

MOMENT AND REACTION TABLES

INTERIOR GIRDER MOMENT TABLE	
0.5 Sp.	
$I_s$	(in <sup>4</sup> ) 9,727
$I_c$ (n)	(in <sup>4</sup> ) 29,532
$I_c$ (3n)	(in <sup>4</sup> ) 20,805
$S_s$	(in <sup>3</sup> ) 711
$S_c$ (n)	(in <sup>3</sup> ) 985
$S_c$ (3n)	(in <sup>3</sup> ) 910
$Z$	(in <sup>3</sup> )
$\bar{\rho}$	(k/ft.) 0.85
$M\bar{\rho}$	(k) 917
$s\bar{\rho}$	(k/ft.) 0.35
$M_s\bar{\rho}$	(k) 378
$M\bar{L}$	(k) 844
$M$ (Imp)	(k) 193
$\bar{S}_2[M\bar{L} + M(\text{Imp})]$	(k) 1,730
$M_a$	(k) 3,931
* $M_u$	(k) 4,509
$f_s\bar{\rho}$ non-comp (k.s.i.)	15.5
$f_s\bar{\rho}$ (comp) (k.s.i.)	5.0
$f_s\bar{S}_2$ (k + Imp) (k.s.i.)	12.6
$f_s$ (Overload) (k.s.i.)	41.5
* $f_s$ (Total) (k.s.i.)	54.0
VR	(k) 54.0

INTERIOR GIRDER REACTION TABLE		
	W. Abut.	E. Abut.
R $\bar{\rho}$	(k) 55.7	55.7
R $\bar{L}$	(k) 43.9	43.9
Imp.	(k) 10.1	10.1
R (Total)	(k) 109.7	109.7

$I_s, S_s$ : Non-composite moment of inertia and section modulus of the steel section used for computing  $f_s$  (Total and Overload) due to non-composite dead loads (in<sup>4</sup> and in<sup>3</sup>).

$I_c(n), S_c(n)$ : Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing  $f_s$  (Total and Overload) due to short-term composite live loads (in<sup>4</sup> and in<sup>3</sup>).

$I_c(3n), S_c(3n)$ : Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing  $f_s$  (Total and Overload) due to long-term composite (superimposed) dead loads (in<sup>4</sup> and in<sup>3</sup>).

$Z$ : Plastic Section Modulus of the steel section in non-composite areas (in<sup>3</sup>).

$\bar{\rho}$ : Un-factored non-composite dead load (kips/ft.).

$M\bar{\rho}$ : Un-factored moment due to non-composite dead load (kip-ft.).

$s\bar{\rho}$ : Un-factored long-term composite (superimposed) dead load (kips/ft.).

$M_s\bar{\rho}$ : Un-factored moment due to long-term composite (superimposed) dead load (kip-ft.).

$M\bar{L}$ : Un-factored live load moment (kip-ft.).

$M$  (Imp): Un-factored moment due to impact (kip-ft.).

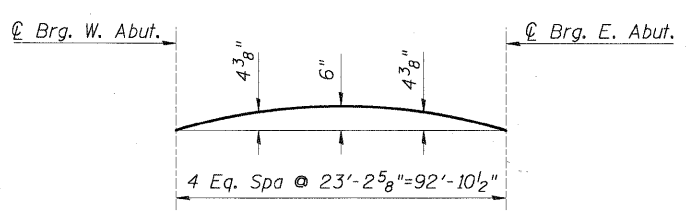
$M_a$ : Factored design moment (kip-ft.).  
 $1.3 [M\bar{\rho} + M_s\bar{\rho} + \frac{5}{8} (M\bar{L} + M_{\text{Imp}})]$

$M_u$ : Compact composite moment capacity according to AASHTO LFD 10.50.1.1. or compact non-composite moment capacity according to AASHTO LFD 10.48.1 (kip-ft.).

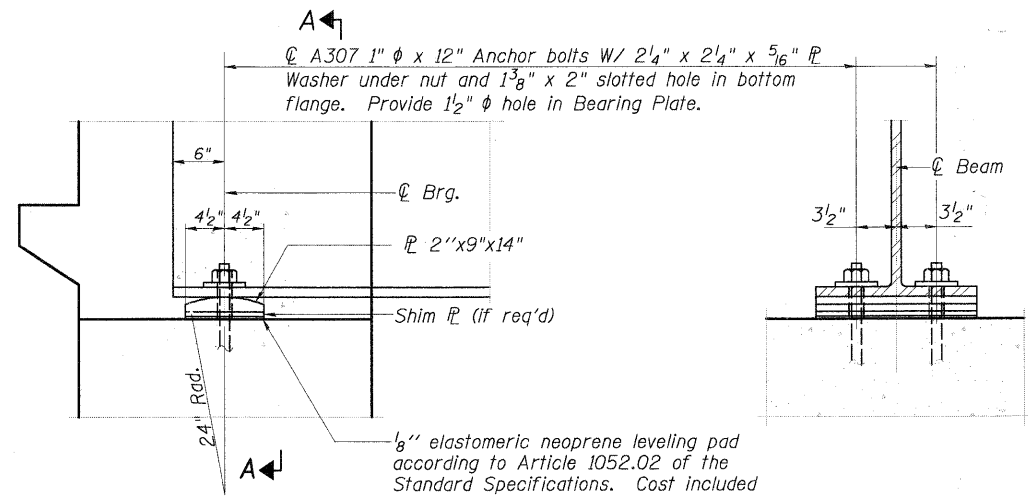
$f_s$  (Overload): Sum of stresses as computed from the moments below (ksi).  
 $M\bar{\rho} + M_s\bar{\rho} + \frac{5}{8} (M\bar{L} + M_{\text{Imp}})$

$f_s$  (Total): Sum of stresses as computed from the moments below on non-compact section (ksi).  
 $1.3 [M\bar{\rho} + M_s\bar{\rho} + \frac{5}{8} (M\bar{L} + M_{\text{Imp}})]$

VR: Maximum  $\bar{L}$  + impact horizontal shear range within the composite portion of the span for stud shear connector design (kips).



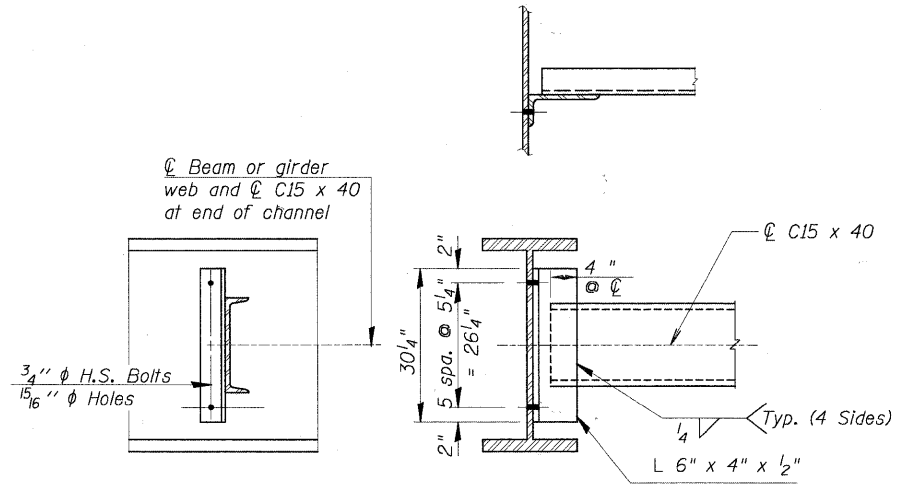
CAMBER DIAGRAM



ELEVATION

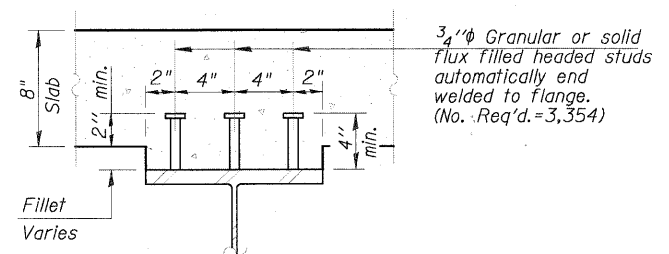
SECTION A-A

BEARING DETAILS

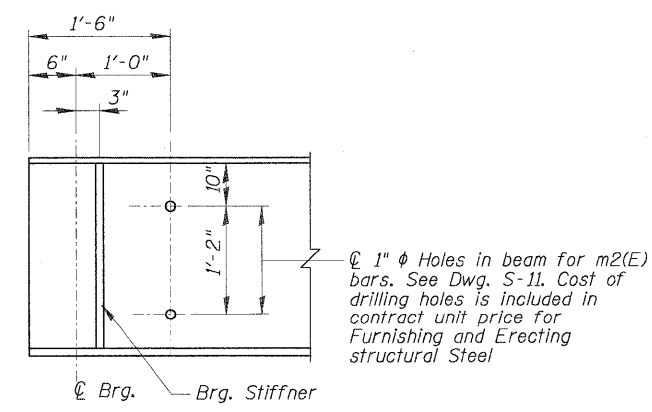


INTERIOR DIAPHRAGM

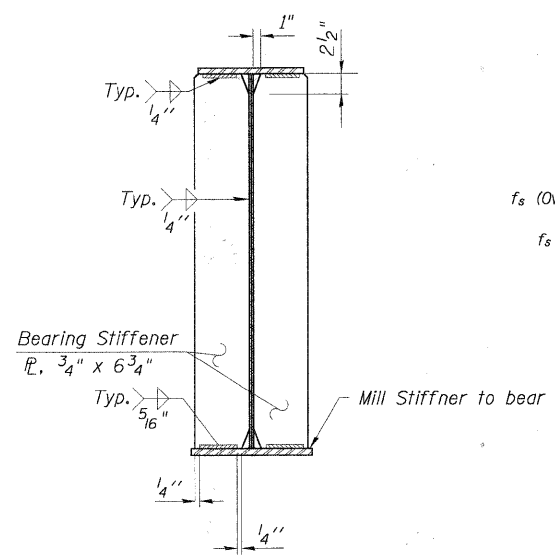
Note:  
Two hardened washers shall be required over all oversize holes for diaphragms.



SECTION A-A



TYPICAL END OF BEAM ELEVATION



BEARING STIFFNER DETAIL

CHRISTOPHER B. BURKE ENGINEERING, LTD.  
 8575 W. Higgins Road, Suite 600  
 Rosemont, Illinois 60018  
 (847) 823-0600



FILE NAME =	USER NAME = BLUKE	DESIGNED - MM	REVISED -
N:\kanecounty\B4198\STRUCT.2\B4198-S14.SHT		DRAWN - PDR	REVISED -
	PLOT SCALE = 1"	CHECKED - MM	REVISED -
	PLOT DATE = 2/7/2011	DATE -	REVISED -

STATE OF ILLINOIS  
 DEPARTMENT OF TRANSPORTATION

STEEL DETAILS

SHEET NO. S-14 OF S-21

F.A.S. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
0130	01-00266-00-BR	KANE	70	51
				CONTRACT NO. 63196
FED. ROAD DIST. NO. 1 [ILLINOIS] FED. AID PROJECT BRM-80030431				

F.A.S. 0130 - BIG TIMBER ROAD  
 OVER TYLER AND PINGREE CREEK  
 SECTION 01-00266-00-BR  
 KANE COUNTY, ILLINOIS  
 STA. 135+80.00  
 STRUCTURE NO. 045-3323