STRUCTURE GEOTECHNICAL REPORT BOX CULVERTS US ROUTE 45 (FAP 344) OVER TRIBUTARIES TO MILBURN CREEK PROPOSED SN 049-C006, 049-0611, 049-C007 SECTION 39R, CONTRACT 60T75 IDOT PROJECT D-91-424-12, PTB 164/04 LAKE COUNTY, ILLINOIS

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11. Abstract	arts will correct the US Doute 45 Durage of	war Tributarias ta Milburn Craak. Tha		

A series of three box culverts will carry the US Route 45 Bypass over Tributaries to Milburn Creek. The culverts are single concrete box culverts with barrel openings of 4×4, 10×5, and 4×5 feet with lengths of 109'-5", 109'-4", and 108'-3" measured out-to-out of the culverts headwalls. Culvert headwalls are proposed as continuous Mechanically Stabilized Earth (MSE) with total lengths of 112'-2" and 113'-3" for east and west walls, respectively. This report provides geotechnical recommendations for the design of proposed culverts and MSE walls.

At the site, the general soil profile consists of up to 18-inch thick black loam topsoil overlying up to 4.5 feet thick of very soft to stiff silty clay to silty clay loam underlain by very stiff to hard silty loam to silty clay loam, stiff to hard clay to silty clay loam, and very loose to dense silt to sand gravelly sandy loam. Groundwater was encountered at depths of 15.5 to 48 feet below the existing grade, or elevations ranging from 684 to 710 feet.

With minor foundation soils treatments, it will be feasible to construct the culverts on shallow foundations. Settlement analyses show the foundation soils will undergo settlement of 1.0 inches or less and differential settlement of 0.5 inches or less.

The roadway will require 10 to 11 feet of fill at the culvert approach sections. The proposed MSE walls will have a maximum supported height of about 12 feet. With minor foundation soils treatment, the proposed MSE walls are feasible. The west MSE wall sections have FOS against global instability of 6.2 and 2.0 for the short-term and long-term conditions, and will experience total long-term post-construction consolidation settlement 1.0 inches or less. We recommend the MSE walls be designed based on a factored bearing resistance of 5, 800 psf.

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1.0 INTRODUCTION

This report presents the results of Wang Engineering, Inc. (Wang) subsurface investigation, laboratory testing, geotechnical evaluations, and recommendations for the design and construction of the proposed culverts over Tributaries to Milburn Creek included in the construction of US Route 45 in the Lake County, Illinois. A *Site Location Map* is presented as Exhibit 1.

The purpose of our investigation was to characterize the site soil and groundwater conditions, perform geotechnical analyses, and provide recommendations for the design and construction of new culverts and associated retaining walls.

1.1 Project Description

The project includes realignment of new roadway US Route 45 (US 45 Bypass) approximately 1,000 feet to the west of the existing US Route 45. The US 45 Bypass will be constructed from County Place on the south to 1,500 feet north of Independence Boulevard on the north, a length of 7,200 feet. In addition, Grass Lake Road will be realigned south of its current location to form the west leg of the intersection of US 45 and Milburn Road. The project lies within the municipal boundaries of the Village of Lindenhurst on the west, and the Village of Old Mill Creek on the east. The project also lies within unincorporated areas of Lake County within Lake Villa and Newport Townships.

The proposed improvements also include construction of, a three-sided structure and a series of box culverts to carry US 45 Bypass over Milburn Creek and Unnamed Tributaries to Milburn Creek,



several retaining walls, and detention ponds.

1.2 Proposed Structures

Wang understands Parsons Transportation Group, Inc. (Parsons) envisions a series of three box culverts for the US 45 Bypass over Tributaries to the Milburn Creek. The type, size, and location (TSL) Plan provided by Parsons shows a single cell concrete box culverts and details are summarized in Table 1. The TSL Plan dated November 4, 2015 received on November 5, 2015 is included in Appendix D.

	Table 1: Summary of Box Culverts for Tributaries to Milburn Creek								
			Proposed Length	.	Invert Elevations				
	Station	Interior Cell		Approximate	Upstream	Downstream			
Structure ID				BRew	Face	Face			
		(ft, span×ft,	(feet-inch)	(°)	(feet)	(feet)			
		height)							
049-C006	134+68.75	4×4	109-5	81	724.25	722.75			
049-0611	134+77.87	10×5	109-4	81	723.75	722.00			
049-C007	135+19.39	4×5	108-3	86	724.85	723.30			

The roadway will require 10 to 11 feet of fill at the culvert approach sections, and about 3 to 4 feet of vertical fill on the culvert top slabs. The roadway approach fill and fill above the culverts will be supported by the Mechanically Stabilized Earth (MSE) walls. The proposed MSE walls will have a maximum supported height of about 12 feet. The proposed length of east and west MSE walls is 112.2 and 113.3 feet, respectively.

Stage construction is not required.

1.3 Existing Structure

There are no existing culverts at these locations.



2.0 SITE CONDITIONS AND GEOLOGICAL SETTING

The project area is located in northcentral Lake County along the border of the Villages of Lindenhurst and Old Mill Creek. On the USGS Antioch Quadrangle 7.5 Minute Series map, the proposed structure is located in the SE ¹/₄ of Section 36, Tier 46 North, and Range 10 East of the 3rd Principal Meridian. A Site Location Map is presented as Exhibit 1

The following review of the published geologic data, with emphasis on factors that might influence the design and construction of the proposed engineering works, is meant to place the project area within a regional framework and, thus, to confirm the dependability and consistency of the subsurface investigation results. For the study of the regional geologic framework, Wang considered northeastern Illinois in general and northcentral Lake County in particular. Exhibit 2 illustrates the Site and Regional Geology.

2.1 Physiography

Northcentral Lake County, part of the Wheaton Morainal Country within the Great Lake Physiographic Section (Leighton et al. 1948), is characterized by hummocky topography as a result of numerous advances and retreats of ice sheets during the Wisconsin Episode of glaciation. The project site is located along the north to south trending Valparaiso Moraine, which contains abundant kettle lakes and wetland areas. Millburn Creek drains from McDonald Lake, located west of the project area, and crosses the existing US 45 flowing east toward North Mill Creek. Ground elevations at the project site are approximately 720 to 726 feet.

2.2 Surficial Cover

The surficial cover is primarily the result of Wisconsin-age glacial activity (Hansel and Johnson, 1996). The glacigenic deposits were emplaced during pulsating advances and retreats of an ice sheet lobe responsible for the formation of end moraines and associated low-relief till and lake plains. Many kettle depressions and other low-lying areas that scar the Valparaiso Moraine were filled with peat and marl of the Grayslake Peat. The Valparaiso Moraine contains diamicton of the Wadsworth Formation, consisting of clay to silty clay loam and includes lenses of sand, silt, and clay (Hansel and Johnson 1996). The Wadsworth Formation is underlain by sand and gravel outwash deposits of the Henry Formation. The drift thickness along the project alignment ranges from 200 to 260 feet (Dixon-Warren and O'Malley 2004).



2.3 Bedrock

In northcentral Lake County the surficial cover rests unconformably on top of nearly horizontal Silurian-age dolomite. The top of the bedrock lies approximately 200 to 260 feet below the ground surface (bgs) at approximately 500 to 520 feet elevation (Dixon-Warren and O'Malley 2004).

Our subsurface investigation results fit into the local geologic context. In descending order, the borings drilled in the project area revealed that the native sediments along the site consist of clay, silty clay, and silty clay loam diamicton of the Wadsworth Formation overlying sand and gravel outwash of the Henry Formation. None of the borings drilled for this investigation encountered organic soils of the Grayslake Peat or bedrock.

3.0 METHODS OF INVESTIGATION

The following sections outline the subsurface and laboratory investigations performed by Wang.

3.1 Subsurface Investigation

The subsurface investigation performed by Wang consisted of ten structure borings, designated as BSB2-01 through BSB2-03, and BSB3-01 through BSB3-03 for the box culverts, RWB3-01 and RWB3-02 for the west wall, and RWB4-01 and RWB4-02 for the east wall. The borings were drilled in September 2014 from elevations of 725.8 to 729.6 feet to depths of 20.0 to 85.0 feet below ground surface (bgs). Boring locations proposed by Wang and approved by Parsons were staked in the field using a mapping-grade GPS. The as-drilled boring locations were surveyed by Dynasty Group and stations and offsets were provided by Parsons. The boring location data are shown in the *Boring Logs* (Appendix A), and the as-drilled locations are shown in the *Boring Location Plan* (Exhibit 3).

An ATV-mounted drill rig, equipped with hollow stem augers, was used to advance and maintain an open borehole. Soil sampling was performed according to AASHTO T 206, "*Penetration Test and Split Barrel Sampling of Soils*." The soil was sampled at 2.5-foot intervals to 30 feet bgs and at 5.0-foot intervals, thereafter. Soil samples from each interval were placed in sealed jars for further laboratory testing.

Field boring logs, prepared and maintained by a Wang geologist, include lithological descriptions, visual-manual soil classifications (IDH Textural Classification), results of Rimac and pocket



penetrometer unconfined compressive strength tests, and results of Standard Penetration Tests (SPT), recorded as blows per 6 inches of penetration.

Groundwater observations were made during and after drilling operations. The borings were backfilled with soil cuttings and bentonite chips after completion.

3.2 Laboratory Testing

The soil samples were tested in the laboratory for moisture content (AASHTO T 265). Selected soils were tested for Atterberg limits (AASHTO T 89/90) and particle size (AASHTO T 88) analyses. The soils were classified according to the IDH Textural Classification system and field visual-manual descriptions were verified in the laboratory. The laboratory results are shown in the *Boring Logs* (Appendix A) and in the *Laboratory Test Results* (Appendix B).

4.0 RESULTS OF FIELD AND LABORATORY INVESTIGATIONS

Detailed descriptions of the soil conditions encountered during the subsurface investigation are presented in the attached *Boring Logs* (Appendix A) and in the *Soil Profiles* (Exhibits 4-1 through 4-5). Please note that strata contact lines represent approximate boundaries between soil types. The actual transition between soil types in the field may be gradual in horizontal and vertical directions.

4.1 Soil Conditions

At the surface, the borings sampled 12- to 18-inch thick black loam to silty loam topsoil. In descending order, the general lithologic succession encountered in the borings includes 1) very soft to stiff silty clay to silty clay loam; 2) very stiff to hard silty loam to silty clay loam; 3) stiff to hard clay to silty clay loam; and 4) very loose to dense silt to sand and gravelly sandy loam.

1) Very soft to stiff silty clay to silty clay loam

Immediately beneath the topsoil, the borings encountered up to 4.5 feet of very soft to stiff silty clay to silty clay loam to depths of 3.0 to 5.5 feet bgs (elevations 720.3 to 723.5 feet). The cohesive soils consist of brown/grayish brown/orange brown to brownish gray silty clay to silty clay loam. Generally, this unit has unconfined compressive strength (Q_u) values of less than 0.25 to 1.6 tsf with an average of 0.97 tsf and moisture content values of 15 to 27% with an average of 22%. This layer is generally discontinuous at the site and primarily encountered at the proposed box culvert locations, and east retaining wall section.



2) Very stiff to hard silty loam to silty clay loam

Underlying the very soft to stiff cohesive soils, at elevations 720.3 to 726.1 feet, the borings revealed very stiff to hard silty loam to silty clay loam. Over all, this unit has Q_u values of 1.3 to 9.3 tsf with an average value of 4 tsf and moisture content values of 13 to 26% with an average of 18%. Laboratory index testing on samples shows liquid limit (L_L) value ranging from 27 to 31% and plastic limit (P_L) value ranging from 14 to 16%. According to the AASHTO soil classification, the soils belong to the A-6 group.

3) Stiff to hard clay to silty clay loam

At elevations 709.7 to 726.2 feet, the borings revealed very stiff to hard clay to silty clay loam containing silt to sand and sandy loam layers. Generally, this unit has Q_u values of 0.8 to 4.8 tsf with an average value of 2 tsf and moisture content values of 12 to 30% with an average of 22%. Laboratory index testing on samples shows liquid limit (L_L) value ranging from 34 to 44% and plastic limit (P_L) value ranging from 16 to 18%. According to the AASHTO soil classification, the soils belong to the A-6 and A-7 groups.

4) Very loose to dense silt to sand and gravelly sandy loam

Underlying the cohesive soils, at elevations of 667.7 to 685.6 feet, the deeper borings encountered very loose to dense, brown to gray, silt to sand, and gravelly sandy loam extending to the boring termination depths (elevations 661.5 to 640.8 feet). These granular soils have SPT N-values ranging from 0 to 33 blows/foot with an average of 13 blows/foot and moisture contents values of 7 to 24% with an average of 17%.

A layer of very soft to hard silty to clay measuring up to 15 feet in thickness was interbedded within the granular soils. The cohesive soil has Q_u values of less than 0.2 to 5.0 tsf with an average of 2.5 tsf and moisture content values ranging from 21 to 27% with an average of 24%.

4.2 Groundwater Conditions

Groundwater was encountered within the granular soil layers while drilling between elevations of 684 and 710 feet (43 to 15.5 feet bgs). Upon completion of drilling, groundwater was measured between elevations of 680 and 710 feet (17 to 48 feet bgs).



5.0 FOUNDATION ANALYSIS AND RECOMMENDATIONS

Geotechnical evaluations and recommendations for the box culvert and retaining wall foundations and our engineering analyses are included in the following sections. Based on the subsurface soil conditions, it is our opinion that it is feasible to construct precast or cast-in-place culverts.

5.1 Culvert Foundations

5.1.1 Culvert at Station 134+68.75, SN 049-C006

The construction of the Culvert at Station 134+68.75 will require excavation up to a depth of 4.5 feet below the existing grade at boring locations. The borings indicate that foundation soils below culvert bearing elevation of 722.2 feet might consist of up to 2 feet of very soft to medium stiff silty clay to silty clay loam overlying stiff to hard silty loam to silty clay loam.

We recommend removing the very soft to medium stiff soil to an elevation 720 feet for the full culvert length and width and replace with IDOT gradation CA-6 (structural fill) to provide adequate bearing capacity and tolerable settlement for the proposed culvert. The excavation and structural fill should extend at least 2 feet laterally beyond the edge of the culvert. The actual extent of the removal shall be determined in the field based on actual soils conditions during construction.

Considering the structural fill improvement for the settlement evaluation, the estimated culvert and roadway fill pressures, we estimate that the culvert will undergo long-term settlement of 1.0 inches or less and a differential settlement of 0.5 inches or less.

5.1.2 Culvert at Station 134+77.87, SN 049-0611

The construction of the Culvert at Station 134+77.87 will require excavation up to a depth of 5.5 feet below the existing grade at boring locations. The borings indicate that foundation soils below culvert bearing elevation of 721.3 feet will consist of up to 1.0 feet of very soft to medium stiff silty clay to silty clay loam overlying stiff to hard silty loam to silty clay loam.

We recommend removing the very soft to medium stiff soil to an elevation 720 feet for the full culvert length and width and replace with structural fill to provide adequate bearing capacity and tolerable settlement for the proposed culvert. The excavation and structural fill should extend laterally at least two feet laterally beyond the edge of the culvert.



Considering the structural fill improvement for the settlement evaluation, the estimated culvert and roadway fill pressures, we estimate that the culvert will undergo long-term settlement of 1.0 inches or less and a differential settlement of 0.5 inches or less.

5.1.3 Culvert at Station 135+19.39, SN 049-C007

The construction of the Culvert at Station 135+19.39 will require excavation up to a depth of 4.5 feet below the existing grade at boring locations. The borings indicate that foundation soils below culvert bearing elevation of 722.8 feet will consist of medium dense silt and stiff to very stiff silty clay to silty clay loam overlying very stiff to hard silty loam to silty clay loam or medium dense silt.

We recommend removing the foundation soils to an elevation 721.5 feet (Boring BSB3-03) for the full barrel width for an approximate length of 25 feet of east end of the culvert and replace with structural fill to provide adequate bearing capacity and tolerable settlement for the proposed culvert. The excavation and structural fill should extend at least 2 feet laterally beyond the edge of the culvert.

We estimate that the culvert will undergo long-term settlement of 1.0 inches or less and a differential settlement of 0.5 inches or less.

5.2 MSE Walls

We understand culvert headwalls are proposed to be continuous between the culverts and extend north and south of the culvert series. The selected MSE type wall is feasible and economical with minor foundation soils treatment.

The 112.2-foot long **east** wall begins at Station 134+30.00 and ends at Station 135+45.00 and top of sidewalk elevations range from 731.83 to 732.21 feet.

The 113.3-foot long **west** wall begins at Station 134+45.00 and ends at Station 135+55.00 and top of sidewalk elevations range from 733.83 to 734.13 feet.

The maximum retained height for both walls ranges from 4 feet on top culverts to 11 feet for the approach roadways.



5.2.1 Bearing Resistance and Sliding

Wang recommends the top of MSE leveling pad at a minimum of 3.5 feet below the finished grade at front face of the wall as required by IDOT (2012a).

Based on borings for some portion along the **east** wall, very soft to medium stiff silty clay to silty clay loam is expected to be encountered at the base of MSE wall. To provide adequate bearing resistance and tolerable settlement we recommend removing very soft soil ($Q_u < 0.25$ to 0.9 tsf, moisture content = 20 to 24%) to an elevation of 720.0 feet from Station 134+60 to Station 135+30 and removing medium stiff soil ($Q_u = 0.57$ tsf) to an elevation 723.5 feet from Station 135+30 to 135+45. The removed soils should be replaced with compacted structural fill. The actual extent of the removal should be determined in the field during construction.

Based on our borings, the foundation soils along the **west** wall are expected to consist of medium stiff to stiff or hard silty clay to silty clay loam overlying loose silt or very stiff to hard silty loam to silty clay loam. We do not anticipate any removal and replacement.

Considering the foundation treatment at the east wall section, we recommend a nominal bearing resistance of 9,000 psf be considered for the design of MSE wall. Considering a bearing resistance factor of 0.65 (AASTHO, 2012), the factored bearing resistance will be 5,800 psf. We estimate the wall will apply a maximum factored equivalent uniform bearing pressure of about 3,800 psf at the highest wall section adjacent to the box culvert.

The nominal sliding resistance (ultimate value) between the foundation soil and the MSE wall mass can be calculated considering the frictional resistance provided by a foundation soil with an angle of 34 degrees. Sliding resistance factor, as per Table 11.5.7-1 of 2012 AASHTO, should be 1.0. Design lateral pressure from surcharge loads due to roadway traffic and construction equipment should be added to the lateral earth pressure load. The eccentricity lies within the middle third of the walls, and we estimate the resistance against overturning is also sufficient. Our analysis shows the walls with reinforced zone widths of 0.7 times the total height will be stable.



5.2.2 Settlement Analysis

We evaluated the potential consolidation settlements resulting from the proposed fill for the wall using *IDOT Cohesive Soil Settlement Estimate (2014)*. Our evaluations show the foundation soils will undergo long-term settlement of 1.0 inch or less which is acceptable.

5.2.3 Global Stability

The global stability of the proposed wall was analyzed based on the soil profile and the information provided in the cross section drawings. We have analyzed section at Station 134+69 for the west retaining wall where the wall reaches a maximum height of about 12 feet. Wang calculated a FOS of 6.2 (Appendix C-1) in undrained soil conditions (short-term) and FOS of 2.0 (Appendix C-2) in drained soil conditions (long-term). The minimum required factor of safety (FOS) for both short- and long- term conditions is 1.5 (IDOT, 1999). Since the borings drilled for the east wall shows similar soil condition along the west wall, and similar geometry we conclude there are no global stability concerns for the east wall too.

6.0 CONSTRUCTION CONSIDERATIONS

6.1 Site Preparation

Vegetation, topsoil, and debris should be cleared and stripped where foundations and structural fills will be placed. During excavation, the engineer should check for any unstable or unsuitable materials within the culvert and MSE wall foundations. Unstable and unsuitable soils should be removed and replaced with compacted structural fill as described in Section 6.3.

6.2 Excavation and Dewatering

Foundation excavations should be performed in accordance with local, state, and federal regulations. The potential effect of ground movements upon nearby utilities should be considered during construction. Any excavation that cannot be graded 1:2 (V: H) should be properly shored with temporary sheet piling or soil retention systems.

We do not expect the need of special dewatering system since the groundwater was encountered at the site 12 to 42 feet below the proposed culvert excavations; however, depending upon prevailing climatic conditions and the time of the year when construction takes place, control of runoff and maintenance of existing flows will require temporary water diversion and control. Any precipitation allowed to enter excavations should be immediately removed via sump pump. Any soil allowed to soften under



standing water should be removed and replaced with structural fill.

6.3 Filling and Backfilling

Fill material required to attain the final design subgrade elevations should be in accordance with Section 205 (IDOT 2012b). All fill and backfill materials should be pre-approved by the site engineer. The fill should be free of organic materials and debris.

Backfill materials must be pre-approved by the Resident Engineer. To backfill adjacent to the culvert we recommend the porous granular material conforming to the requirements specified in the IDOT Special Provision, *Granular Backfill for Structures*. Backfill material should be placed and compacted in accordance with the Special Provision.

6.4 Earthwork Operations

The required earthwork can be accomplished with conventional construction equipment. Moisture and traffic will cause deterioration of exposed subgrade soils. Precautions should be taken by the Contractor to prevent water erosion of the exposed subgrade. A compacted subgrade will minimize water runoff erosion.

Earth moving operations should be scheduled to not coincide with excessive cold or wet weather (early spring, late fall or winter). Any soil allowed to freeze or soften due to the standing water should be removed. Wet weather can cause problems with subgrade compaction.

It is recommended that an experienced geotechnical engineer be retained to inspect the exposed subgrade, monitor earthwork operations, and provide material inspection services during the construction phase of this project.

6.5 MSE Wall Construction

MSE walls should be constructed using the IDOT Special Provision GBSP38, *Mechanically Stabilized Earth Retaining Walls*.



7.0 QUALIFICATIONS

The analyses and recommendations submitted in this report are based upon the data obtained from the borings drilled at the locations shown on the boring logs and in Exhibit 3. This report does not reflect any variations that may occur between the borings or elsewhere on the site, variations whose nature and extent may not become evident until the course of construction. In the event that any changes in the design and/or location of the structures are planned, we should be timely informed so that our recommendations can be adjusted accordingly.

It has been a pleasure to assist Parsons Transportation Group, Inc. and the Illinois Department of Transportation on this project. Please call if there are any questions, or if we can be of further service.

Respectfully Submitted,

WANG ENGINEERING, INC.

Mohammed A. Kothawala, P.E., D.GE Senior Geotechnical Engineer Corina T. Farez, P.E., P.G. QA/QC Reviewer

Nesam S. Balakumaran, P.Eng. Project Geotechnical Engineer



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EXHIBITS









111X17 3420801.GPJ WANGENG.GDT 6/15/1

APPENDIX A

WANGENGINC 3420801.GPJ WANGENG.GDT 6/3/15

3420801.GPJ WANGENG.GDT 6/3/15 WANGENGINC

VANGENGINC 3420801.GPJ WANGENG.GDT 6/3/15

3420801.GPJ WANGENG.GDT 6/3/15 NANGENGINC

VANGENGINC 3420801.GPJ WANGENG.GDT 6/3/15

WANGENGINC 3420801.GPJ WANGENG.GDT 6/3/15

BORING LOG BSB3-01

WEI Job No.: 342-08-01

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ClientParsons Transportation Group, Inc.ProjectUS 45 - Millburn BypassLocationLake County, Illinois

Datum: NGVD Elevation: 727.31 ft North: 2096765.95 ft East: 1072303.24 ft Station: 135+25.69 Offset: 56.54' LT

Profile	Example in the second s	Sample Type	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ff)	Sample Type recovery Sample No	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	673.3 Medium dense, brown, fine to medium SAND 55_ Saturated		17	338	NP	17								
	 		18	3 4 8	0.16 B	22								
	665.6 - Brown, fine to medium SAND - Saturated -													
	663.3 Medium dense, gray SILT 662.3Saturated65		19	7 7 7	NP	19								
	Boring terminated at 65.00 ft													
ANGENG.GD1 6/3/15														
	/°											 Тл		
5.108 Be	Begin Drilling 09-18-2014 Complete Drilling 09-18-2014						While Drilling		20 20	.50 ft				
342(10	illing Contractor Wang Testing Servi	ces	. D	Drill Rig	J	D-5	0 AT	V	At Completion of Drilling	Ţ	18	.00 ft		
	iller K&K Logger S.W	lood	S	Che	ecked	by E	3. W	ilson	Time After Drilling NA					
Drilling Method 3.25" HSA; Boring backfilled upon completion						Depth to Water V NA The stratification lines represent the approximate boundary								

Page 2 of 2

between soil types; the actual transition may be gradual

VANGENGINC 3420801.GPJ WANGENG.GDT 6/3/15

APPENDIX B

AB. ŝ d C 000CF2 НО SIZE GRAIN

LAB.GDT ŝ d C 3420801 Ы SIZE GRAIN

IDH 3420801.GPJ WANGENG.GDT 6/8/15

SINCE 1982

Wang Engineering, Inc. 1145 N Main Street Lombard, IL 60148 Telephone: 630 953-9928 Fax: 630 953-9938

IDH Textural Classification Chart

Project: US 45 - Millburn Bypass Location: Lake County, Illinois Number: 342-08-01

APPENDIX C

APPENDIX D

Benchmark: LAK45 1A Station is located 2.8 mi North of Lindenhurst, 1.9 mi Northwest Old Mill Creek in Section 24, T46N, R10E. To reach from the junction of US Rt 45 and IL Rt 173 proceed south on US Rt 45 for 1.10 mi to the station located 53.5 ft east of the centerline of US Rt 45. Station is located 0.1 mi north of Miller Rd. 369.1 ft southeast of end of guardrail, 123.9 ft north of power pole (PP), 119.4 ft south of PP, 111.7 ft east of PP, and 2 ft west of orange fiberglass witness post. Note - Access to datum point is 0.50 ft below cap. PK nails were set in wood physical ties. Elevation: 759.13

Traffic Barrier

Fxistina

Proposed

R.O.W.

R.O.W.

(Typ. on

approach)

FILE NAME : PARSONS

LE NAME =	USER NAME =	DESIGNED - J.W.	REVISED -		
		CHECKED - T.C.U.	REVISED -	STATE OF ILLINOIS	
PARSUNS	PLOT SCALE =	DRAWN - S.R.	REVISED -	DEPARTMENT OF TRANSPORTATION	
	PLOT DATE =	CHECKED - J.W.	REVISED -		SHEET NO.

ta. N/A Sta. N/A							
- Ft. Headwater El.							
Prop.	Exist.	Prop.					
0.1		726.1					
0.1	N/A	726.1					
0.1		726.7					
0.1		726.7					
0.1	N/A	726.7					
0.1		726.9					
0.1		726.9					
0.1	N/A	726.9					
0.1		727.0					
0.1		727.0					
0.1	N/A	727.0					
0.1		727.3					
0.1		727.3					
0.1	N/A	727.3					

F.A.P. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
344	39 R	LAKE	430	257
		CONTRACT	NO. 6	OT 75
	ILLINOIS FED.	AID PROJECT		