverse bonded construction joints in the deck pouring sequence as shown, the next pour shall not be made until both of the following are met:
  1. At least 72 hours shall have elapsed from the end of the previous pour.
  2. The concrete strength shall have attained a minimum flexural strength of 650 psi or a minimum compressive strength of 3500 psi.

FILE NAME: \\B20318-CON-05-SP.DGN USER: JLR DATE: 06/04/10  
 DRAWN: JLR CHECKED: TCU  
 DESIGNED: JLR REVISIONS: 1  
 PLOT SCALE: 1/8"=1'-0" PLOT DATE: 06/04/10  
 TENG & ASSOCIATES, INC. ENGINEERS/ARCHITECTS/PLANNERS CHICAGO, ILLINOIS

STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION I-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR.	TOP OF SLAB ELEVATION PLAN 1 OF 3	F.A.P. RTE. 998	SECTION 82-2-1HVB	COUNTY ST. CLAIR	TOTAL SHEETS 285	SHEET NO. 5-6 OF S-111	STA. 134+22.00 TO STA.	CONTRACT NO. 76L44
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\\S:\PROJECTS\02\CONNECTIONS\02-1-70\02-1-70.DWG  
\\S:\PROJECTS\02\CONNECTIONS\02-1-70\02-1-70.DWG  
\\S:\PROJECTS\02\CONNECTIONS\02-1-70\02-1-70.DWG  
\\S:\PROJECTS\02\CONNECTIONS\02-1-70\02-1-70.DWG  
\\S:\PROJECTS\02\CONNECTIONS\02-1-70\02-1-70.DWG



PLAN - SPANS 3 & 4

NOTE:  
1. Work this sheet with Sheets S-6 through S-21.

FILE NAME :	USER NAME :	DESIGNED - JLR	REVISED -	STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION 1-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR.	TOP OF SLAB ELEVATION PLAN 2 OF 3	SCALE:	SHEET NO. S-7 OF S-111	STA. 134+22.00 TO STA.	F.A.P. RTE.	SECTION	COUNTY	TOTAL SHEET SHEETS: NO.
REVISED -	DRAWN - JLR	REVISED -	998						B2-2-1HVB	ST. CLAIR	285	117
PLOT SCALE :	SCALE:	CHECKED - TCU	REVISED -	SN 082-0318 (EB) & 0319 (WB) CONTRACT NO. 76C44				FED. ROAD DIST. NO.		ILLINOIS FED. AID PROJECT		
DATE :	DATE:	DATE - 06/04/10	REVISED -									









EB I-70 P.G.L. - SPANS 1 & 2

Table with 5 columns: Location, Station, Offset From EB I-70 P.G.L., Theoretical Grade Elevations, Theoretical Grade Elevations Adjusted for DL Deflections. Rows include locations from AA to BV.

EB I-70 P.G.L. - SPANS 3 & 4

Table with 5 columns: Location, Station, Offset From EB I-70 P.G.L., Theoretical Grade Elevations, Theoretical Grade Elevations Adjusted for DL Deflections. Rows include locations from Pier 25 to Pier 26 and locations CZ to DZ.

EB I-70 P.G.L. - SPAN 5

Table with 5 columns: Location, Station, Offset From EB I-70 P.G.L., Theoretical Grade Elevations, Theoretical Grade Elevations Adjusted for DL Deflections. Rows include locations from Pier 27 to Brg Abut.

NOTE:

1. Work this sheet with Sheets S-6 through S-21.

Vertical text on the left margin: X:\082\0318\CONV\05-701-SF.DWG... FILE NAME: ...

Project information and title block including TENG logo, project name (I-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR.), scale, and sheet details (2 OF 13).

GIRDER 2E - SPANS 1 & 2

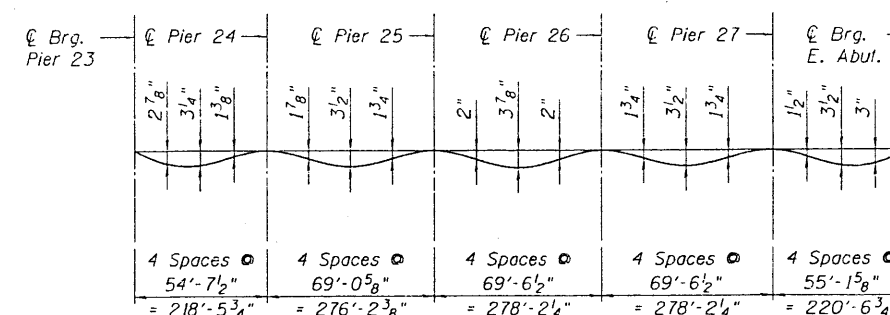
Table with 5 columns: Location, Station, Offset From EB 1-70 P.G.L., Theoretical Grade Elevations, Theoretical Grade Elevations Adjusted for DL Deflections. Rows include locations AA through BV and Pier 24.

GIRDER 2E - SPANS 3 & 4

Table with 5 columns: Location, Station, Offset From EB 1-70 P.G.L., Theoretical Grade Elevations, Theoretical Grade Elevations Adjusted for DL Deflections. Rows include locations from Pier 25 to Pier 26 and locations CZ through DZ.

GIRDER 2E - SPAN 5

Table with 5 columns: Location, Station, Offset From EB 1-70 P.G.L., Theoretical Grade Elevations, Theoretical Grade Elevations Adjusted for DL Deflections. Rows include locations EA through EV and Brg Abut.



DEAD LOAD DEFLECTION DIAGRAM - GIRDER 2E

(Includes weight of concrete only.)

NOTES:

- 1. Work this sheet with Sheets S-6 through S-21.
2. The above deflections are not to be used in the field if the engineer is working from the grade elevations adjusted for dead load deflections as shown on this sheet.





GIRDER 5E - SPANS 1 & 2

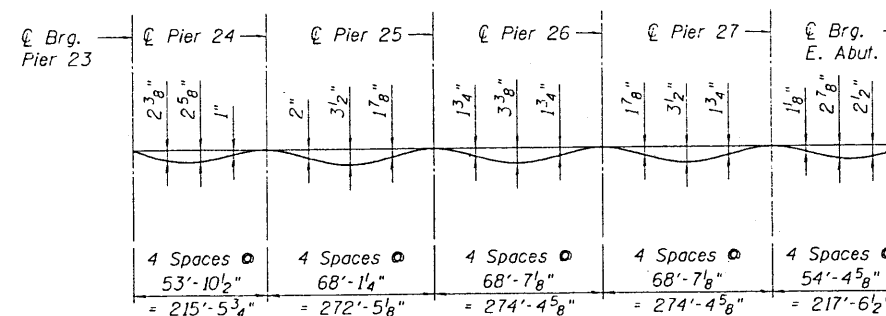
Table with 5 columns: Location, Station, Offset From EB 1-70 P.G.L., Theoretical Grade Elevations, Theoretical Grade Elevations Adjusted for DL Deflections. Rows include locations AA through BV.

GIRDER 5E - SPANS 3 & 4

Table with 5 columns: Location, Station, Offset From EB 1-70 P.G.L., Theoretical Grade Elevations, Theoretical Grade Elevations Adjusted for DL Deflections. Rows include locations CY through DZ.

GIRDER 5E - SPAN 5

Table with 5 columns: Location, Station, Offset From EB 1-70 P.G.L., Theoretical Grade Elevations, Theoretical Grade Elevations Adjusted for DL Deflections. Rows include locations EA through EV.



DEAD LOAD DEFLECTION DIAGRAM - GIRDER 5E (Includes weight of concrete only.)

NOTES:

- 1. Work this sheet with Sheets S-6 through S-21.
2. The above deflections are not to be used in the field if the engineer is working from the grade elevations adjusted for dead load deflections as shown on this sheet.

FILE NAME = ... USER NAME = ... DESIGNED - JLR REVISED - ... DRAWN - JLR REVISED - ... CHECKED - TCU REVISED - ... DATE - 06/20/10 REVISED - ...

Project information including TENG logo, State of Illinois Department of Transportation, 1-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR., and sheet details like TOP OF SLAB ELEVATIONS 6 OF 13.











GIRDER 5W - SPANS 1 & 2

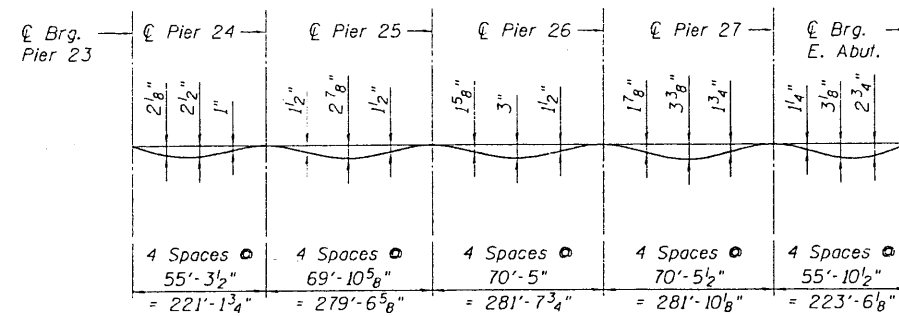
Table with 5 columns: Location, Station, Offset From WB 1-70 P.G.L., Theoretical Grade Elevations, and Theoretical Grade Elevations Adjusted for DL Deflections. Rows include Brg P23 (AA-AV) and Pier 24 (AW-BV).

GIRDER 5W - SPANS 3 & 4

Table with 5 columns: Location, Station, Offset From WB 1-70 P.G.L., Theoretical Grade Elevations, and Theoretical Grade Elevations Adjusted for DL Deflections. Rows include Pier 25 (BW-DZ) and Pier 26 (CY-DZ).

GIRDER 5W - SPAN 5

Table with 5 columns: Location, Station, Offset From WB 1-70 P.G.L., Theoretical Grade Elevations, and Theoretical Grade Elevations Adjusted for DL Deflections. Rows include Pier 27 (EA-EV) and Brg Abut.



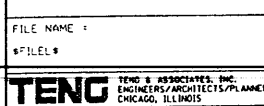
DEAD LOAD DEFLECTION DIAGRAM - GIRDER 5W

(Includes weight of concrete only.)

NOTES:

- 1. Work this sheet with Sheets S-6 through S-21.
2. The above deflections are not to be used in the field if the engineer is working from the grade elevations adjusted for dead load deflections as shown on this sheet.

FILE NAME: ... USER NAME: ... DESIGNED: ... DRAWN: ... CHECKED: ... DATE: ...



STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION I-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR.

TOP OF SLAB ELEVATIONS 11 OF 13

Scale and stationing table: SCALE: SHEET NO. S-19 OF S-111 STA. 134+22.00 TO STA.

F.A.P. RTE. SECTION COUNTY TOTAL SHEETS SHEET NO. 998 62-2-1HVB ST. CLAIR 285 129

WB I-70 P.G.L. - SPANS 1 & 2

Location	Station	Offset From WB I-70 P.G.L.	Theoretical Grade Elevations	Theoretical Grade Elevations Adjusted for DL Deflections
€ Brg P23	127+83.08	0.00	465.70	465.70
AA	127+93.04	0.00	465.65	465.69
AB	128+03.00	0.00	465.60	465.68
AC	128+12.96	0.00	465.55	465.66
AD	128+22.92	0.00	465.50	465.64
AE	128+32.89	0.00	465.45	465.61
AF	128+42.85	0.00	465.40	465.59
AG	128+52.81	0.00	465.35	465.55
AH	128+62.77	0.00	465.30	465.51
AI	128+72.73	0.00	465.25	465.46
AJ	128+82.70	0.00	465.20	465.41
AK	128+92.66	0.00	465.15	465.35
AL	129+02.62	0.00	465.10	465.29
AM	129+12.58	0.00	465.05	465.22
AN	129+22.54	0.00	465.00	465.15
AO	129+32.50	0.00	464.95	465.08
AP	129+42.47	0.00	464.90	465.00
AQ	129+52.43	0.00	464.85	464.93
AR	129+62.39	0.00	464.80	464.86
AS	129+72.35	0.00	464.75	464.79
AT	129+82.31	0.00	464.70	464.72
AU	129+92.27	0.00	464.65	464.66
€ Pier 24	130+03.00	0.00	464.60	464.60
AV	130+12.96	0.00	464.55	464.56
AW	130+22.92	0.00	464.50	464.52
AX	130+32.89	0.00	464.45	464.48
AY	130+42.85	0.00	464.40	464.46
AZ	130+52.81	0.00	464.35	464.43
BA	130+62.77	0.00	464.30	464.40
BB	130+72.73	0.00	464.25	464.38
BC	130+82.69	0.00	464.20	464.36
BD	130+92.66	0.00	464.15	464.33
BE	131+02.62	0.00	464.10	464.30
BF	131+12.58	0.00	464.05	464.27
BG	131+22.54	0.00	464.00	464.23
BH	131+32.50	0.00	463.95	464.19
BI	131+42.46	0.00	463.90	464.14
BJ	131+52.43	0.00	463.85	464.09
BK	131+62.39	0.00	463.80	464.03
BL	131+72.35	0.00	463.75	463.97
BM	131+82.31	0.00	463.70	463.90
BN	131+92.27	0.00	463.65	463.83
BO	132+02.23	0.00	463.60	463.75
BP	132+12.20	0.00	463.55	463.67
BQ	132+22.16	0.00	463.49	463.59
BR	132+32.12	0.00	463.42	463.49
BS	132+42.08	0.00	463.35	463.40
BT	132+52.04	0.00	463.27	463.30
BU	132+62.01	0.00	463.19	463.21
BV	132+71.97	0.00	463.11	463.12

WB I-70 P.G.L. - SPANS 3 & 4

Location	Station	Offset From WB I-70 P.G.L.	Theoretical Grade Elevations	Theoretical Grade Elevations Adjusted for DL Deflections
€ Pier 25	132+81.00	0.00	463.03	463.03
BW	132+90.96	0.00	462.93	462.94
BX	133+00.92	0.00	462.83	462.85
BY	133+10.89	0.00	462.73	462.76
BZ	133+20.85	0.00	462.61	462.67
CA	133+30.81	0.00	462.50	462.58
CB	133+40.77	0.00	462.38	462.49
CC	133+50.73	0.00	462.26	462.39
CD	133+60.69	0.00	462.13	462.29
CE	133+70.66	0.00	461.99	462.18
CF	133+80.62	0.00	461.85	462.06
CG	133+90.58	0.00	461.71	461.93
CH	134+00.54	0.00	461.56	461.79
CI	134+10.50	0.00	461.40	461.65
CJ	134+20.46	0.00	461.24	461.49
CK	134+30.43	0.00	461.08	461.32
CL	134+40.39	0.00	460.91	461.14
CM	134+50.35	0.00	460.73	460.96
CN	134+60.31	0.00	460.55	460.76
CO	134+70.27	0.00	460.37	460.55
CP	134+80.23	0.00	460.18	460.34
CO	134+90.20	0.00	459.99	460.12
CR	135+00.16	0.00	459.79	459.89
CS	135+10.12	0.00	459.58	459.66
CT	135+20.08	0.00	459.37	459.43
CU	135+30.04	0.00	459.16	459.19
CV	135+40.01	0.00	458.94	458.96
CW	135+49.97	0.00	458.72	458.72
CX				
€ Pier 26	135+61.00	0.00	458.46	458.46
CY	135+70.96	0.00	458.23	458.24
CZ	135+80.92	0.00	457.99	458.01
DA	135+90.89	0.00	457.74	457.78
DB	136+00.85	0.00	457.49	457.56
DC	136+10.81	0.00	457.24	457.33
DD	136+20.77	0.00	456.98	457.10
DE	136+30.73	0.00	456.71	456.87
DF	136+40.69	0.00	456.45	456.63
DG	136+50.66	0.00	456.17	456.38
DH	136+60.62	0.00	455.89	456.12
DI	136+70.58	0.00	455.61	455.86
DJ	136+80.54	0.00	455.32	455.58
DK	136+90.50	0.00	455.02	455.30
DL	137+00.46	0.00	454.73	455.01
DM	137+10.43	0.00	454.43	454.70
DN	137+20.39	0.00	454.13	454.39
DO	137+30.35	0.00	453.83	454.08
DP	137+40.31	0.00	453.53	453.75
DQ	137+50.27	0.00	453.23	453.43
DR	137+60.23	0.00	452.93	453.11
DS	137+70.20	0.00	452.63	452.78
DT	137+80.16	0.00	452.34	452.45
DU	137+90.12	0.00	452.04	452.12
DV	138+00.08	0.00	451.74	451.80
DW	138+10.04	0.00	451.44	451.47
DX	138+20.01	0.00	451.14	451.16
DY	138+29.97	0.00	450.84	450.85
DZ				

WB I-70 P.G.L. - SPAN 5

Location	Station	Offset From WB I-70 P.G.L.	Theoretical Grade Elevations	Theoretical Grade Elevations Adjusted for DL Deflections
€ Pier 27	138+41.00	0.00	450.51	450.51
EA	138+50.96	0.00	450.21	450.22
EB	138+60.92	0.00	449.91	449.93
EC	138+70.89	0.00	449.61	449.65
ED	138+80.85	0.00	449.31	449.38
EE	138+90.81	0.00	449.02	449.10
EF	139+00.77	0.00	448.72	448.84
EG	139+10.73	0.00	448.42	448.57
EH	139+20.69	0.00	448.12	448.30
EI	139+30.66	0.00	447.82	448.03
EJ	139+40.62	0.00	447.52	447.75
EK	139+50.58	0.00	447.22	447.47
EL	139+60.54	0.00	446.92	447.18
EM	139+70.50	0.00	446.62	446.89
EN	139+80.46	0.00	446.33	446.59
EO	139+90.43	0.00	446.03	446.28
EP	140+00.39	0.00	445.73	445.97
EQ	140+10.35	0.00	445.43	445.64
ER	140+20.31	0.00	445.13	445.32
ES	140+30.27	0.00	444.83	444.98
ET	140+40.23	0.00	444.53	444.64
EU	140+50.20	0.00	444.23	444.29
EV				
€ Brg Abut	140+63.00	0.00	443.85	443.85

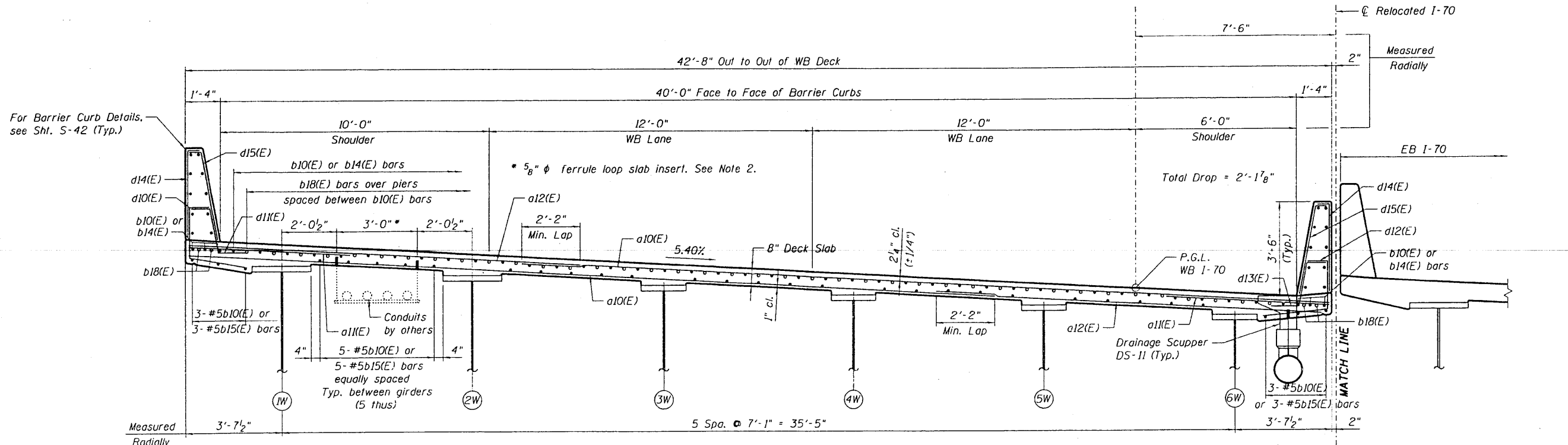
NOTE:

1. Work this sheet with Sheets S-6 through S-21.

\\VBR210\B-COMM-05-881-SP.DWG...WB I-70 P.G.L. - SPAN 5 SHEET 06 OF 08

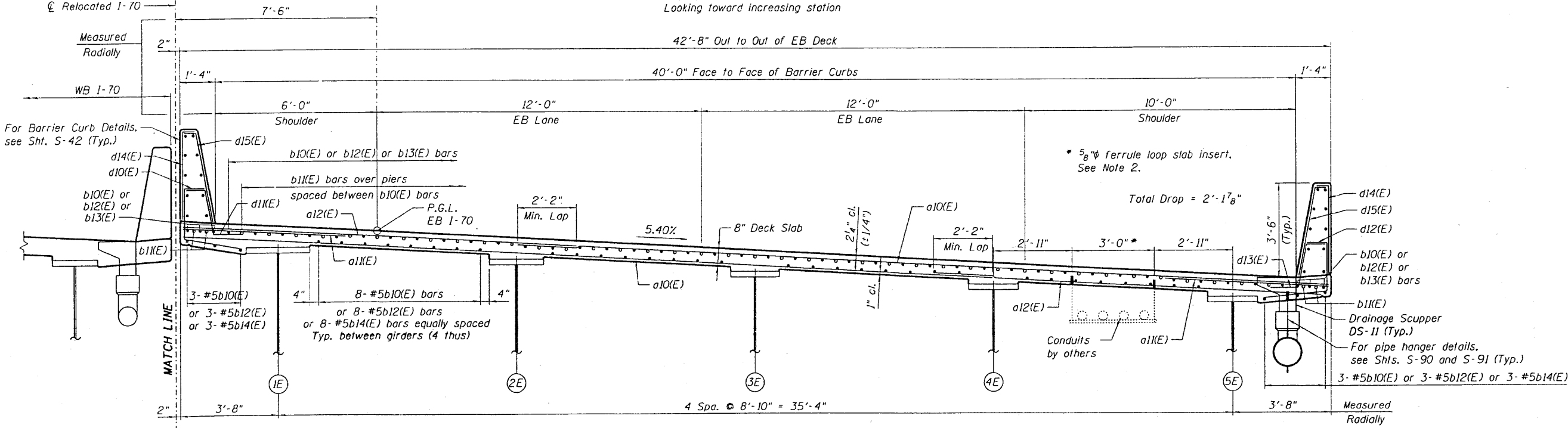
FILE NAME: #FILE#	USER NAME: #USER#	DESIGNED - JLR DRAWN - JLR	REVISED - REVISED -	STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION I-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR.	TOP OF SLAB ELEVATIONS 12 OF 13	F.A.P. RTE. 998 SECTION 82-2-1HVB COUNTY ST. CLAIR TOTAL SHEETS 285 SHEET NO. 130
<b>TENG</b>	TENG & ASSOCIATES, INC. ENGINEERS/ARCHITECTS/SURVEYORS CHICAGO, ILLINOIS	CHECKED - TCU DATE - 06/04/10	REVISED - REVISED -	SCALE:	SHEET NO. S-20 OF S-111   STA. 134+22.00 TO STA.	SN 002 0310 (ED) & 0310 (WD)   CONTRACT NO. 76C44 FED. ROAD DIST. NO.   ILLINOIS FED. AID PROJECT





**SECTION A-A - WESTBOUND I-70**

Sta. 127+81.58 to Sta. 133+42.00  
(Pour 5 & Pour 4 Sections)  
Looking toward increasing station



**SECTION A-A - EASTBOUND I-70**

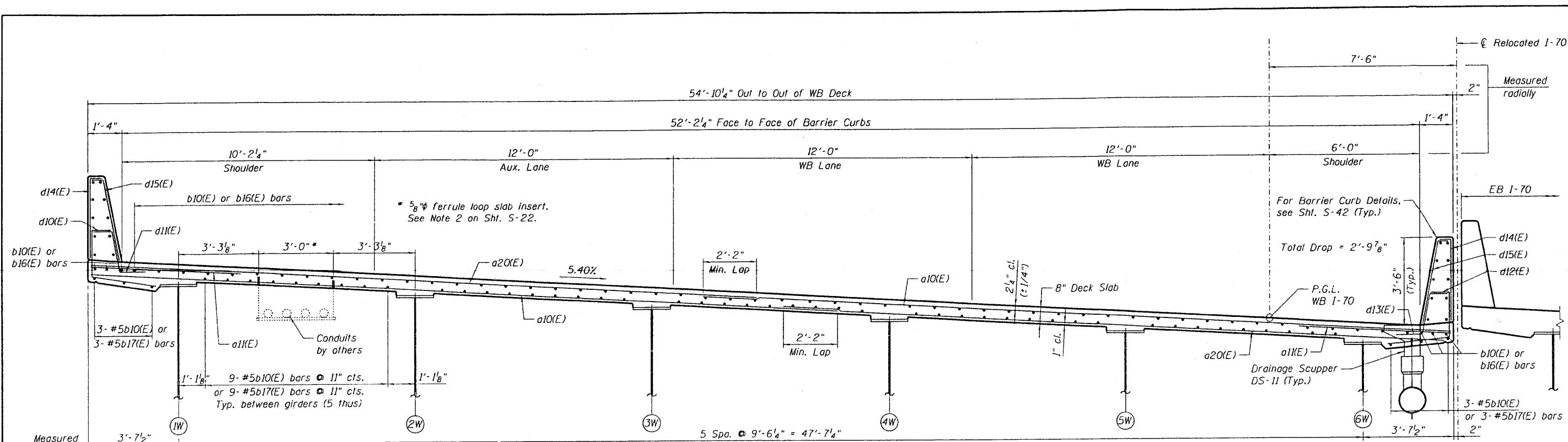
Sta. 127+81.58 to Sta. 140+64.57  
Looking toward increasing station

- NOTES:**
1. Work this sheet with Shts. S-23 thru S-47.
  2. Inserts installed in this contract, conduit and hangers installed in future contract. Space inserts at 5'-0" cts. longitudinally, full length of bridges. The cost of inserts is included in the cost of Reinforcement Bars, Epoxy Coated. Safe working load = 2,200 lbs.
  3. For scupper spacing, see Shts. S-24 thru S-33.

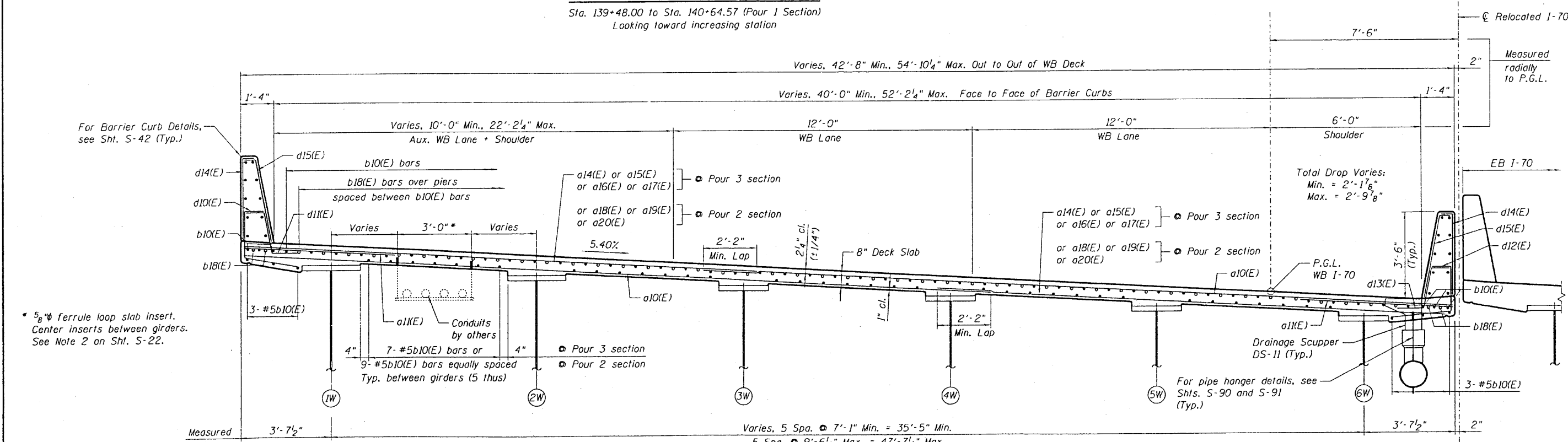
08/22/18 CONN-99-001-001... 08/22/18 CONN-99-001-001... 08/22/18 CONN-99-001-001...  
 08/22/18 CONN-99-001-001... 08/22/18 CONN-99-001-001... 08/22/18 CONN-99-001-001...

FILE NAME :	USCR NAME : *USER*	DESIGNED - JLR	REVISED -	<b>STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION</b>	<b>DECK CROSS SECTIONS 1 OF 2</b>	F.A.P. RFE:	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.	
#FILE#		DRAWN - FD	REVISED -			998	82-2-1HVB	ST. CLAIR	285	132	
		CHECKED - TCU	REVISED -			SN 002-0310 (EB) & 0319 (WB) CONTRACT NO. 76644					
		DATE - 06/04/10	REVISED -			FED. ROAD DIST. NO. ILLINOIS FED. AID PROJECT					
<b>TENG</b> & ASSOCIATES, INC. ENGINEERS/ARCHITECTS/PLANNERS CHICAGO, ILLINOIS				NS, TRRA, MCT AND INDUSTRIAL DR.		SCALE: SHEET NO. S-22 OF S-111 STA. 134+22.00 TO STA.					

FILE NAME = USER NAME = DESIGNED - JLR REVISIONS - DRAWN - FD CHECKED - TCU DATE - 06/04/10  
 06/04/10 10:41:15



**SECTION C-C - WESTBOUND I-70**  
 Sta. 139+48.00 to Sta. 140+64.57 (Pour 1 Section)  
 Looking toward increasing station

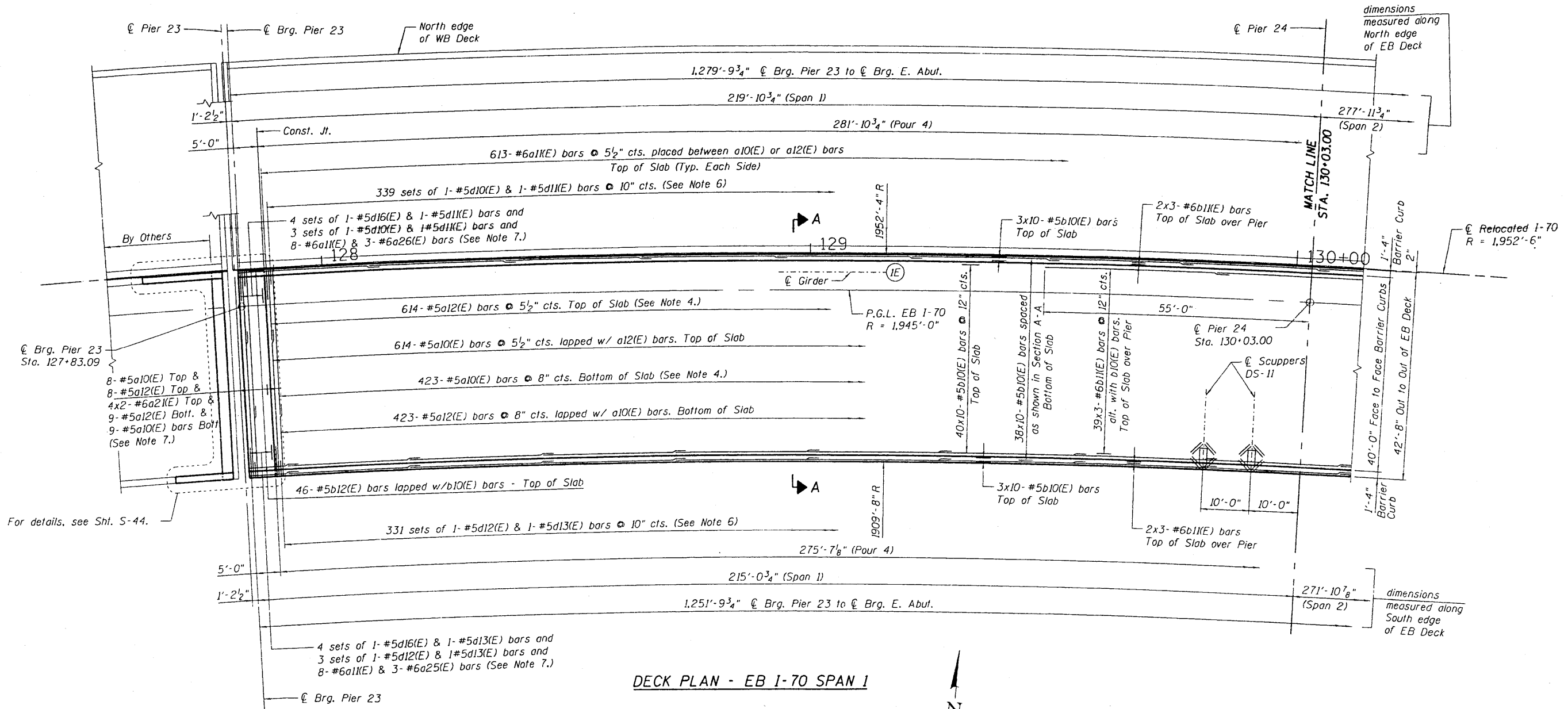


**SECTION B-B - WESTBOUND I-70**  
 Sta. 133+42.00 to Sta. 139+48.00 (Pour 3 & Pour 2 Sections)  
 Looking toward increasing station

**NOTE:**  
 See Sht. S-22 for notes.

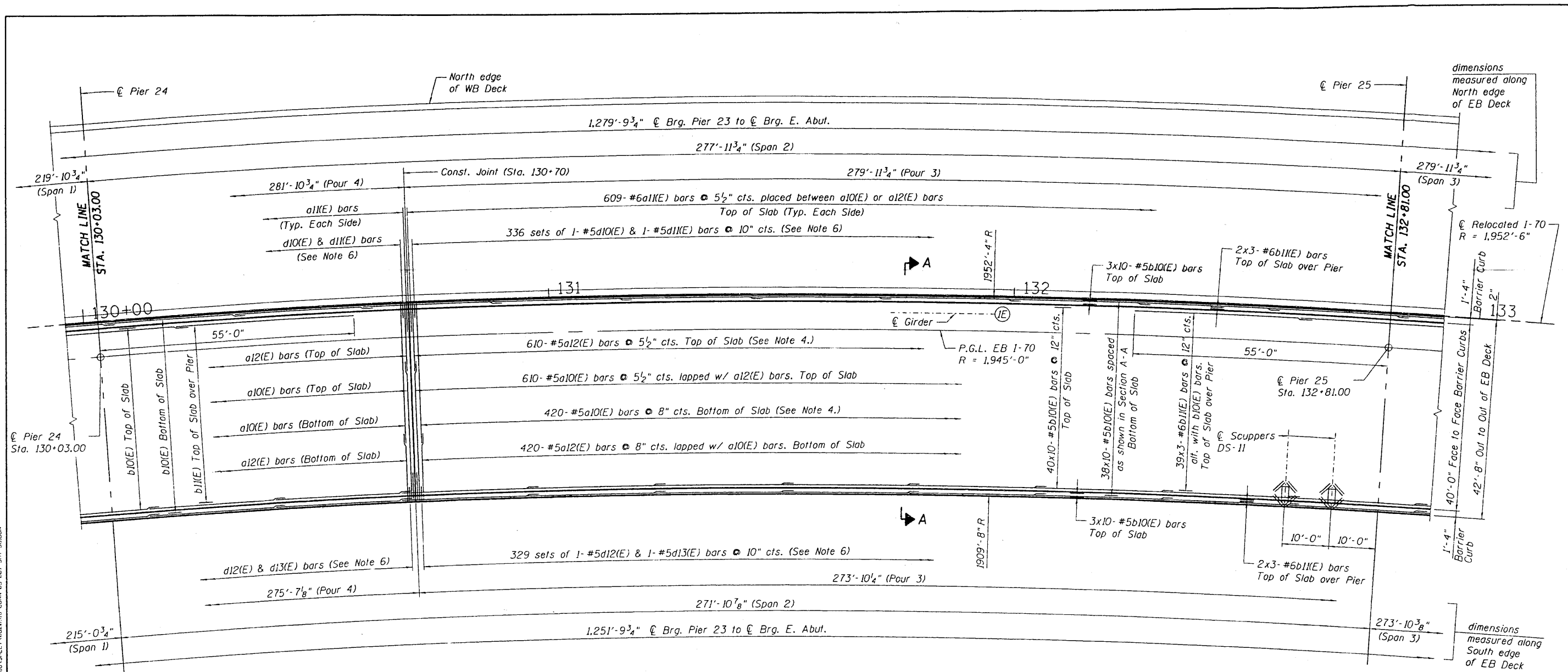
FILE NAME =	USER NAME =	DESIGNED - JLR	REVISIONS -	<b>STATE OF ILLINOIS</b> <b>DEPARTMENT OF TRANSPORTATION</b> <b>I-70 CONNECTION OVER</b> <b>NS, TRRA, MCT AND INDUSTRIAL DR.</b>	<b>DECK CROSS SECTIONS</b> <b>2 OF 2</b>	F.A.P. RTE. 998	SECTION 82-2-IHVB	COUNTY ST. CLAIR	TOTAL SHEETS 285	SHEET NO. 133	
#FILE#	PLOT SCALE =	DRAWN - FD	REVISIONS -			SCALE:	SHEET NO. S-23 OF S-111	STA. 134+22.00 TO STA.	FED. ROAD DIST. NO.	ILLINOIS FED. AID PROJECT	CONTRACT NO. 76C44
DESIGNED - JLR	REVISIONS -	CHECKED - TCU	REVISIONS -			DATE - 06/04/10	REVISIONS -				
DESIGNED - JLR	REVISIONS -	CHECKED - TCU	REVISIONS -			DATE - 06/04/10	REVISIONS -				



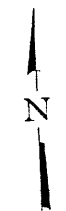


- NOTES:**
1. Work this sheet with Shts. S-22 thru S-47.
  2. Bars indicated thus 20x3- #5 etc. indicates 20 lines of bars with 3 lengths per line.
  3. Longitudinal b(E) bars shall be sprung into place to be concentric at the spacing noted.
  4. Transverse a(E) bars shall be placed radially at the spacing noted. The spacing is measured along @ of Girder IE.
  5. Minimum Lap for Deck Reinforcement:
    - #5 Bars = 2'-2"
    - #6 Bars = 2'-7"
  6. Space bars to miss Barrier Curb Joints.
  7. For layout of bars and additional edge beam reinforcement, see Shts. S-45 and S-46.

FILE NAME : USER NAME : #USER\* DESIGNED - JLR REVISED - DRAWN - FD REVISED - CHECKED - TCU REVISED - DATE - 06/04/10 REVISED -  
 TENG & ASSOCIATES, INC. ENGINEERS/ARCHITECTS/PLANNERS CHICAGO, ILLINOIS  
 STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION 1-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR. SCALE: SHEET NO. S-24 OF S-111 STA. 134+22.00 TO STA. F.A.P. RTE. 998 SECTION B2-2-1HVB COUNTY ST. CLAIR TOTAL SHEETS 285 SHEET NO. 134 SN 082-031B (EB) & 0319 (WB) CONTRACT NO. 76C44 FED. ROAD DIST. NO. ILLINOIS FED. AID PROJECT



DECK PLAN - EB I-70 SPAN 2

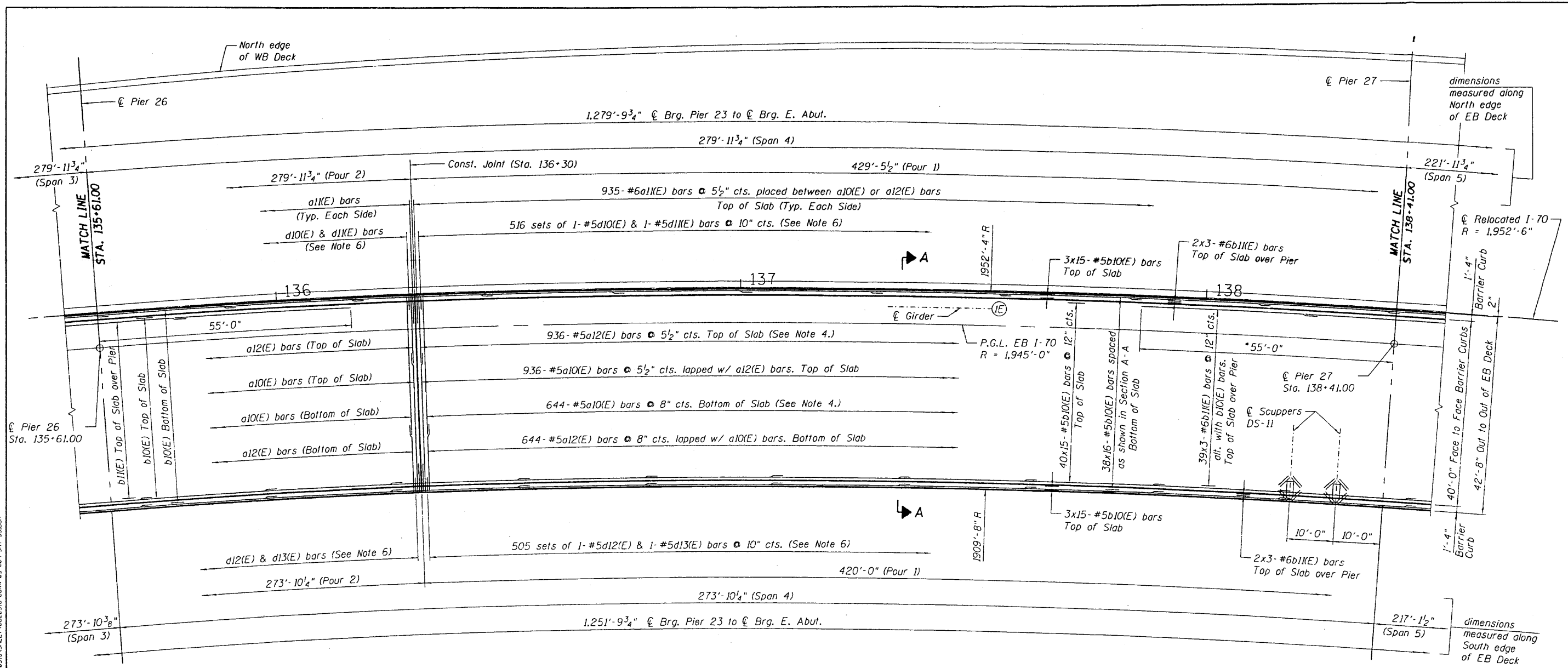


NOTE:  
See Sht. S-24 for notes.

FILE NAME : USER NAME : #USER# DESIGNED - JLR REVISED -  
 #FILE# DRAWN - FD REVISED -  
 CHECKED - TCU REVISED -  
 DATE - 06/04/10 REVISED -  
 TENG & ASSOCIATES, INC. ENGINEERS/ARCHITECTS/PLANNERS CHICAGO, ILLINOIS

STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION I-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR.		DECK PLAN EB I-70 2 OF 5		F.A.P. RTE. 998	SECTION 82-2-1HVB	COUNTY ST. CLAIR	TOTAL SHEETS 285	SHEET NO. 135
SCALE:		SHEET NO. 5-25 OF 5-111		STA. 134+22.00 TO STA.		CONTRACT NO. 76C44		





DECK PLAN - EB I-70 SPAN 4

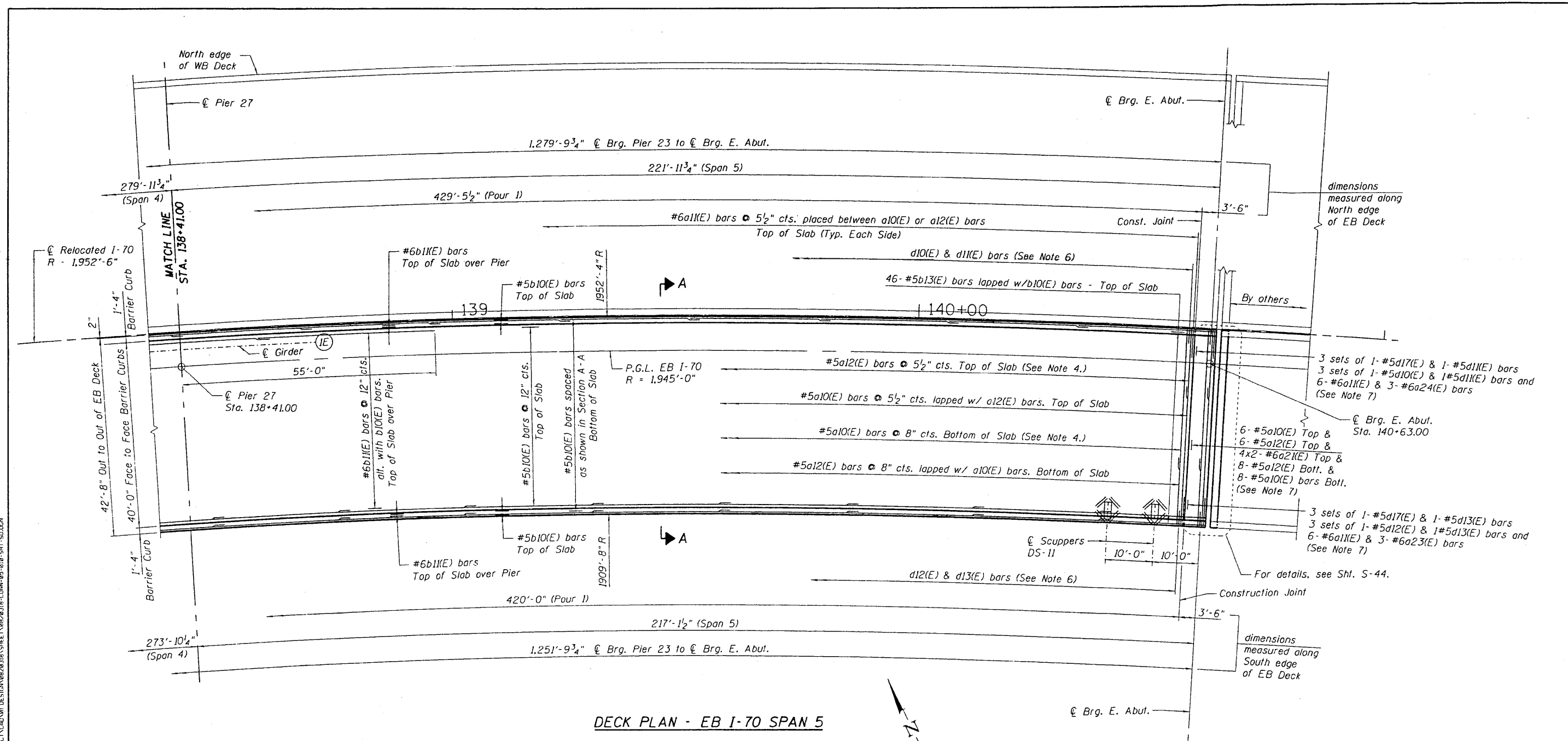


NOTE:  
See Sht. S-24 for notes.

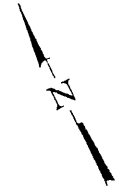
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FILE NAME	USER NAME	DESIGNED - JLR	REVISED -	STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION I-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR.	DECK PLAN EB I-70 4 OF 5	F.A.P. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.	
#FILE#		DRAWN - FD	REVISED -			998	B2-2-IHVB	ST. CLAIR	285	137	
PLT SCALE	SCALE#	CHECKED - TCU	REVISED -			SN 082-0318 (EB) & 0319 (WB) CONTRACT NO. 16L244					
PLT DATE	DATE#	DATE - 06/04/10	REVISED -			FED. ROAD DIST. NO. ILLINOIS FED. AID PROJECT					
						SCALE:	SHEET NO. S-27 OF S-111	STA. 134+22.00 TO STA.			





**DECK PLAN - EB I-70 SPAN 5**

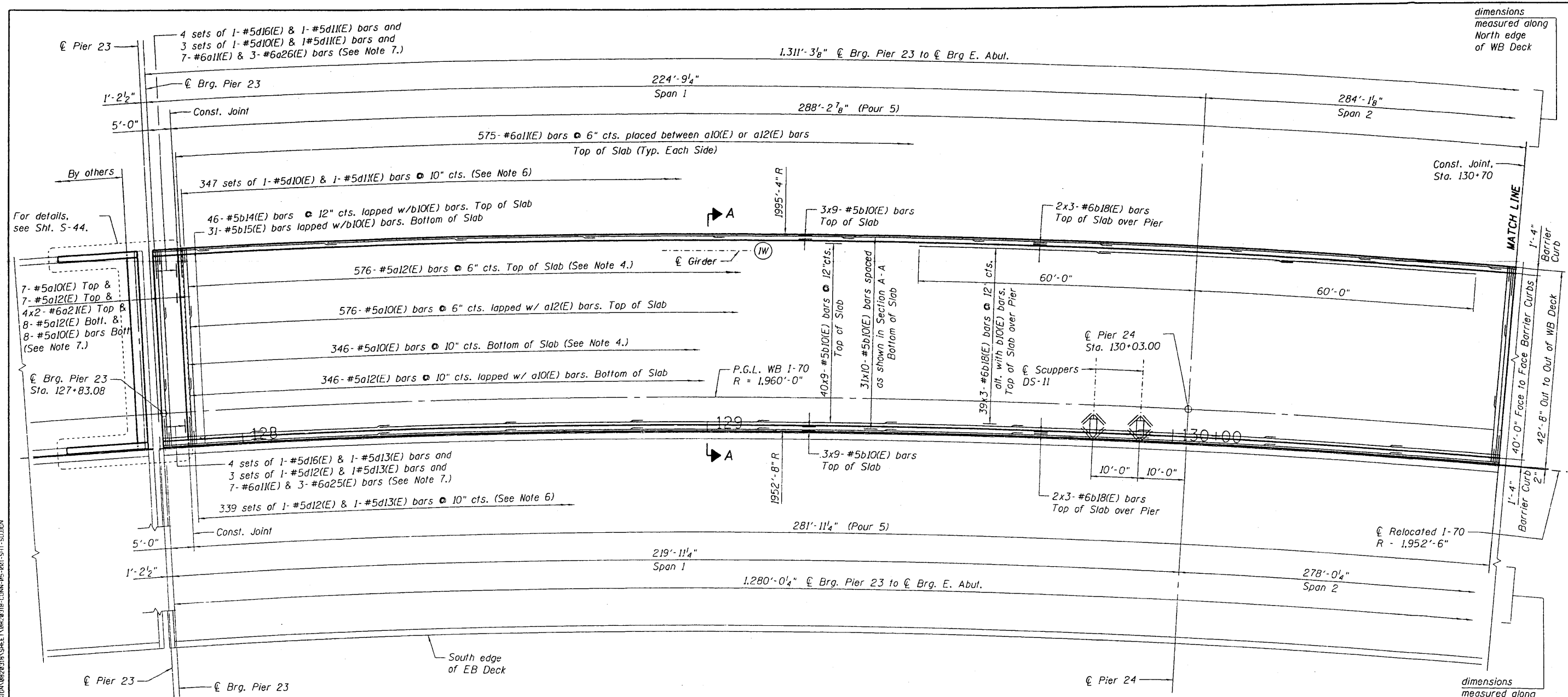


**NOTE:**  
See Sht. S-24 for notes.

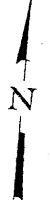
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FILE NAME	USER NAME = #USER#	DESIGNED - JLR	REVISED -	<b>STATE OF ILLINOIS</b> <b>DEPARTMENT OF TRANSPORTATION</b> I-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR.	<b>DECK PLAN EB I-70</b> <b>5 OF 5</b>			F.A.P. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
#FILE#		DRAWN - FD	REVISED -		998	82-2-1HVB	ST. CLAIR	285	138			
		CHECKED - TCU	REVISED -		SN 082-0318 (EB) & 0319 (WB) CONTRACT NO. 76C24							
	PLOT SCALE = #SCALE#	DATE - 06/04/10	REVISED -	SCALE:	SHEET NO. S-28 OF 5-111	STA. 134+22.00 TO STA.	ILLINOIS FED. AID PROJECT					





DECK PLAN - WB I-70 POUR 5



- NOTES:**
- Work this sheet with Shts. S-22 thru S-47.
  - Bars indicated thus 20x3-#5 etc. indicates 20 lines of bars with 3 lengths per line.
  - Longitudinal b(E) bars shall be sprung into place to be concentric at the spacing noted.
  - Transverse a(E) bars shall be placed radially to P.G.L. at the spacing noted. The spacing is measured along C of Girder IW.
  - Minimum Lap for Deck Reinforcement:  
 #5 Bars = 2'-2"  
 #6 Bars = 2'-7"
  - Space bars to miss Barrier Curb Joints.
  - For layout of bars and additional edge beam reinforcement, see Shts. S-45 and S-46.

...C:\WORK\118\CON-05-001-SLIC0A... \NF5-084\AM\VAL1\...  
 ...C:\WORK\118\CON-05-001-SLIC0A... \NF5-084\AM\VAL1\...  
 ...C:\WORK\118\CON-05-001-SLIC0A... \NF5-084\AM\VAL1\...  
 ...C:\WORK\118\CON-05-001-SLIC0A... \NF5-084\AM\VAL1\...

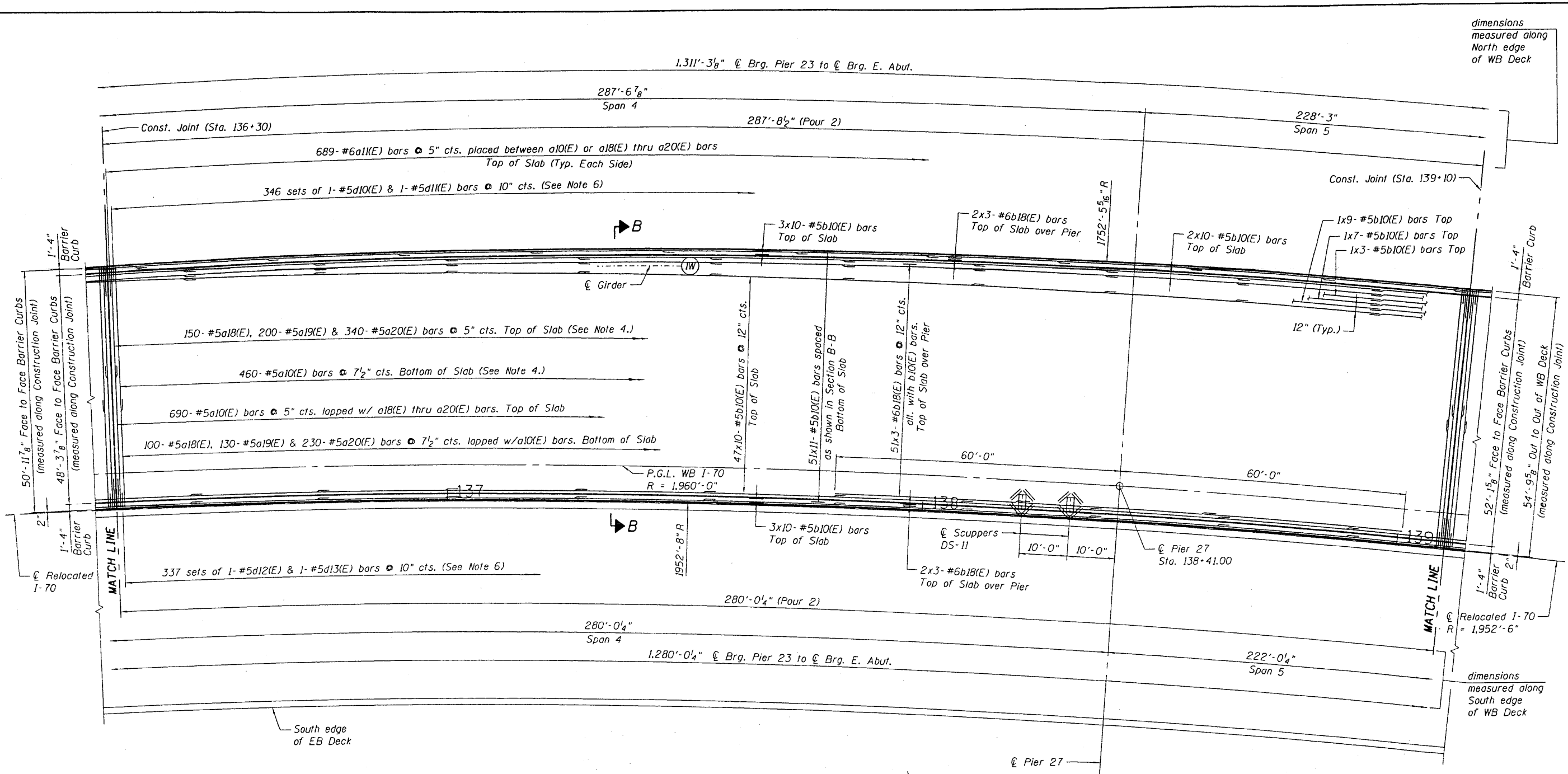
FILE NAME *	USER NAME * #USER#	DESIGNED - JLR	REVISED -	<b>STATE OF ILLINOIS</b> <b>DEPARTMENT OF TRANSPORTATION</b> I-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR.	<b>DECK PLAN WB I-70</b> <b>1 OF 5</b>	F.A.P. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
#FILE#	PLOT SCALE * #SCALE#	DRAWN - FD	REVISED -			998	82-2-1HVB	ST. CLAIR	285	139
	PLOT DATE * #DATE#	CHECKED - TCU	REVISED -			SN 082-0518 (EB) & 0519 (WB)		CONTRACT NO. 76C44		
DATE - 06/04/10					SCALE:	SHEET NO. S-29 OF S-111		STA. 134+22.00 TO STA.		FED. ROAD DIST. NO. ILLINOIS FED. AID PROJECT







dimensions  
measured along  
North edge  
of WB Deck



**DECK PLAN - WB I-70 POUR 2**

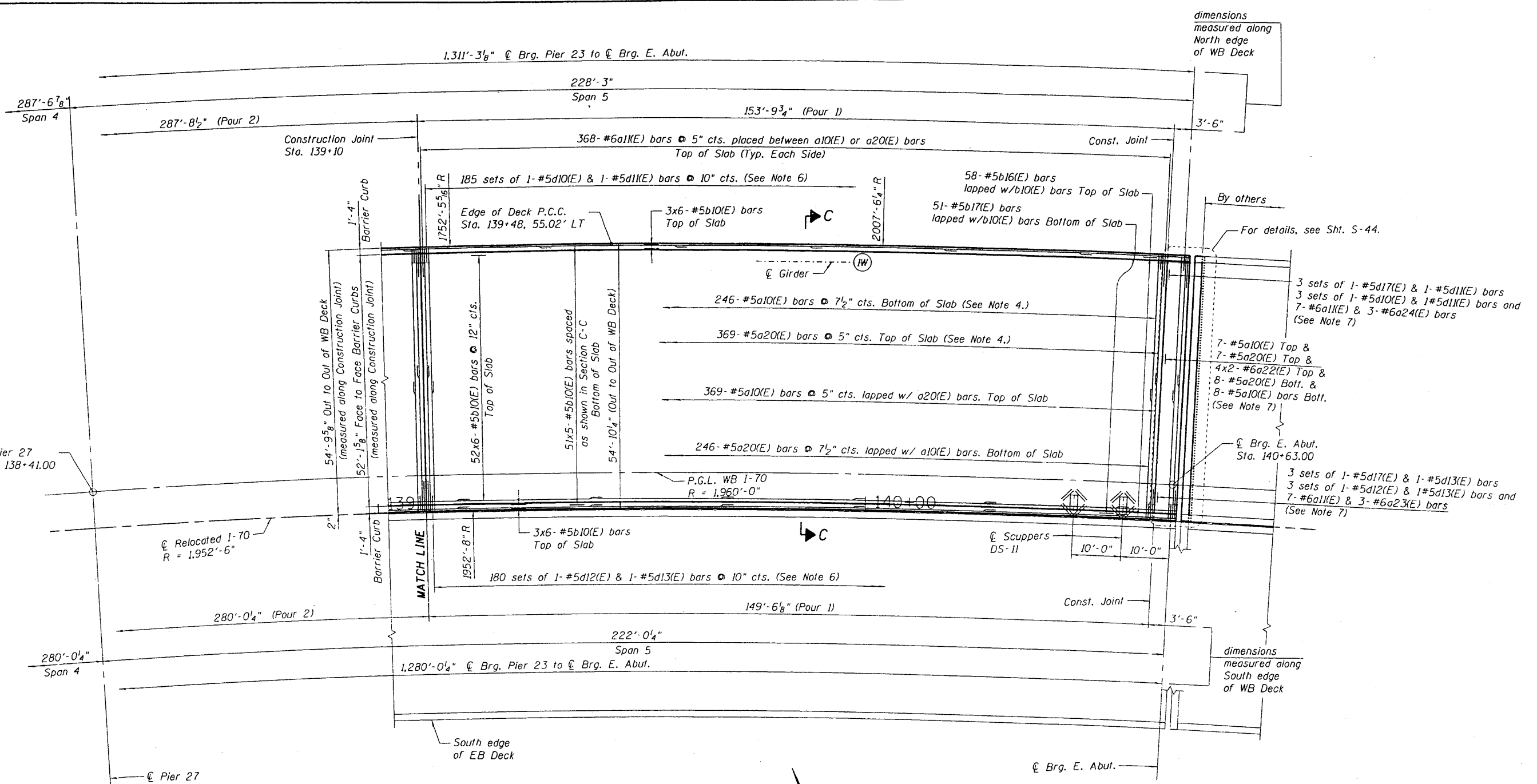
**NOTE:**  
See Sht. S-29 for notes.

FILE NAME : USER NAME : \*USER\* DESIGNED - JLR REVISED - DRAWN - FD REVISED - CHECKED - TCU REVISED - DATE - 06/04/10 REVISED -

STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION I-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR.			DECK PLAN WB I-70 4 OF 5			F.A.P. RTE. SECTION COUNTY TOTAL SHEETS SHEET NO. 998 82-2-1HVB ST. CLAIR 285 142		
SCALE: SHEET NO. S-32 OF S-111 STA. 134+22.00 TO STA.			CONTRACT NO. 76C44			FED. ROAD DIST. NO. ILLINOIS FED. AID PROJECT		



FILE NAME : USER NAME : #USERS DESIGNED - JLR REVISED - DRAWN - FD REVISED - CHECKED - TCU REVISED - DATE - 06/04/10 REVISED -  
 TENC & ASSOCIATES, INC. ENGINEERS ARCHITECTS PLANNERS CHICAGO, ILLINOIS  
 STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION NS, TRRA, MCT AND INDUSTRIAL DR. SCALE: SHEET NO. S-33 OF S-111 STA. 134+22.00 TO STA. SHEET NO. S-34 OF S-111 STA. 134+22.00 TO STA. CONTRACT NO. 76644



DECK PLAN - WB I-70 POUR 1

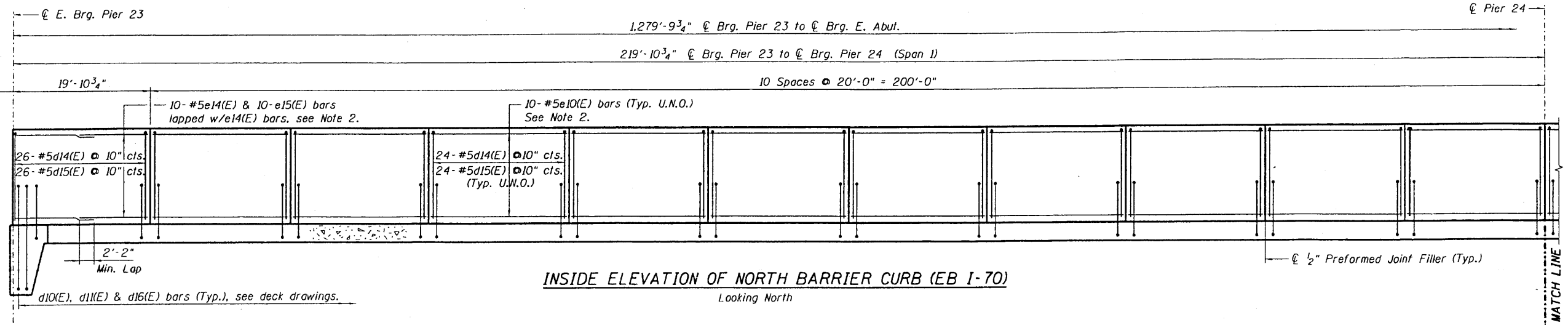
NOTE:  
See Sht. S-29 for notes.

FILE NAME :	USER NAME : #USERS	DESIGNED - JLR	REVISED -	STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION	DECK PLAN WB I-70 5 OF 5	F.A.P. RTE.:	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
#FILE#		DRAWN - FD	REVISED -			998	82-2-14VB	ST. CLAIR	285	143
PLOT SCALE : #SCALE#				CHECKED - TCU	REVISED -	SN 062 0310 (EB) & 0319 (WB)		CONTRACT NO. 76644		
PLOT DATE : #DATE#				DATE - 06/04/10	REVISED -	FED. ROAD DIST. NO.		ILLINOIS FED. AID PROJECT		

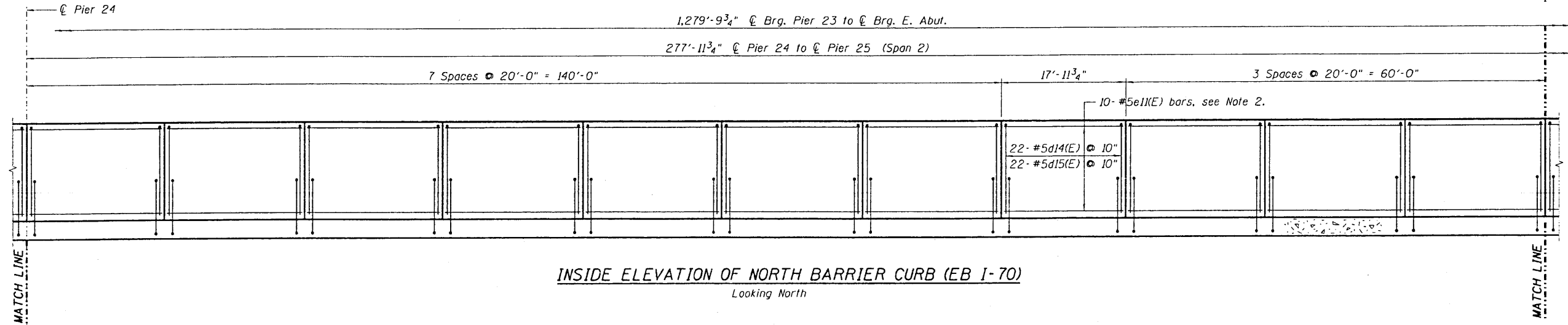
For details of barrier curb panel west of Pier 23, see Sht. S-42.

Barrier Curb joint spacing (Typ.)

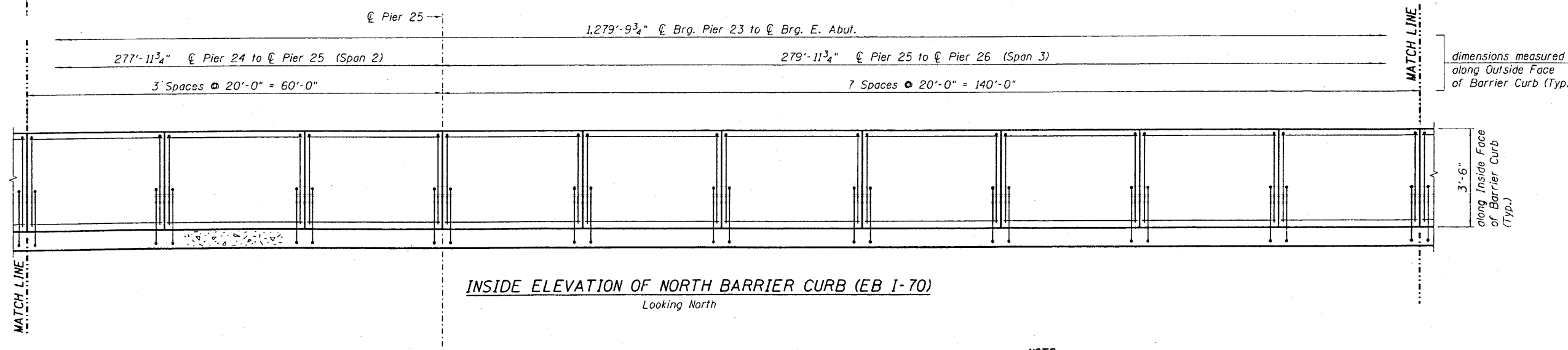
Blockout for joint, see Sht. S-45



**INSIDE ELEVATION OF NORTH BARRIER CURB (EB I-70)**  
Looking North



**INSIDE ELEVATION OF NORTH BARRIER CURB (EB I-70)**  
Looking North



**INSIDE ELEVATION OF NORTH BARRIER CURB (EB I-70)**  
Looking North

NOTE:  
See Sht. S-35 for Notes.

FILE NAME = ... USER NAME = #USERS ... DESIGNED - JLR ... REVISED - ... DRAWN - FD ... REVISED - ... CHECKED - TCJ ... REVISED - ... DATE - 06/04/10 ... REVISED - ...  
 TENC ENGINEERS & ARCHITECTS/PLANNERS CHICAGO, ILLINOIS  
 STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION 1-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR. SCALE: SHEET NO. S-34 OF S-111 STA. 134+22.00 TO STA. F.A.P. RTE. 998 SECTION 82-2-1HVB COUNTY ST. CLAIR TOTAL SHEETS 285 SHEET NO. 144 SN OR2-0318 (EB) & 0319 (WB) CONTRACT NO. 76C44 FED. ROAD DIST. NO. ILLINOIS FED. AID PROJECT



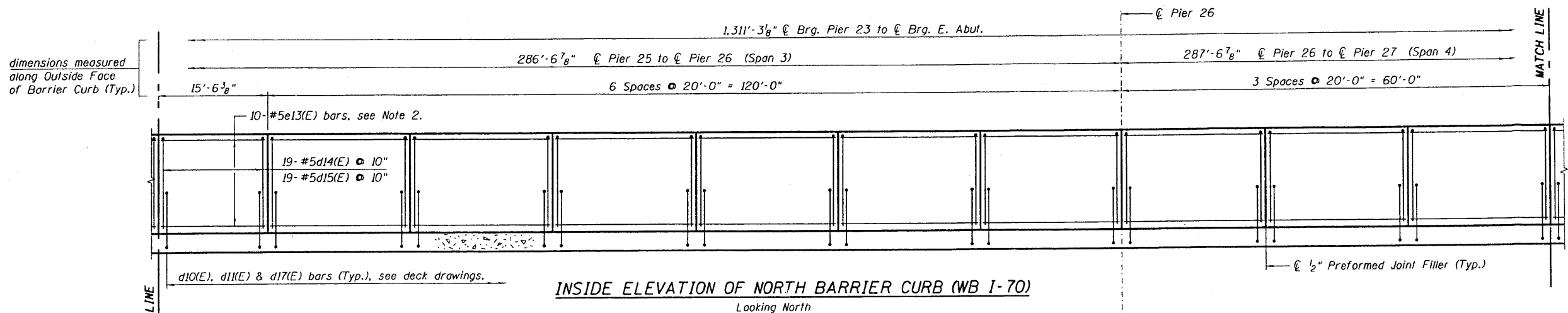




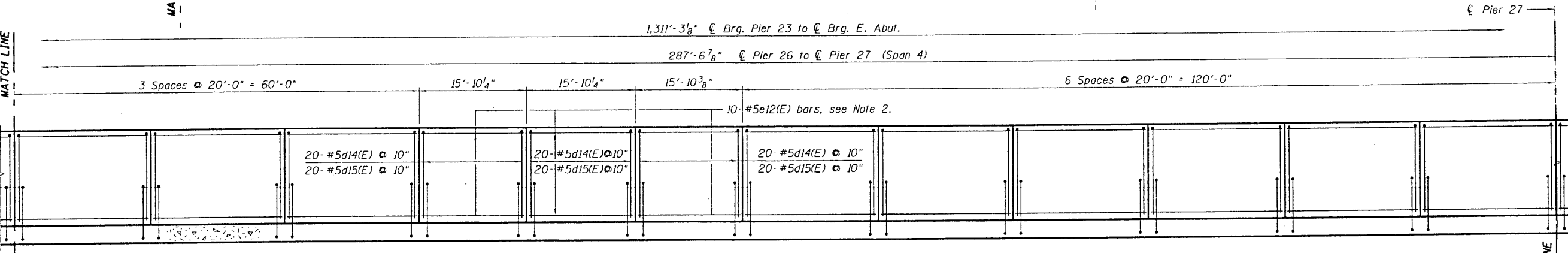


TENG & ASSOCIATES, INC. ENGINEERS/ARCHITECTS/PLANNERS CHICAGO, ILLINOIS  
BONDHUIJ  
C:\P\2013\CONV-05-001-SULCON\_\P\2013\CONV-05-001-SULCON\_\P\2013\DESIGN\0822318\5\SHEET\0822318-COMM-05-18D-SHT-SULCON

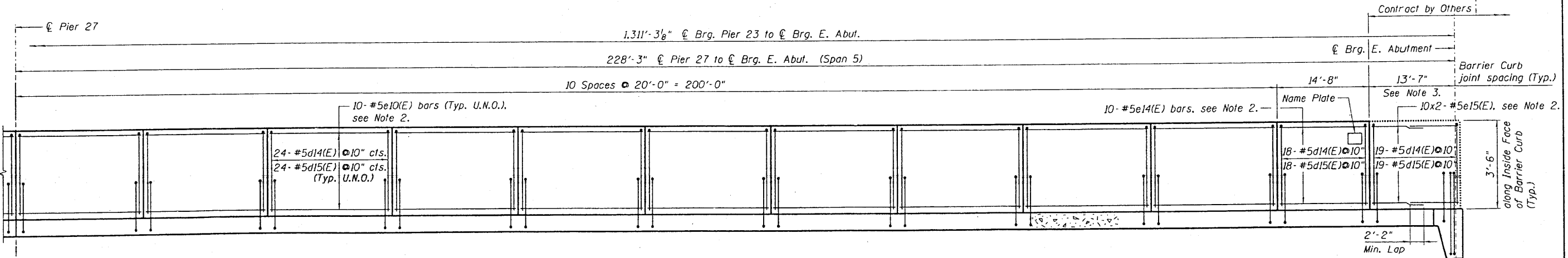
dimensions measured along Outside Face of Barrier Curb (Typ.)



**INSIDE ELEVATION OF NORTH BARRIER CURB (WB I-70)**  
Looking North



**INSIDE ELEVATION OF NORTH BARRIER CURB (WB I-70)**  
Looking North



**INSIDE ELEVATION OF NORTH BARRIER CURB (WB I-70)**  
Looking North

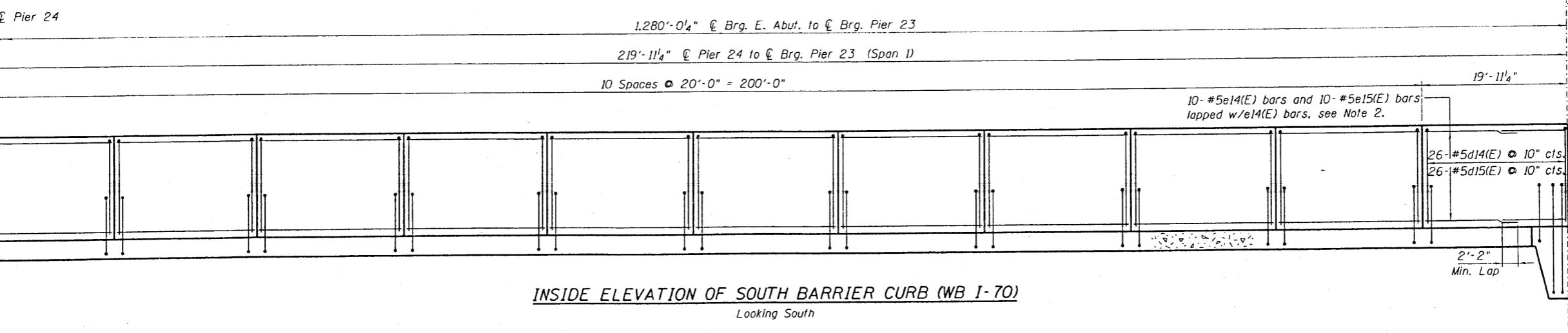
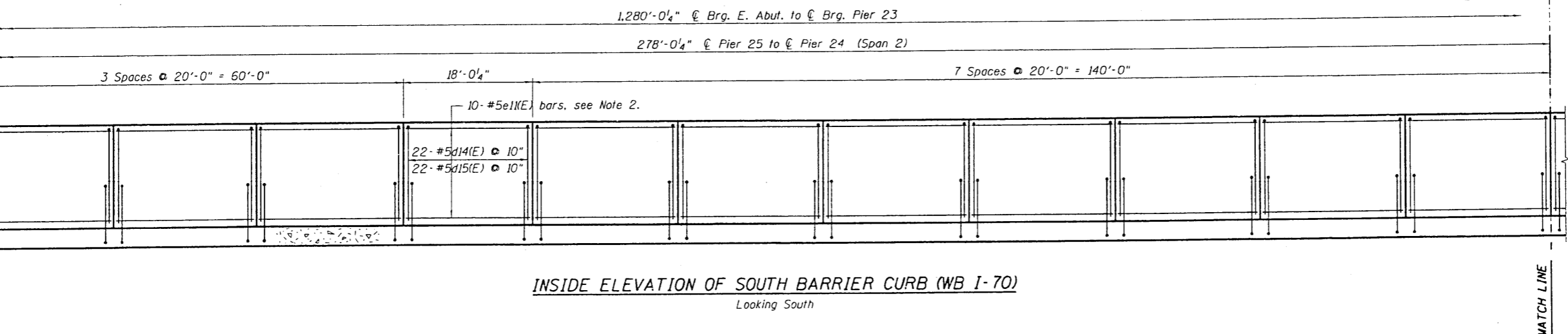
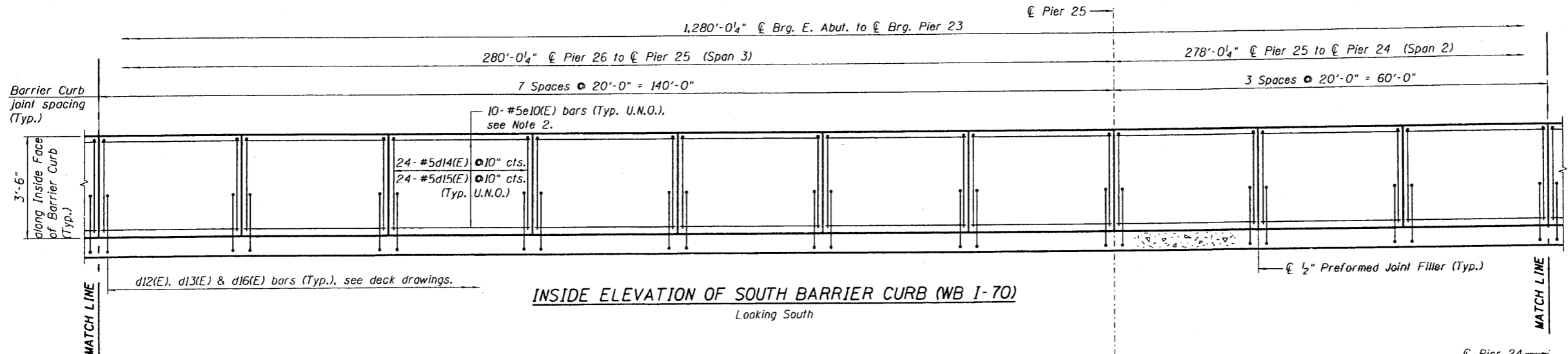
- NOTES:**
1. Work this sheet with Shts. S-22 thru S-47.
  2. Rebar shall be spaced as shown in details on Sht. S-42.
  3. Barrier segment reinforcement included in this Contract.  
Forming and concrete placement for barrier included in Contract by Others.

FILE NAME = PFILE#	USER NAME = #USER#	DESIGNED - JLR DRAWN - FD	REVISED - REVISED -	<b>STATE OF ILLINOIS</b> <b>DEPARTMENT OF TRANSPORTATION</b> I-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR.	<b>PARAPET ELEVATIONS WB I-70</b> <b>2 OF 4</b>	F.A.P. #	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
TENG & ASSOCIATES, INC. ENGINEERS/ARCHITECTS/PLANNERS CHICAGO, ILLINOIS	PLOT SCALE = #SCALE#	CHECKED - TCU	REVISED -			998	82-2-1HVB	ST. CLAIR	285	149
DATE - 06/04/10	PLOT DATE = #DATE#	DATE - 06/04/10	REVISED -			SN 082-0518 (EB) & 0519 (WB)	CONTRACT NO. T6C44	FED. ROAD DIST. NO.	ILLINOISIFIED AID PROJECT	
						SCALE:	SHEET NO. S-39 OF S-111	STA. 134+22.00 TO STA.		

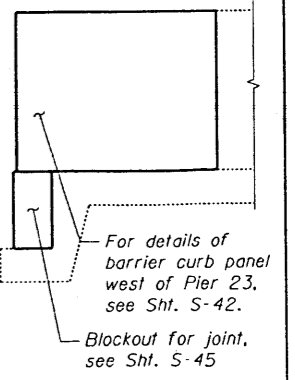




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 USER: BONDHJJD  
 DATE: 06/04/10

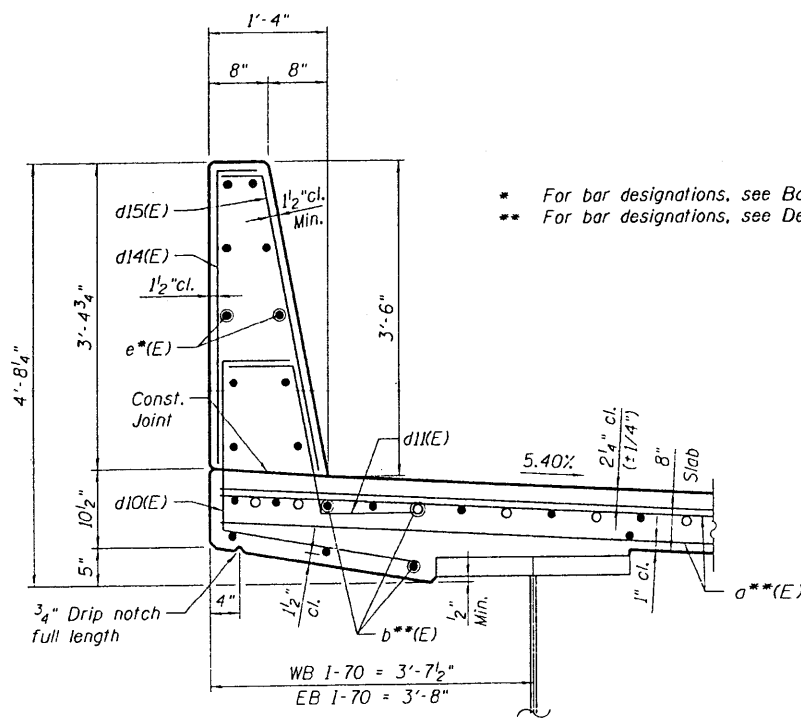


dimensions measured along Outside Face of Barrier Curb (Typ.)

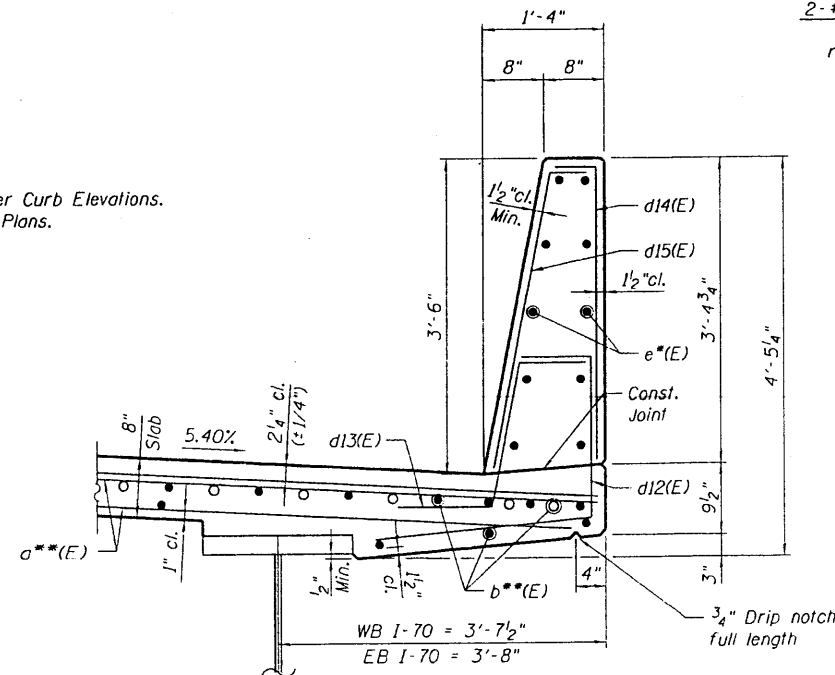


**NOTE:**  
 See Sht. S-39 for Notes.

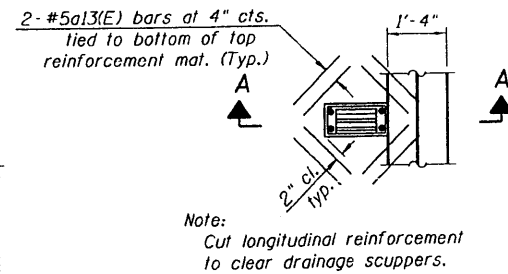
FILE NAME:	USER NAME: BONDHJJD	DESIGNED: JLR	REVISED:	<b>STATE OF ILLINOIS</b> <b>DEPARTMENT OF TRANSPORTATION</b> I-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR.	<b>PARAPET ELEVATIONS WB I-70</b> <b>4 OF 4</b>		F.A.P. RTE. 998	SECTION 82-2-1HVB	COUNTY ST. CLAIR	TOTAL SHEETS 285	SHEET NO. 151	
SCALE:	PLOT SCALE: 1/8" = 1'-0"	CHECKED: TCU	REVISED:		SHEET NO. S-41	OF S-111	STA. 134+22.00	TO STA.	SN 082-0318 (EB) & 0319 (WB) CONTRACT NO. 76C44 FED. ROAD DIST. NO. ILLINOIS FED. AID PROJECT			
DATE:	PLOT DATE:	DATE: 06/04/10	REVISED:									
<b>TENG</b> ENGINEERS & ARCHITECTS/PLANNERS CHICAGO, ILLINOIS												



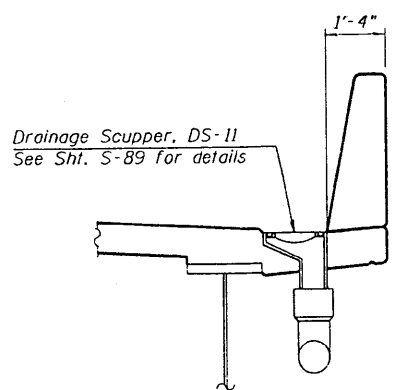
**NORTH BARRIER CURB DETAIL**



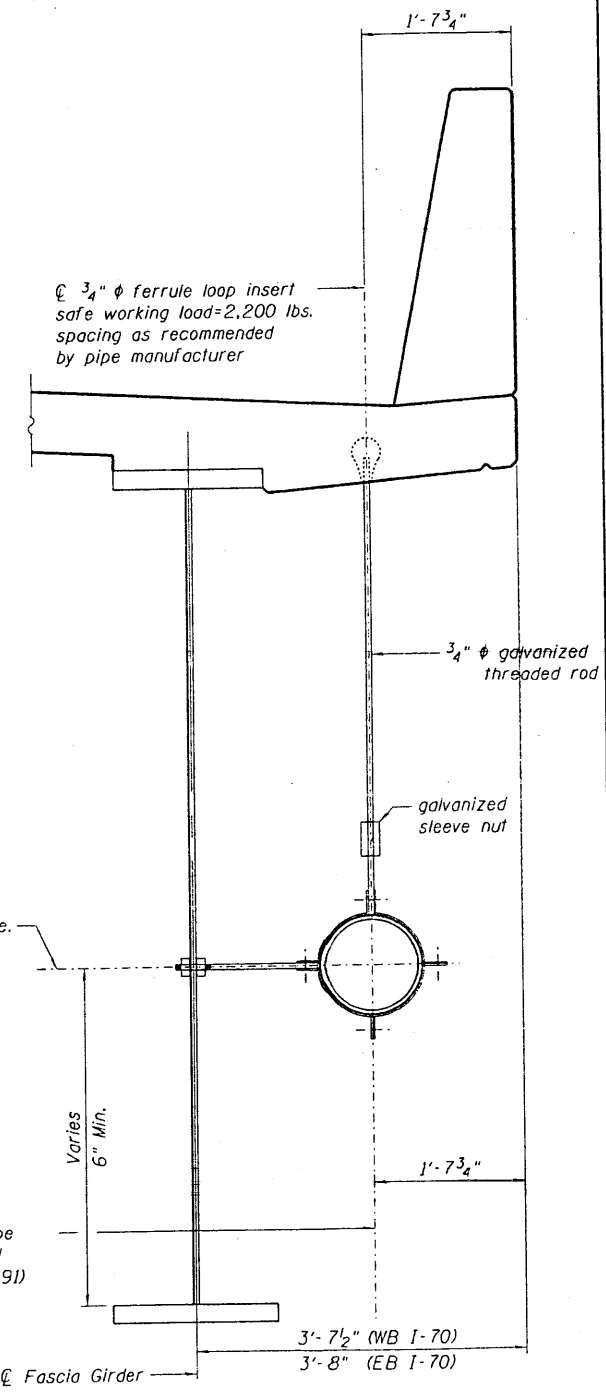
**SOUTH BARRIER CURB DETAIL**



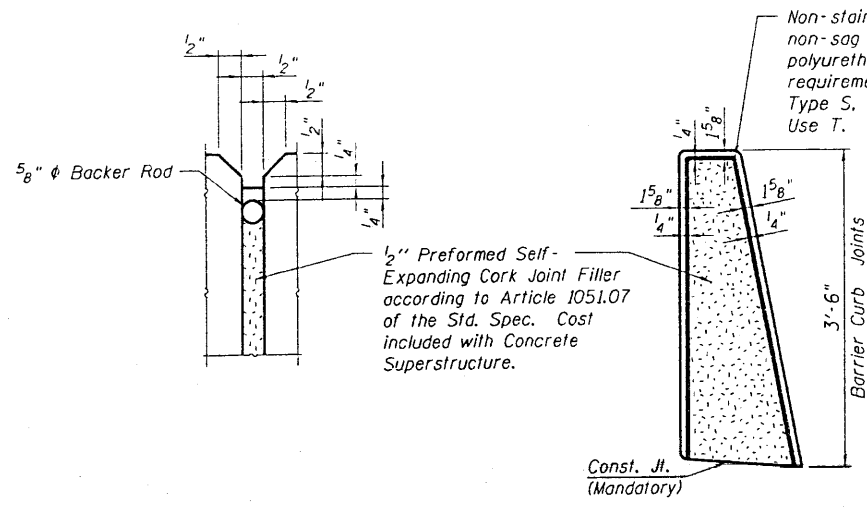
**PLAN**



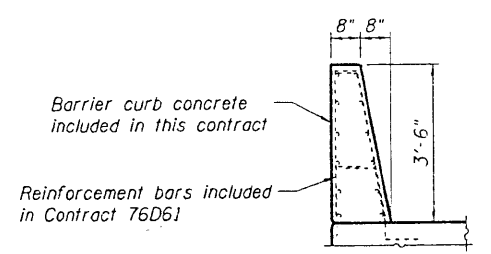
**SECTION A-A**



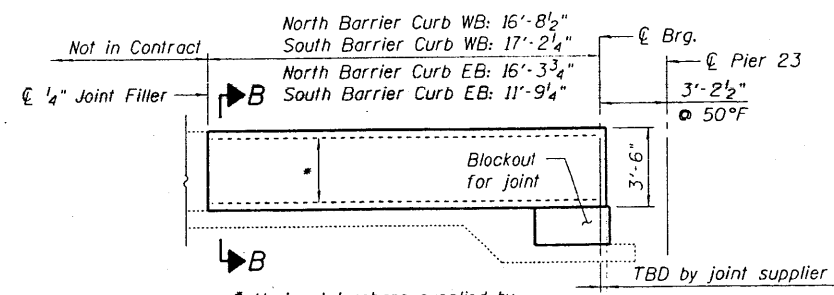
**PIPE HANGER DETAIL**



**BARRIER CURB JOINT DETAILS**



**SECTION B-B**



**BARRIER ELEVATION**

(Barrier at Pier 23, west of Exp. Joint)

**NOTE:**  
Work this sheet with Shts. S-22 thru S-47.

FILE NAME: USER NAME: #USER# DESIGNED - JLR REVISED -  
 #FILE# DRAWN - FD REVISED -  
 PLO: SCALE = #SCALE# CHECKED - TCU REVISED -  
 PLO: DATE = #DATE# DATE - 06/04/10 REVISED -



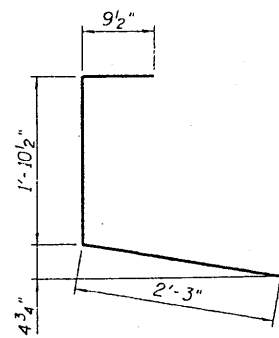
**STATE OF ILLINOIS**  
**DEPARTMENT OF TRANSPORTATION**  
 I-70 CONNECTION OVER  
 NS, TRRA, MCT AND INDUSTRIAL DR.

**DECK DETAILS**

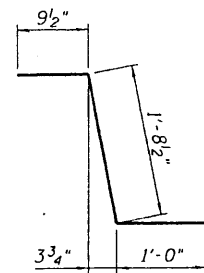
SCALE:	SHEET NO. S-42 OF S-111	STA. 134+22.00 TO STA.
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F.A.P. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
998	B2-2-1HVB	ST. CLAIR	285	152

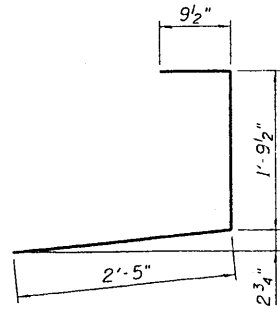
SN 082-0318 (EBI & O319 (WB)) CONTRACT NO. 76C44  
 FED. ROAD DIST. NO. ILLINOIS FED. AID PROJECT



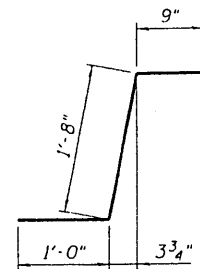
BAR d10(E)



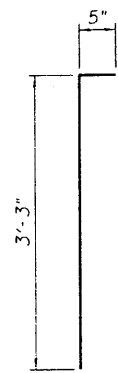
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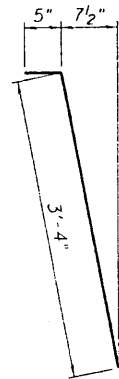
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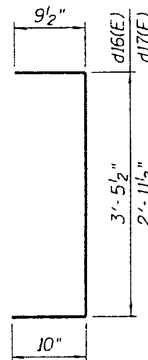
BAR d13(E)



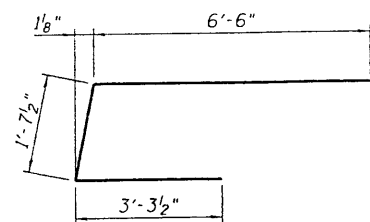
BAR d14(E)



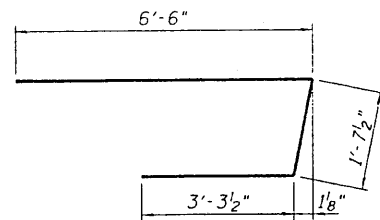
BAR d15(E)



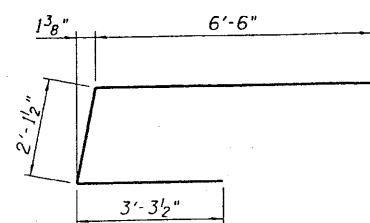
BARS d16(E) & d17(E)



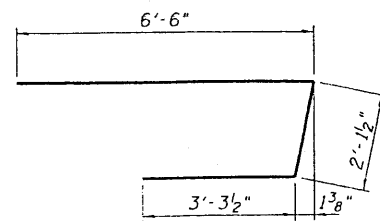
BAR a23(E)



BAR a24(E)



BAR a25(E)



BAR a26(E)

NOTE:  
Work this sheet with Shts. S-22 thru S-47.

EB DECK  
BAR LIST

Bar	No.	Size	Length	Shape
a10(E)	4708	#5	30'-0"	---
a11(E)	5560	#6	6'-6"	---
a12(E)	4708	#5	14'-7"	---
a13(E)	80	#5	1'-6"	---
a21(E)	16	#6	22'-7"	---
a23(E)	3	#6	11'-5"	┌
a24(E)	3	#6	11'-5"	┐
a25(E)	3	#6	11'-11"	┌
a26(E)	3	#6	11'-11"	┐
b10(E)	3818	#5	30'-0"	---
b11(E)	516	#6	38'-5"	---
b12(E)	46	#5	9'-0"	---
b13(E)	46	#5	23'-1"	---
d10(E)	1533	#5	4'-11"	┌
d11(E)	1540	#5	3'-6"	┐
d12(E)	1500	#5	5'-0"	┐
d13(E)	1507	#5	3'-5"	┐
d14(E)	3052	#5	3'-8"	┐
d15(E)	3052	#5	3'-9"	┐
d16(E)	8	#5	5'-1"	┐
d17(E)	6	#5	4'-7"	┐
e10(E)	1170	#5	19'-7"	---
e11(E)	40	#5	17'-7"	---
e12(E)	40	#5	15'-6"	---
e14(E)	10	#5	14'-4"	---
e15(E)	30	#5	8'-6"	---
e16(E)	30	#5	10'-3"	---

WB DECK  
BAR LIST

Bar	No.	Size	Length	Shape
a10(E)	4688	#5	30'-0"	---
a11(E)	5682	#6	6'-6"	---
a12(E)	1853	#5	14'-7"	---
a13(E)	80	#5	1'-6"	---
a14(E)	314	#5	16'-7"	---
a15(E)	213	#5	18'-8"	---
a16(E)	241	#5	20'-9"	---
a17(E)	287	#5	22'-10"	---
a18(E)	250	#5	24'-2"	---
a19(E)	330	#5	25'-6"	---
a20(E)	1200	#5	26'-8"	---
a21(E)	8	#6	22'-7"	---
a22(E)	8	#6	28'-8"	---
a23(E)	3	#6	11'-5"	┌
a24(E)	3	#6	11'-5"	┐
a25(E)	3	#6	11'-11"	┌
a26(E)	3	#6	11'-11"	┐
b10(E)	4184	#5	30'-0"	---
b14(E)	46	#5	23'-6"	---
b15(E)	31	#5	13'-6"	---
b16(E)	58	#5	12'-5"	---
b17(E)	51	#5	22'-5"	---
b18(E)	576	#6	41'-9"	---
d10(E)	1573	#5	4'-11"	┌
d11(E)	1580	#5	3'-6"	┐
d12(E)	1536	#5	5'-0"	┐
d13(E)	1543	#5	3'-5"	┐
d14(E)	3124	#5	3'-8"	┐
d15(E)	3124	#5	3'-9"	┐
d16(E)	8	#5	5'-1"	┐
d17(E)	6	#5	4'-7"	┐
e10(E)	1170	#5	19'-7"	---
e11(E)	20	#5	17'-7"	---
e12(E)	30	#5	15'-6"	---
e13(E)	30	#5	15'-2"	---
e14(E)	70	#5	14'-4"	---
e15(E)	40	#5	8'-6"	---

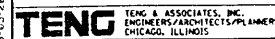
EB DECK  
BILL OF MATERIAL

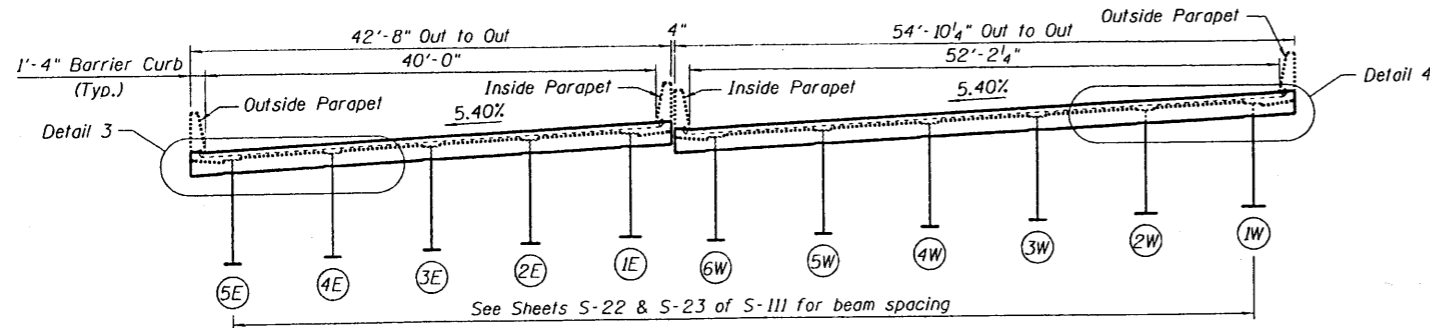
Item	Unit	Total
Concrete Superstructure	Cu. Yd.	1879.5
Reinforcement Bars, Epoxy Coated	Pound	501,230
Bridge Deck Grooving	Sq. Yd.	5,363
Protective Coat	Sq. Yd.	6,835
Name Plates	Each	1

WB DECK  
BILL OF MATERIAL

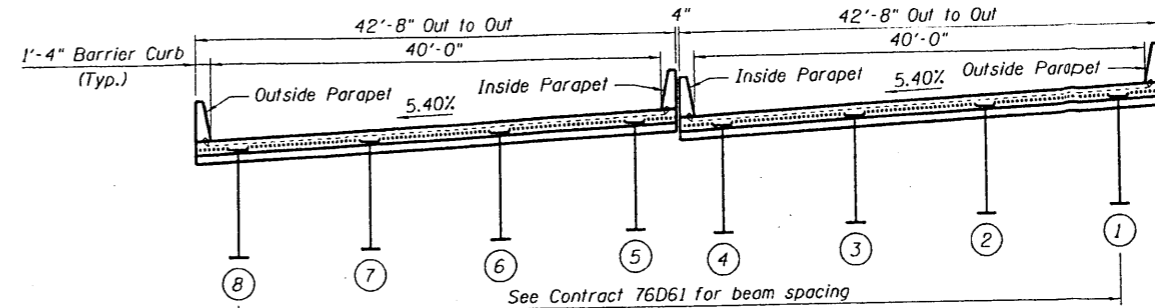
Item	Unit	Total
Concrete Superstructure	Cu. Yd.	2101.9
Reinforcement Bars, Epoxy Coated	Pound	550,130
Bridge Deck Grooving	Sq. Yd.	6,167
Protective Coat	Sq. Yd.	7,674
Name Plates	Each	1

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 B:\000010\104417  
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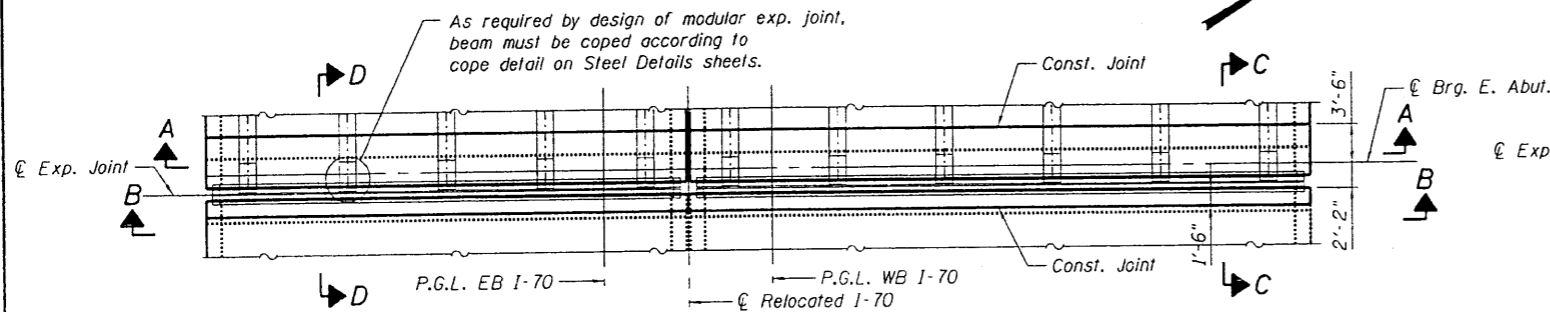




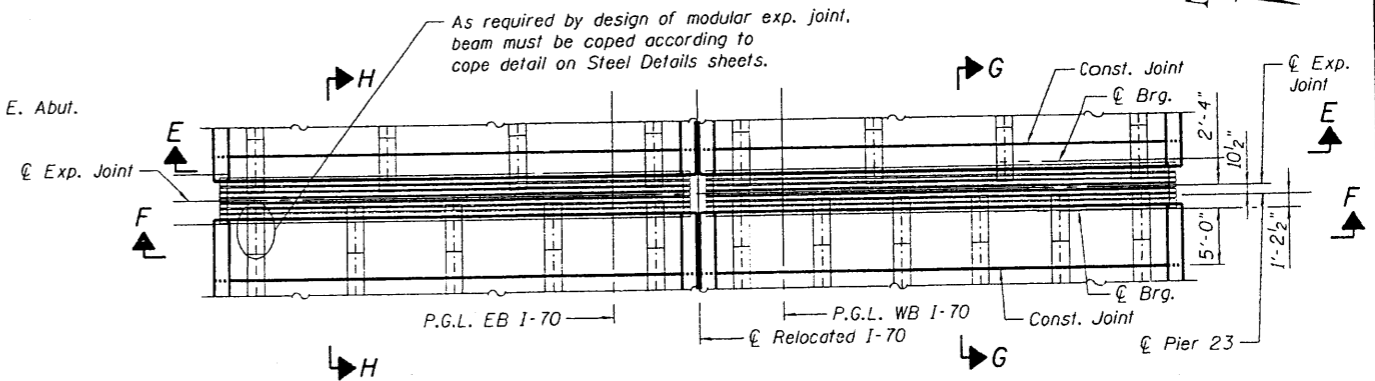
**SECTION A-A**  
Looking West



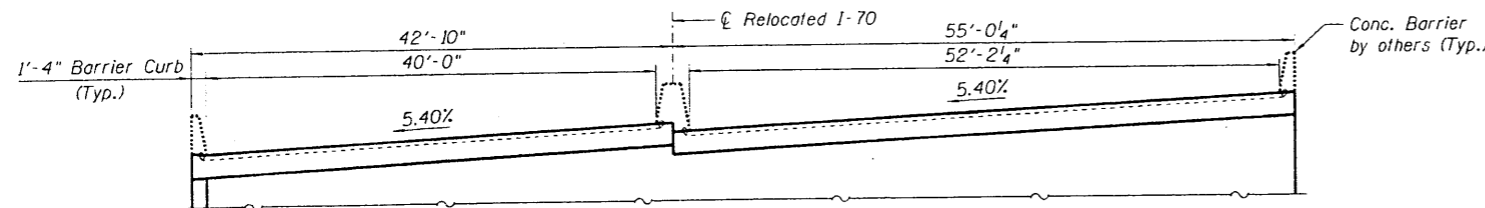
**SECTION E-E**  
Looking West



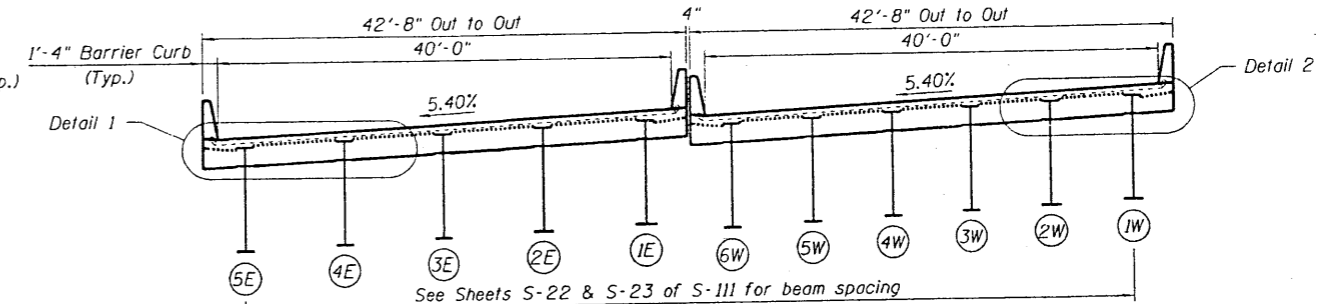
**DECK PLAN AT EAST ABUTMENT**



**DECK PLAN AT PIER 23**



**SECTION B-B**  
Looking West



**SECTION F-F**  
Looking West

**REQUIRED MOVEMENT**

(AASHTO LOAD COMBINATION SERVICE I)

Item	East Abutment	Pier 23
Total longitudinal (open/close) movement	8 1/2"	24"
Total transverse (wracking) movement	1"	1"
Maximum longitudinal break about $\bar{C}$ joint	0.0033 Rad	0.0066 Rad

**BILL OF MATERIAL**

ITEM	UNIT	TOTAL
Modular Expansion Joint - Swivel 9"	Foot	92.5
Modular Expansion Joint - Swivel 24"	Foot	80.0

**NOTES:**

1. Work this sheet with Sheets S-22 through S-47.
2. The expansion joint device shall be a prefabricated modular assembly with multiple support bars and separator beams, providing a continuous seal across the deck. The device shall be capable of accommodating differential (non-parallel) open/close movements and transverse (wracking) movements. The design concept shall have been tested successfully under dynamic conditions representative of seismic demands.
3. Joint longitudinal opening shall be adjusted according to Article 520.04 of the Standard Specifications when the end of the deck is cast at an ambient temperature other than 50° F.
4. The opposing sides of the joint assembly shall be positioned with respect to the face of parapet on each deck as shown in the plans. At 50° F, the opposing sides of the joint assembly shall be aligned transversely. The neoprene strip seals shall be secured in place with the opposing sides of the joint aligned transversely.
5. Concrete in end of the deck to be placed after the Modular Joint is fixed in position.
6. Modular expansion joints shall be assembled in their final relative position with the ends in place for shop inspection and acceptance.
7. For sections C-C, D-D, G-G & H-H, see Sht. S-45.





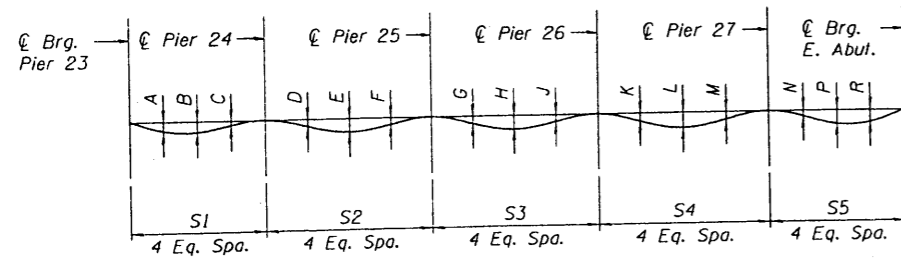








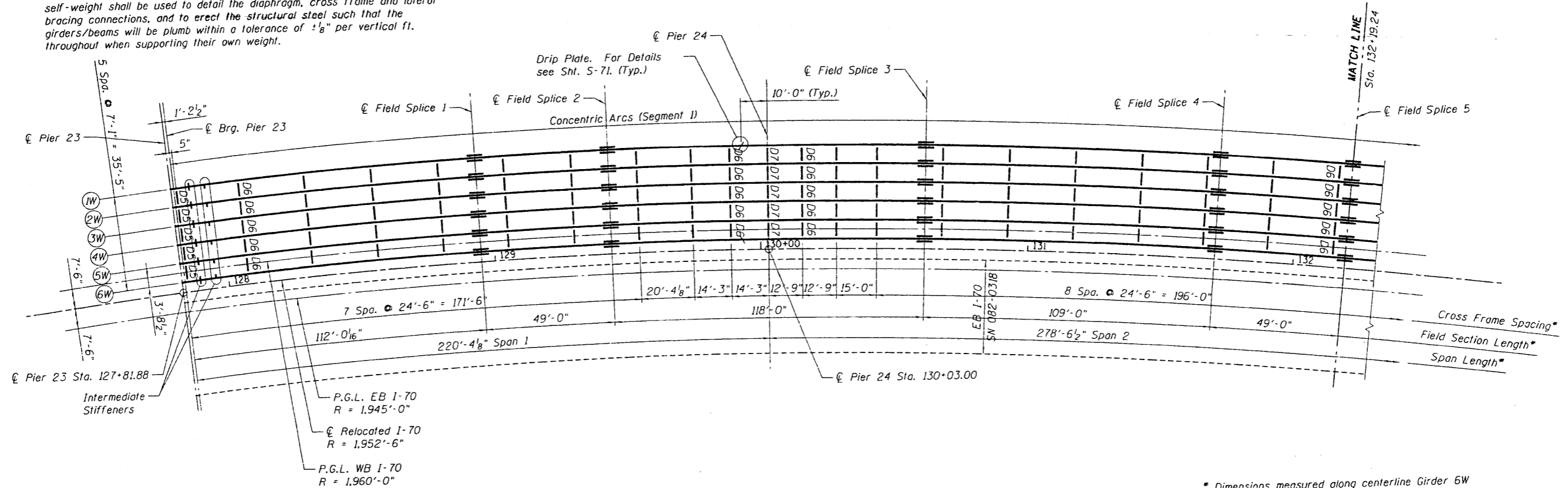




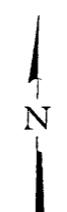
	S1	S2	S3	S4	S5	A	B	C	D	E	F	G	H	J	K	L	M	N	P	R
Girder 1W	224'-4 <sup>5</sup> / <sub>16</sub> "	283'-7"	286'-0 <sup>9</sup> / <sub>16</sub> "	287'-0 <sup>5</sup> / <sub>8</sub> "	227'-10 <sup>1</sup> / <sub>16</sub> "	1 <sup>3</sup> / <sub>8</sub>	1 <sup>9</sup> / <sub>16</sub>	5 <sub>8</sub>	7 <sub>8</sub>	1 <sup>1</sup> / <sub>16</sub>	7 <sub>8</sub>	7 <sub>8</sub>	1 <sup>3</sup> / <sub>4</sub>	7 <sub>8</sub>	7 <sub>8</sub>	1 <sup>1</sup> / <sub>16</sub>	7 <sub>8</sub>	5 <sub>8</sub>	1 <sup>5</sup> / <sub>8</sub>	1 <sup>7</sup> / <sub>16</sub>
Girder 2W	223'-6 <sup>1</sup> / <sub>16</sub> "	282'-6 <sup>7</sup> / <sub>8</sub> "	284'-11 <sup>3</sup> / <sub>8</sub> "	285'-9"	226'-9 <sup>1</sup> / <sub>16</sub> "	1 <sup>3</sup> / <sub>16</sub>	1 <sup>1</sup> / <sub>2</sub>	5 <sub>8</sub>	7 <sub>8</sub>	1 <sup>1</sup> / <sub>16</sub>	7 <sub>8</sub>	7 <sub>8</sub>	1 <sup>1</sup> / <sub>16</sub>	7 <sub>8</sub>	7 <sub>8</sub>	1 <sup>5</sup> / <sub>8</sub>	1 <sup>3</sup> / <sub>16</sub>	5 <sub>8</sub>	1 <sup>7</sup> / <sub>16</sub>	1 <sup>1</sup> / <sub>4</sub>
Girder 3W	222'-9 <sup>1</sup> / <sub>16</sub> "	281'-6 <sup>1</sup> / <sub>16</sub> "	283'-10 <sup>3</sup> / <sub>16</sub> "	284'-5 <sup>3</sup> / <sub>8</sub> "	225'-8 <sub>8</sub> "	1 <sup>1</sup> / <sub>4</sub>	1 <sup>7</sup> / <sub>16</sub>	9 <sub>16</sub>	7 <sub>8</sub>	1 <sup>5</sup> / <sub>8</sub>	7 <sub>8</sub>	7 <sub>8</sub>	1 <sup>5</sup> / <sub>8</sub>	7 <sub>8</sub>	1 <sup>3</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>16</sub>	9 <sub>16</sub>	5 <sub>16</sub>	1 <sup>3</sup> / <sub>8</sub>	1 <sup>3</sup> / <sub>16</sub>
Girder 4W	221'-11 <sup>3</sup> / <sub>8</sub> "	280'-6 <sup>1</sup> / <sub>16</sub> "	282'-9"	283'-1 <sup>3</sup> / <sub>4</sub> "	224'-7 <sub>8</sub> "	1 <sup>3</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>8</sub>	9 <sub>16</sub>	1 <sup>3</sup> / <sub>16</sub>	1 <sup>9</sup> / <sub>8</sub>	1 <sup>3</sup> / <sub>16</sub>	7 <sub>8</sub>	1 <sup>5</sup> / <sub>8</sub>	7 <sub>8</sub>	1 <sup>3</sup> / <sub>16</sub>	1 <sup>9</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>16</sub>	1 <sup>2</sup> / <sub>2</sub>	1 <sup>3</sup> / <sub>16</sub>	1 <sub>8</sub>
Girder 5W	221'-1 <sup>3</sup> / <sub>4</sub> "	279'-6 <sup>9</sup> / <sub>16</sub> "	281'-7 <sup>3</sup> / <sub>4</sub> "	281'-10 <sup>1</sup> / <sub>8</sub> "	223'-6 <sub>8</sub> "	1 <sub>8</sub>	1 <sup>1</sup> / <sub>4</sub>	9 <sub>16</sub>	1 <sup>3</sup> / <sub>16</sub>	1 <sup>9</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>16</sub>	7 <sub>8</sub>	1 <sup>5</sup> / <sub>8</sub>	7 <sub>8</sub>	1 <sup>3</sup> / <sub>16</sub>	1 <sup>9</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>16</sub>	1 <sup>2</sup> / <sub>2</sub>	1 <sup>3</sup> / <sub>16</sub>	1 <sub>8</sub>
Girder 6W	220'-4 <sub>8</sub> "	278'-6 <sup>1</sup> / <sub>2</sub> "	280'-6 <sup>1</sup> / <sub>2</sub> "	280'-6 <sup>1</sup> / <sub>2</sub> "	222'-5 <sup>3</sup> / <sub>16</sub> "	1 <sub>16</sub>	1 <sup>3</sup> / <sub>16</sub>	1 <sub>2</sub>	1 <sup>3</sup> / <sub>16</sub>	1 <sup>9</sup> / <sub>16</sub>	1 <sup>3</sup> / <sub>16</sub>	7 <sub>8</sub>	1 <sup>9</sup> / <sub>16</sub>	7 <sub>8</sub>	1 <sup>3</sup> / <sub>16</sub>	1 <sup>2</sup> / <sub>2</sub>	1 <sup>3</sup> / <sub>16</sub>	1 <sub>2</sub>	1 <sup>1</sup> / <sub>4</sub>	1 <sub>16</sub>

**DEAD LOAD DEFLECTION - STEEL SELF WEIGHT**  
(Includes weight of structural steel only.)

**NOTE:**  
The calculated deflections of the primary girders/beams under steel self-weight shall be used to detail the diaphragm, cross frame and lateral bracing connections, and to erect the structural steel such that the girders/beams will be plumb within a tolerance of  $\pm \frac{1}{8}$ " per vertical ft. throughout when supporting their own weight.



**FRAMING PLAN**  
**WB I-70 SN 082-0319**



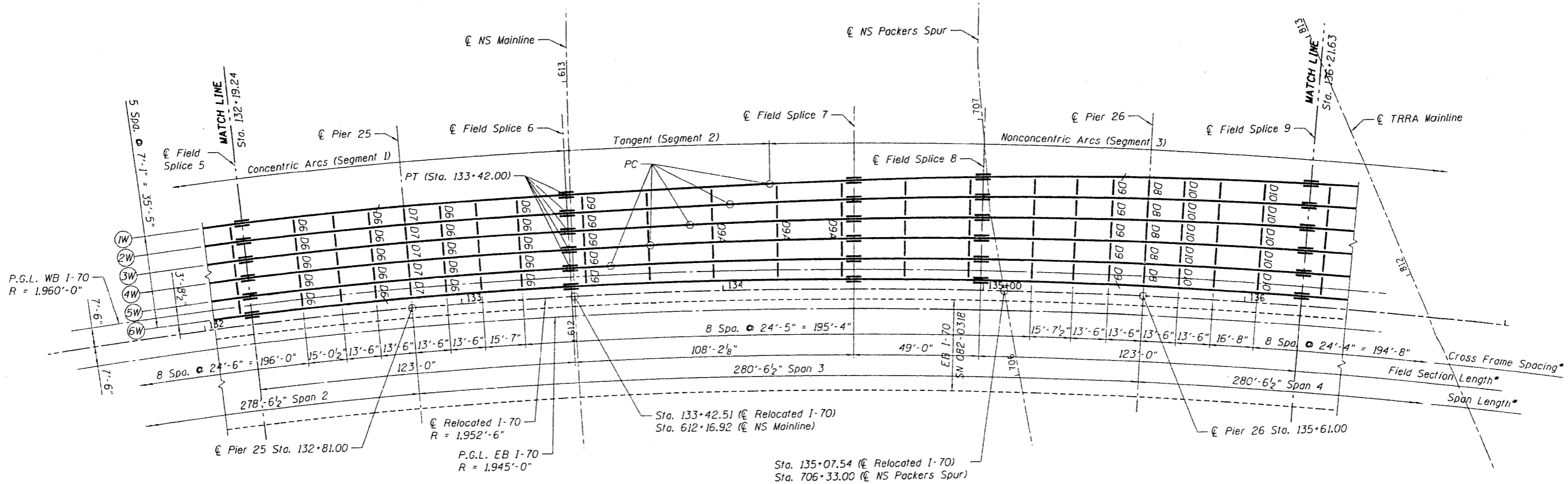
**NOTES:**

1. Work this sheet with Sheets S-52 and S-53.
2. All cross frames or diaphragms between beams or girders shall be installed with erection pins and bolts in accordance with the erection plan approved by the Engineer. Individual cross frames or diaphragms at supports may be temporarily disconnected to install bearing anchor rods.
3. All cross frames shall be installed radial to  $\text{\textcircled{C}}$  Relocated I-70 or parallel to  $\text{\textcircled{C}}$  of bearing of Pier 23.
4. The Contractor shall either:
  1. Ream diaphragm and/or cross frame connection holes during shop assembly, or
  2. Provide detailing and fabrication controls acceptable to the Engineer which ensures accuracy such that field reaming will not exceed the amount permitted in Article 505.08(l) of the Standard Specifications.

\* Dimensions measured along centerline Girder 6W

C:\0820319\0820319-CONV-99-001-BUILDING\0820319-CONV-99-004-CO.DWG, C:\0820319\0820319-SHEET\0820319-CONV-99-001-SHT-FP.DWG  
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<b>TENG</b> TENG & ASSOCIATES, INC. ENGINEERS/ARCHITECTS/PLANNERS CHICAGO, ILLINOIS	USER NAME : *USER* DESIGNED - CCE DRAWN - CCE CHECKED - TCU DATE - 06/04/10	REVISED - REVISED - REVISED - REVISED -	STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION I-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR.	FRAMING PLAN WB I-70 1 OF 3	F.A.P. RTEL. 998 SECTION 82-2-1HVB COUNTY ST. CLAIR TOTAL SHEETS 285 SHEET NO. 161 SN 082-0318 (EB) & 0319 (WB) CONTRACT NO. 76C44 FED. ROAD DIST. NO. ILLINOIS FED. AID PROJECT
	PLOT SCALE : *SCALE* PLOT DATE : *DATE*	SHEET NO. S-51 OF S-111 STA. 134+22.00 TO STA.	SCALE:	STA. 134+22.00 TO STA.	CONTRACT NO. 76C44



**FRAMING PLAN  
WB I-70 SN 082-0319**

**FLARED GIRDERS 1W-5W RADII**

Girder	PC Sta. € I-70	PC Offset € I-70	Radius Segment 1	Radius Segment 3	Radius Segment 4
1W	134+18.33	-40.73	1991'-8 1/2"	1748'-9 13/16"	2003'-10 3/4"
2W	134+03.29	-33.10	1984'-7 1/2"	1790'-3 3/4"	1994'-4 1/2"
3W	133+88.14	-25.59	1977'-6 1/2"	1831'-9 11/16"	1984'-10 1/4"
4W	133+72.87	-18.20	1970'-5 1/2"	1873'-3 5/8"	1975'-4"
5W	133+57.49	-10.94	1963'-4 1/2"	1914'-9 9/16"	1965'-9 3/4"

\* Dimensions measured along centerline Girder 6W

**NOTE:**  
Work this sheet with Sheets S-51 and S-53.

FILE NAME: \\S:\944\CONV\PL\1\1\TRANS\07\2828-2868\08A\STRUCT\CAOV\01\DESIGN\WB20319\WB20319-CONV-RF-082-SHT-FP.DWG  
 6-03-2010 10:46:01  
 USER: BONDHOUJO  
 PROJECT: SN 082-0319 (WB) & 0319 (WB)  
 SHEET: 285 OF 285  
 CONTRACT NO. 76C44



DESIGNED - CCE	REVISED -
DRAWN - CCE	REVISED -
CHECKED - TCU	REVISED -
DATE - 06/04/10	REVISED -

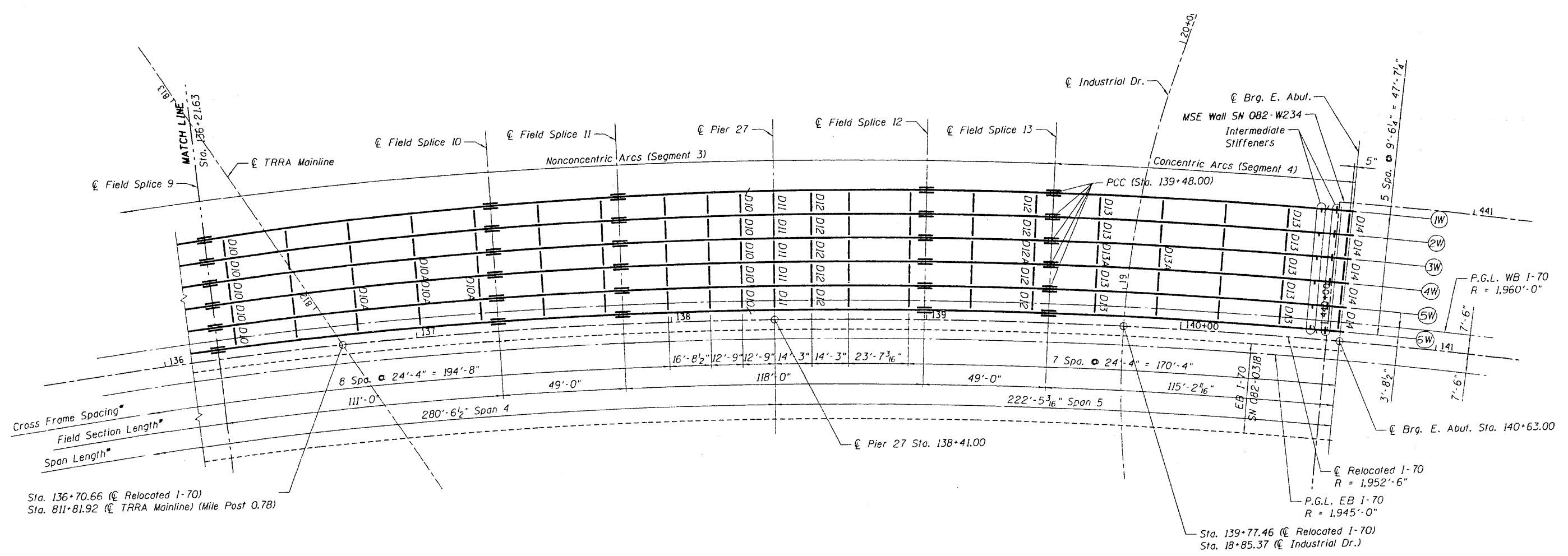
**STATE OF ILLINOIS**  
**DEPARTMENT OF TRANSPORTATION**  
 I-70 CONNECTION OVER  
 NS, TRRA, MCT AND INDUSTRIAL DR.

**FRAMING PLAN WB I-70**  
**2 OF 3**

SCALE: SHEET NO. 5-52 OF 5-111 STA. 134+22.00 TO STA.

F.A.P. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
998	82-2-IHVB	ST. CLAIR	285	162
SN 082-0318 (EB) & 0319 (WB)		CONTRACT NO. 76C44		
FED. ROAD DIST. NO.		ILLINOIS FED. AID PROJECT		

I:\Projects\082-0318\CONV-99-081-FP.DWG, I:\Projects\082-0318\CONV-99-081-05.DWG, I:\Projects\082-0318\CONV-99-081-06.DWG, I:\Projects\082-0318\CONV-99-081-07.DWG, I:\Projects\082-0318\CONV-99-081-08.DWG, I:\Projects\082-0318\CONV-99-081-09.DWG, I:\Projects\082-0318\CONV-99-081-10.DWG, I:\Projects\082-0318\CONV-99-081-11.DWG, I:\Projects\082-0318\CONV-99-081-12.DWG, I:\Projects\082-0318\CONV-99-081-13.DWG, I:\Projects\082-0318\CONV-99-081-14.DWG, I:\Projects\082-0318\CONV-99-081-15.DWG, I:\Projects\082-0318\CONV-99-081-16.DWG, I:\Projects\082-0318\CONV-99-081-17.DWG, I:\Projects\082-0318\CONV-99-081-18.DWG, I:\Projects\082-0318\CONV-99-081-19.DWG, I:\Projects\082-0318\CONV-99-081-20.DWG, I:\Projects\082-0318\CONV-99-081-21.DWG, I:\Projects\082-0318\CONV-99-081-22.DWG, I:\Projects\082-0318\CONV-99-081-23.DWG, I:\Projects\082-0318\CONV-99-081-24.DWG, I:\Projects\082-0318\CONV-99-081-25.DWG, I:\Projects\082-0318\CONV-99-081-26.DWG, I:\Projects\082-0318\CONV-99-081-27.DWG, I:\Projects\082-0318\CONV-99-081-28.DWG, I:\Projects\082-0318\CONV-99-081-29.DWG, I:\Projects\082-0318\CONV-99-081-30.DWG, I:\Projects\082-0318\CONV-99-081-31.DWG, I:\Projects\082-0318\CONV-99-081-32.DWG, I:\Projects\082-0318\CONV-99-081-33.DWG, I:\Projects\082-0318\CONV-99-081-34.DWG, I:\Projects\082-0318\CONV-99-081-35.DWG, I:\Projects\082-0318\CONV-99-081-36.DWG, I:\Projects\082-0318\CONV-99-081-37.DWG, I:\Projects\082-0318\CONV-99-081-38.DWG, I:\Projects\082-0318\CONV-99-081-39.DWG, I:\Projects\082-0318\CONV-99-081-40.DWG, I:\Projects\082-0318\CONV-99-081-41.DWG, I:\Projects\082-0318\CONV-99-081-42.DWG, I:\Projects\082-0318\CONV-99-081-43.DWG, I:\Projects\082-0318\CONV-99-081-44.DWG, I:\Projects\082-0318\CONV-99-081-45.DWG, I:\Projects\082-0318\CONV-99-081-46.DWG, I:\Projects\082-0318\CONV-99-081-47.DWG, I:\Projects\082-0318\CONV-99-081-48.DWG, I:\Projects\082-0318\CONV-99-081-49.DWG, I:\Projects\082-0318\CONV-99-081-50.DWG, I:\Projects\082-0318\CONV-99-081-51.DWG, I:\Projects\082-0318\CONV-99-081-52.DWG, I:\Projects\082-0318\CONV-99-081-53.DWG, I:\Projects\082-0318\CONV-99-081-54.DWG, I:\Projects\082-0318\CONV-99-081-55.DWG, I:\Projects\082-0318\CONV-99-081-56.DWG, I:\Projects\082-0318\CONV-99-081-57.DWG, I:\Projects\082-0318\CONV-99-081-58.DWG, I:\Projects\082-0318\CONV-99-081-59.DWG, I:\Projects\082-0318\CONV-99-081-60.DWG, I:\Projects\082-0318\CONV-99-081-61.DWG, I:\Projects\082-0318\CONV-99-081-62.DWG, I:\Projects\082-0318\CONV-99-081-63.DWG, I:\Projects\082-0318\CONV-99-081-64.DWG, I:\Projects\082-0318\CONV-99-081-65.DWG, I:\Projects\082-0318\CONV-99-081-66.DWG, I:\Projects\082-0318\CONV-99-081-67.DWG, I:\Projects\082-0318\CONV-99-081-68.DWG, I:\Projects\082-0318\CONV-99-081-69.DWG, I:\Projects\082-0318\CONV-99-081-70.DWG, I:\Projects\082-0318\CONV-99-081-71.DWG, I:\Projects\082-0318\CONV-99-081-72.DWG, I:\Projects\082-0318\CONV-99-081-73.DWG, I:\Projects\082-0318\CONV-99-081-74.DWG, I:\Projects\082-0318\CONV-99-081-75.DWG, I:\Projects\082-0318\CONV-99-081-76.DWG, I:\Projects\082-0318\CONV-99-081-77.DWG, I:\Projects\082-0318\CONV-99-081-78.DWG, I:\Projects\082-0318\CONV-99-081-79.DWG, I:\Projects\082-0318\CONV-99-081-80.DWG, I:\Projects\082-0318\CONV-99-081-81.DWG, I:\Projects\082-0318\CONV-99-081-82.DWG, I:\Projects\082-0318\CONV-99-081-83.DWG, I:\Projects\082-0318\CONV-99-081-84.DWG, I:\Projects\082-0318\CONV-99-081-85.DWG, I:\Projects\082-0318\CONV-99-081-86.DWG, I:\Projects\082-0318\CONV-99-081-87.DWG, I:\Projects\082-0318\CONV-99-081-88.DWG, I:\Projects\082-0318\CONV-99-081-89.DWG, I:\Projects\082-0318\CONV-99-081-90.DWG, I:\Projects\082-0318\CONV-99-081-91.DWG, I:\Projects\082-0318\CONV-99-081-92.DWG, I:\Projects\082-0318\CONV-99-081-93.DWG, I:\Projects\082-0318\CONV-99-081-94.DWG, I:\Projects\082-0318\CONV-99-081-95.DWG, I:\Projects\082-0318\CONV-99-081-96.DWG, I:\Projects\082-0318\CONV-99-081-97.DWG, I:\Projects\082-0318\CONV-99-081-98.DWG, I:\Projects\082-0318\CONV-99-081-99.DWG, I:\Projects\082-0318\CONV-99-081-100.DWG



**FRAMING PLAN**  
**WB I-70 SN 082-0318**

\* Dimensions measured along centerline Girder 6W

NOTE:  
Work this sheet with Sheets S-51 and S-52.

FILE NAME * USER NAME * #USER*		DESIGNED - CCE DRAWN - CCE	REVISED - REVISED -	STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION I-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR.	FRAMING PLAN WB I-70 3 OF 3	F.A.P. RTE. 99B SECTION 82-2-1HVB COUNTY ST. CLAIR TOTAL SHEETS 285 SHEET NO. 163
#FILE#	PLOT SCALE = #SCALE* PLOT DATE = #DATE*	CHECKED - TCU DATE - 06/04/10	REVISED - REVISED -			















		0.4 Span 1	Pier 24	0.5 Span 2	Pier 25	0.5 Span 3	Pier 26	0.5 Span 4	Pier 27	0.6 Span 5
$I_s$	(in <sup>4</sup> )	225,958	490,545	225,958	490,545	225,958	490,545	225,958	490,545	225,958
$I_c(n)$	(in <sup>4</sup> )	463,114	514,254	463,114	514,254	463,114	514,254	463,114	514,254	463,114
$I_c(3n)$	(in <sup>4</sup> )	339,716	514,254	339,716	514,254	339,716	514,254	339,716	514,254	339,716
$S_s$	(in <sup>3</sup> )	4,589	8,490	4,589	8,490	4,589	8,490	4,589	8,490	4,589
$S_c(n)$	(in <sup>3</sup> )	6,052	9,175	6,052	9,175	6,052	9,175	6,052	9,175	6,052
$S_c(3n)$	(in <sup>3</sup> )	5,449	9,175	5,449	9,175	5,449	9,175	5,449	9,175	5,449
$S_{xt}$	(in <sup>3</sup> )	121	327	121	327	121	327	121	327	121
DC1	(k/')	1.46	1.75	1.46	1.75	1.46	1.75	1.46	1.75	1.46
MDC1	('k)	4,758	11,419	3,840	11,233	4,187	11,307	3,889	11,696	4,824
DC2	(k/')	0.21	0.21	0.21	0.21	0.21	0.21	0.21	0.21	0.21
MDC2	('k)	726	1,551	632	1,549	662	1,564	642	1,584	741
DW	(k/')	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40
MDW	('k)	1,383	2,955	1,204	2,950	1,261	2,978	1,224	3,018	1,411
$M_t \cdot I_M$	('k)	6,029	7,248	6,298	7,806	6,562	7,852	6,353	7,344	6,111
$M_u$ (Strength I) *	('k)	20,453	34,995	19,340	35,767	20,408	36,011	19,549	35,678	20,756
$M_{br}$	('k)	26	19	24	20	25	22	24	21	26
$f_s$ DC1	(ksi)	12.44	16.14	10.04	15.88	10.95	15.98	10.17	16.53	12.61
$f_s$ DC2	(ksi)	1.60	2.03	1.39	2.03	1.46	2.05	1.41	2.07	1.63
$f_s$ DW	(ksi)	3.05	3.86	2.65	3.86	2.78	3.90	2.69	3.95	3.11
$f_s$ 1.3(I+IM)	(ksi)	15.54	12.32	16.23	13.27	16.91	13.35	16.38	12.49	15.75
$f_t$	(ksi)	2.53	0.71	2.41	0.75	2.53	0.81	2.42	0.76	2.53
$f_s$ (Service II)	(ksi)	32.63	34.36	30.32	35.03	32.10	35.27	30.66	35.04	33.11
$f_s$ (Total)(Strength I) *	(ksi)	45.19	47.35	42.13	48.34	44.57	48.67	42.60	48.28	45.86
$F_{cr}$ (Service II)	(ksi)	36.39	47.54	36.39	47.54	36.39	47.54	36.39	47.54	36.39
$V_r$	(k)	40.61	58.12	45.39	59.56	48.06	60.42	48.08	60.03	46.35
$F_{cr}$	(ksi)	50.00	49.70	50.00	49.70	50.00	49.70	50.00	49.70	50.00

\* LRFD Strength I Load Combinations include an Operational Importance Factor,  $\gamma_I = 1.05$

		0.4 Span 1	Pier 24	0.5 Span 2	Pier 25	0.5 Span 3	Pier 26	0.5 Span 4	Pier 27	0.6 Span 5
$I_s$	(in <sup>4</sup> )	218,738	429,447	218,738	429,447	218,738	429,447	218,738	429,447	218,738
$I_c(n)$	(in <sup>4</sup> )	457,420	455,321	457,420	455,321	457,420	455,321	457,420	455,321	457,420
$I_c(3n)$	(in <sup>4</sup> )	336,065	455,321	336,065	455,321	336,065	455,321	336,065	455,321	336,065
$S_s$	(in <sup>3</sup> )	4,343	7,416	4,343	7,416	4,343	7,416	4,343	7,416	4,343
$S_c(n)$	(in <sup>3</sup> )	5,794	8,155	5,794	8,155	5,794	8,155	5,794	8,155	5,794
$S_c(3n)$	(in <sup>3</sup> )	5,215	8,155	5,215	8,155	5,215	8,155	5,215	8,155	5,215
$S_{xt}$	(in <sup>3</sup> )	100	240	100	240	100	240	100	240	100
DC1	(k/')	1.41	1.64	1.41	1.64	1.41	1.64	1.41	1.64	1.41
MDC1	('k)	4,327	10,430	3,648	10,299	3,938	10,368	3,736	10,645	4,441
DC2	(k/')	0.21	0.21	0.21	0.21	0.21	0.21	0.21	0.21	0.21
MDC2	('k)	678	1,466	601	1,471	625	1,484	611	1,494	692
DW	(k/')	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40
MDW	('k)	1,291	2,793	1,145	2,802	1,190	2,826	1,164	2,846	1,318
$M_t \cdot I_M$	('k)	4,736	5,685	4,949	6,098	5,146	6,126	4,994	5,752	4,798
$M_u$ (Strength I) *	('k)	17,303	30,458	16,475	31,068	17,318	31,264	16,715	30,985	17,629
$M_{br}$	('k)	21	17	21	17	21	19	21	18	22
$f_s$ DC1	(ksi)	11.96	16.88	10.08	16.67	10.88	16.78	10.32	17.23	12.27
$f_s$ DC2	(ksi)	1.56	2.16	1.38	2.16	1.44	2.18	1.41	2.20	1.59
$f_s$ DW	(ksi)	2.97	4.11	2.64	4.12	2.74	4.16	2.68	4.19	3.03
$f_s$ 1.3(I+IM)	(ksi)	12.75	10.88	13.33	11.66	13.85	11.72	13.45	11.00	12.92
$f_t$	(ksi)	2.57	0.84	2.47	0.87	2.56	0.95	2.48	0.89	2.58
$f_s$ (Service II)	(ksi)	29.24	34.02	27.43	34.62	28.91	34.84	27.85	34.61	29.82
$f_s$ (Total)(Strength I) *	(ksi)	40.44	46.83	38.03	47.70	40.06	48.00	38.62	47.64	41.23
$F_{cr}$ (Service II)	(ksi)	37.79	47.77	37.79	47.77	37.79	47.77	37.79	47.77	37.79
$V_r$	(k)	22.98	35.63	26.24	37.98	26.25	38.40	28.10	38.39	27.39
$F_{cr}$	(ksi)	50.00	49.60	50.00	49.60	50.00	49.60	50.00	49.60	50.00

\* LRFD Strength I Load Combinations include an Operational Importance Factor,  $\gamma_I = 1.05$

		0.4 Span 1	Pier 24	0.5 Span 2	Pier 25	0.5 Span 3	Pier 26	0.5 Span 4	Pier 27	0.6 Span 5
$I_s$	(in <sup>4</sup> )	211,175	398,895	211,175	398,895	211,175	398,895	211,175	398,895	211,175
$I_c(n)$	(in <sup>4</sup> )	438,834	424,785	438,834	424,785	438,834	424,785	438,834	424,785	438,834
$I_c(3n)$	(in <sup>4</sup> )	323,671	424,785	323,671	424,785	323,671	424,785	323,671	424,785	323,671
$S_s$	(in <sup>3</sup> )	4,097	6,879	4,097	6,879	4,097	6,879	4,097	6,879	4,097
$S_c(n)$	(in <sup>3</sup> )	5,487	7,613	5,487	7,613	5,487	7,613	5,487	7,613	5,487
$S_c(3n)$	(in <sup>3</sup> )	4,933	7,613	4,933	7,613	4,933	7,613	4,933	7,613	4,933
$S_{xt}$	(in <sup>3</sup> )	81	202	81	202	81	202	81	202	81
DC1	(k/')	1.40	1.61	1.40	1.61	1.40	1.61	1.40	1.61	1.40
MDC1	('k)	3,914	9,641	3,384	9,593	3,532	9,664	3,390	9,845	3,993
DC2	(k/')	0.21	0.21	0.21	0.21	0.21	0.21	0.21	0.21	0.21
MDC2	('k)	619	1,367	562	1,380	577	1,392	570	1,393	631
DW	(k/')	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40
MDW	('k)	1,179	2,603	1,071	2,629	1,099	2,651	1,085	2,653	1,202
$M_t \cdot I_M$	('k)	3,830	4,716	4,005	5,002	4,134	5,024	4,034	4,768	3,873
$M_u$ (Strength I) *	('k)	14,845	27,213	14,225	27,732	14,721	27,916	14,319	27,690	15,079
$M_{br}$	('k)	18	15	18	15	18	17	18	16	18
$f_s$ DC1	(ksi)	11.47	16.82	9.91	16.73	10.35	16.86	9.93	17.18	11.70
$f_s$ DC2	(ksi)	1.51	2.15	1.37	2.18	1.40	2.19	1.39	2.20	1.53
$f_s$ DW	(ksi)	2.87	4.10	2.60	4.14	2.67	4.18	2.64	4.18	2.92
$f_s$ 1.3(I+IM)	(ksi)	10.89	9.66	11.39	10.25	11.75	10.30	11.47	9.77	11.01
$f_t$	(ksi)	2.71	0.89	2.61	0.92	2.68	1.00	2.61	0.94	2.70
$f_s$ (Service II)	(ksi)	26.73	32.74	25.27	33.30	26.18	33.53	25.42	33.32	27.17
$f_s$ (Total)(Strength I) *	(ksi)	36.93	45.03	35.00	45.83	36.25	46.14	35.22	45.82	37.54
$F_{cr}$ (Service II)	(ksi)	39.35	47.91	39.35	47.91	39.35	47.91	39.35	47.91	39.35
$V_r$	(k)	27.24	39.97	29.71	42.41	29.66	42.78	31.58	42.42	32.63
$F_{cr}$	(ksi)	50.00	49.60	50.00	49.60	50.00	49.60	50.00	49.60	50.00

\* LRFD Strength I Load Combinations include an Operational Importance Factor,  $\gamma_I = 1.05$

		0.4 Span 1	Pier 24	0.5 Span 2	Pier 25	0.5 Span 3	Pier 26	0.5 Span 4	Pier 27	0.6 Span 5
$I_s$	(in <sup>4</sup> )	211,175	398,895	211,175	398,895	211,175	398,895	211,175	398,895	211,175
$I_c(n)$	(in <sup>4</sup> )	438,834	424,785	438,834	424,785	438,834	424,785	438,834	424,785	438,834
$I_c(3n)$	(in <sup>4</sup> )	323,671	424,785	323,671	424,785	323,671	424,785	323,671	424,785	323,671
$S_s$	(in <sup>3</sup> )	4,097	6,879	4,097	6,879	4,097	6,879	4,097	6,879	4,097
$S_c(n)$	(in <sup>3</sup> )	5,487	7,613	5,487	7,613	5,487	7,613	5,487	7,613	5,487
$S_c(3n)$	(in <sup>3</sup> )	4,933	7,613	4,933	7,613	4,933	7,613	4,933	7,613	4,933
$S_{xt}$	(in <sup>3</sup> )	81	202	81	202	81	202	81	202	81
DC1	(k/')	1.40	1.61	1.40	1.61	1.40	1.61	1.40	1.61	1.40
MDC1	('k)	3,804	9,519	3,337	9,502	3,453	9,611	3,394	9,701	3,868
DC2	(k/')	0.21	0.21	0.21	0.21	0.21	0.21	0.21	0.21	0.21
MDC2	('k)	588	1,337	548	1,353	557	1,368	556	1,360	599
DW	(k/')	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40
MDW	('k)	1,120	2,546	1,045	2,578	1,061	2,605	1,060	2,590	1,141
$M_t \cdot I_M$	('k)	3,861	4,850	4,066	5,149	4,178	5,181	4,096	4,903	3,902
$M_u$ (Strength I) *	('k)	14,623	27,170	14,217	27,769	14,612	28,034	14,381	27,607	14,828
$M_{br}$	('k)	18	15	18	15	18	17	18	16	18
$f_s$ DC1	(ksi)	11.14	16.61	9.78	16.58	10.12	16.77	9.94	16.92	11.33
$f_s$ DC2	(ksi)	1.43	2.11	1.33	2.13	1.35	2.16	1.35	2.14	1.46
$f_s$ DW	(ksi)	2.73	4.01	2.54	4.06	2.58	4.11	2.58	4.08	2.77
$f_s$ 1.3(I+IM)	(ksi)	10.98	9.94	11.56	10.55	11.88	10.62	11.65	10.05	11.09
$f_t$	(ksi)	2.65	0.88	2.61	0.92	2.65	1.00	2.61	0.94	2.65
$f_s$ (Service II)	(ksi)	26.27	32.67	25.21	33.32	25.93	33.65	25.52	33.20	26.65
$f_s$ (Total)(Strength I) *	(ksi)	36.31	44.93	34.92	45.87	35.91	46.31	35.35	45.66	36.83
$F_{cr}$ (Service II)	(ksi)	39.35	47.91	39.35	47.91	39.35	47.91	39.35	47.91</	

**GIRDER 5E MOMENT TABLE**

	0.4 Span 1	Pier 24	0.5 Span 2	Pier 25	0.5 Span 3	Pier 26	0.5 Span 4	Pier 27	0.6 Span 5
$I_s$	(in <sup>4</sup> )	211,175	398,895	211,175	398,895	211,175	398,895	211,175	398,895
$I_c(n)$	(in <sup>4</sup> )	427,725	422,655	427,725	422,655	427,725	422,655	427,725	422,655
$I_c(3n)$	(in <sup>4</sup> )	316,093	422,655	316,093	422,655	316,093	422,655	316,093	422,655
$S_s$	(in <sup>3</sup> )	4,097	6,879	4,097	6,879	4,097	6,879	4,097	6,879
$S_c(n)$	(in <sup>3</sup> )	5,442	7,550	5,442	7,550	5,442	7,550	5,442	7,550
$S_c(3n)$	(in <sup>3</sup> )	4,888	7,550	4,888	7,550	4,888	7,550	4,888	7,550
$S_{xt}$	(in <sup>3</sup> )	81	202	81	202	81	202	81	202
DC1	(k/ft)	1.44	1.64	1.44	1.64	1.44	1.64	1.44	1.64
MDC1	(k)	3,513	9,572	3,350	9,676	3,353	9,776	3,381	9,770
DC2	(k/ft)	0.21	0.21	0.21	0.21	0.21	0.21	0.21	0.21
MDC2	(k)	539	1,311	520	1,341	521	1,352	527	1,334
DW	(k/ft)	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40
MDW	(k)	1,027	2,496	990	2,555	992	2,576	1,004	2,542
$M_L \cdot IM$	(k)	4,427	5,794	4,715	6,222	4,840	6,255	4,751	5,865
$M_u$ (Strength I)*	(k)	15,070	28,861	15,303	29,916	15,540	30,157	15,440	29,356
$M_{br}$	(k)	19	16	19	17	19	18	19	17
$f_s$ DC1	(ksi)	10.29	16.70	9.81	16.88	9.82	17.05	9.90	17.04
$f_s$ DC2	(ksi)	1.32	2.08	1.28	2.13	1.28	2.15	1.29	2.12
$f_s$ DW	(ksi)	2.52	3.97	2.43	4.06	2.44	4.09	2.46	4.04
$f_s$ 1.3(L+IM)	(ksi)	12.69	11.97	13.51	12.86	13.87	12.93	13.62	12.12
$f_r$	(ksi)	2.75	0.94	2.82	0.99	2.83	1.08	2.81	1.00
$f_s$ (Service II)	(ksi)	26.82	34.72	27.04	35.93	27.41	36.22	27.28	35.32
$f_s$ (Total)(Strength I)*	(ksi)	37.15	47.82	37.49	49.52	38.01	49.92	37.83	48.65
$F_{cr}$ (Service II)	(ksi)	39.35	47.91	39.35	47.91	39.35	47.91	39.35	47.91
$V_r$	(k)	35.46	52.33	39.60	52.76	41.69	53.24	41.69	52.85
$F_{er}$	(ksi)	50.00	49.60	50.00	49.60	50.00	49.60	50.00	49.60

\* LRFD Strength I Load Combinations include an Operational Importance Factor,  $\gamma_I = 1.05$

$I_s, S_s$ : Non-composite moment of inertia and section modulus of the steel section used for computing  $f_s$  (Total-Strength I, and Service II) due to non-composite dead loads (in<sup>4</sup> and in<sup>3</sup>).

$I_c(n), S_c(n)$ : Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing  $f_s$  (Total-Strength I, and Service II) due to short-term composite live loads (in<sup>4</sup> and in<sup>3</sup>).

$I_c(3n), S_c(3n)$ : Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing  $f_s$  (Total-Strength I, and Service II) due to long-term composite (superimposed) dead loads (in<sup>4</sup> and in<sup>3</sup>).

$S_{xt}$ : Section modulus about the major axis of section to the controlling flange, tension or compression, taken as yield moment with respect to the controlling flange over the yield strength of the controlling flange (in<sup>3</sup>).

DC1: Un-factored non-composite dead load (kips/ft.).

MDC1: Un-factored moment due to non-composite dead load (kip-ft.).

DC2: Un-factored long-term composite (superimposed excluding future wearing surface) dead load (kips/ft.).

MDC2: Un-factored moment due to long-term composite (superimposed excluding future wearing surface) dead load (kip-ft.).

DW: Un-factored long-term composite (superimposed future wearing surface only) dead load (kips/ft.).

MDW: Un-factored moment due to long-term composite (superimposed future wearing surface only) dead load (kip-ft.).

$M_L \cdot IM$ : Un-factored live load moment plus dynamic load allowance (impact)(kip-ft.).

$M_u$  (Strength I): Factored design moment (kip-ft.).  
 $1.25 (M_{DC1} + M_{DC2}) + 1.5 M_{DW} + 1.75 M_L \cdot IM$

$M_{br}$ : Factored lateral bending moment for controlling flange plate (kip-ft.).

$f_r$ : Factored calculated normal stress at edge of flange for controlling flange plate due to lateral bending (kip-ft.).

$f_s$  (Service II): Sum of stresses as computed from the moments below (ksi).  
 $M_{DC1} + M_{DC2} + M_{DW} + 1.3 M_L \cdot IM$

$f_s$  (Total)(Strength I): Sum of stresses as computed from the moments below on non-compact section (ksi).  
 $1.25 (M_{DC1} + M_{DC2}) + 1.5 M_{DW} + 1.75 M_L \cdot IM$

$F_{cr}$  (Service II): Critical flange stress at Service II computed according to Article 6.10.4.2 (ksi).

$F_{er}$ : Critical flange stress computed according to Article 6.10.7 or 6.10.8 (ksi).

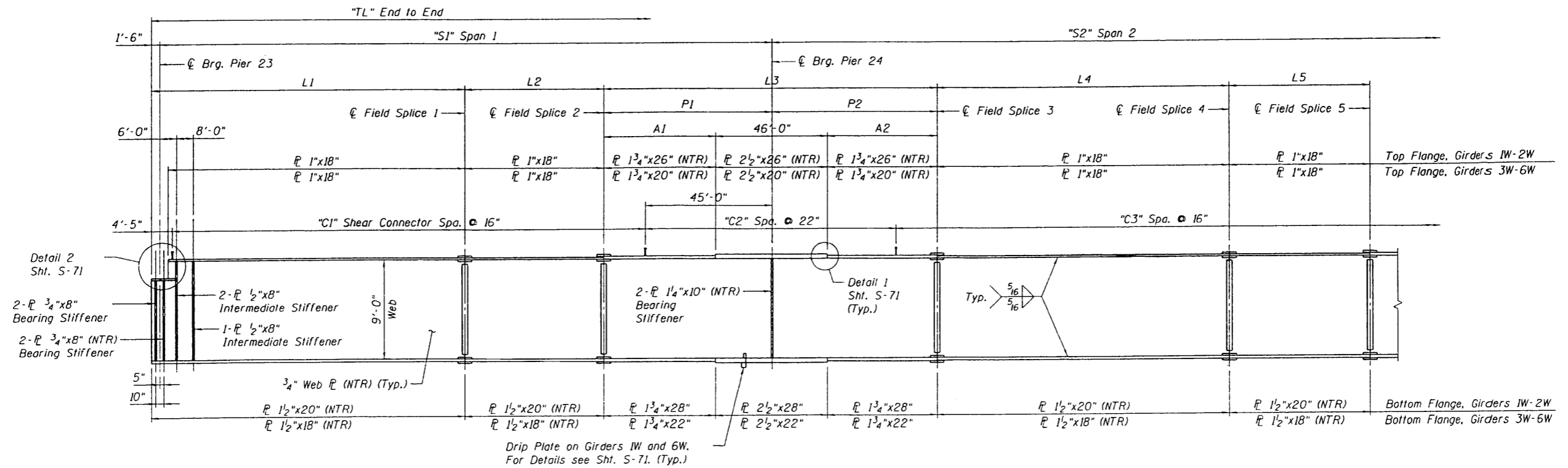
$V_r$ : Maximum factored shear range computed according to Article 6.10.10.

Note:  
 $M_L$  and  $R_L$  include the effects of centrifugal force and superelevation.

**MAXIMUM GIRDER REACTION TABLE**

	Pier 23	Pier 24	Pier 25	Pier 26	Pier 27	E. Abut.
$R_{DC1}$	(k)	123.3	436.0	435.6	437.3	441.5
$R_{DC2}$	(k)	18.5	60.6	61.0	61.4	61.2
$R_{DW}$	(k)	35.2	115.5	116.3	116.9	116.6
$R_L \cdot IM$	(k)	140.6	275.8	284.6	285.1	274.6
$R_{Total}$	(k)	317.6	887.8	897.4	900.6	894.0

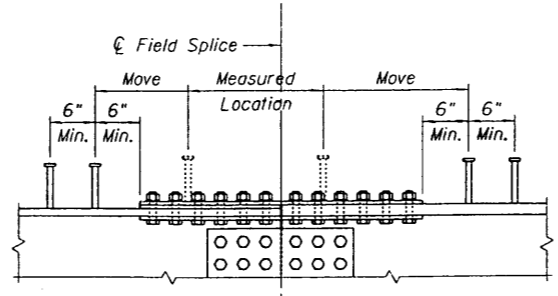
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 BONDPLD  
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 BONDPLD



GIRDERS 1W-6W ELEVATION

GIRDERS 1W-6W DIMENSIONS

Girder	Radius	TL	SI	S2	L1	L2	L3	L4	L5	P1	P2	A1	A2	C1	C2	C3
1W	(See Plan Sht. S-52)	1311'-10 <sup>3</sup> / <sub>16</sub> "	224'-4 <sup>5</sup> / <sub>16</sub> "	283'-7"	115'-6 <sup>5</sup> / <sub>8</sub> "	49'-10 <sup>5</sup> / <sub>8</sub> "	120'-1 <sup>5</sup> / <sub>8</sub> "	110'-11 <sup>1</sup> / <sub>16</sub> "	49'-10 <sup>5</sup> / <sub>8</sub> "	60'-5"	59'-8 <sup>5</sup> / <sub>8</sub> "	37'-5"	36'-8 <sup>5</sup> / <sub>8</sub> "	133	50	146
2W		1306'-7"	223'-6 <sup>1</sup> / <sub>16</sub> "	282'-6 <sup>7</sup> / <sub>8</sub> "	115'-1 <sup>3</sup> / <sub>4</sub> "	49'-8 <sup>1</sup> / <sub>2</sub> "	119'-8 <sup>1</sup> / <sub>2</sub> "	110'-6 <sup>15</sup> / <sub>16</sub> "	49'-8 <sup>1</sup> / <sub>2</sub> "	60'-2 <sup>7</sup> / <sub>16</sub> "	59'-6 <sup>1</sup> / <sub>8</sub> "	37'-2 <sup>7</sup> / <sub>16</sub> "	36'-6 <sup>1</sup> / <sub>8</sub> "	132	50	145
3W		1301'-3 <sup>7</sup> / <sub>16</sub> "	222'-9 <sup>1</sup> / <sub>16</sub> "	281'-6 <sup>13</sup> / <sub>16</sub> "	114'-8 <sup>13</sup> / <sub>16</sub> "	49'-6 <sup>3</sup> / <sub>8</sub> "	119'-3 <sup>3</sup> / <sub>8</sub> "	110'-2 <sup>3</sup> / <sub>16</sub> "	49'-6 <sup>3</sup> / <sub>8</sub> "	59'-11 <sup>13</sup> / <sub>16</sub> "	59'-3 <sup>9</sup> / <sub>16</sub> "	36'-11 <sup>13</sup> / <sub>16</sub> "	36'-3 <sup>9</sup> / <sub>16</sub> "	132	50	144
4W		1295'-11 <sup>15</sup> / <sub>16</sub> "	221'-11 <sup>3</sup> / <sub>8</sub> "	280'-6 <sup>1</sup> / <sub>16</sub> "	114'-3 <sup>7</sup> / <sub>8</sub> "	49'-4 <sup>1</sup> / <sub>4</sub> "	118'-10 <sup>1</sup> / <sub>4</sub> "	109'-2 <sup>3</sup> / <sub>16</sub> "	49'-4 <sup>1</sup> / <sub>4</sub> "	59'-9 <sup>1</sup> / <sub>4</sub> "	59'-1"	36'-9 <sup>1</sup> / <sub>4</sub> "	36'-1"	131	50	143
5W		1290'-8 <sup>8</sup> / <sub>16</sub> "	221'-1 <sup>3</sup> / <sub>4</sub> "	279'-6 <sup>9</sup> / <sub>16</sub> "	113'-11"	49'-2 <sup>8</sup> / <sub>16</sub> "	118'-5 <sup>1</sup> / <sub>8</sub> "	109'-4 <sup>3</sup> / <sub>4</sub> "	49'-2 <sup>8</sup> / <sub>16</sub> "	59'-6 <sup>11</sup> / <sub>16</sub> "	58'-10 <sup>7</sup> / <sub>16</sub> "	36'-6 <sup>1</sup> / <sub>16</sub> "	35'-10 <sup>7</sup> / <sub>16</sub> "	130	50	143
6W		1956'-3 <sup>1</sup> / <sub>2</sub> "	1285'-4 <sup>7</sup> / <sub>8</sub> "	220'-4 <sup>1</sup> / <sub>8</sub> "	278'-6 <sup>1</sup> / <sub>2</sub> "	113'-6 <sup>1</sup> / <sub>16</sub> "	49'-0"	118'-0"	109'-0"	49'-0"	59'-4 <sup>1</sup> / <sub>8</sub> "	58'-7 <sup>7</sup> / <sub>8</sub> "	36'-4 <sup>1</sup> / <sub>8</sub> "	35'-7 <sup>7</sup> / <sub>8</sub> "	130	50



SHEAR CONNECTOR DETAIL AT SPLICES AND FLANGE TRANSITIONS

DO NOT place shear connectors on splice plates.  
Move row of studs to 6" beyond nearest edge of splice plate from measured location.

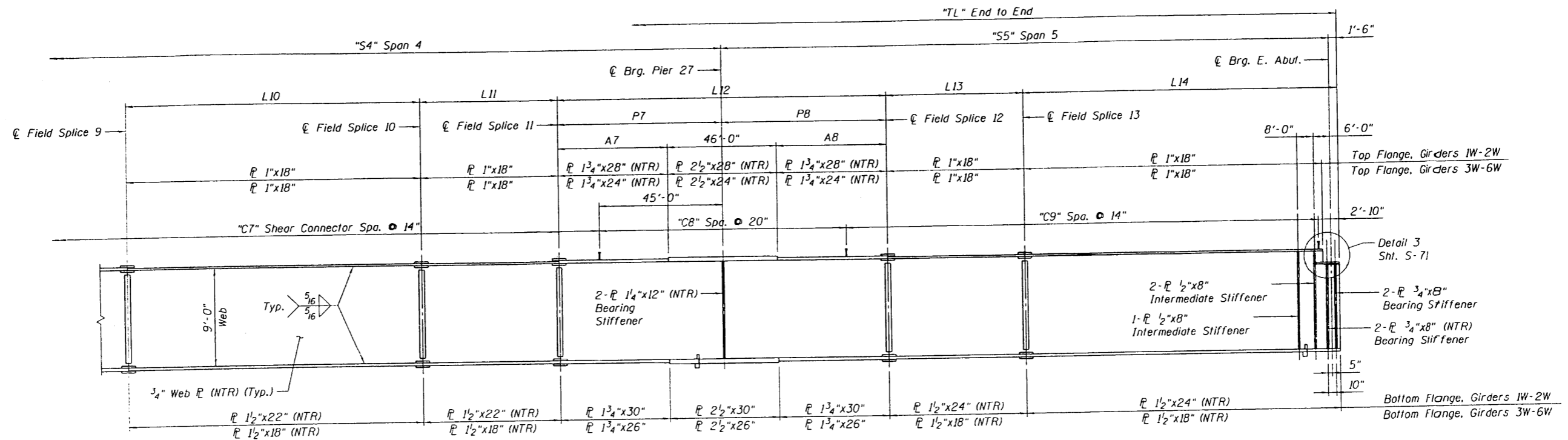
NOTES:

- Work this sheet with Sheets S-62 and S-63.
- Fasteners shall be AASHTO M164 Type 1, mechanically galvanized bolts in painted areas and M164 Type 3 in unpainted areas. Bolts 7/8 in. dia., holes 15/16 in. dia. unless otherwise noted.
- All structural steel shall be AASHTO M 270 Grade 50W except expansion joints which shall be AASHTO M 270 Grade 50.
- Load carrying components designated "NTR" shall conform to the Supplemental Requirements for Notch Toughness, Zone 2.
- Structural steel shall only be painted for a distance of 10 ft. each way from the deck joints and interior supports. All structural steel shall be cleaned as specified in the Special Provision for "Surface Preparation and Painting Requirements for Weathering Steel".
- Single-sided intermediate transverse stiffeners are to be placed on the south face of the web of Girders 1W through 5W and on the north face of the web of Girder 6W. See Framing Plan Sht. S-51.

FILE NAME: ...  
 USER NAME: ...  
 DESIGNED: ...  
 DRAWN: ...  
 CHECKED: ...  
 DATE: ...  
 TENG & ASSOCIATES, INC.  
 CHICAGO, ILLINOIS

STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION I-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR.	GIRDER ELEVATIONS WB I-70 1 OF 3	F.A.P. RTE. 998	SECTION B2-2-14WB	COUNTY ST. CLAIR	TOTAL SHEETS 285	SHEET NO. 171	CONTRACT NO. T6C44
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GIRDERS 1W-6W ELEVATION

GIRDERS 1W-6W DIMENSIONS

Girder	S4	S5	L10	L11	L12	L13	L14	P7	P8	A7	A8	C7	C8	C9
1W	287'-0 <sup>5</sup> / <sub>8</sub> "	227'-10 <sup>1</sup> / <sub>16</sub> "	113'-6 <sup>3</sup> / <sub>4</sub> "	50'-1 <sup>15</sup> / <sub>16</sub> "	120'-10 <sup>1</sup> / <sub>8</sub> "	50'-2 <sup>5</sup> / <sub>16</sub> "	119'-6 <sup>5</sup> / <sub>16</sub> "	61'-2 <sup>3</sup> / <sub>4</sub> "	59'-7 <sup>7</sup> / <sub>16</sub> "	38'-2 <sup>3</sup> / <sub>4</sub> "	36'-7 <sup>7</sup> / <sub>16</sub> "	169	54	156
2W	285'-9"	226'-9 <sup>9</sup> / <sub>16</sub> "	113'-0 <sup>9</sup> / <sub>16</sub> "	49'-11 <sup>7</sup> / <sub>8</sub> "	120'-3 <sup>5</sup> / <sub>16</sub> "	49'-11 <sup>7</sup> / <sub>16</sub> "	118'-11 <sup>5</sup> / <sub>8</sub> "	60'-11 <sup>5</sup> / <sub>16</sub> "	59'-4"	37'-11 <sup>5</sup> / <sub>16</sub> "	36'-4"	168	54	155
3W	284'-5 <sup>3</sup> / <sub>8</sub> "	225'-8 <sup>1</sup> / <sub>8</sub> "	112'-6 <sup>7</sup> / <sub>16</sub> "	49'-8 <sup>3</sup> / <sub>8</sub> "	119'-8 <sup>1</sup> / <sub>2</sub> "	49'-8 <sup>9</sup> / <sub>16</sub> "	118'-4 <sup>7</sup> / <sub>8</sub> "	60'-7 <sup>13</sup> / <sub>16</sub> "	59'-0 <sup>5</sup> / <sub>8</sub> "	37'-7 <sup>13</sup> / <sub>16</sub> "	36'-0 <sup>5</sup> / <sub>8</sub> "	167	54	154
4W	283'-1 <sup>3</sup> / <sub>4</sub> "	224'-7 <sup>7</sup> / <sub>8</sub> "	112'-0 <sup>5</sup> / <sub>16</sub> "	49'-5 <sup>9</sup> / <sub>16</sub> "	119'-1 <sup>1</sup> / <sub>16</sub> "	49'-5 <sup>3</sup> / <sub>4</sub> "	117'-10 <sup>1</sup> / <sub>8</sub> "	60'-4 <sup>3</sup> / <sub>8</sub> "	58'-9 <sup>1</sup> / <sub>4</sub> "	37'-4 <sup>3</sup> / <sub>8</sub> "	35'-9 <sup>1</sup> / <sub>4</sub> "	166	54	153
5W	281'-10 <sup>1</sup> / <sub>8</sub> "	223'-6 <sup>1</sup> / <sub>8</sub> "	111'-6 <sup>1</sup> / <sub>8</sub> "	49'-2 <sup>13</sup> / <sub>16</sub> "	118'-6 <sup>13</sup> / <sub>16</sub> "	49'-2 <sup>7</sup> / <sub>8</sub> "	117'-3 <sup>7</sup> / <sub>16</sub> "	60'-0 <sup>5</sup> / <sub>16</sub> "	58'-5 <sup>7</sup> / <sub>8</sub> "	37'-0 <sup>15</sup> / <sub>16</sub> "	35'-5 <sup>7</sup> / <sub>8</sub> "	165	54	152
6W	280'-6 <sup>1</sup> / <sub>2</sub> "	222'-5 <sup>3</sup> / <sub>16</sub> "	111'-0"	49'-0"	118'-0"	49'-0"	116'-8 <sup>1</sup> / <sub>16</sub> "	59'-9 <sup>1</sup> / <sub>2</sub> "	58'-2 <sup>1</sup> / <sub>2</sub> "	36'-9 <sup>1</sup> / <sub>2</sub> "	35'-2 <sup>1</sup> / <sub>2</sub> "	164	54	151

NOTE:

Work this sheet with Sheets S-61 and S-62.

FILE NAME: \\P022013\CONV-99-001-001001...  
 USER: CCE  
 DATE: 06/04/10  
 SCALE: 1/8"=1'-0"  
 SHEET NO. 5-63 OF 5-111  
 STA. 134+22.00 TO STA. 134+22.00



DESIGNED -	REVISIONS
DRAWN - CCE	REVISIONS
CHECKED - TCU	REVISIONS
DATE - 06/04/10	REVISIONS

STATE OF ILLINOIS  
 DEPARTMENT OF TRANSPORTATION  
 I-70 CONNECTION OVER  
 NS, TRRA, MCT AND INDUSTRIAL DR.

GIRDER ELEVATIONS WB I-70  
 3 OF 3

F.A.P. RTE. 998	SECTION B2-2-1HVB	COUNTY ST. CLAIR	TOTAL SHEETS 285	SHEET NO. 173
SN 082-0318 (EB) & 0319 (WB)		CONTRACT NO. 76C44		





		0.4 Span 1	Pier 24	0.5 Span 2	Pier 25	0.5 Span 3	Pier 26	0.5 Span 4	Pier 27	0.6 Span 5
$I_s$	(in <sup>4</sup> )	218,738	490,545	218,738	490,545	218,738	521,091	225,958	521,091	232,857
$I_c(n)$	(in <sup>4</sup> )	426,644	516,823	426,644	516,823	427,508	549,587	460,251	551,532	481,681
$I_c(3n)$	(in <sup>4</sup> )	311,925	516,823	311,925	516,823	312,447	549,587	333,336	551,532	347,122
$S_s$	(in <sup>3</sup> )	4,343	8,490	4,343	8,490	4,343	9,028	4,589	9,028	4,834
$S_c(n)$	(in <sup>3</sup> )	5,669	9,255	5,669	9,255	5,673	9,865	6,042	9,925	6,364
$S_c(3n)$	(in <sup>3</sup> )	5,069	9,255	5,069	9,255	5,073	9,865	5,411	9,925	5,708
$S_{xt}$	(in <sup>3</sup> )	100	327	100	327	100	375	121	375	144
DC1	(k/')	1.38	1.68	1.38	1.68	1.38	1.77	1.49	1.84	1.53
MDC1	(k)	4,530	10,828	3,774	10,396	3,728	11,451	4,334	12,671	5,318
DC2	(k/')	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17
MDC2	(k)	629	1,358	534	1,325	542	1,345	528	1,348	623
DW	(k/')	0.33	0.33	0.33	0.33	0.35	0.39	0.42	0.43	0.43
MDW	(k)	1,193	2,598	1,031	2,492	1,005	2,926	1,322	3,366	1,540
$M_t \cdot I_w$	(k)	5,350	8,294	5,441	8,718	5,806	8,442	6,193	7,457	6,207
$M_u$ (Strength I)*	(k)	18,481	35,326	17,277	35,330	17,856	36,914	19,843	37,404	21,630
$M_{br}$	(k)	20	27	36	27	49	32	49	33	19
$f_s$ DC1	(ksi)	12.52	15.30	10.43	14.69	10.30	15.22	11.33	16.84	13.20
$f_s$ DC2	(ksi)	1.49	1.76	1.26	1.72	1.28	1.64	1.17	1.63	1.31
$f_s$ DW	(ksi)	2.82	3.37	2.44	3.23	2.38	3.56	2.93	4.07	3.24
$f_s$ 1.3(I+IM)	(ksi)	14.72	13.98	14.97	14.69	15.97	13.35	15.99	11.72	15.22
$f_r$	(ksi)	2.43	0.99	4.33	0.99	5.92	1.04	4.83	1.06	1.57
$f_s$ (Service II)	(ksi)	31.55	34.41	29.11	34.34	29.93	33.76	31.43	34.26	32.97
$f_s$ (Total)(Strength I)*	(ksi)	43.64	47.46	40.36	47.40	41.52	46.60	43.63	47.22	45.65
$F_{cr}$ (Service II)	(ksi)	37.79	47.54	37.79	47.54	37.79	47.44	36.39	47.44	35.12
$V_r$	(k)	42.05	53.23	41.27	53.81	42.88	57.75	46.15	58.80	46.71
$F_{cr}$	(ksi)	50.00	49.70	50.00	49.70	50.00	49.70	50.00	49.70	50.00

\* LRFD Strength I Load Combinations include an Operational Importance Factor,  $\eta_I = 1.05$

		0.4 Span 1	Pier 24	0.5 Span 2	Pier 25	0.5 Span 3	Pier 26	0.5 Span 4	Pier 27	0.6 Span 5
$I_s$	(in <sup>4</sup> )	218,738	490,545	218,738	490,545	218,738	521,091	225,958	521,091	232,857
$I_c(n)$	(in <sup>4</sup> )	425,149	516,527	425,149	516,527	427,980	551,622	474,773	555,382	500,482
$I_c(3n)$	(in <sup>4</sup> )	311,027	516,527	311,027	516,527	312,732	551,622	342,699	555,382	359,358
$S_s$	(in <sup>3</sup> )	4,343	8,490	4,343	8,490	4,343	9,028	4,589	9,028	4,834
$S_c(n)$	(in <sup>3</sup> )	5,663	9,247	5,663	9,247	5,675	9,927	6,099	10,043	6,435
$S_c(3n)$	(in <sup>3</sup> )	5,064	9,247	5,064	9,247	5,074	9,927	5,468	10,043	5,780
$S_{xt}$	(in <sup>3</sup> )	100	327	100	327	100	375	121	375	144
DC1	(k/')	1.29	1.59	1.29	1.59	1.30	1.74	1.49	1.86	1.55
MDC1	(k)	4,286	11,231	3,635	10,925	3,637	12,103	4,188	13,154	5,126
DC2	(k/')	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17
MDC2	(k)	594	1,411	512	1,393	523	1,426	523	1,417	620
DW	(k/')	0.33	0.33	0.33	0.33	0.35	0.39	0.42	0.43	0.43
MDW	(k)	1,127	2,698	986	2,623	976	3,103	1,301	3,533	1,534
$M_t \cdot I_w$	(k)	4,267	6,553	4,332	6,956	4,631	6,967	5,200	6,537	5,358
$M_u$ (Strength I)*	(k)	16,020	32,883	14,956	33,080	15,507	35,446	17,786	36,715	19,802
$M_{br}$	(k)	17	25	31	25	42	30	42	31	17
$f_s$ DC1	(ksi)	11.84	15.87	10.04	15.44	10.05	16.09	10.95	17.50	12.72
$f_s$ DC2	(ksi)	1.41	1.83	1.21	1.81	1.24	1.72	1.15	1.69	1.29
$f_s$ DW	(ksi)	2.67	3.50	2.34	3.40	2.31	3.75	2.86	4.22	3.18
$f_s$ 1.3(I+IM)	(ksi)	11.75	11.05	11.93	11.74	12.73	10.95	13.30	10.15	12.99
$f_r$	(ksi)	2.09	0.92	3.72	0.92	5.01	0.96	4.16	1.01	1.43
$f_s$ (Service II)	(ksi)	27.68	32.26	25.53	32.39	26.33	32.51	28.25	33.57	30.18
$f_s$ (Total)(Strength I)*	(ksi)	38.21	44.38	35.32	44.59	36.44	44.76	39.18	46.19	41.76
$F_{cr}$ (Service II)	(ksi)	37.79	47.54	37.79	47.54	37.79	47.44	36.39	47.44	35.12
$V_r$	(k)	27.50	40.49	29.34	41.06	30.69	41.10	27.12	37.24	29.37
$F_{cr}$	(ksi)	50.00	49.70	50.00	49.70	50.00	49.70	50.00	49.60	50.00

\* LRFD Strength I Load Combinations include an Operational Importance Factor,  $\eta_I = 1.05$

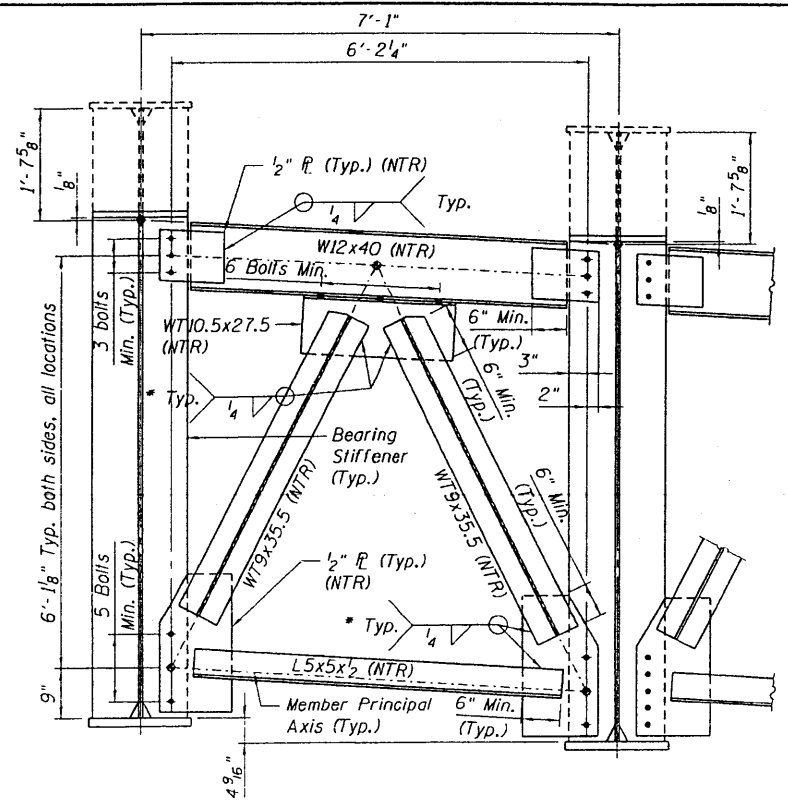
		0.4 Span 1	Pier 24	0.5 Span 2	Pier 25	0.5 Span 3	Pier 26	0.5 Span 4	Pier 27	0.6 Span 5
$I_s$	(in <sup>4</sup> )	211,175	398,895	211,175	398,895	211,175	429,447	211,175	459,997	211,175
$I_c(n)$	(in <sup>4</sup> )	408,332	424,921	408,332	424,921	412,992	460,212	438,539	494,303	445,039
$I_c(3n)$	(in <sup>4</sup> )	299,765	424,921	299,765	424,921	302,610	460,212	319,078	494,303	323,520
$S_s$	(in <sup>3</sup> )	4,097	6,879	4,097	6,879	4,097	7,416	4,097	7,953	4,097
$S_c(n)$	(in <sup>3</sup> )	5,362	7,621	5,362	7,621	5,382	8,306	5,487	8,956	5,512
$S_c(3n)$	(in <sup>3</sup> )	4,787	7,621	4,787	7,621	4,806	8,306	4,907	8,956	4,933
$S_{xt}$	(in <sup>3</sup> )	81	202	81	202	81	240	81	282	81
DC1	(k/')	1.28	1.48	1.28	1.48	1.30	1.64	1.47	1.79	1.52
MDC1	(k)	3,933	9,170	3,403	9,052	3,448	10,148	3,818	11,554	4,506
DC2	(k/')	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17
MDC2	(k)	545	1,191	479	1,190	491	1,228	474	1,266	542
DW	(k/')	0.33	0.33	0.33	0.33	0.35	0.39	0.42	0.43	0.43
MDW	(k)	1,034	2,276	919	2,245	922	2,673	1,174	3,153	1,343
$M_t \cdot I_w$	(k)	3,343	4,305	3,455	4,554	3,600	4,839	3,802	5,095	3,812
$M_u$ (Strength I)*	(k)	13,648	25,095	12,889	25,345	13,237	28,034	14,469	31,153	15,745
$M_{br}$	(k)	15	19	27	19	35	23	33	26	14
$f_s$ DC1	(ksi)	11.52	16.00	9.97	15.79	10.10	16.42	11.18	17.43	13.20
$f_s$ DC2	(ksi)	1.37	1.88	1.20	1.87	1.23	1.77	1.16	1.70	1.32
$f_s$ DW	(ksi)	2.59	3.58	2.30	3.54	2.30	3.86	2.87	4.22	3.27
$f_s$ 1.3(I+IM)	(ksi)	9.73	8.81	10.05	9.32	10.43	9.09	10.81	8.87	10.79
$f_r$	(ksi)	2.19	1.12	3.93	1.14	5.14	1.15	4.85	1.10	2.02
$f_s$ (Service II)	(ksi)	25.20	30.27	23.52	30.52	24.06	31.15	26.03	32.23	28.57
$f_s$ (Total)(Strength I)*	(ksi)	34.74	41.56	32.49	41.93	33.24	42.81	36.01	44.30	39.45
$F_{cr}$ (Service II)	(ksi)	39.35	47.91	39.35	47.91	39.35	47.77	39.35	47.65	39.35
$V_r$	(k)	23.95	31.99	24.12	32.89	24.32	34.11	31.10	44.28	34.50
$F_{cr}$	(ksi)	50.00	49.60	50.00	49.60	50.00	49.60	50.00	49.60	50.00

\* LRFD Strength I Load Combinations include an Operational Importance Factor,  $\eta_I = 1.05$

		0.4 Span 1	Pier 24	0.5 Span 2	Pier 25	0.5 Span 3	Pier 26	0.5 Span 4	Pier 27	0.6 Span 5
$I_s$	(in <sup>4</sup> )	211,175	398,895	211,175	398,895	211,175	429,447	211,175	459,997	211,175
$I_c(n)$	(in <sup>4</sup> )	408,332	424,921	408,332	424,921	414,819	460,410	438,884	494,316	445,039
$I_c(3n)$	(in <sup>4</sup> )	299,765	424,921	299,765	424,921	303,738	460,410	319,311	494,316	323,520
$S_s$	(in <sup>3</sup> )	4,097	6,879	4,097	6,879	4,097	7,416	4,097	7,953	4,097
$S_c(n)$	(in <sup>3</sup> )	5,362	7,621	5,362	7,621	5,389	8,311	5,488	8,957	5,512
$S_c(3n)$	(in <sup>3</sup> )	4,787	7,621	4,787	7,621	4,813	8,311	4,908	8,957	4,933
$S_{xt}$	(in <sup>3</sup> )	81	202	81	202	81	240	81	282	81
DC1	(k/')	1.28	1.48	1.28	1.48	1.32	1.65	1.47	1.79	1.52
MDC1	(k)	3,748	9,123	3,322	9,138	3,410	10,214	3,751	11,409	4,374
DC2	(k/')	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17	0.17
MDC2	(k)	519	1,180	467	1,192	481	1,227	467	1,249	529
DW	(k/')	0.33	0.33	0.33	0.33	0.35	0.39	0.42	0.43	0.43
MDW	(k)	986	2,253	894	2,253	912	2,672	1,150	3,104	1,313
$M_t \cdot I_w$	(k)	3,021	3,888	3,068	4,156	3,295	4,805	3,922	4,991	3,926
$M_u$ (Strength I)*	(k)	12,705	24,216	12,020	24,744	12,598	28,053	14,554	30,672	15,716
$M_{br}$	(k)	14	18	25	19	32	22	32	25	14
$f_s$ DC1	(ksi)	10.98	15.92	9.73	15.94	9.99	16.53	10.99	17.21	12.81
$f_s$ DC2	(ksi)	1.30	1.86	1.17	1.88	1.20	1.77	1.14	1.67	1.29
$f_s$ DW	(ksi)	2.47	3.55	2.24	3.55	2.27	3.86	2.81	4.16	3.19
$f_s$ 1.3(I+IM)	(ksi)	8.79	7.96	8.93	8.51	9.54	9.02	11.15	8.69	11.11
$f_r$	(ksi)	2.03	1.08	3.65	1.10	4.78	1.11	4.72	1.05	2.01
$f_s$ (Service II)	(ksi)	23.54	29.28	22.07	29.87	23.00	31.18	26.09	31.74	28.40
$f_s$ (Total)(Strength I)*	(ksi)	32.43	40.17	30.46	41.00	31.75	42.84	36.11	43.63	39.24
$F_{cr}$ (Service II)	(ksi)	39.35	47.91	39.35	47.91	39.35	47.77	39.35	47.65	39.35

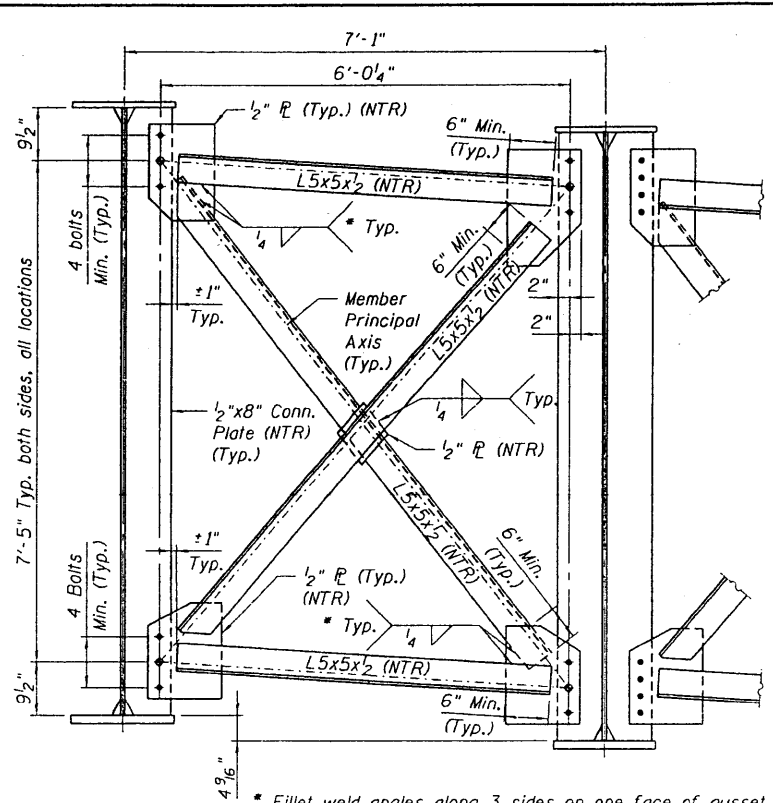






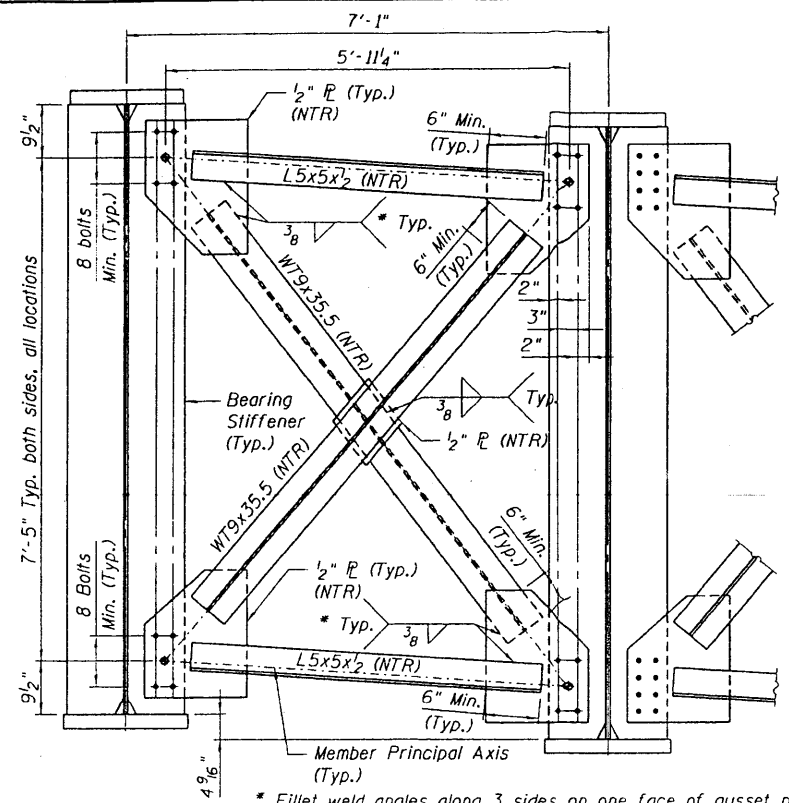
**D5 - CROSS FRAME AT PIER 23**  
(5 thus)

\* Fillet weld tees along 3 sides on one face of gusset plate.



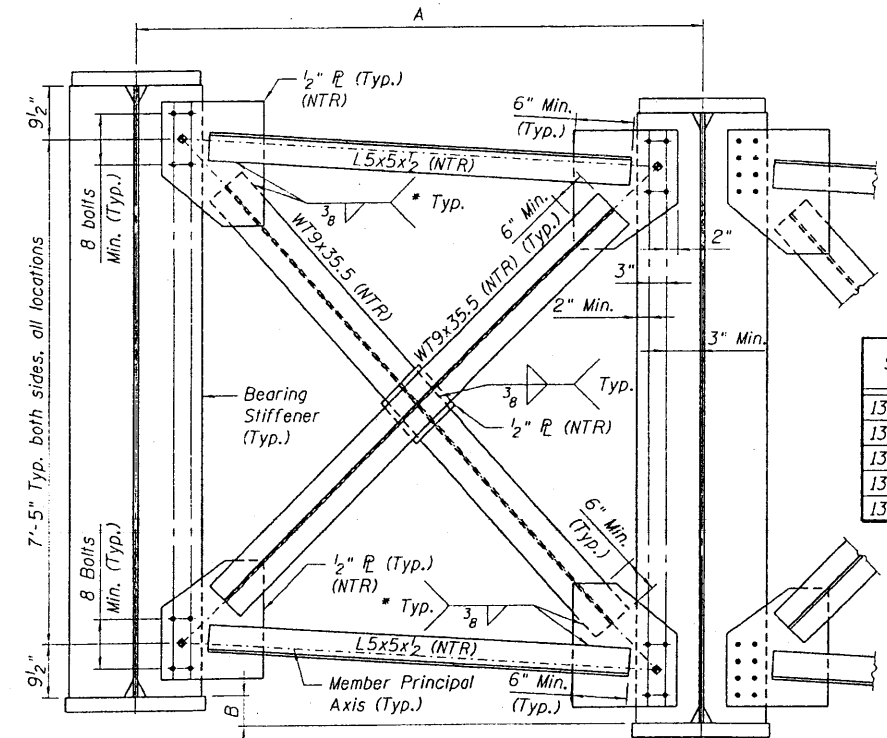
**D6 - TYPICAL INTERIOR CROSS FRAME**  
(125 thus)

\* Fillet weld angles along 3 sides on one face of gusset plate.



**D7 - CROSS FRAME AT PIERS 24 & 25**  
(10 thus)

\* Fillet weld angles along 3 sides on one face of gusset plate.

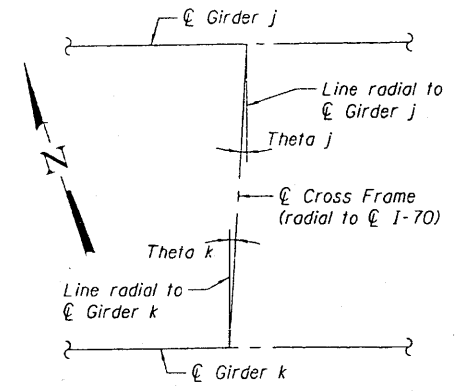


**D8 - CROSS FRAME AT PIER 26**  
(5 thus)

\* Fillet weld angles along 3 sides on one face of gusset plate.

**D8 CROSS FRAME DIMENSIONS**

Station	Bay [j-k]	A	B	Theta j [deg.]	Theta k [deg.]
135+61.00	1-2	8'-3"	5 3/8"	1.65	1.29
135+61.00	2-3	8'-3 1/16"	5 3/8"	1.29	0.94
135+61.00	3-4	8'-4 9/16"	5 7/16"	0.94	0.61
135+61.00	4-5	8'-5 5/16"	5 1/2"	0.61	0.30
135+61.00	5-6	8'-5 5/16"	5 1/2"	0.30	0.00



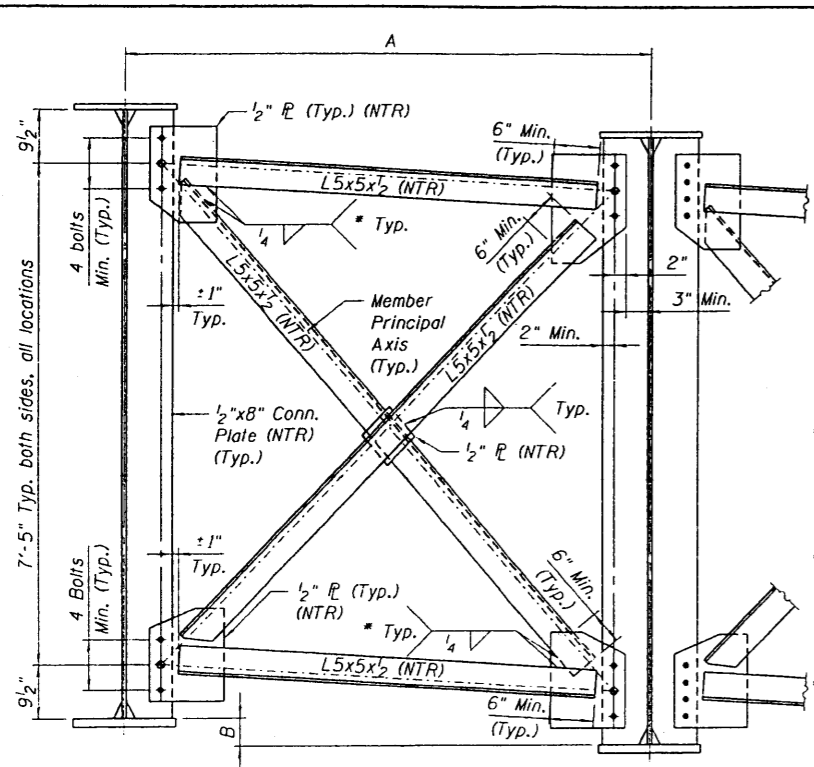
**CROSS FRAME PLAN VIEW**

Note: Cross Frame - Girder skew measured in degrees.

\* Centroid of bolt group and workpoint of member principal axes

**NOTE:**  
See Sht. S-67 for notes.

08220318-CONV-05-08 CD.DGN, \\B20318-CONV-05-08-001-00.DGN  
 08220318-CONV-05-08 BONDHUD \\S-0844-AHVAVUL.LD-TRANS.87.2282-28858-081AS STRUCT.CAD.01 DESIGN\B20318\SHEET\B20318-CONV-05-082-SHT-CDDGN



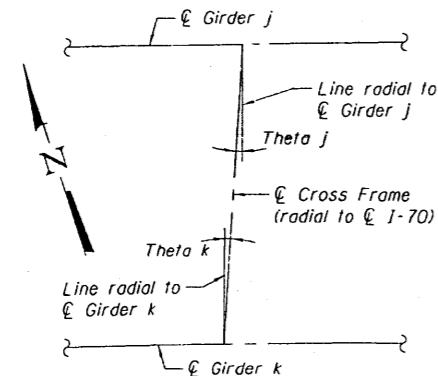
**D9 - TYPICAL INTERIOR CROSS FRAME**

(47 thus)

\*\* D9A similar to D9, except all connection plates shall have 5 bolts, min.

**D9A - TYPICAL INTERIOR CROSS FRAME**

(3 thus)



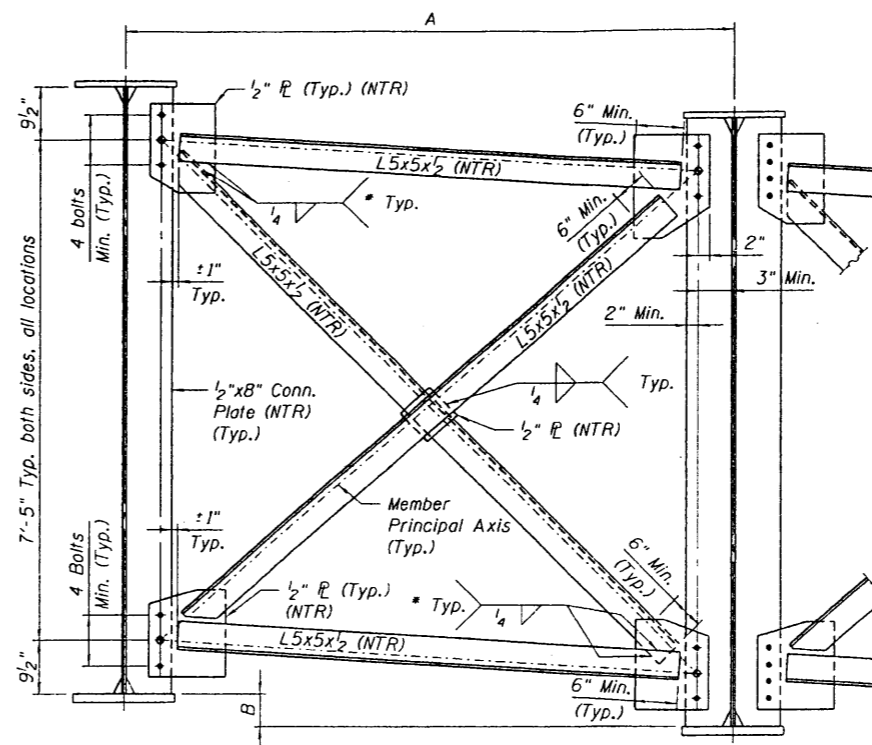
**CROSS FRAME PLAN VIEW**

Note: Cross Frame - Girder skew measured in degrees.

**D9 & D9A CROSS FRAME DIMENSIONS**

Station	Bay [j-k]	A	B	Theta j [deg.]	Theta k [deg.]
133+47.87	1-2	7'-1"	4 <sup>9</sup> / <sub>16</sub> "	0.17	0.17
133+47.87	2-3	7'-1"	4 <sup>9</sup> / <sub>16</sub> "	0.17	0.17
133+47.87	3-4	7'-1"	4 <sup>9</sup> / <sub>16</sub> "	0.17	0.17
133+47.87	4-5	7'-1"	4 <sup>9</sup> / <sub>16</sub> "	0.17	0.17
133+47.87	5-6	7'-1 <sup>1</sup> / <sub>8</sub> "	4 <sup>9</sup> / <sub>16</sub> "	0.17	0.00
133+72.24	1-2	7'-1"	4 <sup>9</sup> / <sub>16</sub> "	0.89	0.89
133+72.24	2-3	7'-1"	4 <sup>9</sup> / <sub>16</sub> "	0.89	0.89
133+72.24	3-4	7'-1"	4 <sup>9</sup> / <sub>16</sub> "	0.89	0.89
133+72.24	4-5	7'-1 <sup>1</sup> / <sub>8</sub> "	4 <sup>9</sup> / <sub>16</sub> "	0.89	0.44
133+72.24	5-6	7'-3 <sup>3</sup> / <sub>8</sub> "	4 <sup>9</sup> / <sub>16</sub> "	0.44	0.00
133+96.61	1-2	7'-1 <sup>1</sup> / <sub>8</sub> "	4 <sup>9</sup> / <sub>16</sub> "	1.60	1.60
133+96.61	2-3	7'-1 <sup>1</sup> / <sub>8</sub> "	4 <sup>9</sup> / <sub>16</sub> "	1.60	1.33
133+96.61	3-4	7'-2 <sup>3</sup> / <sub>8</sub> "	4 <sup>9</sup> / <sub>16</sub> "	1.33	0.87
133+96.61	4-5	7'-4 <sup>1</sup> / <sub>16</sub> "	4 <sup>3</sup> / <sub>4</sub> "	0.87	0.43
133+96.61	5-6	7'-5 <sup>3</sup> / <sub>8</sub> "	4 <sup>13</sup> / <sub>16</sub> "	0.43	0.00
134+20.98	1-2	7'-2 <sup>1</sup> / <sub>8</sub> "	4 <sup>5</sup> / <sub>8</sub> "	2.23	1.74
134+20.98	2-3	7'-3 <sup>3</sup> / <sub>8</sub> "	4 <sup>3</sup> / <sub>4</sub> "	1.74	1.28
134+20.98	3-4	7'-5"	4 <sup>13</sup> / <sub>16</sub> "	1.28	0.83
134+20.98	4-5	7'-6 <sup>5</sup> / <sub>16</sub> "	4 <sup>7</sup> / <sub>8</sub> "	0.83	0.41
134+20.98	5-6	7'-7 <sup>1</sup> / <sub>2</sub> "	4 <sup>15</sup> / <sub>16</sub> "	0.41	0.00
134+45.35	1-2	7'-4 <sup>3</sup> / <sub>8</sub> "	4 <sup>13</sup> / <sub>16</sub> "	2.13	1.66
134+45.35	2-3	7'-6"	4 <sup>1</sup> / <sub>8</sub> "	1.66	1.22
134+45.35	3-4	7'-7 <sup>1</sup> / <sub>4</sub> "	4 <sup>15</sup> / <sub>16</sub> "	1.22	0.79
134+45.35	4-5	7'-8 <sup>1</sup> / <sub>16</sub> "	5"	0.79	0.39
134+45.35	5-6	7'-9 <sup>5</sup> / <sub>16</sub> "	5 <sup>1</sup> / <sub>8</sub> "	0.39	0.00
134+69.72	1-2	7'-7 <sup>1</sup> / <sub>16</sub> "	4 <sup>15</sup> / <sub>16</sub> "	2.03	1.58
134+69.72	2-3	7'-8 <sup>1</sup> / <sub>4</sub> "	5"	1.58	1.16
134+69.72	3-4	7'-9 <sup>1</sup> / <sub>16</sub> "	5 <sup>1</sup> / <sub>16</sub> "	1.16	0.76
134+69.72	4-5	7'-10 <sup>1</sup> / <sub>2</sub> "	5 <sup>1</sup> / <sub>8</sub> "	0.76	0.37
134+69.72	5-6	7'-11 <sup>1</sup> / <sub>2</sub> "	5 <sup>3</sup> / <sub>16</sub> "	0.37	0.00
134+94.09	1-2	7'-9 <sup>5</sup> / <sub>16</sub> "	5 <sup>1</sup> / <sub>16</sub> "	1.93	1.50
134+94.09	2-3	7'-10 <sup>7</sup> / <sub>16</sub> "	5 <sup>1</sup> / <sub>8</sub> "	1.50	1.10
134+94.09	3-4	7'-11 <sup>1</sup> / <sub>2</sub> "	5 <sup>1</sup> / <sub>8</sub> "	1.10	0.72
134+94.09	4-5	8'-0 <sup>1</sup> / <sub>16</sub> "	5 <sup>3</sup> / <sub>16</sub> "	0.72	0.35
134+94.09	5-6	8'-1 <sup>3</sup> / <sub>8</sub> "	5 <sup>1</sup> / <sub>4</sub> "	0.35	0.00
135+18.46	1-2	7'-11 <sup>1</sup> / <sub>2</sub> "	5 <sup>3</sup> / <sub>16</sub> "	1.82	1.43
135+18.46	2-3	8'-0 <sup>1</sup> / <sub>2</sub> "	5 <sup>3</sup> / <sub>16</sub> "	1.43	1.04
135+18.46	3-4	8'-1 <sup>1</sup> / <sub>16</sub> "	5 <sup>1</sup> / <sub>4</sub> "	1.04	0.68
135+18.46	4-5	8'-2 <sup>5</sup> / <sub>16</sub> "	5 <sup>5</sup> / <sub>16</sub> "	0.68	0.33
135+18.46	5-6	8'-3 <sup>1</sup> / <sub>8</sub> "	5 <sup>3</sup> / <sub>8</sub> "	0.33	0.00
135+34.05	1-2	8'-0 <sup>13</sup> / <sub>16</sub> "	5 <sup>1</sup> / <sub>4</sub> "	1.76	1.37
135+34.05	2-3	8'-1 <sup>3</sup> / <sub>4</sub> "	5 <sup>1</sup> / <sub>4</sub> "	1.37	1.01
135+34.05	3-4	8'-2 <sup>5</sup> / <sub>8</sub> "	5 <sup>5</sup> / <sub>16</sub> "	1.01	0.66
135+34.05	4-5	8'-3 <sup>1</sup> / <sub>16</sub> "	5 <sup>3</sup> / <sub>8</sub> "	0.66	0.32
135+34.05	5-6	8'-4 <sup>3</sup> / <sub>16</sub> "	5 <sup>1</sup> / <sub>16</sub> "	0.32	0.00
135+47.53	1-2	8'-1 <sup>15</sup> / <sub>16</sub> "	5 <sup>7</sup> / <sub>16</sub> "	1.70	1.33
135+47.53	2-3	8'-2 <sup>13</sup> / <sub>16</sub> "	5 <sup>5</sup> / <sub>16</sub> "	1.33	0.98
135+47.53	3-4	8'-3 <sup>3</sup> / <sub>8</sub> "	5 <sup>3</sup> / <sub>8</sub> "	0.98	0.64
135+47.53	4-5	8'-4 <sup>3</sup> / <sub>8</sub> "	5 <sup>1</sup> / <sub>16</sub> "	0.64	0.31
135+47.53	5-6	8'-5 <sup>1</sup> / <sub>16</sub> "	5 <sup>1</sup> / <sub>16</sub> "	0.31	0.00

**D10 & D10A CROSS FRAME DIMENSIONS**



**D10 - TYPICAL INTERIOR CROSS FRAME**

(61 thus)

\*\*\* D10A similar to D10, except all connection plates shall have 5 bolts, min.

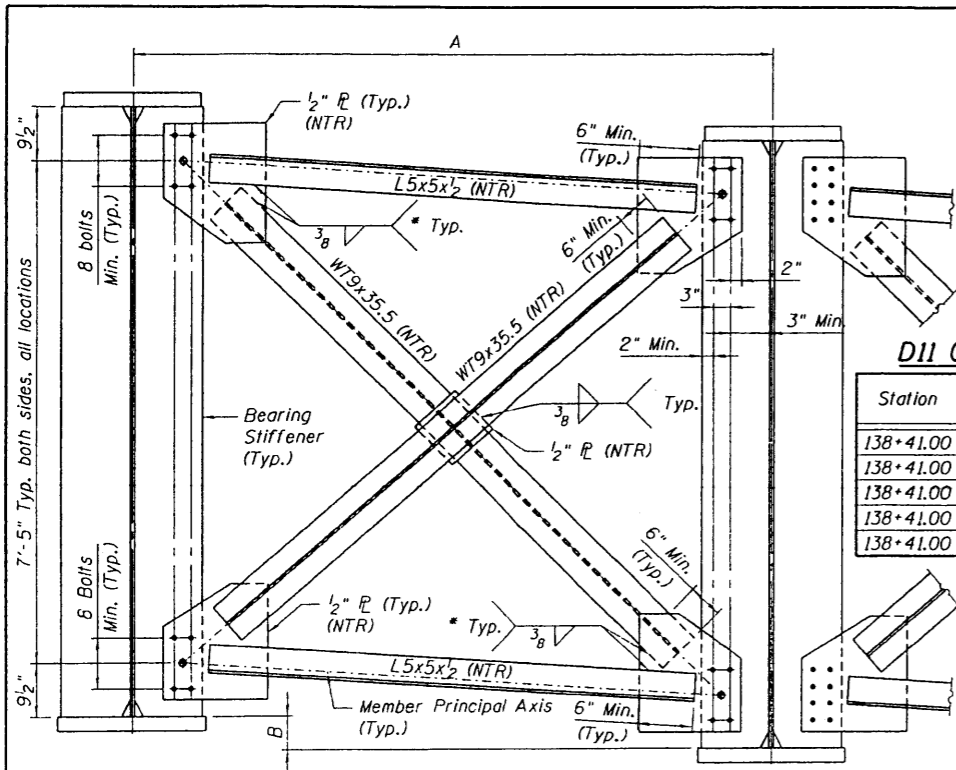
**D10A - TYPICAL INTERIOR CROSS FRAME**

(4 thus)

Station	Bay [j-k]	A	B	Theta j [deg.]	Theta k [deg.]
135+74.47	1-2	8'-4 <sup>1</sup> / <sub>16</sub> "	5 <sup>3</sup> / <sub>8</sub> "	1.59	1.24
135+74.47	2-3	8'-4 <sup>1</sup> / <sub>16</sub> "	5 <sup>1</sup> / <sub>16</sub> "	1.24	0.91
135+74.47	3-4	8'-5 <sup>1</sup> / <sub>2</sub> "	5 <sup>1</sup> / <sub>2</sub> "	0.91	0.59
135+74.47	4-5	8'-6 <sup>1</sup> / <sub>16</sub> "	5 <sup>1</sup> / <sub>2</sub> "	0.59	0.29
135+74.47	5-6	8'-6 <sup>1</sup> / <sub>16</sub> "	5 <sup>9</sup> / <sub>16</sub> "	0.29	0.00
135+87.95	1-2	8'-5 <sup>1</sup> / <sub>16</sub> "	5 <sup>1</sup> / <sub>16</sub> "	1.53	1.20
135+87.95	2-3	8'-5 <sup>3</sup> / <sub>4</sub> "	5 <sup>1</sup> / <sub>2</sub> "	1.20	0.88
135+87.95	3-4	8'-6 <sup>1</sup> / <sub>16</sub> "	5 <sup>1</sup> / <sub>2</sub> "	0.88	0.57
135+87.95	4-5	8'-7"	5 <sup>9</sup> / <sub>16</sub> "	0.57	0.28
135+87.95	5-6	8'-7 <sup>7</sup> / <sub>8</sub> "	5 <sup>5</sup> / <sub>8</sub> "	0.28	0.00
136+04.58	1-2	8'-6 <sup>1</sup> / <sub>4</sub> "	5 <sup>1</sup> / <sub>2</sub> "	1.46	1.14
136+04.58	2-3	8'-6 <sup>7</sup> / <sub>8</sub> "	5 <sup>9</sup> / <sub>16</sub> "	1.14	0.84
136+04.58	3-4	8'-7 <sup>1</sup> / <sub>2</sub> "	5 <sup>1</sup> / <sub>16</sub> "	0.84	0.55
136+04.58	4-5	8'-8 <sup>1</sup> / <sub>16</sub> "	5 <sup>5</sup> / <sub>8</sub> "	0.55	0.27
136+04.58	5-6	8'-8 <sup>1</sup> / <sub>16</sub> "	5 <sup>5</sup> / <sub>8</sub> "	0.27	0.00
136+28.87	1-2	8'-7 <sup>7</sup> / <sub>8</sub> "	5 <sup>5</sup> / <sub>8</sub> "	1.36	1.06
136+28.87	2-3	8'-8 <sup>1</sup> / <sub>16</sub> "	5 <sup>5</sup> / <sub>8</sub> "	1.06	0.78
136+28.87	3-4	8'-8 <sup>5</sup> / <sub>16</sub> "	5 <sup>1</sup> / <sub>16</sub> "	0.78	0.51
136+28.87	4-5	8'-9 <sup>1</sup> / <sub>16</sub> "	5 <sup>1</sup> / <sub>16</sub> "	0.51	0.25
136+28.87	5-6	8'-9 <sup>7</sup> / <sub>8</sub> "	5 <sup>1</sup> / <sub>16</sub> "	0.25	0.00
136+53.15	1-2	8'-9 <sup>1</sup> / <sub>8</sub> "	5 <sup>1</sup> / <sub>16</sub> "	1.26	0.98
136+53.15	2-3	8'-9 <sup>7</sup> / <sub>8</sub> "	5 <sup>1</sup> / <sub>16</sub> "	0.98	0.72
136+53.15	3-4	8'-10 <sup>3</sup> / <sub>16</sub> "	5 <sup>1</sup> / <sub>4</sub> "	0.72	0.47
136+53.15	4-5	8'-10 <sup>1</sup> / <sub>16</sub> "	5 <sup>3</sup> / <sub>4</sub> "	0.47	0.23
136+53.15	5-6	8'-11 <sup>1</sup> / <sub>8</sub> "	5 <sup>1</sup> / <sub>16</sub> "	0.23	0.00
136+77.44	1-2	8'-10 <sup>1</sup> / <sub>16</sub> "	5 <sup>3</sup> / <sub>4</sub> "	1.15	0.90
136+77.44	2-3	8'-11 <sup>1</sup> / <sub>16</sub> "	5 <sup>1</sup> / <sub>16</sub> "	0.90	0.66
136+77.44	3-4	8'-11 <sup>9</sup> / <sub>16</sub> "	5 <sup>1</sup> / <sub>16</sub> "	0.66	0.43
136+77.44	4-5	8'-11 <sup>1</sup> / <sub>4</sub> "	5 <sup>1</sup> / <sub>16</sub> "	0.43	0.21
136+77.44	5-6	9'-0 <sup>1</sup> / <sub>4</sub> "	5 <sup>7</sup> / <sub>8</sub> "	0.21	0.00
137+01.73	1-2	9'-0 <sup>1</sup> / <sub>16</sub> "	5 <sup>1</sup> / <sub>16</sub> "	1.05	0.82
137+01.73	2-3	9'-0 <sup>3</sup> / <sub>8</sub> "	5 <sup>7</sup> / <sub>8</sub> "	0.82	0.60
137+01.73	3-4	9'-0 <sup>1</sup> / <sub>16</sub> "	5 <sup>1</sup> / <sub>8</sub> "	0.60	0.39
137+01.73	4-5	9'-1"	5 <sup>7</sup> / <sub>8</sub> "	0.39	0.19
137+01.73	5-6	9'-1 <sup>1</sup> / <sub>4</sub> "	5 <sup>1</sup> / <sub>8</sub> "	0.19	0.00
137+26.01	1-2	9'-1 <sup>1</sup> / <sub>4</sub> "	5 <sup>7</sup> / <sub>8</sub> "	0.95	0.74
137+26.01	2-3	9'-1 <sup>1</sup> / <sub>2</sub> "	5 <sup>1</sup> / <sub>16</sub> "	0.74	0.54
137+26.01	3-4	9'-1 <sup>3</sup> / <sub>4</sub> "	5 <sup>5</sup> / <sub>16</sub> "	0.54	0.35
137+26.01	4-5	9'-2"	5 <sup>5</sup> / <sub>16</sub> "	0.35	0.17
137+26.01	5-6	9'-2 <sup>1</sup> / <sub>16</sub> "	5 <sup>5</sup> / <sub>16</sub> "	0.17	0.00
137+50.30	1-2	9'-2 <sup>1</sup> / <sub>4</sub> "	5 <sup>1</sup> / <sub>16</sub> "	0.84	0.66
137+50.30	2-3	9'-2 <sup>1</sup> / <sub>2</sub> "	5 <sup>5</sup> / <sub>16</sub> "	0.66	0.48
137+50.30	3-4	9'-2 <sup>1</sup> / <sub>16</sub> "	6"	0.48	0.32
137+50.30	4-5	9'-2 <sup>1</sup> / <sub>8</sub> "	6"	0.32	0.15
137+50.30	5-6	9'-3"	6"	0.15	0.00
137+74.59	1-2	9'-3 <sup>1</sup> / <sub>16</sub> "	6"	0.74	0.58
137+74.59	2-3	9'-3 <sup>5</sup> / <sub>16</sub> "	6"	0.58	0.42
137+74.59	3-4	9'-3 <sup>1</sup> / <sub>2</sub> "	6"	0.42	0.28
137+74.59	4-5	9'-3 <sup>5</sup> / <sub>8</sub> "	6"	0.28	0.14
137+74.59	5-6	9'-3 <sup>3</sup> / <sub>4</sub> "	6 <sup>1</sup> / <sub>16</sub> "	0.14	0.00
137+98.87	1-2	9'-4"	6 <sup>1</sup> / <sub>16</sub> "	0.64	0.50
137+98.87	2-3	9'-4 <sup>3</sup> / <sub>16</sub> "	6 <sup>1</sup> / <sub>16</sub> "	0.50	0.37
137+98.87	3-4	9'-4 <sup>3</sup> / <sub>16</sub> "	6 <sup>1</sup> / <sub>16</sub> "	0.37	0.24
137+98.87	4-5	9'-4 <sup>1</sup> / <sub>16</sub> "	6 <sup>1</sup> / <sub>16</sub> "	0.24	0.12
137+98.87	5-6	9'-4 <sup>7</sup> / <sub>16</sub> "	6 <sup>1</sup> / <sub>16</sub> "	0.12	0.00
138+15.55	1-2	9'-4 <sup>1</sup> / <sub>16</sub> "	6 <sup>1</sup> / <sub>16</sub> "	0.57	0.44
138+15.55	2-3	9'-4 <sup>9</sup> / <sub>16</sub> "	6 <sup>1</sup> / <sub>16</sub> "	0.44	0.32
138+15.55	3-4	9'-4 <sup>3</sup> / <sub>8</sub> "	6 <sup>1</sup> / <sub>16</sub> "	0.32	0.21
138+15.55	4-5	9'-4 <sup>3</sup> / <sub>4</sub> "	6 <sup>1</sup> / <sub>16</sub> "	0.21	0.10
138+15.55	5-6	9'-4 <sup>1</sup> / <sub>16</sub> "	6 <sup>1</sup> / <sub>16</sub> "	0.10	0.00
138+28.27	1-2	9'-4 <sup>13</sup> / <sub>16</sub> "	6 <sup>1</sup> / <sub>16</sub> "	0.51	0.40
138+28.27	2-3	9'-4 <sup>1</sup> / <sub>8</sub> "	6 <sup>1</sup> / <sub>8</sub> "	0.40	0.29
138+28.27	3-4	9'-4 <sup>15</sup> / <sub>16</sub> "	6 <sup>1</sup> / <sub>8</sub> "	0.29	0.19
138+28.27	4-5	9'-5"	6 <sup>1</sup> / <sub>8</sub> "	0.19	0.09
138+28.27	5-6	9'-5 <sup>1</sup> / <sub>16</sub> "	6 <sup>1</sup> / <sub>8</sub> "	0.09	0.00

◆ Centroid of bolt group and workpoint of member principal axes

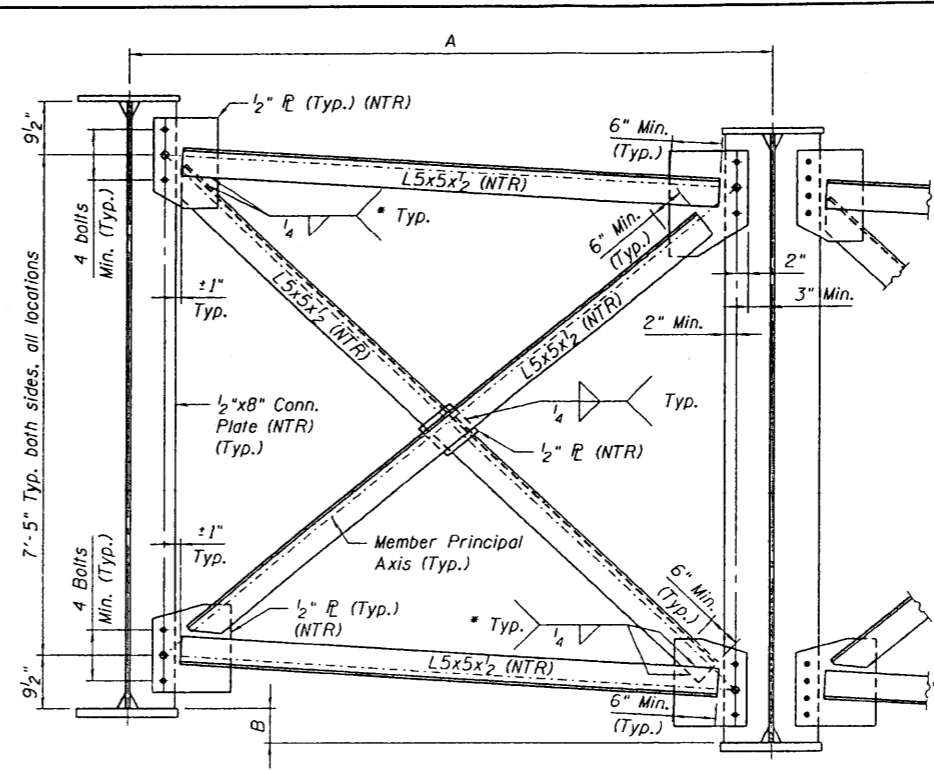
NOTE:  
See Sht. S-67 for notes.



**D11 CROSS FRAME DIMENSIONS**

Station	Bay [j-k]	A	B	Theta j [deg.]	Theta k [deg.]
138+41.00	1-2	9'-5 1/16"	6 3/8"	0.46	0.36
138+41.00	2-3	9'-5 3/8"	6 3/8"	0.36	0.26
138+41.00	3-4	9'-5 3/16"	6 3/8"	0.26	0.17
138+41.00	4-5	9'-5 1/4"	6 3/8"	0.17	0.08
138+41.00	5-6	9'-5 5/16"	6 3/8"	0.08	0.00

\* Fillet weld angles along 3 sides on one face of gusset plate.  
**D11 - CROSS FRAME AT PIER 27**  
 (5 thus)

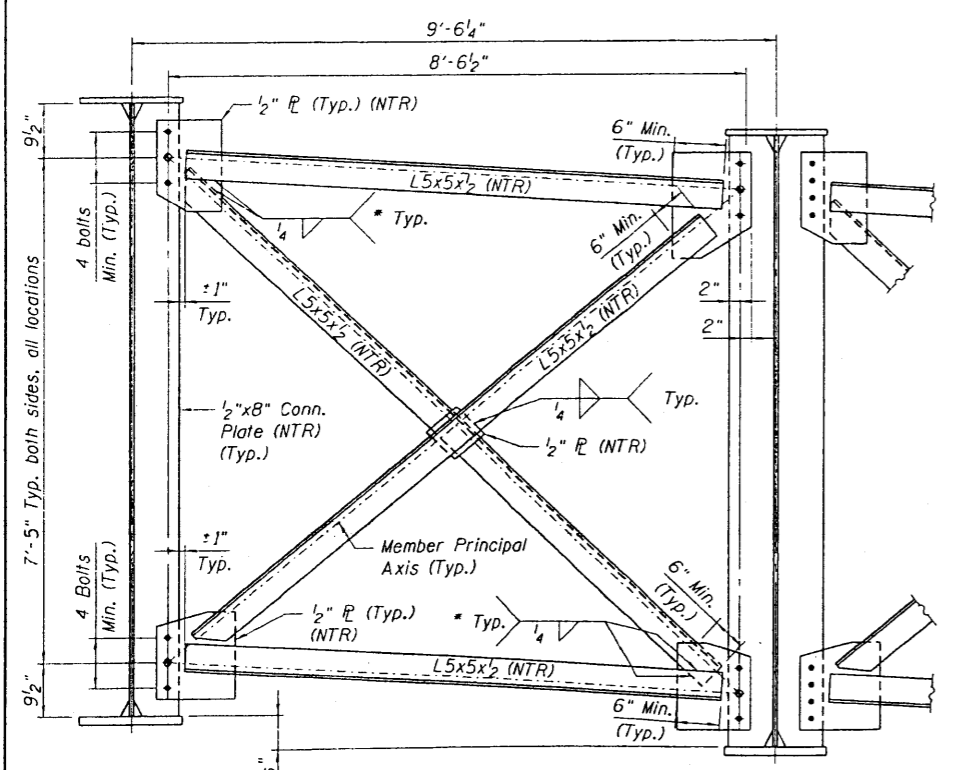


\* Fillet weld angles along 3 sides on one face of gusset plate.  
**D12 - TYPICAL INTERIOR CROSS FRAME**  
 (24 thus)

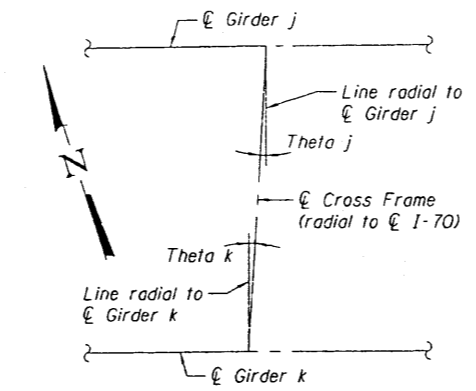
**D12 & D12A CROSS FRAME DIMENSIONS**

Station	Bay [j-k]	A	B	Theta j [deg.]	Theta k [deg.]
138+55.22	1-2	9'-5 3/8"	6 3/8"	0.40	0.31
138+55.22	2-3	9'-5 1/16"	6 3/8"	0.31	0.23
138+55.22	3-4	9'-5 7/16"	6 3/8"	0.23	0.15
138+55.22	4-5	9'-5 1/2"	6 3/8"	0.15	0.07
138+55.22	5-6	9'-5 9/16"	6 3/8"	0.07	0.00
138+69.44	1-2	9'-5 5/8"	6 3/8"	0.34	0.26
138+69.44	2-3	9'-5 5/8"	6 3/8"	0.26	0.19
138+69.44	3-4	9'-5 1/2"	6 3/8"	0.19	0.13
138+69.44	4-5	9'-5 1/16"	6 3/8"	0.13	0.06
138+69.44	5-6	9'-5 3/4"	6 3/8"	0.06	0.00
138+93.00	1-2	9'-5 15/16"	6 3/8"	0.24	0.18
138+93.00	2-3	9'-5 15/16"	6 3/8"	0.18	0.13
138+93.00	3-4	9'-6"	6 3/8"	0.13	0.09
138+93.00	4-5	9'-6"	6 3/8"	0.09	0.04
138+93.00	5-6	9'-6"	6 3/8"	0.04	0.00
139+17.28	1-2	9'-6 3/16"	6 3/16"	0.13	0.10
139+17.28	2-3	9'-6 3/16"	6 3/16"	0.10	0.08
139+17.28	3-4	9'-6 3/16"	6 3/16"	0.08	0.05
139+17.28	4-5	9'-6 3/16"	6 3/16"	0.05	0.02
139+17.28	5-6	9'-6 3/16"	6 3/16"	0.02	0.00
139+41.57	1-2	9'-6 1/4"	6 3/16"	0.03	0.02
139+41.57	2-3	9'-6 1/4"	6 3/16"	0.02	0.02
139+41.57	3-4	9'-6 1/4"	6 3/16"	0.02	0.01
139+41.57	4-5	9'-6 1/4"	6 3/16"	0.01	0.01
139+41.57	5-6	9'-6 1/4"	6 3/16"	0.01	0.00

\*\*\* D12A similar to D12, except all connection plates shall have 5 bolts, min.  
**D12A - TYPICAL INTERIOR CROSS FRAME**  
 (1 thus)

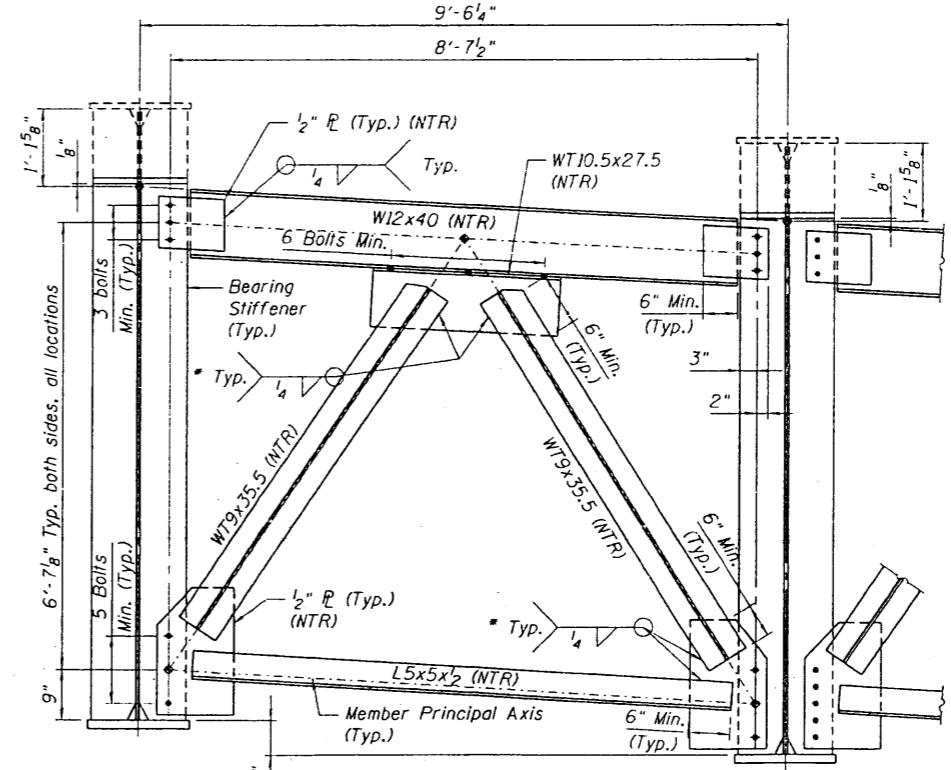


\* Fillet weld angles along 3 sides on one face of gusset plate.  
**D13 - TYPICAL INTERIOR CROSS FRAME**  
 (18 thus)



**CROSS FRAME PLAN VIEW**  
 Note: Cross Frame - Girder skew measured in degrees.

\*\* D13A similar to D13, except all connection plates shall have 5 bolts, min.  
**D13A - TYPICAL INTERIOR CROSS FRAME**  
 (2 thus)



\* Fillet weld tees along 3 sides on one face of gusset plate.  
**D14 - CROSS FRAME AT E. ABUT.**  
 (5 thus)

Centroid of bolt group and workpoint of member principal axes  
**NOTE:**  
 See Sht. S-67 for notes.

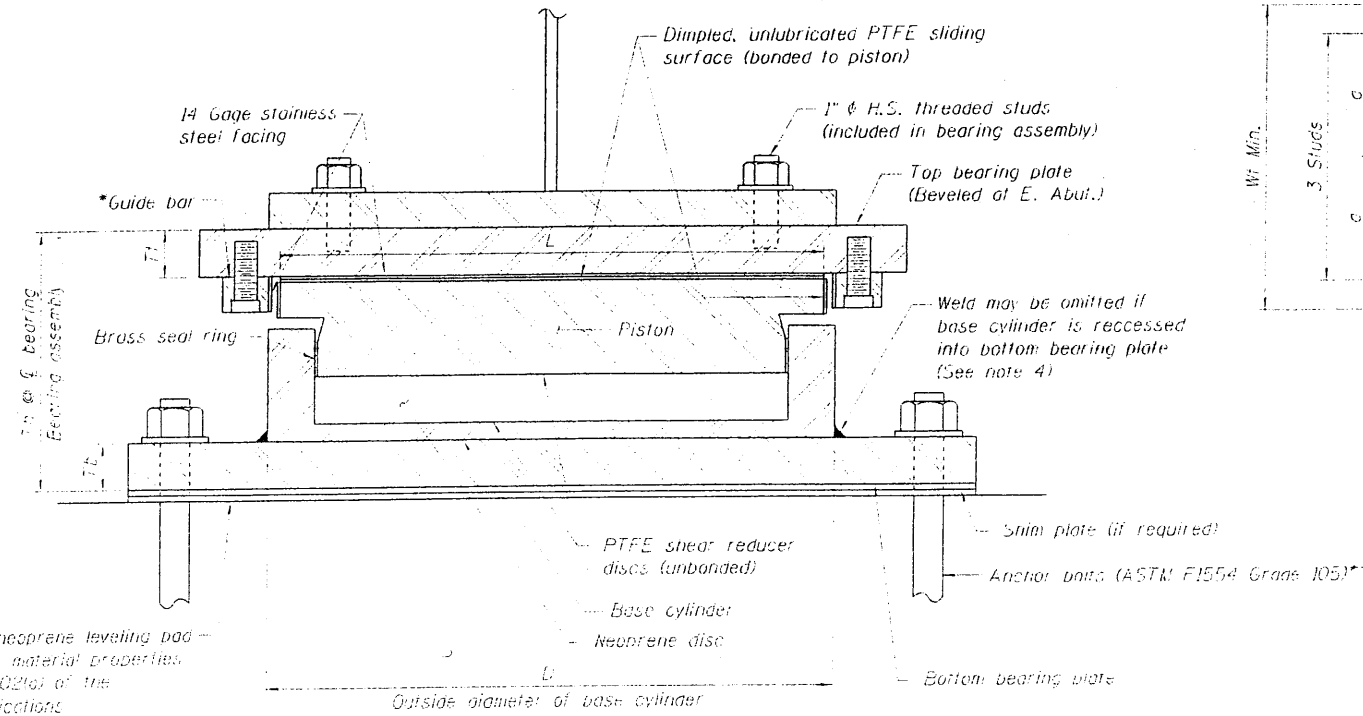
FILE NAME: ... USER NAME: \*USER\* ... DESIGNED - JLR ... DRAWN - MDB ... CHECKED - TCU ... DATE: 06/04/10 ...



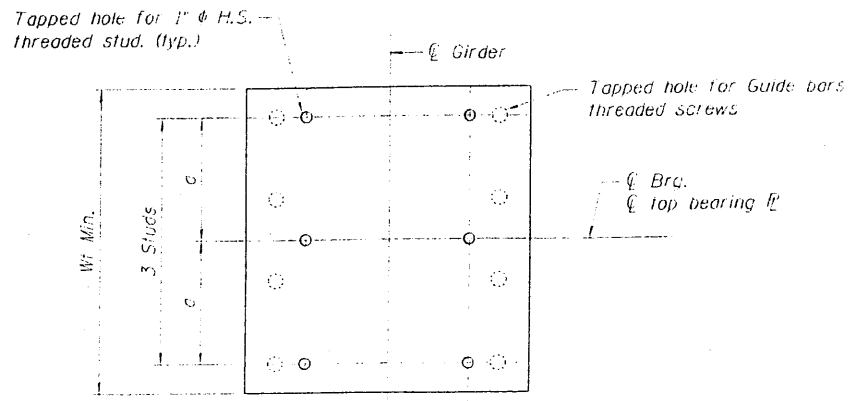




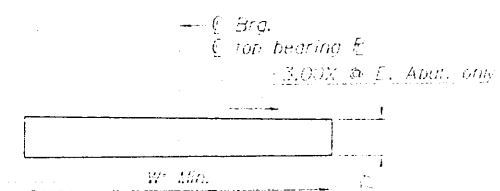
\* As alternate to the bolted connection shown, the guide bars may be connected to the top bearing plate by groove welds or the guide bars and top bearing plate may be fabricated as a single piece.



**GUIDED EXPANSION POT BEARING**  
(Pier 23 & E. Abutment)



**TOP BEARING P PLAN**



**TOP BEARING P ELEVATION**

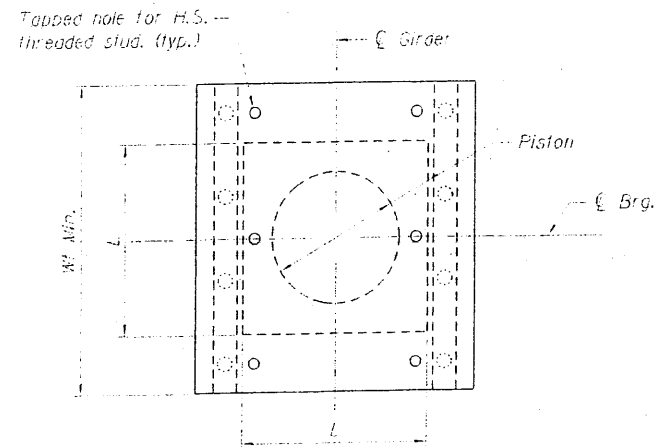
DIMENSIONS (IN)		
Dimension	Pier 23	E. Abut.
D	13 7/8	13 7/8
L	14	14
T <sub>1</sub>	2	2
T <sub>2</sub>	10 3/8	10 5/8
T <sub>3</sub>	2	2
W <sub>1</sub>	26	26
g	11	11
h	7	7
e	9	9
c	13	13

**DESIGN DATA**

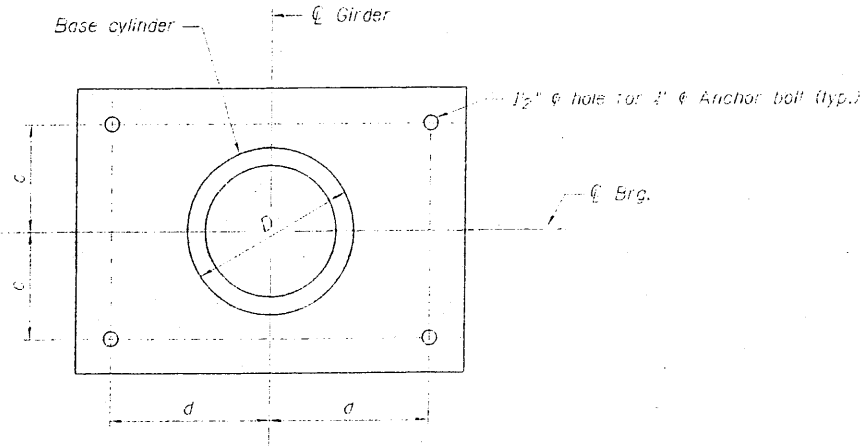
Data	Pier 23	E. Abut.
Service vertical Design Load (kips)	290	290
Factored horizontal Design Load (kips)	75	90
Factored Design Rotation (rad)	0.02	0.02
Total Required Movement (in)	2	2 1/2

**BILL OF MATERIAL**

Item	Unit	Total
High Load Multi-Rotation Bearings, Guided Expansion, 300K	Each	22
Anchor Bolts, 1" Ø	Each	88



**TOP BEARING P AND PISTON PLAN**



**BOTTOM BEARING P AND BASE CYLINDER PLAN**

**NOTES:**

- The structural steel plates of the bearing assembly shall conform to the requirements of AASHTO M 270 Grade 50W.
- Two 1/8 in. adjusting shims shall be provided for each bearing in addition to all other plates or shims and placed as shown on bearing details.
- H.S. bolts in bearing assembly shall be galvanized according to AASHTO M298 Class 50.
- If base cylinder is recessed into the bottom bearing plate, the thickness of the bottom plate shall be T<sub>3</sub> plus the depth of the recess.







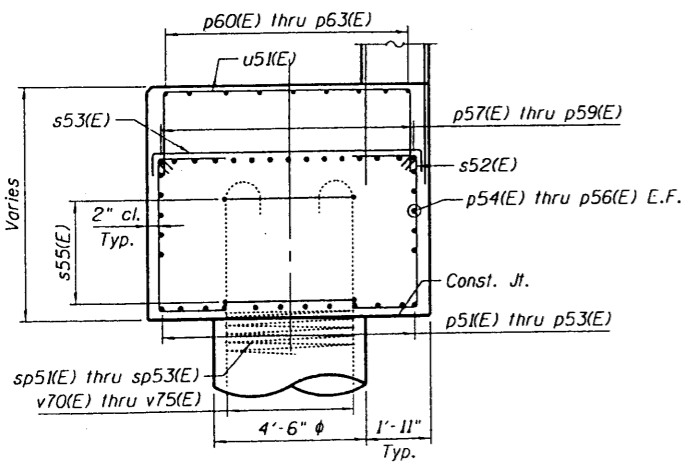


**BILL OF MATERIAL**

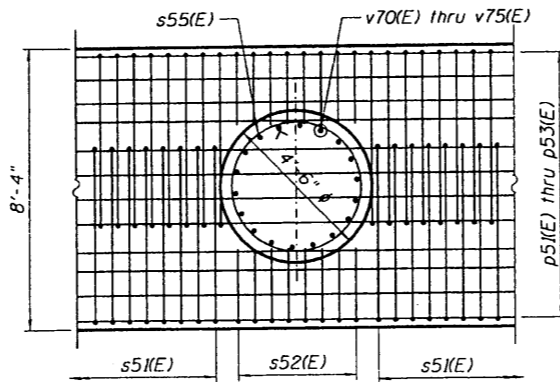
Item	Unit	Total
Concrete Structures	Cu. Yd.	331.5
Reinforcement Bars	Pound	119,150
Reinforcement Bars, Epoxy Coated	Pound	61,530
Bar Splicer	Each	97
Permanent Casing	Foot	672
Drilled Shaft in Soil	Cu. Yd.	396
Drilled Shaft in Rock	Cu. Yd.	6
Concrete Sealer	Sq. Ft.	1727
Mechanical Splicers	Each	216
Crosshole Sonic Logging	Each	1

**BAR LIST**

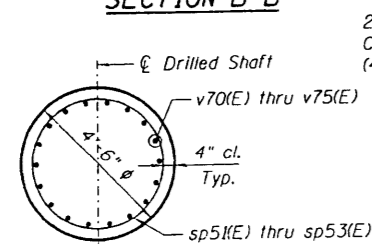
Bar	No.	Size	Length	Shape
h51(E)	10	#6	22'-10"	
h52(E)	10	#6	29'-1"	
h53(E)	58	#5	30'-0"	
h54(E)	2	#5	14'-10"	
h55(E)	2	#5	27'-5"	
h56(E)	18	#5	16'-3"	
h57(E)	11	#5	5'-10"	
h58(E)	11	#5	5'-8"	
h59(E)	22	#5	24'-3"	
n51(E)	33	#6	14'-11"	
p51(E)	12	#9	44'-10"	
p52(E)	12	#9	39'-1"	
p53(E)	12	#9	28'-1"	
p54(E)	28	#6	25'-3"	
p55(E)	28	#6	19'-8"	
p56(E)	14	#6	25'-7"	
p57(E)	16	#9	50'-6"	
p58(E)	16	#9	44'-0"	
p59(E)	16	#9	27'-9"	
60(E)	27	#5	10'-10"	
p61(E)	9	#5	7'-11"	
p62(E)	27	#5	11'-6"	
p63(E)	9	#5	7'-2"	
p64(E)	2	#5	19'-10"	
p65(E)	12	#8	25'-6"	
p66(E)	14	#6	24'-2"	
s51(E)	282	#5	20'-9"	
s52(E)	80	#5	9'-0"	
s53(E)	40	#5	9'-0"	
s54(E)	19	#5	19'-7"	
s55(E)	78	#5	13'-0"	
s56(E)	24	#5	24'-7"	
s57(E)	12	#5	23'-11"	
sp51(E)	1	#5	18'-8"	
sp52(E)	2	#5	17'-2"	
sp53(E)	3	#5	15'-8"	
sp54	6	#5	35'-0"	
sp55	6	#5	78'-11"	
u51(E)	74	#5	12'-8"	
u52(E)	4	#5	14'-11"	
v51(E)	97	#5	3'-9"	
v52(E)	128	#7	13'-2"	
v53(E)	128	#7	14'-8"	
v54(E)	97	#4	3'-2"	
v55(E)	66	#6	8'-11"	
v66(E)	25	#5	4'-10"	
v67(E)	6	#5	4'-8"	
v68(E)	25	#5	4'-11"	
v69(E)	6	#5	4'-8"	
v70(E)	9	#14	22'-11"	
v71(E)	9	#14	20'-11"	
v72(E)	18	#14	21'-5"	
v73(E)	18	#14	19'-5"	
v74(E)	27	#14	19'-11"	
v75(E)	27	#14	17'-11"	
v76	54	#14	57'-0"	
v77	162	#14	58'-11"	



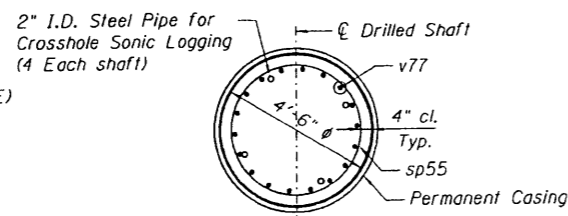
**SECTION B-B**



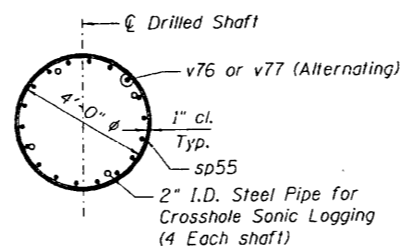
**SECTION C-C**



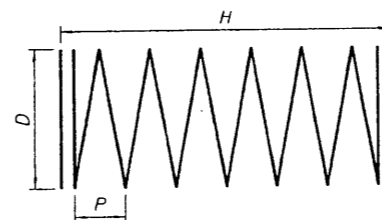
**SECTION D-D**



**SECTION E-E**

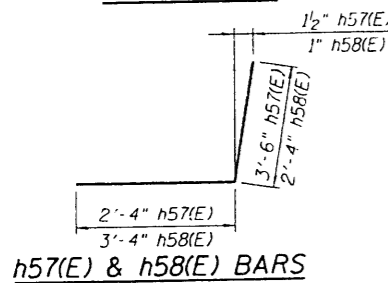


**SECTION F-F**

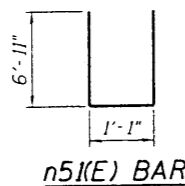


Bar	H	D	P
sp51(E)	18'-8"	3'-10"	3"
sp52(E)	17'-2"	3'-10"	3"
sp53(E)	15'-8"	3'-10"	3"
sp54	35"	3'-10"	3"
sp55	78'-11"	3'-10"	6"

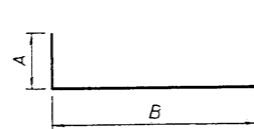
**sp1(E) thru sp5 BARS**



**h57(E) & h58(E) BARS**

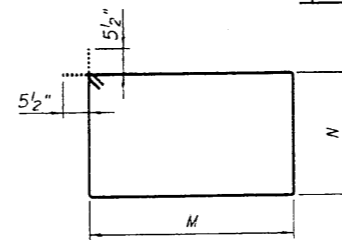


**n51(E) BAR**



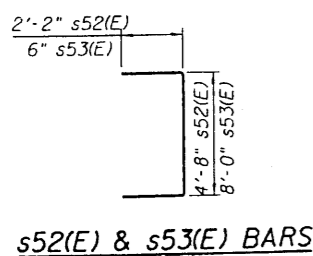
**p51(E), p52(E), p57(E) p59(E) & p65(E)**

Bar	A	B
p51(E)	1'-6"	43'-4"
p52(E)	1'-6"	37'-7"
p57(E)	1'-7"	48'-11"
p59(E)	1'-7"	26'-2"
p65(E)	1'-4"	24'-2"

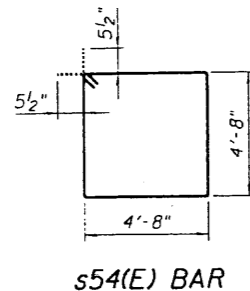


**s51(E), s56(E) & s57(E) BARS**

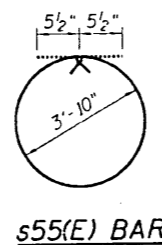
Bar	M	N
s51(E)	5'-3"	4'-8"
s56(E)	5'-3"	6'-7"
s57(E)	5'-3"	6'-3"



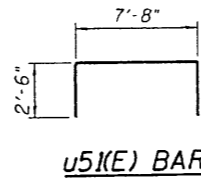
**s52(E) & s53(E) BARS**



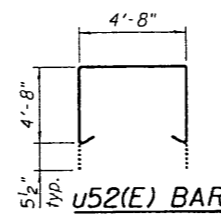
**s54(E) BAR**



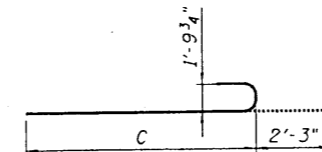
**s55(E) BAR**



**u51(E) BAR**

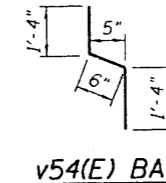


**u52(E) BAR**

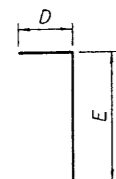


**v70(E) thru v75(E) BARS**

Bar	C
v70(E)	20'-8"
v71(E)	18'-8"
v72(E)	19'-2"
v73(E)	17'-2"
v74(E)	17'-8"
v75(E)	15'-8"

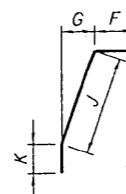


**v54(E) BAR**



**v51(E), v66(E) & v67(E) BARS**

Bar	D	E
v51(E)	1'-11"	1'-10"
v66(E)	10"	4'-0"
v67(E)	8"	4'-0"



**v68(E) & v69(E) BARS**

Bar	F	G	J	K
v68(E)	10"	3"	1'-6"	2'-7"
v69(E)	8"	1"	6"	3'-6"

**NOTES:**

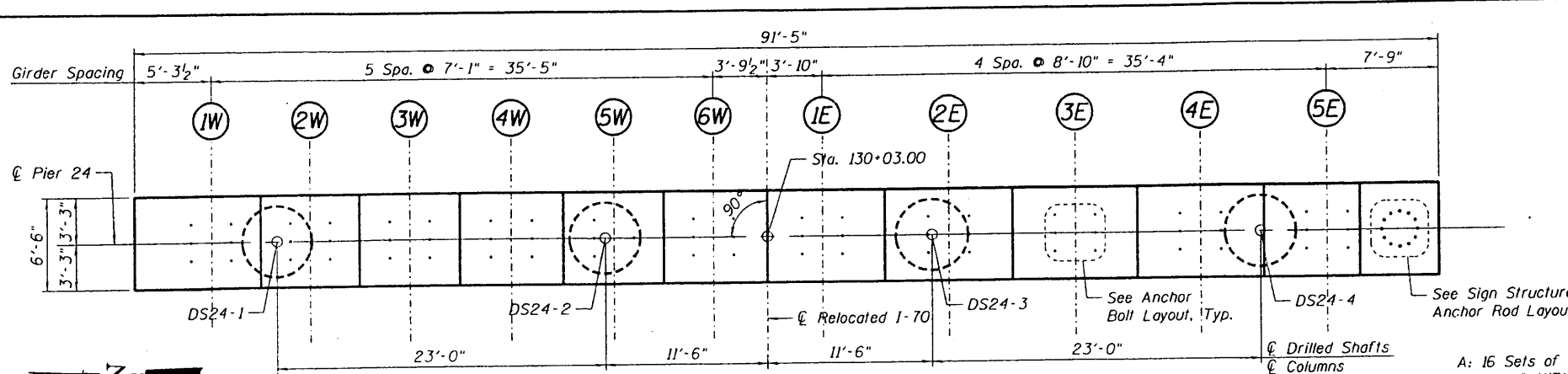
- Work this sheet with Shts. S-75, S-76 & S-77.
- The cost of steel pipes, pipe caps, and couplers for crosshole sonic logging shall be included in Drilled Shaft in Soil and Drilled Shaft in Rock.
- v(E) bars in the column/drilled shaft shall be placed as shown to provide space for p(E) bars in cap.
- Quantities and reinforcement detailing shown are based on the top of shaft and estimated top of rock elevations shown and may change based on the actual elevations encountered at each shaft.
- Concrete Sealer shall be applied to all exposed abutment areas including the bearing seats and steps, front face of backwall, top 1 ft. of the abutment face, north side of the backwall, and north and south face of abutment.
- The exposed end of v51(E) bars are to be protected. The unused half of the abutment bar splicers to be incorporated into the approach slab are to be stored by the Contractor at a location as directed by the Engineer.

\* Height of the spiral (not length) is provided in the Bar List.

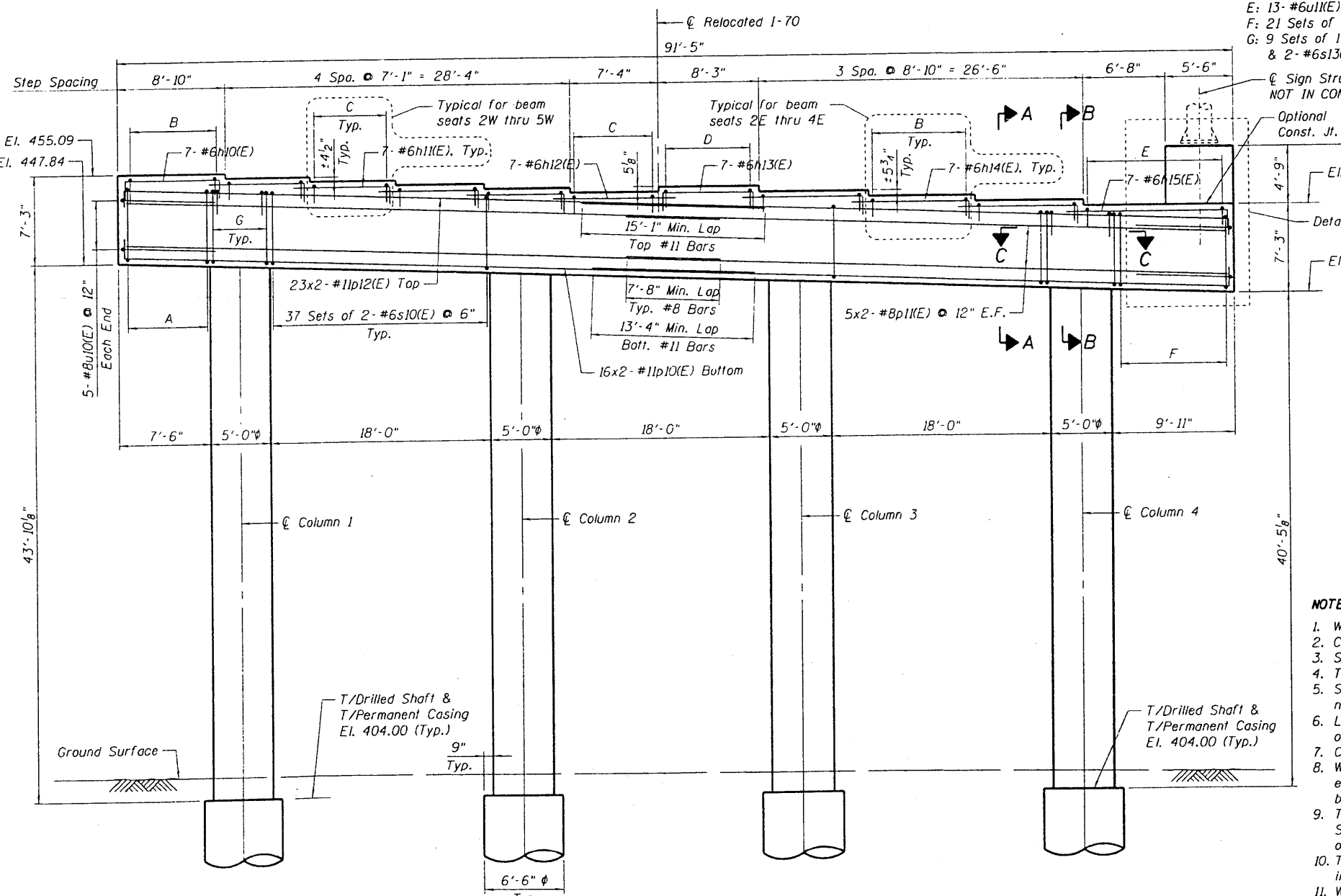
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 BONDHUJIO \V5-09\44\_AHVAUL.D.DWG  
 07-2282-26858-021\STRUCTURE\CAD\01\_DESIGN\1820318-SHEET\1820318-CONV-95-004-SHT-AB.DDN  
 \PROJECTS\CONTRACTS\081-AR.DDN\1820318-CONV-99-02-ROD.DWG  
 6-03-2010 10:15:36  
 BONDHUJIO \V5-09\44\_AHVAUL.D.DWG  
 07-2282-26858-021\STRUCTURE\CAD\01\_DESIGN\1820318-SHEET\1820318-CONV-95-004-SHT-AB.DDN

**BEARING SEAT ELEVATIONS**

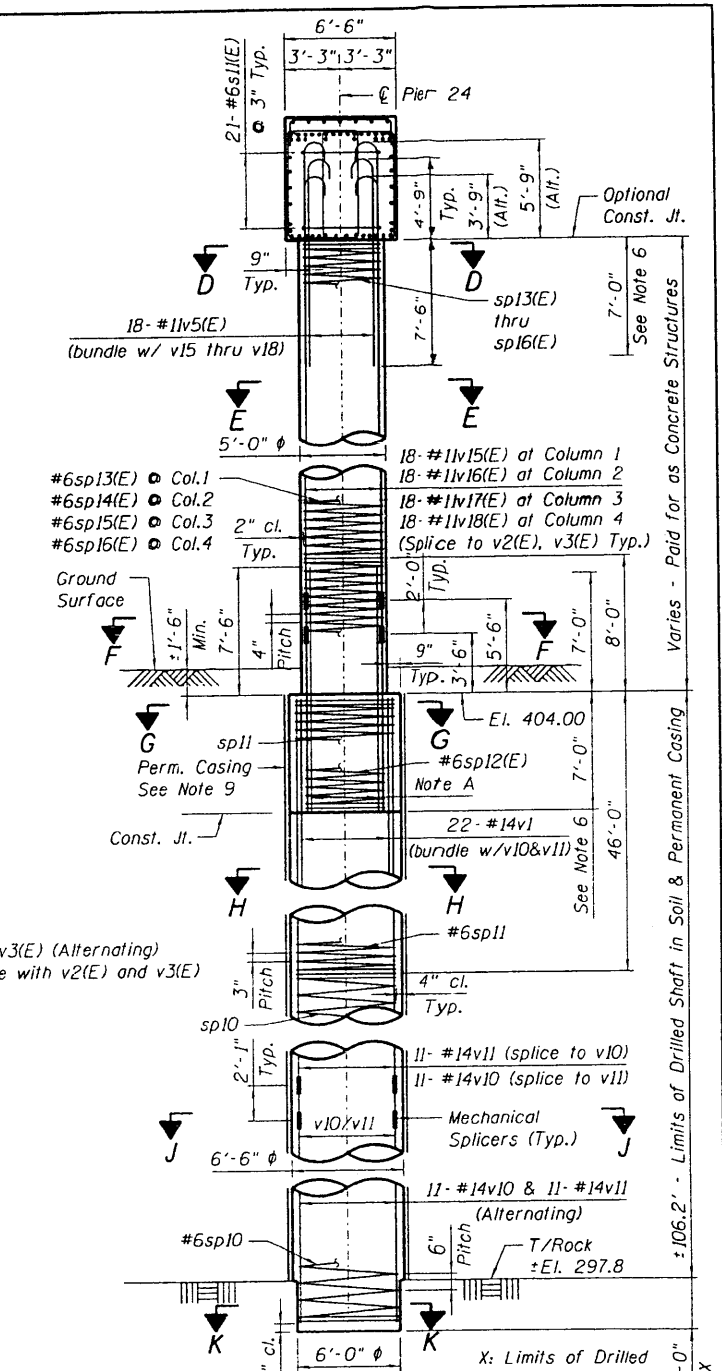
Girder	Elev.
1W	455.09
2W	454.70
3W	454.33
4W	453.95
5W	453.56
6W	453.18
1E	453.58
2E	453.11
3E	452.64
4E	452.16
5E	451.68



**PIER 24 PLAN**



**PIER 24 ELEVATION**  
(Looking East)



**PIER 24 END VIEW**

**NOTES:**

1. Work this sheet with Shts. S-80 and S-81.
2. Cast steps monolithically with cap.
3. Space top reinforcement in cap to miss anchor bolts.
4. The hooks of v15(E) thru v18(E) bars embedded in pier cap shall be oriented inward.
5. Splice locations of v and v(E) bars shall be staggered by 2'-0" min. Lap splicing of v and v(E) bars is not allowed, full-mechanical bar splicers or full-welding of bars is required.
6. Lapping of spiral reinforcement is not allowed within 7'-0" of T/Column and B/Column in either the columns or drilled shafts. Where splicing is necessary, fully-welded or full-mechanical splices are allowed.
7. Continue sp13(E) thru sp16(E) to bottom of pier cap stirrup bars.
8. When splicing of spiral reinforcement is necessary, the spirals shall be provided with 1/2 extra turns at the ends to be spliced. These additional turns shall either be welded together according to AWS D1.4, or shall both terminate with a 135° standard hook. Provide min. 4-#4 spacers or equivalent.
9. The Contractor is responsible for determining the casing thickness and the actual lip elevation to be used. See Article 516.06(d) of the Standard Specifications. Pay limits for the Permanent Casing shall be based on the minimum length shown.
10. The drilled shaft foundation design is based on end bearing in bedrock. The limits shown for Drilled Shaft in Rock is the minimum penetration required to achieve the factored resistance used in design (200 ksf).
11. Wet construction methods within the permanent casing may be required. The Contractor's installation procedure shall clearly address cleaning and inspection methods proposed for use with wet construction methods which will ensure adequate end bearing on rock is achieved.

FILE NAME: ... USER NAME: ... DESIGNED: MDB ... DRAWN: MDB ... CHECKED: TCU ... DATE: 06/04/10 ...  
 TENO ENGINEERS/ARCHITECTS/PLANNERS CHICAGO, ILLINOIS

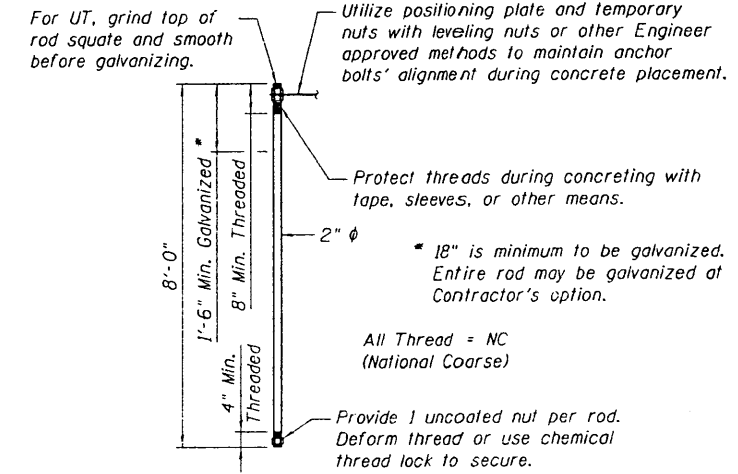
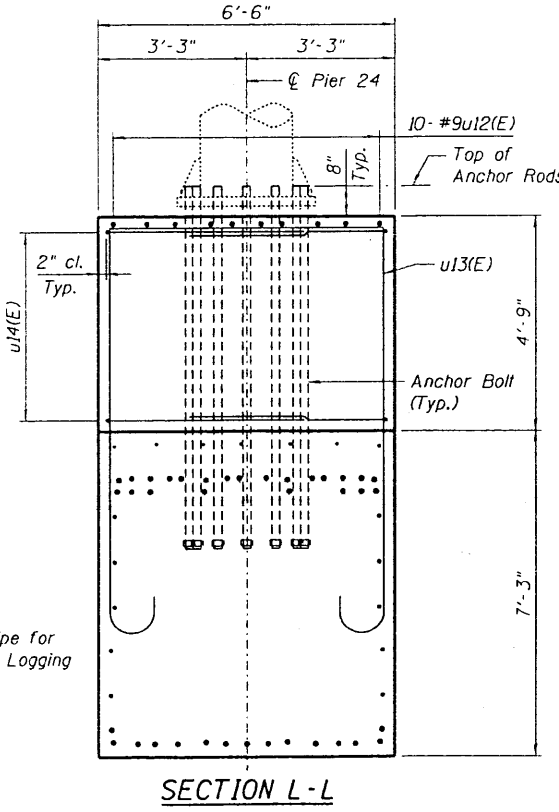
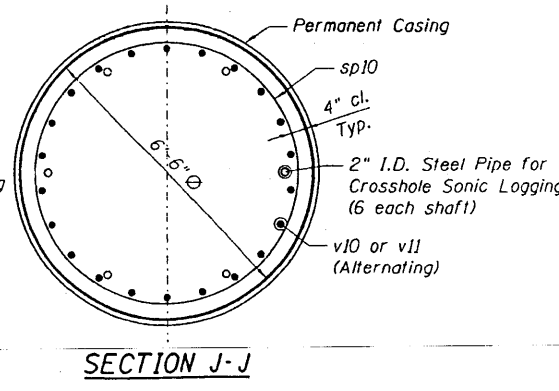
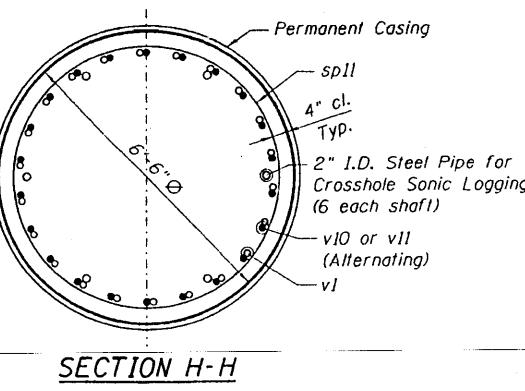
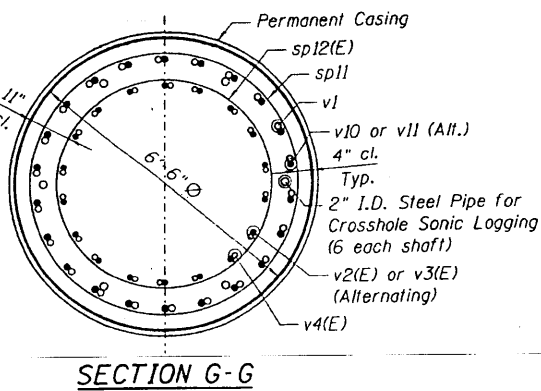
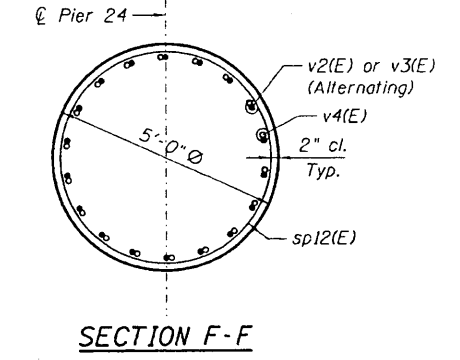
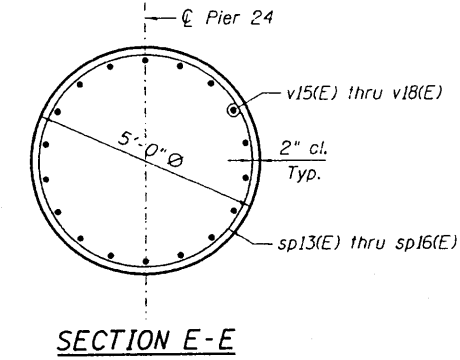
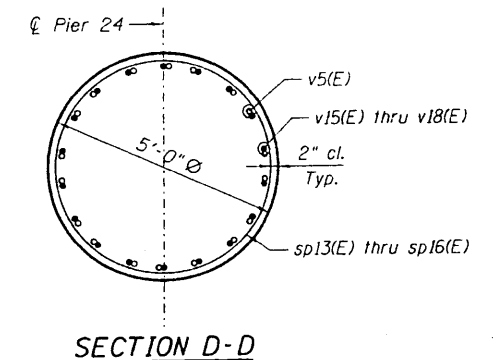
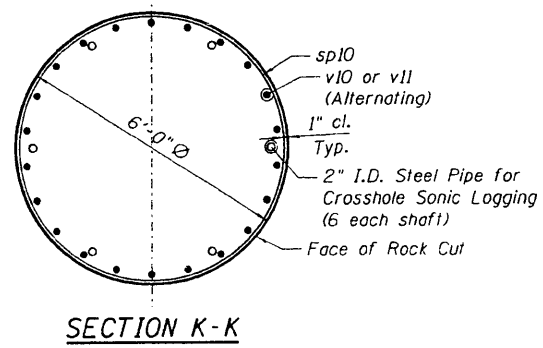
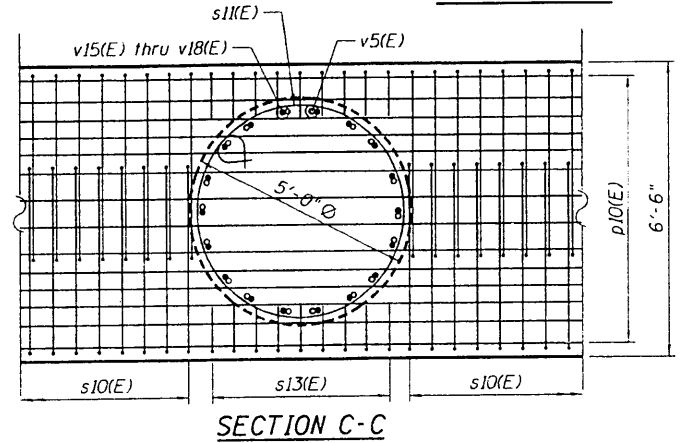
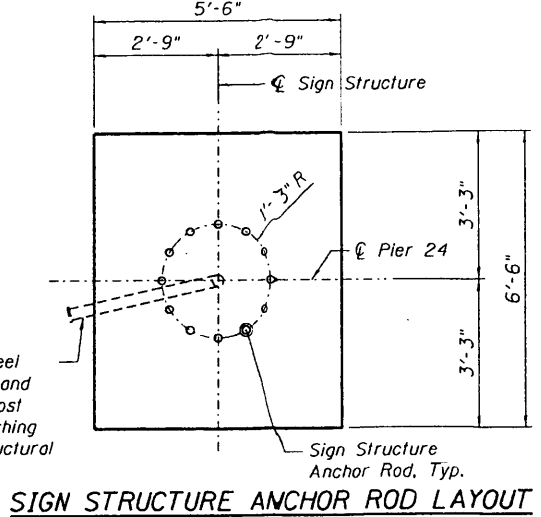
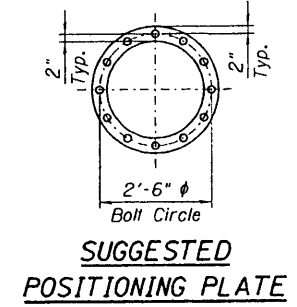
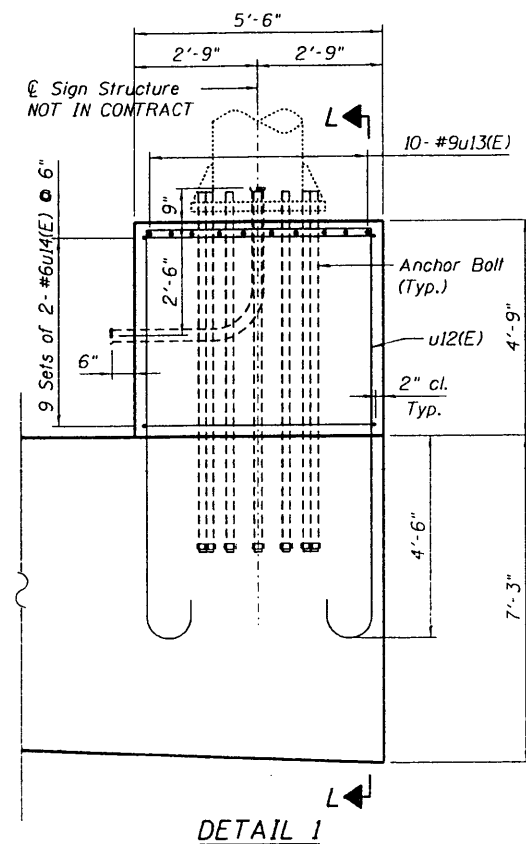
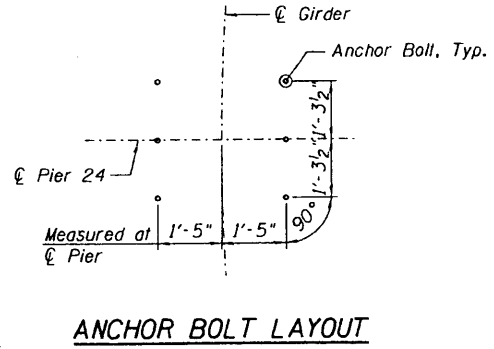
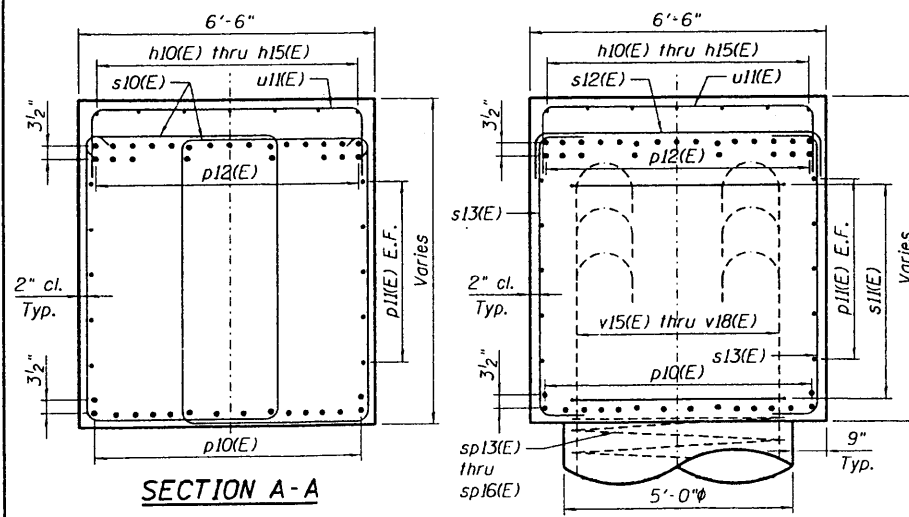
**STATE OF ILLINOIS**  
**DEPARTMENT OF TRANSPORTATION**  
 I-70 CONNECTION OVER  
 NS, IRRR, MCT AND INDUSTRIAL DR.

PIER 24 PLAN & ELEVATION

F.A.P. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
99B	B2-2-1HVB	ST. CLAIR	285	189
SN 082-0318 (EB) & 0319 (WB)		CONTRACT NO. 76C44		

SCALE: SHEET NO. 3-19 OF 5-11 STA. 134+22.00 TO 374





**SIGN STRUCTURE ANCHOR ROD DETAIL**

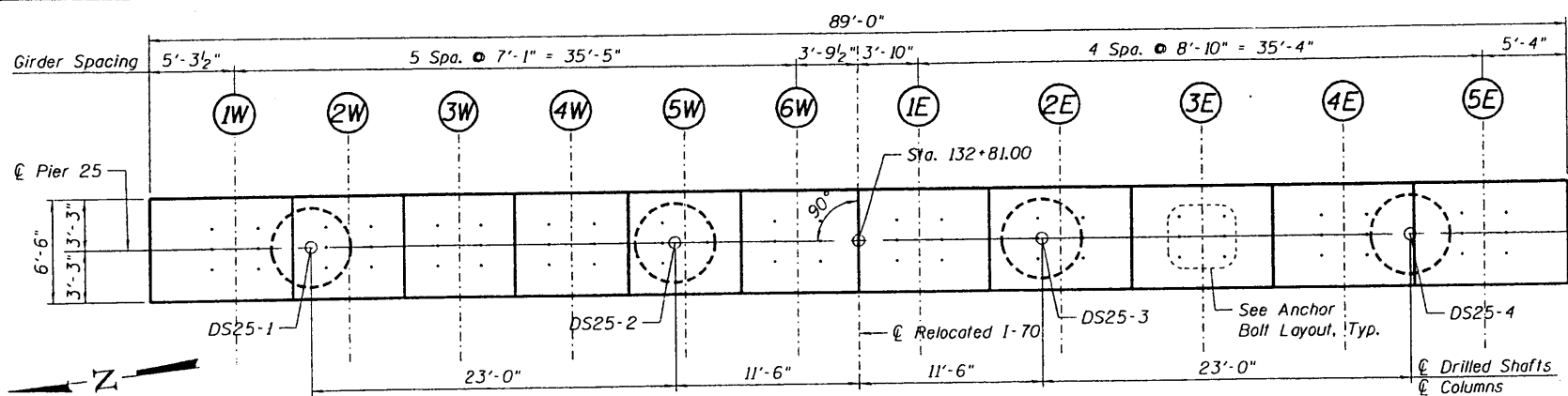
Anchor rods shall conform to AASHTO M314 Grade 105 and meet Charpy V-Notch (CVN) energy of 15 lb.-ft. at 10° F. before galvanizing. Galvanize the upper 18" (minimum) and associated M291, Grade A, C or DH heavy hex nuts and hardened washers per AASHTO M232. No welding shall be permitted on rods. Provide an unfinished nut at bottom, a hexagon locknut and washer above base plate and a leveling nut and washer below base plate. Nuts shall each be tightened with 200 lb.-ft. minimum torque against base plate. Before or after threading, but before galvanizing, each anchor rod shall be ultrasonically tested (UT) by a Level II or III inspector, qualified in accord with ANSI guidelines, using a straight beam, 1/2" φ 3.5 mhz. transducer, to insure no rejectable flaws exist in the upper 18" (tension criteria). Cost of testing included in Furnishing and Erecting Structural Steel (Pounds). Anchor rods, nuts and positioning plate shall be paid for as Furnishing and Erecting Structural Steel (Pounds).

- NOTES:**
1. Work this sheet with Shts. S-79 & S-81.
  2. The cost of steel pipes, pipe caps and couplers for crosshole sonic logging shall be included in Drilled Shaft in Soil and Drilled Shaft in Rock.
  3. v(E) bars in columns shall be placed as shown to provide space for p10(E) bars in cap.
  4. For Anchor Bolt and bearing details, see Sht. S-74.
  5. Sign structure to be furnished and installed in future contract. Anchor rods and conduit to be installed in this contract.

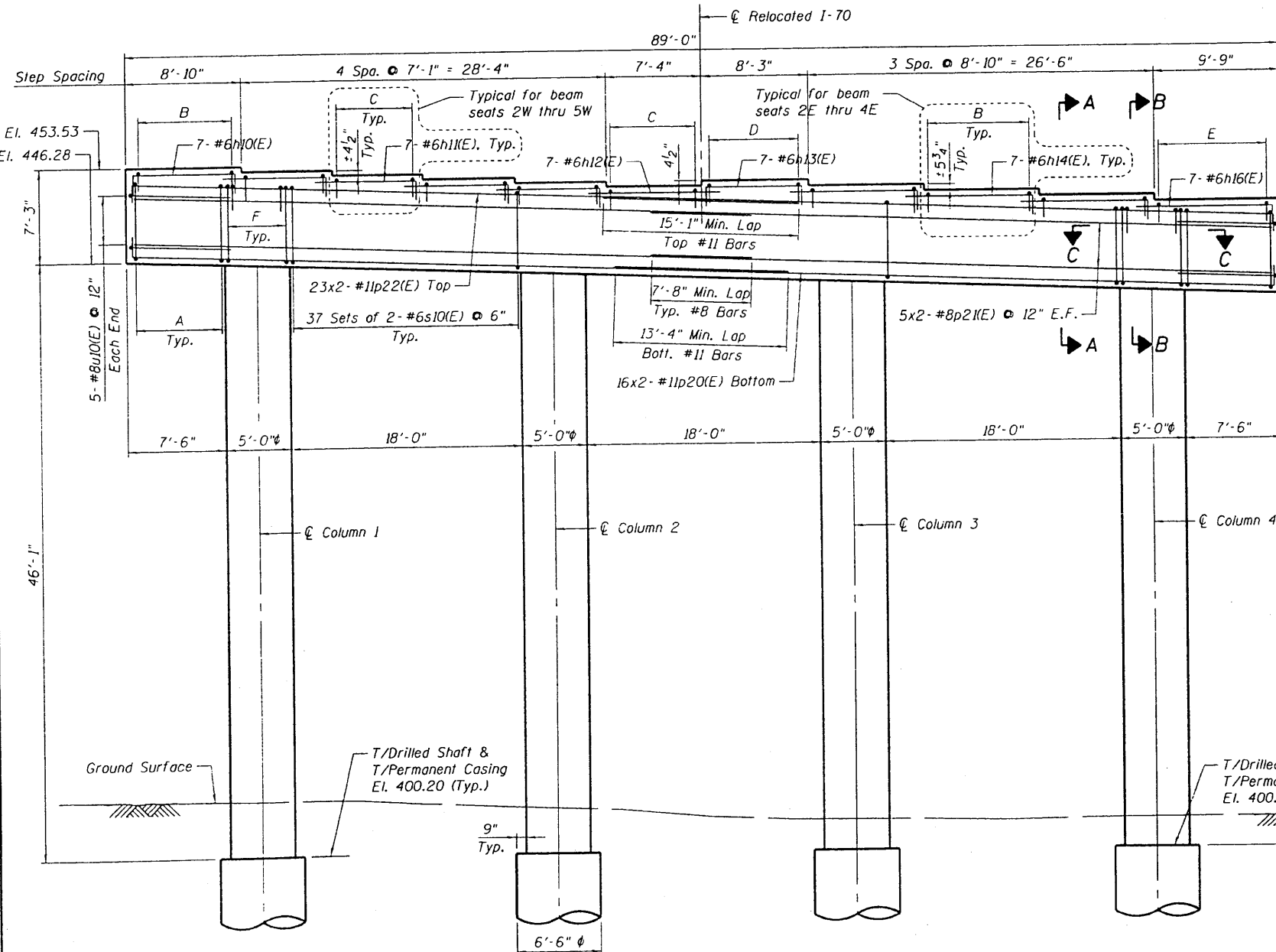
FILE NAME: I:\PROJECTS\CONNECTIONS\PIER 24\PIER 24.DWG  
 USER: TENG  
 DATE: 06/04/10  
 TENG & ASSOCIATES, INC.  
 CHICAGO, ILLINOIS

FILE NAME	USER NAME	DESIGNED	REVISIONS	STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION I-70 CONNECTION OVER NS, FRRA, MCT AND INDUSTRIAL DR.		PIER 24 DETAILS		F.A.P. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
FILE#	#USER#	MOB	REVISED					998	82-2-IHVB	ST. CLAIR	285	190
PLT SCALE	#SCALE#	CHECKED	REVISED					SN 082-0318 (EB) & 0319 (WB) CONTRACT NO. 76C44				
PLT DATE	#DATE#	TCU	REVISED	DATE: 06/04/10		SCALE:		SHEET NO. S-80 OF S-111		STA. 134+22.00 TO STA.		FED. ROAD DIST. NO. ILLINOIS-FED. AID PROJECT





**PIER 25 PLAN**

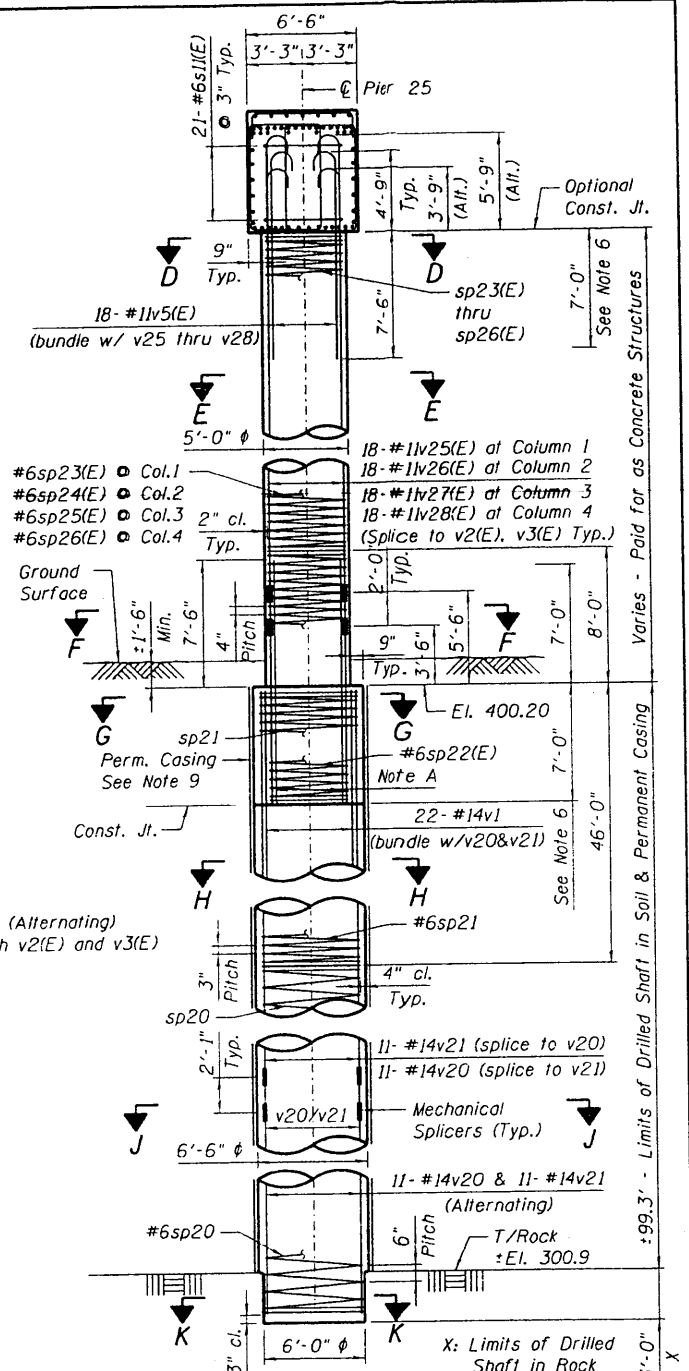


**PIER 25 ELEVATION**  
(Looking East)

**BEARING SEAT ELEVATIONS**

Girder	Elev.
1W	453.53
2W	453.15
3W	452.78
4W	452.39
5W	452.01
6W	451.63
1E	452.01
2E	451.54
3E	451.07
4E	450.59
5E	450.11

- A: 16 Sets of 2-#6s10(E) @ 6"
- B: 10-#6u11(E) @ 12"
- C: 8-#6u11(E) @ 12"
- D: 9-#6u11(E) @ 12"
- E: 11-#6u11(E) @ 12"
- F: 9 Sets of 1-#6s12(E) & 2-#6s13(E) @ 6"



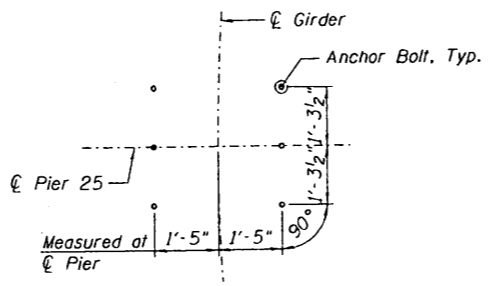
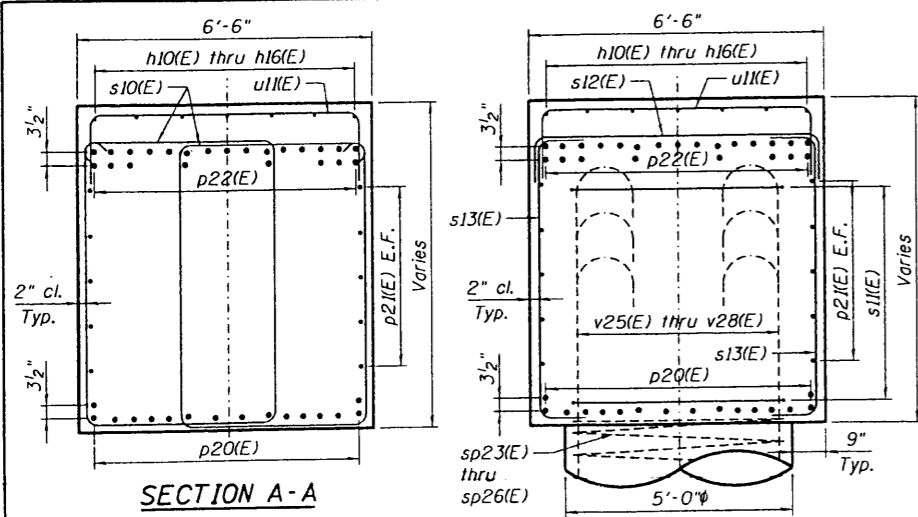
**PIER 25 END VIEW**

**NOTES:**

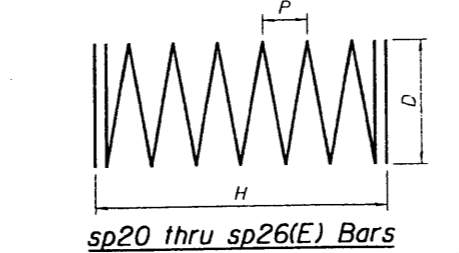
1. Work this sheet with Sht. S-83.
2. Cast steps monolithically with cap.
3. Space top reinforcement in cap to miss anchor bolts.
4. The hooks of v25(E) thru v28(E) bars embedded in pier cap shall be oriented inward.
5. Splice locations of v and v(E) bars shall be staggered by 2'-0" min. Lap splicing of v and v(E) bars is not allowed, full-mechanical bar splicers or full-welding of bars is required.
6. Lapping of spiral reinforcement is not allowed within 7'-0" of T/Column and B/Column in either the columns or drilled shafts. Where splicing is necessary, fully-welded or full-mechanical splices are allowed.
7. Continue sp23(E) thru sp26(E) to bottom of pier cap stirrup bars.
8. When splicing of spiral reinforcement is necessary, the spirals shall be provided with 1/2 extra turns at the ends to be spliced. These additional turns shall either be welded together according to AWS D1.4, or shall both terminate with a 135° standard hook. Provide min. 4-#4 spacers or equivalent.
9. The Contractor is responsible for determining the casing thickness and the actual tip elevation to be used. See Article 516.06(d) of the Standard Specifications. Pay limits for the Permanent Casing shall be based on the minimum length shown.
10. The drilled shaft foundation design is based on end bearing in bedrock. The limits shown for Drilled Shaft in Rock is the minimum penetration required to achieve the factored resistance used in design (200 ksf).
11. Wet construction methods within the permanent casing may be required. The Contractor's installation procedure shall clearly address cleaning and inspection methods proposed for use with wet construction methods which will ensure adequate end bearing on rock is achieved.

FILE NAME: ... USER: ... DESIGNED: ... DRAWN: ... CHECKED: ... DATE: ...

<b>TENGO</b> ENGINEERING ASSOCIATES, INC. CHICAGO, ILLINOIS	USER NAME: *USER* PLOT SCALE: *SCALE* PLOT DATE: *DATE*	DESIGNED: MDB DRAWN: MDB CHECKED: TCU DATE: 06/04/10	REVISED: _____ REVISED: _____ REVISED: _____ REVISED: _____	<b>STATE OF ILLINOIS</b> <b>DEPARTMENT OF TRANSPORTATION</b> I-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR.	<b>PIER 25 PLAN &amp; ELEVATION</b> SHEET NO. 5-02 OF 5-111 STA. 134+22.00 TO STA.	F.A.P. R.I.E.: 998 SECTION: 82-2-1HWB COUNTY: ST. CLAIR TOTAL SHEETS: 285 SHEET NO.: 192 CONTRACT NO.: T6C44
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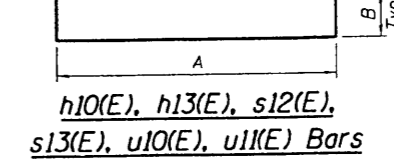


ANCHOR BOLT LAYOUT

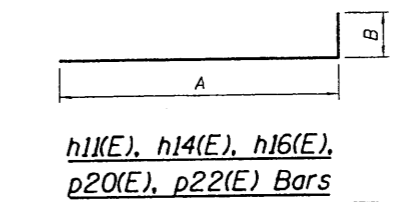


Bar	H	D	P	Length*
sp20	56'-1"	5'-10"	6"	2,088'
sp21	45'-10"	5'-10"	3"	3,379'
sp22(E)	15'-0"	4'-8"	4"	695'
sp23(E)	37'-11"	4'-8"	4"	1,689'
sp24(E)	37'-0"	4'-8"	4"	1,649'
sp25(E)	36'-1"	4'-8"	4"	1,610'
sp26(E)	35'-3"	4'-8"	4"	1,574'

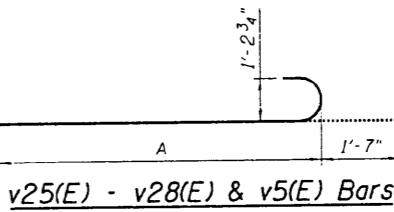
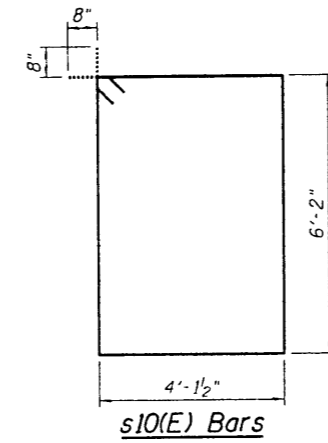
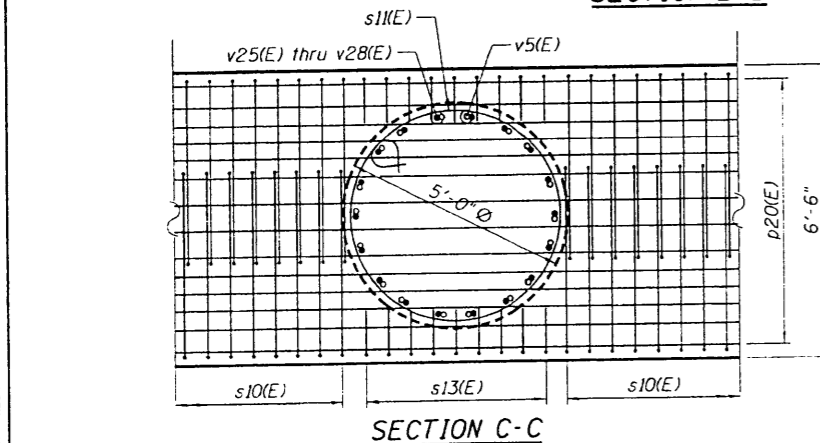
\* For Information Only - length calculated as continuous bar (ignoring splices).



Bar	A	B	Length
h10(E)	8'-6"	1'-6"	11'-6"
h13(E)	7'-11"	1'-6"	10'-11"
s12(E)	6'-2"	1'-0"	8'-2"
s13(E)	6'-2"	1'-0"	8'-2"
u10(E)	6'-0"	7'-9"	21'-6"
u11(E)	6'-2"	1'-6"	9'-2"



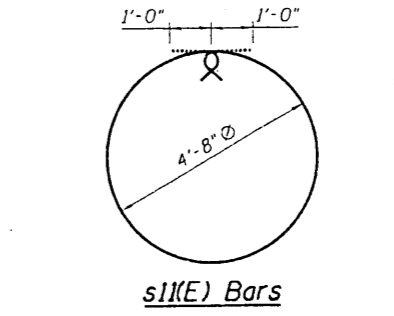
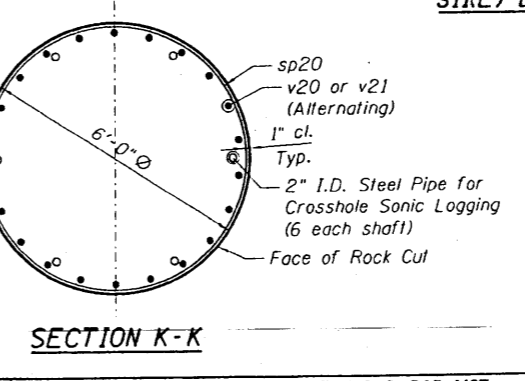
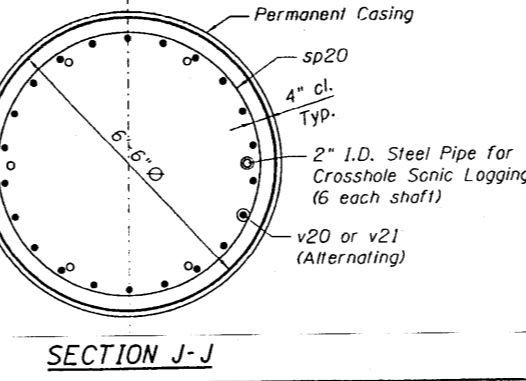
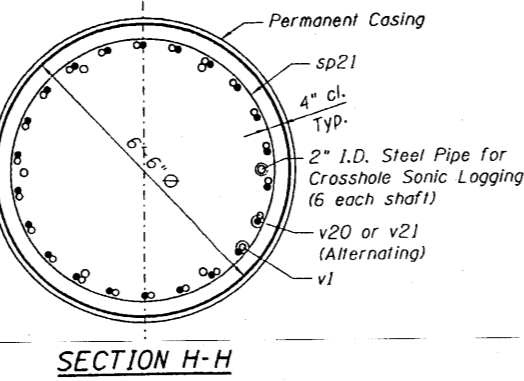
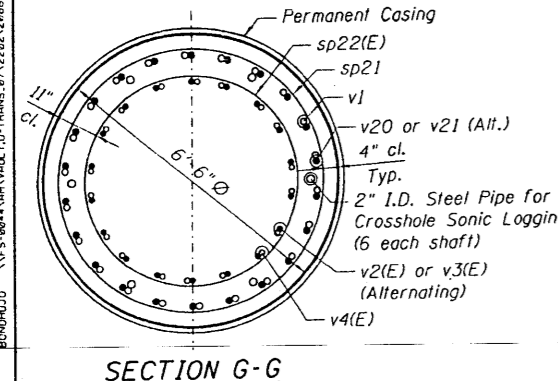
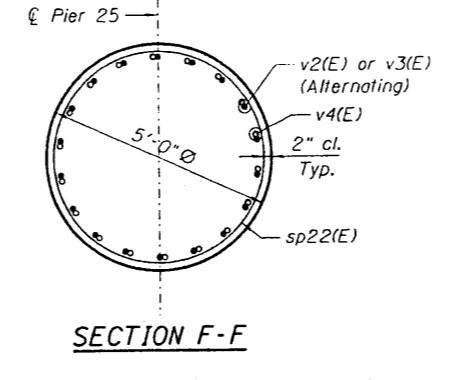
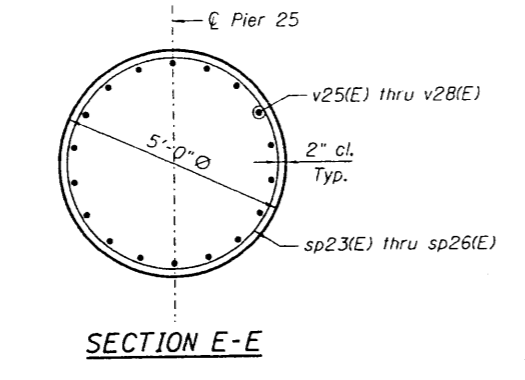
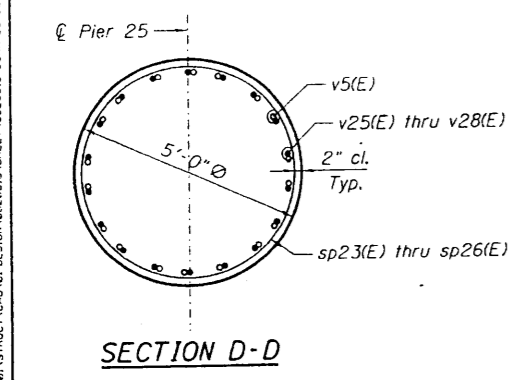
Bar	A	B	Length
h11(E)	8'-5"	1'-6"	9'-11"
h14(E)	10'-2"	1'-6"	11'-8"
h16(E)	11'-1"	1'-6"	12'-7"
p20(E)	51'-0"	2'-0"	53'-0"
p22(E)	51'-10"	2'-0"	53'-10"



Bar	A	Length
v25(E)	46'-0"	47'-7"
v26(E)	45'-1"	46'-8"
v27(E)	44'-2"	45'-9"
v28(E)	43'-4"	44'-11"
v5(E)	12'-3"	13'-10"

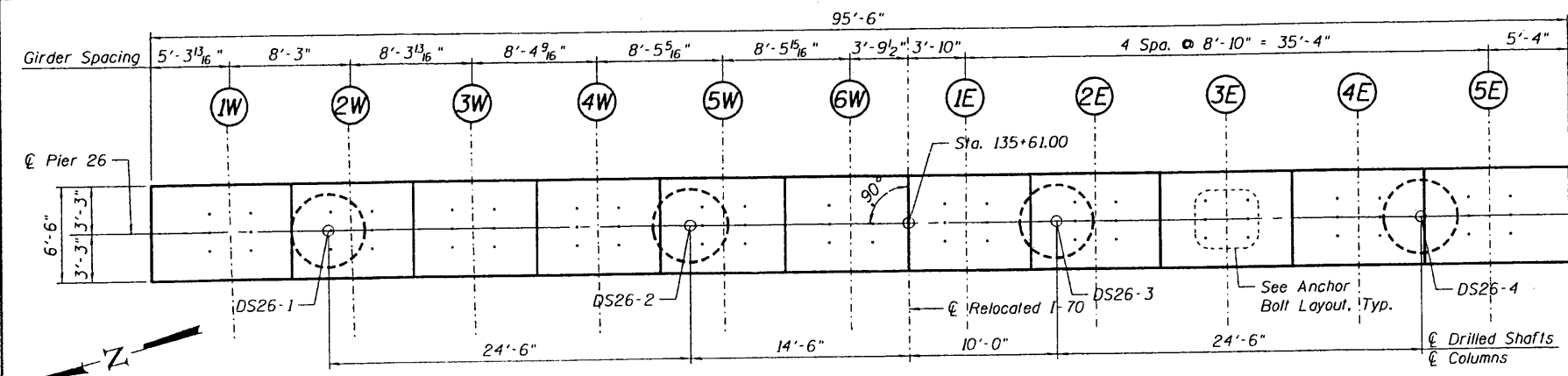
PIER 25 BAR LIST				
Bar	No.	Size	Length	Shape
h10(E)	7	#6	11'-6"	[Symbol]
h11(E)	28	#6	9'-11"	[Symbol]
h12(E)	7	#6	10'-4"	[Symbol]
h13(E)	7	#6	10'-11"	[Symbol]
h14(E)	21	#6	11'-8"	[Symbol]
h16(E)	7	#6	12'-7"	[Symbol]
p20(E)	32	#11	53'-0"	[Symbol]
p21(E)	20	#8	48'-2"	[Symbol]
p22(E)	46	#11	53'-10"	[Symbol]
s10(E)	286	#6	21'-11"	[Symbol]
s11(E)	84	#6	16'-8"	[Symbol]
s12(E)	36	#6	8'-2"	[Symbol]
s13(E)	72	#6	8'-2"	[Symbol]
u10(E)	10	#8	21'-6"	[Symbol]
u11(E)	100	#6	9'-2"	[Symbol]
v20	88	#14	49'-11"	[Symbol]
v21	88	#14	52'-0"	[Symbol]
v1	88	#14	38'-10"	[Symbol]
v2(E)	36	#11	10'-6"	[Symbol]
v3(E)	36	#11	12'-6"	[Symbol]
v4(E)	72	#11	14'-6"	[Symbol]
v25(E)	18	#11	47'-7"	[Symbol]
v26(E)	18	#11	46'-8"	[Symbol]
v27(E)	18	#11	45'-9"	[Symbol]
v28(E)	18	#11	44'-11"	[Symbol]
v5(E)	72	#11	13'-10"	[Symbol]

\* Length is height of spiral

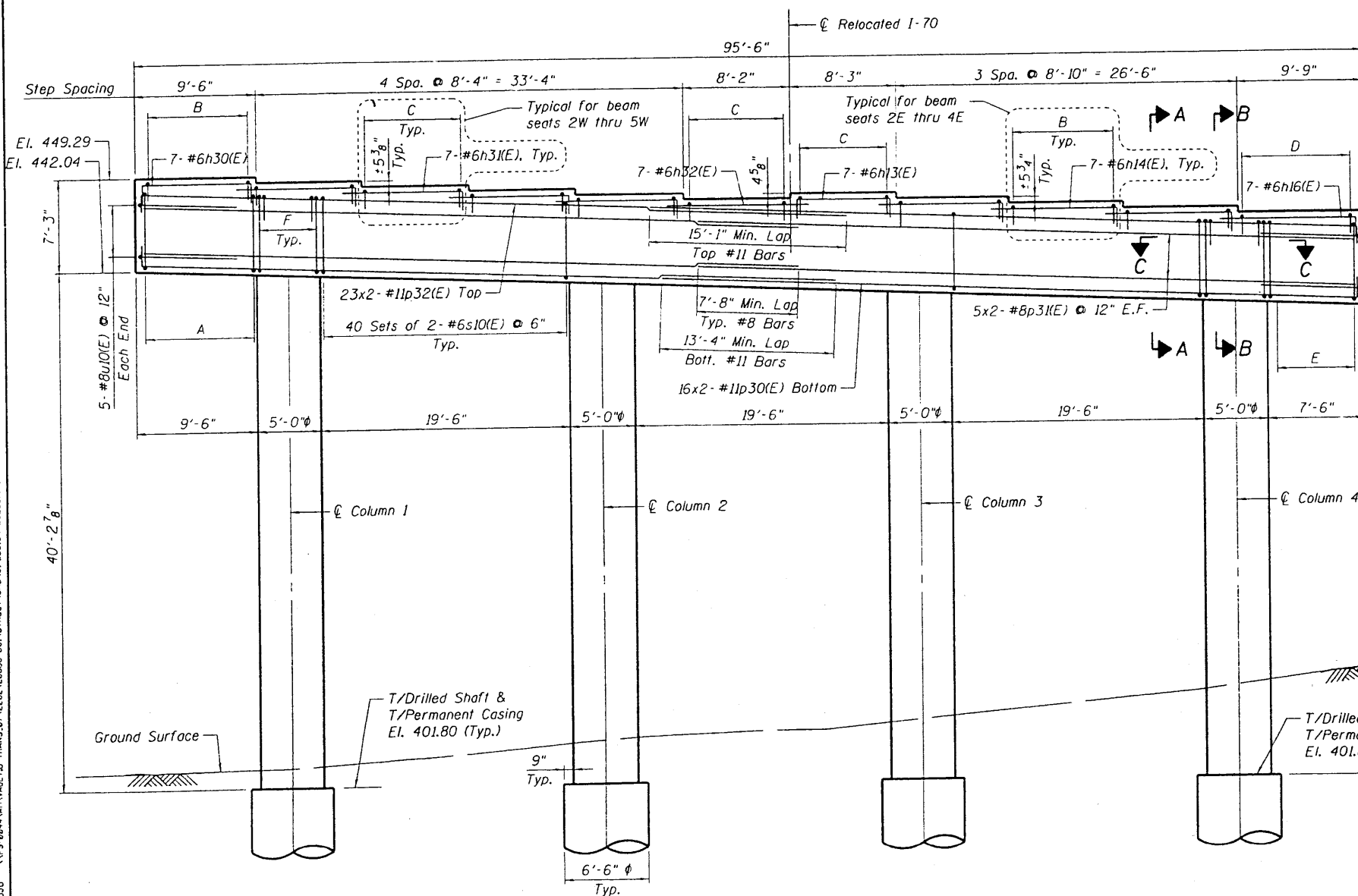


PIER 25 BILL OF MATERIAL		
Item	Unit	Total
Structure Excavation	Cu. Yd.	101
Concrete Structures	Cu. Yd.	284.5
Reinforcement Bars	Pound	127,590
Reinforcement Bars, Epoxy Coated	Pound	87,680
Permanent Casing	Foot	398
Drilled Shaft in Soil	Cu. Yd.	489
Drilled Shaft in Rock	Cu. Yd.	13
Mechanical Splicers	Each	160
Crosshole Sonic Logging	Each	1

- NOTES:
- Work this sheet with Sht. S-82.
  - The quantities and reinforcement detailing shown are based on the top of shaft and estimated top of rock elevations shown and may change based on the actual elevations encountered at each shaft.
  - The cost of steel pipes, pipe caps and couplers for crosshole sonic logging shall be included in Drilled Shaft in Soil and Drilled Shaft in Rock.
  - v(E) bars in columns shall be placed as shown to provide space for p20(E) bars in cap.
  - For Anchor Bolt and bearing details, see Sht. S-74.



**PIER 26 PLAN**



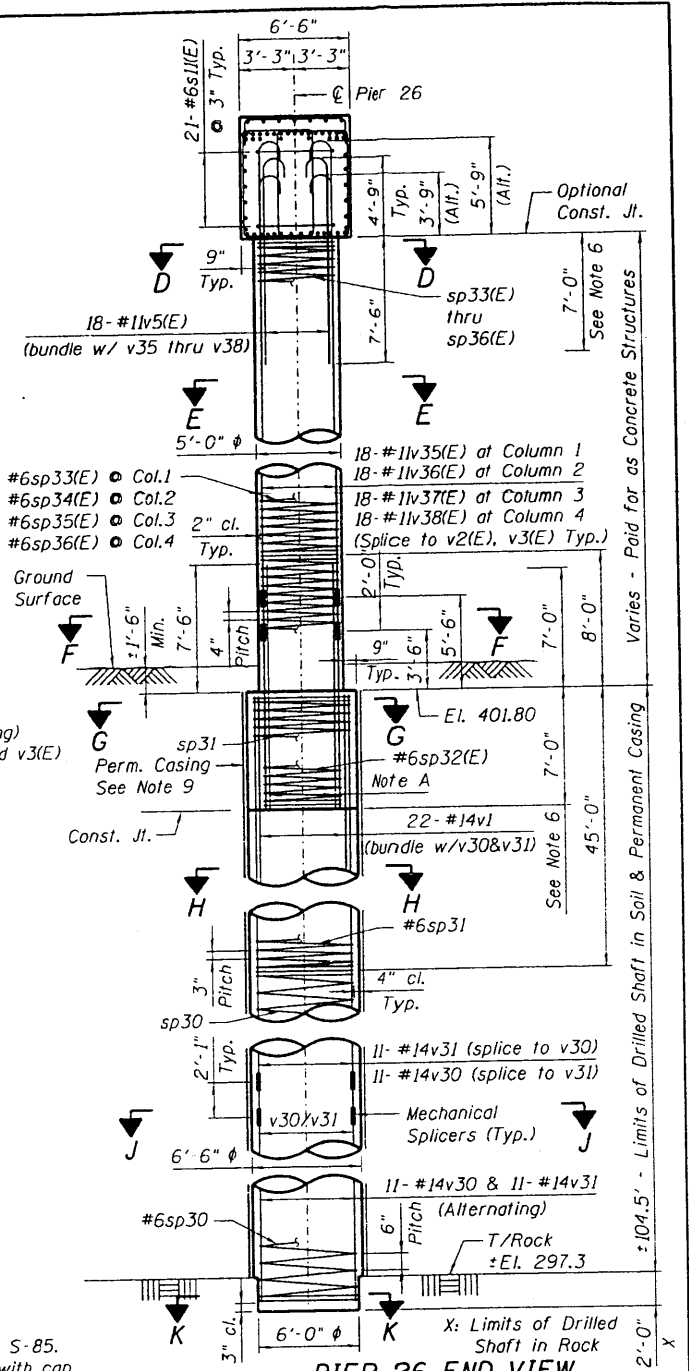
**PIER 26 ELEVATION**  
(Looking East)

**BEARING SEAT ELEVATIONS**

Girder	Elev.
1W	449.29
2W	448.84
3W	448.41
4W	447.96
5W	447.50
6W	447.04
1E	447.42
2E	446.95
3E	446.48
4E	446.00
5E	445.52

- A: 20 Sets of 2-#6s10(E) 6"
- B: 10-#6u11(E) 12"
- C: 9-#6u11(E) 12"
- D: 11-#6u11(E) 12"
- E: 16 Sets of 2-#6s10(E) 6"
- F: 9 Sets of 1-#6s12(E) & 2-#6s13(E) 6"

- Note A: 9-#11v2(E) & 9-#11v3(E) (Alternating)
- 18-#11v4(E) - bundle with v2(E) and v3(E)

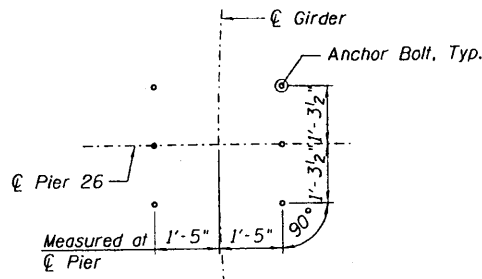
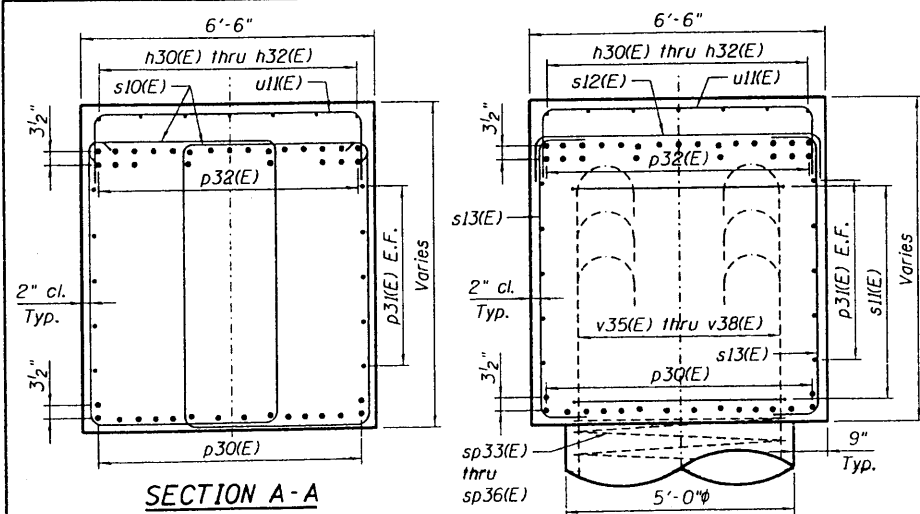


**PIER 26 END VIEW**

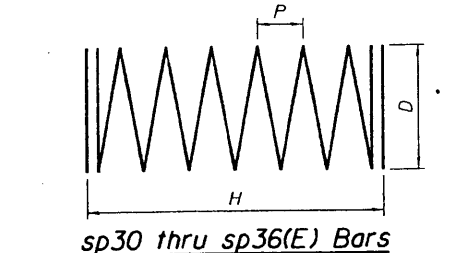
**NOTES:**

1. Work this sheet with Sht. S-85.
2. Cast steps monolithically with cap.
3. Space top reinforcement in cap to miss anchor bolts.
4. The hooks of v35(E) thru v38(E) bars embedded in pier cap shall be oriented inward.
5. Splice locations of v and v(E) bars shall be staggered by 2'-0" min. Lap splicing of v and v(E) bars is not allowed, full-mechanical bar splicers or full-welding of bars is required.
6. Lapping of spiral reinforcement is not allowed within 7'-0" of T/Column and B/Column in either the columns or drilled shafts. Where splicing is necessary, fully-welded or full-mechanical splices are allowed.
7. Continue sp33(E) thru sp36(E) to bottom of pier cap stirrup bars.
8. When splicing of spiral reinforcement is necessary, the spirals shall be provided with 1/2 extra turns at the ends to be spliced. These additional turns shall either be welded together according to AWS D1.4, or shall both terminate with a 135° standard hook. Provide min. 4-#4 spacers or equivalent.
9. The Contractor is responsible for determining the casing thickness and the actual tip elevation to be used. See Article 516.06(d) of the Standard Specifications. Pay limits for the Permanent Casing shall be based on the minimum length shown.
10. The drilled shaft foundation design is based on end bearing in bedrock. The limits shown for Drilled Shaft in Rock is the minimum penetration required to achieve the factored resistance used in design (200 ksf).
11. Wet construction methods within the permanent casing may be required. The Contractor's installation procedure shall clearly address cleaning and inspection methods proposed for use with wet construction methods which will ensure adequate end bearing on rock is achieved.

082218-CONN-05-001-P1.DGN, \\V820318-CONN-05-001-P1.DGN, \\V820318-CONN-05-001-P1.DGN, \\V820318-CONN-05-001-P1.DGN  
 082218-CONN-05-001-P1.DGN, \\V820318-CONN-05-001-P1.DGN, \\V820318-CONN-05-001-P1.DGN, \\V820318-CONN-05-001-P1.DGN  
 082218-CONN-05-001-P1.DGN, \\V820318-CONN-05-001-P1.DGN, \\V820318-CONN-05-001-P1.DGN, \\V820318-CONN-05-001-P1.DGN

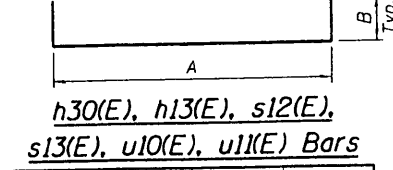


ANCHOR BOLT LAYOUT

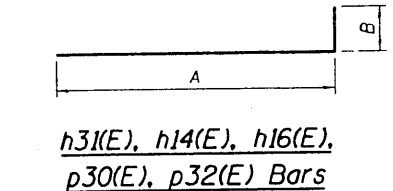


Bar	H	D	P	Length*
sp30	61'-3"	5'-10"	6"	2,276'
sp31	44'-10"	5'-10"	3"	3,306'
sp32(E)	15'-0"	4'-8"	4"	695'
sp33(E)	31'-11"	4'-8"	4"	1,429'
sp34(E)	31'-0"	4'-8"	4"	1,389'
sp35(E)	30'-0"	4'-8"	4"	1,346'
sp36(E)	29'-0"	4'-8"	4"	1,302'

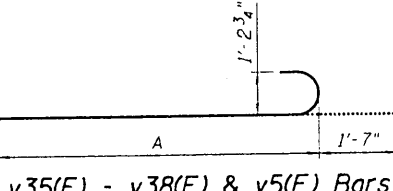
\* For Information Only - length calculated as continuous bar (ignoring splices).



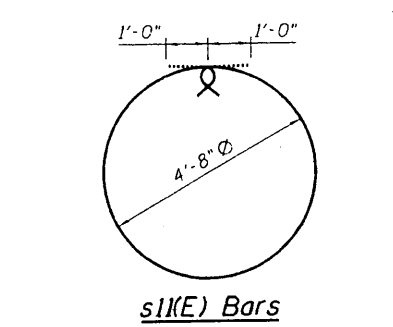
Bar	A	B	Length
h30(E)	9'-2"	1'-6"	12'-2"
h13(E)	7'-11"	1'-6"	10'-11"
s12(E)	6'-2"	1'-0"	8'-2"
s13(E)	6'-2"	1'-0"	8'-2"
u10(E)	6'-0"	7'-9"	21'-6"
u1(E)	6'-2"	1'-6"	9'-2"



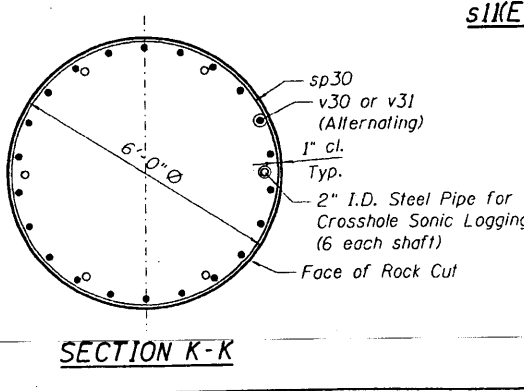
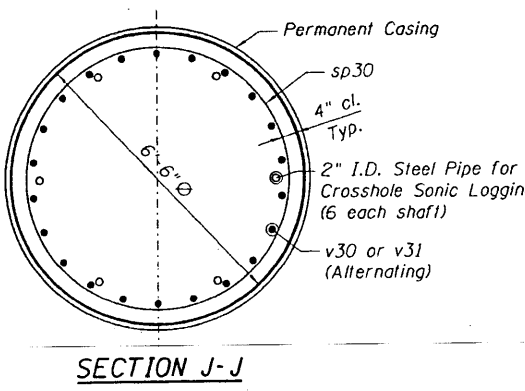
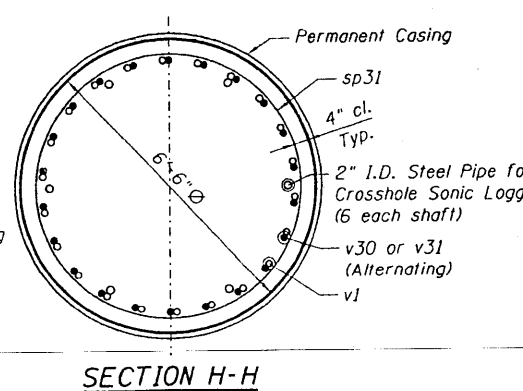
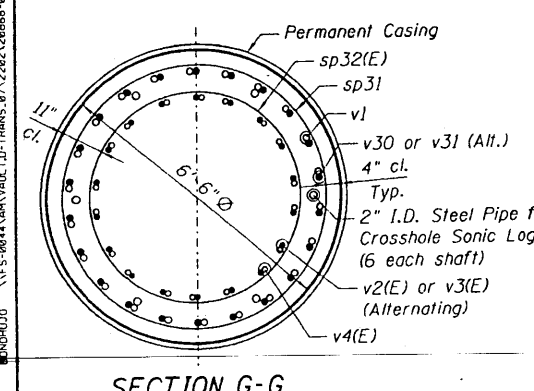
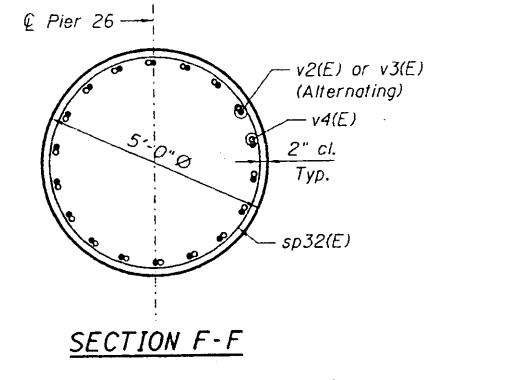
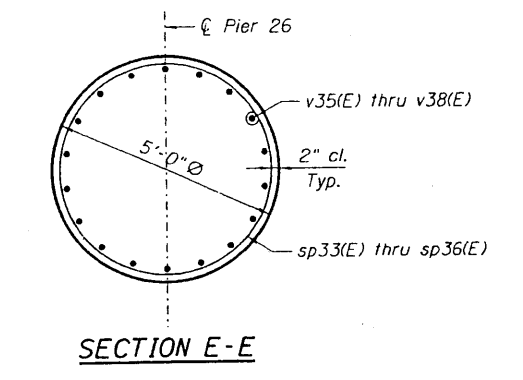
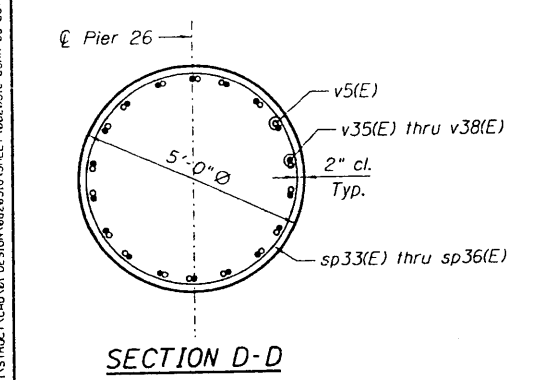
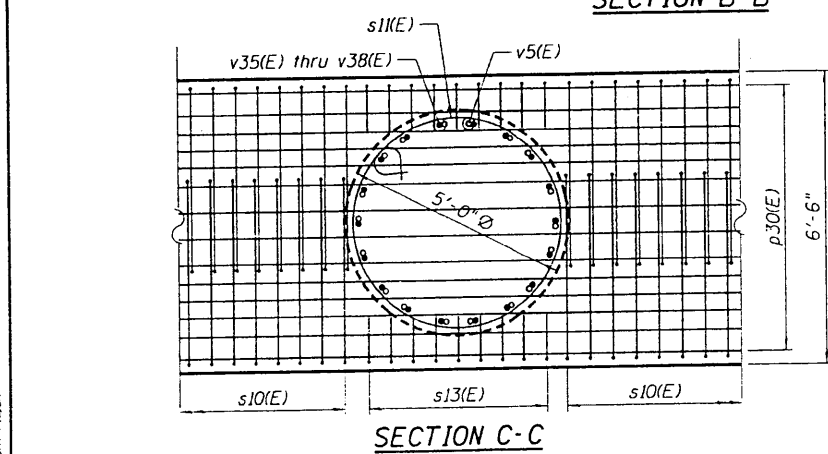
Bar	A	B	Length
h31(E)	9'-8"	1'-6"	11'-2"
h14(E)	10'-2"	1'-6"	11'-8"
h16(E)	11'-1"	1'-6"	12'-7"
p30(E)	54'-3"	2'-0"	56'-3"
p32(E)	55'-1"	2'-0"	57'-1"



Bar	A	Length
v35(E)	40'-0"	41'-7"
v36(E)	39'-1"	40'-8"
v37(E)	38'-1"	39'-8"
v38(E)	37'-1"	38'-8"
v5(E)	12'-3"	13'-10"



NOTES:  
 1. Work this sheet with Sht. S-84.  
 2. The quantities and reinforcement detailing shown are based on the top of shaft and estimated top of rock elevations shown and may change based on the actual elevations encountered at each shaft.  
 3. The cost of steel pipes, pipe caps and couplers for crosshole sonic logging shall be included in Drilled Shaft in Soil and Drilled Shaft in Rock.  
 4. v(E) bars in columns shall be placed as shown to provide space for p30(E) bars in cap.  
 5. For Anchor Bolt and bearing details, see Sht. S-74.

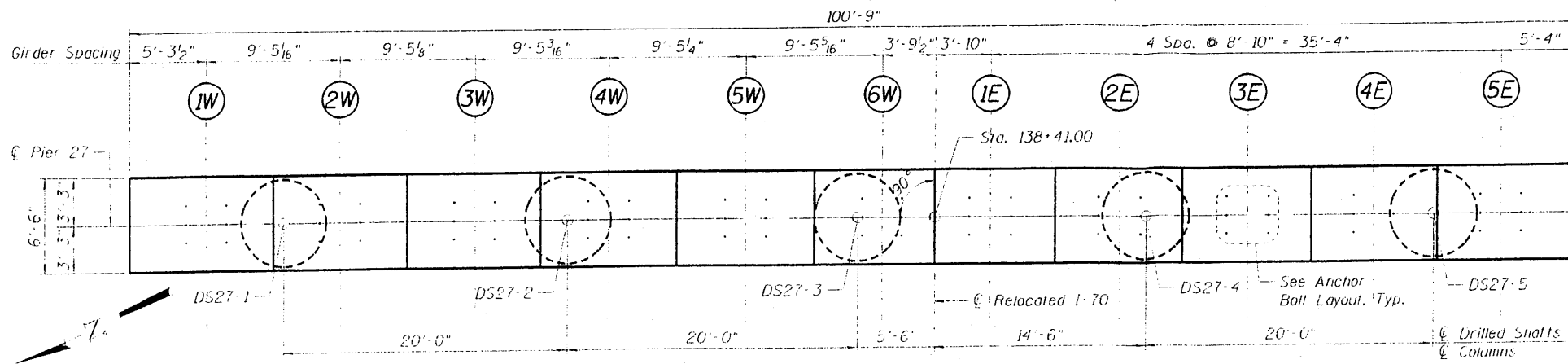


### PIER 26 BAR LIST

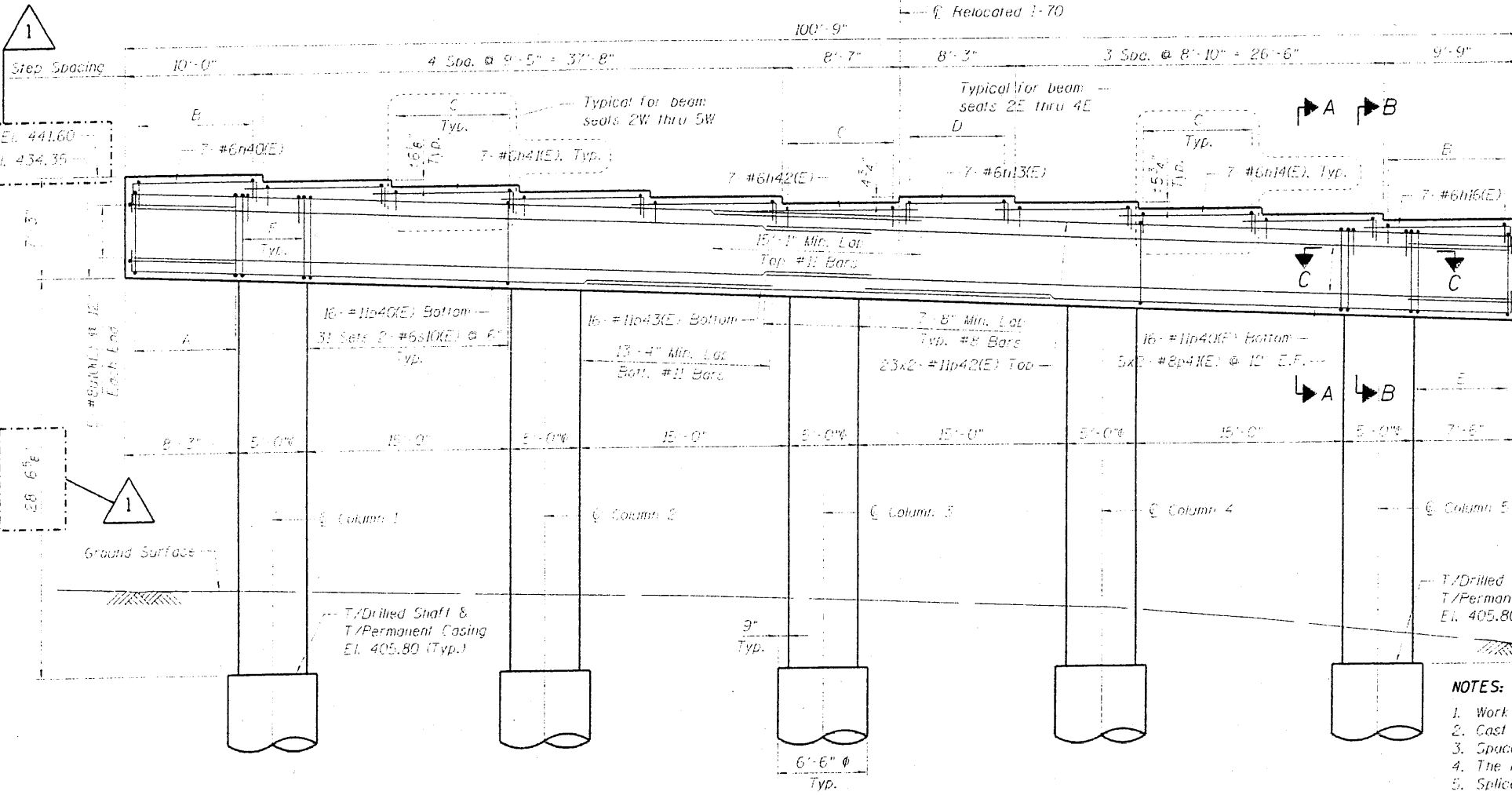
Bar	No.	Size	Length	Shape
h30(E)	7	#6	12'-2"	
h32(E)	28	#6	11'-2"	
h32(E)	7	#6	11'-2"	
h13(E)	7	#6	10'-11"	
h14(E)	21	#6	11'-8"	
h16(E)	7	#6	12'-7"	
p30(E)	32	#11	56'-3"	
p31(E)	20	#8	51'-5"	
p32(E)	46	#11	57'-1"	
s10(E)	312	#6	21'-11"	
s11(E)	84	#6	16'-8"	
s12(E)	36	#6	8'-2"	
s13(E)	72	#6	8'-2"	
u10(E)	10	#8	21'-6"	
u1(E)	105	#6	9'-2"	
v30	88	#14	52'-0"	
v31	88	#14	54'-1"	
v1	88	#14	38'-10"	
v2(E)	36	#11	10'-6"	
v3(E)	36	#11	12'-6"	
v4(E)	72	#11	14'-6"	
v35(E)	18	#11	41'-7"	
v36(E)	18	#11	40'-8"	
v37(E)	18	#11	39'-8"	
v38(E)	18	#11	38'-8"	
v5(E)	72	#11	13'-10"	

### PIER 26 BILL OF MATERIAL

Item	Unit	Total
Structure Excavation	Cu. Yd.	145
Concrete Structures	Cu. Yd.	277.6
Reinforcement Bars	Pound	131,090
Reinforcement Bars, Epoxy Coated	Pound	86,280
Permanent Casing	Foot	418
Drilled Shaft in Soil	Cu. Yd.	514
Drilled Shaft in Rock	Cu. Yd.	9
Mechanical Splicers	Each	160
Crosshole Sonic Logging	Each	1



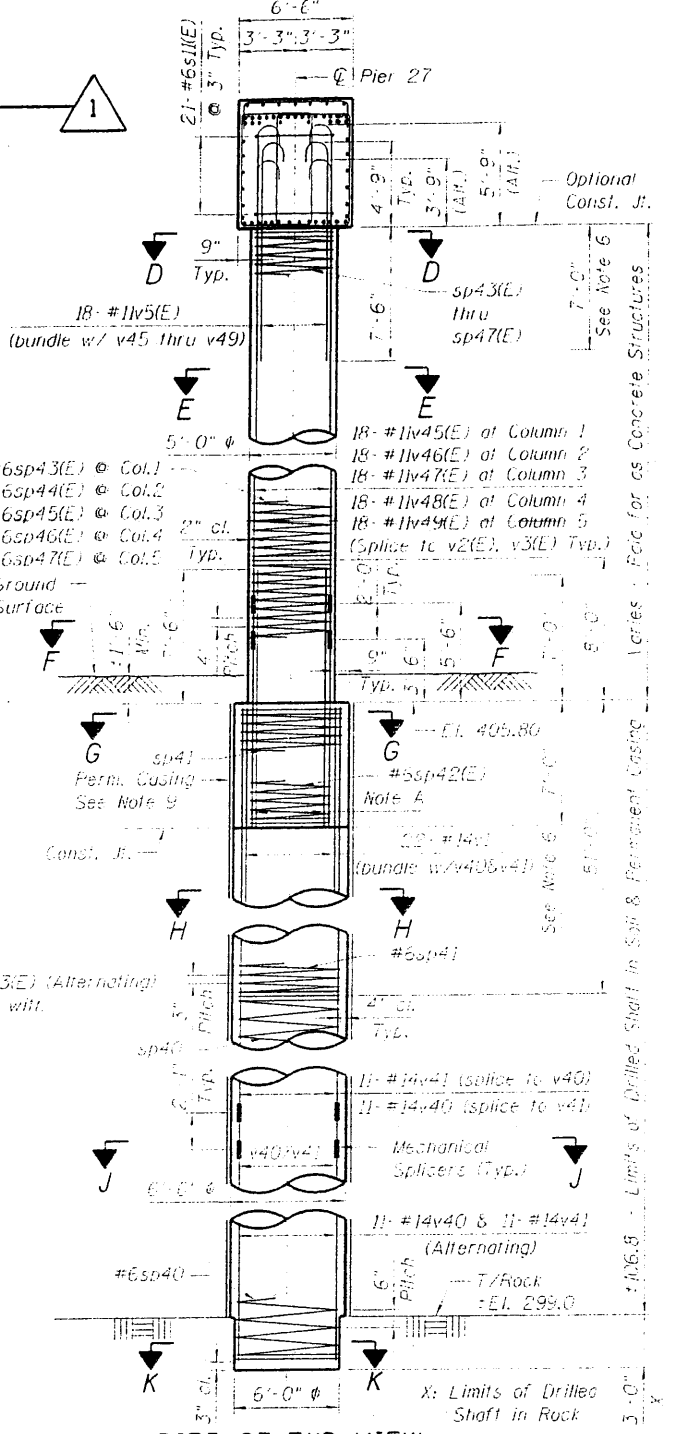
**PIER 27 PLAN**



**PIER 27 ELEVATION**  
(Looking East)

**BEARING SEAT ELEVATIONS**

Girder	Elev.
1W	441.60
2W	441.09
3W	440.59
4W	440.08
5W	439.57
6W	439.05
1E	439.46
2E	438.99
3E	438.51
4E	438.03
5E	437.55



**PIER 27 END VIEW**

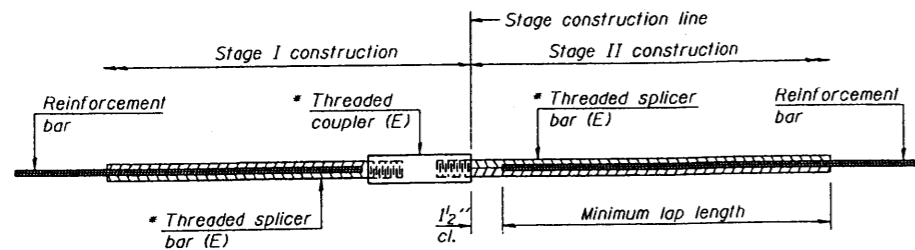
- A: 17 Sets of 2-#6s10(E) @ 6"
- B: 12-#6u18(E) @ 12"
- C: 10-#6u18(E) @ 12"
- D: 9-#6u18(E) @ 12"
- E: 16 Sets of 2-#6s10(E) @ 6"
- F: 9 Sets of 1-#6s12(E) & 2-#6s13(E) @ 6"

**NOTES:**

1. Work this sheet with Sht. S-87.
2. Cast steps monolithically with cap.
3. Space top reinforcement in cap to miss anchor bolts.
4. The hooks of v45(E) thru v49(E) bars embedded in pier cap shall be oriented inward.
5. Splice locations of v and v(E) bars shall be staggered by 2'-0" min. Lap splicing of v and v(E) bars is not allowed, full-mechanical bar splicers or full-welding of bars is required.
6. Lapping of spiral reinforcement is not allowed within 7'-0" of T/Column and E/Column in either the columns or drilled shafts. Where splicing is necessary, fully welded or full-mechanical splicers are allowed.
7. Continue sp43(E) thru sp47(E) to bottom of pier cap stirrup bars.
8. When splicing of spiral reinforcement is necessary, the spirals shall be provided with 1/2 extra turns at the ends to be spliced. These additional turns shall either be welded together according to AWS D1.4, or shall both terminate with a 135° standard hook. Provide min. 4 #4 spacers or equivalent.
9. The Contractor is responsible for determining the casing thickness and the actual tip elevation to be used. See Article 5J6.06(d) of the Standard Specifications. Pay limits for the Permanent Casing shall be based on the minimum length shown.
10. The drilled shaft foundation design is based on end bearing in bedrock. The limits shown for Drilled Shaft in Rock is the minimum penetration required to achieve the factored resistance used in design (200 ksf).
11. Wet construction methods within the permanent casing may be required. The Contractor's installation procedure shall clearly address cleaning and inspection methods proposed for use with wet construction methods which will ensure adequate end bearing on rock is achieved.







**STANDARD BAR SPLICER ASSEMBLY**

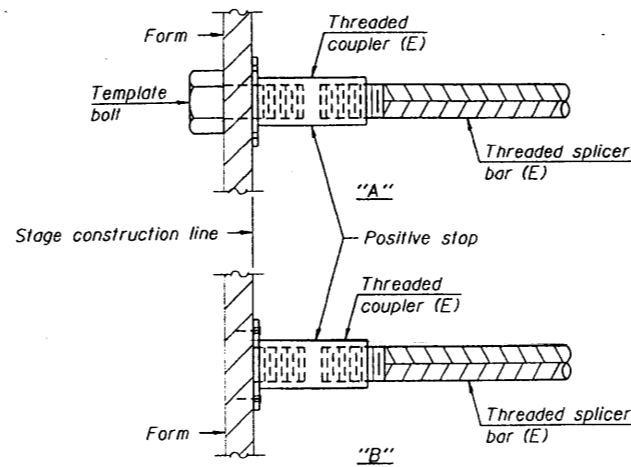
Bar size to be spliced	Minimum Lap Lengths			
	Table 1	Table 2	Table 3	Table 4
3, 4	1'-5"	1'-11"	2'-1"	2'-4"
5	1'-9"	2'-5"	2'-7"	2'-11"
6	2'-1"	2'-11"	3'-1"	3'-6"
7	2'-9"	3'-10"	4'-2"	4'-8"
8	3'-8"	5'-1"	5'-5"	6'-2"
9	4'-7"	6'-5"	6'-10"	7'-9"

Table 1: Black bar, 0.8 Class C  
 Table 2: Black bar, Top bar lap, 0.8 Class C  
 Table 3: Epoxy bar, 0.8 Class C  
 Table 4: Epoxy bar, Top bar lap, 0.8 Class C

Threaded splicer bar length = min. lap length + 1 1/2" + thread length

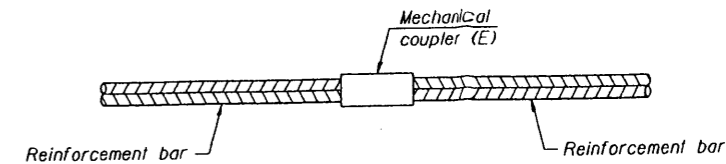
\* Epoxy not required on Bar Splicer Assembly components used in conjunction with black bars.

Location	Bar size	No. assemblies required	Table for minimum lap length



**INSTALLATION AND SETTING METHODS**

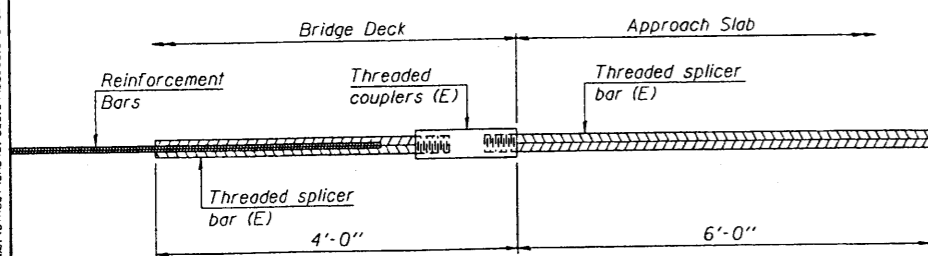
"A": Set bar splicer assembly by means of a template bolt.  
 "B": Set bar splicer assembly by nailing to wood forms or cementing to steel forms.  
 (E): Indicates epoxy coating.



**STANDARD MECHANICAL SPLICER**

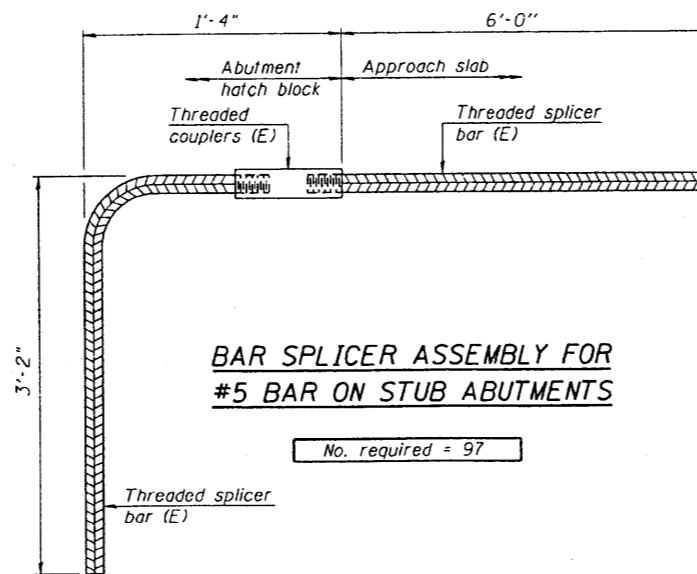
Location	Bar size	No. assemblies required
Pier 24	#14	88
	#11	72
Pier 25	#14	88
	#11	72
Pier 26	#14	88
	#11	72
Pier 27	#14	110
	#11	90

C:\FS-084\KVA\VAL.L.D.-TRANS.9712282-28665-081\STRUCT\LOAD\01 DESIGN\02\03\B\SEE1\02282310-COMM-95-821-SMT-HS.DGN  
 BSD-1  
 11-1-09  
 TENG & ASSOCIATES, INC.  
 ENGINEERS/ARCHITECTS/PLANNERS  
 CHICAGO, ILLINOIS



**BAR SPLICER ASSEMBLY FOR #5 BAR ON INTEGRAL OR SEMI-INTEGRAL ABUTMENTS**

No. required =



**BAR SPLICER ASSEMBLY FOR #5 BAR ON STUB ABUTMENTS**

No. required = 97

**NOTES**

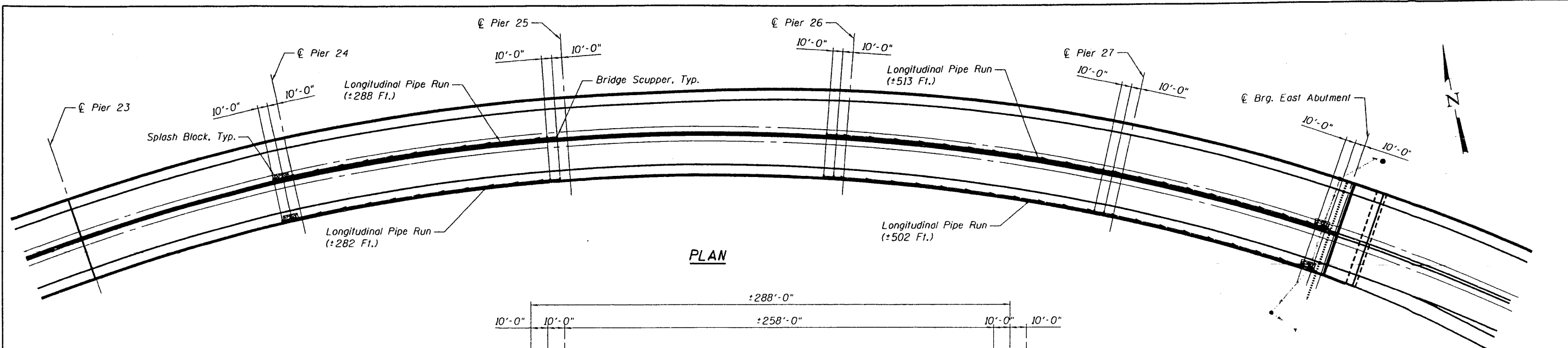
Splicer bars shall be deformed with threaded ends and have a minimum 60 ksi yield strength.  
 All reinforcement shall be lapped and tied to the splicer bars.  
 Bar splicer assemblies shall be epoxy coated according to the requirements for reinforcement bars. See Section 508 of the Standard Specifications.  
 See special provision for Mechanical Splicers.  
 See approved list of bar splicer assemblies and mechanical splicers for alternatives.

BSD-1

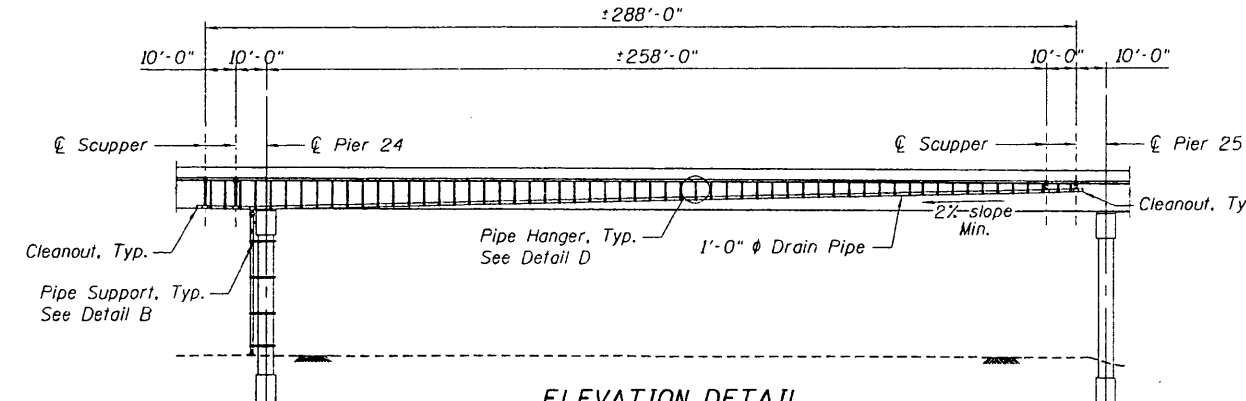
11-1-09

FILE NAME :	USER NAME : #USER#	DESIGNED - JLR	REVISED -	STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION 1-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR.	BAR SPLICER DETAILS	F.A.P. RTE.:	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
FILE# :	PLT SCALE : #SCALE#	DRAWN - CFB	REVISED -			998	62-2-1HVB	ST. CLAIR	285	198
TENG & ASSOCIATES, INC. ENGINEERS/ARCHITECTS/PLANNERS CHICAGO, ILLINOIS	PLT DATE : #DATE#	CHECKED - JLR	REVISED -			SN 082-0318 (EB) & 0319 (WB)	CONTRACT NO. 76C44		FED. ROAD DIST. NO. ILLINOIS FED. AID PROJECT	
DATE - 06/04/10	REVISED -	SCALE:	SHEET NO. S-BB OF S-111			STA. 134+22.00 TO STA.				





**PLAN**

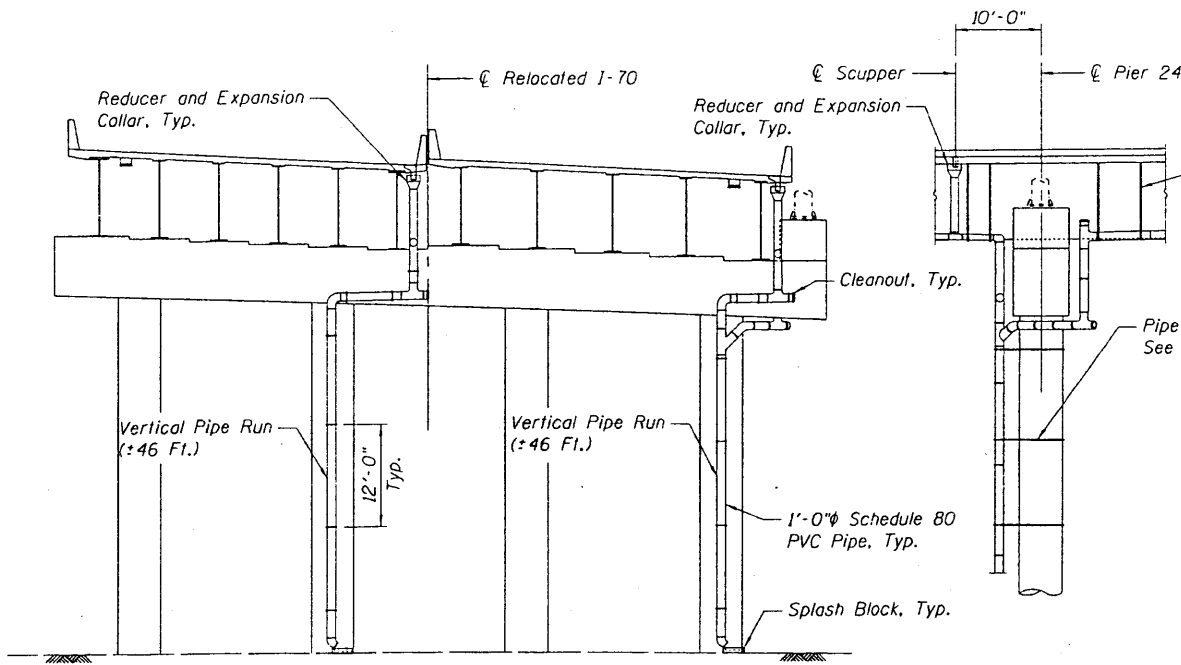


**ELEVATION DETAIL**

(Looking North, WB Pipe Run shown)

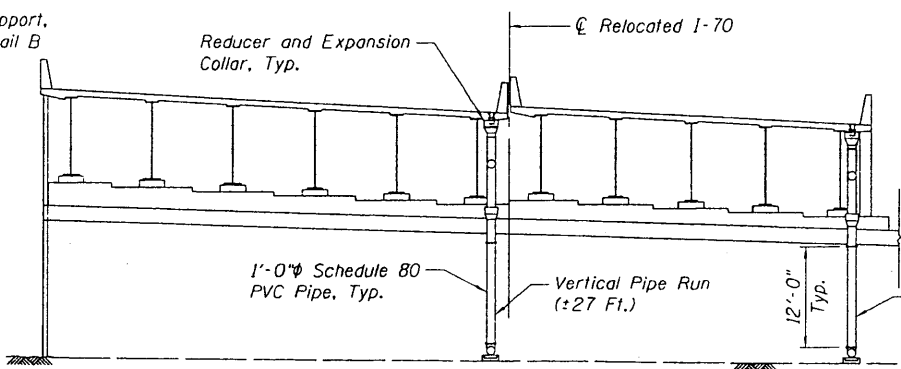
**NOTES:**

1. Work this sheet with Sheet S-91.
2. Pipe hangers shall be provided on all horizontal collector pipes at each tee, elbow, or change in direction and at intermediate points as recommended by pipe manufacturer. Collector pipe hangers shall have a load capacity of not less than 2000 lbs. and shall be designed so as not to apply excessive compressive stress to the pipe. Pipe supports shall be provided on all vertical drain pipes at points not more than 12'-0" on centers.

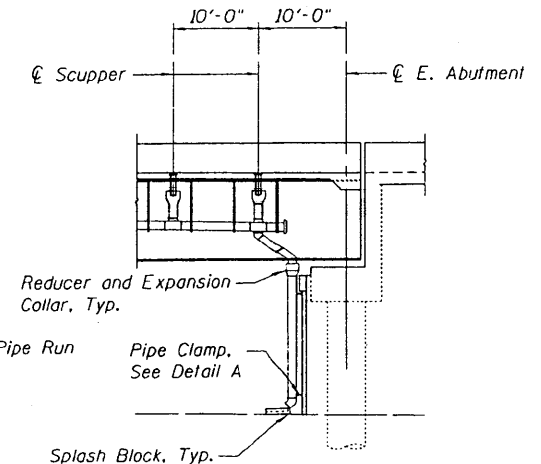


**ELEVATION - PIER 24**  
(Looking East)

**END VIEW - PIER 24**  
(Looking North)



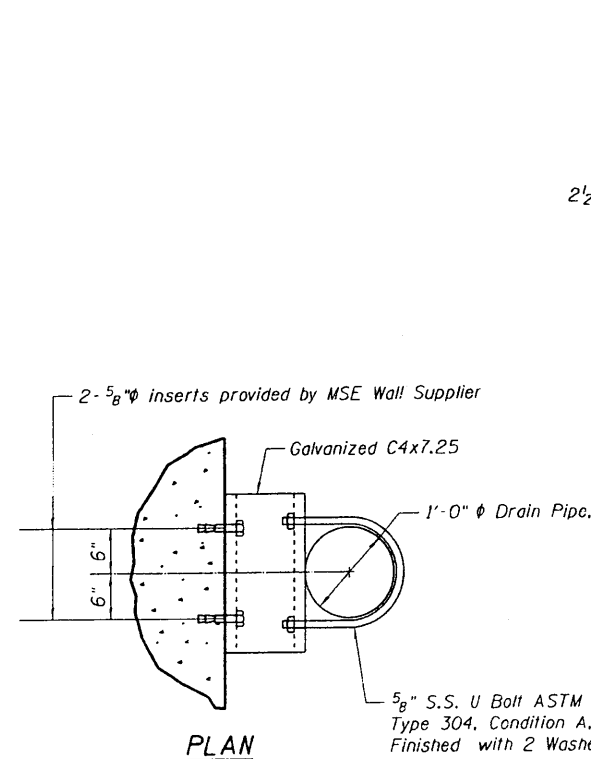
**ELEVATION - EAST ABUTMENT**  
(Looking East)



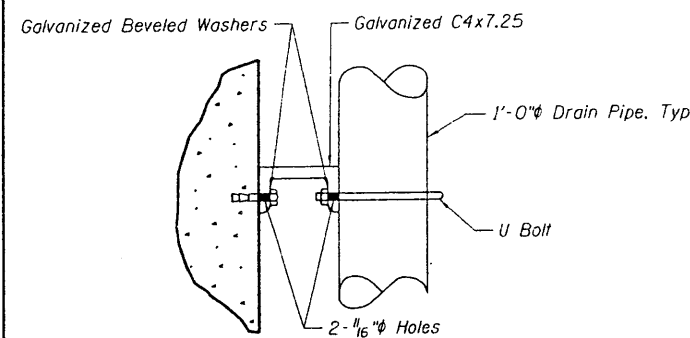
**END VIEW - EAST ABUTMENT**  
(Looking North)

FILE NAME : USER NAME : #USER# DESIGNED - TKL REVISED - DRAWN - CPB REVISED - CHECKED - TCU REVISED - DATE - 06/04/10 REVISED -  
 TENG & ASSOCIATES, INC. ENGINEERS/ARCHITECTS/PLANNERS CHICAGO, ILLINOIS  
 STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION BRIDGE DRAINAGE SYSTEM  
 I-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR. SCALE: SHEET NO. S-90 OF S-111 STA. 134+22.00 TO STA.

FILE NAME :	USER NAME : #USER#	DESIGNED - TKL	REVISED -	STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION I-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR.	BRIDGE DRAINAGE SYSTEM	F.A.P. RTE.	SECTION	COUNTY	TOTAL SHEET NO.
PLLOT SCALE : #SCALE#	CHECKED - TCU	REVISED -	998			82-2-1HVB	ST. CLAIR	285	200
PLLOT DATE : #DATE#	DATE - 06/04/10	REVISED -	SN 002-0318 (E) & 0319 (W)			CONTRACT NO. 76C44			
			FED. ROAD DIST. NO.			ILLINOIS FED. AID PROJECT			



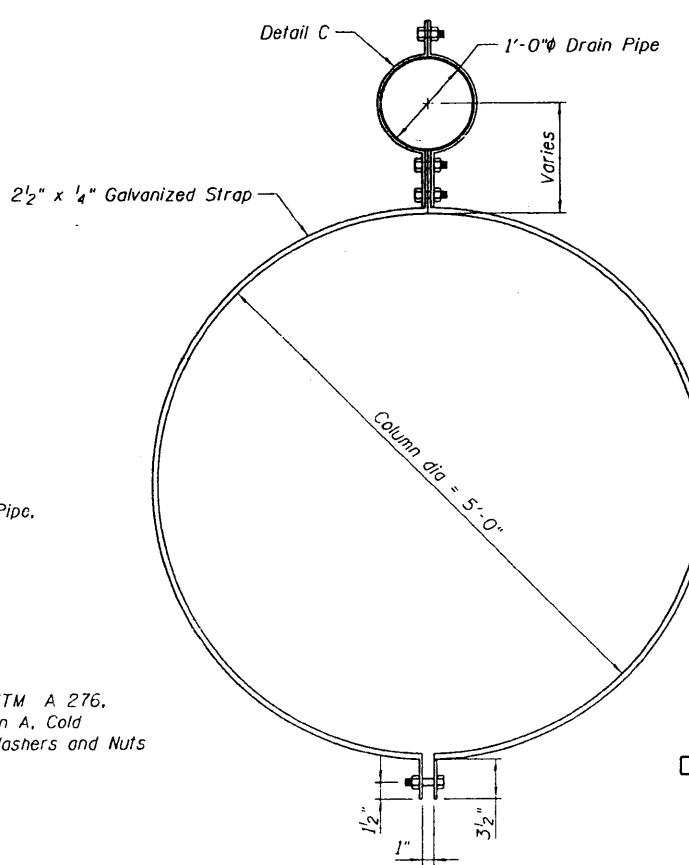
PLAN



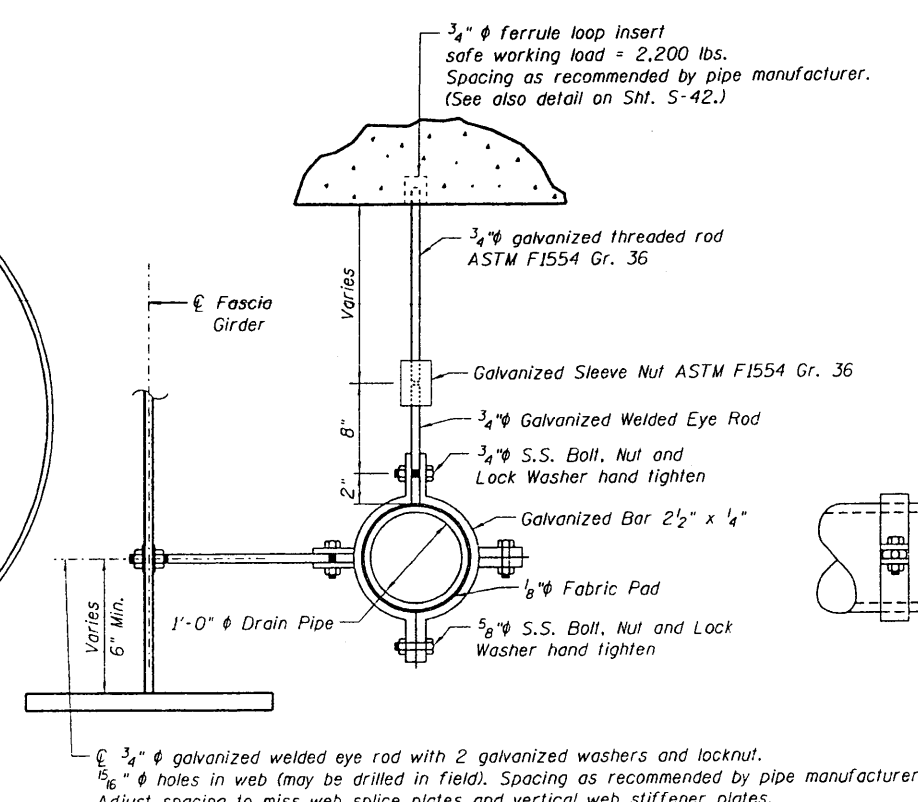
ELEVATION

**DETAIL A - PIPE CLAMP DETAIL**  
(Use to support horizontal pipe runs along pier cap and vertical pipe runs along existing pier wall and abutment face.)

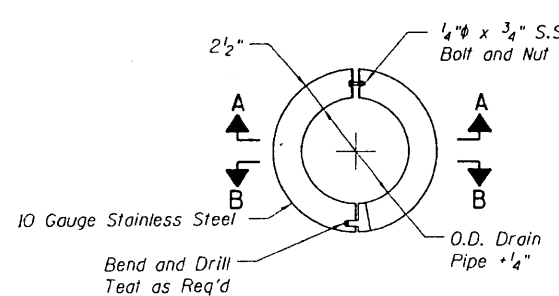
**NOTE:**  
All pipe hangers, supports and hardware shall be hot-dipped galvanized in accordance with AASHTO M232 (ASTM A153) unless otherwise noted. All bolts, nuts and washers shall be stainless steel. Stainless steel bolts shall conform to the requirements of ASTM A 193M (A193), Class 1, ASTM F593, TYPE 304 Grade B8. Stainless steel nuts shall conform to the requirements of AASHTO M 292, ASTM F594, TYPE 304 Grade B or BF, and the washers shall conform to ASTM A 240, Type 302 or 304.



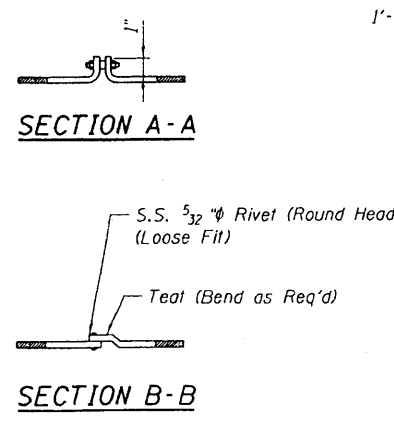
**DETAIL B - PIPE SUPPORT DETAIL**  
(Use to support Vertical Pipe runs along Column Piers)



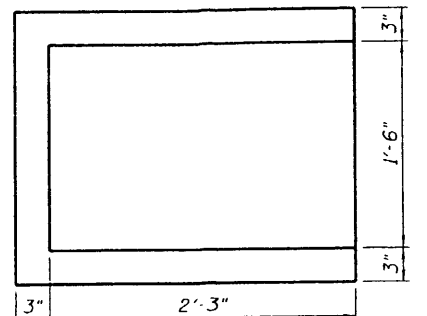
**TYPICAL SECTION**  
**DETAIL D - PIPE HANGER DETAILS**  
(Use similar pipe clamp at horizontal supports.)



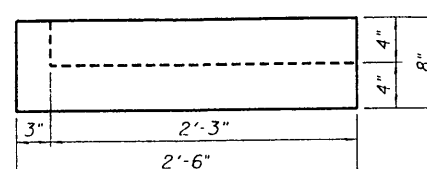
PLAN  
(Looking Down)



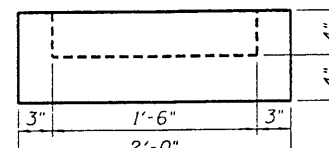
**EXPANSION COLLAR DETAIL**



PLAN

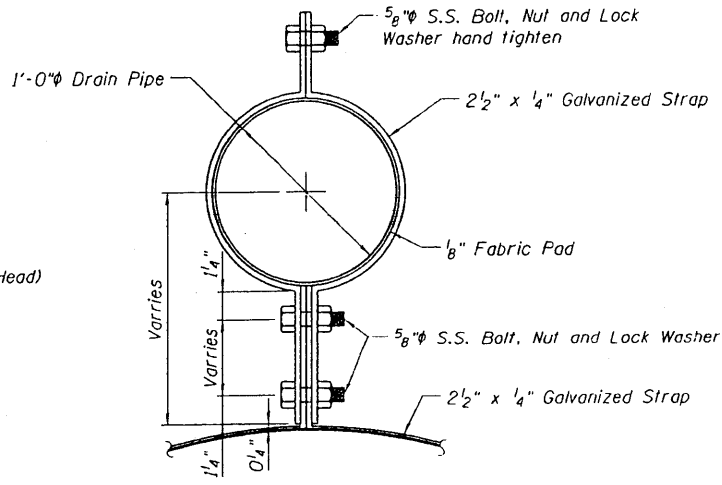


ELEVATION



END VIEW

**SPLASH BLOCK DETAIL**



DETAIL C

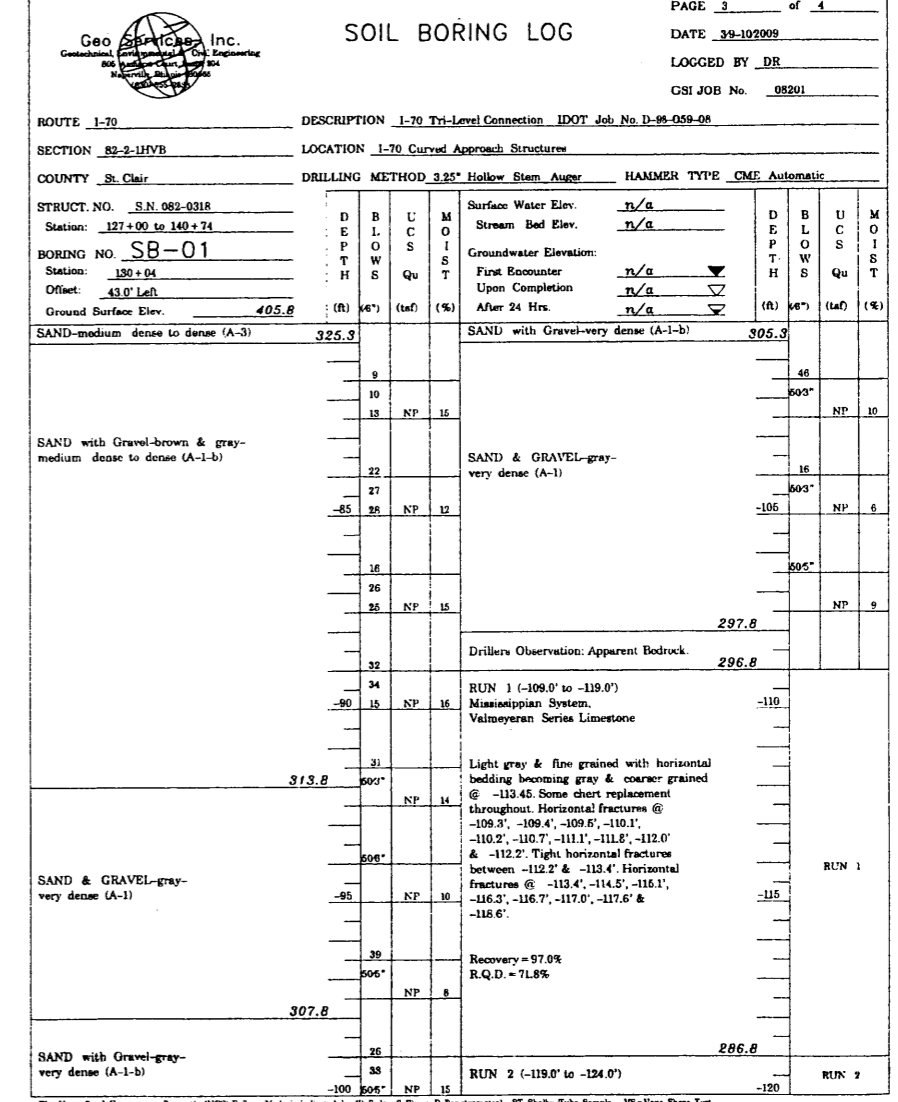
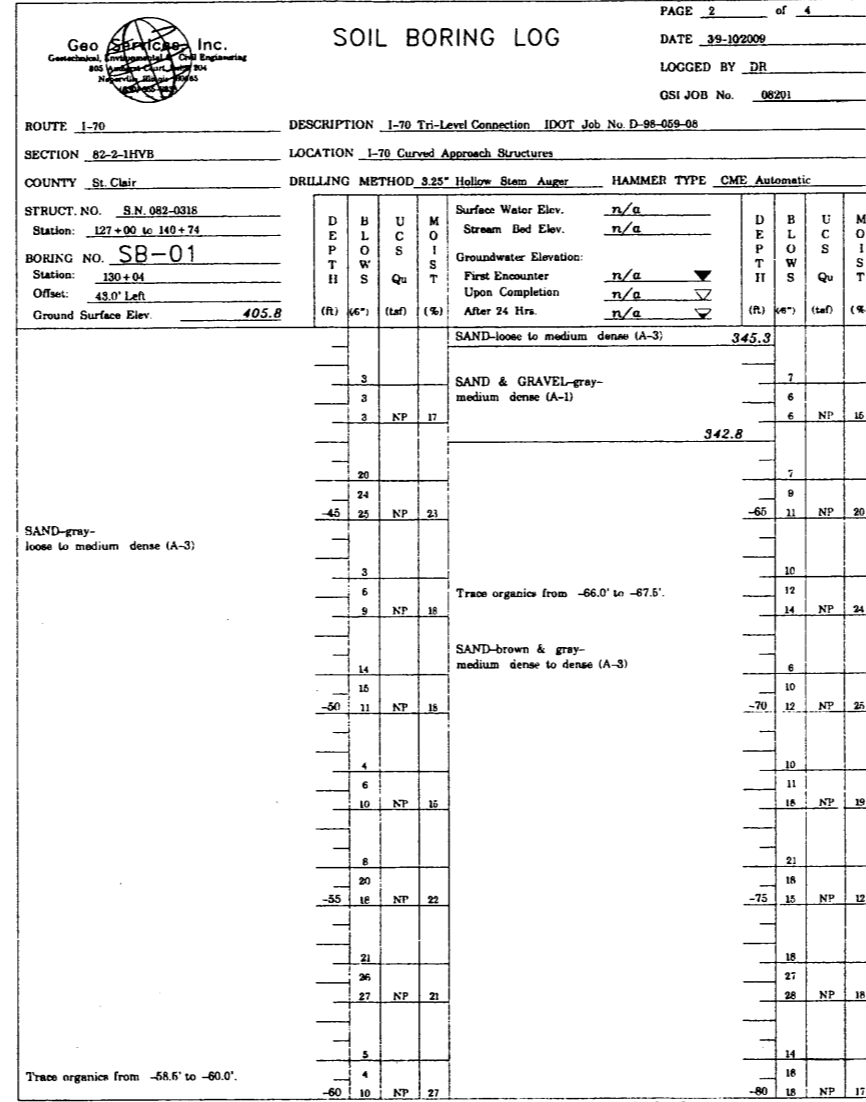
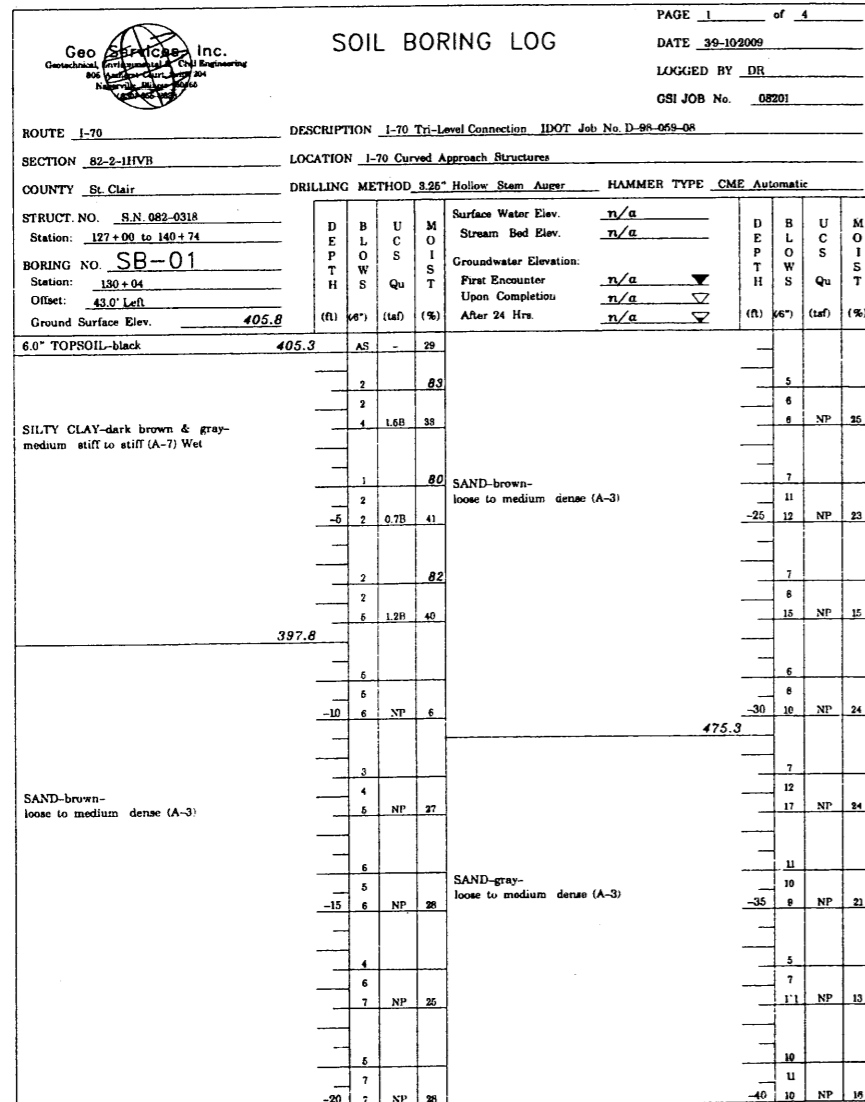
FILE NAME: USER NAME: DESIGNED - TKL REVISED - DRAWN - CPR REVISED - CHECKED - TCU REVISED - DATE - 06/04/10 REVISED -  
 TENG & ASSOCIATES, INC. ENGINEERS/ARCHITECTS/PLANNERS CHICAGO, ILLINOIS  
 STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION BRIDGE DRAINAGE SYSTEM DETAILS  
 SN 082-0318 (EB) & 0319 (WB) CONTRACT NO. 76C44  
 FED. ROAD DIST. NO. ILLINOIS FED. AID PROJECT

FILE NAME:	USER NAME:	DESIGNED - TKL	REVISED -	STATE OF ILLINOIS		BRIDGE DRAINAGE SYSTEM DETAILS		F.A.P. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
FILE #		DRAWN - CPR	REVISED -	DEPARTMENT OF TRANSPORTATION				998	B2-2-1HVB	ST. CLAIR	285	201
PLOT SCALE: #SCALE#		CHECKED - TCU	REVISED -	1-70 CONNECTION OVER				SN 082-0318 (EB) & 0319 (WB) CONTRACT NO. 76C44				
PLOT DATE: #DATE#		DATE - 06/04/10	REVISED -	NS, TRRA, MCT AND INDUSTRIAL DR.		SCALE:		FED. ROAD DIST. NO. ILLINOIS FED. AID PROJECT				
						SHEET NO. S-91 OF S-11		STA. 134+22.00 TO STA.				

SB-01

SB-01

SB-01



FILE NAME: \S:\082-0318-CONV-05-018-MS.DGN... USER: B0820318-CONV-05-018-MS.DGN... DATE: 06/04/10

TENG & ASSOCIATES, INC. ENGINEERS/ARCHITECTS/PLANNERS CHICAGO, ILLINOIS

STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION 1-70 CONNECTION OVER NS, TRRA, MCT AND INDUSTRIAL DR.

SOIL BORING LOGS 1 OF 20

F.A.P. RTE. 998 SECTION 82-2-1HVB COUNTY ST. CLAIR TOTAL SHEET SHEETS NO. 285 202

SN 082-0318 (EB) & 0319 (WB) CONTRACT NO. 76C44

SCALE: SHEET NO. S-92 OF S-111 STA. 134+22.00 TO STA.















# SB-04 Run-2

# SB-05

# SB-05

PAGE 2 of 2

**ROCK CORE LOG**

Geo Services Inc.  
Geotechnical Engineering & Construction  
800 Madison Street, Suite 204  
Naperville, Illinois 60563

DATE 3/2/2009  
LOGGED BY DR  
GSI JOB No. 08201

ROUTE 1-70 DESCRIPTION 1-70 Tri-Level Connection IDOT Job No. D-98-059-08  
SECTION 82-2-IHVB LOCATION 1-70 Curved Approach Structures  
COUNTY St. Clair CORING METHOD Rotary Wash

STRUCT. NO. S.N. 082-0318 CORING BARREL TYPE & SIZE NX Double Swivel-5 R  
Station: 127+00 to 140+74 Core Diameter 2.0 in  
BORING NO. SB-04 Top of Rock Elev. 301.2  
Station: 132+64 Begin Core Elev. 299.7  
Offset: 43.0' Right  
Ground Surface Elev. 403.7

DEPTH (ft)	DESCRIPTION	UCS (psi)	Failure Mode	Notes
289.7	MISSISSIPPIAN SYSTEM, VALMEYERAN SERIES LIMESTONE RUN 2 (-114.0' to -119.0')	2	100.0	59.0
Light gray & fine grained with horizontal bedding becoming gray & sandy @ -114.5'. Some tight vertical fractures & chert replacement throughout. Horizontal fractures @ -114.1', -114.5', -115.0', -115.2', -115.7', -116.3', -116.9', -117.1', -117.5', -117.6', -118.1', -118.3' & -118.8'.				
-119.0				

Color pictures of the cores  Yes. Cores will be stored for examination for the "Strength" column represents the uniaxial compressive strength of the core sample (ASTM D-2938)

PAGE 1 of 4

**SOIL BORING LOG**

Geo Services Inc.  
Geotechnical Engineering & Construction  
800 Madison Street, Suite 204  
Naperville, Illinois 60563

DATE 3/30/2009  
LOGGED BY DR  
GSI JOB No. 08201

ROUTE 1-70 DESCRIPTION 1-70 Tri-Level Connection IDOT Job No. D-98-059-08  
SECTION 82-2-IHVB LOCATION 1-70 Curved Approach Structures  
COUNTY St. Clair DRILLING METHOD 3.25" Hollow Stem Auger HAMMER TYPE CME Automatic

STRUCT. NO. S.N. 082-0318  
Station: 127+00 to 140+74  
BORING NO. SB-05  
Station: 135+64  
Offset: 43.0' Left  
Ground Surface Elev. 403.8

DEPTH (ft)	DESCRIPTION	UCS (psi)	Failure Mode	Notes
402.8	SANDY LOAM with Cinders-black (F31)	AS	NP	32
400.8	TOPSOIL-black (A-7)	2	NP	50
	SAND-brown-medium dense (A-3)			
	LOAM-brown-loose (A-4)			
395.3				
	SILT LOAM-brown-very loose (A-4)			
	SAND-brown-medium dense (A-3)			
	SAND-dark gray to gray-medium dense to dense (A-3)			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Parasitic), ST-Shallow Tube Sample, VB-Vane Shear Test. The SPT (N value) is the sum of the last two blow values in each sampling zone (ASTM D-1586). The Unit Dry Weight (pcf) is noted in italics above each (S). NR-No Recovery.

PAGE 2 of 4

**SOIL BORING LOG**

Geo Services Inc.  
Geotechnical Engineering & Construction  
800 Madison Street, Suite 204  
Naperville, Illinois 60563

DATE 3/30/2009  
LOGGED BY DR  
GSI JOB No. 08201

ROUTE 1-70 DESCRIPTION 1-70 Tri-Level Connection IDOT Job No. D-98-059-08  
SECTION 82-2-IHVB LOCATION 1-70 Curved Approach Structures  
COUNTY St. Clair DRILLING METHOD 3.25" Hollow Stem Auger HAMMER TYPE CME Automatic

STRUCT. NO. S.N. 082-0318  
Station: 127+00 to 140+74  
BORING NO. SB-05  
Station: 135+64  
Offset: 43.0' Left  
Ground Surface Elev. 403.8

DEPTH (ft)	DESCRIPTION	UCS (psi)	Failure Mode	Notes
343.3	SAND-medium dense to dense (A-3)			
	SAND with Gravel-brown & gray-loose to medium dense (A-1-b)			
338.3				
	SAND-brown & gray-medium dense to very dense (A-3)			
328.3				
	SAND with Gravel-brown & gray-medium dense (A-1-b)			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Parasitic), ST-Shallow Tube Sample, VS-Vane Shear Test. The SPT (N value) is the sum of the last two blow values in each sampling zone (ASTM D-1586). The Unit Dry Weight (pcf) is noted in italics above each (S). NR-No Recovery.

\082018 CONN-05-010-HS.DGN, \082018 CONN-05-018-HS.DGN, \082018 CONN-05-021-HS.DGN, \082018 CONN-05-022-HS.DGN, \082018 CONN-05-023-HS.DGN, \082018 CONN-05-024-HS.DGN, \082018 CONN-05-025-HS.DGN, \082018 CONN-05-026-HS.DGN, \082018 CONN-05-027-HS.DGN, \082018 CONN-05-028-HS.DGN, \082018 CONN-05-029-HS.DGN, \082018 CONN-05-030-HS.DGN, \082018 CONN-05-031-HS.DGN, \082018 CONN-05-032-HS.DGN, \082018 CONN-05-033-HS.DGN, \082018 CONN-05-034-HS.DGN, \082018 CONN-05-035-HS.DGN, \082018 CONN-05-036-HS.DGN, \082018 CONN-05-037-HS.DGN, \082018 CONN-05-038-HS.DGN, \082018 CONN-05-039-HS.DGN, \082018 CONN-05-040-HS.DGN, \082018 CONN-05-041-HS.DGN, \082018 CONN-05-042-HS.DGN, \082018 CONN-05-043-HS.DGN, \082018 CONN-05-044-HS.DGN, \082018 CONN-05-045-HS.DGN, \082018 CONN-05-046-HS.DGN, \082018 CONN-05-047-HS.DGN, \082018 CONN-05-048-HS.DGN, \082018 CONN-05-049-HS.DGN, \082018 CONN-05-050-HS.DGN

















# SB-08 Run-3

# SB-08 Run-4

# SB-09

PAGE 2 of 3

**ROCK CORE LOG**

Geo Services Inc. Geotechnical, Environmental & Civil Engineering  
100 Lakeside Drive, Suite 204  
Morton, IL 61550

ROUTE 1-70 DESCRIPTION 1-70 Tri-Level Connection IDOT Job No. D-98-059-08  
SECTION 82-2-IHVB LOCATION 1-70 Curved Approach Structures  
COUNTY St. Clair CORING METHOD Rotary Wash

STRUCT. NO. S.N. 082-0318 CORING BARREL TYPE & SIZE NX Double Swivel-10 ft.  
Station: 127+00 to 140+74 Core Diameter 2.0 in  
BORING NO. SB-08 Top of Rock Elev. 299.0  
Station: 138+34 Begin Core Elev. 300.8  
Offset: 43.0' Right  
Ground Surface Elev. 404.3

DEPTH (ft)	DIAMETER (#)	UNIT WEIGHT (%)	WATER CONTENT (%)	SHRINKAGE (%)	TEMPERATURE (min)	REMARKS (ft)
297.3	3	100.0	34.5	NA	1000	297.3
-112.0						
-117.0						

RUN 3 (-107.0' to -117.0')  
Mississippian System,  
Valmeyeran Series Limestone

Light gray with horizontal bedding. Fine grained with some chert replacement. Numerous horizontal fractures throughout with some thin clay partings.

Color pictures of the cores  Yes. Cores will be stored for examination for  XX  
The "Strength" column represents the uniaxial compressive strength of the core sample (ASTM D-2938)

PAGE 3 of 3

**ROCK CORE LOG**

Geo Services Inc. Geotechnical, Environmental & Civil Engineering  
100 Lakeside Drive, Suite 204  
Morton, IL 61550

ROUTE 1-70 DESCRIPTION 1-70 Tri-Level Connection IDOT Job No. D-98-059-08  
SECTION 82-2-IHVB LOCATION 1-70 Curved Approach Structures  
COUNTY St. Clair CORING METHOD Rotary Wash

STRUCT. NO. S.N. 082-0318 CORING BARREL TYPE & SIZE NX Double Swivel-6 ft.  
Station: 127+00 to 140+74 Core Diameter 2.0 in  
BORING NO. SB-08 Top of Rock Elev. 299.0  
Station: 138+34 Begin Core Elev. 300.8  
Offset: 43.0' Right  
Ground Surface Elev. 404.3

DEPTH (ft)	DIAMETER (#)	UNIT WEIGHT (%)	WATER CONTENT (%)	SHRINKAGE (%)	TEMPERATURE (min)	REMARKS (ft)
287.3	4	91.5	76.0	NA	1000	287.3
-122.0						
-127.0						

RUN 3 (-117.0' to -122.0')  
Mississippian System,  
Valmeyeran Series Limestone

Light gray with horizontal bedding. Fine grained with some chert replacement. Horizontal fractures @ -117.3', -117.4', -117.5', -118.8', -119.0', -120.4', -121.4' & -121.6'.

Color pictures of the cores  Yes. Cores will be stored for examination for  XX  
The "Strength" column represents the uniaxial compressive strength of the core sample (ASTM D-2938)

PAGE 1 of 4

**SOIL BORING LOG**

Geo Services Inc. Geotechnical, Environmental & Civil Engineering  
100 Lakeside Drive, Suite 204  
Morton, IL 61550

ROUTE 1-70 DESCRIPTION 1-70 Tri-Level Connection IDOT Job No. D-98-059-08  
SECTION 82-2-IHVB LOCATION 1-70 Curved Approach Structures  
COUNTY St. Clair DRILLING METHOD 3.25" Hollow Stem Auger HAMMER TYPE CME Automatic

STRUCT. NO. S.N. 082-0318  
Station: 127+00 to 140+74  
BORING NO. SB-09  
Station: 140+74  
Offset: 43.0' Left  
Ground Surface Elev. 406.1

DEPTH (ft)	DIAMETER (#)	UNIT WEIGHT (%)	WATER CONTENT (%)	SHRINKAGE (%)	TEMPERATURE (min)	REMARKS (ft)
405.1	AS	-	39			405.1
2						2
4						4
5	1.25P	40				5
2						2
2						2
-5	2.0P	30				-5
						84
	ST 1.2B	33				
2						2
2						2
-10	3 1.25P	31				-10
						375.6
						14
						12
						11
						11
						17
						4
						8
						-35
						11
						NP
						24
						7
						8
						10
						NP
						18
						10
						16
						NP
						23

TOPSOIL-black

SAND-brown & gray-medium dense (A-3)

SILT CLAY-dark brown-stiff to very stiff (A-7) Wet

Clay seams from -26.0' to -27.5'

SANDY LOAM-brown-very loose (A-2)

SAND-brown & gray-medium dense (A-3)

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B) Bulge, (S) Shear, (P) Fracture, (T) Tensile, (V) Vertical, (H) Horizontal, (C) Compression, (T) Tension, (N) None. The SPT (N) value is the sum of the last two blow values in each sampling zone (ASTM T206). The Unit Dry Weight (pcf) is noted in italics above most (%) values.

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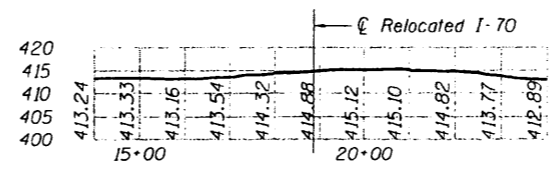
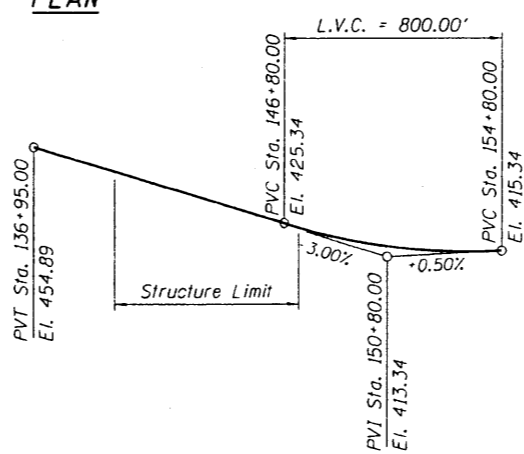
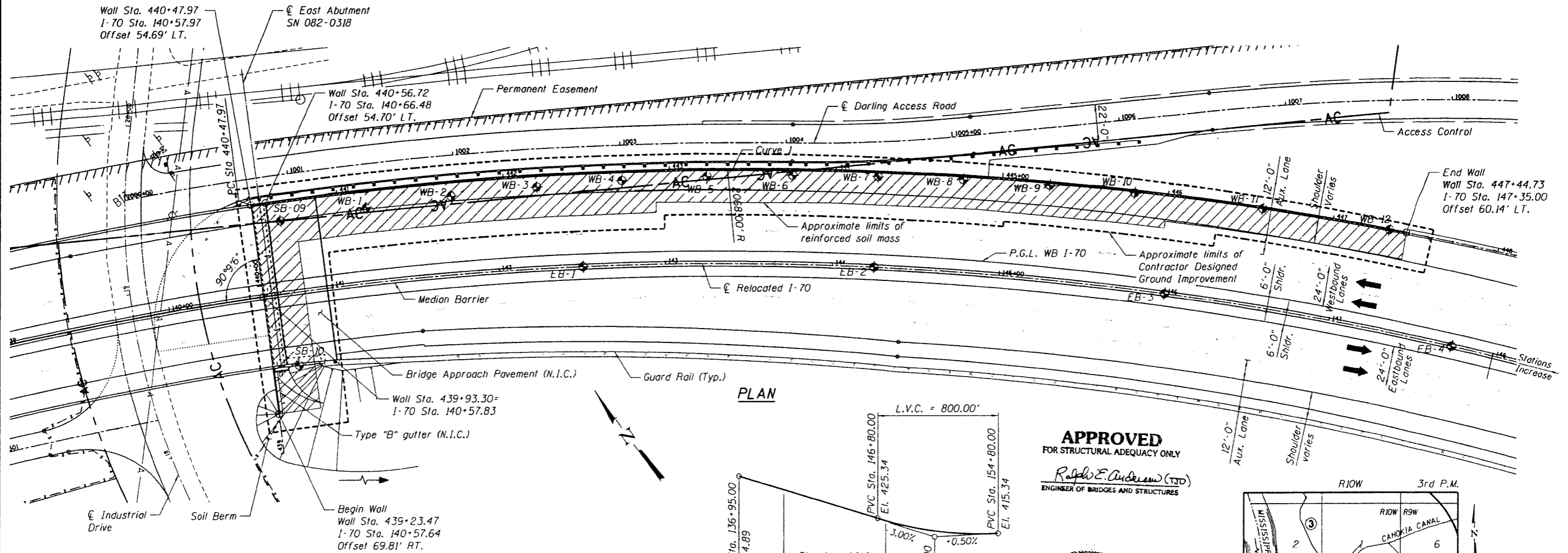




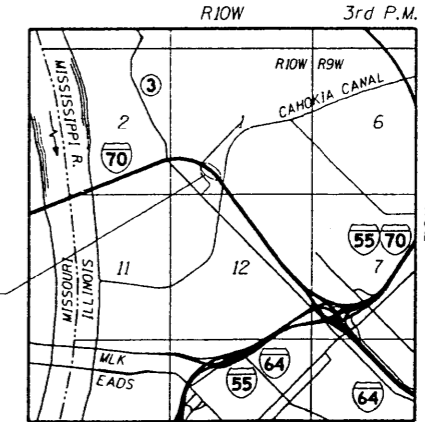




**BENCH MARK:**  
 Monument No. 11: Aluminum disk set in the back of a 4.5' concrete walk (end of walk), located on the west side of Illinois Route 3 approximately 0.3 miles south of Canal Street (Brooklyn). El. 414.02



**APPROVED**  
 FOR STRUCTURAL ADEQUACY ONLY  
*Ralph E. Anderson* (TJ)  
 ENGINEER OF BRIDGES AND STRUCTURES



- Notes:**
- Stations and offsets are measured from the Centerline Relocated I-70 to the front face of the MSE wall panels.
  - MSE Wall to be constructed in this Contract. Parapet, Moment Slab, Wall Coping, Approach Pavement and Roadway to be constructed in later Contract.
  - Design of the wall shall include consideration of seismic force effects. Under the 1000-year seismic demand, the performance objective is uninterrupted use of the supported roadway. Wall displacements shall thus be limited to effectively "undamaged" levels. Under the 2500-year seismic demand, the performance objective is availability of the supported roadway to emergency services vehicles (only). Large wall displacements and significant local damage is permissible, but large-scale collapse shall be prevented.

**DESIGN SPECIFICATIONS**

2002 AASHTO Standard Specifications for Highway Bridges, 17th Edition

**DESIGN STRESSES**

**FIELD UNITS**

$f'_c = 3,500$  psi  
 $f_y = 60,000$  psi (Reinforcement)

**PRECAST UNITS**

$f'_c = 4,500$  psi (Precast Panels)

**SEISMIC DATA \***

Soil Site Class = D		
Return Period, $T_r$ [yrs]	1000	2500
Modified Peak Ground Acceleration, $A_s$ [g]	0.20	0.26
Importance Category	Critical	Essential
Seismic Performance Zone	2	2

\* Seismic Data based on site-specific analysis.

**CURVE DATA - WALL CURVE 1**

PI Sta. 444+33.90  
 $\Delta = 21^\circ 08' 30''$  (RT)  
 $D = 2^\circ 46' 14''$   
 $R = 2,068.00'$   
 $L = 763.07'$   
 $T = 385.92'$   
 $E = 35.70'$   
 $SE = N/A$   
 PC Sta. 440+47.97  
 PT Sta. 448+11.04

**RELOCATED I-70 CURVE 17003**

PI Sta. = 138+29.72  
 $\Delta = 74^\circ 40' 52''$  (RT)  
 $D = 2^\circ 56' 04''$   
 $R = 1,952.50'$   
 $T = 1,489.60'$   
 $L = 2,544.95'$   
 $E = 503.34'$   
 $SE = 5.40\%$   
 PC Sta. = 123+40.13  
 PT Sta. = 148+85.08

**INDEX OF SHEETS**

- W-1 MSE Wall Plan
- W-2 MSE Wall Elevation
- W-3 MSE Wall Details
- W-4 to W-14 Soil Boring Logs 1 to 14

**LEGEND:**

- Soil Boring
- Ditch

**BILL OF MATERIAL**

Item	Unit	Total
MSE Wall	Sq. Ft.	18,598
Contractor Designed Ground Improvement	L. Sum	1

**MSE WALL PLAN**

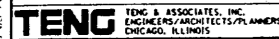
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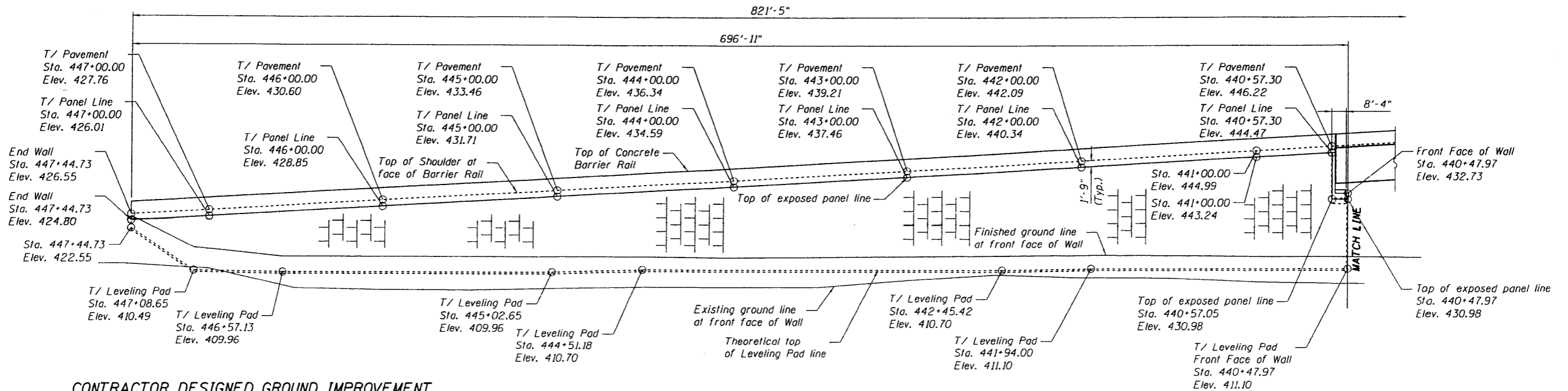
STATE OF ILLINOIS  
 DEPARTMENT OF TRANSPORTATION  
 I-70 CONNECTION  
 RETAINING WALL

F.A.P. RITE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
998	82-2-1HV8	ST. CLAIR	285	222
SN 082-W234		CONTRACT NO. 76C44		
FED. ROAD DIST. NO. ILLINOIS FED. AID PROJECT				

FILE NAME	USER NAME	DESIGNED	REVISION
TENG & ASSOCIATES, INC.	HLUSER	JLR	
ENGINEERS/ARCHITECTS/PLANNERS		HDJ	
CHICAGO, ILLINOIS		TCU	

DRAWN	CHECKED	DATE	REVISION
HDJ	TCU	06/04/10	

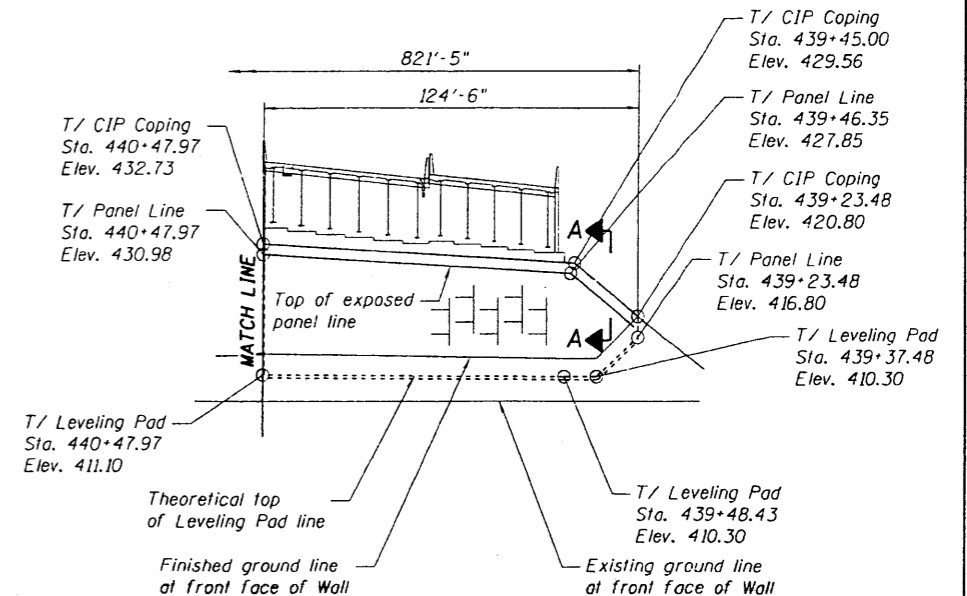




**CONTRACTOR DESIGNED GROUND IMPROVEMENT PERFORMANCE CRITERIA**

MSE Wall Station	Bearing	Maximum Settlement		Stability - Static		Global Stability - Dynamic		
		Bearing Demand [ksf]	at Tc • 3 month [In]	at Tc • 1 year [In]	Factor of Safety Required		Factor of Safety Required	
					Sliding	Global	Tr = 1000 yr	Tr = 2500 yr
439+23	4.0	2	3	1.5	1.5	1.0	1.0	
439+50	6.0	2	3	1.5	1.5	1.0	1.0*	
440+23	6.0	2	3	1.5	1.5	1.0	1.0*	
441+23	6.0	2	3	1.5	1.5	1.0	1.0	
443+70	5.0	2	3	1.5	1.5	1.0	1.0	
445+70	4.5	2	3	1.5	1.5	1.0	1.0	
447+50	4.0	2	3	1.5	1.5	1.0	1.0	

**ELEVATION**  
(Looking South)



**ELEVATION**  
(Looking East)

**Bearing**

Bearing demand is the unfactored, static, equivalent uniform demand acting at T/Leveling Pad. Bearing demand includes the envelope of dead load, live load and potential downdrag associated with settlement of adjacent unreinforced embankment acting on an MSE wall of assumed typical proportions. The improved ground shall provide factor of safety = 2.5, calculated as Nominal Bearing Capacity / Bearing Demand.

**Settlement**

Settlement shall be measured at T/Leveling pad, and referred to a reference elevation taken prior to placement of wall panels. Tc shall be the time of completion of the MSE wall fill.

**Stability - Static**

Factor of safety calculations shall be based on an assumed MSE wall design of typical proportions. Factor of safety for global stability shall be based on the envelope of trial and error solution of feasible sliding block and rotating wedge failure surfaces.

**Liquefaction**

Liquefaction analyses reflecting the presence of increased vertical stress due to the proposed wall have been performed and are reported in the Structure Geotechnical Reports for the Darling Spur Wall (SN 082-W234) and the I-70 Connector Bridge (SN 082-0318 and -0319). Mitigation of liquefaction occurrence is not a performance criteria for Contractor Designed Ground Improvement. The occurrence and hazard associated with liquefaction is recognized through performance criteria on global stability which include the effects of predicted liquefaction.

**Stability - Dynamic**

Factor of safety calculation shall be based on an assumed MSE wall design of typical proportions. Factor of safety for global stability shall be based on the envelope of trial and error solution of feasible sliding block and rotating wedge failure surfaces.

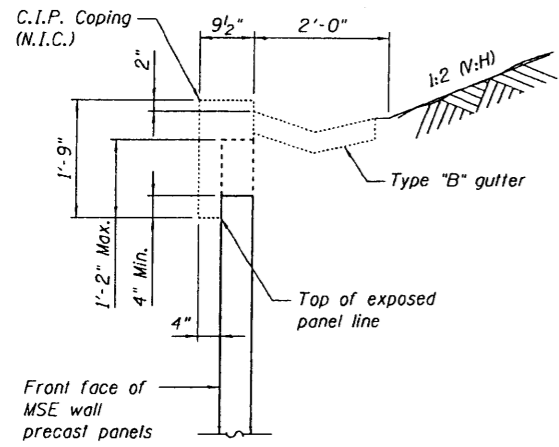
Factor of safety calculations for global stability shall:

- be based on the envelope of trial and error solution of feasible sliding block and rotating wedge failure surfaces.
- reflect a driving inertial force from acceleration equal to 75% of the Modified Peak Ground Acceleration  $A_s$ .
- include reduced soil properties to represent liquefaction for the return periods, locations, and depths at which it is indicated in the Structure Geotechnical Reports for the Darling Spur Retaining Wall and the MRB Connector Bridge.

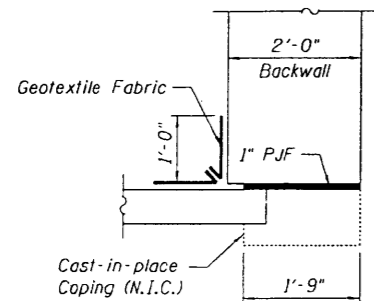
\* For the 2500-year event (only), the stability calculation for sections cut through the abutment may consider a stabilizing contribution from the bridge abutment foundation. The design of these foundations has included an allowance for delivering a restoring shear force of 16.5 kips per foot of wall on an assumed failure plane which intersects the foundations at elevation 392'.

FILE NAME: \\B022214-COM-05-083-PC.DWG, USER: B022214-COM-05-083-PC, DATE: 06/04/10  
 SHEET NO.: 223 OF 285  
 PROJECT: I-70 CONNECTION RETAINING WALL  
 CONTRACT NO.: 16C44

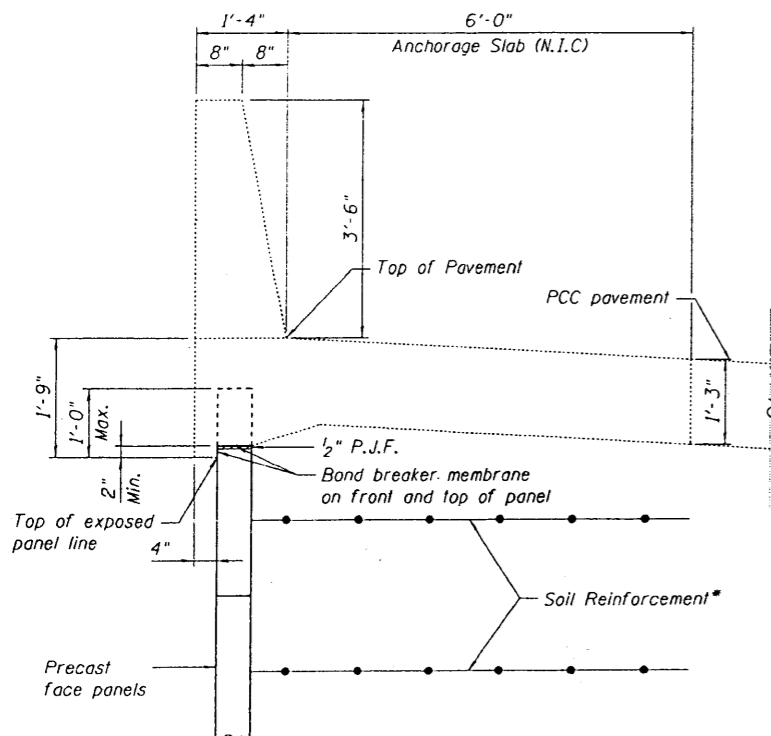
FILE NAME: \\B022214-COM-05-083-PC.DWG	USER: B022214-COM-05-083-PC	DESIGNED: TCG	REVISED:	<b>STATE OF ILLINOIS</b> <b>DEPARTMENT OF TRANSPORTATION</b> I-70 CONNECTION RETAINING WALL	<b>MSE WALL ELEVATION</b>	F.A.P. RTE. 998	SECTION 82-2-1HVB	COUNTY ST. CLAIR	TOTAL SHEETS 285	SHEET NO. 223	
TENG & ASSOCIATES, INC.	PLOT SCALE: #SCALE#	CHECKED: TCU	REVISED:			SCALE: NTS	SHEET NO. W-2 OF W-14	STA. 140+57.64 TO STA. 147+35.00	SN 082-W234 ILLINOIS FED. AID PROJECT		
ENGINEERS/ARCHITECTS/PLANNERS/CONSULTANTS	PLOT DATE: #DATE#	DATE: 06/04/10	REVISED:								
CHICAGO, ILLINOIS											



**SECTION A-A**

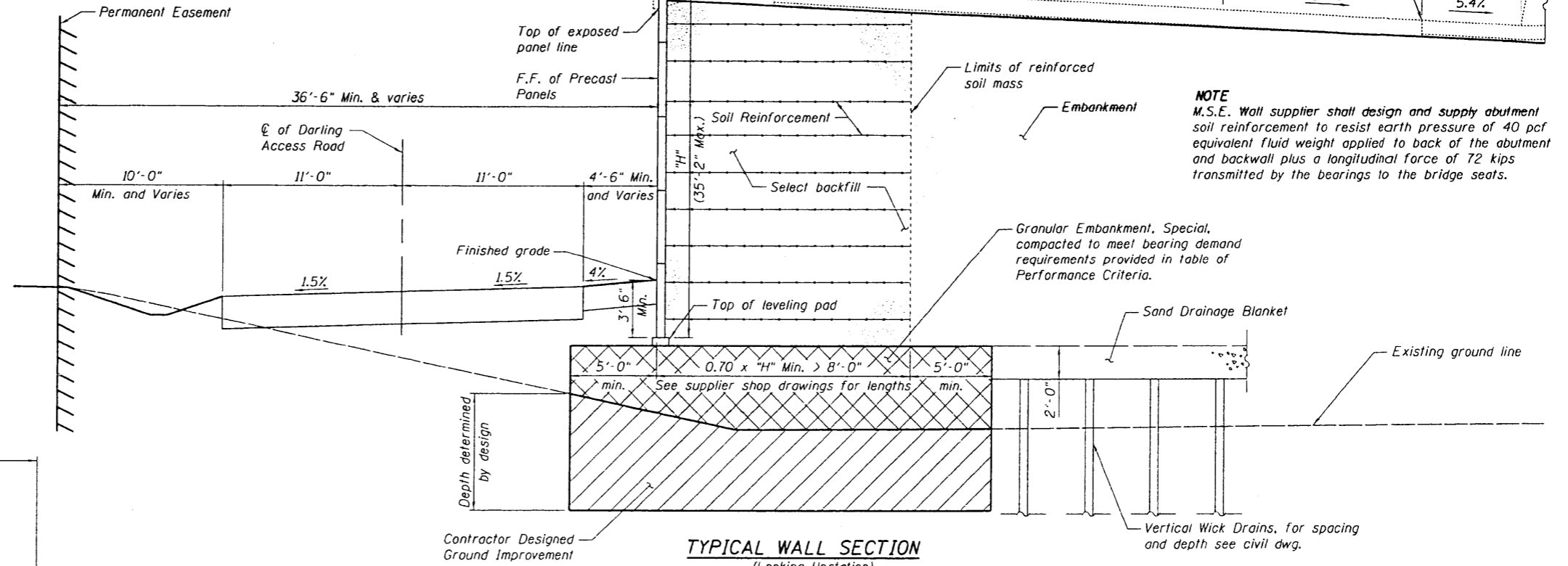


**SECTION B-B**



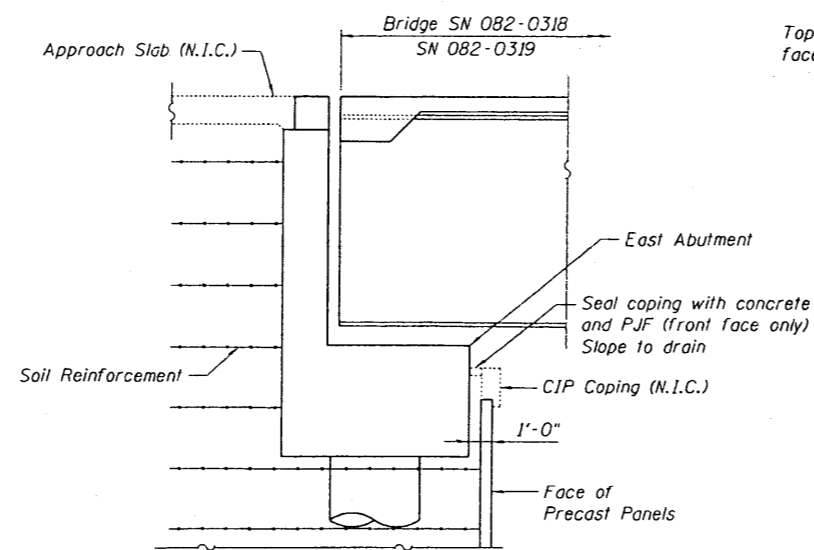
**SECTION THROUGH ANCHORAGE SLAB**

\*The M.S.E. wall supplier's internal stability design shall account for the anchorage slab's bearing pressure surcharge of 0.24 ksf and horizontal sliding force of 0.5 kip/ft of wall

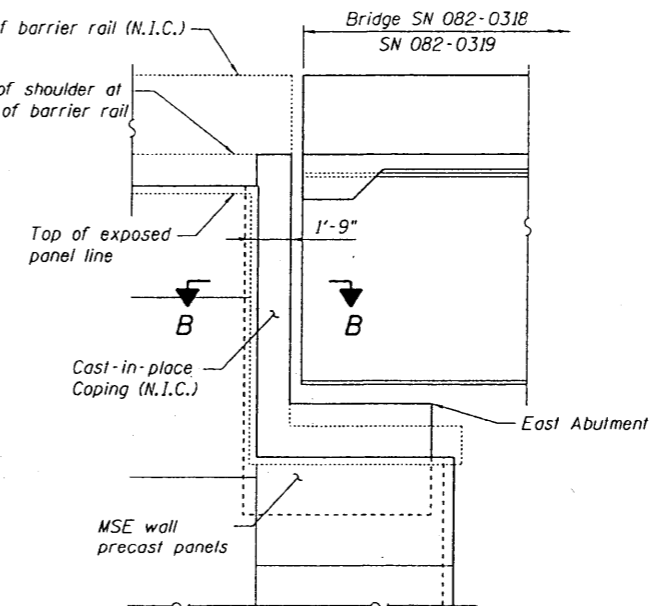


**TYPICAL WALL SECTION**  
(Looking Upstation)

**NOTE**  
M.S.E. Wall supplier shall design and supply abutment soil reinforcement to resist earth pressure of 40 pcf equivalent fluid weight applied to back of the abutment and backwall plus a longitudinal force of 72 kips transmitted by the bearings to the bridge seats.



**SECTION THROUGH ABUTMENT**  
(Looking South)



**COPING DETAIL AT ABUTMENT**  
(Looking South)

**NOTE:**  
N.I.C. indicates Not In Contract. The items constructed in a later contract include Bridge Approach Slab, cast-in-place coping for MSE Wall, anchorage slab and parapet on MSE Wall, and concrete gutter adjacent to coping.

FILE NAME: ... USER NAME: #USER# ... DESIGNED: ... REVISIONS: ... DRAWN: TCG ... CHECKED: TCU ... DATE: 06/04/10 ...  
 TENG & ASSOCIATES, INC. ENGINEERS/ARCHITECTS/PLANNERS CHICAGO, ILLINOIS  
 STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION I-70 CONNECTION RETAINING WALL  
 F.A.P. RTE. 998 SECTION B2-2-1HVB COUNTY ST. CLAIR TOTAL SHEETS 285 SHEET NO. 224  
 SN 082-W234 CONTRACT NO. 76C44  
 SCALE: NTS SHEET NO. W-3 OF W-14 STA. 140+57.64 TO STA. 147+35.00 FED. ROAD DIST. NO. ILLINOIS FED. AID PROJECT





WB-05

WB-06

WB-06

Geo SPT/Cas Inc. SOIL BORING LOG PAGE 2 of 2 DATE 7/23/2009 LOGGED BY MR GSI JOB No. 08201

ROUTE I-70 DESCRIPTION I-70 Tri-Level Connection IDOT Job No. D-88-058-08 SECTION XX LOCATION I-70 Curved Approach Structure-Retaining Wall COUNTY St. Clair DRILLING METHODS Straight Flight Auger Rotary HAMMER TYPE Diedrich Automatic

STRUCT. NO. XX Station: 140+70 to 147+35 BORING NO. WB-05 Station: 143+75 Offset: 51.5' Left Ground Surface Elev. 405.7

DEPTH (ft)	SOIL DESCRIPTION	DRILLING METHOD	REMARKS	DEPTH (ft)	SOIL DESCRIPTION	DRILLING METHOD	REMARKS
0	SAND-brown-medium dense (A-3)	XX		0	SAND-brown-medium dense (A-3)	XX	
2				2			
4				4			
6				6			
8				8			
10				10			
12				12			
14				14			
16				16			
18				18			
20				20			
22				22			
24				24			
26				26			
28				28			
30				30			
32				32			
34				34			
36				36			
38				38			
40				40			
42				42			
44				44			
46				46			
48				48			
50				50			
52				52			
54				54			
56				56			
58				58			
60				60			

Geo SPT/Cas Inc. SOIL BORING LOG PAGE 1 of 2 DATE 7/23/2009 LOGGED BY MR GSI JOB No. 08201

ROUTE I-70 DESCRIPTION I-70 Tri-Level Connection IDOT Job No. D-88-058-08 SECTION XX LOCATION I-70 Curved Approach Structure-Retaining Wall COUNTY St. Clair DRILLING METHODS Straight Flight Auger Rotary HAMMER TYPE Diedrich Automatic

STRUCT. NO. XX Station: 140+70 to 147+35 BORING NO. WB-06 Station: 143+75 Offset: 52.5' Left Ground Surface Elev. 405.8

DEPTH (ft)	SOIL DESCRIPTION	DRILLING METHOD	REMARKS	DEPTH (ft)	SOIL DESCRIPTION	DRILLING METHOD	REMARKS
0	TOPSOIL-black	XX		0	SAND-loose to medium dense (A-3)	XX	
2				2			
4				4			
6				6			
8				8			
10				10			
12				12			
14				14			
16				16			
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60				60			

Geo SPT/Cas Inc. SOIL BORING LOG PAGE 2 of 2 DATE 7/23/2009 LOGGED BY MR GSI JOB No. 08201

ROUTE I-70 DESCRIPTION I-70 Tri-Level Connection IDOT Job No. D-88-058-08 SECTION XX LOCATION I-70 Curved Approach Structure-Retaining Wall COUNTY St. Clair DRILLING METHODS Straight Flight Auger Rotary HAMMER TYPE Diedrich Automatic

STRUCT. NO. XX Station: 140+70 to 147+35 BORING NO. WB-06 Station: 143+75 Offset: 52.5' Left Ground Surface Elev. 405.8

DEPTH (ft)	SOIL DESCRIPTION	DRILLING METHOD	REMARKS	DEPTH (ft)	SOIL DESCRIPTION	DRILLING METHOD	REMARKS
0	SAND-brown-medium dense to dense (A-3)	XX		0	SAND-brown-medium dense to dense (A-3)	XX	
2				2			
4				4			
6				6			
8				8			
10				10			
12				12			
14				14			
16				16			
18				18			
20				20			
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