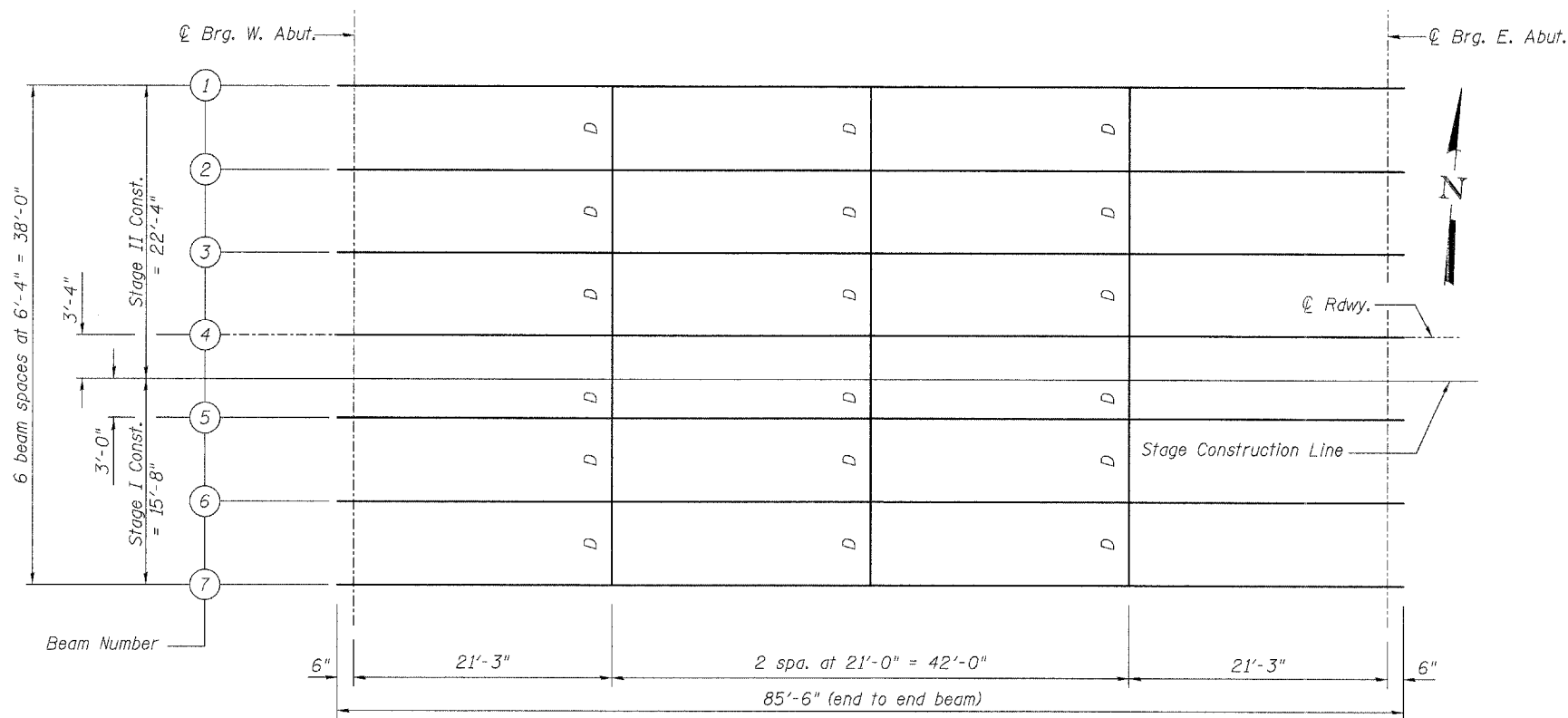


Contract # 98775



**FRAMING PLAN**

		0.5 Span
$I_s$	(in <sup>4</sup> )	9750
$I_c(n)$	(in <sup>4</sup> )	24016
$I_c(3n)$	(in <sup>4</sup> )	17392
$S_s$	(in <sup>3</sup> )	542
$S_c(n)$	(in <sup>3</sup> )	773
$S_c(3n)$	(in <sup>3</sup> )	694
DC1	(k/')	0.798
M <sub>DC1</sub>	(k)	713
DC2	(k/')	0.129
M <sub>DC2</sub>	(k)	115
DW	(k/')	0.289
M <sub>DW</sub>	(k)	258
$M_L + Imp$	(k)	1224
$M_u$ (Strength I)	(k)	3564
$\phi_r M_n$	(k)	3851
$f_s$ DC1	(ksi)	15.79
$f_s$ DC2	(ksi)	1.99
$f_s$ DW	(ksi)	4.46
$f_s$ 1.3(I+I)	(ksi)	24.70
$f_s$ (Service II)	(ksi)	46.94
$f_s$ (Total)(Strength I)	(ksi)	62.16
$V_f$	(k)	28.2

$I_s, S_s$ : Non-composite moment of inertia and section modulus of the steel section used for computing  $f_s$  (Total-Strength I, and Service II) due to non-composite dead loads (in<sup>4</sup> and in<sup>3</sup>).

$I_c(n), S_c(n)$ : Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing  $f_s$  (Total-Strength I, and Service II) due to short-term composite live loads (in<sup>4</sup> and in<sup>3</sup>).

$I_c(3n), S_c(3n)$ : Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing  $f_s$  (Total-Strength I, and Service II) due to long-term composite (superimposed) dead loads (in<sup>4</sup> and in<sup>3</sup>).

DC1: Un-factored non-composite dead load (kips/ft.).

M<sub>DC1</sub>: Un-factored moment due to non-composite dead load (kip-ft.).

DC2: Un-factored long-term composite (superimposed excluding future wearing surface) dead load (kips/ft.).

M<sub>DC2</sub>: Un-factored moment due to long-term composite (superimposed excluding future wearing surface) dead load (kip-ft.).

DW: Un-factored long-term composite (superimposed future wearing surface only) dead load (kips/ft.).

M<sub>DW</sub>: Un-factored moment due to long-term composite (superimposed future wearing surface only) dead load (kip-ft.).

$M_L + Imp$ : Un-factored live load moment plus dynamic load allowance (Impact) (kip-ft.).

$M_u$  (Strength I): Factored design moment (kip-ft.).

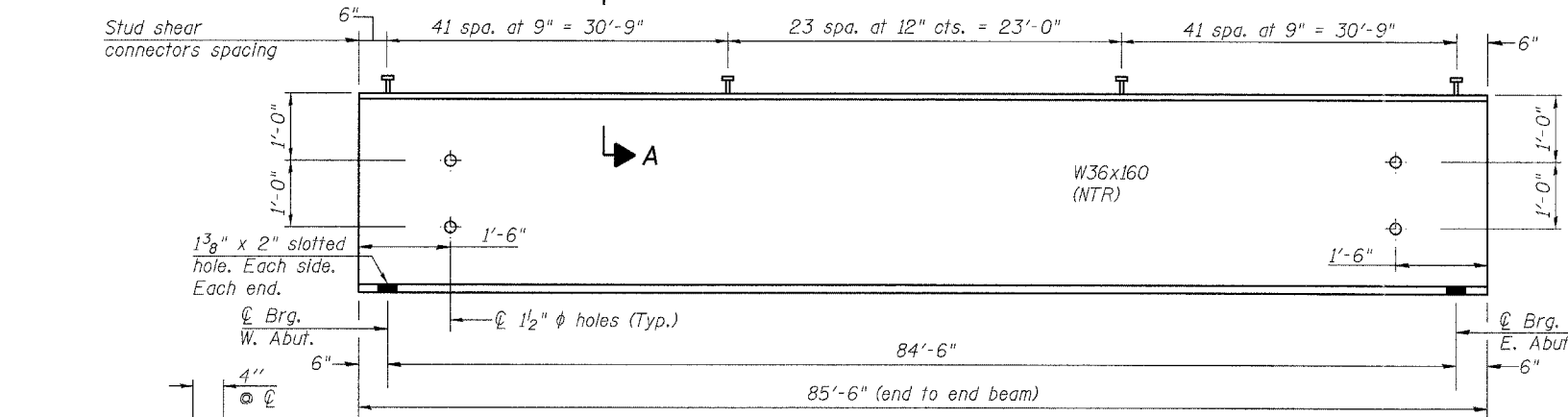
$\phi_r M_n$ : Compact composite positive moment capacity computed according to Article 6.10.7.1 (kip-ft.).

$f_s$  (Service II): Sum of stresses as computed from the moments below (ksi).

$f_s$  (Total)(Strength I): Sum of stresses as computed from the moments below on non-compact section (ksi).

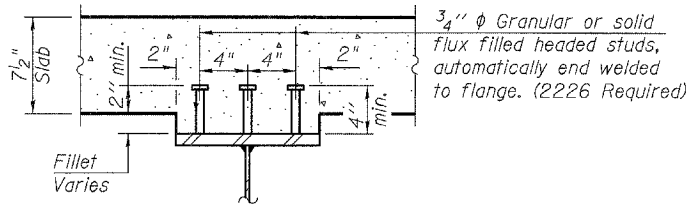
$V_f$ : Factored shear range computed according to Article 6.10.10.

	Abut.
R <sub>DC1</sub>	(k) 33.7
R <sub>DC2</sub>	(k) 5.5
R <sub>DW</sub>	(k) 12.2
R <sub>L + imp</sub>	(k) 78.0
R <sub>Total</sub>	(k) 129.4

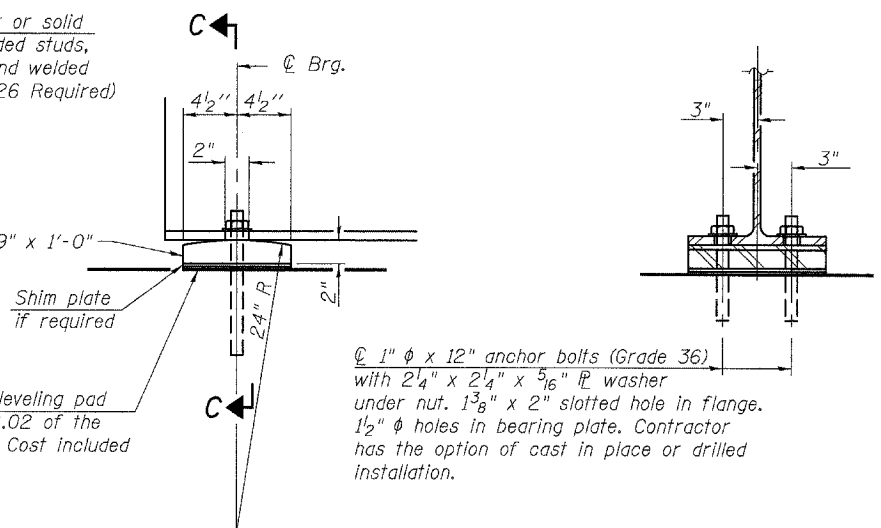


**BEAM ELEVATION**

"NTR" denotes members to which notch toughness requirements are applicable.



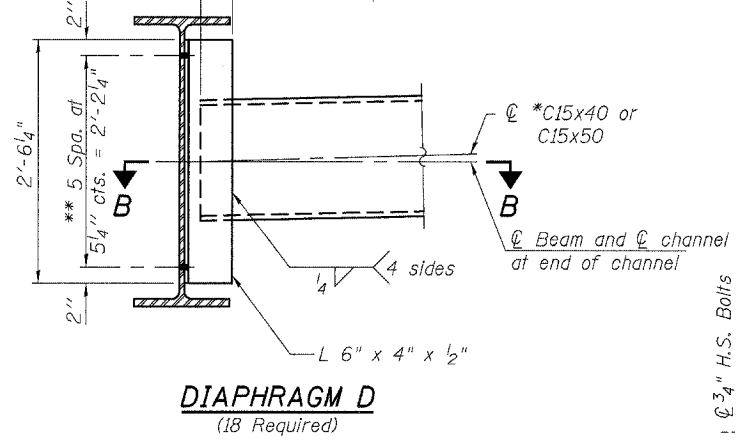
**SECTION A-A**



**ELEVATION AT ABUTMENT**

**SECTION C-C**

**FIXED BEARING**



**DIAPHRAGM D**  
(18 Required)

Note:  
Two hardened washers required for each set of oversized holes and 5/16 inch plate washer over slotted holes.

\* Alternate channels are permitted to facilitate material acquisition. Calculated weight of structural steel is based on the lighter section.  
\*\* 3/4 inch diameter HS bolts, 1 1/2 inch diameter holes. For diaphragms at stage construction provide 1 3/8 inch x 1 7/8 inch vertical slotted holes at south side of beam 4 in angle and beam and for north side of beam 5 provide oversized holes in angle and beam. Bolts in slotted holes shall be finger tightened prior to the deck slab pouring and then fully tightened after completion of the pour.

**NOTES:**

- All beams shall be W36x160 AASHTO M270 Grade 50 (NTR). All diaphragms and connecting angles shall be AASHTO M270 Grade 36.
- All diaphragms shall be installed as steel is erected and secured with erection pins and bolts except as otherwise noted.
- Load carrying components designated "NTR" shall conform to the Supplemental Requirements for Notch Toughness, Zone 2.
- Anchor bolts shall be ASTM F1554 all-thread (or an Engineer-approved alternate material) of the grade(s) and diameter(s) specified. ASTM A307 Grade C anchor bolts may be used in lieu of ASTM F1554 Grade 36 (Fy=36ksi). The corresponding specified grade of AASHTO M314 anchor bolts may be used in lieu of ASTM F1554.
- Drilled and set anchor bolts shall be installed according to Article 521.06 of the Standard Specifications.

**SECTION B-B**

**TOP OF BEAM ELEVATIONS**

(For Fabrication Only)

Location	Beam 1	Beam 2	Beam 3	Beam 4	Beam 5	Beam 6	Beam 7
© Brg. W. Abut.	395.11	395.23	395.35	395.48	395.60	395.72	395.84
© Brg. E. Abut.	395.62	395.72	395.81	395.91	396.00	396.10	396.19

**Lin Engineering, L.T.D.**  
Consulting Engineers  
Chatham, Illinois

Designed By: JDF    Checked By: MTH    Drawn By: AUF  
Date: 12/06    File: 028-0076.DGN

REVISIONS	
NAME	DATE

ILLINOIS DEPARTMENT OF TRANSPORTATION  
**FRAMING PLAN & STEEL DETAILS**  
ILLINOIS ROUTE 14 OVER  
ANDY CREEK  
F.A.P. ROUTE 869 - SECTION 104B-2  
FRANKLIN COUNTY  
STATION 603+80.00  
STRUCTURE NO. 028-0076