

Structure Geotechnical Report

PTB 196-017 Work Order 7

FAI 55 (Interstate Route 55)

I-55 Frontage Roads – Culvert Ends Replacement
North and South Frontage Roads over Sawmill Creek

SN 022-0513

DuPage County

Section 2021-068-CR

Contract 62P06

Prepared For:



**Illinois Department
of Transportation**

Submitted: July 28, 2022

Submitted By:

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Testing • Inspection • Training • Consulting • Research • Geotechnical

July 28, 2022

Mr. Giancarlo Gierbolini, P.E.
District One Geotechnical Engineer
Illinois Department of Transportation
Region 1/District 1
201 West Center Court
Schaumburg, IL 60196-1096

Re: Structure Geotechnical Report
I-55 Frontage Roads – Culvert Ends Replacement
North and South Frontage Roads over Sawmill Creek
SN 022-0513
Section: 2021-068-CR
Contract: 62P06
PTB: 196/017 (WO 7)

CTL Project Number 22F761

Dear Mr. Gierbolini,

Enclosed are the results of the subsurface exploration and geotechnical engineering evaluation for the above referenced project. The report provides a description of the site investigation, site condition and analysis and recommendations for the proposed culvert ends reconstruction. The site investigation included advancing four (4) soil borings to depths of 30 feet below ground surface (bgs).

Chicago Testing Laboratory, Inc. (CTL) appreciates the opportunity to work with you on this project and look forward to serving as your Geotechnical Engineering Consultant on future projects. We would be pleased to discuss any questions you have about the contents of this report.

Respectfully Submitted,

CHICAGO TESTING LABORATORY, INC.

Riyad Wahab, Ph.D., P.E.
Senior Geotechnical Engineer

Jeffrey Rothamer, P.E.
Director of Technical Services



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1.0 Introduction

Chicago Testing Laboratory, Inc. (CTL) completed a geotechnical engineering analysis for the proposed culvert extensions, which include replacement of the north and south ends of the existing box culvert (SN 022-0513) carrying Sawmill Creek under I-55 and the frontage roads. The project is located on Interstate Route 55 (I-55) North and South Frontage Roads at the crossing with Sawmill Creek in DuPage County (see Appendix A - Site Location Map). The objective and scope of the subsurface exploration and geotechnical analysis were to characterize the subsurface soil conditions in order to provide information regarding the physical characteristics and engineering properties of the subsurface soils, and to provide geotechnical recommendations regarding the design and construction of the proposed improvement.

1.1 Project Information

Based on the preliminary General Plan & Section (Appendix D, undated) provided by Mr. Robert Claussen of District 1, the limits of the culvert replacement are north and south of I-55, extending only under the north and south frontage roads. The proposed project will include removing and replacing the existing culvert ends at Sawmill Creek. The existing culvert has end opening dimension of 12 foot by 5 foot and a length of approximately 360 feet. The proposed culvert ends' openings will match the existing openings' dimensions, with the south end invert elevation of 681.42 feet MSL and the north end invert elevation of 683.72 feet MSL. Wing walls are proposed at the north and south ends. Also, based on the "Culvert Inspection Tech Memo" (dated 3/3/2016), by Ciorba Group Consulting Engineers (Ciorba Group), the new culvert replacements will be connected to the existing culvert with settlement collars to prevent any future cracking due to settlement.

There are two proposed retaining walls, one on the north end of the culvert and one on the south end. The north retaining wall will extend from the culvert to approximately 150 feet east of the culvert. The south retaining wall will extend from the culvert to approximately 150 feet west of the culvert. Both walls will a maximum exposed height of approximately 6 feet. As directed by the district, the two walls will be covered under a separate Technical Memorandum.

2.0 Subsurface Exploration

This section describes the subsurface exploration completed as part of this project. The subsurface investigation program was performed according to IDOT's Geotechnical Manual.

2.1 Subsurface Site Investigation

The subsurface investigation was conducted on June 21, June 22, and July 7, 2022. which included advancing a total of four (4) soil borings to depths of 30 feet bgs within the vicinity of the proposed improvements. The borings were performed on the south and north ends of the proposed culvert replacements (see Appendix A – Boring Location Plan). The boring locations were selected by



CTL and were conducted in the field by Wang Engineering, Inc. (Wang) based on site conditions and accessibility, using 2.25-inch ID hollow stem augers, as stated on the boring logs. Ground surface elevations, stations and offsets of the borings were provided by Wang. Table 1 below presents a summary of the borings completed for the proposed culvert extensions.

Table 1: Summary of Soil Borings

Boring	Station	Offset (ft)	Ground Surface Elevation (ft MSL)	Depth (ft)	Location
SB-3	563+99.57	120.02 RT	688.76	30	EB S Frontage Road
SB-4	564+69.27	66.21 RT	691.44	30	EB I-55 RT Shoulder
SB-5	565+43.75	62.24 LT	691.59	30	WB I-55 LT Shoulder
SB-6	566+45.78	118.26 LT	691.18	30	WB N Frontage Road

Based on the information in the boring logs provided by Wang, it appears that soil sampling was performed using the Standard Penetration Test (SPT, ASTM D 1556). In this procedure, a 2-inch O.D. split barrel or split spoon sampler is driven 18 inches into undisturbed soil using a 30-inch drop of a 140-pound hammer. The number of hammer drops (blow counts) is recorded in 6-inch intervals for each sample collected. The number of blow counts to advance the sampler the final 12 inches is called the SPT “N-value”. The N-values are shown on the Soil Boring Logs in Appendix B. Soil samples were obtained with the split barrel sampler at 2.5-foot intervals to the boring termination depths.

Also, based on the information presented in the boring logs provided by Wang, it is our understand that unconfined compressive strength values (Qu and Qp) were obtained in the field for the cohesive soils encountered during the subsurface investigation, using a calibrated Rimac compressive tester to determine the “Qu” according to IDOT procedure or a calibrated hand penetrometer to determine the “Qp”. The hand penetrometer is typically used when a full-length sample could not be obtained to conduct the Rimac Qu test. Moisture content values for representative soil samples collected from each split spoon sampler are also shown on the boring logs. To verify soil classifications, Atterberg limits and particle size analysis tests were performed on select samples by Wang, Test results are included in Appendix C (Laboratory Test Results).

2.2 General Subsurface Conditions

General subsurface conditions are described below and are grouped based on similar soils encountered throughout the proposed improvements.

Generally, the borings encountered near surface material consisting of 14 inches of asphalt in three borings (except Boring SB-3 with 6 inches of asphalt) underlain by 9 inches of sandy gravel base course (except in SB-3 where it is 6 feet thick). Below the surficial layers, the borings encountered layers of silty clay, silty clay loam and silty loam to the boring termination depths in the four



borings. The strength of these cohesive soil layers varied from medium stiff to very stiff with Q_u values ranging from 0.49 tsf (in one layer, in SB-6) to 6.72 tsf (in one layer, in SB-4).

An intermittent buried topsoil, black silty clay from 1.5 feet to 5 feet thick, was encountered at varying depths of 5.5 feet to 9 feet bgs (Q_u from 0.9 to 2.38 tsf). Also, loose to medium dense saturated sand layers (2.5 feet and 3 feet thick) were encountered at depths of 11 feet and 18 feet bgs, in borings SB-4 and SB-5, respectively. These borings were selected to be as close as possible to the new-existing culvert connections on both ends, as access allows, and thus the sand layers observed on the two borings appear to be close to or below the invert elevations. The particle size analysis tests results shown in Appendix C (Laboratory Test results) generally confirmed the original field soil descriptions, except for a 2.7-ft thick layer encountered at Elevation of 676.1 bgs in boring SB-5, described as stiff gravelly loam. This minor change in soil stratification would not significantly affect the geotechnical analyses and recommendations in this report.

Detailed descriptions of the soil borings are provided in Appendix B (Soil Boring Logs) which provides specific conditions encountered at each soil boring location. The stratifications shown on the soil boring logs represent the conditions only at the actual soil boring locations and represent the approximate boundary between subsurface materials; however, the actual transition may be gradual.

2.3 Groundwater Conditions

Water level measurements were taken in the soil borings when water was encountered while drilling and after the completion of the soil borings. We assume that Wang did not leave any one of the borings open to collect delayed water readings after leaving the site due to safety concerns. Groundwater depths are shown in Table 2 below.

Table 2: Summary of Groundwater Depths (feet bgs)

Soil Boring	While Drilling	At Completion of Drilling
SB-3	Dry	Dry
SB-4	11.30	Dry
SB-5	15.00	Dry
SB-6	10.00	13.5

3.0 Geotechnical Analysis

This section provides the geotechnical analysis for the proposed culvert improvements based on the results of the field exploration and testing.



3.1 Settlement

Based on the culvert ends' replacement dimensions and the proposed 3 feet of fill on top for both the south and north ends and utilizing soil borings SB-4 and SB-5, the estimated settlement is less than 0.5 inches. It should be noted that the actual soils immediately below the proposed replacements are more likely stream sediments that are not represented in the two borings which are drilled at a distance from the stream bed due to difficulty with access.

Although the soils were already consolidated under the existing culvert on both ends, and the anticipate total settlement and the differential settlements between the existing box and replacements would be negligible, District One prefers to use collars as recommended in the Ciorba Group's Tech Memo. However, according to the Culvert Manual, multiple cell precast concrete box culvert replacements may be considered as viable options because of the anticipated small settlements.

3.2 Seismic Parameters

No seismic design is required for box culverts as they are considered buried structures.

3.3 Scour

Although a design scour table is no longer required for culverts, scour should be taken into consideration, and be taken at the bottom of the toe wall. The wingwalls are designed to support and protect the soil slopes adjacent to the culvert from being eroded by scour. It is recommended that riprap or an apron be placed as scour countermeasures at open ends of the culvert.

3.4 Slope Stability

Base on Figure 9 of the Ciorba Group "Tech Memo" dated 3/3/2016, slope failure was observed at the northeast wingwall; however, it is our opinion the figure rather indicates surficial sloughing or erosion than a typical slope failure. According to the Geotechnical Manual, embankment slopes less 15 feet high do not require slope stability analysis. The proposed cross sections at Stations 563+00, 563+50, 566+25 and 566+50 indicate slopes of 1V:1.5H (steeper than the standard 1:2). Based on the strength data in the soil borings, our preliminary stability analyses indicated adequate factors of safety (greater than the minimum required 1.5 for embankment fill). However, we recommend that the standard stepping and benching be followed when placing the new fill over the existing fill to avoid future slope failure. Also, standard, and timely erosion control measures should be constructed over the exposed slopes to avoid sloughing/erosion in the future.

4.0 Geotechnical Recommendations

This section provides the geotechnical recommendations for the proposed improvements based on the results of the subsurface investigation and testing, and geotechnical analysis.



4.1 Retaining Wall Bearing Capacity and Sliding Resistance

Based on the 7/19/2022 email correspondence with Mr. Robert Claussen of District 1, it is our understanding that the wing walls are planned as horizontal cantilever. However, should the design change to non-cantilever walls to be supported on footings, the footings are assumed to be placed at the elevations shown in Table 3 below. The factored bearing resistance was calculated for the strength limit and service limit states using the AASHTO LRFD Bridge Design Specifications. Table 3 provides the recommended bearing capacity and sliding resistance values to use in the footings design.

Table 3: LRFD Bearing Capacity Parameters

Elevation* (feet MSL)	Nominal Bearing Resistance (ksf)	Bearing Resistance Factor	Factored Bearing at Service Limit (ksf)	Factored Sliding Resistance** (ksf)	Anticipated Bearing Soil
S. End 677.59 N. End 679.89	8.00	0.50	4.00	0.57 V***	Stiff to Very Stiff Silty Clay

*Assuming 2-ft thick footings

**Assuming 35-degree friction angle of CA-7 and sliding resistance factor of 0.85

***V = Total Vertical Force, applied at the footing base

A minimum of 12-inch compacted crushed stone (like IDOT CA-7) bed should be constructed below the bottom of the proposed culvert ends and the wingwalls footings (if non-cantilevered wings are selected). Since the south and north ends invert elevations are 681.42 and 683.72, respectively, the bottom of the 12-inch undercut elevations beneath the box would be 679.25 and 681.55, respectively. Similarly, the bottom of the undercut elevations beneath the footings would be 676.59 and 678.89 for the south and north ends, respectively. The 12-inch compacted crushed stone should extend a minimum of 12 inches on each side of the box culvert and footings with a maximum side slope of 1H:1V.

On the south side replacement, low strength soils encountered at Elevation 680.80 in boring SB-3, and it extends below the culvert bearing grade. Therefore, CTL recommends additional undercut on the south end to elevation 678.3 and replacement with rockfill per the Culvert Manual. The exact depths needed after the soils are exposed can be determined in the field according to IDOT Subgrade Stability Manual, using the dynamic cone penetrometer (DCP). The CA-7 stone should be placed to 12 inches above the water table, in 12-inch lifts, and should be compacted with the use of a heavy smooth drum roller or heavy vibratory plate compactor until stable.



4.2 Culvert Headwall and Wingwall Lateral Earth Pressure

The culvert headwalls and the horizontal cantilevered wingwalls should be designed using Table 4.1.1.2-1 of the Culvert Manual, which is based on the “equivalent fluid pressure” outlined in Article 3.11.5.5 (Table 3.11.5.5-1) of AASHTO LRFD Bridge Design Specifications. The values in AASHTO are based on an angle of internal friction of 30 degrees, assuming either zero (flat) backslope or 25-degree backslope. The actual backslope angle should be measured perpendicular to the face of the wall and calculated using the procedure shown in Figure 4.1.1.2-2 of the Culvert Manual.

Based on the soil strength data in soil borings SB-3 and SB-6 close to the south and north end wingwalls, respectively, we recommend using an average 30 degrees friction angle for the backfill material (which is equivalent to an active earth pressure coefficient K_a of 0.33, or an equivalent fluid pressure of 45 pcf) assuming a 25-degree backslope. Based on the cross sections at Stations 563+50 and 564+00, the backslopes vary from 1V:1.5H to 1V:2H for the south end wingwalls, and hence an average backslope of 1V:2H (26 degrees) may be assumed in Figure 4.1.12-2. For the north end wingwalls, a backslope of 1V:1.5H should be used based on the cross sections at Stations 566+50.

5.0 Construction Recommendations

This section provides the construction recommendations for the proposed improvements based on the results of the subsurface investigation and testing, as well as the geotechnical analysis and recommendations. All work performed for the proposed project should conform to the requirements of IDOT Standard Specifications.

5.1 Construction Platform

The proposed culvert ends replacement areas are typically constructed on a streambed with loose, wet sand and silt materials that might extend to several feet below grade, in which case a construction platform (crushed stone) will be necessary for the placement of rebar reinforcement and concrete. The depth of crushed stone (CA-7) might extend below the elevations recommended in Section 4.1 above, depending on the actual field soil condition. The need for construction platform will be determined by the contractor and will not be paid for; however, a geotechnical engineer or a qualified soil inspector can assist with determining the required depth of stone (using the DCP) to ensure a stable platform.

If water seepage occurs during footing construction or where wet conditions are encountered, such that the water cannot be removed with conventional sumping, CTL recommends placing open grade stone like IDOT CA-7 to stabilize the bottom of the excavation below the water table.



5.2 Site Excavation and Temporary Soil Retention

It is our understanding that the north and south frontage roads will be detoured and thus stage construction will not be necessary. Therefore, the 3 feet of fill on top of culvert can be sloped at 1V:2H without the need for a geotextile wall, since there will be no traffic. However, if the excavation on both sides of the box cannot be sloped due to space limitations, temporary sheet piling is feasible based on the soil strength not exceeding 4 tsf in most soil layers (except in two layers where the strength marginally exceeds 4 tsf).

The contractor will be responsible to provide a safe excavation during the construction activities of the project. All excavations should be conducted in accordance with applicable federal, state, and local safety regulations, including, but not limited to the Occupational Safety and Health Administration (OSHA) excavation safety standards. Excavation stability and soil pressures on temporary shoring are dependent on soil conditions, depth of excavations, installation procedures, and the magnitude of any surcharge loads on the ground surface adjacent to the excavation. Excavation near existing structures and underground utilities should be performed with extreme care to avoid undermining existing structures. Excavations should not extend below the level of adjacent existing foundations or utilities unless underpinning or other support is installed. It is the responsibility of the contractor for field determinations of applicable conditions and providing adequate shoring for all excavation activities.

5.3 Groundwater Management

The Culvert Manual (Item 7, page 2-34) requires that the design high-water elevation (at upstream end of culvert) and the estimated water surface elevation (EWSE) be provided in the SGR and to be shown on the TSL plan. However, District 1 indicated that no hydraulic report is available at this time, and thus the ESWE cannot be provided herein to determine if a cofferdam will be needed, or water can be diverted. In a review comment on the draft SGR by District One, it was recommended that the current water flow through the culvert be provided in this report. However, no such observation was made by Wang during the field drilling operations, and thus this information is not available. It is CTL's opinion that the water elevations could be different at the time of construction in which case the current water flow condition would not be useful to determine the method of securing dry construction condition.

The contractor should control groundwater and surface water infiltration to provide a dry condition for construction. Temporary ditches, sumps, granular drainage blankets, stone ditch protection, or hand-laid riprap with geotextile underlayment could be used to divert groundwater if significant seepage is encountered during construction.

6.0 Professional Disclaimer

This report was prepared on the basis of the project information supplied by the client and is intended only for use on this project. This report was prepared by interpreting the data from the



soil borings and field tests made during the field investigation, and from the results of any laboratory tests obtained from the samples taken. The report gives a representative, but not exhaustive, picture of the project subsurface conditions. The geotechnical engineer warrants that the findings, recommendations, specifications, and professional advice given within this report have been prepared using generally accepted professional engineering practices. The recommendations provided in the report are specific to the project described herein and are based on the information obtained from the soil boring locations within the proposed improvements. Changes involving the proposed improvements from those enumerated within this report should be submitted for our review to evaluate our recommendations.

APPENDIX A

SITE LOCATION MAP AND BORING LOCATION PLAN



 **SITE LOCATION**



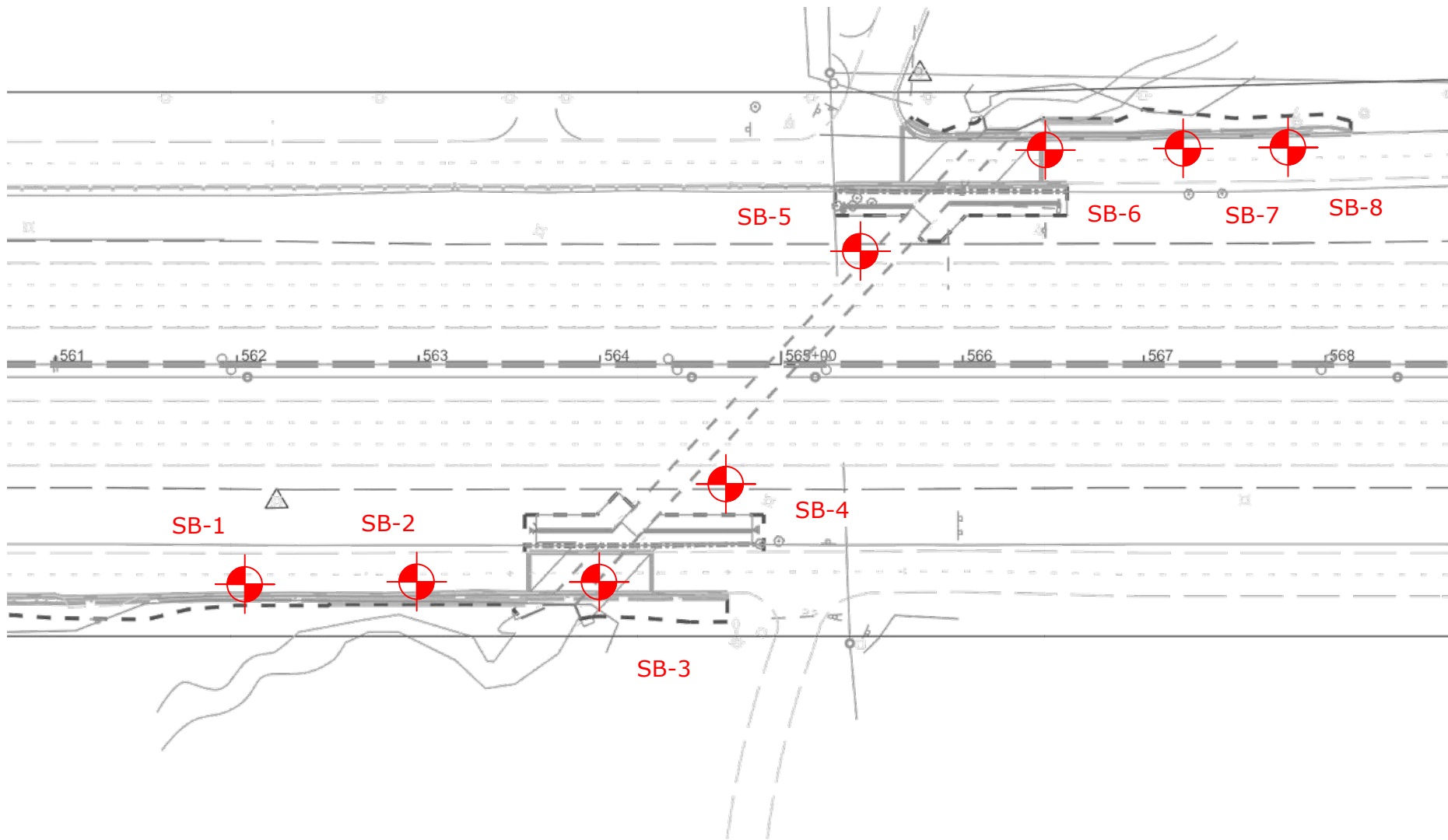
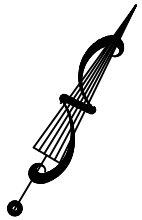
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 NTS

DRAWN BY: JAR
CHECKED BY: RW
DATE: 7/20/22

SITE LOCATION MAP
 IDOT PTB 196-017 WORK ORDER 7
 I-55 FRONTAGE ROADS OVER SAWMILL CREEK
 DUPAGE COUNTY, IL



 BORING LOCATION



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DRAWN BY:

JAR

CHECKED BY:

RW

DATE:

7/20/22

BORING LOCATION PLAN

IDOT PTB 196-017 WORK ORDER 7
 I-55 FRONTAGE ROADS OVER SAWMILL CREEK
 DUPAGE COUNTY, IL

APPENDIX B
SOIL BORING LOGS

BORING LOG LEGEND

Relative Drilling Resistance		
RDR	Term	Criterion
1	Very Easy	No chatter, very little resistance, very fast and steady drill advance
2	Easy	No chatter, some resistance, fast and steady drill advance rate
3	Moderate	Some chatter, firm drill resistance, moderate advance
4	Hard	Frequent chatter, variable drill resistance, slow advance rate
5	Very Hard	Constant chatter, variable and very slow drill advance, nearly refusal

Coarse Gradation (mm) (ASTM D2488)	
Gravel	4.75 to 75
Cobbles	75 to 300
Boulders	> 300

Proportional Terms (%) (ASTM D2488)	
Trace	< 5
Few	5 to 10
Little	15 to 25
Some	30 to 45
Mostly	50 to 100

Soil Moisture Conditions	
Term	Appearance and Feel
Dry	Soil sample looks and feels powdery or dusty; no indication of moisture. Free-running granular soils.
Damp	Cohesive soils cannot be molded easily without adding water. Granular soil may not flow very easily.
Moist	Soil is near the optimum moisture content. Cohesive soils are near the plastic limit. Soil changes color slightly when exposed to air for a short period.
Wet	One may feel a high degree of moisture, yet no free water is visible. Water may become visible if the sample is squeezed. Cohesive soil appears weak and sticks to and/or stains hands. Granular soils tend to cohere.
Saturated	Applied to granular soils that have free surface water; water drains freely from the sample.

Relative Density of Non-Cohesive Soils (ASTM D1586)	
No. of Blows/ft	Relative Density
0 - 4	Very Loose
4 - 10	Loose
10 - 30	Medium Dense
30 - 50	Dense
> 50	Very Dense

Consistency of Cohesive Soils (ASTM D1586)	
Qu (tsf)	Consistency
< 0.25	Very Soft
0.25 - 0.50	Soft
0.50 - 1.00	Medium Stiff
1.00 - 2.00	Stiff
2.00 - 4.00	Very Stiff
> 4.00	Hard

Rock Quality Designation (ASTM D6032)	
RQD (%)	Classification
0 - 25	Very Poor
25 - 50	Poor
50 - 75	Fair
75 - 90	Good
90 - 100	Excellent

Sample Type Symbols



Split Spoon



Shelby Tube



No Recovery (NR)



Pitcher



Auger Cuttings



Rock Core

Drill Rig:

17 D50 A [87%]

SPT Hammer Efficiency

Rig Type (A or T)

Rig Model

Calibration Year

A = All Terrain Vehicle Rig

T = Truck Mounted Rig

SPT = Standard Penetration Test

Qu = Unconfined Compressive Strength Test

P = Pocket Penetrometer

S = Shear failure (Rimac)

B = Bulge failure (Rimac)

SSA = Solid Stem Auger

HSA = Hollow Stem Auger



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Telephone:
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BORING LOG SB-3

WEI Job No.: KE225150 (555-17-07)

Client **IDOT Dist One PTB 196-017 WO 7**
Project **I-55 Frontage Rd over Sawmill Creek**
Location **DuPage County, Illinois**

Datum: NAVD 88
Elevation: 688.76 ft
North: 1846683.91 ft
East: 1086704.95 ft
Station: 563+99.57
Offset: 120.02 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	688.3	6-inch thick ASPHALT --PAVEMENT--															
		Loose to medium dense, brown SANDY GRAVEL; damp to moist			1	7 12 11	NP	6						11	3 5 8	1.48 B	14
		--RDR 2--															
			5		2	3 2 2	NP	6						12	8 6 11	2.87 B	14
	682.3	Stiff, black CLAY; moist --BURIED TOPSOIL--			3	4 2 3	1.50 P	32		658.8							
	680.8	Medium stiff, brown and gray SILTY CLAY to CLAY, trace gravel; damp			4	6 4 3	0.74 B	23									
		--RDR 2--															
	678.3	Stiff to hard, brown to gray SILTY CLAY LOAM to SILTY LOAM, trace gravel; damp to moist			5	11 4 5	2.38 B	16									
		--RDR 2-- --L _L (%)=26, P _L (%)=14-- --%Gravel=5.3-- --%Sand=25.6-- --%Silt=49.9-- --%Clay=19.3-- --A-6 (6)--															
					6	3 7 8	2.30 B	13									
					7	3 6 7	3.94 B	12									
			20		8	3 6 7	3.12 B	12									
					9	6 9 8	3.94 B	11									
					10	5 7 10	4.35 B	12									
			25														
		Boring terminated at 30.00 ft															

GENERAL NOTES

Begin Drilling **06-22-2022** Complete Drilling **06-22-2022**
Drilling Contractor **Wang Testing Services** Drill Rig **20D50T [80%]**
Driller **RR&JD** Logger **L. Varzaru** Checked by **J. Bensen**
Drilling Method **2.25" ID HSA; boring backfilled upon completion**

WATER LEVEL DATA

While Drilling **DRY**
At Completion of Drilling **DRY**
Time After Drilling **NA**
Depth to Water **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

WANGENG INC KE225150.GPJ WANGENG.GDT 7/25/22



wangeng@wangeng.com

Telephone:
Fax:

BORING LOG SB-4

WEI Job No.: KE225150 (555-17-07)

Client **IDOT Dist One PTB 196-017 WO 7**
 Project **I-55 Frontage Rd over Sawmill Creek**
 Location **DuPage County, Illinois**

Datum: NAVD 88
 Elevation: 691.44 ft
 North: 1846762.02 ft
 East: 1086745.62 ft
 Station: 564+69.27
 Offset: 66.21 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	690.3	14-inch thick ASPHALT --PAVEMENT--															
	689.9	Gray SANDY GRAVEL --BASE COURSE--			1	16 5 5	4.50 P	15						11	4 3 5	1.56 B	15
		Stiff to hard, brown to gray SILTY CLAY to CLAY, trace gravel; damp to moist --FILL-- --RDR 2--	5		2	3 4 4	6.72 B	18						12	3 5 7	1.80 B	14
		--L _L (%)=36, P _L (%)=16-- --%Gravel=1.7-- --%Sand=16.9-- --%Silt=47.4-- --%Clay=34.0-- --A-6 (15)--			3	3 1 2	3.44 B	17		661.4	Boring terminated at 30.00 ft	30					
	682.5	Stiff, black SILTY CLAY, trace gravel; moist --BURIED TOPSOIL--	10		4	1 2 2	1.00 P	24				35					
	680.1	Very loose, gray SAND; saturated --RDR 2--			5	1 1 2	NP	19									
	677.4	Stiff to very stiff, gray SILTY CLAY LOAM to SILTY LOAM, trace gravel; damp to moist --RDR 2--	15		6	5 2 5	2.95 B	11				40					
					7	3 6 6	1.50 P	13									
			20		8	5 6 9	2.25 P	14				45					
					9	3 6 9	3.20 B	13									
			25		10	3 5 6	1.72 B	14				50					

GENERAL NOTES

Begin Drilling **07-07-2022** Complete Drilling **07-07-2022**
 Drilling Contractor **Wang Testing Services** Drill Rig **17B57T [91%]**
 Driller **KS&PH** Logger **L. Varzaru** Checked by **J. Bensen**
 Drilling Method **2.25" ID HSA; boring backfilled upon completion**

WATER LEVEL DATA

While Drilling **11.30 ft**
 At Completion of Drilling **DRY**
 Time After Drilling **NA**
 Depth to Water **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

WANGENGINC KE225150.GPJ WANGENG.GDT 7/25/22



wangeng@wangeng.com

Telephone:
Fax:

BORING LOG SB-5

WEI Job No.: KE225150 (555-17-07)

Client **IDOT Dist One PTB 196-017 WO 7**
Project **I-55 Frontage Rd over Sawmill Creek**
Location **DuPage County, Illinois**

Datum: NAVD 88
Elevation: 691.59 ft
North: 1846910.23 ft
East: 1086759.11 ft
Station: 565+43.75
Offset: 62.64 LT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	690.4	14-inch thick ASPHALT															
	690.2	--PAVEMENT--															
		Gray SANDY GRAVEL			1	6 4 5	4.50	16						11	3 4 6	0.41	16
		--BASE COURSE--															
		Hard, brown SILTY CLAY, trace gravel; damp															
	687.5	--FILL--			2	6 10 5	NP	8						12	6 6 10	2.38	13
		--RDR 2--															
		Medium dense, brown SANDY GRAVEL; damp															
	686.1	--FILL--			3	3 4 4	2.38	21									
		--RDR 2--															
		Very stiff, black and gray SILTY CLAY, trace gravel; damp															
	683.6	--BURIED TOPSOIL--			4	2 3 3	1.64	20									
		--RDR 2--															
		Medium stiff to stiff, brown and gray SILTY CLAY to CLAY, trace gravel; damp	10														
		--RDR 2--			5	1 2 4	0.66	24									
	678.6																
		Hard, gray SILTY CLAY LOAM, trace gravel; damp			6	4 8 8	5.00	16									
		--RDR 2--	15														
	676.1																
		Stiff, brown and gray GRAVELLY LOAM; moist			7	4 6 7	1.39	9									
		--RDR 2--															
		--L _L (%)=15, P _L (%)=10--															
		--%Gravel=17.0--															
		--%Sand=40.6--															
		--%Silt=31.7--															
		--%Clay=10.7--															
		--A-4 (0)--			8	3 5 5	NP	12									
	673.6																
		Medium dense, gray SAND; saturated			9	3 5 6	2.62	13									
		--RDR 2--															
	671.1																
		Soft to vey stiff, gray SILTY CLAY LOAM to SILTY LOAM, trace gravel; damp			10	3 4 7	1.23	15									
		--RDR 2--	25														

GENERAL NOTES	
Begin Drilling	07-07-2022
Complete Drilling	07-07-2022
Drilling Contractor	Wang Testing Services
Drill Rig	17B57T [91%]
Driller	KS&PH
Logger	L. Varzaru
Checked by	J. Bensen
Drilling Method	2.25" ID HSA; boring backfilled upon completion

WATER LEVEL DATA	
While Drilling	15.50 ft
At Completion of Drilling	DRY
Time After Drilling	NA
Depth to Water	NA
The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.	

WANGENGINC KE225150.GPJ WANGENG.GDT 7/25/22



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BORING LOG SB-6

WEI Job No.: KE225150 (555-17-07)

Client **IDOT Dist One PTB 196-017 WO 7**
 Project **I-55 Frontage Rd over Sawmill Creek**
 Location **DuPage County, Illinois**

Datum: NAVD 88
 Elevation: 691.18 ft
 North: 1847003.55 ft
 East: 1086828.36 ft
 Station: 566+45.78
 Offset: 118.26 LT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	690.0	14-inch thick ASPHALT --PAVEMENT--															
	689.4	Loose, brown SANDY GRAVEL; damp --BASE COURSE--			1	4 3 4	3.00 P	13						11	5 5 9	2.62 B	13
		Very stiff, brown, gray and black SILTY CLAY, trace gravel; damp --FILL-- --RDR 2--	5		2	3 2 3	2.95 B	17		661.2		30		12	4 6 9	2.79 B	12
	685.7	Medium stiff to stiff, black CLAY to SILTY CLAY, trace gravel; damp --BURIED TOPSOIL-- --RDR 2--			3	2 2 3	0.90 B	28			Boring terminated at 30.00 ft						
		--wet spoon recovery; possible sand lens-- Soft, gray CLAY LOAM, trace gravel; wet --RDR 2--	10		4	2 2 4	1.80 B	33									
	680.7	Stiff to very stiff, gray SILTY CLAY LOAM to SILTY LOAM, trace gravel; damp to moist --RDR 2--			5	2 3 5	0.49 B	17									
	678.2				6	2 3 9	1.23 B	15									
					7	5 6 7	3.44 B	12									
					8	6 6 7	3.36 B	12									
		--L_L(%)=23, P_L(%)=9-- --%Gravel=9.3-- --%Sand=20.9-- --%Silt=49.0-- --%Clay=20.8-- --A-6 (6)--			9	3 6 8	3.94 B	12									
					10	5 6 12	2.95 B	12									

GENERAL NOTES

Begin Drilling **06-21-2022** Complete Drilling **06-21-2022**
 Drilling Contractor **Wang Testing Services** Drill Rig **20D50T [80%]**
 Driller **RR&JD** Logger **L. Varzaru** Checked by **J. Bensen**
 Drilling Method **2.25" ID HSA; boring backfilled upon completion**

WATER LEVEL DATA

While Drilling **10.00 ft**
 At Completion of Drilling **13.50 ft**
 Time After Drilling **NA**
 Depth to Water **NA**

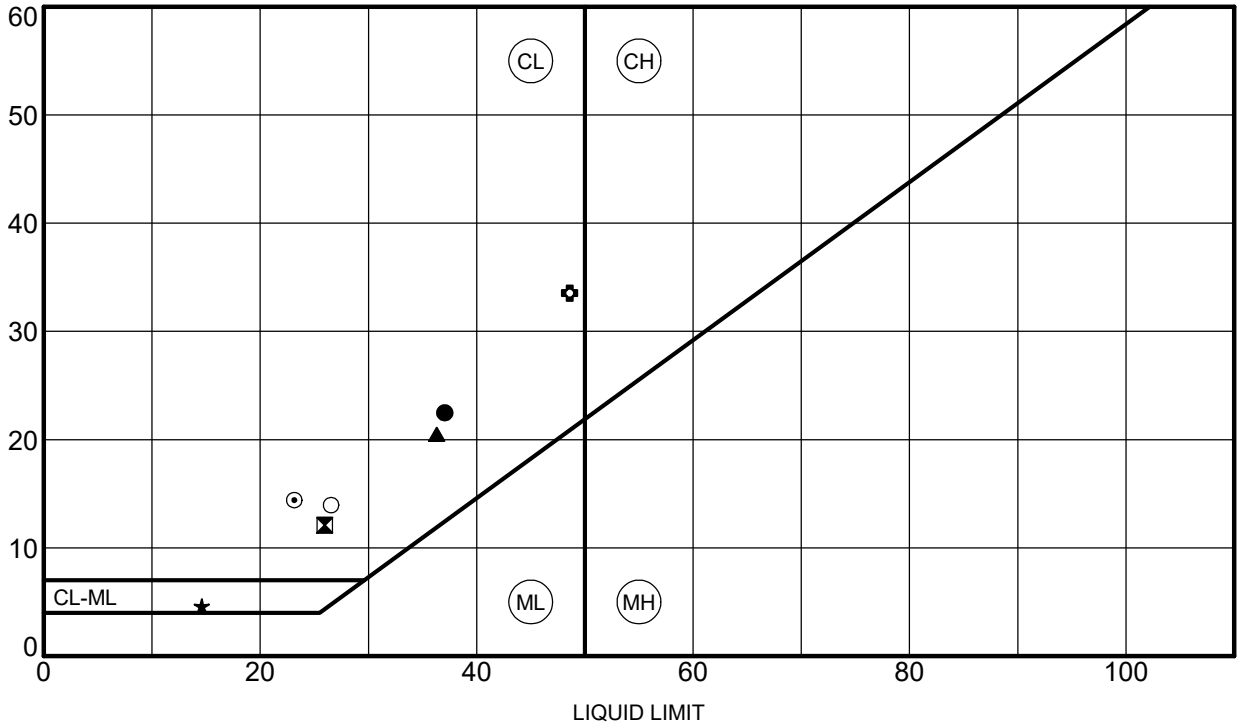
The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

WANGENGINC KE225150.GPJ WANGENG.GDT 7/25/22

APPENDIX C

LABORATORY TEST RESULTS

P L A S T I C I T Y
I N D E X



	Specimen Identification	LL	PL	PI	Fines	IDH Classification	
●	SB-1#3	6.0 ft	37	15	22	84	Silty Clay
⊠	SB-3#5	11.0 ft	26	14	12	69	Silty Clay Loam
▲	SB-4#2	3.5 ft	36	16	20	81	Clay
★	SB-5#7	16.0 ft	15	10	5	43	Gravelly Loam
⊙	SB-6#9	21.0 ft	23	9	14	70	Silty Clay Loam
⊕	SB-7#4	8.5 ft	49	15	34	75	Clay
○	SB-8#10	23.5 ft	27	13	14	82	Silty Clay

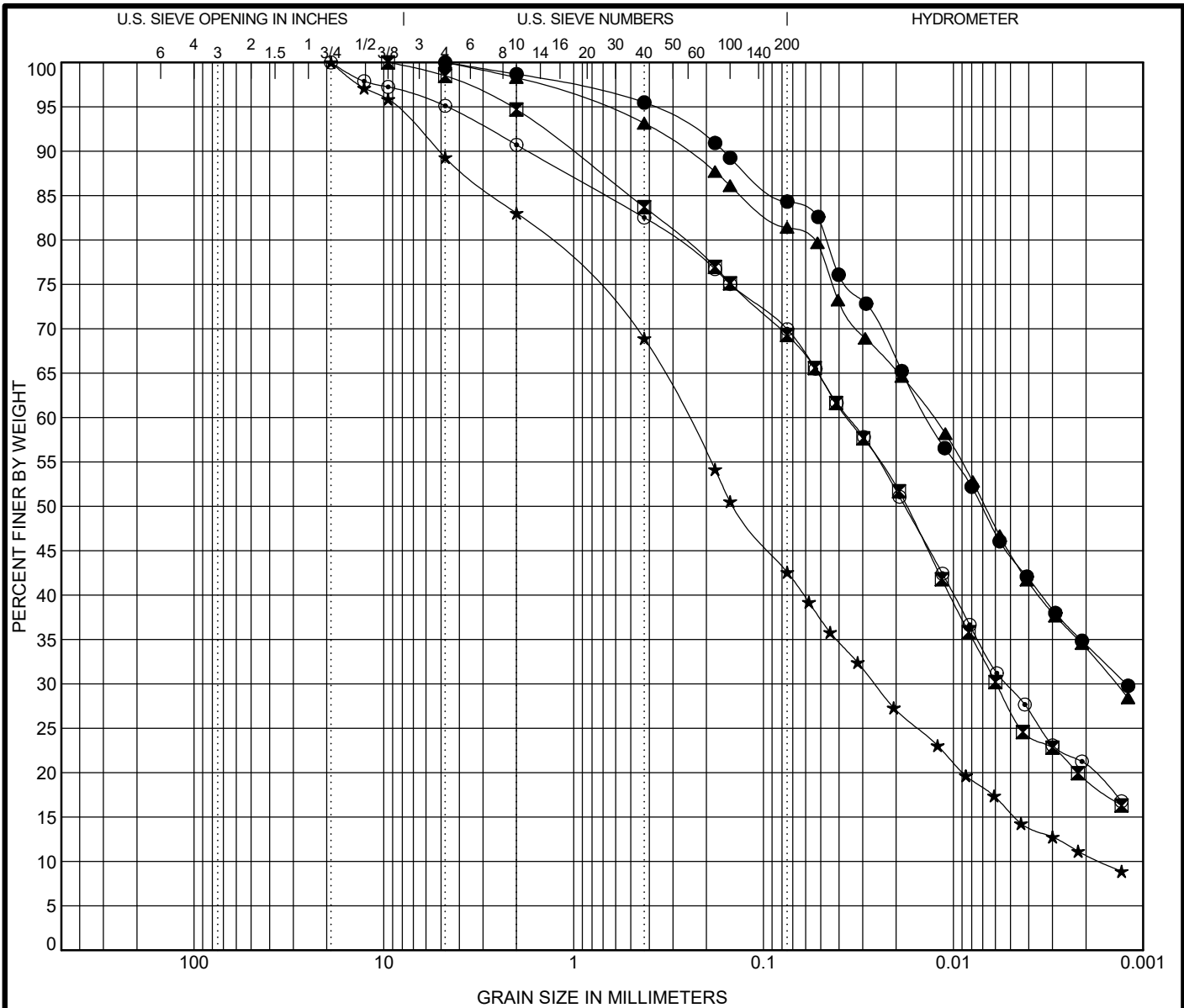
WEI/ATTERBERG LIMITS IDH KE225150.GPJ US LAB.GDT 7/25/22



Terracon
Telephone:
Fax:

ATTERBERG LIMITS' RESULTS

Project: I-55 Frontage Rd over Sawmill Creek
Location: DuPage County, Illinois
Number: KE225150 (555-17-07)



COBBLES	GRAVEL	SAND		SILT AND CLAY
		coarse	fine	

Specimen Identification		IDH Classification	LL	PL	PI	Cc	Cu
●	SB-1#3 6.0 ft	Silty Clay	37	15	22		
☒	SB-3#5 11.0 ft	Silty Clay Loam	26	14	12		
▲	SB-4#2 3.5 ft	Clay	36	16	20		
★	SB-5#7 16.0 ft	Gravelly Loam	15	10	5	1.58	150.13
◎	SB-6#9 21.0 ft	Silty Clay Loam	23	9	14		

Specimen Identification		D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay
●	SB-1#3 6.0 ft	4.75	0.014	0.001		1.3	14.4	49.9	34.4
☒	SB-3#5 11.0 ft	9.5	0.036	0.006		5.3	25.6	49.9	19.3
▲	SB-4#2 3.5 ft	4.75	0.013	0.001		1.7	16.9	47.4	34.0
★	SB-5#7 16.0 ft	19	0.253	0.026	0.002	17.0	40.6	31.7	10.7
◎	SB-6#9 21.0 ft	19	0.036	0.005		9.3	20.9	49.0	20.8

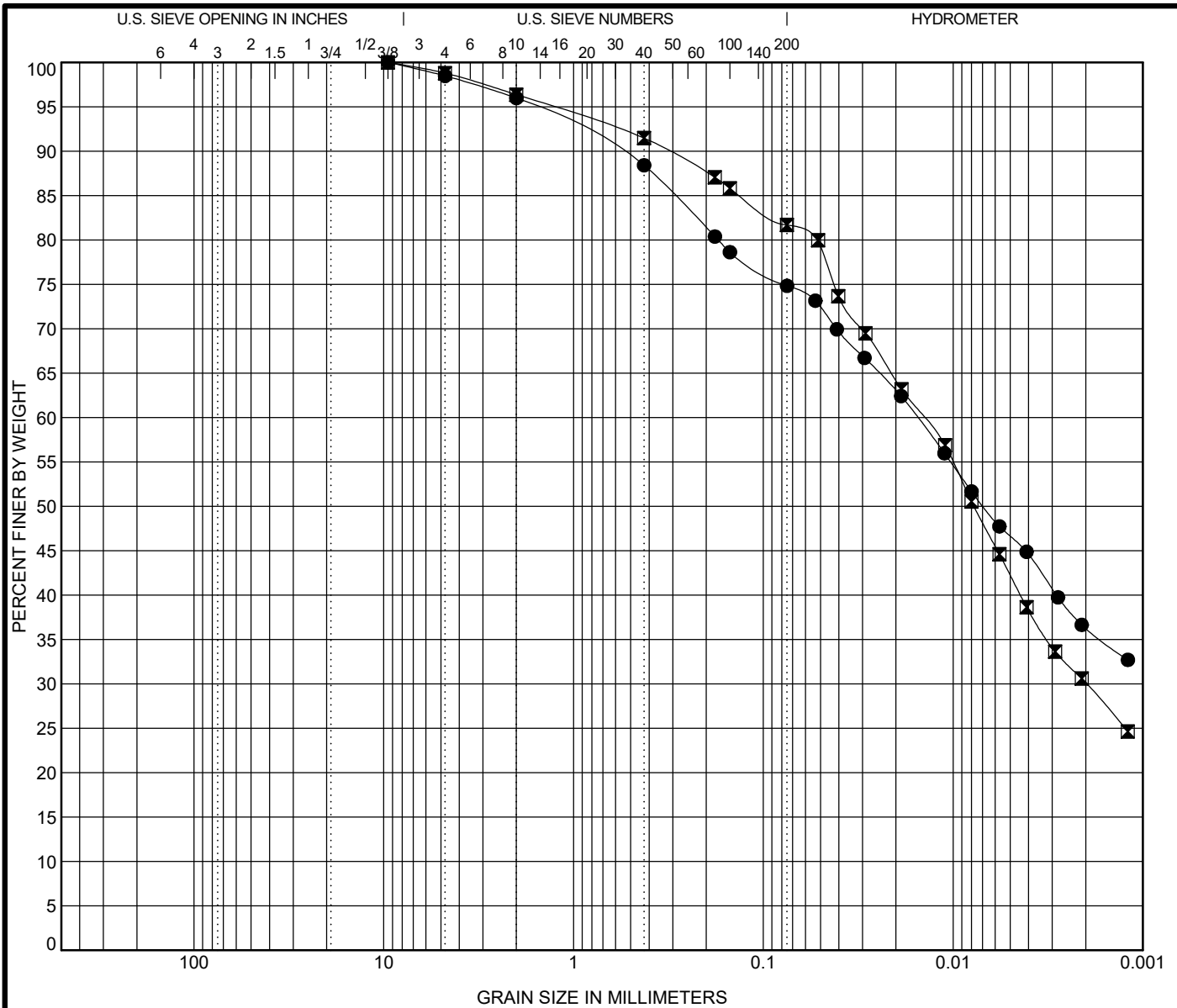
WEI GRAIN SIZE IDH KE225150.GPJ US LAB.GDT 7/25/22



Terracon
Telephone:
Fax:

GRAIN SIZE DISTRIBUTION

Project: I-55 Frontage Rd over Sawmill Creek
Location: DuPage County, Illinois
Number: KE225150 (555-17-07)



COBBLES	GRAVEL	SAND		SILT AND CLAY
		coarse	fine	

Specimen Identification		IDH Classification					LL	PL	PI	Cc	Cu
●	SB-7#4 8.5 ft	Clay					49	15	34		
■	SB-8#10 23.5 ft	Silty Clay					27	13	14		

Specimen Identification		D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay
●	SB-7#4 8.5 ft	9.5	0.015			4.0	21.2	38.5	36.3
■	SB-8#10 23.5 ft	9.5	0.014	0.002		3.6	14.7	51.6	30.1

WEI GRAIN SIZE IDH KE225150.GPJ US LAB.GDT 7/25/22



Terracon
Telephone:
Fax:

GRAIN SIZE DISTRIBUTION

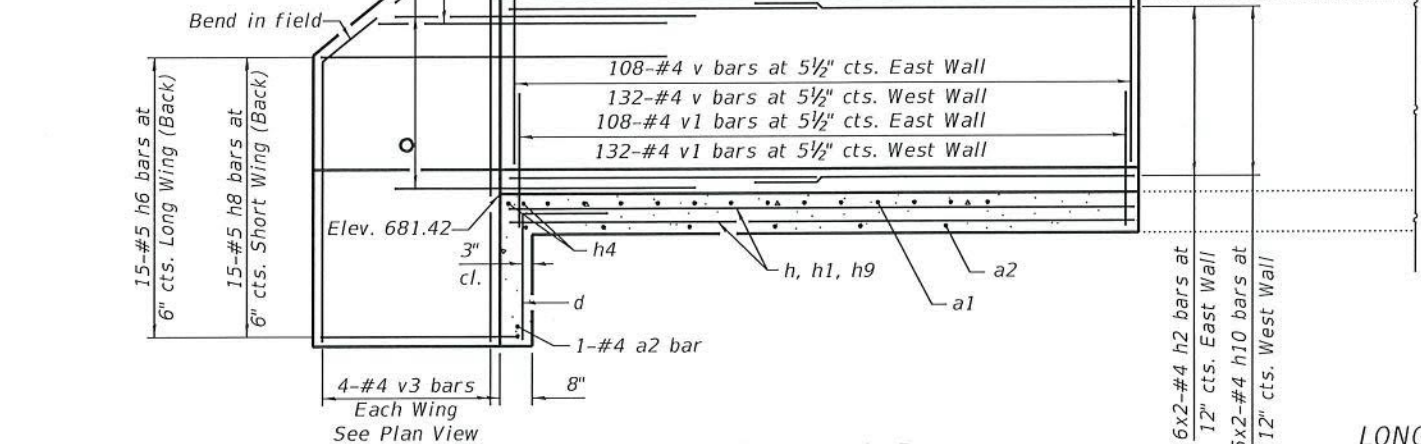
Project: I-55 Frontage Rd over Sawmill Creek
 Location: DuPage County, Illinois
 Number: KE225150 (555-17-07)

APPENDIX D

GENERAL PLAN AND LONGITUDINAL SECTION (PROVIDED BY IDOT)

(Back)
2-#5 h3 bars at 6" cts. Short Wing
2-#5 h7 bars at 6" cts. Long Wing

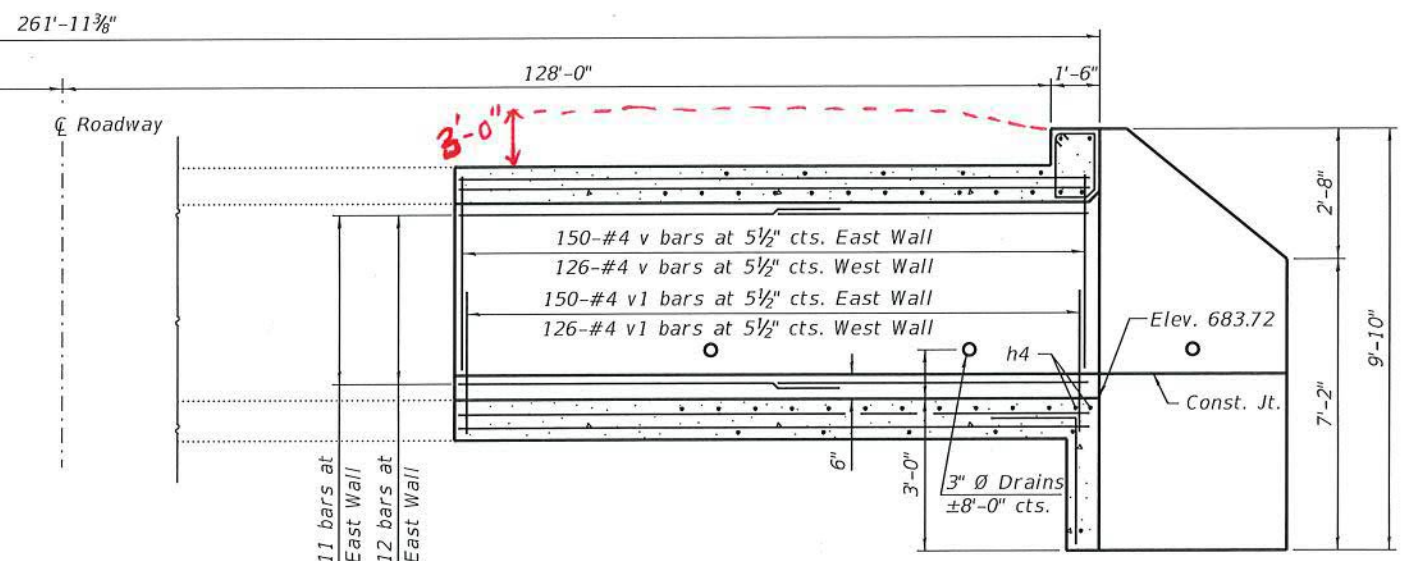
(Front)
10-#5 h3 bars at 6" cts. Short Wing
10-#5 h7 bars at 6" cts. Long Wing



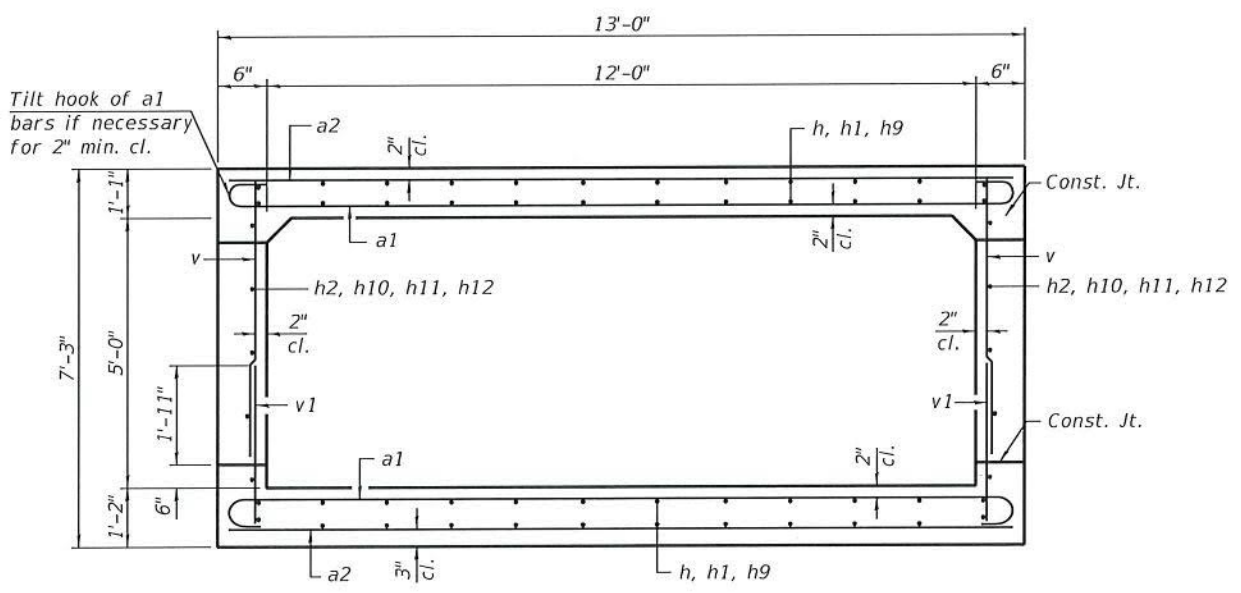
SOUTH END

MIN. BAR LAP
#4 bar = 2'-3"

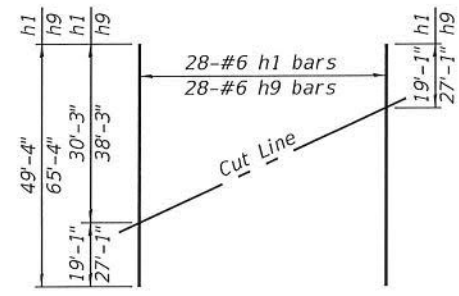
LONGITUDINAL SECTION
(Dimensions at Rt. L's to \bar{C} Roadway)



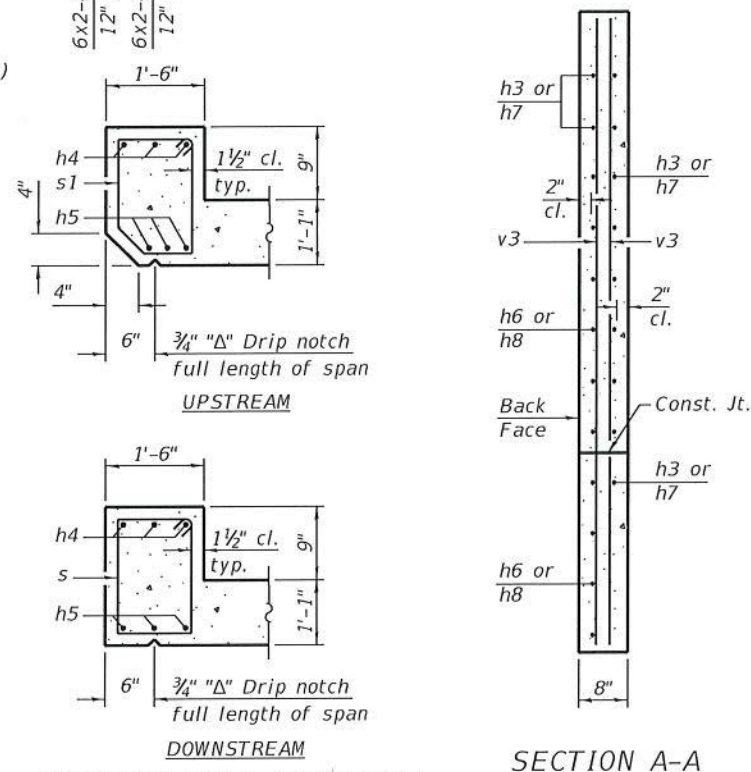
NORTH END



SECTION THRU BARREL



FIELD CUTTING DIAGRAM
Order h1 and h9 bars full length. Cut as shown for top of slab and use remainder of bars for bottom of slab.



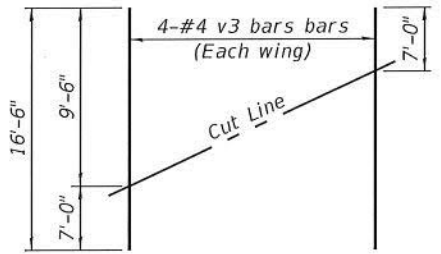
SECTION THRU HEADWALL

SECTION A-A

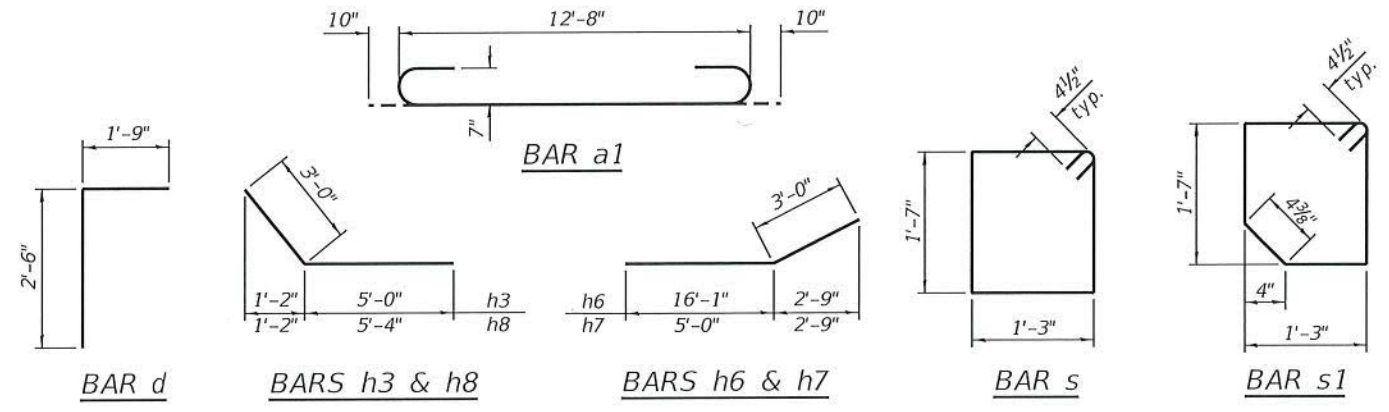
BILL OF MATERIAL

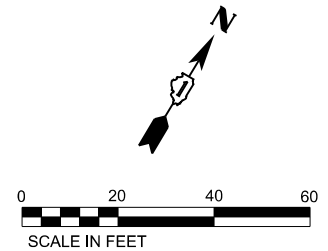
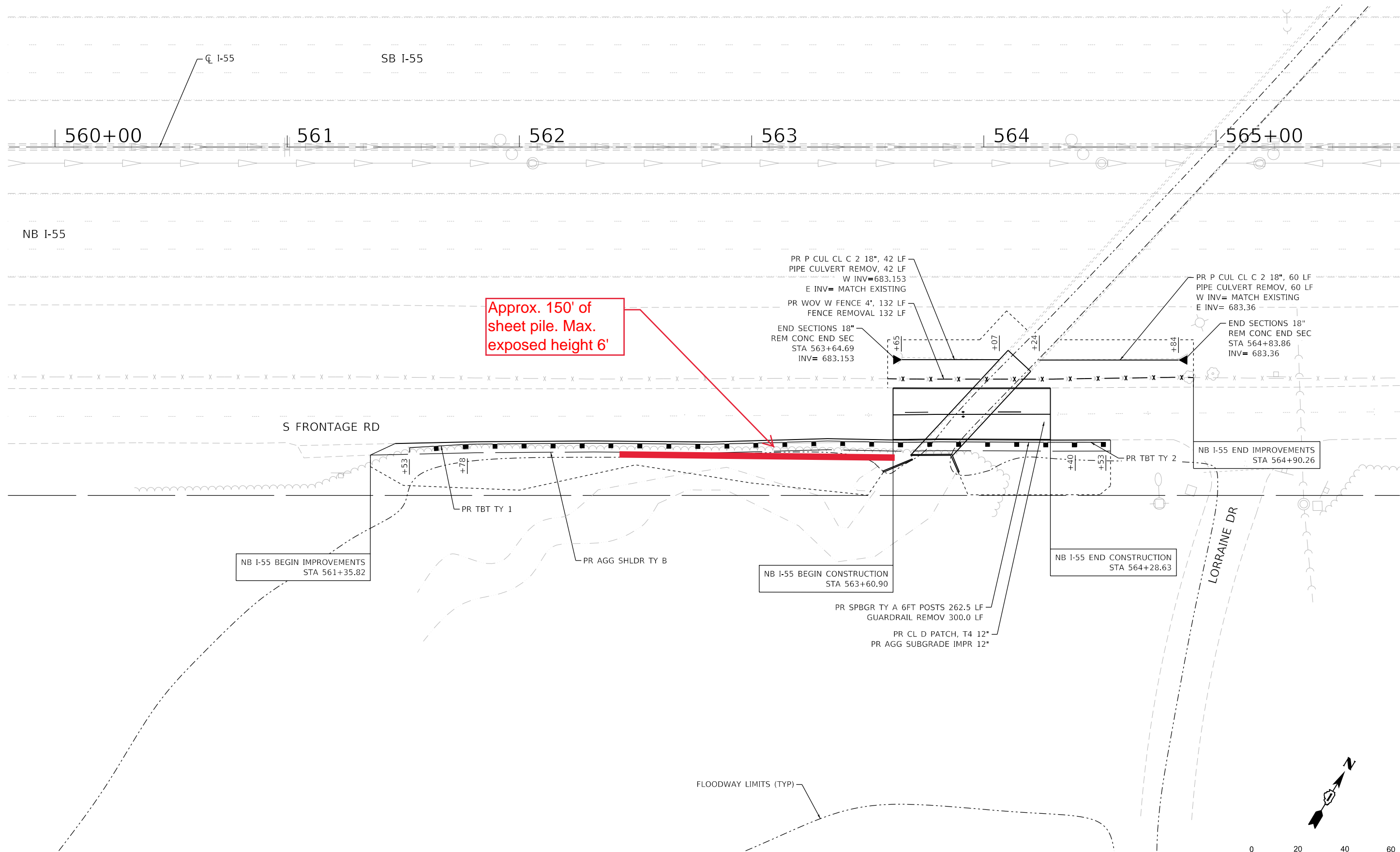
Bar No.	Size	Length	Shape
a1	512 #7	14'-4"	U
a2	274 #6	12'-8"	—
d	34 #4	4'-3"	L
h	112 #6	33'-4"	—
h1	56 #6	49'-4"	—
h2	12 #4	25'-8"	—
h3	24 #5	8'-0"	—
h4	10 #6	16'-1"	—
h5	6 #9	16'-1"	—
h6	30 #5	19'-1"	—
h7	24 #5	8'-0"	—
h8	30 #5	8'-4"	—
h9	56 #6	65'-4"	—
h10	12 #4	31'-3"	—
h11	12 #4	35'-3"	—
h12	12 #4	29'-8"	—
s	17 #4	6'-5"	□
s1	17 #4	6'-3"	□
v	520 #4	5'-3"	—
v1	520 #4	3'-4"	—
v3	16 #4	16'-6"	—
Concrete Box Culverts			Cu. Yd.
Reinforcement Bars			Pound

Notes:
A distance of half the length of the wingwall but not less than six feet of the barrel shall be poured monolithically with the wingwalls.
Bars indicated thus 12 x 4-#5 etc. indicates 12 lines of bars with 4 lengths per line.
At the Contractor's option, a longer v1 bar may be ordered to replace the v bar.
No reduction in quantities shall be made for this substitution.



FIELD CUTTING DIAGRAM
Order v3 bars full length. Cut as shown and use remainder of bars in opposite end wingwall.

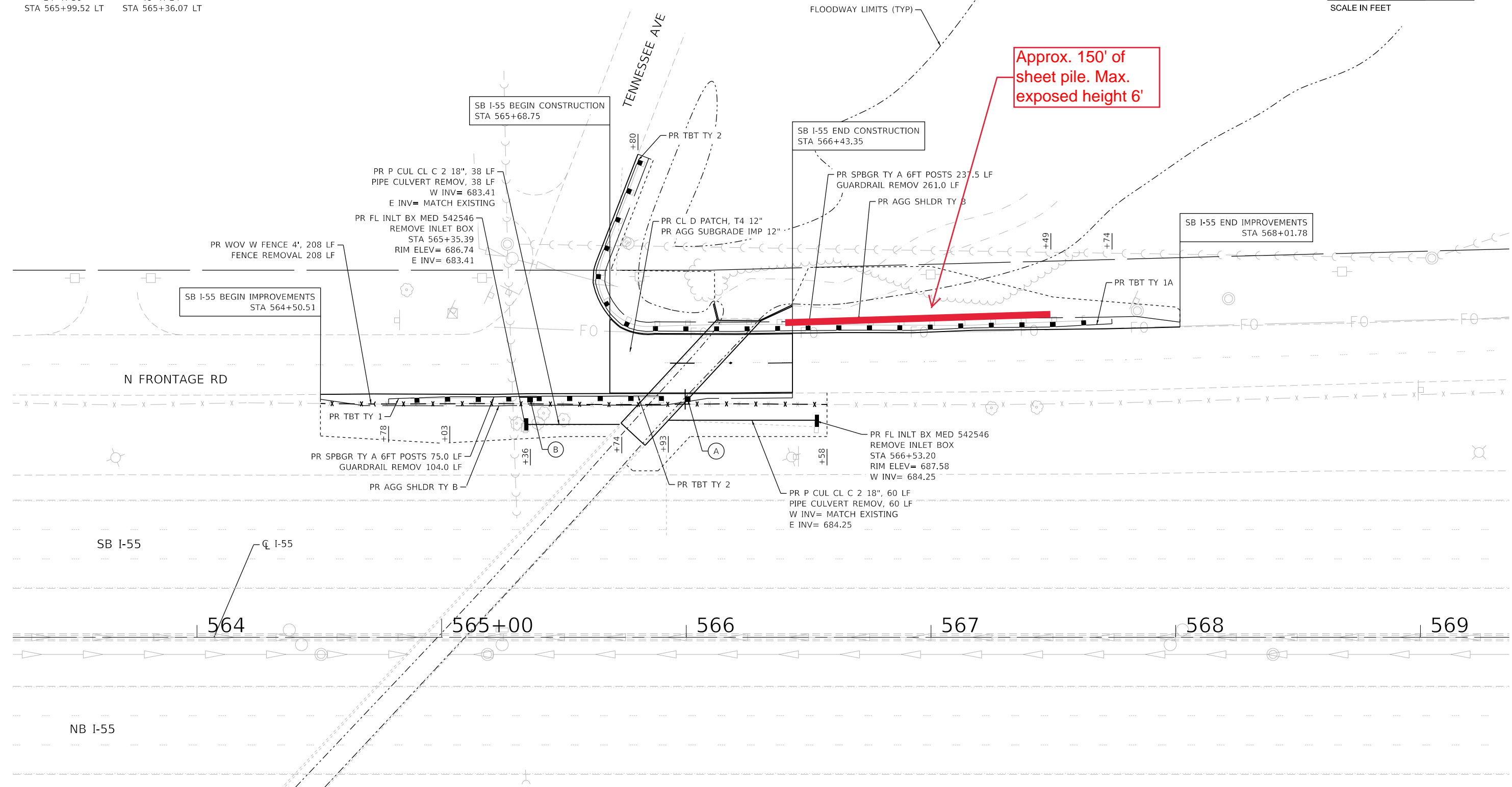
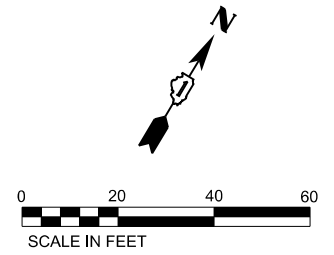
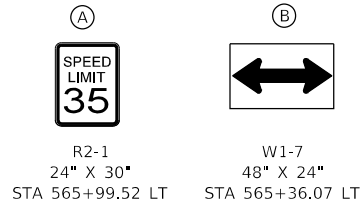




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DRAWN - RC	REVISIONS -	
PLOT SCALE = 40,0000 ' / in.	CHECKED - ST	REVISED -
PLOT DATE = 5/4/2022	DATE - 5/2022	REVISED -

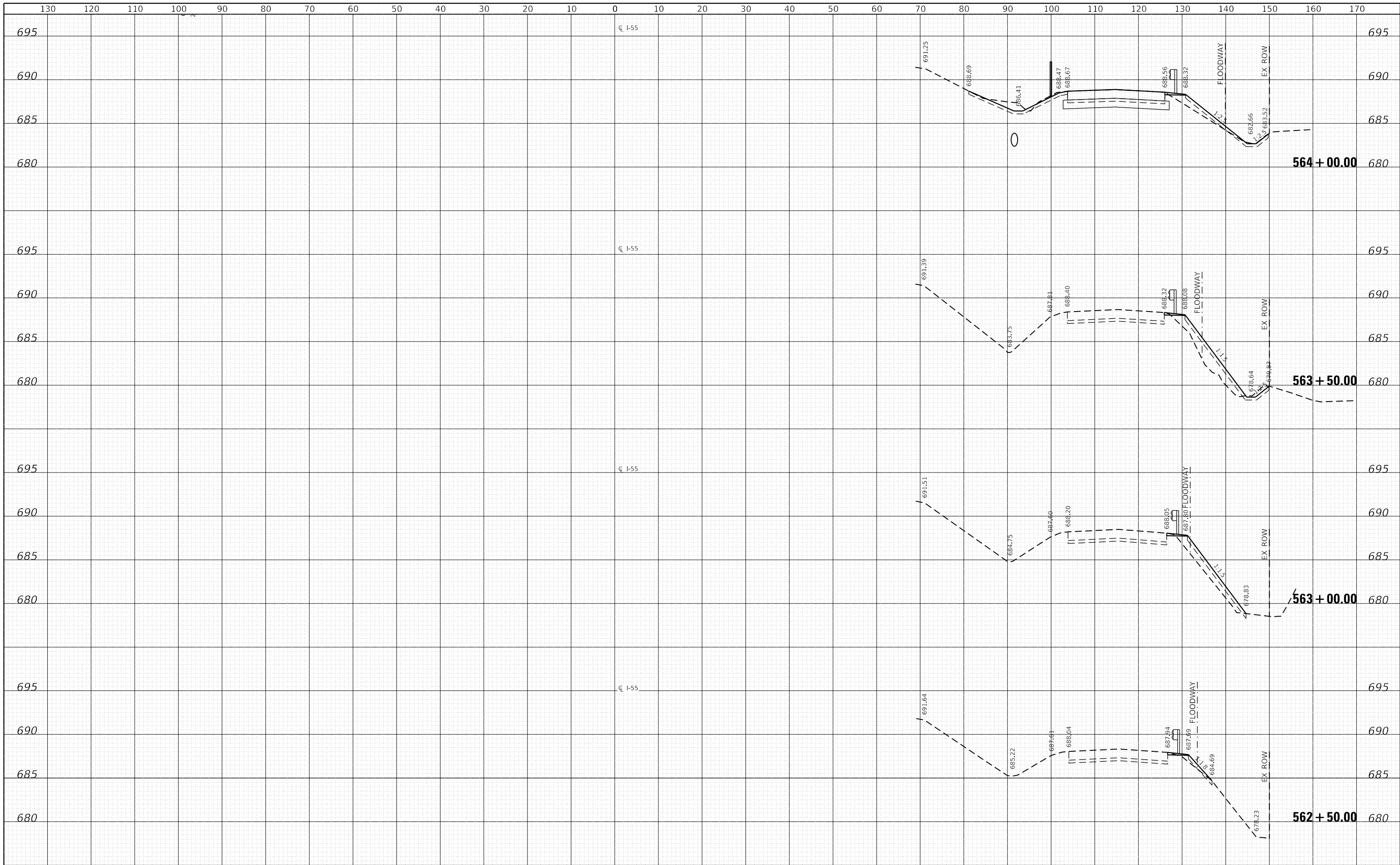
F.A.I. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
55	2021-068-CR	DUPAGE	4	1
ILLINOIS FED. AID PROJECT			CONTRACT NO. 62P06	

LEGEND



USER NAME = rober	DESIGNED - RC	REVISED -
DRAWN - RC	REVISIONS -	
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PLOT DATE = 5/4/2022	DATE - 5/2022	REVISED -

F.A.I. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
55	2021-068-CR	DUPAGE	4	2
CONTRACT NO. 62P06			ILLINOIS FED. AID PROJECT	



Lin Engineering, Ltd.
Consulting Engineers
Westmont, Illinois

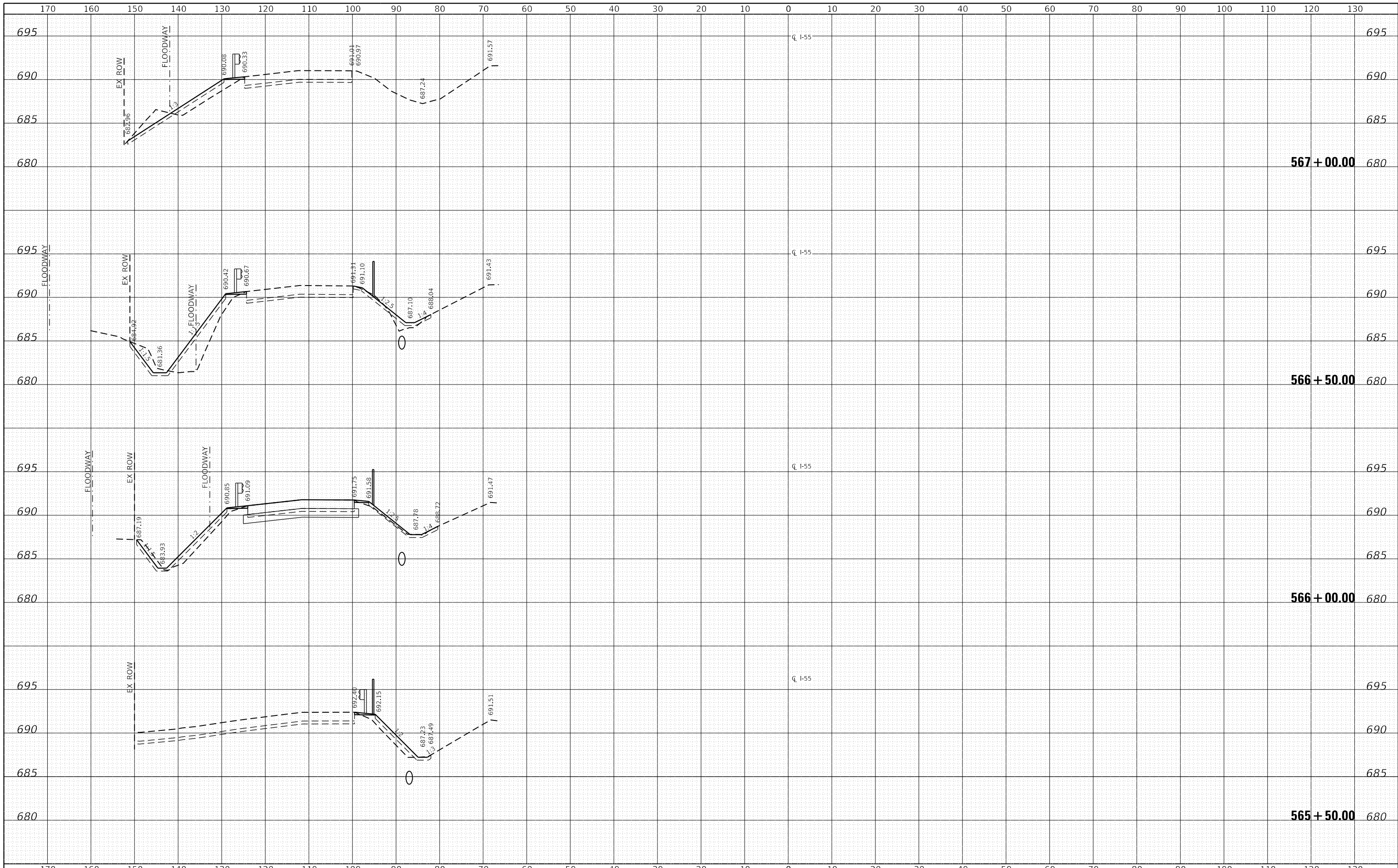
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	DATE - 5/2022	REVISED -

**STATE OF ILLINOIS
DEPARTMENT OF TRANSPORTATION**

**F.A.I. 55 NORTH AND SOUTH FRONTAGE ROADS OVER SAWMILL CREEK
S FRONTAGE ROAD CROSS SECTIONS**

SCALE: 1"=10'H, 5'V SHEET 1 OF 2 SHEETS STA. 562+50.00 TO STA. 564+00.00

F.A.I. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
55	2021-068-CR	DUPAGE	4	3
			CONTRACT NO. 62P06	
			ILLINOIS FED. AID PROJECT	



LIN ENGINEERING, LTD.
 Consulting Engineers
 Westmont, Illinois

USER NAME = rober	DESIGNED - RC	REVISED -
PLOT SCALE = 20.0000' / in.	DRAWN - RC	REVISED -
PLOT DATE = 5/4/2022	CHECKED - ST	REVISED -
	DATE - 5/2022	REVISED -

**STATE OF ILLINOIS
 DEPARTMENT OF TRANSPORTATION**

**F.A.I. 55 NORTH AND SOUTH FRONTAGE ROADS OVER SAWMILL CREEK
 N FRONTAGE ROAD CROSS SECTIONS**
 SCALE: 1"=10'H, 5'V SHEET 2 OF 2 SHEETS STA. 562+50.00 TO STA. 564+00.00

F.A.I. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
55	2021-068-CR	DUPAGE	4	4
CONTRACT NO. 62P06			ILLINOIS FED. AID PROJECT	