



INTERIOR GIRDER MOMENT TABLE				
		0.4 Sp. 1 or 0.6 Sp. 3	Pier 1 or 2	0.5 Sp. 2
$I_s$	(in <sup>4</sup> )	2,850	2,850	2,850
$I_c(n)$	(in <sup>4</sup> )	8,593	8,593	8,593
$I_c(3n)$	(in <sup>4</sup> )	6,310	6,310	6,310
$I_c(cr)$	(in <sup>4</sup> )	-	-	-
$S_s$	(in <sup>3</sup> )	213	213	213
$S_c(n)$	(in <sup>3</sup> )	334	334	334
$S_c(3n)$	(in <sup>3</sup> )	301	301	301
$S_c(cr)$	(in <sup>3</sup> )	-	-	-
DC1	(k/')	0.64	0.64	0.64
M <sub>DC1</sub>	('k)	73	137	72
DC2	(k/')	0.04	0.04	0.04
M <sub>DC2</sub>	('k)	4	8	4
DW	(k/')	0.26	0.26	0.26
M <sub>DW</sub>	('k)	30	56	29
$M_k + IM$	('k)	375	326	387
$M_u$ (Strength I)	('k)	798	836	816
* $\phi_r M_n$	('k)	1,739	-	1,741
$f_s$ DC1	(ksi)	4.1	7.7	4.1
$f_s$ DC2	(ksi)	0.2	0.3	0.2
$f_s$ DW	(ksi)	1.2	2.2	1.2
$f_s$ 1.3(LL+IM)	(ksi)	17.5	15.2	18.1
$f_s$ (Service II)	(ksi)	23.0	25.5	23.4
0.95R <sub>n</sub> F <sub>yr</sub>	(ksi)	47.5	47.5	47.5
** $f_s$ (Total)(Strength I)	(ksi)	-	33.9	-
** $\phi_r F_n$	(ksi)	-	-	-
V <sub>r</sub>	(k)	18.9	18.9	20.0

\* Compact sections  
 \*\* Non-compact sections

INTERIOR GIRDER REACTION TABLE		
		Abut. Pier 1 or 2
R <sub>DC1</sub>	(k)	9.7 32.8
R <sub>DC2</sub>	(k)	0.6 1.8
R <sub>DW</sub>	(k)	4.0 13.3
R <sub>k + IM</sub>	(k)	49.9 75.8
R <sub>Total</sub>	(k)	64.2 123.7

$I_s, S_s$ : Non-composite moment of inertia and section modulus of the steel section used for computing  $f_s$  (Total-Strength I, and Service II) due to non-composite dead loads (in.4 and in.3).

$I_c(n), S_c(n)$ : Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing  $f_s$  (Total-Strength I, and Service II) due to short-term composite live loads (in.4 and in.3).

$I_c(3n), S_c(3n)$ : Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing  $f_s$  (Total-Strength I, and Service II) due to long-term composite (superimposed) dead loads (in.4 and in.3).

$I_c(cr), S_c(cr)$ : Composite moment of inertia and section modulus of the steel and longitudinal deck reinforcement, used for computing  $f_s$  (Total-Strength I and Service II) in cracked sections, due to both short-term composite live loads and long-term composite dead loads (in.4 and in.3).

DC1: Un-factored non-composite dead load (kips/ft.).  
 M<sub>DC1</sub>: Un-factored moment due to non-composite dead load (kip-ft.).  
 DC2: Un-factored long-term composite (superimposed excluding future wearing surface) dead load (kips/ft.).  
 M<sub>DC2</sub>: Un-factored moment due to long-term composite (superimposed excluding future wearing surface) dead load (kip-ft.).  
 DW: Un-factored long-term composite (superimposed future wearing surface only) dead load (kips/ft.).  
 M<sub>DW</sub>: Un-factored moment due to long-term composite (superimposed future wearing surface only) dead load (kip-ft.).  
 $M_k + IM$ : Un-factored live load moment plus dynamic load allowance (impact) (kip-ft.).  
 $M_u$  (Strength I): Factored design moment (kip-ft.).  
 $1.25 (M_{DC1} + M_{DC2}) + 1.5 M_{DW} + 1.75 M_k + IM$   
 $\phi_r M_n$ : Compact composite positive moment capacity computed according to Article 6.10.7.1 (kip-ft.).  
 0.95R<sub>n</sub>F<sub>yr</sub>: Composite stress capacity for Service II loading according to Article 6.10.4.2 (ksi).  
 $\phi_r M_{nc}$ : Compact non-composite negative moment capacity computed according to Article A6.1.1 (kip-ft.).  
 $f_s$  (Service II): Sum of stresses as computed from the moments below (ksi).  
 $M_{DC1} + M_{DC2} + M_{DW} + 1.3 M_k + IM$   
 $f_s$  (Total)(Strength I): Sum of stresses as computed from the moments below on non-compact section (ksi).  
 $1.25 (M_{DC1} + M_{DC2}) + 1.5 M_{DW} + 1.75 M_k + IM$   
 V<sub>r</sub>: Maximum factored shear range in composite portion of span computed according to Article 6.10.10.

Notes:  
 Load carrying components designated "NTR" shall conform to the Supplemental Requirements for Notch Toughness, Zone 2.  
 All beams and splices shall be M270 Grade 50W.