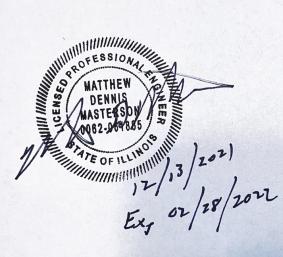
#### STRUCTURE GEOTECHNICAL REPORT

FAP RTE 312 Culvert – IL. Route 3 Over Stream

Existing S.N. 039-2013 Proposed S.N. 039-7126



FAP 312 SECTION 123B-5 JACKSON COUNTY, ILLINOIS JOB NO. D-99-036-17 PTB 184/034 CONTRACT NO. 78790 KEG NO. 17-1095.08

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May 5, 2021 REVISED December 13, 2021

Kaskaskia Engineering Group, LLC

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## TABLES

# Table 3.1 – Slope Stability Critical FOS. 3

## **EXHIBITS**

- Exhibit A Location Map
- Exhibit B Type, Size, and Location Plan (TS&L) Exhibit C Boring Logs Exhibit D Subsurface Profile

- Exhibit E Slope/W Slope Stability Analysis

#### Page

#### 1.0 **Project Description and Scope**

#### 1.1 Introduction

The geotechnical study summarized in this report was performed by Kaskaskia Engineering Group, LLC (KEG) for the replacement of a double barrel reinforced concrete box culvert for IL-3 over Stream in Jackson County, Illinois. The purpose of this report is to document subsurface geotechnical conditions, provide analyses of anticipated site conditions as they pertain to the project described herein, and to present design and construction recommendations for the proposed structure.

#### 1.2 **Project Description**

The project consists of the replacement of a double barrel reinforced concrete box culvert (existing SN 039-2013) located at IL 3 over a Stream in Jackson County, Illinois.

The general location of the proposed structure is shown on a Location Map, Exhibit A. The project is located approximately 0.8 miles northwest of Jones Ridge Road in Rockwood, Illinois. The site lies within the limits of the Third Principal Meridian (T. 8S R. 5W) within the Shawnee Hills Section of the Interior Low Plateaus Province.

#### 1.3 **Proposed Structure Information**

The proposed structure will consist of a cast-in-place (C.I.P.) double box culvert with apron supported wingwalls on each end of the culvert. The proposed structure will be built on a 30-degree skew and will provide a 24 ft.-wide driving width consisting of 12 ft. lanes and 4 ft. shoulders. The proposed culvert centerline station will be 530+10. The culvert will consist of a 6 ft. by 17 ft. single-barrel and will measure 87 ft. – 2-1/4 in. out-to-out of headwalls. A Type, Size, and Location Plan (TS&L) is included in Exhibit B. Class A5 stone riprap will be placed at both ends of the culvert.

Further substructure details will be based on the findings of this SGR.

#### 2.0 Field Exploration

#### 2.1 Subsurface Exploration and Testing

The site exploration plan was developed and completed by IDOT. Two standard penetration test (SPT) borings, designated 1-S and 2-S were drilled April 10, 2020. Detailed information regarding the nature and thickness of the soils encountered and the results of the field sampling and laboratory testing are shown on the Boring Logs, Exhibit C. The soil profile for the above mentioned borings can be found in Subsurface Profile, Exhibit D.

#### 2.2 Subsurface Conditions

The profiles at the two boring locations exhibited layers of silty clays and silts. The borings were terminated at 21 ft. below ground surface elevation (GSE). Boring 1-S has an estimated GSE of 372.9 ft. and 2-S has an estimated GSE of 373.0 ft. In general, the lithologic succession is as follows:

- a) Silty Clay The borings encountered approximately 3.5 ft. (1-S) to 6 ft. (2-S) of silty clay below the pavement at ground surface elevation (GSE). The driving resistances (N-values) ranged from 7 to 10 blows per foot (bpf), with unconfined compressive strength (Q<sub>u</sub>) values between 1.2 to 2.5 tons per square foot (tsf). The moisture contents varied from 17 to 26 percent.
- b) Silt Below the silty clay layer in both borings, a silt layer was encountered between 4.5 and 7 ft. below GSE, extending to the termination of the borings at 21 ft. below GSE. The N-values ranged from 0 bpf to 7 bpf, with Q<sub>u</sub> values between 0.2 tsf and 1.1 tsf, and moisture contents of 21 percent to 35 percent.

Groundwater was encountered in Boring 1-S and Boring 2-S at 17 ft. below GSE. Stream bed elevation was noted to be approximately El. 362.8. below GSE for 1-S and 2-S, respectively. It should be noted that the groundwater level is subject to seasonal and climatic variations, including the flow of the Tributary. In addition, without extended periods of observation, measurement of true groundwater levels may not be possible. Bedrock was not encountered in either boring.

#### 3.0 Geotechnical Evaluations

#### 3.1 Settlement

Due to the presence of soft soils in the vicinity of the proposed upstream (El. 361.8) and downstream (El. 361.7) inverts and the possibility of remaining materials from the existing structure, settlement calculations were necessary.

Based on our analysis, the proposed new culvert and wingwalls with up to 3.8 feet of new roadbed fill and pavement section could experience settlements of up to 11 inches if the culvert bears on the existing soils. Differential settlement between the main box and proposed end sections with horizontal cantilever wingwalls was estimated to be a maximum of 2 inches. KEG recommends the removal and disposal of unsuitable material is necessary for proper support of the new construction. KEG recommends overexcavation of the soils a minimum of 5 feet to El. 355.0. The horizontal limits of removal shall extend to 3 feet beyond the outer limits of the culvert and wingwall footprints. The overexcavation and replacement of the soils are necessary for proper support of the new construction.

#### 3.2 Slope Stability

A stability analysis using SLOPE/W was performed using the proposed roadway and culvert geometry on the TS&L and soil characteristics from Boring 1-S and 2-S. Two conditions were modeled for each scenario: end-of-construction and long-term stability. A critical factor of safety (FOS) was calculated for each condition. According to current standard of practice, the target FOS is 1.5 for end-of-construction and long-term slope stability. The slope stability analyses indicated that the required minimum FOS for all conditions were met.

In order to model the end-of-construction condition, full cohesion and a friction angle of 0 degrees were assumed. Nominal values for cohesion were used with full friction angle to model the long-term condition to analyze the theoretical condition where pore water pressure has dissipated. Nominal values were between 50 and 100 psf for the cohesive soils, and friction angles ranged from 26 to 28 degrees.

The Bishop Circular Method, which generates circular-shaped failure surfaces, was used to calculate the critical failure surfaces and FOS for the proposed conditions. The FOS obtained in the analysis is shown in Table 3.1. SLOPE/W program output from this analysis can be found in SLOPE/W Slope Stability Analysis, Exhibit E.

	Critical	FOS
Location (2H:1V Slope)		
	End-of Construction	Long Term
Northwest Culvert Wingwall	3.6	1.7
Southeast Culvert Wingwall	3.6	1.8

#### Table 3.1 – Slope Stability Critical FOS

#### 3.3 Scour

The approximate elevation at the upstream invert (TS&L, Exhibit B) is El. 361.8, and at the downstream invert is El. 361.7. Class A5 stone dumped riprap will be placed on both the upstream and downstream end of the double box culvert to reduce the potential for future scour.

#### 3.4 Seismic Considerations

As per IDOT Geotechnical Manual v. 2020, Section 7.4.5.4, seismic data is not required for buried structures, including box culverts.

#### 4.0 Foundation Evaluations and Design Recommendations

AASHTO Table 12.5.5-1 and Article 12.11 do not require box culverts to be designed for bearing capacity. Culverts weigh less than the soil around them and tend to "float" in the soil medium and are supported by the soil on the sides and below.

The soil encountered in the borings at the anticipated bearing elevation of the culvert consist of a very soft to medium-stiff silt material. The soil characteristics from Borings 1-S and 2-S at the assumed bearing elevation has a Qu value of 0.4 tsf. The total applied bearing pressure from the culvert box, including the proposed 3.8 feet of roadbed fill and pavement is estimated to be 905 psf. The applied bearing pressure from the end sections with wingwalls and roadbed fill is estimated to be 681 psf for the north and south end sections. Based on these estimates, the service bearing pressures will be satisfied, however, settlement of 9 to 11 inches is estimated.

Horizontal cantilever wingwalls may provide overall lower applied pressures than other walls, and may reduce any differential settlement resulting from the walls bearing on some previously unloaded material. While this analysis shows the proposed Horizontal cantilever wingwalls to be feasible, other wingwall types may be considered, such as apron supported walls.

If after final design the bearing elevation changes, KEG should be informed to review that the above information is still accurate.

#### 4.1 Box Culvert

Varying depths of existing stream bed will require excavation and removal to reach the proposed bottom elevation of the box culvert (El. 360+/-). Typically, excavations to these depths will result in suitable bearing soils for construction. As indicated above, KEG recommends the removal and disposal of unsuitable material a minimum of 5 feet below proposed bearing elevation of the culvert to El. 355.0 for proper support of the new construction. In addition, care must be taken during excavation to prevent disturbing the final bearing surface soils. If the foundation soils are disturbed or soft pockets of material are encountered during construction, they must also be removed and replaced.

#### 5.0 Construction Considerations

#### 5.1 Construction Activities

Construction activities should be performed in accordance with the current IDOT Standard Specifications for Road and Bridge Construction and any pertinent Special Provisions or Policies.

Should any design considerations assumed by KEG change, KEG should be contacted to determine if the recommendations stated in this report still apply.

#### 5.2 Temporary Shoring and Soil Retention

Temporary shoring may be required at various stages of this project due to the proposed stagedconstruction layout shown in the TS&L.

Temporary Soil Retention Systems may be required versus Temporary Shoring, depending upon the surcharge loading and retained heights required to be supported during construction. An Illinois-licensed Structural Engineer is required to seal the design of Temporary Soil Retention Systems, if deemed necessary.

#### 5.3 Site and Soil Conditions

Provisions of the Standard Specifications should adequately address site and soil conditions.

#### 6.0 Computations

Computations and analyses for special circumstances, if any, are included as exhibits. Please refer to each section of the report for reference to the exhibit containing any such calculations or analysis used.

#### 7.0 Geotechnical Data

Soil boring logs can be found in Exhibit C. The Subsurface Profile can be found in Exhibit D.

#### 8.0 Limitations

The recommendations provided herein are for the exclusive use of Veenstra & Kimm, Inc and the Illinois Department of Transportation (IDOT). They are specific only to the project described and are based on the subsurface information obtained by IDOT at two boring locations within the

structure area in 2013, KEG's understanding of the project as described herein, and geotechnical engineering practice consistent with the standard of care. No other warranty is expressed or implied. KEG should be contacted if conditions encountered during construction are not consistent with those described.

EXHIBIT A

LOCATION MAP





LOCATION MAP IL 3 (FAP 312) over Stream Section 123B-5 Existing SN 039-2013 Proposed SN 039-7126 Jackson County, Illinois

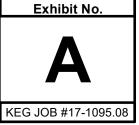
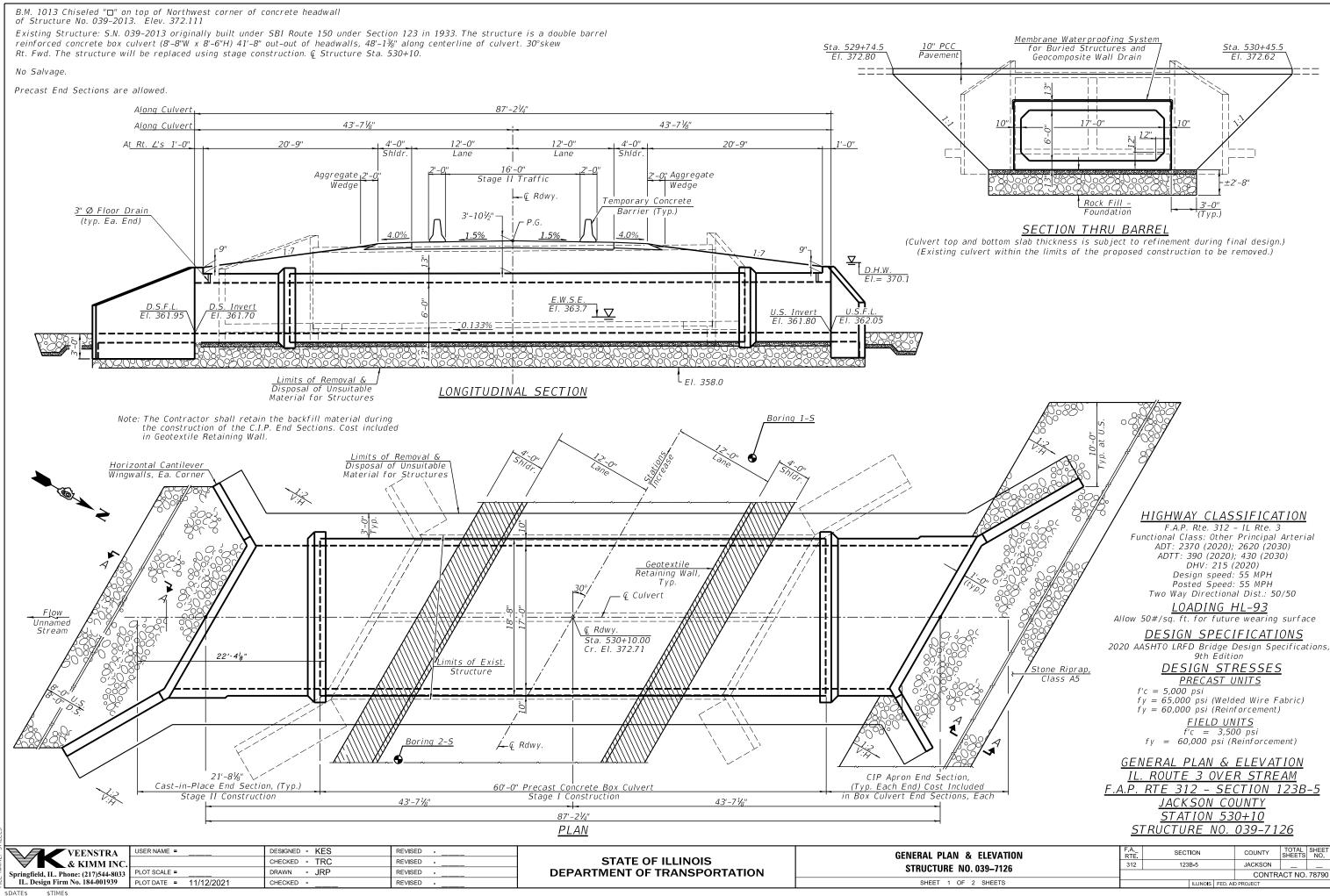
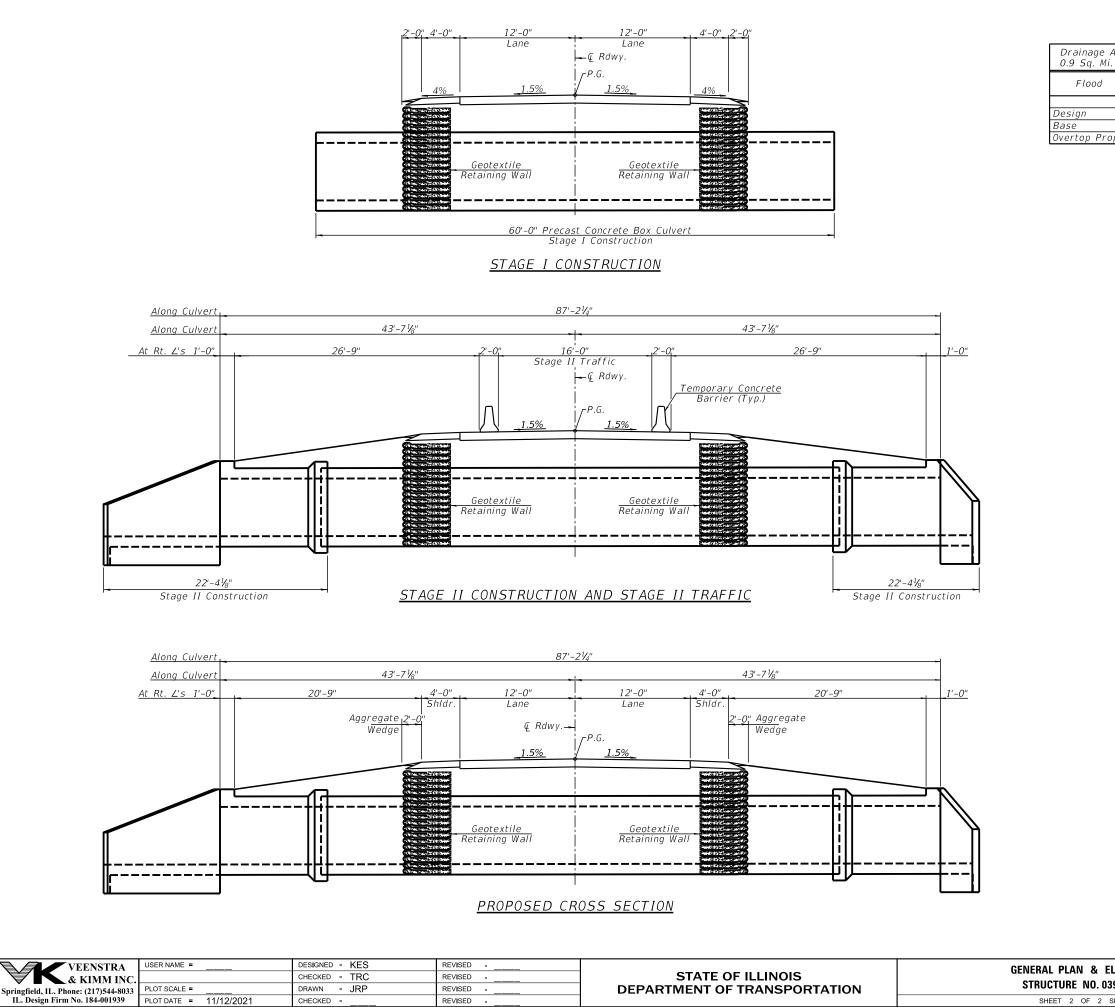


EXHIBIT B

TYPE, SIZE, AND LOCATION PLAN (TS&L)

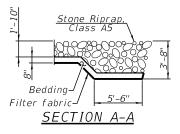


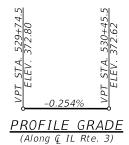


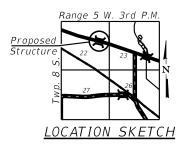
		WAL	ERWA	<u>INFC</u>	IRMAI	TON					
je Are	a =	Exist. Overtopping Elev. = 372.15 @ Sta. 531+25									
Mi.			Prop	Overtop	oping El	lev. = 3	872.15 (	@ Sta. 5	31+25		
d	Freq.	Q	Opening	I Sq. Ft.	Nat.	Head	– Ft.	Headwa	ater El.		
u	Yr.	C.F.S.	Exist.	Prop.	H.W.E.	Exist.	Prop.	Exist.	Prop.		
	10	730	125	98	369.6	2.1	1.9	371.7	371.5		
	50	1,260	134	98	370.1	2.4	2.4	372.5	372.5		
	100	1,520	138	98	370.3	2.2	2.2	372.5	372.5		
Prop.	50	1260	134	98	370.1	2.4	2.4	372.5	372.5		
10 Yr. Outlet Velocity through Exist. Structure = 5.8 ft/s											

WATERWAY INFORMATION

10 Yr. Outlet Velocity through Prop. Structure = 7.4 ft/s







<u>GENERAL PLAN &amp; ELEVATION</u>
IL. ROUTE 3 OVER STREAM
F.A.P. RTE 312 - SECTION 123B-5
JACKSON COUNTY
<u>STATION 530+10</u>
<u>STRUCTURE NO. 039-7126</u>

e ELEVATION . 039–7126		SECT	SECTION		COUNTY	TOTAL SHEETS	SHEET NO.
		312 123B-5		JACKSON	_	_	
					CONTR/	ACT NO.	78790
2 SHEETS	ILLINOIS FED. AID PROJECT						

EXHIBIT C

**BORING LOGS** 

of Transpo	partr ortati	ne on	nt		SC	DIL BORING LOG		raye	<u> </u>	01
Division of Highways District 9								Date	4/1	0/20
ROUTE IL 3 DESC	RIPTION	۱			Box C	ulvert over stream LOGGE	D BY	<u> </u>	.ee Es	stel
<b>SECTION</b> 123B-5	LO	CATI	ON _	<u>1.8 mi</u>	. E of	Randolph County line, <b>SEC.</b> 22, <b>TWP.</b> 8S, <b>R</b>	NG. 5	5W, 3	PM	
COUNTY Jackson D	RILLING	6 ME	THOD	Hollow	stem	auger (8" O.D., 3.25" I.D.)HAMMER TYPE	A	uto SF	PT 140	) lb
STRUCT. NO.         039-2013           Station         530+10		D E P T	B L O W	U C S	M O I S	Surface Water Elev.   ft     Stream Bed Elev.   362.8     ft	D E P T	B L O W	U C S	M O I S
BORING NO.         1-S           Station         530+37           Offset         9.0ft RT		H	S	Qu	T	Groundwater Elev.: ⊈First Encounter355.9_ ft	H	S	Qu	T
Offset 9.0ft RT Ground Surface Elev. 372.9	ft	(ft)		(tsf)	(%)	v Upon Completion ft ▼After Hrs ft	(ft)		(tsf)	(%)
Cored Pavement, 2.5" HMA over						V. Soft Brown, Moist SILT		WOH	0.2	29
9.5" PCC Stiff Brown, Moist SILTY CLAY	371.90		-			(continued) 351.90		WOH	В	
			2 5	1.8	17	-	_			
			5	В						
	368.40		-							
M. Stiff Brown, Moist SILT		-5	1	0.9	21	-	-25			
			4	B		_				
			-				_			
			1	0.0	0.1	_				
			2 4	0.8 B	21					
			-							
Soft Brown, Moist SILT	363.40	-10	wон				-30			
			2	0.4 B	21	Bottom of hole @ 21.0 ft	_			
			-			Elevation referenced to BM 1013, Cut Square on NW Corner HDWL				
M. Stiff Brown, Moist SILT	360.90		wон			of 039-2013; EL. 372.11				
			WOH WOH		28	To convert "N" values to "N60", multiply by 1.5				
			10011							
			wон				25			
		-10	WOH	0.5	28		35			
			WOH	В		-				
Σ			พกม							
			WOH WOH		26	-				
			WOH	В		-	_			
	353.40									
V. Soft Brown, Moist SILT		_20	WOH				_10			

-- - -

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer, E-Estimated) Abbreviations W.O.H - Sampler Advanced By Weight of Hammer, W.O.P - Advanced by Weight of Pipe, B.S. - Before Seating The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206) BBS, from 137 (Rev. 8-99)

Page 1 of 1

of Transpo	ortatio	ient on		SC	<b>DIL BORING LO</b>	G	i age	<u> </u>	ы. -
Division of Highways District 9							Date	4/1	0/20
ROUTE IL 3 DESC	RIPTION			Box C	ulvert over stream	LOGGED	BY	Lee Es	stel
<b>SECTION</b> 123B-5	LOC	ATION _	<u>1.8 mi</u>	. E of I	Randolph County line, SEC. 22, TW	P. 8S, RNG	. 5W, 3	PM	
COUNTY Jackson D		METHOD	H <u>ollow</u>	<u>stem</u>	auger (8" O.D., 3.25" I.D.) <b>HAMMER</b>		Auto S	PT 140	) lb
STRUCT. NO.         039-2013           Station         530+10		D B E L P O	U C S	M O I	Surface Water Elev Stream Bed Elev362.8	ft   ⊑   P	L	U C S	M O I
BORING NO.         2-S           Station         529+85		T W H S	Qu	S T	Groundwater Elev.: ⊈First Encounter356.0	ft H		Qu	S T
Offset 9.5ft LT Ground Surface Elev. 373.0	ff	(ft)	(tsf)	(%)	v Upon Completion     v After Hrs	ft	:)	(tsf)	(%)
Cored Pavement, 2.5" HMA over 9.5" PCC	372.00	_			M. Stiff Brown, Moist SILT (continued)		, 1 2	0.5 P	35
V. Stiff Brown, Moist SILTY CLAY		_				-	_		
	_	1	2.5	26					
	_	4	2.5 B	20					
	_						_		
(Stiff)	_		1.2	20	-		25		
	_	4	B	20		-			
	366.00	_				-			
Stiff Brown, Moist SILT		1	1.1	21	_	-	_		
	_	4	В		_		_		
	363.50								
M. Stiff Brown, Moist SILT	_	- <u>10</u> 1 2	0.5	23	Bottom of hole @ 21.0 ft		30		
	_	2	В		Elevation referenced to BM 1013,		$\neg$		
	_				Cut Square on NW Corner HDWL of 039-2013; EL. 372.11	 	_		
	_	2	0.8	29	To convert "N" values to "N60",	-			
		2	В		multiply by 1.5	-	_		
V. Soft Brown, Moist SILT	358.50	WOH							
	_	WOH	0.2	28	-	<u></u>	35		
	-	WOH	P		-		-		
∑	_								
	_	WOH	0.2	28		-			
	_	WOH	P		-	-			
M. Stiff Brown, Moist SILT	353.50	WOH				-4	10		

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer, E-Estimated) Abbreviations W.O.H - Sampler Advanced By Weight of Hammer, W.O.P - Advanced by Weight of Pipe, B.S. - Before Seating The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206) BBS, from 137 (Rev. 8-99)

(ক্স)	Illinois Department
	of Transportation

EXHBIT D

### SUBSURFACE PROFILE

			2.8
	374	1-S 530+37 9.0 ft RT N Qu w% 372.9 Cored Pavement: 2.5" HMA over 9.5" PCC	529+85 9.5 ft LT N Qu w%373.0 Cored Pavement: 2.5" HMA over 9.5" of PCC
	372	10 1.8 17 B	7 2.5 26 B
	370	SILTY CLAY: Brown, stiff, moist	B. SILTY CLAY: Brown, very stiff, moist
	368	7 0.9 21 B	7 1.2 20 B
	366	6 0.8 21 B	7 1.1 21 B
on ( ft)	364	3 0,4 21 B	4 0.5 23 B
	360	0 0.7 28 SILT: Brown, medium stiff, moist	4 0.8 29 B
	358	0.05.29	SILT: Brown, moist, stiff
	356	0 0.5 28 B	0'0.2'29' P
	354	0 0.7 26 B	0 0.2 28 P
	352	0 0.2 29 B	3 0.5 35 P
		LTTT 351.9	
	350		



## NOT TO HORIZONTAL SCALE

Route: F.A.P. RTE 312 Section: 123B-5 County: Jackson County, IL

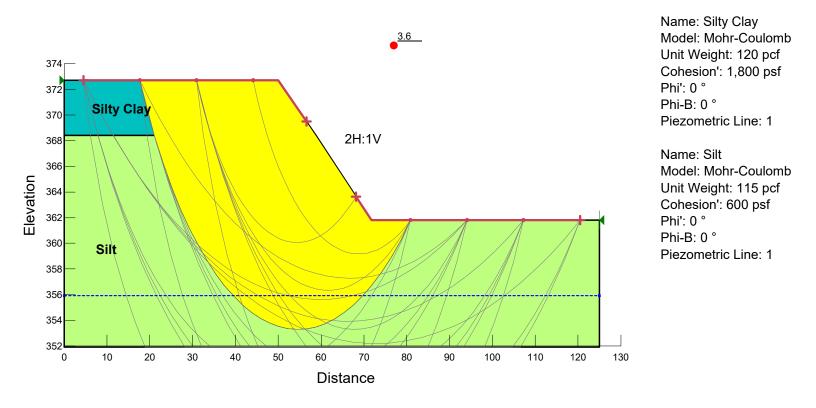
 	374
 	372
 	370
 	368
 	366
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	358
 	356
 	354
	352
	<b>JJZ</b>
 	350

# SUBSURFACE DATA PROFILE

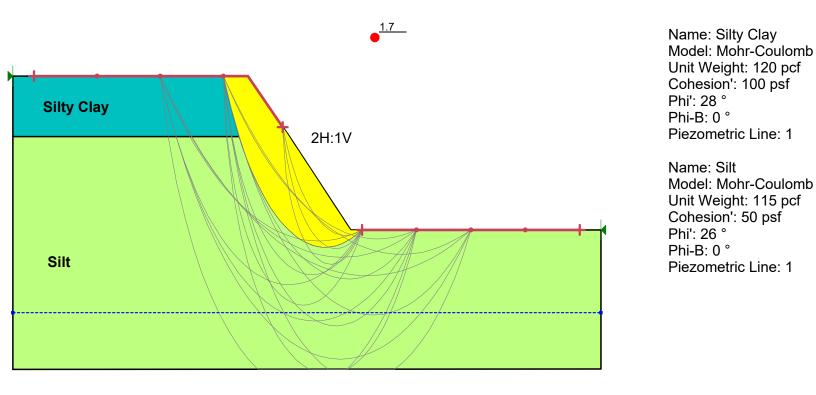
EXHIBIT E

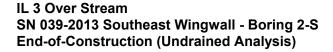
SLOPE/W SLOPE STABILITY ANALYSIS

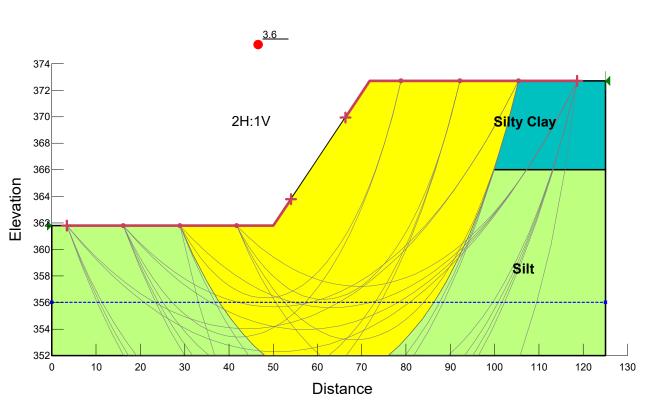
IL 3 Over Stream SN 039-2013 Northwest Wingwall - Boring 1-S End-of-Construction (Undrained Analysis)



IL 3 Over Stream SN 039-2013 Northwest Wingwall - Boring 1-S Long Term (Drained Analysis)



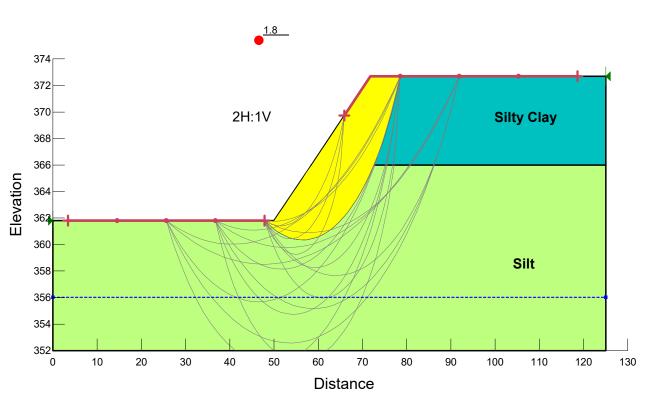




Name: Silty Clay Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion': 1,850 psf Phi': 0 ° Phi-B: 0 ° Piezometric Line: 1

Name: Silt Model: Mohr-Coulomb Unit Weight: 115 pcf Cohesion': 550 psf Phi': 0 ° Phi-B: 0 ° Piezometric Line: 1





Name: Silty Clay Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion': 100 psf Phi': 28 ° Phi-B: 0 ° Piezometric Line: 1

Name: Silt Model: Mohr-Coulomb Unit Weight: 115 pcf Cohesion': 50 psf Phi': 26 ° Phi-B: 0 ° Piezometric Line: 1