



Abbreviated Structure Geotechnical Report

Original Report Date: 9/10/17 **Proposed SN:** 053-2582 **Route:** FAI-55 (I-55)
Revised Date: 11-2-17 **Existing SN:** 053-0126&0127 **Section:** (53-5)R&I
Geotechnical Engineer: Terry McCleary of McCleary Engineering **County:** Livingston
Structural Engineer: Vincent Tabor, Lin Engineering **Contract:** 66B64

Indicate the proposed structure type, substructure types, and foundation locations (attach plan and elevation drawing): The existing bridges are twin 2 span structures (northbound and southbound), 148.83 ft. back to back of abutments. SN 046-0126 is the southbound structure and SN 046-0127 is the northbound structure. The existing stub abutments are supported on two rows of steel H-piles. There is no skew. The proposed improvements include the removal of both structures, lowering of the profile grade and replacing them with a single 14 ft. x 10 ft. box culvert. Factored loadings are calculated to be 3000 ksf at the bottom of the bottom slab. Please refer to the attached TS&L drawing for further details.

Discuss the existing boring data, existing plans foundation information, new subsurface exploration and need for any additional exploration to be provided with SGR Technical Memo (attach all data and subsurface profile plot): As mentioned above the existing plans show the piers and abutments are supported by driven H-piles. The 1970 and 2017 borings both show shale, but at differing elevations. The 1970 borings show the Shale to be near the elevation of 622.0 ft. The 2017 borings show auger refusal in the realm of 634.0 ft. This auger refusal could have been on a boulder described in the lithology above the refusal elevation.

The 1970 borings are approximately 12 ft. deeper than the 2017 borings. The 1970 borings show 3.5 ft. of stiff clay soils over very stiff to hard clay till with occasional pockets of very dense gravel within the till layers over a green to blue/green shale.

The four 2017 borings show a varying soils profile. Boring 01 shows 2.5 ft. of black silty clay loam fill over 2.5 ft. of very stiff brown silty clay loam over loose very loamy fine sand to coarse gravel to cobbles/boulders. Boring 02 shows 2.5 ft. black silty clay loam fill over 5 ft. of very stiff brown and gray silty clay loam fill with cobbles and boulders. The boring was stopped at 7.5 ft. with auger refusal. Boring 03 did not sample the soils, but rather was advanced to a depth of 9.5 ft. with auger refusal. Boring 04 shows 2.5 ft. of black silty clay loam fill over 2 ft. of very stiff silty clay loam fill over 7.5 ft. of stiff to very stiff silty clay loam till fill with large limestone gravel pieces to cobbles/boulders. This boring ended with auger refusal at a depth of 12 ft.

Please see the attached boring logs for a more detailed description of the soils encountered.

Provide the location and maximum height of any new soil fill or magnitude of footing bearing pressure. Estimate the amount and time of the expected settlement. Indicate if further testing, analysis, and/or ground improvement/treatment is necessary: The area surrounding the bridges is very flat with no hydraulic issues; the proposed design will require the placement of as much as 19 ft. of new fill adjacent to the proposed box with approximately 9 ft. of new fill above the proposed box. Using two separate combinations of borings, the first being boring 2 (2017) with boring 7 (1970) and the second combination using boring 2 (1970) with boring 4 (2017), both with and without the culvert. As much as 0.78 inches of settlement is expected using boring 2 with boring 7 adjacent to the box culvert structure where the fill is its highest. Using the same loading, but with boring 2 and boring 4 together the resulting settlement is estimated to be 0.70 inches. To estimate the settlement under the culvert the thickness of the fill was reduced to 9 ft. in the analysis. The estimated settlement is 0.52 inches and 0.48 inches, respectively. A differential settlement as much as 0.3 inches may be expected. These amounts of settlement are typically not large enough to be a concern for a cast in place box culvert.

A more extensive analysis could be performed and the settlement amounts refined, however that would require shelly tube samples for consolidation testing. However, because of the rocky nature and in many places the soils density, the successful collection of shelly tube samples is unlikely. The rudimentary analysis performed is an estimation because of the shallow depths of the borings and assumptions needed to complete the analysis. With the lack of necessary laboratory test results, a more detailed analysis could not be performed. Since the soils moisture contents and unconfined compressive strengths were provided in the boring logs, the IDOT spreadsheet for the calculation of settlement for cohesive soils was used. The proposed fill material should be placed in accordance with article 205 of the standard specifications and be benched into the existing embankments.

Identify any new cuts or fill slope angles and heights. Estimate the factor of safety against slope failure. Indicate if further testing, analysis or ground improvement/treatment is necessary: With the lowering of the profile grade, the height of the side slopes will be significantly reduced. The proposed slopes beyond the wing walls, but inside the area of new fill were analyzed using the commercial software, Slide 6.0, using the Bishop Method. The slopes from the edge of shoulder to the headwall are to be a 1:6 (V:H) and 1:2 (V:H) from the head wall out to the tip of the wing wall. The resulting FOS is 6.6 for the undrained (Short Term) condition, which is much greater than the desired 1.5, therefore no further testing or analysis is recommended.

Indicate at each substructure, the 100-year and 200-year total scour depths in the Hydraulics report, the non-granular scour depth reduction, the proposed ground surface, and the recommended foundation design scour elevations: Scour will not be an issue at this site as it does not cross a waterway, but rather is a pedestrian/bike path on the alignment of a past railroad bed.

Determining the seismic soil site class, the seismic performance zone, the 0.2 and 1.0 second design spectral accelerations and indicate if that the soils are liquefiable: This structure is a buried structure. Per Section 2.3.10 of the Departments Bridge Manual seismic data is not needed for most walls or buried structures.

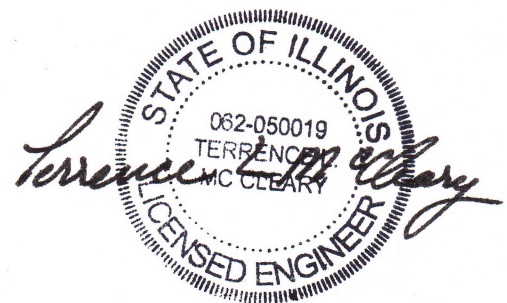
Confirm feasibility of the proposed foundation or wall type and provide design parameters. Attach a pile design table indicating feasible pile types, various nominal required bearings, factored resistances available and corresponding estimated lengths at locations where piles will be used. Provide factored bearing resistance and unit sliding resistance at various elevations and confirm no ground improvement/treatment is necessary where spread footings are proposed. Estimated top of rock elevations as well as preliminary factored unit side and tip resistance values shall be indicated when drilled shafts are proposed:

The fill height and size of structure currently allows for the use of horizontal cantilever wingwalls. Using the methodology shown in Chapter 4 of the Department's Culvert Manual, the unfactored loads on the proposed 16 ft. long wingwalls are estimated to be; $P_A = 825$ lbs/ft. at the tallest point of the wingwall, $P_B = 462$ lbs/ft. at the shortest point of the wall with a moment of 102 k-ft. These walls are expected to be designed using this same manual.

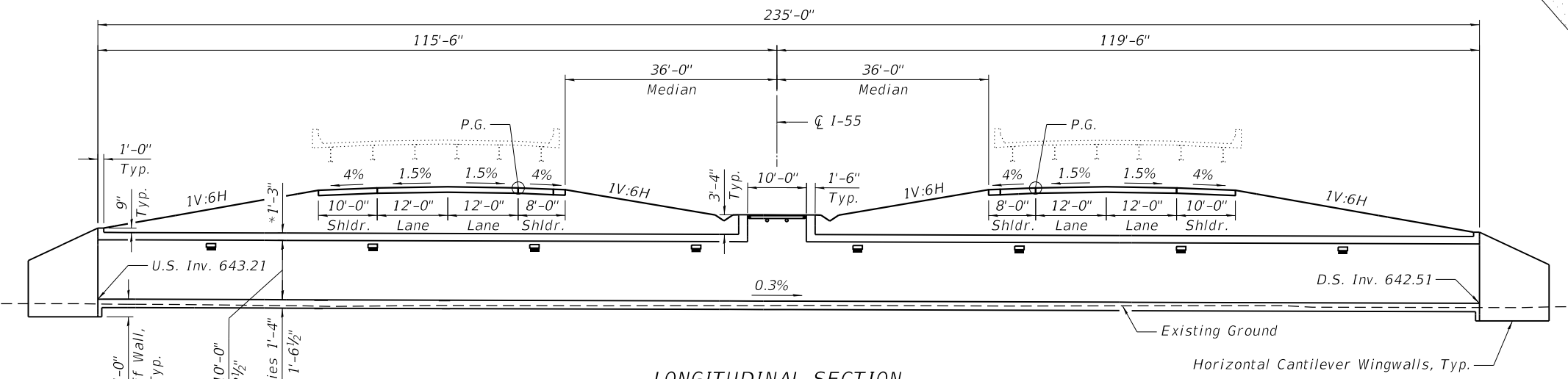
Calculate the estimated water surface elevation and determine the need for cofferdams (type 1 or 2), and seal coat: Neither cofferdams nor seal coats will be needed at this site as the project does not involve any in-stream work.

Assess the need for sheeting or soil retention or temporary construction slope and provide recommendation for other construction concerns: This project will be constructed using staged Traffic Control with crossovers, dictating the need for soil retention at a stage line in the median. The bedrock is relatively shallow and may not allow the required embedment depth for sheet pile walls. The use of the pay item for a "Temporary Soil Retention System" is recommended. Since this is a fill condition, the use of a Temporary MSE Wall or a Temporary Geotextile Wall is recommended.

Prepared by McCleary Engineering
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office – 815-780-8486

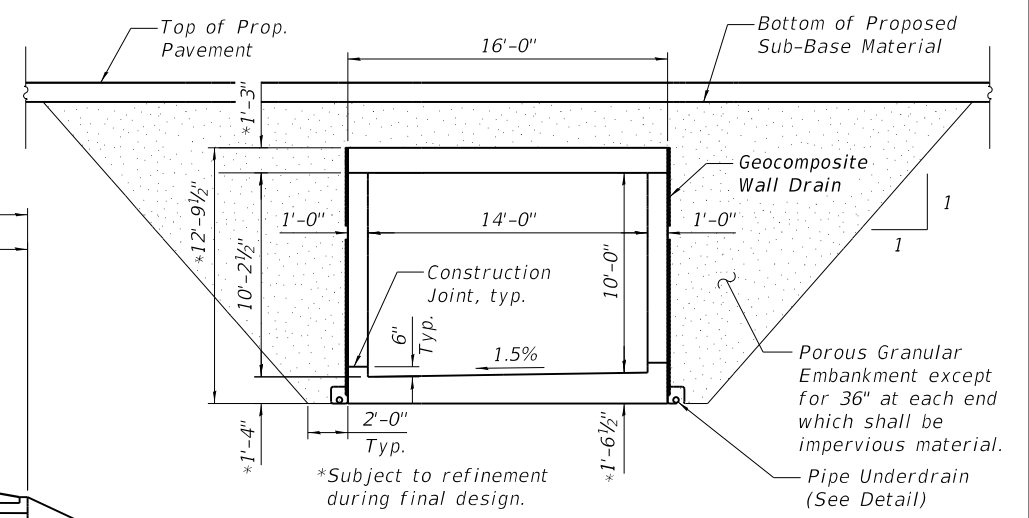


Benchmark: BM 83 - Chiseled "I" on top of Southeast wingwall, S.N. 053-0126, Southbound I-55, Elev. 672.14.
 Existing Structure: S.N. 053-0126 & 053-0127 were built in 1973 as F.A.I. 55, Section 53-5VB-1 at Sta. 136+65.28. Existing structures are 3-span continuous bridges with W30 steel beams, stub abutments and multi-column piers. 148'-10" bk to bk. abutments, 42'-0" out to out deck with no skew. Both existing structures will be removed and replaced with a shared use path culvert. The culvert will be constructed in its entirety, followed by removal of the existing structures and construction of the roadway by halves using crossovers in order to maintain one lane of traffic in each direction.
 No Salvage.
 Precast alternate is not allowed.



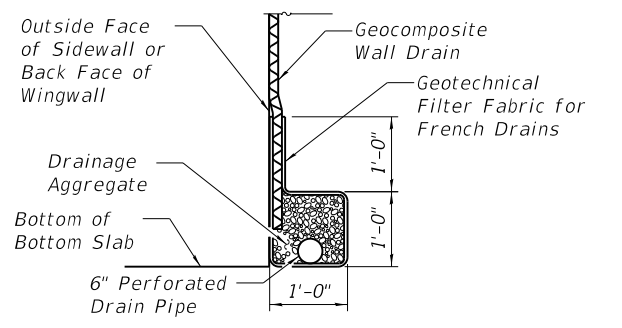
Future lights by others. Number and spacing to be determined.

LONGITUDINAL SECTION
 (Invert Elevations at Centerline of Barrel)

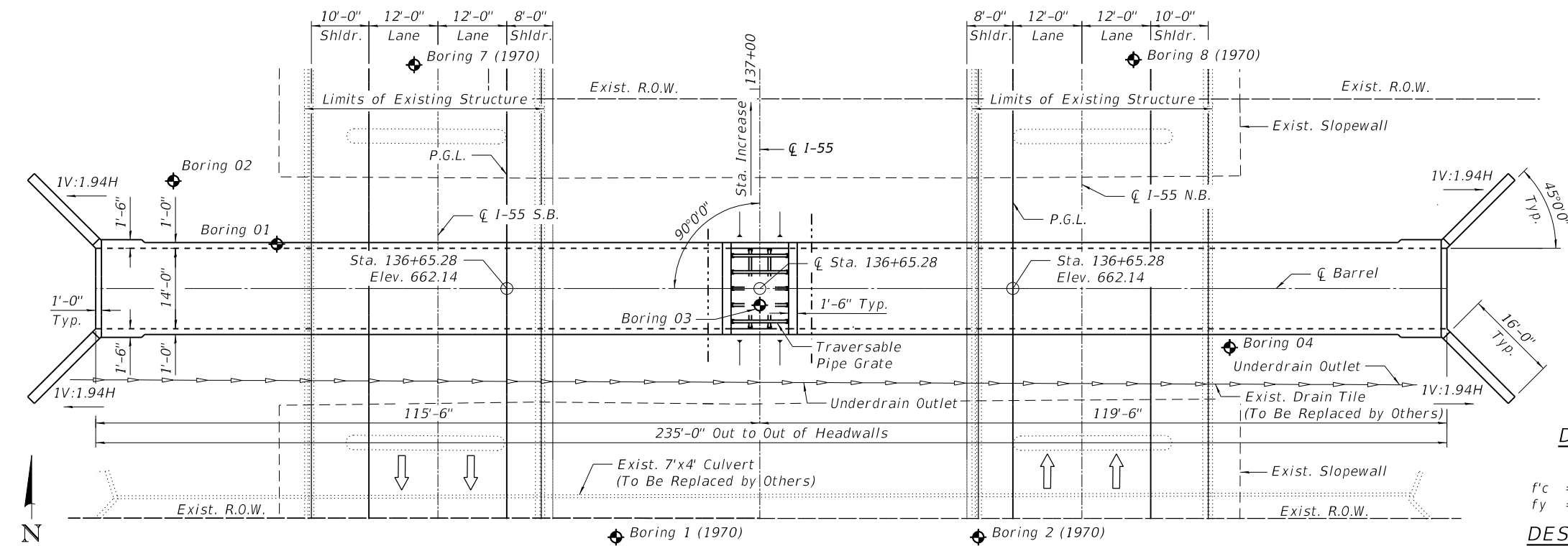


SECTION THRU BARREL
 (Looking West)

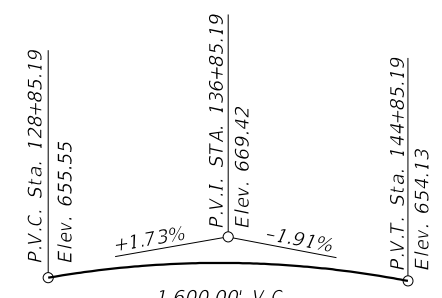
HIGHWAY CLASSIFICATION
 F.A.I. Route 55 (I-55)
 Functional Class: Interstate
 ADT: 22,973 (2019), 27,300 (2039)
 DHV: 2,184 (2039)
 ADTT: 8,190 (2039)
 Design Speed: 75 mph
 Posted Speed: 70 mph
 Two-Way Traffic
 Directional Distribution 50:50



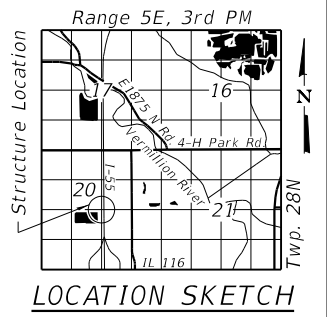
PIPE UNDERDRAIN DETAIL



PLAN



PROFILE GRADE
 (Along inside E.O.P.)



LOCATION SKETCH

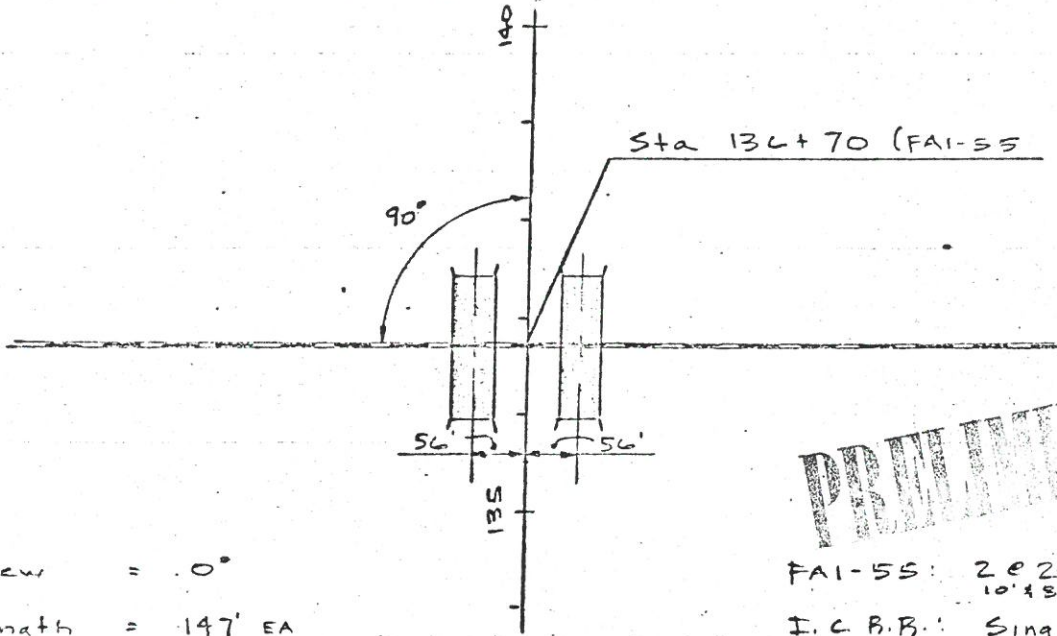
DESIGN STRESSES
 FIELD UNITS
 f'c = 3,500 psi
 fy = 60,000 psi (reinforcement)

DESIGN SPECIFICATIONS
 2014 AASHTO LRFD Bridge Design Specifications
 7th Edition with 2015 & 2016 interims
LOADING HL-93
 Allow 50#/sq. ft. for Future Wearing Surface

GENERAL PLAN AND ELEVATION
I-55 OVER ABANDONED R.R.
F.A.I. 55 SEC. (53-5)R&I
LIVINGSTON COUNTY
STATION 136+65.28
S.N. 053-2582

Structure Data - FAI-55 over I. C. R. R.

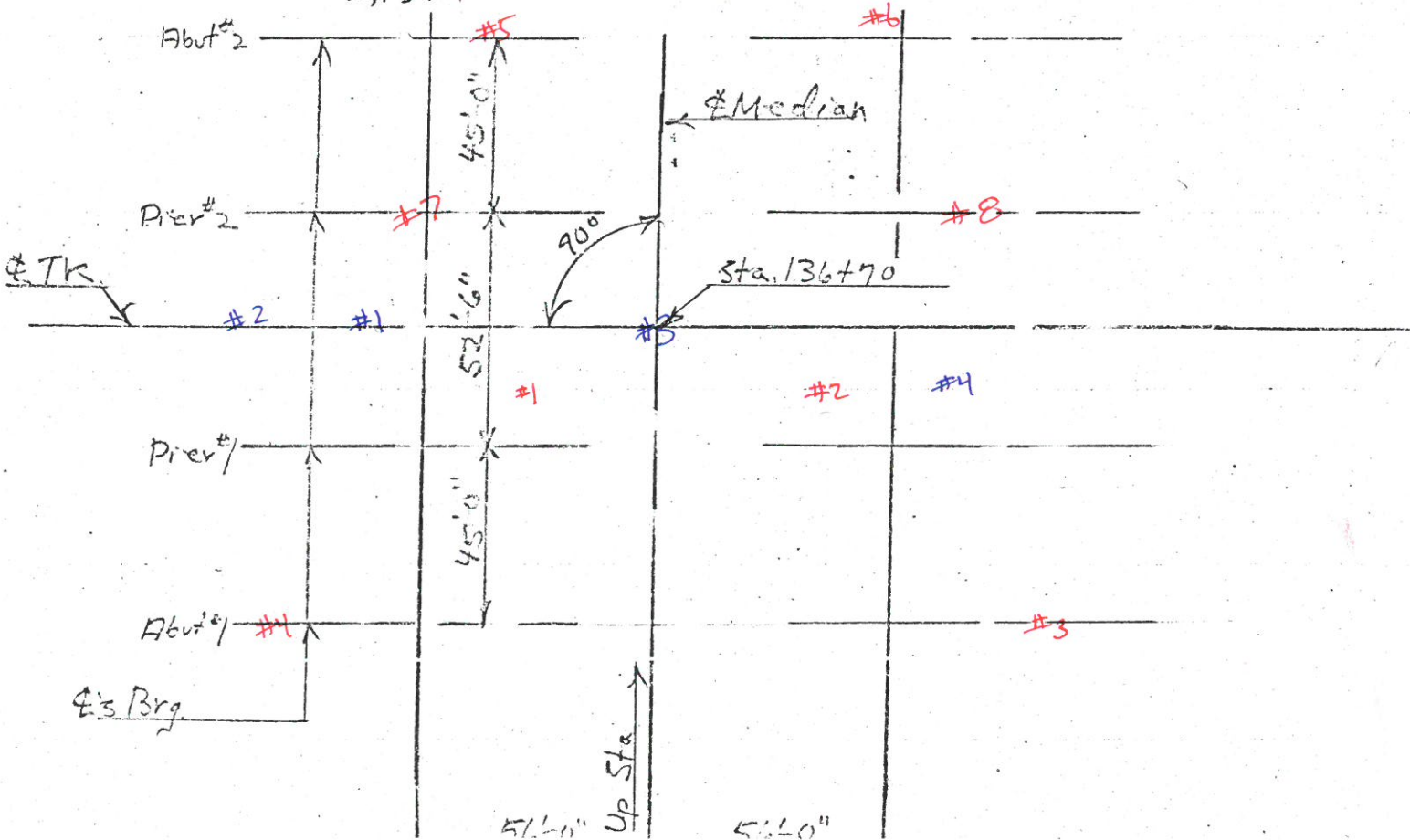
53-5VB



PRELIMINARY

Skew = 0°
 Length = 147' EA
 Width = 44' EA
 Deck Area = 6,468 # x 2 Structures
 = 12,936 #

FAI-55: 2 @ 24' w/ 8' Median
 10' @ 8' Shldrs
 I. C. R. R.: Single track





SOIL BORING LOG

ROUTE FAI-55 (I-55) DESCRIPTION I-55 over I.C. Railroad, 0.5 miles North of IL 116 LOGGED BY J. Safranski

SECTION 53-5VB-1 LOCATION SW 1/4, SEC. 20, TWP. 28N, RNG. 5E, 3rd PM,
Latitude , Longitude

COUNTY Livingston DRILLING METHOD _____ HAMMER TYPE _____

STRUCT. NO. 053-0126/0127
Station 136+65.28

BORING NO. 1
Station 136+22
Offset 25.0 ft Lt.
Ground Surface Elev. 641.48 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
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Surface Water Elev. None ft
Stream Bed Elev. _____ ft

Groundwater Elev.:
First Encounter _____ ft
Upon Completion Dry ft
After 26 Hrs. 636.5 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
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Stiff Yellow - Brown Clay to Clay Till, Slight amount of Organic Material present				Very Stiff Green to Purple Clay, seems to be a Reworked Shale (continued)	23	S	
	3						
	4	1.8	25		619.48	70	
	4	P		Rock - Blue to Green Shale	619.44	100/0.5"	6
637.98				End of Boring			
Hard Tan to Brown Clay Till	7						
	11	4.5	15				
	14	S			-25		
635.48							
Very Dense Yellow - Brown to Gray Gravel and Fine Sand, same Clay Till present	94						
	39		8				
	26						
	17						
	32		7				
	17				-30		
2" Layer of Limestone at 10.5'							
630.48							
Very Stiff Gray - Blue Clay to Clay Till	10						
	17	3.9	13				
	27	S					
627.98							
Very Stiff Brick Red to Blue Clay Till	17						
	16	3.9	11				
	26	S			-35		
	15						
	19	4.6	12				
	24	S					
622.98							
Very Stiff Green to Purple Clay, seems to be a Reworked Shale	9						
	14	3.2	11				
					-40		

SOIL BORING 053-0126, 0127.GPJ IL_DOT.GDT 5/24/17

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



SOIL BORING LOG

ROUTE FAI-55 (I-55) DESCRIPTION I-55 over I.C. Railroad, 0.5 miles North of IL 116 LOGGED BY J. Safranski

SECTION 53-5VB-1 LOCATION SE 1/4, SEC. 20, TWP. 28N, RNG. 5E, 3rd PM,
Latitude , Longitude

COUNTY Livingston DRILLING METHOD _____ HAMMER TYPE _____

STRUCT. NO. 053-0126/0127
Station 136+65.28

BORING NO. 2
Station 136+22
Offset 38.0 ft Rt.
Ground Surface Elev. 641.26 ft

D E P T H H	B L O W S	U C S Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

Surface Water Elev.	<u>None</u>	ft
Stream Bed Elev.	_____	ft
Groundwater Elev.:		
First Encounter	_____	ft
Upon Completion	<u>Dry</u>	ft
After <u>22</u> Hrs.	<u>636.3</u>	ft ∇

D E P T H H	B L O W S	U C S Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

Stiff Yellow - Brown to Tan Clay Till, Very Slightly Stratified				End of Boring				
	3							
	3	1.2	22					
	3	B						
	5							
	∇ -5	6	1.6	15				
	30	B						
635.26								
Hard Light Yellow - Brown Clay Till	6							
	12	4.1	13					
Small Sandstone Pebbles at 8.0'	20	B						
632.76								
Very Stiff Green to Brown Clay Till Some Organic Materials at 9.0'	6							
	-10	11	3.1	17				
	11	B						
	7							
	13	4.5	13					
	18	P						
627.76								
Very Stiff Brick Red to Green Clay Till	9							
	-15	14	3.5	11				
	21	S						
	16							
	22	4.2	12					
	22	S						
621.68								
Rock - Green Reworked? Shale	8							
	-20	90	4.0	10				

SOIL BORING 053-0126, 0127.GPJ IL_DOT.GDT 5/24/17

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



ROUTE FAI-55 (I-55) DESCRIPTION I-55 over I.C. Railroad, 0.5 miles North of IL 116 LOGGED BY J. Safranski

SECTION 53-5VB-1 LOCATION SE 1/4, SEC. 20, TWP. 28N, RNG. 5E, 3rd PM,
Latitude , Longitude

COUNTY Livingston DRILLING METHOD _____ HAMMER TYPE _____

STRUCT. NO. 053-0126/0127
Station 136+65.28

BORING NO. 3
Station 135+99
Offset 78.0 ft Rt.
Ground Surface Elev. 641.42 ft

DEPTH H S Qu T	B L O W S	U C S Qu	M O I S T T	Surface Water Elev.	None	D E P T H H	B L O W S	U C S Qu	M O I S T T
				Stream Bed Elev.					

DEPTH H S Qu T	B L O W S	U C S Qu	M O I S T T	Surface Water Elev.	None	D E P T H H	B L O W S	U C S Qu	M O I S T T
				Stream Bed Elev.					
	4	1.6 B	24						
	6								
	3								
	-5	0.9 B	23						
	6								
	5								
	6	2.3 B	20						
	9								
	5								
	8	1.8 S	20						
	11								
	7								
	15	3.7 S	14						
	19								
	11								
	24	4.4 S	13						
	31								
	19								
	27	4.5 P	12						
	51								
	9								
	18	1.7	11						

SOIL BORING 053-0126, 0127.GPJ IL_DOT.GDT 5/24/17

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



SOIL BORING LOG

ROUTE FAI-55 (I-55) DESCRIPTION I-55 over I.C. Railroad, 0.5 miles North of IL 116 LOGGED BY J. Safranski

SECTION 53-5VB-1 LOCATION SW 1/4, SEC. 20, TWP. 28N, RNG. 5E, 3rd PM,
Latitude , Longitude

COUNTY Livingston DRILLING METHOD _____ HAMMER TYPE _____

STRUCT. NO. 053-0126/0127
Station 136+65.28

BORING NO. 4
Station 135+99
Offset 78.0 ft Lt.
Ground Surface Elev. 642.22 ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
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Surface Water Elev. None ft
Stream Bed Elev. _____ ft

Groundwater Elev.:
First Encounter Dry ft
Upon Completion _____ ft
After _____ Hrs. _____ ft

D E P T H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
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Stiff Yellow - Brown Clay to Clay Till				621.78	70/5"		
	3			621.72	100/0.25"		
	5	1.9	25				
	6	B					
638.72							
Very Stiff Yellow - Brown Clay Till, Stratified	2						
	-5	2	17		-25		
	3	P					
636.22							
Very Dense Yellow - Brown to Gray Gravel							
At 7.0', Hit Large Gravel Layer - No Recovery							
633.72							
Very Stiff Black - Brown to Gray Clay Till	7						
	-10	9	15		-30		
	9	S					
631.22							
Hard Gray - Green to Tan Clay Till, Stratified	10						
		18	17				
		26	S				
628.72							
Very Stiff Brick Red to Green Clay Till	9						
	-15	18	16		-35		
		28	S				
		12					
		24	4.2				
		39	S				
		20					
-20	70				-40		

SOIL BORING 053-0126, 0127.GPJ IL_DOT.GDT 5/24/17

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



SOIL BORING LOG

ROUTE FAI-55 (I-55) DESCRIPTION I-55 over I.C. Railroad, 0.5 miles North of IL 116 LOGGED BY J. Safranski

SECTION 53-5VB-1 LOCATION NW 1/4, SEC. 20, TWP. 28N, RNG. 5E, 3rd PM,
Latitude , Longitude

COUNTY Livingston DRILLING METHOD _____ HAMMER TYPE _____

STRUCT. NO. 053-0126/0127
Station 136+65.28

BORING NO. 5
Station 137+40
Offset 42.0 ft Lt.
Ground Surface Elev. 640.92 ft

D E P T H	B L O W S	U C S Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

Surface Water Elev. None ft
Stream Bed Elev. _____ ft
Groundwater Elev.:
First Encounter Dry ft
Upon Completion _____ ft
After _____ Hrs. _____ ft

Stiff Yellow - Brown Clay Till	3			
	5	1.5	20	
	5	P		
	7			
634.92	-5	10	1.0	15
	11	P		
	6			
	10	3.3	14	
Very Stiff Lemon - Yellow to Gray - Green Clay Till, Slightly Stratified	18	B		
	10			
	-10	11	3.1	12
	14	S		
4" thick layer of Limestone at 12.0'	26			
	24		6	
	19			
	627.42			
Very Stiff Gray - Green Clay Till, Well Stratified	7			
	-15	11	3.5	12
	15	S		
	624.17			
Rock - Green Shale, Very Soft End of Boring	150/3"			
	-20			

SOIL BORING 053-0126, 0127.GPJ IL_DOT.GDT 5/24/17

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



ROUTE FAI-55 (I-55) DESCRIPTION I-55 over I.C. Railroad, 0.5 miles North of IL 116 LOGGED BY J. Safranski

SECTION 53-5VB-1 LOCATION NE 1/4, SEC. 20, TWP. 28N, RNG. 5E, 3rd PM,
 Latitude , Longitude

COUNTY Livingston DRILLING METHOD _____ HAMMER TYPE _____

STRUCT. NO. 053-0126/0127
 Station 136+65.28

BORING NO. 6
 Station 137+40
 Offset 42.0 ft Rt.
 Ground Surface Elev. 640.98 ft

DEPTH (ft)	BLOWS (/6")	UCS (tsf)	MOIST (%)
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Surface Water Elev. None ft
 Stream Bed Elev. _____ ft

Groundwater Elev.:
 First Encounter 639.0 ft ▼
 Upon Completion _____ ft
 After _____ Hrs. _____ ft

Soil Description	DEPTH (ft)	BLOWS (/6")	UCS (tsf)	MOIST (%)
Medium Yellow - Brown Clay ▼	3			
	3	0.9	19	
	3	B		
637.48				
Medium Yellow - Brown Clay Till	2			
	-5	6	0.9	12
	9	B		
634.98				
Very Stiff Gray - Green Clay Till Small Silt Seams present	9			
	9	2.9	14	
	17	S		
	9			
	-10	11	3.3	11
	15	S		
	9			
	15	4.1	15	
	26	B		
	9			
	-15	28	4.8	13
	40	S		
624.48				
Stiff Green to Brick Red Clay Till, Slightly Stratified	623.71	75/9"		
Rock - Blue to Green Shale End of Boring		100/0.25"	1.8	14
		S		
	-20			

SOIL BORING 053-0126, 0127.GPJ IL_DOT.GDT 5/24/17

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
 The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



SOIL BORING LOG

ROUTE FAI-55 (I-55) DESCRIPTION I-55 over I.C. Railroad, 0.5 miles North of IL 116 LOGGED BY J. Safranski

SECTION 53-5VB-1 LOCATION NW 1/4, SEC. 20, TWP. 28N, RNG. 5E, 3rd PM,
Latitude , Longitude

COUNTY Livingston DRILLING METHOD _____ HAMMER TYPE _____

STRUCT. NO. 053-0126/0127
Station 136+65.28

BORING NO. 7
Station 137+06
Offset 59.0 ft Lt.
Ground Surface Elev. 640.78 ft

DEPTH H S	B L O W S	U C S Qu	M O I S T	Surface Water Elev. _____ ft	D E P T H	B L O W S	U C S Qu	M O I S T
(ft)	(/6")	(tsf)	(%)	Stream Bed Elev. _____ ft	(ft)	(/6")	(tsf)	(%)

Stiff Yellow - Brown Clay Till
Silt Seams present
4
5 1.4 23
8 B

Very Dense Light Gray Limestone
with Alternating Thin Layers of
Shale (Rock Core)
Total Recovery of Rock Core = 18
inches out of 60 inches of Core
617.78 100/0.25"

End of Boring
3
-5 5 0.6 16
7 B
634.78

Stiff Black - Brown Silty Clay Till,
Very High in Organic Material
9
9 1.2 12
15 S
632.28

Very Stiff Gray to Green - Blue
Clay Till
34
-10 23 3.7 13
181 S
2" thick Shale Layer at 10.0'
13
25 3.5 12
47 S
627.28

Very Stiff Gray Clay Till, Slightly
Stratified
12
-15 13 3.3 15
12 S
624.78

Very Stiff Blue - Green Clay Till,
Well Stratified
8
16 2.5 14
622.78 100/4" S

Very Dense Gray Shale (Rock
Core)
100/0.5"
620.78 -20

SOIL BORING 053-0126, 0127.GPJ IL_DOT.GDT 5/24/17

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



Illinois Department of Transportation
 Division of Highways
 Illinois Department of Transportation

SOIL BORING LOG

ROUTE FAI-55 (I-55) DESCRIPTION I-55 over I.C. Railroad, 0.5 miles North of IL 116 LOGGED BY J. Safranski

SECTION 53-5VB-1 LOCATION NE 1/4, SEC. 20, TWP. 28N, RNG. 5E, 3rd PM,
 Latitude , Longitude

COUNTY Livingston DRILLING METHOD _____ HAMMER TYPE _____

STRUCT. NO. 053-0126/0127
 Station 136+65.28

BORING NO. 8
 Station 137+06
 Offset 65.0 ft Rt.
 Ground Surface Elev. 640.38 ft

DEPTH (ft)	BLOW S (1/6")	UCS (tsf)	MOIST (%)
4			
5	1.4	23	
7	B		
4			
-5	3	1.3	20
7	P		
7			
10	0.2	12	
20	B		
8			
9	3.7	14	
11	B		
11			
17	2.5	18	
32	B		
15			
25	3.7	12	
32	S		
19			
62	3.1	13	
79/4"	S		
100/1"			

Surface Water Elev. None ft
 Stream Bed Elev. _____ ft

Groundwater Elev.:
 First Encounter 638.4 ft ▼
 Upon Completion _____ ft
 After _____ Hrs. _____ ft

Stiff Yellow - Brown Clay Till			
	▼	4	
		5	1.4
		7	B
		4	
1" Thick Layer of Limestone at 5.0'	634.38	-5	3
		7	P
Very Soft Yellow - Brown to Brown Clay Loam		7	
	631.88	10	0.2
		20	B
Very Stiff Gray - Green Clay Till		8	
	629.38	-10	9
		11	3.7
			B
Very Stiff Gray Clay Till, Very Well Stratified		11	
	626.88	17	2.5
		32	B
Very Stiff Brick Red to Brown Clay Till, Slightly Stratified		15	
	624.38	-15	25
		32	3.7
			S
Very Stiff Green Clay, Well Stratified		19	
	622.88	62	3.1
Rock - Blue to Green Shale	622.46	79/4"	S
End of Boring		100/1"	
		-20	

SOIL BORING 053-0126, 0127, GPJ IL_DOT.GDT 5/24/17

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
 The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



**Illinois Department
of Transportation**

Division of Highways
Illinois Department of Transportation

SOIL BORING LOG

ROUTE FAI-55 (I-55) DESCRIPTION I-55 over Abandoned I.C. Railroad, 0.5 miles North of IL 116 LOGGED BY Larry Myers

SECTION (53-5)R&I LOCATION NW 1/4, SEC. 20, TWP. 28N, RNG. 5E, 3rd PM, Latitude 40.880764, Longitude -88.671625

COUNTY Livingston DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME Automatic

STRUCT. NO. 053-2582 (P)
053-0126/0127 (E)
Station 136+65.28

BORING NO. 01
Station 136+73
Offset 84.0 ft Lt.
Ground Surface Elev. 642.50 ft

DEPTH (ft)	BLOW COUNT (/6")	UCS (tsf)	MOISTURE (%)
---------------	------------------------	--------------	-----------------

Surface Water Elev.	_____	ft
Stream Bed Elev.	_____	ft
Groundwater Elev.:		
First Encounter	<u>635.0</u>	ft ▼
Upon Completion	<u>638.0</u>	ft ▼
After _____ Hrs.	_____	ft

Augered Brown Sand & Gravel Fill, Black Silty Clay Loam Fill				
640.00				
Very Stiff Brown Silty Clay Loam	3			
	4	3.1	25	
	5	B		
637.50	-5			
Loose Very Loamy Fine Sand to Coarse Gravel - Cobble / Boulders felt @ 9' Auger Refusal @ 9' on Limestone Cobble / Boulder - Potential Railroad Fill	3			
	2		19	
	3			
632.17	-10			
End of Boring		100/4"	2	
	-20			

SOIL BORING 053-0126, 0127.GPJ IL_DOT.GDT 6/27/17

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



Illinois Department of Transportation

Division of Highways
Illinois Department of Transportation

SOIL BORING LOG

ROUTE FAI-55 (I-55) DESCRIPTION I-55 over Abandoned I.C. Railroad, 0.5 miles North of IL 116 LOGGED BY Larry Myers

SECTION (53-5)R&I LOCATION NW 1/4, SEC. 20, TWP. 28N, RNG. 5E, 3rd PM, Latitude 40.880772, Longitude -88.67186

COUNTY Livingston DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME Automatic

STRUCT. NO. 053-2582 (P)
053-0126/0127 (E)
Station 136+65.28

BORING NO. 02
Station 136+84
Offset 102.0 ft Lt.
Ground Surface Elev. 641.93 ft

DEPTH (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
---------------	--------------------------------	----------------------------	------------------------------

Surface Water Elev. _____ ft
Stream Bed Elev. _____ ft
Groundwater Elev.:
First Encounter Dry ft
Upon Completion 634.9 ft ∇
After _____ Hrs. _____ ft

Augered Black Silty Clay Loam Fill			
639.43			
Very Stiff Brown & Gray Silty Clay Loam Fill	4		
Heavy Limestone Gravel, Boulders, Cobbles (Fill?) @7'	4	3.0	25
	5	P	
-5			
	3		
	3		21
	4		
∇ 634.43			
Auger Refusal @ 7.5' End of Boring	100/5"		0
-10			
-15			
-20			

SOIL BORING 053-0126, 0127.GPJ IL_DOT.GDT 6/27/17

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



Illinois Department of Transportation

Division of Highways
Illinois Department of Transportation

SOIL BORING LOG

ROUTE FAI-55 (I-55) DESCRIPTION I-55 over Abandoned I.C. Railroad, 0.5 miles North of IL 116 LOGGED BY Larry Myers

SECTION (53-5)R&I LOCATION NW 1/4, SEC. 20, TWP. 28N, RNG. 5E, 3rd PM, Latitude 40.880724, Longitude -88.671482

COUNTY Livingston DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME Automatic

STRUCT. NO. 053-2582 (P)
Station 053-0126/0127 (E)
136+65.28

BORING NO. 03
Station 136+65
Offset 0.0 ft Centerline
Ground Surface Elev. 642.76 ft

DEPTH T H	B L O W S	U C S Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

Surface Water Elev.	_____	ft
Stream Bed Elev.	_____	ft
Groundwater Elev.:		
First Encounter	<u>Dry</u>	ft
Upon Completion	_____	ft
After _____ Hrs.	_____	ft

Augered Material, No Samples

Auger Refusal @ 9.5' on Limestone Fill 633.26
End of Boring

SOIL BORING 053-0126, 0127.GPJ IL_DOT.GDT 6/27/17

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



Illinois Department of Transportation

Division of Highways
Illinois Department of Transportation

SOIL BORING LOG

Date 6/1/17

ROUTE FAI-55 (I-55) DESCRIPTION I-55 over Abandoned I.C. Railroad, 0.5 miles North of IL 116 LOGGED BY Larry Myers

SECTION (53-5)R&I LOCATION SE 1/4, SEC. 20, TWP. 28N, RNG. 5E, 3rd PM,
Latitude 40.880728, Longitude -88.67115

COUNTY Livingston DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME Automatic

STRUCT. NO. <u>053-2582 (P)</u> <u>053-0126/0127 (E)</u>	D E P T H	B L O W S	U C S	M O I S T	Surface Water Elev. _____ ft
					Stream Bed Elev. _____ ft
BORING NO. <u>04</u> Station <u>136+55</u> Offset <u>85.0 ft Rt.</u> Ground Surface Elev. <u>642.53</u> ft	(ft)	(/6")	(tsf)	(%)	Groundwater Elev.:
					First Encounter _____ <u>Dry</u> ft
					Upon Completion <u>630.5</u> ft ∇
					After _____ Hrs. _____ ft

Augered Brown Sand & Gravel Fill and Black Silty Clay Loam Fill 640.03 Very Stiff Brown Silty Clay Loam Fill 638.03 Very Stiff to Stiff Gray Silty Clay Loam Till Fill with Large Limestone Gravel Pieces @ 8' up to Cobbles / Boulders -5 3 22 21 -10 12 10 10 630.53 Auger Refusal @ 12' End of Boring -15 -20					
	3	4	2.5	27	
	5	P			
	3	3	2.0	21	
	3	P			
	3				
	22			5	
	21				
	12				
	10	3.5	9		
	10	P			
	41				
	100/3"			2	

SOIL BORING 053-0126_0127.GPJ IL_DOT.GDT 6/27/17

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)
BBS, form 137 (Rev. 8-99)

COHESIVE SOIL SETTLEMENT ESTIMATE

LOCATION AND BORING USED ===== West End/Boring #2 (2017) and #7 (1970) WITH CULVERT

TYPE OF SURCHARGE ===== 1 (1=2:1 bridge cone, 2=continuous embank., 3=rectangular surch.)

DEPTH TO WATER TABLE (below top of existing embankment) == 7 FT

NEW EMBANKMENT:

NEW EMBANKMENT FILL UNIT WEIGHT ===== 120 PCF
 NEW EMBANKMENT FILL HEIGHT ===== 19 FT
 PROPOSED WIDTH AT TOP ===== 156 FT
 PROPOSED WIDTH AT BOTTOM ===== 250 FT (which is a 2.5:1 slope)

ASSUMPTIONS:

Soil Deposit is Normally Consolidated
 Cohesive Layers are Saturated
 Soils have a Low Sensitivity
 Liquid Limit (LL)=Moist. Content (MC%)
 Initial Void Ratio (Eo)=2.7*(MC%)/100
 Comp. Index (Cc)=0.009*(LL-10)
 Neglecting Granular & Secondary Settlement

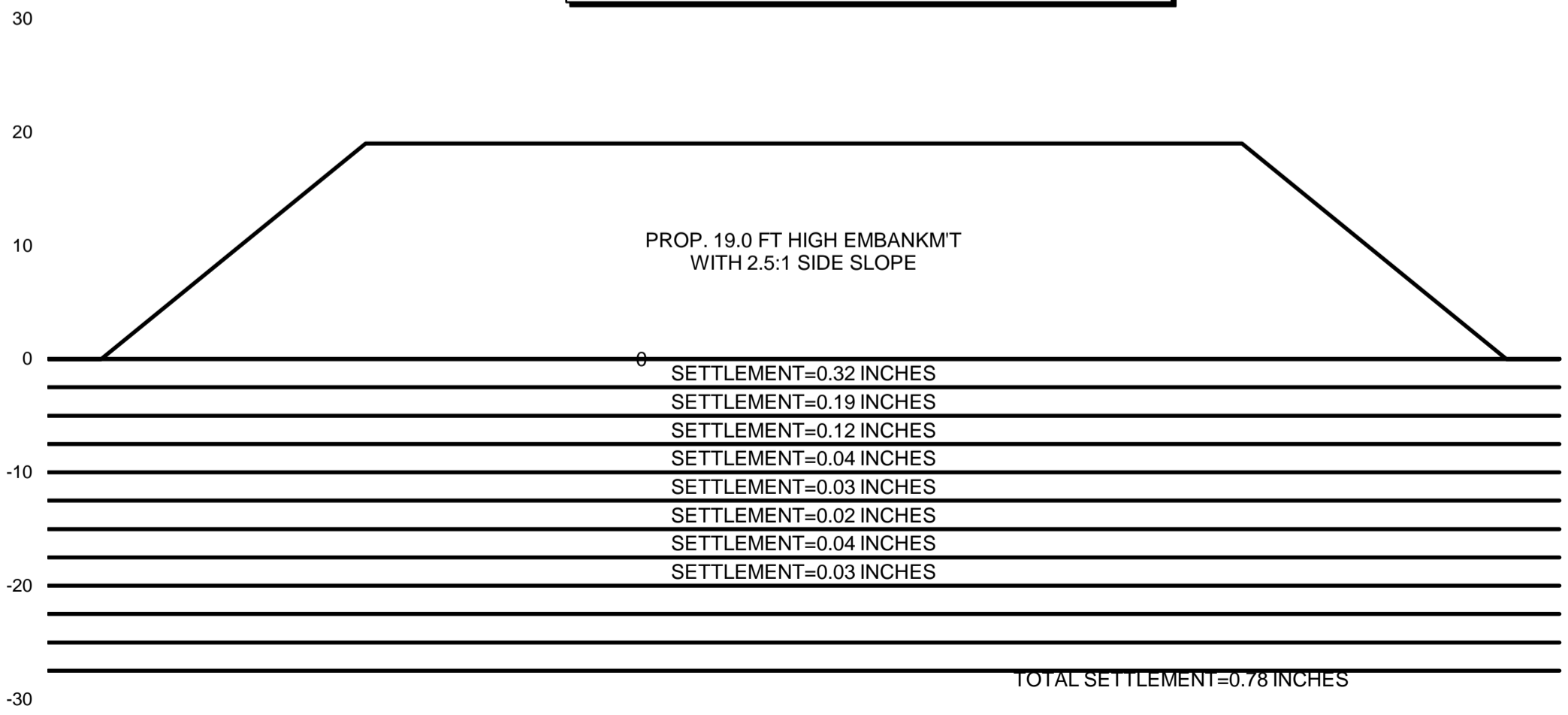
EXISTING EMBANKMENT (IF ANY):

EXISTING EMBANKMENT UNIT WEIGHT ===== 120 PCF
 EXISTING EMBANKMENT HEIGHT ===== 0 FT
 EXISTING WIDTH AT TOP ===== 0 FT
 EXISTING WIDTH AT BASE ===== 0 FT (which is a 0.0:1 slope)

LAYER THICK (FT)	TOTAL UNIT WT. (PCF)	UNCONF. COMP. STRENGTH (Qu) (TSF)	MOIST. CONTENT (%)	EXISTING PRESSURE (KSF)	PRESSURE INCREASE (KSF)	INITIAL VOID RATIO	COMPRESSION INDEX (Cc)	Qu CORRECTION FACTOR	LAYER SETTLEMENT (IN.)
2.5	120	2.00	25	0.150	2.256	0.675	0.135	0.111	0.32
2.5	120	3.00	25	0.450	2.209	0.675	0.135	0.100	0.19
2.5	120	2.00	21	0.750	2.162	0.567	0.099	0.111	0.12
2.5	120	1.20	12	0.941	2.115	0.324	0.018	0.171	0.04
2.5	120	3.70	13	1.085	2.070	0.351	0.027	0.100	0.03
2.5	120	3.50	12	1.229	2.027	0.324	0.018	0.100	0.02
2.5	120	3.30	15	1.373	1.985	0.405	0.045	0.100	0.04
2.5	120	2.50	14	1.517	1.944	0.378	0.036	0.100	0.03
2.5	120	5.00	7	1.661	1.905	0.189	0.000	0.100	0.00
2.5	120	5.00	7	1.805	1.868	0.189	0.000	0.100	0.00
2.5	120	5.00	7	1.949	1.833	0.189	0.000	0.100	0.00

TOTAL SETTLEMENT UNDER CENTER OF BRIDGE CONE = 0.78 IN.

EMBANKMENT AND SOIL PROFILE



COHESIVE SOIL SETTLEMENT ESTIMATE

LOCATION AND BORING USED ===== West End/Boring #2 (2017) and #7 (1970) WITHOUT CULVERT

TYPE OF SURCHARGE ===== 1 (1=2:1 bridge cone, 2=continuous embank., 3=rectangular surch.)

DEPTH TO WATER TABLE (below top of existing embankment) == 7 FT

NEW EMBANKMENT:

NEW EMBANKMENT FILL UNIT WEIGHT ===== 120 PCF
 NEW EMBANKMENT FILL HEIGHT ===== 9 FT
 PROPOSED WIDTH AT TOP ===== 156 FT
 PROPOSED WIDTH AT BOTTOM ===== 250 FT (which is a 5.2:1 slope)

ASSUMPTIONS:

Soil Deposit is Normally Consolidated
 Cohesive Layers are Saturated
 Soils have a Low Sensitivity
 Liquid Limit (LL)=Moist. Content (MC%)
 Initial Void Ratio (Eo)=2.7*(MC%)/100
 Comp. Index (Cc)=0.009*(LL-10)
 Neglecting Granular & Secondary Settlement

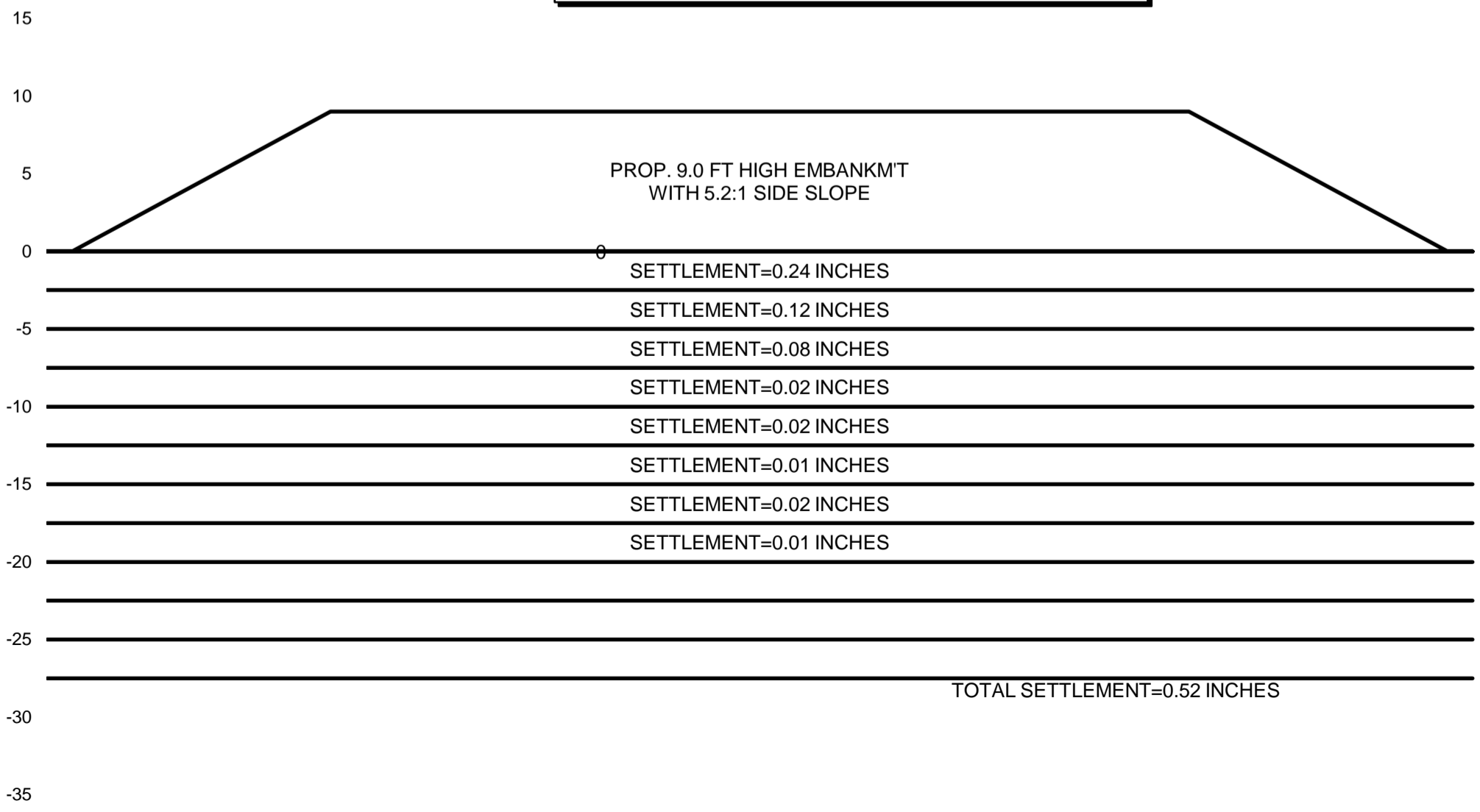
EXISTING EMBANKMENT (IF ANY):

EXISTING EMBANKMENT UNIT WEIGHT ===== 120 PCF
 EXISTING EMBANKMENT HEIGHT ===== 0 FT
 EXISTING WIDTH AT TOP ===== 0 FT
 EXISTING WIDTH AT BASE ===== 0 FT (which is a 0.0:1 slope)

LAYER THICK (FT)	TOTAL UNIT WT. (PCF)	UNCONF. COMP. STRENGTH (Qu) (TSF)	MOIST. CONTENT (%)	EXISTING PRESSURE (KSF)	PRESSURE INCREASE (KSF)	INITIAL VOID RATIO	COMPRESSION INDEX (Cc)	Qu CORRECTION FACTOR	LAYER SETTLEMENT (IN.)
2.5	120	2.00	25	0.150	1.056	0.675	0.135	0.111	0.24
2.5	120	3.00	25	0.450	1.009	0.675	0.135	0.100	0.12
2.5	120	2.00	21	0.750	0.965	0.567	0.099	0.111	0.08
2.5	120	1.20	12	0.941	0.924	0.324	0.018	0.171	0.02
2.5	120	3.70	13	1.085	0.888	0.351	0.027	0.100	0.02
2.5	120	3.50	12	1.229	0.855	0.324	0.018	0.100	0.01
2.5	120	3.30	15	1.373	0.827	0.405	0.045	0.100	0.02
2.5	120	2.50	14	1.517	0.801	0.378	0.036	0.100	0.01
2.5	120	5.00	7	1.661	0.779	0.189	0.000	0.100	0.00
2.5	120	5.00	7	1.805	0.760	0.189	0.000	0.100	0.00
2.5	120	5.00	7	1.949	0.743	0.189	0.000	0.100	0.00

TOTAL SETTLEMENT UNDER CENTER OF BRIDGE CONE = 0.52 IN.

EMBANKMENT AND SOIL PROFILE



COHESIVE SOIL SETTLEMENT ESTIMATE

LOCATION AND BORING USED ===== West End/Boring #4 and 2 WITH CULVERT

TYPE OF SURCHARGE ===== 1 (1=2:1 bridge cone, 2=continuous embank., 3=rectangular surch.)

DEPTH TO WATER TABLE (below top of existing embankment) == 7 FT

NEW EMBANKMENT:

NEW EMBANKMENT FILL UNIT WEIGHT ===== 120 PCF
 NEW EMBANKMENT FILL HEIGHT ===== 19 FT
 PROPOSED WIDTH AT TOP ===== 156 FT
 PROPOSED WIDTH AT BOTTOM ===== 250 FT (which is a 2.5:1 slope)

ASSUMPTIONS:

Soil Deposit is Normally Consolidated
 Cohesive Layers are Saturated
 Soils have a Low Sensitivity
 Liquid Limit (LL)=Moist. Content (MC%)
 Initial Void Ratio (Eo)=2.7*(MC%)/100
 Comp. Index (Cc)=0.009*(LL-10)
 Neglecting Granular & Secondary Settlement

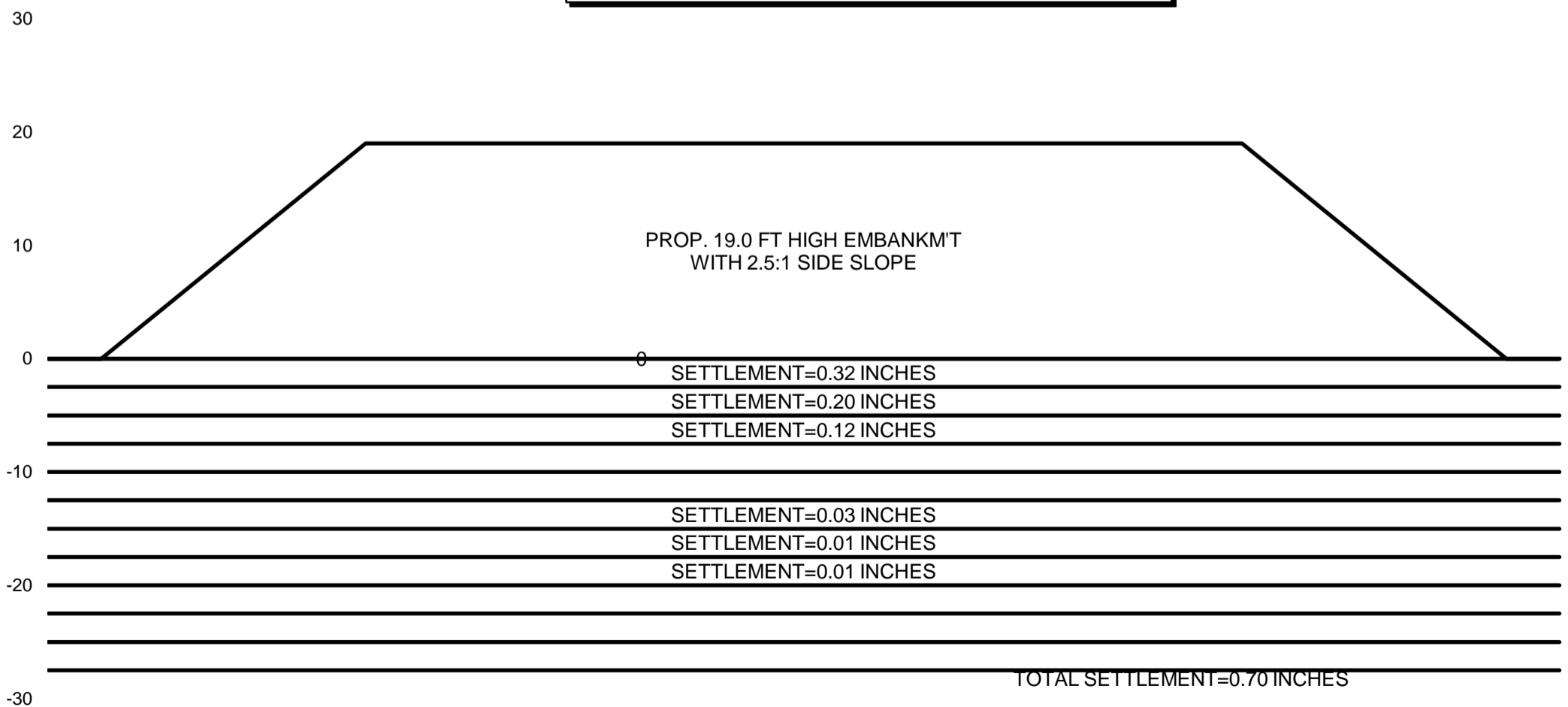
EXISTING EMBANKMENT (IF ANY):

EXISTING EMBANKMENT UNIT WEIGHT ===== 120 PCF
 EXISTING EMBANKMENT HEIGHT ===== 0 FT
 EXISTING WIDTH AT TOP ===== 0 FT
 EXISTING WIDTH AT BASE ===== 0 FT (which is a 0.0:1 slope)

LAYER THICK (FT)	TOTAL UNIT WT. (PCF)	UNCONF. COMP. STRENGTH (Qu) (TSF)	MOIST. CONTENT (%)	EXISTING PRESSURE (KSF)	PRESSURE INCREASE (KSF)	INITIAL VOID RATIO	COMPRESSION INDEX (Cc)	Qu CORRECTION FACTOR	LAYER SETTLEMENT (IN.)
2.5	120	2.00	25	0.150	2.256	0.675	0.135	0.111	0.32
2.5	120	2.50	27	0.450	2.209	0.729	0.153	0.100	0.20
2.5	120	2.00	21	0.750	2.162	0.567	0.099	0.111	0.12
2.5	120	3.50	5	0.941	2.115	0.135	0.000	0.100	0.00
2.5	120	3.50	9	1.085	2.070	0.243	0.000	0.100	0.00
2.5	120	4.50	13	1.229	2.027	0.351	0.027	0.100	0.03
2.5	120	3.50	11	1.373	1.985	0.297	0.009	0.100	0.01
2.5	120	4.20	12	1.517	1.944	0.324	0.018	0.100	0.01
2.5	120	4.00	10	1.661	1.905	0.270	0.000	0.100	0.00
2.5	120	4.00	10	1.805	1.868	0.270	0.000	0.100	0.00
2.5	120	5.00	7	1.949	1.833	0.189	0.000	0.100	0.00

TOTAL SETTLEMENT UNDER CENTER OF BRIDGE CONE = 0.70 IN.

EMBANKMENT AND SOIL PROFILE



COHESIVE SOIL SETTLEMENT ESTIMATE

LOCATION AND BORING USED ===== West End/Boring #4 and 2 WITHOUT CULVERT

TYPE OF SURCHARGE ===== 1 (1=2:1 bridge cone, 2=continuous embank., 3=rectangular surch.)

DEPTH TO WATER TABLE (below top of existing embankment) == 7 FT

NEW EMBANKMENT:

NEW EMBANKMENT FILL UNIT WEIGHT ===== 120 PCF
 NEW EMBANKMENT FILL HEIGHT ===== 9 FT
 PROPOSED WIDTH AT TOP ===== 156 FT
 PROPOSED WIDTH AT BOTTOM ===== 250 FT (which is a 5.2:1 slope)

ASSUMPTIONS:

Soil Deposit is Normally Consolidated
 Cohesive Layers are Saturated
 Soils have a Low Sensitivity
 Liquid Limit (LL)=Moist. Content (MC%)
 Initial Void Ratio (Eo)=2.7*(MC%)/100
 Comp. Index (Cc)=0.009*(LL-10)
 Neglecting Granular & Secondary Settlement

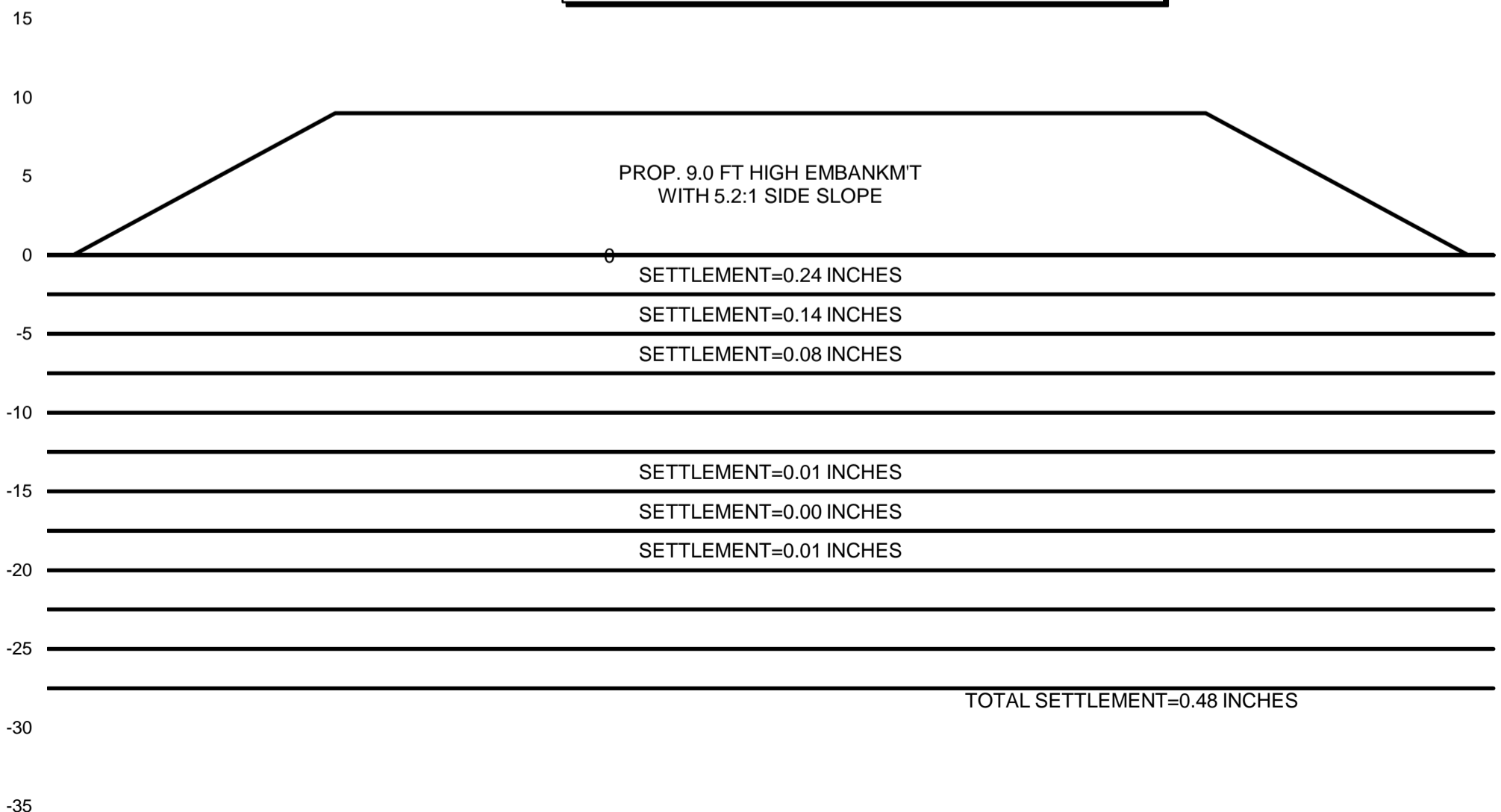
EXISTING EMBANKMENT (IF ANY):

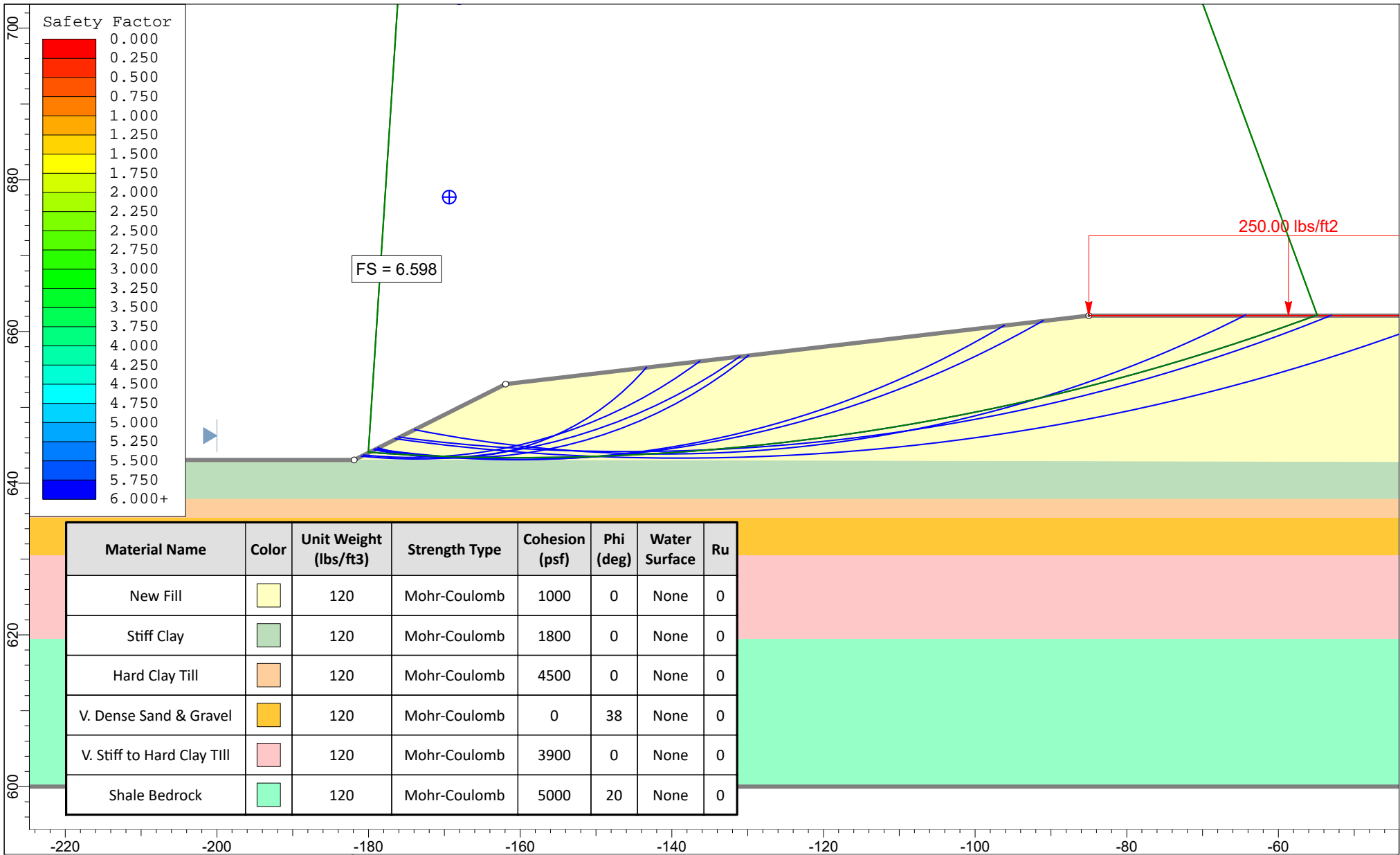
EXISTING EMBANKMENT UNIT WEIGHT ===== 120 PCF
 EXISTING EMBANKMENT HEIGHT ===== 0 FT
 EXISTING WIDTH AT TOP ===== 0 FT
 EXISTING WIDTH AT BASE ===== 0 FT (which is a 0.0:1 slope)

LAYER THICK (FT)	TOTAL UNIT WT. (PCF)	UNCONF. COMP. STRENGTH (Qu) (TSF)	MOIST. CONTENT (%)	EXISTING PRESSURE (KSF)	PRESSURE INCREASE (KSF)	INITIAL VOID RATIO	COMPRESSION INDEX (Cc)	Qu CORRECTION FACTOR	LAYER SETTLEMENT (IN.)
2.5	120	2.00	25	0.150	1.056	0.675	0.135	0.111	0.24
2.5	120	2.50	27	0.450	1.009	0.729	0.153	0.100	0.14
2.5	120	2.00	21	0.750	0.965	0.567	0.099	0.111	0.08
2.5	120	3.50	5	0.941	0.924	0.135	0.000	0.100	0.00
2.5	120	3.50	9	1.085	0.888	0.243	0.000	0.100	0.00
2.5	120	4.50	13	1.229	0.855	0.351	0.027	0.100	0.01
2.5	120	3.50	11	1.373	0.827	0.297	0.009	0.100	0.00
2.5	120	4.20	12	1.517	0.801	0.324	0.018	0.100	0.01
2.5	120	4.00	10	1.661	0.779	0.270	0.000	0.100	0.00
2.5	120	4.00	10	1.805	0.760	0.270	0.000	0.100	0.00
2.5	120	5.00	7	1.949	0.743	0.189	0.000	0.100	0.00

TOTAL SETTLEMENT UNDER CENTER OF BRIDGE CONE = 0.48 IN.

EMBANKMENT AND SOIL PROFILE





	<i>Project</i>		
	Slope Stability Analysis of SN053-2582		
	<i>Analysis Description</i>		
	Short Term (Undrained) Analysis - Bishop		
	<i>Drawn By</i>	Terry McCleary	<i>Scale</i>
<i>Date</i>	8/3/2017	<i>Company</i>	McCleary Engineering
		<i>File Name</i>	053-2582 Without Culvert.slim