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**STRUCTURE GEOTECHNICAL REPORT  
I-80 RECONSTRUCTION FROM RIDGE ROAD  
TO HOUBOLT ROAD  
SOUTHEAST RETAINING WALL ALONG RIVER ROAD  
WILL COUNTY, ILLINOIS**

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**For  
Stantec**

**350 North Orleans Street, Suite 1301  
Chicago, IL 60654**

**Submitted by  
Wang Engineering, Inc.  
1145 North Main Street  
Lombard, IL 60148**

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<b>9. Prepared by</b> Wang Engineering, Inc. 1145 N Main Street Lombard, IL 60148	<b>Contributor(s)</b> Author: Azza Hamad, PE Nesam Balakumaran, P.Eng QC/QA: Corina T. Farez, PE, PG PM: Azza Hamad, PE	<b>Contact</b> (630) 953-9928 ext. 1035 <a href="mailto:ahamad@wangeng.com">ahamad@wangeng.com</a>	
<b>10. Prepared for</b> Stantec 350 North Orleans Street Suite 1301 Chicago, IL, 60654	<b>Design Engineer</b> HBM Engineering Group, LLC John Saraceno, PE, SE	<b>Contacts</b> (312) 262-2245 <a href="mailto:Dave.Pieniazek@stantec.com">Dave.Pieniazek@stantec.com</a> (708) 236-0900 <a href="mailto:john.saraceno@hbmengineering.com">john.saraceno@hbmengineering.com</a>	
<b>11. Abstract</b>			
<p>A new retaining wall is proposed along northbound River Road to support a new 10.0-foot wide multi-use path in Will County, Illinois. The wall will be about 360.0-foot long, extending from Station 28+00.42 to Station 31+62.09. The face of the wall will be constructed about 27.4 to 28.0 feet east of the River Road centerline. The wall will have a maximum exposed height of 12.9 feet. This report provides geotechnical recommendations for the design and construction of the proposed retaining wall.</p> <p>The pavement structure along River Road consists of 4 to 11 inches of asphalt pavement over 5 to 17 inches of aggregate base. Along the proposed wall alignment, the foundation soils consists of up to 24.0 feet of stiff to hard silty clay to silty clay loam fill followed by 2.0 to 6.5 feet of stiff to hard silty clay and silty clay loam overlying medium dense to very dense silty loam to loam and very dense sandy gravel. Dolostone bedrock was encountered at 565 to 562 feet elevation. The groundwater level was measured at elevations ranging from 570 to 566 feet.</p> <p>The proposed retaining wall will be in a fill section. Fill wall types such as Mechanically Stabilized Earth (MSE) and Reinforced Concrete Cantilever (RCC) will require additional open cut excavations into the existing embankment slope and possibly a temporary soil retention system. Cut wall types such as drilled soldier pile walls could be considered as they will not require excavation and temporary support, thus would be easier to build and more economical.</p> <p>The designer envisions a drilled soldier-pile wall type at the site. Geotechnical parameters for the design and construction of soldier pile walls are provided. A cantilevered pile embedment depth to a minimum pile tip elevation of 564.5 feet is necessary to achieve a minimum factor of safety of 1.7 for global stability. We understand the designer proposes soldier piles installed in the bedrock.</p> <p>The drilled soldier-pile wall construction should expect hard drilling conditions in certain areas along the wall as discussed in the report. Excavation may be required.</p>			
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**FOR**  
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## 1.0 INTRODUCTION

This report presents the results of our subsurface investigation, laboratory testing, geotechnical evaluations, and recommendations in support of the design and construction of a new retaining wall proposed along northbound River Road just south of the bridge carrying River Road over Interstate 80 (I-80) in Troy Township, Illinois. The project area is located in west central Will County, along I-80, about 1.0 mile southwest of the City of Joliet limits. On the USGS *Channahon Quadrangle 7.5 Minute Series* map, the project is located in SW  $\frac{1}{4}$  of Section 28, Tier 35 N, Range 9 E of the Third Principal Meridian (Exhibit 1).

Wang Engineering, Inc. (Wang) understands the proposed work will also include the replacement of the River Road Bridge and the reconstruction and widening of about 300 and 350 feet of the approach roadway north and south of the bridge replacement, respectively. New retaining walls are proposed along the northeast and southeast sides of the River Road Bridge over I-80 to retain the new fill for the roadway widening. This report addresses the southeast wall. The northeast wall is addressed in a separate Structure Geotechnical Report (SGR). The River Road Bridge over I-80 replacement, new retaining walls along the River Road approach embankments, and the reconstruction of a section of River Road are part of the proposed widening and reconstruction of I-80 from east of Ridge Road to west of Houbolt Road in Will County, Illinois. The River Road Bridge, retaining walls, and roadway will be reconstructed as part of Advanced Contract CR-2.

The purpose of this investigation was to characterize the site soil and groundwater conditions, perform geotechnical analyses, and provide recommendations for the design and construction of the proposed retaining wall. Recommendations pertaining to the River Road roadway reconstruction will be included in the Roadway Geotechnical Report that will be prepared for the I-80 mainline (Contract ML-1) whereas recommendations pertaining to the construction of the River Road Bridge and northeast retaining wall are provided in separate SGRs.

## **1.1 Existing Structure and Ground Conditions**

There is no existing structure at the proposed retaining wall site. The site surface elevation slopes gently east toward the DuPage River, from as high as 575.0 feet to as low as 562.0 feet near the River. DuPage River runs south about 0.25 miles east of the River Road Bridge over I-80. Surface elevations are about 593.0 feet along River Road near the abutments and about 571.0 feet along I-80 near the piers. Along River Road, the roadway elevation varies from 593.0 to 573.0 feet.

In the project area (see Exhibit 2), and below about 10- to 20-foot thick embankment fill, about 15-foot thick overburden made up of low to moderate plasticity, medium to high strength, and low to moderate moisture content silty clayey diamicton resting over granular, very dense, low compressibility sand and gravel outwash unconformably covers the bedrock (Bauer et al. 1991, Hansel and Johnson 1996, Leighton et al. 1948, Willman et al. 1971). The bedrock is made up of shale and dolostone. Top of bedrock is mapped at about 565.0 feet elevation. The site is located within the inactive Sandwich Fault Zone (Kolata 2005). The shallow bedrock is highly weathered and may show the presence of cavities more likely filled with fine sediment. Records of mining activity in the vicinity of the bridge are missing. Neither the overburden nor the upper bedrock is known to include significant sources of water supply (Woller and Sanderson 1983).

## **1.2 Proposed Structure**

Based on the *GPE* drawing prepared by HBM and dated January 21, 2022, Wang understands the proposed retaining wall will measure about 360.0 feet in length, extending along northbound River Road from Station 28+00.42 to Station 31+62.09. The front face of the wall will be constructed at a distance of about 27.4 to 28.0 feet east of the existing River Road centerline. The wall will support a new 10.0-foot wide multi use path to be constructed along northbound River Road. A drilled soldier-pile wall type installed into the bedrock is currently shown on the in-progress *GPE* sheets. Based on the drawings and *Cross-Sections*, we estimate the wall will have a maximum exposed height of approximately 12.9 feet at Station 28+60.58 where the wall meets the River Road Bridge south approach. The *GPE* drawing is included as Appendix E, whereas the *Cross-Sections* are included as Appendix F.

## **2.0 METHODS OF INVESTIGATION**

The following sections outline the subsurface and laboratory investigations performed by Wang.

### **2.1 Field Investigation**

The subsurface investigation consisted of three retaining wall borings, designated as RIV-RWB-07 to

RIV-RWB-09, four hand auger borings, designated as RIV-RWB-06-HA to RIV-RWB-09-HA, two subgrade/stability borings, designated as RIV-SGB-03 and RIV-SGB-04, and one bridge boring, designated as RIV-BSB-03, drilled by Wang in November of 2021. The borings were drilled from elevations of 593.1 to 580.3 feet and were advanced to depths of 14.5 to 44.5 feet bgs. The as-drilled northings and eastings were acquired with a mapping-grade GPS unit. Stations, offsets, and elevations were provided by Stantec. Boring location data are presented in the *Boring Logs* (Appendix A) and the as-drilled boring locations are shown in the *Boring Location Plan* (Exhibit 3).

A truck-mounted drilling rig, equipped with hollow stem augers, was used to advance and maintain open boreholes. Soil sampling was performed according to AASHTO T206, "*Penetration Test and Split Barrel Sampling of Soils.*" The soil in the bridge and retaining wall borings was sampled at 2.5-foot intervals to 30.0 feet bgs and at 5.0-foot intervals thereafter to the boring termination depth or top of bedrock whereas the soil in the stability borings was sampled continuously to 10.0 feet bgs and at 2.5-foot intervals thereafter to the boring termination depth. Jackhammer driven Geoprobe samplers were used to continuously sample the soil in the hand auger borings. Bedrock cores were obtained from Borings RIV-BSB-03, RIV-RWB-07, and RIV-RWB-09 in 3 to 10-foot runs with an NWD4-sized core barrel. Soil samples collected from each sampling interval were placed in sealed jars, and rock cores were placed into boxes, and transported to the laboratory for further examination and testing.

Field boring logs, prepared and maintained by a Wang field engineer, included lithological descriptions, visual-manual soil (IDH Textural) classifications, results of Rimac and pocket penetrometer unconfined compressive strength tests, and results of Standard Penetration Tests (SPT) recorded as blows per 6 inches of penetration.

Groundwater levels were measured while drilling and at completion of each of the borings. Given the location of the boreholes and limited access requiring traffic control, it was not feasible to delay backfilling of the borings to obtain 24-hour water level measurements. Each borehole location was backfilled upon completion with lean grout, soil cuttings, and/or bentonite chips and, where necessary, the pavement surface was restored as much as possible to its original condition.

## **2.2 Laboratory Testing**

The soil samples were tested in the laboratory for moisture content (AASHTO T265). Atterberg limits (AASHTO T89 and T90) and particle size (AASHTO T88) analyses were performed on selected samples. Unconfined compressive strength tests were performed on selected bedrock cores. Field visual descriptions of the soil samples were verified in the laboratory and index tested soils were

classified according to the IDH Soil Classification System. The laboratory test results are shown in the *Boring Logs* (Appendix A) and in the *Laboratory Test Results* (Appendix B).

### **3.0 INVESTIGATION RESULTS**

Detailed descriptions of the soil conditions encountered during the subsurface investigation are presented in the attached *Boring Logs* (Appendix A) and in the *Soil Profile* (Exhibit 4). Please note that strata contact lines represent approximate boundaries between soil types. The actual transition between soil types in the field may be gradual in horizontal and vertical directions.

Our subsurface investigation results fit into the local geologic context. The borings drilled in the project area revealed the native sediments consists of silty clay to silty clay loam diamicton (unit 2) with occasional lenses of silt and sand, over sand and gravel outwash (unit 3) resting over weathered bedrock. Unit 3 is water-bearing with seasonal fluctuation. Top of dolostone bedrock was encountered at elevations of 565 to 562 feet (23.5 to 30.0 feet bgs) as predicted based on geologic data.

#### **3.1 Lithological Profile**

Borings RIV-BSB-03, RIV-RWB-07 to RWB-09, RIV-SGB-03, and RIV-SGB-04 were drilled along River Road and encountered 4 to 11 inches of asphalt pavement overlying 5 to 17 inches of sandy gravel aggregate base. In descending order, the general lithologic succession encountered beneath the pavement or at the surface includes: 1) man-made ground (fill); 2) stiff to hard silty clay and silty loam; 3) medium dense to very dense silty loam to loam; 4) very dense sandy gravel; and 5) strong, very poor to poor quality dolostone.

##### *1) Man-made ground (fill)*

Beneath the pavement or at the surface, the borings encountered up to 24.0 feet of cohesive fill. The cohesive fill consists of stiff to hard, black, brown, and gray silty clay to silty clay loam with unconfined compressive strength ( $Q_u$ ) values of 1.0 to 7.7 tsf and moisture content values of 10 to 22%. Laboratory index testing on a sample from the fill layer showed liquid limit (LL) and plastic limit (PL) values of 29 to 35% and 15 to 19%, respectively. Rig chatter indicating the presence of cobbles was noted within this layer at a depth of 16.0 feet (elevation 578 feet) in Boring RIV-BSB-03.

A 2- to 43-inch thick layer of buried, black silty clay to silty clay loam topsoil with moisture content values of 25 to 26% was sampled beneath the fill in Borings RIV-RWB-08, RIV-RWB-09, RIV-



RWB-09-HA, and RIV-BSB-03. The presence of this layer most likely indicates the boundary between fill and natural soils.

2) *Stiff to hard silty clay and silty loam*

Beneath the fill, at elevations of 577 to 570 feet, the borings advanced through 2.0 to 6.5 feet of stiff to hard, brown to gray silty clay to silty clay loam. The silty clay to silty clay loam is characterized by  $Q_u$  values of 1.0 to 4.0 tsf and moisture content values of 21 to 29%. This layer was encountered to the termination depth in Borings RIV-RWB-07-HA and RIV-RWB-08-HA.

3) *Medium dense to very dense silty loam to loam*

At depths of 12.0 to 24.0 feet bgs, or elevations of about 570 to 568 feet, the borings encountered 0.7 to 2.5 feet of medium dense to very dense, brown to gray, damp to saturated silty loam to loam. This soil unit has N-values of 12 to 23 blows per foot and a moisture content value of 11 to 15%. Rig chatter indicating the presence of cobbles was noted within this layer at a depth of 25.5 feet (elevation 569 feet) in Boring RIV-BSB-03.

4) *Very dense sandy gravel*

At elevations of 570 to 568 feet, the borings advanced through 2.0 feet of very dense, brown, damp to saturated sandy gravel with N-values of 60 blows per foot to more than 50 blows per inch and moisture content values of 7 to 12%. Rig chatter indicating the presence of cobbles was noted within this layer at a depth of 20.0 feet (elevation 566 feet) in Boring RIV-RWB-09.

At elevations of 567 to 565 feet, the borings advanced through up to 2.5 feet of very dense, brown, damp to saturated weathered dolostone bedrock. This soil unit has N-values of 50 blows per 3 inches to 50 blows per inch and moisture content values of 2 to 6%.

5) *Strong, very poor to poor quality dolostone*

At elevations of 565 to 562 feet (23.5 to 30.0 feet bgs), the borings encountered strong, very poor to poor quality, highly to moderately weathered dolostone bedrock. The rock quality designation (RQD) ranges from 0 to 26% and uniaxial compressive strength testing revealed  $Q_u$  values of 6,081 to 7,459 psi. The bedrock core data are shown in the *Bedrock Core Photographs* (Appendix C).

### 3.2 Groundwater Conditions

Groundwater was encountered while drilling at elevations of 570 to 566 feet (14.0 to 26.0 feet bgs) within the sandy gravel and weathered bedrock layers. At the completion of drilling, the groundwater was observed in Borings RIV-RWB-07-HA and RIV-RWB-09-HA at elevations of 570 to 568

feet (12.0 to 16.0 feet bgs). For the purpose of analysis, the design groundwater elevation is considered at elevation 570 feet. It should be noted that groundwater levels might change with seasonal rainfall patterns and long-term climate fluctuations or may be influenced by local site conditions.

#### **4.0 FOUNDATION ANALYSIS AND RECOMMENDATIONS**

The retaining wall will support a new 10.0-foot wide multi-use path proposed along northbound River Road. Based on the *GPE* and *Cross-Sections* (Appendixes E and F), the wall will have a total length of 360.0 feet and a maximum exposed height of 12.9 feet near Station 28+60.58. The proposed wall will retain the new fill to be placed for the roadway widening. Additionally, the plans indicate the existing grade in front of the wall will be lowered by up to 4.0 feet and the finished grade in front of the wall will be graded at slopes ranging from 1:2.5 to 1:3 (V: H). As such, the wall is a combination of cut and fill.

Fill wall types, such as Mechanically Stabilized Earth (MSE) and Reinforced Concrete Cantilever (RCC) walls would require large open cut excavations into the existing embankment slope, temporary soil retention systems, and will impact the existing roadway. The construction of these wall types would likely also require more backfilling thus longer construction time. In our opinion, non-gravity wall types such as a sheet pile or soldier pile type wall would be more appropriate considering the soil conditions, constructability, and cost. A driven sheet pile wall type will not be feasible due to potential difficulty of driving the sheet piles in cohesive soils with unconfined compressive strength values of greater than 4.5 tsf. The final wall type should be selected based on a wall-type study including cost and construction considerations. We understand a drilled-soldier pile wall type installed in the bedrock is proposed by the designer. Recommendations for the design and construction of the proposed wall type are discussed in the following sections.

##### **4.1 Seismic Design Considerations**

Seismic design is not required for retaining wall structures located in Seismic Performance Zone (SPZ) 1 in accordance with the IDOT *Bridge Manual* (2012).

##### **4.2 Soldier-Pile and Lagging Wall**

A soldier-pile wall type could be considered at this location. If soldier piles are designed to support the wall, they could be installed by setting them within prebored holes with diameters sized in accordance with IDOT criteria. The wall should be designed for both lateral earth pressure and lateral deformation. The embedment depth in moment equilibrium for the wall sections should be designed in accordance with the AASHTO LRFD guidelines (AASHTO 2020).

Generally, both granular soils and overconsolidated clayey soils, such as the stiff to hard silty clay to silty clay loam encountered in the borings will exhibit lower overall shear strength in the long-term condition. Therefore, in accordance with AASHTO (2020), the lateral earth pressure analysis should be performed for walls in the long-term (drained) condition using the soil parameters recommended in Table 1. Elevations provided in Table 1 are based on the average layer elevations across the soil profile and may vary from one boring location to another. The active and passive earth pressure coefficients are provided for straight backfill behind the wall and a slope of 1:3 (V: H) in front of the wall.

The design of the wall should ignore 3.0 feet of soil in front of the wall measured from the finished ground surface elevation in providing passive pressure due to excavations required for installation of concrete facing, drainage systems, and frost-heave conditions. In developing the design lateral pressure, the pressure due to construction equipment surcharge loads should be added to the lateral earth pressure. Drainage behind the wall should be in accordance with IDOT guidelines (IDOT 2012). The water pressures should be added to the earth pressure if drainage is not provided.

Table 1: Drained Geotechnical Parameters for Design of Soldier-Pile Walls

Elevation Range (feet) Soil Description	Unit Weight, $\gamma$ (pcf)	Drained Shear Strength Properties		Earth Pressure Coefficients	
		Cohesion (psf)	Friction Angle ( $^{\circ}$ )	Active Pressure (Straight)	Passive Pressure (straight to 1V:3H)
Proposed Finished Grade to Existing Grade NEW FILL	120	0	30	0.33	--
Existing Grade to EL 573 Stiff to Hard SI CLAY to SI CLAY LOAM FILL	120	100	30	0.33	--
EL 573 to 570 V Stiff SI CLAY to SI CLAY LOAM	120	100	30	0.33	2.29 <sup>(1)</sup>
EL 570 to 567 M Dense SILTY LOAM	58 <sup>(2)</sup>	0	30	0.33	3.00
EL 567 to 565 V Dense SANDY GRAVEL	58 <sup>(2)</sup>	0	33	0.29	3.39
EL 565 to 563 <sup>(3)</sup> V Dense WEATHERED BEDROCK	63 <sup>(2)</sup>	0	35	0.27	3.69

(1) Earth pressure coefficients for 1:3 (V: H) front slope; (2) Submerged unit weight; (3) Approximate top of Bedrock

The lateral deformation of the wall should be designed for movement and moment fixity at the base of the pile. The roadway and utilities should not be impacted by the lateral movement of the wall. Therefore, the design of the soldier pile wall should establish lateral movement limits. The evaluations should be performed using the recommended soil parameters shown in Tables 2 and 3, via the p-y curve (COM624) method. Elevations provided in Tables 2 and 3 are based on the average layer elevations across the profile and may vary from one boring location to another.

Table 2: Recommended Soil Parameters for Lateral Load Analysis of Soldier Pile Walls

Elevation Range (feet) Soil Type (Layer)	Unit Weight, $\gamma$ (pcf)	Undrained Shear Strength, $c_u$ (psf)	Estimated Friction Angle, $\Phi$ ( $^\circ$ )	Estimated Lateral Soil Modulus Parameter, k (pci)	Estimated Soil Strain Parameter, $\epsilon_{50}$ (%)
Finished Grade to Existing Grade NEW FILL	120	1000	0	500	0.7
Existing Grade to EL 573 Stiff to Hard SI CLAY to SI CLAY LOAM FILL	120	2500	0	1000	0.5
EL 573 to 570 V Stiff SI CLAY to SI CLAY LOAM	120	3500	0	1000	0.5
EL 570 to 567 M Dense SILTY LOAM	58 <sup>(1)</sup>	0	30	60	--
EL 567 to 565 V Dense SANDY GRAVEL	58 <sup>(1)</sup>	0	33	125	--
EL 565 to 563 <sup>(2)</sup> V Dense WEATHERED BEDROCK	63 <sup>(1)</sup>	0	35	125	--

(1) Submerged unit weight; (2) Approximate top of bedrock

Table 3: Recommended Bedrock Parameters for Lateral Load Analysis of Soldier Pile Walls  
 (Borings RIV-BSB-03, RIV-RWB-07, and RIV-RWB-09)

Bedrock	Total Unit Weight, $\gamma$ (pcf)	Modulus of Rock Mass (ksi)	Poisson's Ratio, $\mu$	Uniaxial Compressive Strength (psi)	RQD (%)	Strain Factor
Dolostone	140	300	0.3	6,081 to 7,459	0 to 12	0.0005

### 4.3 Settlement

On the east side of River Road, where the retaining wall is proposed, the widening for the multi-use path will require the placement of up to 9.0 feet of new fill along the existing embankment slopes. Wang has performed evaluations of the potential consolidation settlements resulting from the proposed grade change for the wall. Settlement estimates have been made based on correlations to measured index properties obtained from the laboratory tests (Appendix B). Based on the soil conditions, we estimate the foundation soils will undergo long-term settlements of less than 1.0 inch under the new fill.

### 4.4 Global Stability

The global stability of the proposed wall was analyzed based on the soil profile described in Section 3.1 and the information provided in the design drawings and cross-sections. The stability was analyzed at the critical section near Station 28+50 where the maximum exposed height is 12.9 feet. The minimum required factor of safety (FOS) is 1.7 in both short-term (undrained) and long-term (drained) conditions (IDOT 2020a).

Details of the global stability analysis with critical failure surfaces and results are presented in Appendix D. The short-term and long-term analyses do not consider the resistance from the top 3.0 feet measured from the proposed finished grade at the front face of the wall. We estimate the wall will have an adequate FOS of 3.4 (Appendix D-1) in the undrained condition. Global stability evaluations were performed to estimate the minimum pile tip elevation required to achieve an FOS of 1.7 in the drained condition. The embedded portion of the cantilevered piles will provide resistance against the slope instability above the tip of the piles. The results of our analysis are summarized in Table 4. We recommend that the wall tip elevations be installed at or deeper than the minimum elevation shown in Table 4 to provide long-term global stability FOS values of at least 1.7 as shown in Appendix D-2. It should be noted that typically, the lateral earth pressure and deformation analyses will determine the minimum embedment depth for cantilevered pile walls. Therefore, the designer should perform other analyses including lateral earth pressure and deflection analyses to determine the required design pile embedment. We understand the designer proposes soldier piles installed in the bedrock.

Table 4: Results of Global Stability Analysis

Station	Reference Boring(s)	Exposed Wall Height (feet)	Short-term (Undrained) Condition		Long-term (Drained) Condition	
			FOS	Minimum Tip Elevation (feet)	FOS	Minimum Tip Elevation (feet)
28+50	RIV-BSB-03 and RIV-RWB-06HA	12.9	3.5	-/-	1.7	564.5

## 5.0 CONSTRUCTION CONSIDERATIONS

### 5.1 Site Preparation

Vegetation, surface topsoil, and debris should be cleared and stripped where the structure will be placed. If unstable or unsuitable materials are exposed during excavation, they should be removed and replaced with compacted structural fill as described in Section 5.3.

### 5.2 Excavation, Dewatering, and Utilities

Excavations should be performed in accordance with local, state, and federal regulations. The potential effect of ground movements upon nearby utilities should be considered during construction. Excavations for the construction of the wall should be sloped at no steeper than 1:2 (V: H). Any slope that cannot be graded at 1:2 (V:H) should be properly shored in accordance with the temporary sheet piling charts provided in *IDOT Design Guide-Simplified Temporary Sheet Piling Design Charts* (IDOT 2020a). Dewatering may be necessary if groundwater perched within the granular layers is encountered

For cantilevered pile walls, it should be noted that hard drilling conditions, frequent rig chatter, and possible cobbles were noted in Borings RIV-BSB-03 and RIV-RWB-09 at elevations of 577 to 566 feet (16.0 to 27.5 feet bgs), and should be anticipated during pile driving or drilling. Pile shoes or excavation may be needed due to the presence of cobbles as observed by drill rig chatter during drilling.

Groundwater was encountered while drilling at elevations of 570 to 566 feet (14.0 to 26.0 feet bgs) within the sandy gravel and weathered bedrock layers. At the completion of drilling, the groundwater was observed in Borings RIV-RWB-07-HA and RIV-RWB-09-HA at elevations of 570 to 568 feet (12.0 to 16.0 feet bgs). We do not anticipate groundwater concerns during the construction of the cantilevered soldier pile walls if piles are driven; however, if drilled soldier piles are designed, temporary casing and wet installation methods will be needed for drilling and setting into the granular layers below an elevation of 570 feet. Additionally, perched or temporary water may be encountered during times of heavy precipitation while excavating within the upper fill soils and will require dewatering efforts. Water that does accumulate in open excavations by seepage or runoff should be immediately removed by sump pump. Any soils allowed to soften under standing water should be removed and replaced with compacted fill as described in Section 5.3.

The construction of the new walls should be coordinated with the pile driving for the proposed River Road bridge replacement and the Contractor should perform a vibration analysis and provide vibration monitoring during construction, if needed.

### **5.3 Filling and Backfilling**

Fill material used to attain final design elevations should be pre-approved, compacted, cohesive or granular soil conforming to Section 204, *Borrow and Furnished Excavation* (IDOT 2016). The fill material should be free of organic matter and debris and should be placed in lifts and compacted according to Section 205, *Embankment* (IDOT 2016). Backfill materials must be pre-approved by the Resident Engineer.

### **5.4 Earthwork Operations**

The required earthwork can be accomplished with conventional construction equipment. Moisture and traffic will cause deterioration of exposed subgrade soils. Precautions should be taken by the Contractor to prevent water erosion of the exposed subgrade. A compacted subgrade will minimize water runoff erosion.

Earth moving operations should be scheduled to not coincide with excessive cold or wet weather (early spring, late fall or winter). Any soil allowed to freeze or soften due to the standing water should be removed. Wet weather can cause problems with subgrade compaction.

It is recommended that an experienced geotechnical engineer be retained to inspect the exposed subgrade, monitor earthwork operations, and provide material inspection services during the construction phase of this project.

## **6.0 QUALIFICATIONS**

The analysis and recommendations submitted in this report are based upon the data obtained from the borings drilled at the locations shown on the boring logs and in Exhibit 3. This report does not reflect any variations that may occur between the borings or elsewhere on the site, variations whose nature and extent may not become evident until the course of construction. In the event that any changes in the design and/or location of the structure are planned, we should be timely informed so that our recommendations can be adjusted accordingly.

It has been a pleasure to assist Stantec, HBM Engineering Group, LLC, and the Illinois Department of Transportation on this project. Please call if there are any questions, or if we can be of further service.

Respectfully Submitted,

### **WANG ENGINEERING, INC.**

Azza Hamad, P.E.  
Senior Geotechnical Engineer

Nesam Balakumaran, P.Eng.  
Geotechnical Project Engineer

Corina T. Farez, P.E., P.G.  
QC/QA Reviewer



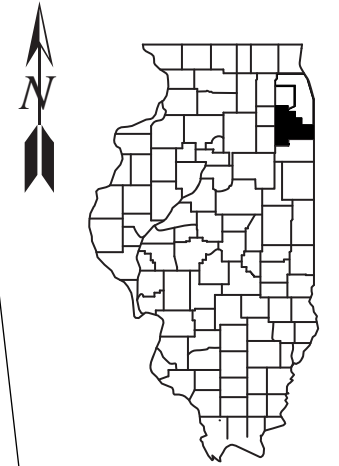
## **REFERENCES**

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- BAUER, R.A., CURRY, B.B., GRAESE, A.M., VAIDEN, R.C., SU, W.J., AND HASEK, M.J. (1991) "*Geotechnical Properties of Selected Pleistocene, Silurian, and Ordovician Deposits of Northeastern Illinois.*" Environmental Geology 139, Illinois State Geological Survey.
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- LEIGHTON, M.M., EKBLAW, G.E., and HORBERG, L. (1948) "*Physiographic Divisions of Illinois.*" The Journal of Geology, v. 56. p. 16-33.
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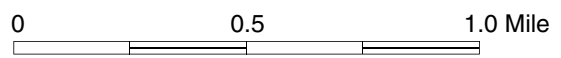
## **EXHIBITS**



SOUTHEAST RETAINING WALL ALONG RIVER ROAD  
 SW 1/4 of Section 28, T 35N, R 9E of 3rd PM



Will County

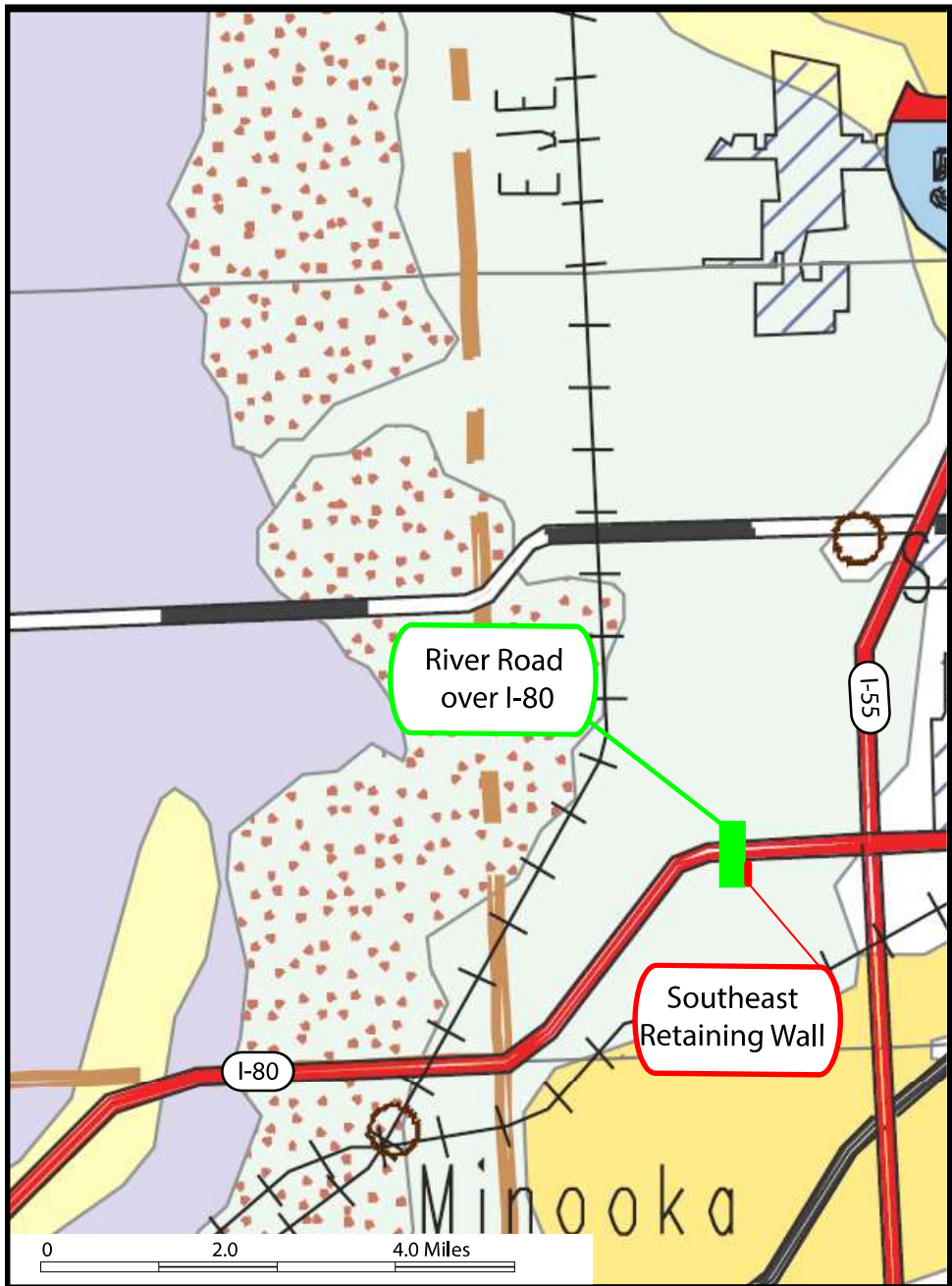


SITE LOCATION MAP: SOUTHEAST RETAINING WALL ALONG RIVER ROAD; I-80 RECONSTRUCTION FROM EAST OF RIDGE RD TO HOUBOLT RD, WILL COUNTY, ILLINOIS

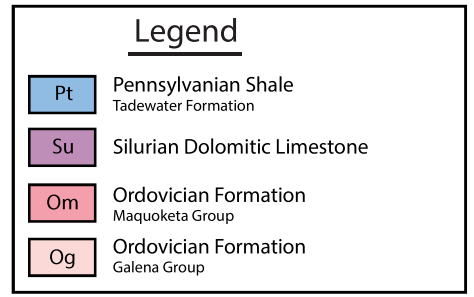
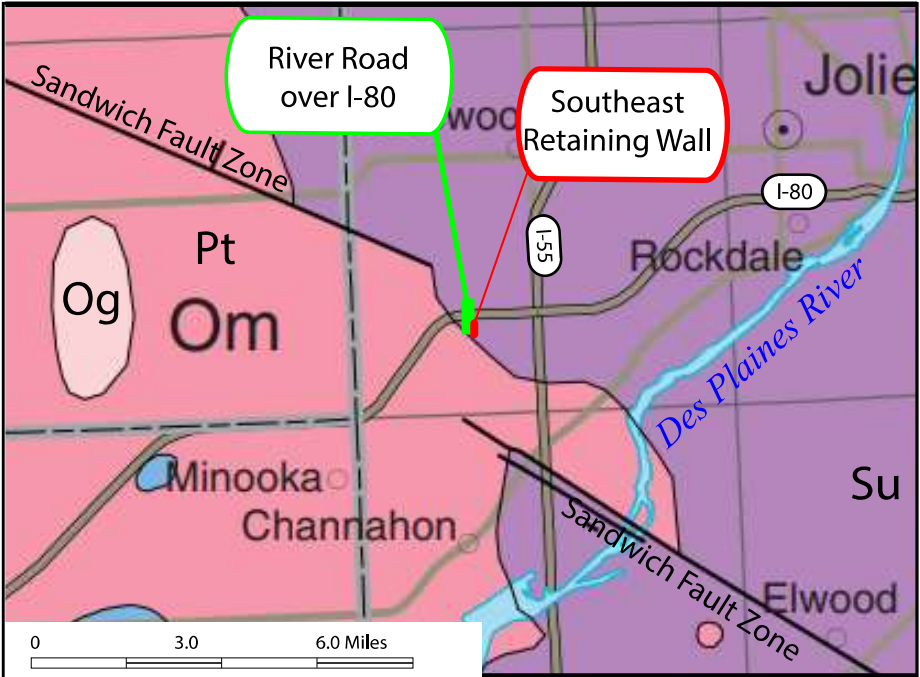
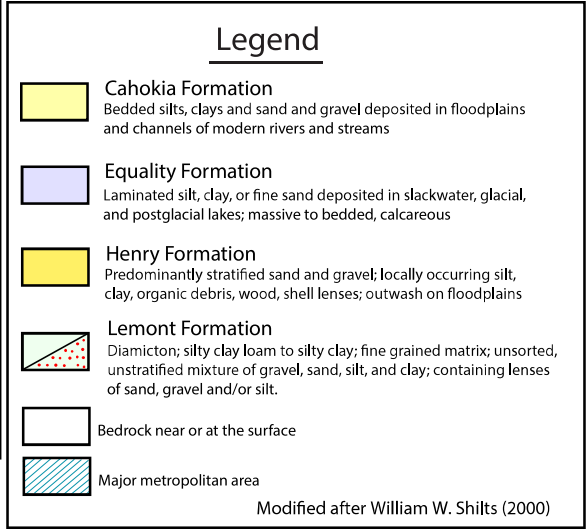
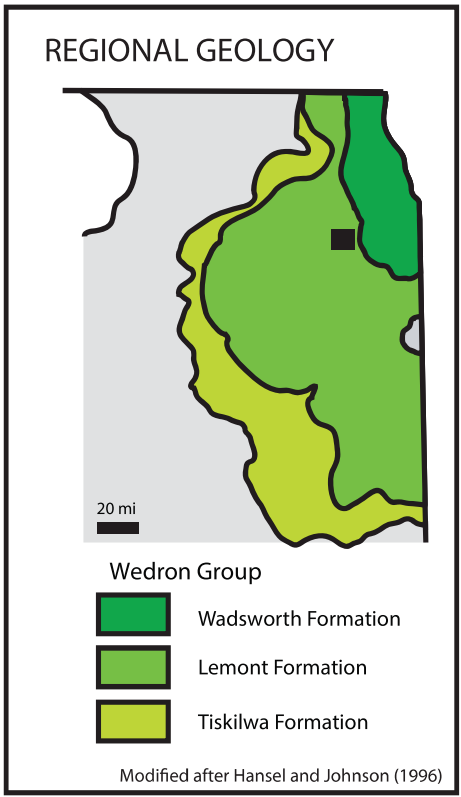
SCALE: GRAPHICAL	<b>EXHIBIT 1</b>	DRAWN BY: J. Benzen CHECKED BY: A. Hamad
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 <b>Wang Engineering</b>	1145 N. Main Street Lombard, IL 60148 www.wangeng.com

FOR STANTEC	255-39-01
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Modified after William W. Shilts (2000)

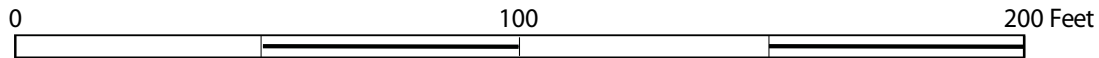
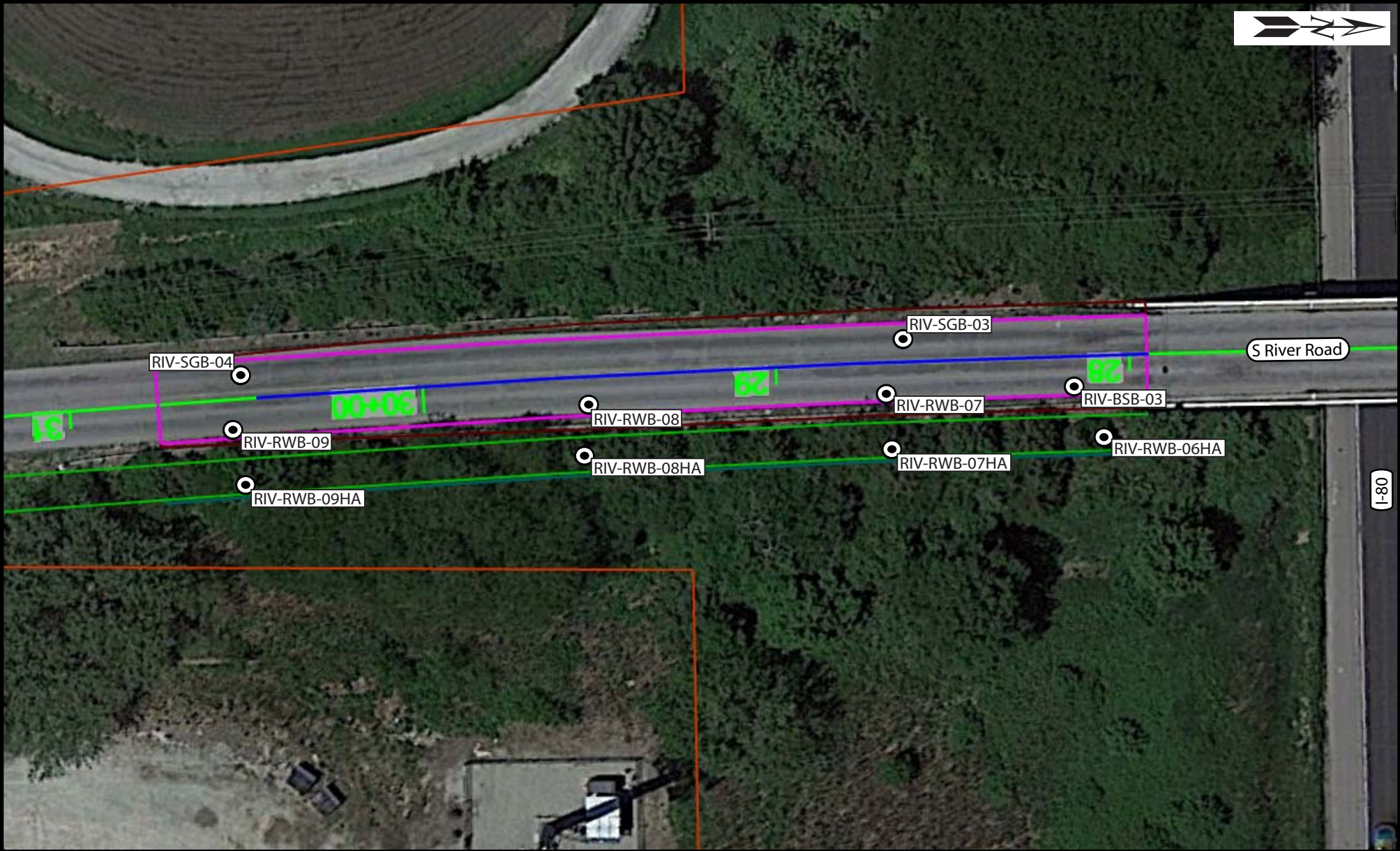


SITE AND REGIONAL GEOLOGY: SOUTHEAST RETAINING WALL ALONG RIVER ROAD, I-80 RECONSTRUCTION FROM EAST OF RIDGE ROAD TO HOUBOLT ROAD, WILL COUNTY, ILLINOIS

SCALE: GRAPHICAL      EXHIBIT 2      DRAWN BY: C. Marin  
CHECKED BY: L. Iordache

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Modified after Dennis R. Kolata (2005)



Legend

⊙ Boring Location

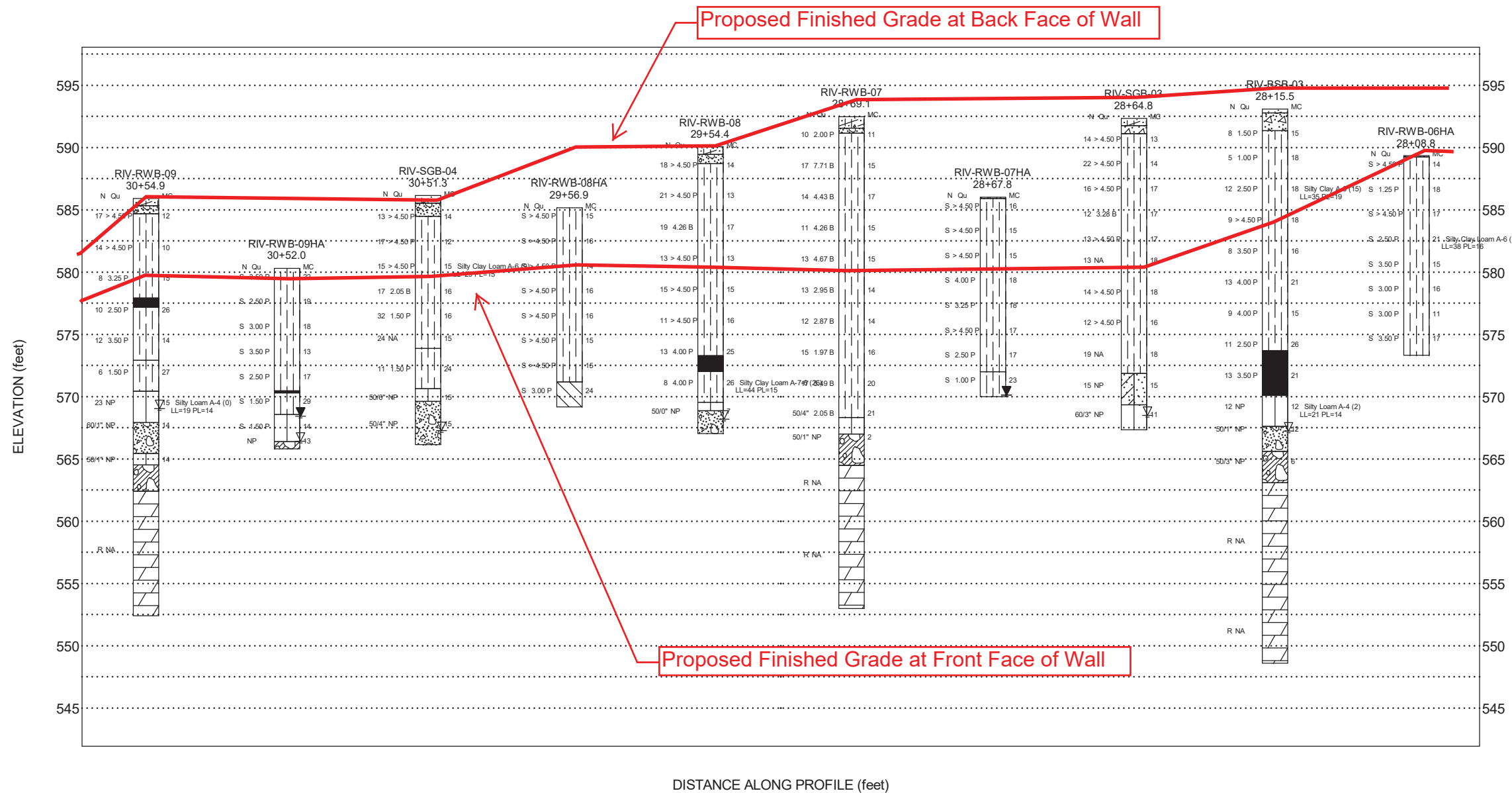
BORING LOCATION PLAN: SOUTHWEST RETAINING WALL ALONG RIVER ROAD; I-80 RECONSTRUCTION FROM EAST OF RIDGE ROAD TO HOUBOLT ROAD, WILL COUNTY, ILLINOIS

SCALE: GRAPHICAL | **EXHIBIT 3** | DRAWN BY: J. Bensen  
CHECKED BY: A. Hamad



1145 N. Main Street  
Lombard, IL 60148  
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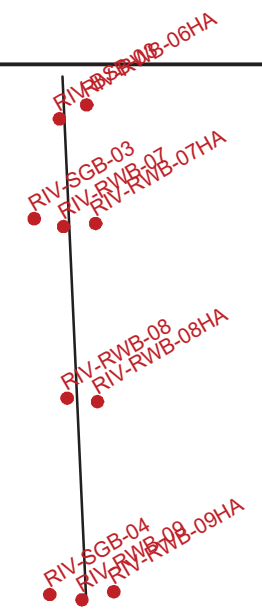
FOR STANTEC | 255-39-01



DISTANCE ALONG PROFILE (feet)

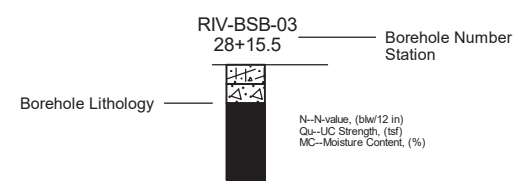
**Lithology Graphics**

- |  |                      |  |                             |  |                                 |  |                                 |
|--|----------------------|--|-----------------------------|--|---------------------------------|--|---------------------------------|
|  | Pavement             |  | Crushed stone               |  | IDH Silty Clay, Silty Clay Loam |  | Topsoil                         |
|  | IDH Silt, Silty Loam |  | Gravelly sand, sandy gravel |  | Weathered bedrock               |  | Dolomite or Dolomitic Limestone |
|  | IDH Clay             |  | IDH Loam                    |  |                                 |  |                                 |

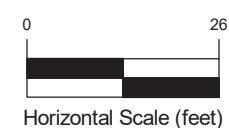


Site Map Scale 1 inch equals 95 feet

**Explanation:**



- Water Level Reading at time of drilling.
- Water Level Reading 24-hr after drilling or at end of drilling



Vertical Exaggeration: 2.5x

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1145 N Main Street  
Lombard, IL 60148

**Soil Profile**  
**Southeast Retaining Wall Along River Road**



I-80 Reconstruction, Ridge Road to Houbolt Road  
Will County, Illinois

JOB NUMBER	PLATE NUMBER
255-39-01	EXHIBIT 4

## **APPENDIX A**



wangeng@wangeng.com  
 1145 N MAIn Street  
 Lombard, IL 60148  
 Telephone: (630) 953-9928  
 Fax: (630) 953-9938

# BORING LOG RIV-BSB-03

WEI Job No.: 255-39-01

Client **Stantec**  
 Project **I-80 Reconstruction, Ridge Road to Houbolt Road**  
 Location **Will County, Illinois**

Datum: NAVD 88  
 Elevation: 593.11 ft  
 North: 1755103.18 ft  
 East: 1016269.75 ft  
 Station: 28+15.5  
 Offset: 8.3 LT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)		
	592.84	1-inch thick ASPHALT --PAVEMENT--								567.6	--%Gravel=11.2-- --%Sand=25.4-- --%Silt=55.9-- --%Clay=7.5-- --A-4 (2)-- --rig chatter; possible cobbles--								
	591.4	White and gray SANDY GRAVEL; damp --AGGREGATE BASE--			1	5 4 4	1.50	15		565.6	Very dense, brown and reddish brown SANDY GRAVEL; wet --RDR 3--	563.1		11	50/1"		NP	12	
		Stiff to hard, brown and gray SILTY CLAY to SILTY CLAY LOAM, trace gravel; damp --FILL-- --RDR 2-3--	5		2	2 2 3	1.00	18			Very dense, brown and reddish brown, weathered dolostone fragments; saturated --Weathered BEDROCK--			12	56/3"		NP	6	
		--L <sub>L</sub> (%)=35, P <sub>L</sub> (%)=19-- --%Gravel=0.8-- --%Sand=5.6-- --%Silt=59.9-- --%Clay=33.7-- --A-6 (15)--			3	2 3 9	2.50	18			Strong, light greenish gray, very poor to poor quality, DOLOSTONE; Moderately to closely spaced, highly weathered, horizontal and vertical JOINTS, with <0.05 inch opening, slicken to slightly rough walls, and <0.2 inch thick clay infill. --RUN 1: 30.0 to 40.0 feet-- --Recovery: 90%-- --RQD: 8%-- --Qu=6,081 psi--			13					
			10		4	4 4 5	4.50	18						14					
					5	3 4 4	3.50	16						15					
			15		6	4 6 7	4.00	21						16					
		--rig chatter; possible cobbles--			7	4 4 5	4.00	15						17					
	573.7	Very stiff, black and gray SILTY CLAY to SILTY CLAY LOAM, trace gravel; damp --Buried TOPSOIL-- --RDR 2--	20		8	3 5 6	2.50	26		548.6	Boring terminated at 44.50 ft	45		18					
	570.1	Medium dense, brown and gray SILTY LOAM, trace gravel --RDR 2-- --L <sub>L</sub> (%)=21, P <sub>L</sub> (%)=14--25			9	3 6 7	3.50	21						19					
					10	9 6 6	NP	12						20					

## GENERAL NOTES

## WATER LEVEL DATA

Begin Drilling **11-16-2021** Complete Drilling **11-16-2021**  
 Drilling Contractor **Wang Testing Services** Drill Rig **20D50T [80%]**  
 Driller **RH&JD** Logger **M. Rojo** Checked by **C. Marin**  
 Drilling Method **2.25" ID HSA; boring backfilled upon completion**

While Drilling **26.00 ft**  
 At Completion of Drilling **core wash 2.5ft**  
 Time After Drilling **NA**  
 Depth to Water **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

WANGENGINC\_2553901.GPJ WANGENG.GDT 12/13/21





wangeng@wangeng.com  
 1145 N MAIn Street  
 Lombard, IL 60148  
 Telephone: (630) 953-9928  
 Fax: (630) 953-9938

# BORING LOG RIV-RWB-06HA

WEI Job No.: 255-39-01

Client **Stantec**  
 Project **I-80 Reconstruction, Ridge Road to Houbolt Road**  
 Location **Will County, Illinois**

Datum: NAVD88  
 Elevation: 589.34 ft  
 North: 1755110.12 ft  
 East: 1016283.21 ft  
 Station: 28+08.8  
 Offset: 21.9 LT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	
	589.2	Brown SANDY GRAVEL --FILL--			1	P C C C H	> 4.50 P	14										
		Stiff to hard, brown and gray SILTY CLAY to SILTY CLAY LOAM, trace gravel; damp --FILL--			2	P C C C H	1.25 P	18										
			5		3	P C C C H	> 4.50 P	17										
		--L <sub>L</sub> (%)=38, P <sub>L</sub> (%)=16-- --%Gravel=1.8-- --%Sand=19.5-- --%Silt=52.1-- --%Clay=26.6-- --A-6 (16)--			4	P C C C H	2.50 P	21										
			10		5	P C C C H	3.50 P	15										
					6	P C C C H	3.00 P	16										
					7	P C C C H	3.00 P	11										
			15		8	P C C C H	3.50 P	17										
	573.3	Boring terminated at 16.00 ft																

### GENERAL NOTES

Begin Drilling **11-30-2021** Complete Drilling **12-01-2021**  
 Drilling Contractor **Wang Testing Services** Drill Rig **Geoprobe HA**  
 Driller **RH&AG** Logger **M. Rojo** Checked by **C. Marin**  
 Drilling Method **.1" ID HSA; boring backfilled upon completion**

### WATER LEVEL DATA

While Drilling  $\nabla$  **DRY**  
 At Completion of Drilling  $\nabla$  **DRY**  
 Time After Drilling **NA**  
 Depth to Water  $\nabla$  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.



wangeng@wangeng.com  
 1145 N MAIn Street  
 Lombard, IL 60148  
 Telephone: (630) 953-9928  
 Fax: (630) 953-9938

# BORING LOG RIV-RWB-07

WEI Job No.: 255-39-01

Client **Stantec**  
 Project **I-80 Reconstruction, Ridge Road to Houbolt Road**  
 Location **Will County, Illinois**

Datum: NAVD 88  
 Elevation: 592.50 ft  
 North: 1755049.72 ft  
 East: 1016271.73 ft  
 Station: 28+69.1  
 Offset: 8.8 LT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	591.6	11-inch thick ASPHALT --PAVEMENT--								567.0	trace gravel; damp						
	591.2	Medium dense, tan SANDY GRAVEL; damp --BASE COURSE--			1	6 4 6	2.00 P	11			Very dense, tan WEATHERED BEDROCK; damp			11	50/1"		2
		Stiff to hard, brown and black SILTY CLAY to SILTY CLAY LOAM, trace gravel; damp --FILL-- --RDR 2--	5		2	5 8 9	7.71 B	15		564.5	Strong, light grayish gray, very poor quality, DOLOSTONE; very closely spaced, moderately weathered, horizontal, oblique, and vertical joints, with <0.05 inch opening, slightly rough walls, and <0.2 inch thick sand infill. --RUN 1: 28.0 to 31.5 feet-- --Recovery: 86%-- --RQD: 0%-- --RUN 2: 31.5 to 39.5 feet-- --Recovery: 94%-- --RQD: 0%--	30		12			
					3	5 6 8	4.43 B	17									
			10		4	4 5 6	4.26 B	15									
					5	3 6 7	4.67 B	15									
			15		6	5 6 7	2.95 B	14		553.0	Boring terminated at 39.50 ft	40					
					7	4 6 6	2.87 B	14									
			20		8	4 6 9	1.97 B	16									
					9	6 6 11	5.49 B	20									
	568.3	Very dense, brown SILTY LOAM,	25		10	7 7 50/4"	2.05 B	21				50					

### GENERAL NOTES

Begin Drilling **11-18-2021** Complete Drilling **11-18-2021**  
 Drilling Contractor **Wang Testing Services** Drill Rig **20CME55T[81%]**  
 Driller **RR&AG** Logger **D. You** Checked by **C. Marin**  
 Drilling Method **2.25" ID HSA; boring backfilled upon completion**

### WATER LEVEL DATA

While Drilling  **DRY**  
 At Completion of Drilling  **core wash 7ft**  
 Time After Drilling **NA**  
 Depth to Water  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

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wangeng@wangeng.com  
 1145 N MAIn Street  
 Lombard, IL 60148  
 Telephone: (630) 953-9928  
 Fax: (630) 953-9938

# BORING LOG RIV-RWB-07HA

WEI Job No.: 255-39-01

Client **Stantec**  
 Project **I-80 Reconstruction, Ridge Road to Houbolt Road**  
 Location **Will County, Illinois**

Datum: NAVD88  
 Elevation: 586.01 ft  
 North: 1755051.25 ft  
 East: 1016287.66 ft  
 Station: 28+67.8  
 Offset: 24.8 LT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	585.9	Brown SANDY GRAVEL --FILL--			1	P C C C C H	> 4.50 P	16									
		Very stiff to hard, brown and gray SILTY CLAY to SILTY CLAY LOAM, trace gravel; damp --FILL--			2	P C C C C H	> 4.50 P	15									
			5		3	P C C C C H	> 4.50 P	15									
					4	P C C C C H	4.00 P	18									
					5	P C C C C H	3.25 P	18									
			10		6	P C C C C H	> 4.50 P	17									
					7	P C C C C H	2.50 P	17									
	572.0	Stiff, brown and gray SILTY CLAY to SILTY CLAY LOAM, trace gravel; moist to wet	15		8	P C C C C H	1.00 P	23									
	570.0	Boring terminated at 16.00 ft															

### GENERAL NOTES

### WATER LEVEL DATA

Begin Drilling **11-30-2021** Complete Drilling **11-30-2021**  
 Drilling Contractor **Wang Testing Services** Drill Rig **Geoprobe HA**  
 Driller **RH&AG** Logger **M. Rojo** Checked by **C. Marin**  
 Drilling Method **.1" ID HSA; boring backfilled upon completion**

While Drilling  $\nabla$  **16.00 ft**  
 At Completion of Drilling  $\blacktriangledown$  **16.00 ft**  
 Time After Drilling **NA**  
 Depth to Water  $\nabla$  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.



wangeng@wangeng.com  
 1145 N Main Street  
 Lombard, IL 60148  
 Telephone: (630) 953-9928  
 Fax: (630) 953-9938

# BORING LOG RIV-RWB-08

WEI Job No.: 255-39-01

Client **Stantec**  
 Project **I-80 Reconstruction, Ridge Road to Houbolt Road**  
 Location **Will County, Illinois**

Datum: NAVD88  
 Elevation: 590.05 ft  
 North: 1754964.53 ft  
 East: 1016273.57 ft  
 Station: 29+54.4  
 Offset: 7.3 LT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	589.5	7-inch thick ASPHALT --PAVEMENT--									LOAM; wet						
	588.7	White and gray SANDY GRAVEL; damp --BASE COURSE--			1	13 10 8	> 4.50 P	14			Very dense, brown SANDY GRAVEL; saturated --AUGER REFUSAL-- Boring terminated at 23.00 ft						
		Hard, brown and gray SILTY CLAY to SILTY CLAY LOAM, trace gravel; damp --FILL-- --RDR 2--	5		2	9 10 11	> 4.50 P	13									
					3	7 7 12	4.26 B	17									
			10		4	4 5 8	> 4.50 P	13									
					5	4 7 8	> 4.50 P	15									
			15		6	4 5 6	> 4.50 P	16									
	573.3	Hard, black SILTY CLAY to SILTY CLAY LOAM, trace gravel and organic matter --BURIED TOPSOIL--			7	4 6 7	4.00 P	25									
	572.1	Hard, brown and gray SILTY CLAY to SILTY CLAY LOAM, trace gravel; damp to moist --RDR 2--	20		8	3 4 4	4.00 P	26									
	569.6	trace gravel; damp to moist --L <sub>L</sub> (%)=44, P <sub>L</sub> (%)=15-- --%Gravel=2.2-- --%Sand=8.5-- --%Silt=60.6-- --%Clay=28.6-- --A-7-6 (26)--			9	10 10 10	NP	7									
	568.9																
	567.1	Brown and gray SILTY LOAM to	25														

## GENERAL NOTES

## WATER LEVEL DATA

Begin Drilling **11-17-2021** Complete Drilling **11-17-2021**  
 Drilling Contractor **Wang Testing Services** Drill Rig **20D50T [80%]**  
 Driller **RH&JD** Logger **M. Rojo** Checked by **C. Marin**  
 Drilling Method **3.25" ID HSA; boring backfilled upon completion**

While Drilling  $\nabla$  **22.00 ft**  
 At Completion of Drilling  $\nabla$  **DRY**  
 Time After Drilling **NA**  
 Depth to Water  $\nabla$  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.



wangeng@wangeng.com  
 1145 N MAIn Street  
 Lombard, IL 60148  
 Telephone: (630) 953-9928  
 Fax: (630) 953-9938

# BORING LOG RIV-RWB-08HA

WEI Job No.: 255-39-01

Client **Stantec**  
 Project **I-80 Reconstruction, Ridge Road to Houbolt Road**  
 Location **Will County, Illinois**

Datum: NGVD  
 Elevation: 585.18 ft  
 North: 1754962.78 ft  
 East: 1016288.59 ft  
 Station: 29+56.9  
 Offset: 22.2 LT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)		
		Very stiff to hard, brown and gray SILTY CLAY to SILTY CLAY LOAM, trace gravel; damp --FILL-- --RDR 2--			1	P C C C H	> 4.50 P	15											
						2	P C C C H	> 4.50 P	16										
						3	P C C C H	> 4.50 P	14										
						4	P C C C H	> 4.50 P	16										
						5	P C C C H	> 4.50 P	16										
						6	P C C C H	> 4.50 P	15										
						7	P C C C H	> 4.50 P	15										
						8	P C C C H	3.00 P	24										
	571.2	Very stiff, black and gray CLAY to SILTY CLAY; damp	15																
	569.2	Boring terminated at 16.00 ft																	

### GENERAL NOTES

Begin Drilling **11-29-2021** Complete Drilling **11-29-2021**  
 Drilling Contractor **Wang Testing Services** Drill Rig **Geoprobe HA**  
 Driller **RH&AG** Logger **M. Rojo** Checked by **C. Marin**  
 Drilling Method **.1" ID HSA; boring backfilled upon completion**

### WATER LEVEL DATA

While Drilling  $\nabla$  **DRY**  
 At Completion of Drilling  $\nabla$  **DRY**  
 Time After Drilling **NA**  
 Depth to Water  $\nabla$  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.



wangeng@wangeng.com  
 1145 N MAIn Street  
 Lombard, IL 60148  
 Telephone: (630) 953-9928  
 Fax: (630) 953-9938

# BORING LOG RIV-RWB-09

WEI Job No.: 255-39-01

Client **Stantec**  
 Project **I-80 Reconstruction, Ridge Road to Houbolt Road**  
 Location **Will County, Illinois**

Datum: NAVD 88  
 Elevation: 585.93 ft  
 North: 1754864.40 ft  
 East: 1016280.92 ft  
 Station: 30+54.9  
 Offset: 8.8 LT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	585.3	7-inch thick ASPHALT --PAVEMENT--									BEDROCK --auger refusal at 23.5 feet--						
	584.7	White and gray SANDY GRAVEL; damp --BASE COURSE--			1	7 9 8	4.50 P	12			Strong, light grayish gray, very poor quality, DOLOSTONE; Closely spaced, moderately weathered, horizontal and vertical joints, with <0.05 inch opening, slightly rough walls, and no infill. --RUN 1: 23.5 to 33.5 feet-- --Recovery: 91%-- --RQD: 12%--			10			
		Very stiff to hard, brown and gray SILTY CLAY to SILTY CLAY LOAM, trace gravel; damp --FILL-- --RDR 2--			2	3 6 8	4.50 P	10									
					3	3 4 4	3.25 P	15									
	577.9	Very stiff, black SILTY CLAY to SILTY CLAY LOAM, trace gravel and organic matter --BURIED TOPSOIL--			4	4 5 5	2.50 P	26		552.4	Boring terminated at 33.50 ft						
	577.2	Very stiff to hard (>4.50P), brown and gray SILTY CLAY to SILTY CLAY LOAM, trace gravel; damp --RDR 2--			5	5 5 7	3.50 P	14									
	572.9	Stiff, bluish gray and brown SILTY CLAY, trace gravel; moist --RDR 2--			6	3 3 3	1.50 P	27									
	570.4	Medium dense, brown SILTY LOAM, trace gravel; saturated --RDR 2-- --L <sub>L</sub> (%)=19, P <sub>L</sub> (%)=14-- --%Gravel=13.7-- --%Sand=24.6-- --%Silt=54.3-- --%Clay=7.4-- --A-4 (0)--			7	4 4 19	NP	15									
	567.9	Very dense, brown GRAVEL; saturated --RDR 2-3-- --rig chatter; possible cobbles--			8	60/1"	NP	14									
	565.4	Very dense, white and gray SILTY LOAM, trace gravel --RDR 3--			9	11 50/1"	NP	14									
	564.5	White and gray WEATHERED															
	562.4																

## GENERAL NOTES

## WATER LEVEL DATA

Begin Drilling **11-23-2021** Complete Drilling **11-23-2021**  
 Drilling Contractor **Wang Testing Services** Drill Rig **20CME55T[81%]**  
 Driller **RH&AG** Logger **M. Rojo** Checked by **C. Marin**  
 Drilling Method **3.25" ID HSA; boring backfilled upon completion**

While Drilling **17.00 ft**  
 At Completion of Drilling **core wash 13ft**  
 Time After Drilling **NA**  
 Depth to Water **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.



wangeng@wangeng.com  
 1145 N MAin Street  
 Lombard, IL 60148  
 Telephone: (630) 953-9928  
 Fax: (630) 953-9938

# BORING LOG RIV-RWB-09HA

WEI Job No.: 255-39-01

Client **Stantec**  
 Project **I-80 Reconstruction, Ridge Road to Houbolt Road**  
 Location **Will County, Illinois**

Datum: NAVD88  
 Elevation: 580.31 ft  
 North: 1754868.40 ft  
 East: 1016296.74 ft  
 Station: 30+52.0  
 Offset: 24.9 LT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
		Very stiff, brown and gray SILTY CLAY to SILTY CLAY LOAM, trace gravel; damp			1	P C C C H	3.50 P	22									
		--FILL-- --RDR 2--			2	P C C C H	2.50 P	19									
			5		3	P C C C H	3.00 P	18									
					4	P C C C H	3.50 P	13									
					5	P C C S H	2.50 P	17									
	570.5 570.3	Black SILTY CLAY to SILTY CLAY LOAM, trace gravel --BURIED TOPSOIL--	10		6	P C S H	1.50 P	29									
	568.6	Stiff, bluish-green gray SILTY CLAY to SILTY CLAY LOAM, trace gravel; damp --RDR 2--			7	P C S H	1.50 P	14									
	566.4 565.8	Stiff, brown and gray SILTY LOAM to SILTY CLAY LOAM, trace gravel; damp --RDR 2-- Brown SANDY GRAVEL; wet --Weathered BEDROCK-- --spoon refusal-- Boring terminated at 14.5 ft	15		8		NP	13									

### GENERAL NOTES

### WATER LEVEL DATA

Begin Drilling **11-29-2021** Complete Drilling **11-29-2021**  
 Drilling Contractor **Wang Testing Services** Drill Rig **Geoprobe HA**  
 Driller **RH&AG** Logger **M. Rojo** Checked by **C. Marin**  
 Drilling Method **.1" ID HSA; boring backfilled upon completion**

While Drilling  $\nabla$  **14.00 ft**  
 At Completion of Drilling  $\nabla$  **12.00 ft**  
 Time After Drilling **NA**  
 Depth to Water  $\nabla$  **NA**

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wangeng@wangeng.com  
 1145 N Main Street  
 Lombard, IL 60148  
 Telephone: (630) 953-9928  
 Fax: (630) 953-9938

# BORING LOG RIV-SGB-03

WEI Job No.: 255-39-01

Client **Stantec**  
 Project **I-80 Reconstruction, Ridge Road to Houbolt Road**  
 Location **Will County, Illinois**

Datum: NAVD 88  
 Elevation: 592.36 ft  
 North: 1755053.60 ft  
 East: 1016257.18 ft  
 Station: 28+64.8  
 Offset: 5.4 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	591.8	7-inch thick ASPHALT --PAVEMENT--															
	591.1	Gray and white SANDY GRAVEL; damp --AGGREGATE BASE--				8									4		
		Very stiff to hard, brown and gray SILTY CLAY to SILTY CLAY LOAM, trace gravel; damp --FILL-- --RDR 2--			1	7 7 7 8	4.50 P	13						8	5 7	4.50 P	16
					2	10 11 11 11	4.50 P	14						9	9 10 9	NA	18
					3	6 7 9 7	4.50 P	17						10	4 7 8	NP	15
					4	7 6 6 5	3.28 B	17		571.9	Medium dense, brown and gray LOAM, trace gravel; moist --FILL-- --RDR 2--			11	7 9	NP	11
					5	5 7 6 7	4.50 P	17		569.4	Very dense, brown SILTY LOAM, trace gravel; wet to saturated --RDR 2--			11	60/3"		
					6	3 5 8	NA	18		567.4	Boring terminated at 24.75 ft						
					7	5 6 8	4.50 P	18									

### GENERAL NOTES

Begin Drilling **11-22-2021** Complete Drilling **11-22-2021**  
 Drilling Contractor **Wang Testing Services** Drill Rig **20CME55T[81%]**  
 Driller **RR&AG** Logger **M. Rojo** Checked by **C. Marin**  
 Drilling Method **2.25" ID HSA; boring backfilled upon completion**

### WATER LEVEL DATA

While Drilling  $\nabla$  **24.00 ft**  
 At Completion of Drilling  $\nabla$  **DRY**  
 Time After Drilling **NA**  
 Depth to Water  $\nabla$  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

WANGENGINC 2553901.GPJ WANGENG.GDT 12/15/21





wangeng@wangeng.com  
 1145 N Main Street  
 Lombard, IL 60148  
 Telephone: (630) 953-9928  
 Fax: (630) 953-9938

# BORING LOG RIV-SGB-04

WEI Job No.: 255-39-01

Client **Stantec**  
 Project **I-80 Reconstruction, Ridge Road to Houbolt Road**  
 Location **Will County, Illinois**

Datum: NAVD 88  
 Elevation: 586.14 ft  
 North: 1754867.01 ft  
 East: 1016264.92 ft  
 Station: 30+51.3  
 Offset: 7.2 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft)	Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
	585.6	7-inch thick ASPHALT --PAVEMENT--								570.6							
	584.5	Medium dense, gray and white SANDY GRAVEL --BASE COURSE--				13				569.6	Very dense, brown SILTY LOAM to SILTY CLAY LOAM; moist --RDR 2--			8	5	NP	15
		Stiff to hard, brown and gray SILTY CLAY to SILTY CLAY LOAM, trace gravel; damp --FILL-- --RDR 2--			1	7 6 7	4.50 P	14			Very dense, brown and gray GRAVEL to SANDY GRAVEL; moist to saturated --RDR 2--				50/6"		
					2	4 7 10 11	4.50 P	12						9	50/4"	NP	15
		--L <sub>L</sub> (%)=29, P <sub>L</sub> (%)=15-- --%Gravel=5.5-- --%Sand=15.8-- --%Silt=55.6-- --%Clay=23.0-- --A-6 (9)--	5		3	7 8 7 9	4.50 P	15		566.1	Boring terminated at 20.00 ft	20					
					4	5 8 9 10	2.05 B	16									
			10		5	20 21 11 9	1.50 P	16				25					
					6	10 13 11	NA	15									
	573.9	Stiff, gray and brown SILTY CLAY to SILTY CLAY LOAM, trace gravel; damp to moist --RDR 2--			7	3 2 9	1.50 P	24				30					

### GENERAL NOTES

Begin Drilling **11-23-2021** Complete Drilling **11-23-2021**  
 Drilling Contractor **Wang Testing Services** Drill Rig **20CME55T[81%]**  
 Driller **RR&AG** Logger **M. Rojo** Checked by **C. Marin**  
 Drilling Method **2.25" ID HSA; boring backfilled upon completion**

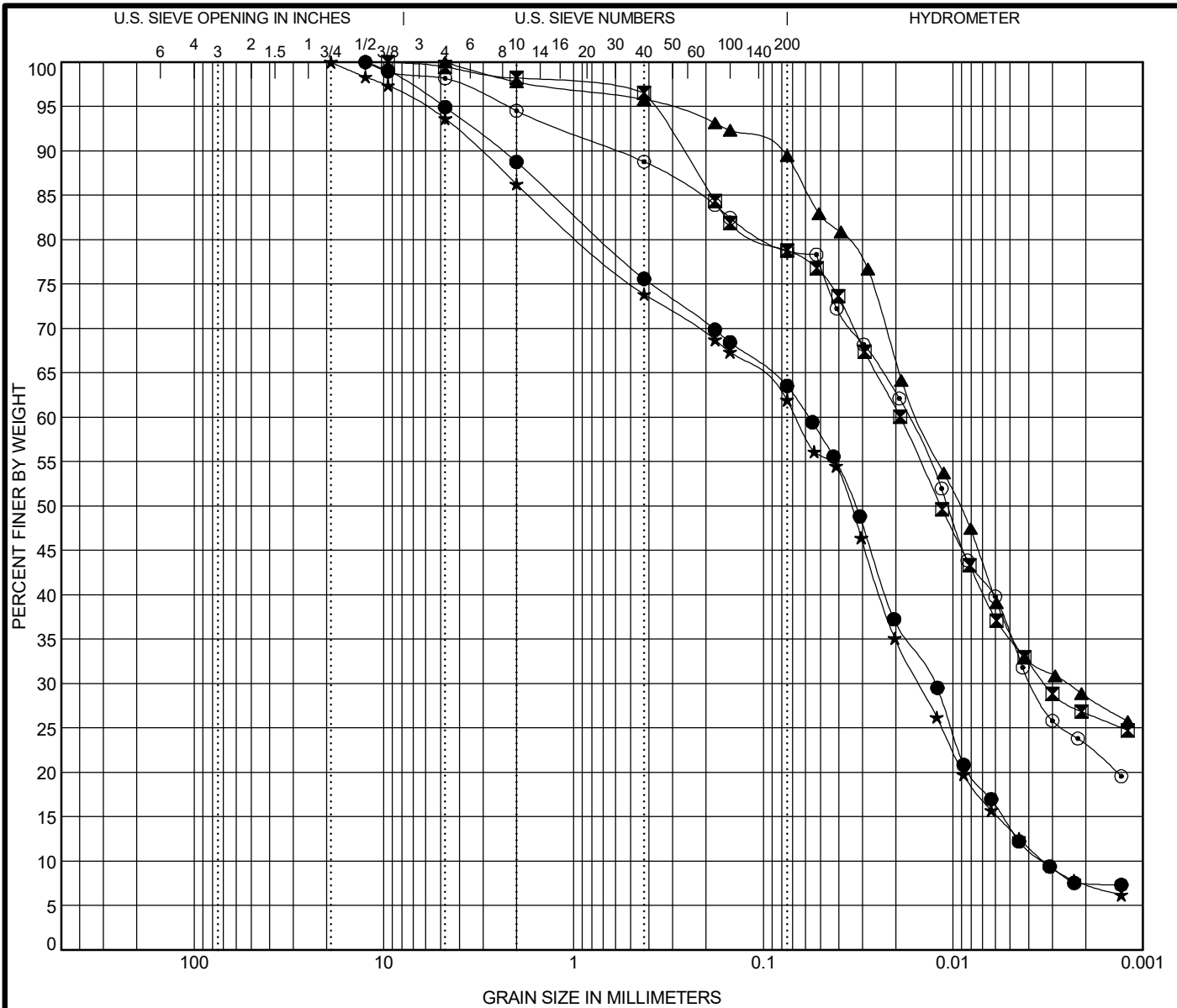
### WATER LEVEL DATA

While Drilling  $\nabla$  **19.00 ft**  
 At Completion of Drilling  $\nabla$  **DRY**  
 Time After Drilling **NA**  
 Depth to Water  $\nabla$  **NA**

The stratification lines represent the approximate boundary between soil types; the actual transition may be gradual.

WANGENGINC 2553901.GPJ WANGENG.GDT 12/15/21

## **APPENDIX B**



COBBLES	GRAVEL	SAND		SILT AND CLAY
		coarse	fine	

Specimen Identification		IDH Classification					LL	PL	PI	Cc	Cu
●	RIV-BSB-03#10 23.5 ft	<b>Silty Loam</b>					21	14	7	0.81	17.16
☒	RIV-RWB-06HA#4 6.0 ft	<b>Silty Clay Loam</b>					38	16	22		
▲	RIV-RWB-08#8 18.5 ft	<b>Silty Clay Loam</b>					44	15	29		
★	RIV-RWB-09#7 16.0 ft	<b>Silty Loam</b>					19	14	5	1.02	20.13
⊙	RIV-SGB-04#3 5.0 ft	<b>Silty Clay Loam</b>					29	15	14		
Specimen Identification		D100	D60	D30	D10	%Gravel	%Sand	%Silt	%Clay		
●	RIV-BSB-03#10 23.5 ft	12.5	0.058	0.012	0.003	11.2	25.4	55.9	7.5		
☒	RIV-RWB-06HA#4 6.0 ft	9.5	0.019	0.003		1.8	19.5	52.1	26.6		
▲	RIV-RWB-08#8 18.5 ft	4.75	0.015	0.003		2.2	8.5	60.6	28.6		
★	RIV-RWB-09#7 16.0 ft	19	0.067	0.015	0.003	13.7	24.6	54.3	7.4		
⊙	RIV-SGB-04#3 5.0 ft	12.5	0.017	0.004		5.5	15.8	55.6	23.0		

WEI GRAIN SIZE IDH 2553901.GPJ US LAB.GDT 12/15/21



Wang Engineering, Inc.  
 1145 N MAin Street  
 Lombard, IL 60148  
 Telephone: (630) 953-9928  
 Fax: (630) 953-9938

**GRAIN SIZE DISTRIBUTION**

Project: I-80 Reconstruction, Ridge Road to Houbolt Road  
 Location: Will County, Illinois  
 Number: 255-39-01





### Unconfined Compressive Strength of Intact Rock Core Specimens

**Project:** I-80 Reconstruction

**Client:** Stantec

**WEI Job No.:** 255-39-01

Field Sample ID	Run #	Depth (ft)	Location	Sample Description	Length (in)		Diameter (in)	Total Load (lbs)	Total Pressure (psi)	Fracture Type*	Break Date	Tested By	Area (in <sup>2</sup> )
					Before Capping	After Capping							
RIV-BSB-03	1	39.0	South Abutment	Dolostone	4.27	NA	2.05	20110	6081	3	11/18/21	MAC	3.31
RIV-RWB-09	1	25.5	Southeast Retaining Wall	Dolostone	4.14	NA	2.05	24620	7459	3	12/13/21	MAC	3.30

**\* Fracture Types:**

- Type 1 - Reasonably well-formed cones on both ends, less than 1 in. [25 mm] of cracking through caps;
- Type 2 - Well-formed cone on one end, vertical cracks running through caps, no well defined cone on other end;
- Type 3 - Columnar vertical cracking through both ends, no well-formed cones;
- Type 4 - Diagonal fracture with no cracking through ends; tap with hammer to distinguish from Type 1;
- Type 5 - Side fractures at top or bottom (occur commonly with unbonded caps);
- Type 6 - Similar to Type 5 but end of cylinder is pointed.

Prepared by: \_\_\_\_\_

Checked by: \_\_\_\_\_

## APPENDIX C

Run #1



0 6 inches

Boring RIV-RWB-07:  
Run #1, 28.0 to 31.5 feet, RECOVERY=86%, RQD=0%

BEDROCK CORE: SOUTHEAST RETAINING WALL ALONG RIVER ROAD; I-80  
RECONSTRUCTION FROM EAST OF RIDGE RD TO HOUBOLT RD, WILL COUNTY, ILLINOIS

SCALE: GRAPHICAL

APPENDIX C-1

DRAWN BY: J. Bensen  
CHECKED BY: A. Hamad



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Lombard, IL 60148  
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FOR STANTEC

255-39-01

Run #2



Boring RIV-RWB-07:  
Run #2, 31.5 to 39.5 feet, RECOVERY=94%, RQD=0%

BEDROCK CORE: SOUTHEAST RETAINING WALL ALONG RIVER ROAD; I-80 RECONSTRUCTION FROM EAST OF RIDGE RD TO HOUBOLT RD, WILL COUNTY, ILLINOIS		
SCALE: GRAPHICAL	APPENDIX C-2	DRAWN BY: J. Bensen CHECKED BY: A. Hamad
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FOR STANTEC		255-39-01



Run #1



0 6 inches

Boring RIV-RWB-09:  
Run #2, 23.5 to 33.5 feet, RECOVERY=91%, RQD=12%

BEDROCK CORE: SOUTHEAST RETAINING WALL ALONG RIVER ROAD; I-80  
RECONSTRUCTION FROM EAST OF RIDGE RD TO HOUBOLT RD, WILL COUNTY, ILLINOIS

SCALE: GRAPHICAL

APPENDIX C-3

DRAWN BY: J. Bensen  
CHECKED BY: A. Hamad



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255-39-01

Run #1



0 6 inches

Boring RIV-BSB-03:  
Run #1, 30.0 to 40.0 feet, RECOVERY=90%, RQD=8%

BEDROCK CORE: SOUTHEAST RETAINING WALL ALONG RIVER ROAD; I-80  
RECONSTRUCTION FROM EAST OF RIDGE RD TO HOUBOLT RD, WILL COUNTY, ILLINOIS

SCALE: GRAPHICAL

APPENDIX C-4

DRAWN BY: J. Bensen  
CHECKED BY: A. Hamad

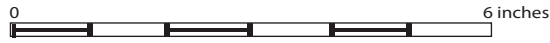
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255-39-01

Run #2



Boring RIV-BSB-03:  
Run #2, 40.0 to 44.5 feet, RECOVERY=81%, RQD=26%

BEDROCK CORE: SOUTHEAST RETAINING WALL ALONG RIVER ROAD; I-80  
RECONSTRUCTION FROM EAST OF RIDGE RD TO HOUBOLT RD, WILL COUNTY, ILLINOIS

SCALE: GRAPHICAL

APPENDIX C-5

DRAWN BY: J. Bensen  
CHECKED BY: A. Hamad

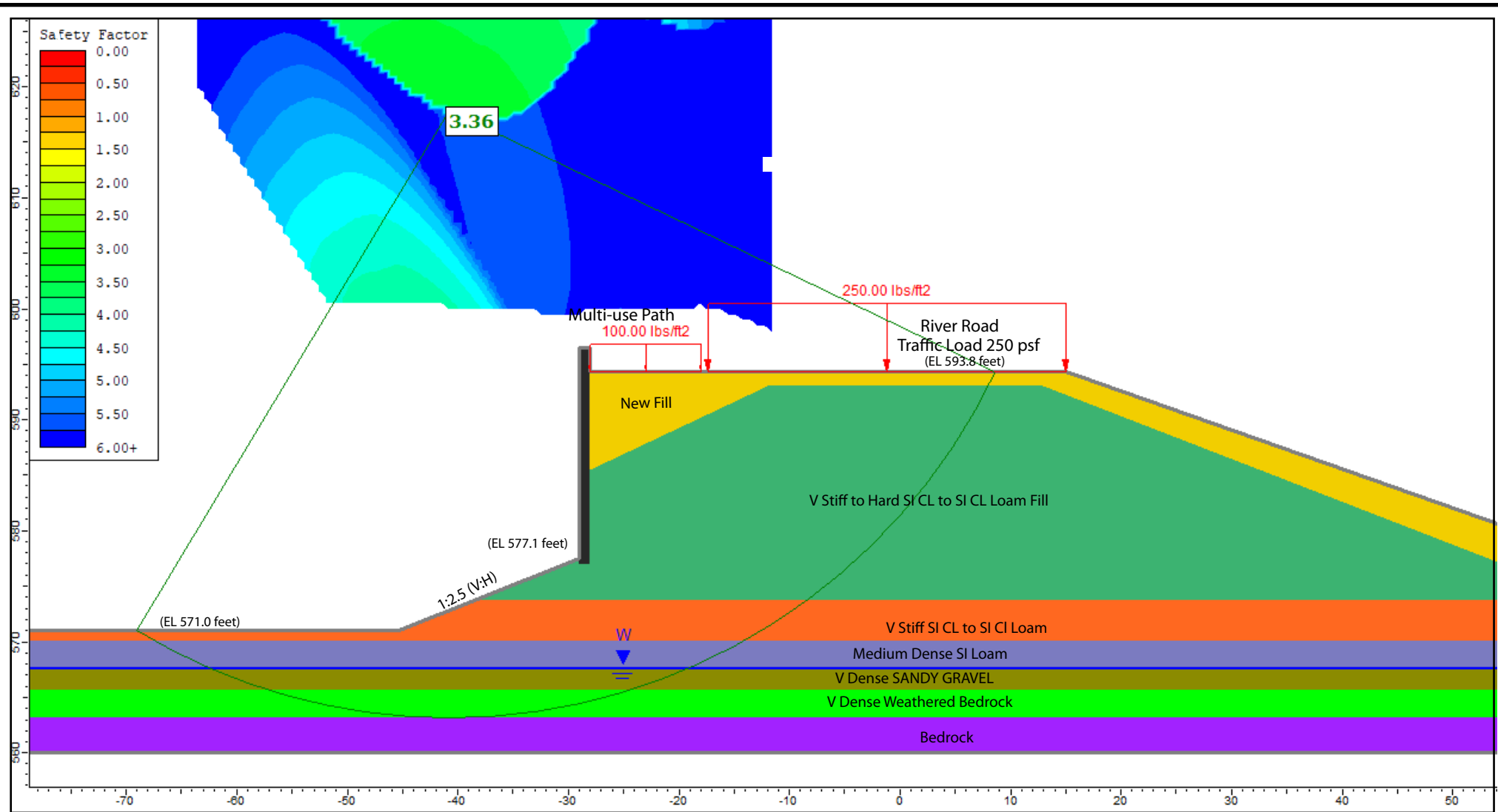


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FOR STANTEC

255-39-01

## **APPENDIX D**



Undrained Analysis, Southeast Retaining Wall, Sta. 28+50, Ref Borings: RIV-BSB-03 and RIV-RWB-06HA

Layer ID	Description	Total Unit Weight (pcf)	Undrained Cohesion (psf)	Undrained Friction Angle (degrees)
1	New Fill	125	1000	0
2	V Stiff to Hard SI CL to SI CL Loam Fill	120	2700	0
3	V Stiff SI CL to SI CL Loam	120	3500	0
4	M Dense SI Loam	120	0	30
5	V Dense Sa GRAVEL	125	0	35
6	V Dense Weathered Bedrock	130	0	35

GLOBAL STABILITY: SOUTHEAST REATINING WALL ALONG RIVER ROAD; I-80  
RECONSTRUCTION FROM EAST OF RIDGE RD TO HOUBOLT ROAD, WILL COUNTY, IL

SCALE: GRAPHICAL

APPENDIX D-1

DRAWN BY: N. Balakumaran  
CHECKED BY: A. Hamad

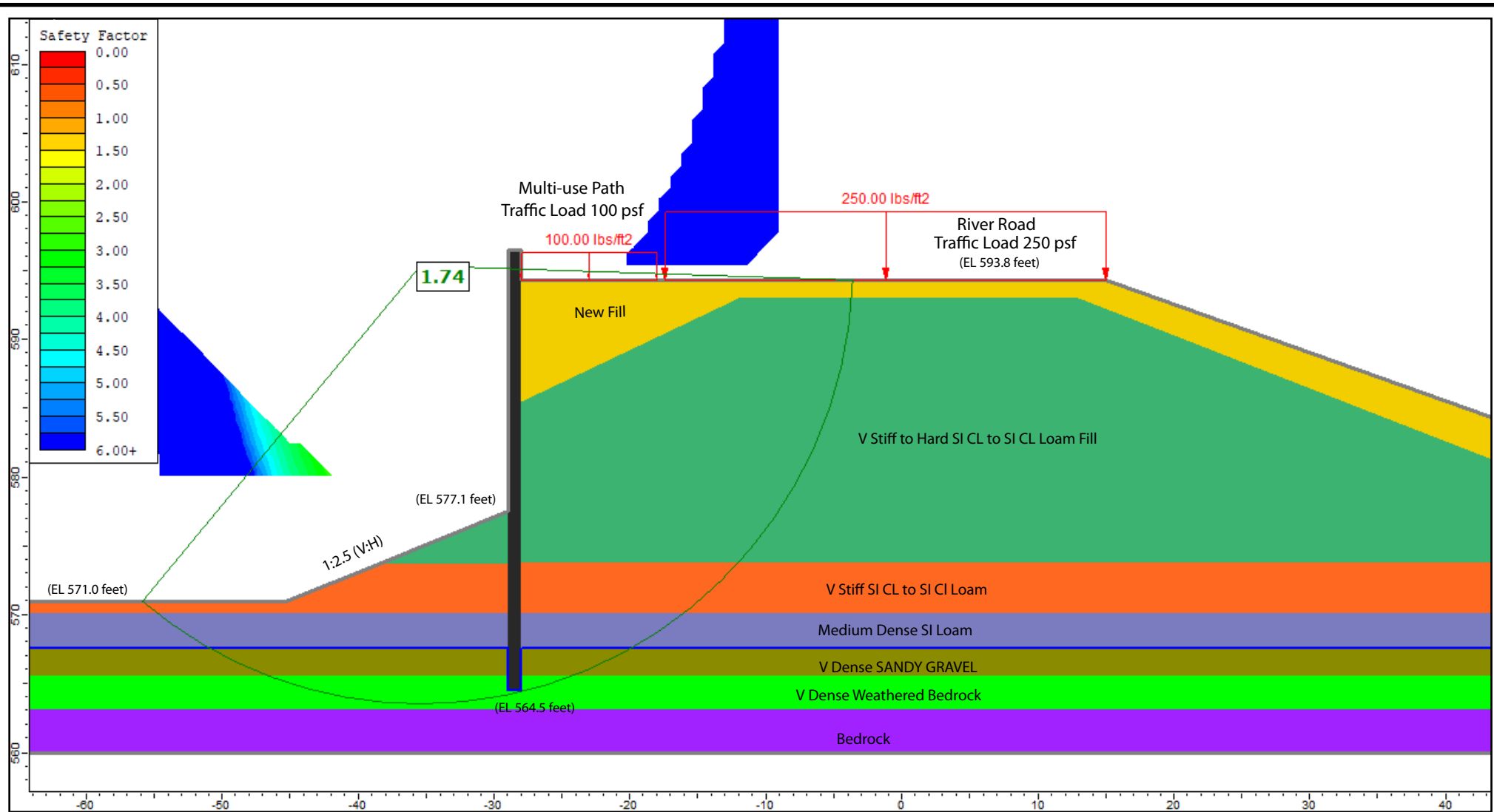


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255-39-01



Drained Analysis, Southeast Retaining Wall, Sta. 28+50, Ref Borings: RIV-BSB-03 and RIV-RWB-06HA

Layer ID	Description	Total Unit Weight (pcf)	Drained Cohesion (psf)	Drained Friction Angle (degrees)
1	New Fill	125	100	30
2	V Stiff to Hard SI CL to SI CL Loam Fill	120	100	30
3	V Stiff SI CL to SI CL Loam	120	100	30
4	M Dense SI Loam	120	0	30
5	V Dense Sa GRAVEL	125	0	35
6	V Dense Weathered Bedrock	130	0	35

GLOBAL STABILITY: SOUTHEAST RETAINING WALL ALONG RIVER ROAD; I-80 RECONSTRUCTION FROM EAST OF RIDGE RD TO HOUBOLT ROAD, WILL COUNTY, ILLINOIS

SCALE: GRAPHICAL

APPENDIX D-2

DRAWN BY: N. Balakumaran  
CHECKED BY: A. Hamad



**Wang**  
**Engineering**

1145 N. Main Street  
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FOR STANTEC

255-39-01

## **APPENDIX E**

Benchmark: Set 2" CWA Aluminum disc in concrete pier seat in southerly pier of River Road bridge on south side of eastbound I-80, Elev. 575.61

Existing Structure: None.

Traffic Control: Traffic will be detoured during construction.

**DESIGN STRESSES**

**FIELD UNITS**  
 f'c = 3,500 psi  
 fy = 60,000 psi (Reinforcement)  
 fy = 50,000 psi (M270 Grade 50) Soldier Piles

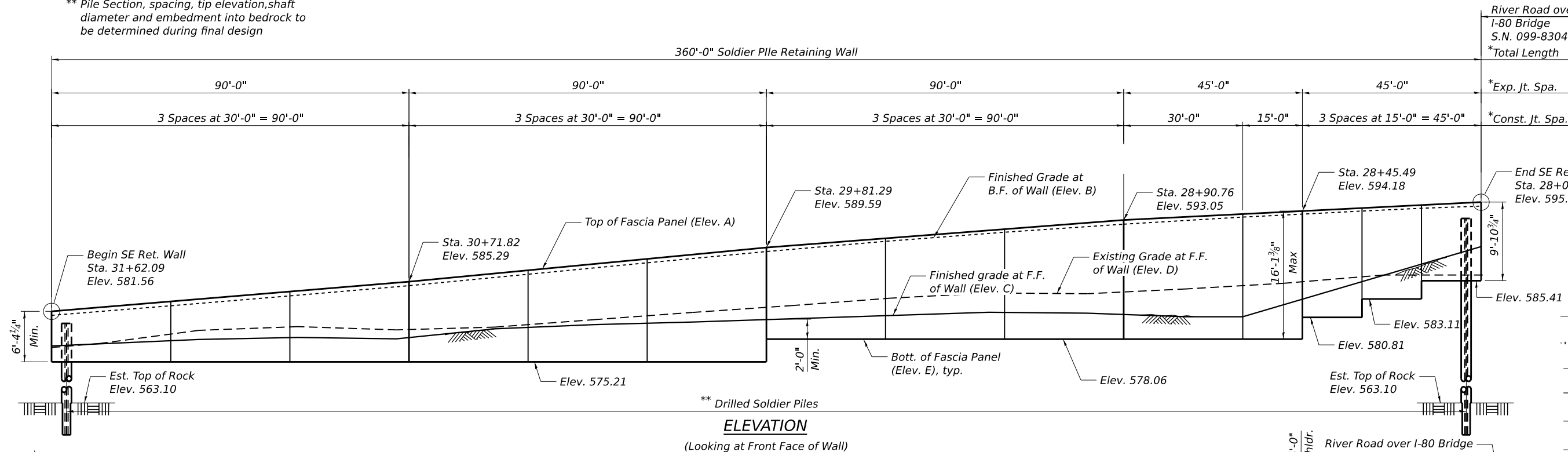
**DESIGN SPECIFICATIONS**

2020 AASHTO LRFD Bridge Design Specifications, 9th Edition

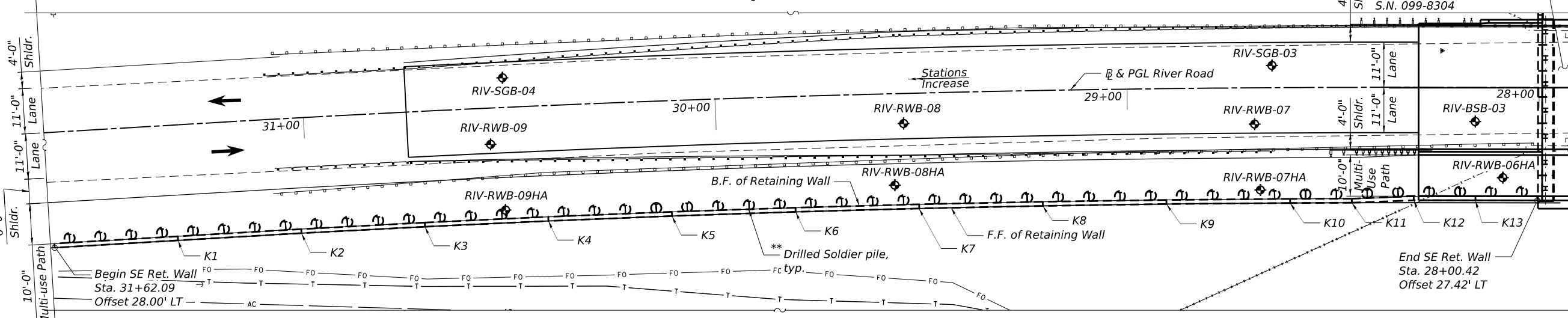
**HIGHWAY CLASSIFICATION**

Township Road 056-River Rd. Functional Class: Local Road ADT: 1,750 (2019) ; 2,146 (2032) ADTT: 158 (2019) ; 194 (2032) DHV: 236 (2032) Design Speed: 40 m.p.h. Posted Speed: 30 m.p.h. 2-Way Traffic Directional Distribution: 50-50	F.A.I. Rte. 80 - I-80 Functional Class: Interstate ADT: 57,400 (2019); 61,284 (2032) ADTT: 10,906 (2019); 11,644 (2032) DHV: 6,741 (2032) Design Speed: 70 m.p.h. Posted Speed: 70 m.p.h. 2-Way Traffic Directional Distribution: 50-50
---	---

\* Measured along F.F. of Wall  
 \*\* Pile Section, spacing, tip elevation, shaft diameter and embedment into bedrock to be determined during final design



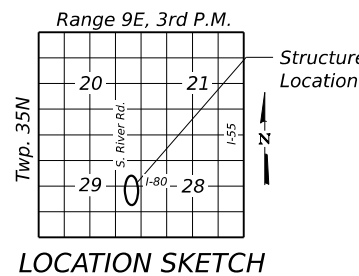
**ELEVATION**  
(Looking at Front Face of Wall)



**PLAN**

**LEGEND**

◆	Soil Boring
— A —	Exist. Aerial Line
---	Prop. Fence
—○—	Exist. Guardrail
—○—	Prop. Guardrail
—	Exist. ROW
— T —	Exist. Telephone
— FO —	Exist. Fiber Optic
F.F.	Front Face
B.F.	Back Face



**GENERAL PLAN & ELEVATION  
 SOUTHEAST RETAINING WALL  
 ALONG RIVER ROAD  
 F.A.I. RTE. I-80  
 SECTION 2021-151-B  
 WILL COUNTY  
 STA. 28+00.42 TO STA. 31+62.09  
 STRUCTURE NO. 099-W806**

**NOTES:**

- Stations and offsets are measured from the  $\square$  of River Road to the front face of cast-in-place concrete facing.
- Wall to be built along straight chords between construction joints.
- The Contractor shall exercise extreme caution during wall construction to make certain that the construction activities will not have detrimental effects on the adjacent utilities and other facilities.
- "K1" denotes wall kink point - Number 1.



USER NAME	DESIGNED - SK, JJS	REVISIONS	REVISOR
	CHECKED - MI, JJS, SK	REVISIONS	REVISOR
PLOT SCALE	DRAWN - JMI, SK	REVISIONS	REVISOR
PLOT DATE	CHECKED - MI, JJS, SK	REVISIONS	REVISOR

**STATE OF ILLINOIS  
 DEPARTMENT OF TRANSPORTATION**

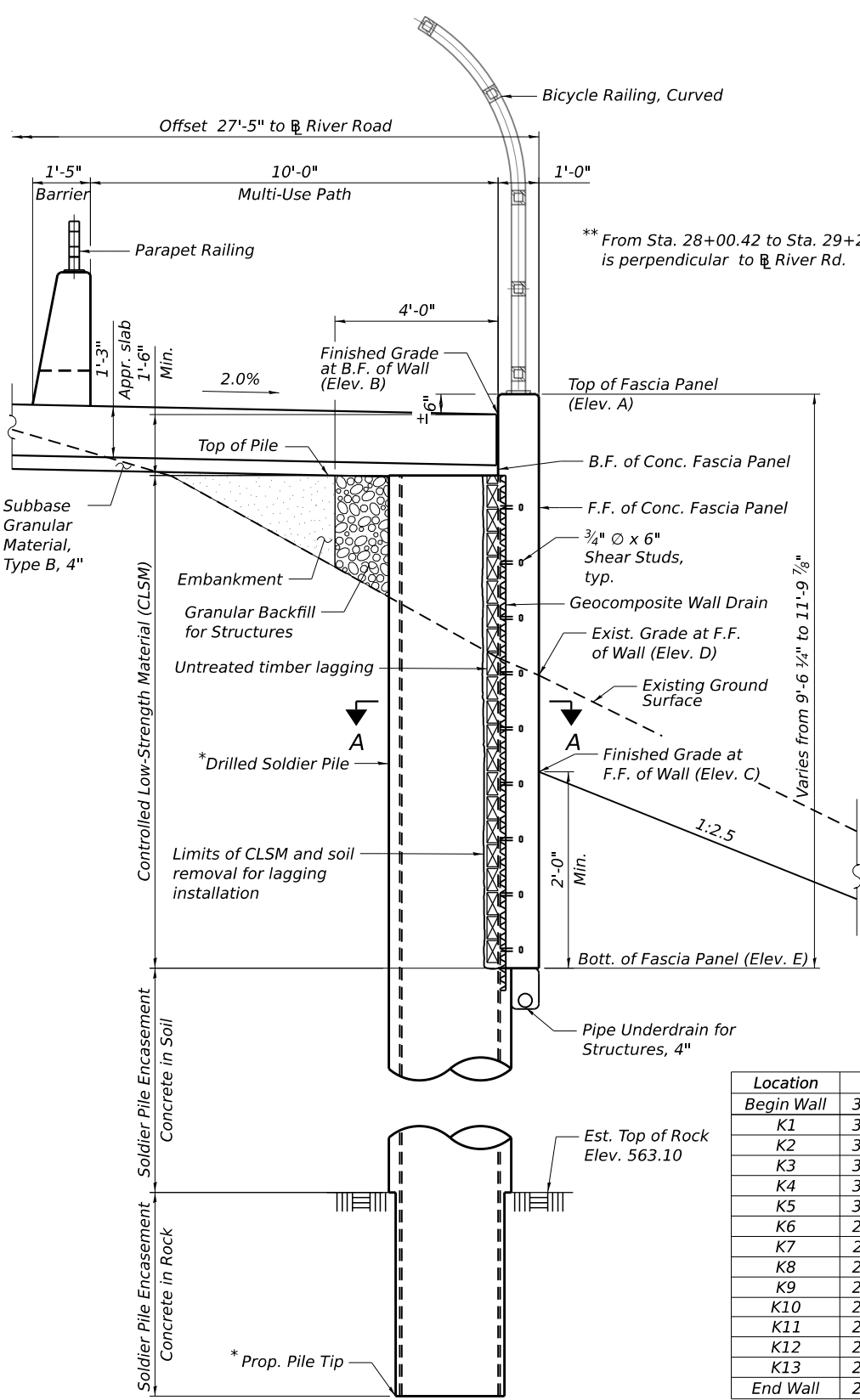
SHEET 1 OF 3 SHEETS

F.A.I. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
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CONTRACT NO. 62P67				
ILLINOIS FED. AID PROJECT				

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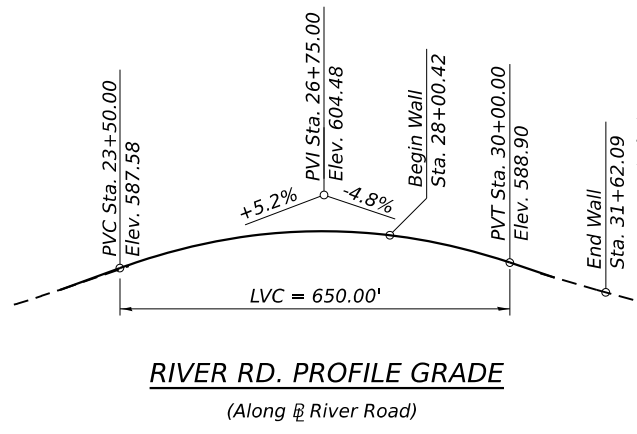
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**TYPICAL CROSS SECTION**  
 (Looking North)  
 (Sta. 28+00.42 to 28+30.42)

\*Pile section, spacing, tip elevation, shaft diameter and emedment into bedrock to be determined during final design.

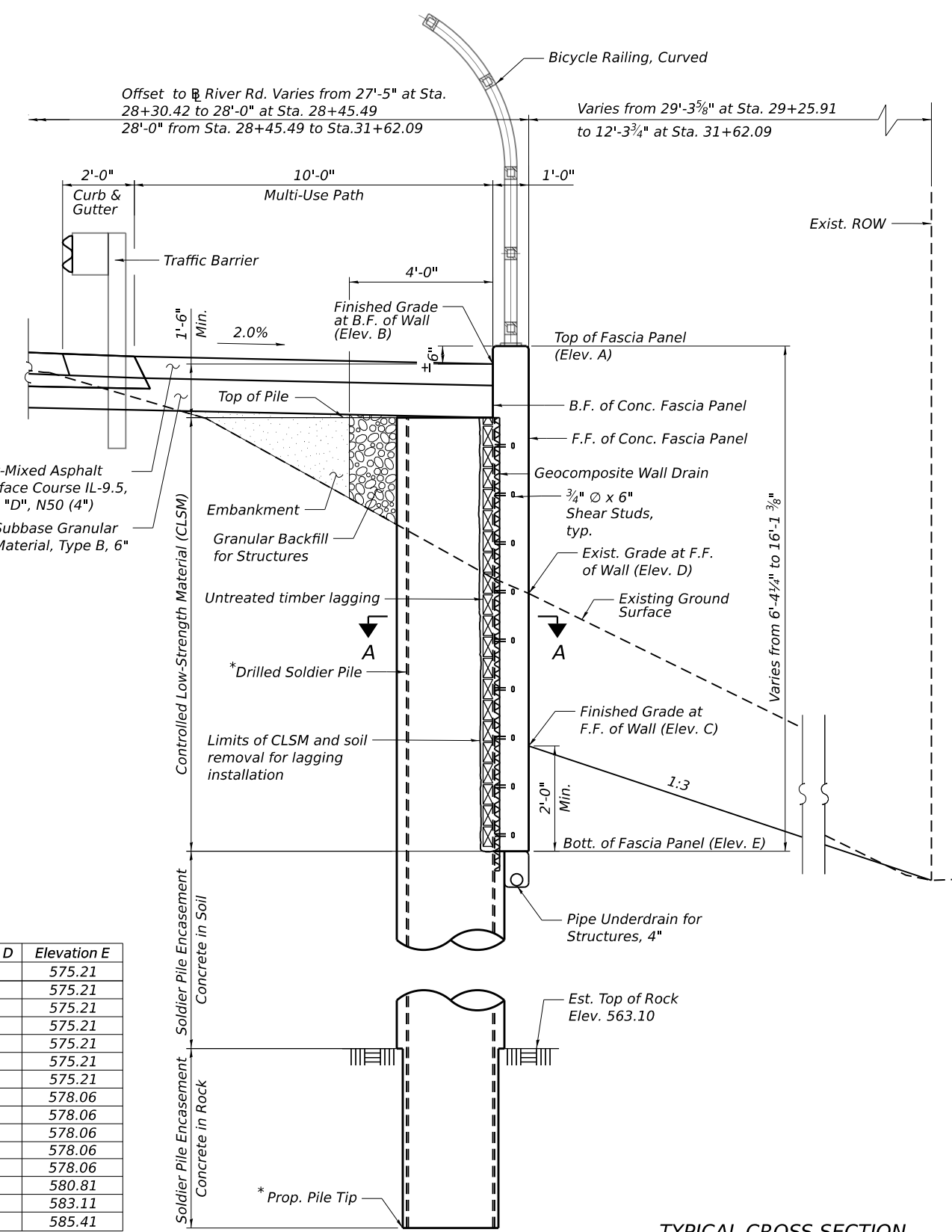
**PR CURVE  
 RR CURVE 2**  
 P.I. Sta. = 29+74.71  
 $\Delta = 03^{\circ}26'42''$  (LT)  
 $D = 01^{\circ}12'04''$   
 $R = 4,770.00'$   
 $T = 143.44'$   
 $L = 286.80'$   
 $E = 2.16'$   
 $e = N.C.$   
 $T.R. = N/A$   
 $S.E. Run = N/A$   
 P.C. Sta. = 28+31.27  
 P.T. Sta. = 31+18.07



**WALL ELEVATIONS TABLE**

Location	Station	Offset	Elevation A	Elevation B	Elevation C	Elevation D	Elevation E
Begin Wall	31+62.09	28.00' Lt.	581.56	581.06	577.21	577.02	575.21
K1	31+32.09	28.00' Lt.	582.80	582.26	577.88	578.70	575.21
K2	31+02.00	28.00' Lt.	584.05	583.52	578.25	579.60	575.21
K3	30+71.82	28.00' Lt.	585.29	584.79	578.26	579.28	575.21
K4	30+41.64	28.00' Lt.	586.72	586.24	579.54	579.90	575.21
K5	30+11.46	28.00' Lt.	588.16	587.69	580.08	581.01	575.21
K6	29+81.29	28.00' Lt.	589.59	589.09	580.57	582.07	575.21
K7	29+51.11	28.00' Lt.	590.74	590.38	581.07	583.17	578.06
K8	29+20.93	28.00' Lt.	591.90	591.54	581.43	583.86	578.06
K9	28+90.76	28.00' Lt.	593.05	592.55	581.17	584.01	578.06
K10	28+60.58	28.00' Lt.	593.80	593.42	580.89	584.80	578.06
K11	28+45.49	28.00' Lt.	594.18	593.80	583.10	585.30	578.06
K12	28+30.42	27.42' Lt.	594.56	594.19	585.30	585.92	580.81
K13	28+15.42	27.42' Lt.	594.93	594.53	587.51	586.14	583.11
End Wall	28+00.42	27.42' Lt.	595.31	594.81	589.71	586.14	585.41

Elev. A = Top of Fascia Panel  
 Elev. B = Finished Grade at B. F. of Wall  
 Elev. C = Finished Grade at F. F. of Wall  
 Elev. D = Exist. Grade at F.F. of Wall  
 Elev. E = Bott. of Fascia Panel



**TYPICAL CROSS SECTION**  
 (Looking North)  
 (Sta. 28+30.42 to 31+62.09)

**TYPICAL CROSS SECTION  
 SOUTHEAST RETAINING WALL  
 ALONG RIVER ROAD  
 F.A.I. RTE. I-80  
 SECTION 2021-151-B  
 WILL COUNTY  
 STA. 28+00.42 TO STA. 31+62.09  
 STRUCTURE NO. 099-W806**

**STATE OF ILLINOIS  
 DEPARTMENT OF TRANSPORTATION**

SHEET 2 OF 3 SHEETS

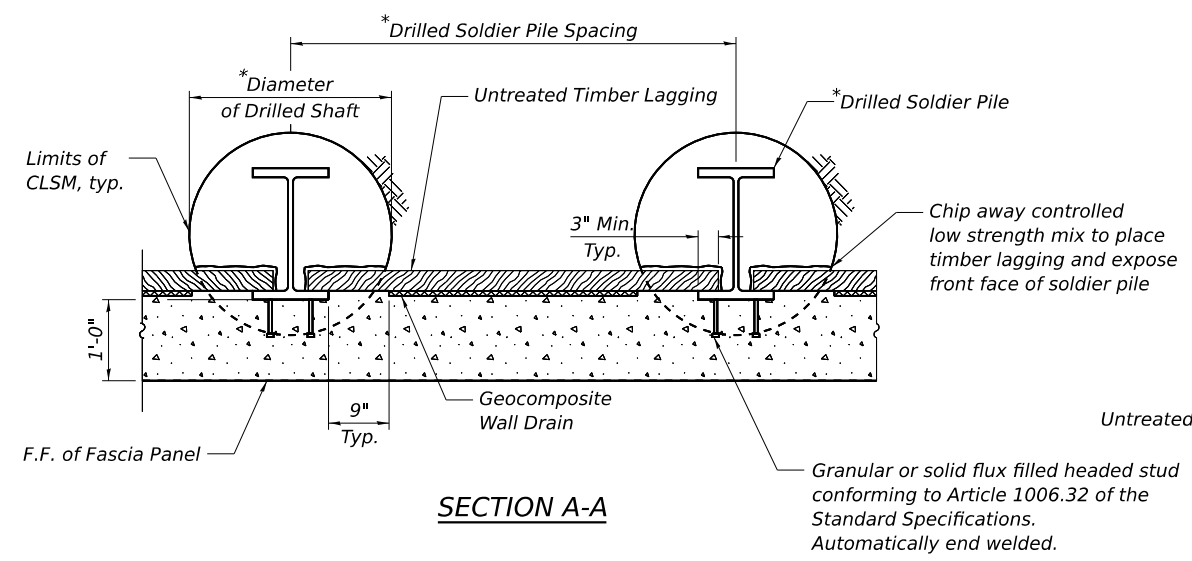
F.A.I. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
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CONTRACT NO. 62P67				
ILLINOIS FED. AID PROJECT				

**HBM**  
 ENGINEERING GROUP, LLC

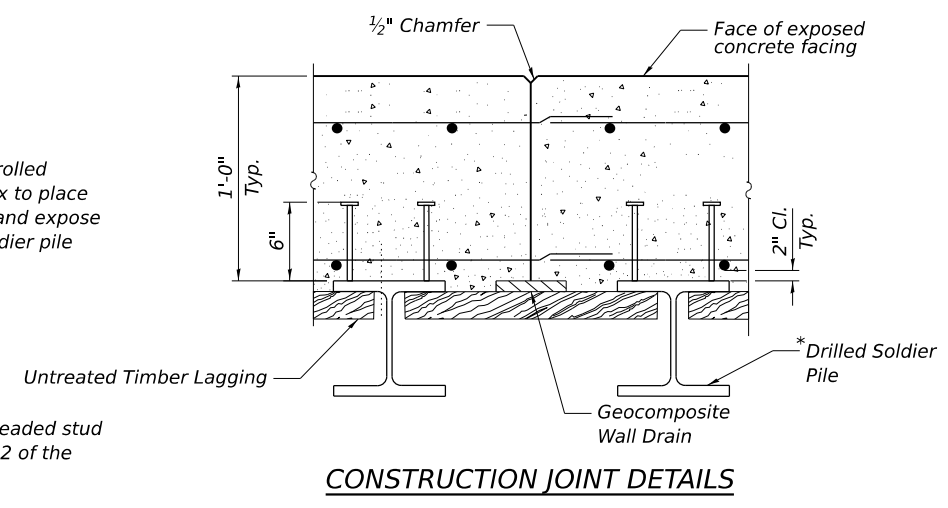
USER NAME	DESIGNED	CHECKED	REVISIONS
SK, JJS	SK, JJS	MI, JJS, SK	REVISIONS
JMI, SK	JMI, SK	MI, JJS, SK	REVISIONS

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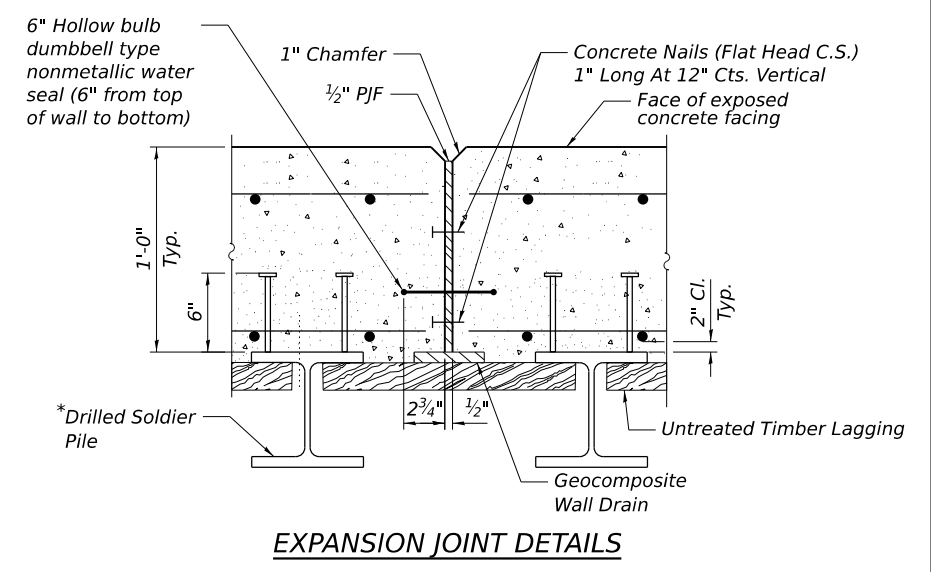
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**SECTION A-A**

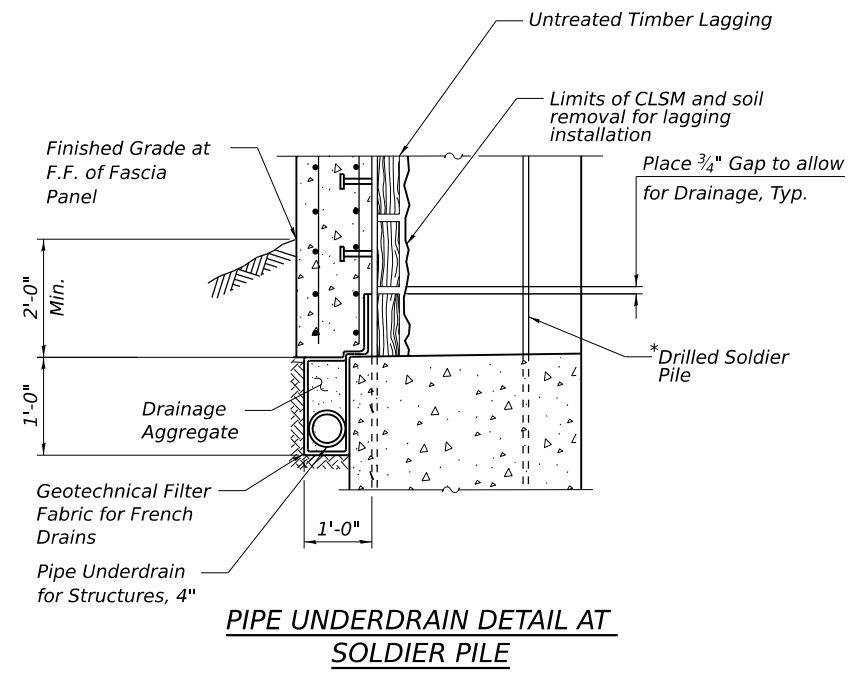


**CONSTRUCTION JOINT DETAILS**

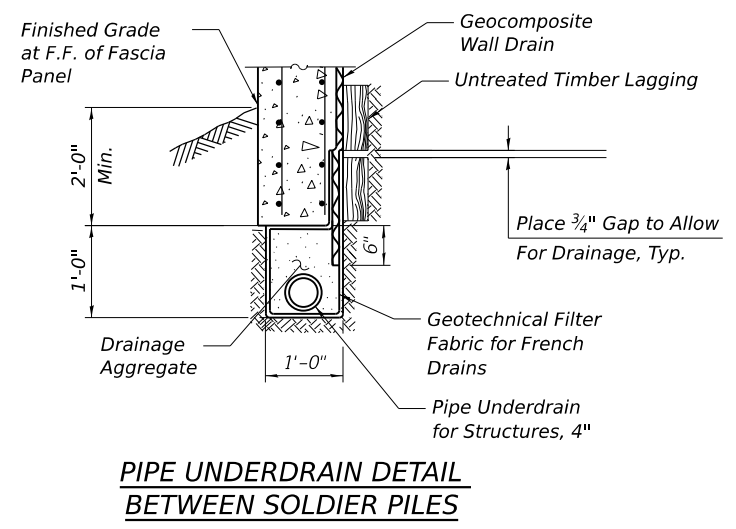


**EXPANSION JOINT DETAILS**

\*Pile section, spacing, tip elevation, shaft diameter and embedment into bedrock to be determined during final design.



**PIPE UNDERDRAIN DETAIL AT SOLDIER PILE**



**PIPE UNDERDRAIN DETAIL BETWEEN SOLDIER PILES**

**DRILLED SOLDIER PILE WALL DETAILS**  
**SOUTHEAST RETAINING WALL**  
**ALONG RIVER ROAD**  
**F.A.I. RTE. I-80**  
**SECTION 2021-151-B**  
**WILL COUNTY**  
**STA. 28+00.42 TO STA. 31+62.09**  
**STRUCTURE NO. 099-W806**



USER NAME =	DESIGNED - SK, JJS	REVISED -
PLOT SCALE =	CHECKED - MI, JJS, SK	REVISED -
PLOT DATE =	DRAWN - JMI, SK	REVISED -
	CHECKED - MI, JJS, SK	REVISED -

**STATE OF ILLINOIS**  
**DEPARTMENT OF TRANSPORTATION**

SHEET 3 OF 3 SHEETS

F.A.I. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
80	2021-151-B	WILL	3	3
CONTRACT NO. 62P67				
ILLINOIS FED. AID PROJECT				

## **APPENDIX F**





















