STRUCTURE GEOTECHNICAL REPORT CIRCLE INTERCHANGE RECONSTRUCTION RETAINING WALL 10 (PROPOSED SN 016-1729) F.A.I. ROUTE SB 90/94 (DAN RYAN EXPRESSWAY) STATION 7309+74.27 TO STATION 7316+31.15 SECTION 2015-022-I, IDOT D-91-227-13/PTB 163-001 COOK COUNTY, ILLINOIS

> For AECOM 303 East Wacker Drive Chicago, IL 60601 (312) 938-0300

Submitted by Wang Engineering, Inc. 1145 North Main Street Lombard, IL 60148 (630) 953-9928

> Original: December 22, 2016 Revised: May 19, 2017

#### **Technical Report Documentation Page**

1. Title and Subtitle		2. Report Date				
Structure Geotechnical R		Revised: May 19, 2017				
Circle Interchange Recon		3. Report Type SGR RGR				
Retaining Wall 10, F.A.I.	Route SB 90/94 (Dan Ryan expressway)	$\Box$ Draft $\Box$ Final $\boxtimes$ Revised				
Station 7309+74.27 to Sta	ation 7316+31.15					
4. Route / Section / County		5. IDOT Job No./Contract				
F.A.I. 90/94/ 2015-022-I	F.A.I. 90/94/ 2015-022-I / Cook					
6. PTB / Item No.	7. Existing Structure Number(s)	8. Proposed Structure Number(s)				
163/001	<b>e</b>					
9. Prepared by	Contributor(s)	Author Phone Number/Email Address (630) 953-9928 Ext 1018				
Wang Engineering, Inc.	Wang Engineering, Inc. Author: Metin W. Seyhun, P.E.					
1145 N Main Street	mseyhun@wangeng.com					
Lombard, IL 60148	PIC: Corina T. Farez, P.E., P.G.					
10. Prepared for	Structural Engineer	Contact Phone Number				
AECOM	Amish T. Bhatt, S.E., P.E.	(312) 373-6829				
303 East Wacker Drive	AECOM					
Chicago, IL 60601						
11. Abstract						
A 654.75-foot long. 2	22.5 feet maximum exposed/retained her	ight new retaining wall will be				
	from Station 7309+74.27 to Station 7316					
	Street Exit to SB I-90/94 (Dan Ryan Ex					
	ndations for the design and construction o					
geoteeninearrecomme	neations for the design and construction of	The proposed retaining wars.				
Based on our subsurfa	ce investigation results, the soils consists	s of up to 15 feet of fill up to 9				
	ery stiff clay crust, up to 38 feet of very s					
	to hard silty clay to silty clay loam, and					
	boring termination depths or bedrock. Be					
	s of 491.5 to 492.4 feet.) Water-bearing la					
deeper levels within th	e granular materials and weathered dolost	one.				

The proposed wall is a cut wall. Our wall type evaluations show the most technically feasible type of wall is drilled shaft with lagging. Other non-gravity walls such as soldier pile and lagging type or tangent wall may also be used. The drilled shaft with lagging wall was considered for a length of 570 feet between Stations 7309+74.27 and 7315+46.05. For southern portion, MSE wall was considered for a length of 84.75 feet between Stations7315+46.05 and 7316+31.15 due to the existing T-type foundations with piles and other utility constrains. There will be a temporary retention system adjacent to the UIC building as well as a permanent soil retention system providing full lateral support for the excavation and MSE wall section.

The design soil parameters for drilled shaft with lagging wall and other walls are included in the report. Global stability analyses performed for the maximum height of this wall showed satisfactory factor of safety against slope failure with a critical shaft embedment elevation of 547.0 feet. For the MSE wall, we recommend the wall be designed based on a factored resistance of 2,000 psf using resistance factor of 0.65. The MSE wall fill alternatives are included in the report.

#### 12. Path to archived file

Vetprojects\11000401\Reports\SGRs\Walls\1729 Wall 10\PDF\_Report May 19, 2017\RPT\_Wang\_MWS\_11000401SGRFinalWall10V03\_20170519.doc



## TABLE OF CONTENTS

1.0	INTRODUCTION	1
1.1	1 PROJECT DESCRIPTION	1
1.2	2 PROPOSED STRUCTURE	2
1.3	3 EXISTING STRUCTURE	2
2.0	SITE CONDITIONS AND GEOLOGICAL SETTING	2
2.1	1 Physiography	
2.2	2 SURFICIAL COVER	
2.3	3 BEDROCK	4
3.0	EXISTING GEOTECHNICAL DATA	4
4.0	METHODS OF INVESTIGATION	
<b>4.</b> ]	1 SUBSURFACE INVESTIGATION	4
4.2		
4.3	3 LABORATORY TESTING	5
5.0	RESULTS OF FIELD AND LABORATORY INVESTIGATIONS	6
5.0 5.1		
	1 SOIL CONDITIONS	6
5.1	<ol> <li>SOIL CONDITIONS</li> <li>GROUNDWATER CONDITIONS</li> </ol>	
5.1 5.2	<ol> <li>SOIL CONDITIONS</li> <li>GROUNDWATER CONDITIONS</li> </ol>	
5.1 5.2 5.3	<ol> <li>SOIL CONDITIONS</li></ol>	
5.1 5.2 5.3 6.0	<ol> <li>SOIL CONDITIONS</li></ol>	
5.1 5.2 5.3 6.0 6.1	<ol> <li>SOIL CONDITIONS</li></ol>	
5.1 5.2 5.3 6.0 6.1 6.2	<ol> <li>SOIL CONDITIONS</li></ol>	



7.0	CONSTRUCTION CONSIDERATIONS
7.1	EXCAVATION AND DEWATERING
7.2	FILLING AND BACKFILLING
7.3	DRILLED SHAFT WITH LAGGING WALL
7.4	MSE WALL
7.5	DRILLED SHAFTS
7.6	CONSTRUCTION MONITORING17
8.0	QUALIFICATIONS
REF	ERENCES

#### **EXHIBITS**

- 1. Site Location Map
- 2. Site and Regional Geology
- 3. Boring Location Plan
- 4. Subsurface Soil Data Profile

#### APPENDIX A

Boring Logs, Rock Core Photographs, and Laboratory Test Results

#### **APPENDIX B**

Global Stability Analysis Results

#### APPENDIX C

Type Size Location Plan

#### APPENDIX D

Ground Movement Estimates



## STRUCTURE GEOTECHNICAL REPORT CIRCLE INTERCHANGE RECONSTRUCTION RETAINING WALL 10 (PROPOSED SN 016-1729) F.A.I. ROUTE SB 90/94 (DAN RYAN EXPRESSWAY) STATION 7309+74.27 TO STATION 7316+31.15 IDOT D-91-227-12/PTB 163-001 COOK COUNTY, ILLINOIS FOR AECOM

## **1.0 INTRODUCTION**

This report presents the results of Wang Engineering, Inc. (Wang) subsurface investigation, laboratory testing, and geotechnical engineering evaluations for the proposed wall SN 016-1729 (Retaining Wall 10) along EB I-290 Ramp to Taylor Street Exit to SB I-90/94 (Dan Ryan Expressway) in connection with the Circle Interchange Reconstruction program in the City of Chicago, Cook County, Illinois. A Site Location Map is presented as Exhibit 1.

The purpose of our investigation was to characterize the site soil and groundwater conditions, perform geotechnical engineering analyses, and provide recommendations for the design and construction of the new wall structure.

#### **1.1 Project Description**

The Circle Interchange is over 50 years old and has significant congestion and safety problems. The project is aiming to improve safety and mobility as well as upgrade the mainline and interchange facilities. The project will also improve other modes of transportation such as transit, pedestrians and bicyclists within the same corridor.

The Circle Interchange Reconstruction project is along Interstate 90/94 (I-90/94) from south of Roosevelt Road to north of Lake Street, along Interstate 290 (I-290) from Loomis Street to the Circle Interchange; and along Congress Parkway from the Circle Interchange to Canal Street/Old Post Office. The routes typically have three lanes of traffic in each direction with mostly one lane ramp at interchanges. Locally, the north leg is known as the Kennedy Expressway, the south leg as the Dan Ryan



Expressway and the west leg as the Eisenhower Expressway. Within the project area, there are several cross street bridges over I-90/94 and I-290 considered for reconstruction. Along I-90/94, from south to north, the cross street overpasses include Taylor Street, Van Buren Street, Jackson Boulevard, and Adams Street. Along I-290, from west to east, the cross street overpasses include Morgan Street, Peoria Street, and Halsted Street.

The proposed improvements include additional through lanes in each direction on I-90/94. The horizontal alignment and vertical profiles throughout the interchange will be improved. A new two-lane flyover, Ramp NW (Flyover) will be constructed for I-90/94 northbound to I-290 westbound traffic. Cross street bridges, Morgan Street, Harrison Street, Halsted Street, Peoria Street, Taylor Street, Adams Street, Jackson Boulevard, and Van Buren Street will be reconstructed. Various existing ramps will be reconstructed and up to fifty new retaining walls will be constructed.

## 1.2 Proposed Structure

Based on latest TSL provided by AECOM, the new retaining wall (SN 016-1729) will be about 654.75foot long measured along wall's front face extending from Station 7309+74.27 to Station 7316+31.15. Wall 10 will run along I-290 Ramp to Taylor Street Exit and will have a maximum retained height of about 22.5 feet. The maximum wall height measured from the finished grade behind the wall to the bottom of concrete facing is 24.5 feet. There will be 570 feet of Drilled Shaft with Lagging wall and 84.75 feet of MSE wall. Noise Abutment wall 270 feet long mounted on top of the wall will also be provided. The cross sections show the existing ground surface on the back of the wall will be mostly flat. The wall is a cut wall type. The latest TSL is shown in the Type Size Location Plan (Appendix C).

## 1.3 Existing Structure

There is an existing concrete retaining wall with footings on piles that will overlap with the proposed MSE wall from Station 7315+61.16 to 7316+31.15. The footings and piles will remain but the stems will be removed to make space for the new MSE wall.

## 2.0 SITE CONDITIONS AND GEOLOGICAL SETTING

The site is located within the City of Chicago at the I-90/94 and I-290 Circle Interchange. On the USGS Chicago Loop 7.5 Minute Series map, the bridge is located in the SW<sup>1</sup>/<sub>4</sub> of Section 16, Tier 39 N, Range 14 E of the Third Principal Meridian.



The following review of published geologic data, with emphasis on factors that might influence the design and construction of the proposed engineering works, is meant to place the project area within a geological framework and confirm the dependability and consistency of the present subsurface investigation results. For the study of the regional geologic framework, Wang considered northeastern Illinois in general and Cook County in particular. Exhibit 2 illustrates the Site and Regional Geology.

## 2.1 Physiography

The site is situated within the northern section of the Chicago/Calumet lacustrine plain (Chrzatowsky and Thompson 1992). The area's flat, lakeward-sloping surface is a wave-scoured groundmoraine covered by thin and discontinuous lacustrine offshore silt and clay (Willman 1971).

The retaining wall along proposed F.A.I Route 90/94 (Dan Ryan expressway) south ramp from the Harrison Bridge is constructed within a 20- to 25-foot deep cut. Elevations along the proposed wall range from 597 feet at the south end to 600 feet at the north end.

#### 2.2 Surficial Cover

Within the project area, 100-foot thick or more, Wisconsinan-age glacial drift covers the bedrock (Leetaru et al. 2004). The glacial cover is made up of clay and silt of the Equality Formation of the Mason Group and diamictons of the Wadsworth and Lemont Formations of the Wedron Group (Hansel and Johnson 1996). The Equality Formation is made up of bedded silt and clay, locally laminated, with lenses and/or thin beds of sand and gravel. The Wadsworth Formation consists of relatively homogenous, massive, gray till with clay to silty clay matrix, with dolostone and shale clasts and occasional lenses of sorted and stratified silt. The Wadsworth Formation is underlain by the pebbly silty clay loam to silty loam diamicton of the Yorkville Member of the Lemont Formation, known informally as the Chicago "hardpan."

From a geotechnical viewpoint, the Equality Formation is characterized by low strength, medium to high plasticity, and medium to high moisture content, whereas the Wadsworth Formation is characterized by low plasticity, medium to low moisture content, medium to very stiff consistency, poor permeability, and low compressibility. The Yorkville Member hardpan is characterized by low plasticity, high blow counts, and low moisture content (Bauer et al. 1991; Peck and Reed 1954).



## 2.3 Bedrock

In the project area, the glacigenic deposits rest unconformably over a 350-foot thick Silurian-age dolostone. The top of bedrock may be encountered at elevations lower than 500 feet or 100 feet below ground surface (bgs). The Silurian dolostone dips gently eastward at a pace of 15 feet per mile. Only inactive faults are known in the area, and the seismic risk to the proposed structure from the existing faults is minimal (Leetaru et al. 2004; Willman 1971). There are no records of mining activity in the area, but deep tunnel excavations are known to exist.

Our subsurface investigation results fit into the local geologic context. The borings drilled in the project area revealed the native sediments consist of silty clay lacustrine deposits of the Equality Formation and silty clay diamicton of the Wadsworth Formation resting on top of more competent silty clay loam diamicton (hardpan) of the Lemont Formation. Bedrock was encountered by the borings at elevations ranging from 491.5 to 492.4 feet corresponding to 101 to 102 feet bgs.

## 3.0 EXISTING GEOTECHNICAL DATA

There is no existing geotechnical information along the proposed retaining wall.

## 4.0 METHODS OF INVESTIGATION

The following sections outline the methods of subsurface and laboratory investigations. All elevations in this report are based on NAVD 1988.

#### 4.1 Subsurface Investigation

Six structure borings were drilled by Wang between February 2, 2014 and April 03, 2014 along the proposed wall alignment. In addition we performed one vane shear, and a piezometer boring on December 1, 2015 and December 12, 2015 respectively, which were designated as 10-RWB-01 through 10-RWB-04, 15-RWB-01, 15-RWB-02, VST-01 and 10-PZ-01. Subsequently, two additional vane shear tests designated as 1729-VST-01 and 1729-VST-02 were undertaken on July 26 and 27, 2016.

The as-drilled boring locations were surveyed by Dynasty Group Inc. and station and offset information for each boring were provided by AECOM. The station and offset referenced the wall alignment. Boring location data are presented in the Boring Logs (Appendix A). The as-drilled boring locations are shown in the Boring Location Plan (Exhibit 3).



Truck-mounted or ATV drilling rigs equipped with hollow stem augers were used to advance and maintain open boreholes to 10 feet and mud rotary drilling technique was used below 10 to boring termination depths or to the bedrock. Soil sampling was performed according to AASHTO T 206, "Penetration Test and Split Barrel Sampling of Soils." The soil was sampled at 2.5-foot intervals to 30 feet below ground surface (bgs) and at 5-foot intervals to boring termination depths. Soil samples collected from each sampling interval were placed in sealed jars and transported to Wang Geotechnical Laboratory in Lombard, Illinois for further examination and laboratory testing.

Field boring logs, prepared and maintained by a Wang engineer or geologist, include lithological descriptions, visual-manual soil/rock classifications, results of Rimac and pocket penetrometer unconfined compressive strength tests, results of Standard Penetration Tests (SPT) recorded as blows per 6 inches of penetration. Vane Shear Test (VST) were also recorded on special forms. The SPT N value, shown on the soil profile, is the sum of the second and third blows per 6 inches. The soils were described and classified according to Illinois Division of Highways (IDH) Textural Classification system. The field logs were finalized by an experienced engineering geologist after verifying the field visual classifications and laboratory test results.

Groundwater observations were made during and at the end of drilling operations. Due to safety considerations, boreholes were grouted immediately upon completion.

#### 4.2 Vane Shear Tests

Wang performed vane shear tests in separate boreholes designated as Boring VST-01, 1729-VST-01 and 1729-VST-02 to determine in-situ shear strength of very soft to soft silty clay layer. This borehole was performed with partial soil sampling. After drilling to the desired depth, casing was installed and vane shear test was performed using a Rocktest Vane Borer. Tests were performed in undisturbed and remolded soil conditions. The sensitivity shown in the boring logs is the ratio of shear strength in undisturbed and remolded conditions. In general, the vane shear values for soft to medium stiff clays were significantly higher than the corresponding values from unconfined compressive strength tests using the RIMAC apparatus.

#### 4.3 Laboratory Testing

All soil samples were tested in the laboratory for moisture content (AASHTO T-265). Field visual descriptions of the soil samples were verified in the laboratory. Laboratory test results are shown in the



Boring Logs (Appendix A) and in the Soil Profile (Exhibit 4). Rock core photographs are shown in Appendix A.

The soil samples will be retained in our laboratory for 60 days following this report submittal. After that time, soil samples will be discarded unless a specific written request is received as to their disposition.

## 5.0 RESULTS OF FIELD AND LABORATORY INVESTIGATIONS

Detailed descriptions of the soil conditions encountered during our subsurface investigation are presented in the attached Boring Logs (Appendix A) and in the Soil Profile (Exhibit 4). Please note that strata contact lines represent approximate boundaries between soil types. The actual transition between soil types in the field may be gradual in horizontal and vertical directions.

## 5.1 Soil Conditions

Along the proposed wall, the borings encountered pavement and topsoil. The pavement structure consists of 6.0-inch thick asphalt over 2.5-foot thick gravelly loam base course. The top soil consists of 4.0 to 14.0 inch thick silty loam. In descending order, the general lithologic succession encountered beneath the pavement structure or topsoil includes 1) man-made ground (fill); 2) medium stiff to very stiff silty clay to clay loose to medium dense gravelly sand to sand ; 3) very soft to medium stiff clay to silty clay; 4) very stiff to hard silty clay to silty clay loam and silty loam diamicton; 5) hard silty clay loam or loose to very dense silty loam to silt and sand; and 6) strong dolostone bedrock.

## 1) Man-made ground (fill)

Underneath the pavement structure and topsoil, at elevations of 577.9 to 593.55 feet, the borings encountered 3.0 to 15.0 feet of cohesive and/or granular fill. The granular fill consists of very loose to dense, black, brown and reddish brown silty loam, loam, sandy loam, sand, and gravelly loam with SPT N-value of 3 to 49 blows/foot averaging 13 blows/foot and moisture content (MC) value of 4 to 57% averaging 16%. The cohesive fill consists of very stiff, brown and gray silty clay loam with unconfined compressive strength (Qu) values of 2.05 to 2.75 tsf with an average of 2.40 tsf and moisture content (MC) values of 14 and 17% averaging 16%.

## 2) Medium stiff to very stiff silty clay to clay and loose to medium dense gravelly sand to sand

Below the fill, a 4.3- to 9.2-foot thick layer of medium stiff to very stiff, brown and gray to gray silty clay, silty clay loam and clay was sampled in Borings 10-RWB-01 through 10-RWB-03, 15-RWB-01,



15-RWB-02, VST-01, 729-VST-01 and 1729-VST-02 starting at elevations of 575.1 to 586.8 feet. This layer has Qu values of 0.98 to 3.69 tsf averaging 2.0 tsf and MC values of 16 to 29% averaging 24%. Laboratory index testing performed on a sample from this layer shows liquid limit (LL) and plastic limit (PL) values of 37% and 19%, respectively. According to the AASHTO soil classification, the subgrade soils belong mainly to the A-6 group. The granular soils encountered in the borings VST-01, 15-RWB-02 and 10-RWB-04 having SPT N values of 5 to 16 averaging 10 blows/foot and MC content of 7 to 22% averaging 14%.

## 3) Very soft to medium stiff clay to silty clay

At elevations 540.6 to 580.5 feet, the borings encountered up to 40 feet of very soft to medium stiff, gray clay to silty clay with Qu values of 0.08 to 0.9 tsf and occasionally 1.0 tsf with an average of 0.36 tsf and MC values of 15 to 36% averaging 25%. Laboratory index testing performed on samples from this layer shows LL and PL values of 33 and 34%, 17 and 18%, respectively. According to the AASHTO soil classification, the subgrade soils belong mainly to the A-6 group. This layer is commonly known as the "Chicago Blue Clay."

## 4) Very stiff to hard silty clay to silty clay loam and silty loam diamiction

At elevations of 521.9 to 543.8 feet, the borings advanced through up to 20.0 feet of very stiff to hard, gray silty clay to silty clay loam and silty loam. It has Qu values of 3.28 to 8.12 tsf averaging 5.5 tsf and MC values of 12 to 21% averaging 16%. The medium dense to very dense , gray silty loam encountered in borings 10-RWB-02 and 15-RWB-02, has SPT N values of 21 to 53 blows/foot averaging 38 blows/foot and MC values of 19 to 50% averaging 26%. Laboratory index testing performed on a sample from this layer shows LL and PL values of 23% and 15%, respectively. According to the AASHTO soil classification, the subgrade soils belong mainly to the A-4 group.

## 5) Very stiff to hard silty clay loam or loose to very dense silty loam, gravelly silty loam and sand

At elevations of 492.1 to 541.7 feet, the borings advanced through very stiff to hard, gray silty clay loam or loose to very dense silty loam, gravelly silty loam, sand. The cohesive soils have Qu values of 3.61 to 10.25 tsf averaging 7.22 tsf and MC values of 13 to 15% averaging 14%. The granular soils encountered have SPT N values of 9 to 76 blows/foot, averaging 49 blows/foot and MC content of 9 to 24% averaging 16%. Laboratory index testing performed on samples from this layer shows LL and PL values of 0 to 26% and 0 to 16%, respectively. According to the AASHTO soil classification, the subgrade soils belong mainly to the A-4 group. This layer is commonly known as the "Chicago Hardpan."



#### 6) Strong dolostone bedrock

Dolostone bedrock was confirmed by coring at 101.0 to 102.0 feet bgs in Borings 10-RWB-01, 10-RWB-02 and 10-RWB-04, at elevations of 491.5 to 492.4 feet. Based on a 10-foot rock core taken, RQD is about 8 to 71% corresponding to very poor to fair quality rock. Dolostone bedrock was strong, light gray, bedded fresh, and moderately vuggy. Possible weathered bedrock was encountered at 491.5 to 496.4 feet, resting on top of the fair quality bedrock. The weathered dolostone layer may be water-bearing. *Rock Core Photographs* are included in Appendix A.

#### 5.2 Groundwater Conditions

Groundwater was observed in Borings 10-RWB-01, 10-RWB-02, 10-RWB-04 and 15-RWB-02 during drilling at elevations of 580.4 to 586.8 feet (5.5 to 13.0 feet bgs). After drilling the groundwater was measured in Boring 10-RWB-01 at an elevation of 503.6 feet (90.0 feet bgs). Groundwater level measured after 72 and 144 hrs of drilling completion in Borings 10-RWB-04 and 10-RWB-02 show at elevations of 558.4 and 577.5 feet, respectively (35.0 and 16.0 feet bgs).

A Piezometer 10-PZ-01 installed at station 7315+23.78 about 8.0 feet east from proposed retaining wall 10 was set with in silty loam to sandy loam deposit with the top and bottom of piezometer screen elevations at 519.3 and 499.3 feet (73.0 and 93.0 feet bgs), respectively. The groundwater levels monitored in the piezometer show elevations ranging from 549.2 to 554.5 feet with an average water table elevation of 552.4 feet. Encountering under pressure groundwater bearing layer should be accounted for during design and construction of the wall foundations.

#### 5.3 Seismic Design Considerations

The retaining wall is located in Seismic Performance Zone (SPZ) 1 and is not required to be designed for seismic forces as per 2012 IDOT Bridge Manual (IDOT, 2012).

## 6.0 ANALYSIS AND RECOMMENDATIONS

## 6.1 Retaining Wall Type Evaluation

The proposed retaining wall will be a cut wall along EB I-290 Ramp to Taylor Street Exit to SB I-90/94. Consideration was given in using standard cast-in-place cantilever concrete (T-type) walls with spread footings, however, it was ruled out due to low bearing resistance, excessive settlements unless drilled shaft support or ground improvement is performed. In addition, the construction of these wall types



would require a temporary soil retention system to retain the slope during construction for excavation of the foundations.

Finally, a drilled shaft with lagging wall type system was considered. Other non-gravity walls such as soldier pile and lagging type or tangent wall may also be used. The lateral movement of this type of wall is relatively smaller compared to more flexible walls.

For the southern portion of the wall alignment between Station 7315+46.05 and Station 7316+31.15, MSE wall was proposed to minimize the impact of the existing T-type wall with footings and piles, and other utility constrains in this area. There are several utilities such as existing 60-inch combined sewer that will be removed and relocated to in the MSE wall area. There will be a temporary retention system adjacent to the UIC building as well as a permanent soil retention system providing full lateral support for the excavation and MSE wall section. The design of the wall needs to account for these in the final design.

The geotechnical parameters and our evaluations for proposed walls are included in the next sections.

## 6.2 Drilled Shaft with Lagging Wall

The tip elevation of the drilled shafts will be determined by the lateral resistance. The design embedment depth of the wall sections should include a minimum FOS of 1.5 against earth pressure failure for walls in the long-term (drained) condition using the soil parameters shown in Tables 1 and 2. The design of the wall should ignore 3 feet of soil in front of the wall measured from the finished ground surface elevation in providing passive pressure due to excavation required for installation of concrete facing, drainage system and frost-heave condition. In developing the design lateral pressure, the lateral pressure due to construction equipment surcharge load should be added to the lateral earth pressure. Drainage behind the wall and underdrain should be as per 2012 IDOT Bridge Manual (IDOT, 2012). The water pressure distributions shown in 2014 AASHTO LRFD Bridge Design Specifications should be used. The wall design needs to account for the proposed drainage system.



## Table 1: Earth Pressure Parameters for Design of Walls

#### Stations 7309+74.27 to 7313+30.00

(Reference Borings 10-RWB-01, 10-RWB-02, 15-RWB-01, 1729-VST-01, and 1729-VST-02)

	Moist		d Shear Properties	Earth Pressure coefficients <sup>(1)</sup>			
Layer Elevations/ Soil Description	Unit Weight (pcf)	Cohesion Cu (psf)	Friction Angle, φ' (Degree)	Active Pressure	Passive Pressure		
593.60 <sup>(2)</sup> to 583.00 Silty Loam to Sand	115	0	30	0.33	3.00		
583.00 to 580.50 Clay to Silty Clay	115	100	30	0.33	3.00		
580.50 to 556.00 Clay to Silty Clay	110	50	30	0.33	3.00		
556.00 to 549.00 Clay to Silty Clay	110	50	30	0.33	3.00		
549.00 to 541.80 Clay to Silty Clay	115	100	31	0.32	3.12		
541.80 to 526.80 Silty Clay to Silty Clay Loam	120	100	32	0.31	3.25		
526.80 to 516.80 Silty Loam to Sandy Loam	120	0	31	0.32	3.12		
516.80 to 506.80 Silty Clay Loam	125	100	32	0.31	3.25		
506.80 to 491.50 <sup>(3)</sup> Silty Loam to Gravelly Sand	125	0	32	0.31	3.25		

<sup>(1)</sup>Earth pressure coefficients for straight backfill

<sup>(2)</sup> Existing grade elevation at wall
 <sup>(3)</sup> Top of bedrock elevation



#### Table 2: Earth Pressure Parameters for Design of Walls Stations 7313+30.00 to 7316+31.15 (Reference Borings 10-RWB-03, 10-RWB-04, 15-RWB-02, and VST-01) (02)

		02)					
	Moist		d Shear Properties	Earth Pressure coefficients <sup>(1)</sup>			
Layer Elevations/ Soil Description	Unit Weight (pcf)	Cohesion Cu (psf)	Friction Angle, φ' (Degree)	Active Pressure	Passive Pressure		
593.60 <sup>(2)</sup> to 582.90 Silty Loam to Sand	115	0	30	0.33	3.00		
582.90 to 578.00 Clay to Silty Clay	115	100	30	0.33	3.00		
578.00 to 562.60 Clay to Silty Clay	110	50	30	0.33	3.00		
562.60 to 557.60 Clay to Silty Clay	110	50	30	0.33	3.00		
557.60 to 540.60 Clay to Silty Clay	115	100	31	0.32	3.12		
540.60 to 528.90 Silty Clay to Silty Clay Loam	120	100	32	0.31	3.25		
528.90 to 514.40 Silty Loam to Sand	120	0	33	0.29	3.39		
514.40 to 506.30 Silty Clay Loam	125	100	32	0.31	3.25		
506.30 to 492.40 <sup>(3)</sup> Silty Loam to Gravelly Sand	125	0	33	0.29	3.39		

<sup>(1)</sup>Earth pressure coefficients for straight backfill <sup>(2)</sup>Existing grade elevation at top of wall

<sup>(3)</sup> Top of bedrock elevation



Design considerations should include deflection control at the top of the wall. The lateral deformation of the wall should be designed using the parameters shown in Tables 3 and 4 for two different sections via p-y curve (COMP624) method. The incremental parameters for the soft silty clay (Layer 3) undrained shear values were obtained from vane shear testing conducted at VST-01, 1729-VST-01, and 1729-VST-02.

Stations 7309+74.27 to 7313+30.00 (Reference Borings 10-RWB-01, 10-RWB-02, 15-RWB-01, 1729-VST-01, and 1729-VST-02)										
(Reference Dornigs 1	Moist	Shear Shear	Strength Pro	operties	_	2)- (51-02)				
Layer Elevations/ Soil Description	Unit	Short	Term	Long Term	Estimated Lateral Soil	Estimated				
	Weight	Cohesion	Friction	Friction	Modulus	Soil Strain Parameter <sup>(1)</sup> ,				
	(	Cu	Angle, φ	Angle, φ'	Parameter <sup>(1)</sup> , k (pci)	$\epsilon_{50}$				
	(pcf)	(psf)	(Degree)	(Degree)	<i>ч</i> ,					
593.60 <sup>(2)</sup> to 583.00 Silty Loam to Sand	115	0	30	30	5					
583.00 to 580.50 Clay to Silty Clay	115	2000	0	30	500	0.007				
580.50 to 556.00 Clay to Silty Clay	110	600	0	30	100	0.010 0.010 0.007				
556.00 to 549.00 Clay to Silty Clay	110	750	0	30	100					
549.00 to 541.80 Clay to Silty Clay	115	1050	0	31	500					
541.80 to 526.80 Silty Clay to Silty Clay Loam	120	5500	0	32	2000	0.004				
526.80 to 516.80 Silty Loam to Sandy Loam	526.80 to 516.80 Silty Loam to 120			31	45					
516.80 to 506.80 Silty Clay Loam	125	8000	0	32	2000	0.004				
506.80 to 491.50 <sup>(3)</sup> Silty Loam to Gravelly Sand	125	0	32	32	60					
<sup>(1)</sup> Based on L-Pile Technical Manual 2012										

Table 3:	Geotechnical	Parameters	for Design	n of Walls
----------	--------------	------------	------------	------------

<sup>(2)</sup> Top of boring elevation

<sup>(3)</sup> Top of bedrock elevation



Table 4: Geotechnical Parameters for Design of Walls											
(D - f - m - m - m		Stations 7313				`					
(Reference	Borings I				02, and VST-01	)					
	Moist		Strength Pro								
	Unit	Short	Term	Long	Estimated	Estimated					
Layer Elevations/	Weight	<u> </u>	<b>D</b> • • •	Term	Lateral Soil	Soil Strain					
Soil Description	U	Cohesion	Friction	Friction	Modulus	Parameter <sup>(1)</sup> ,					
•		Cu	Angle, φ	Angle, φ'	Parameter <sup>(1)</sup> ,	ε <sub>50</sub>					
	(pcf)				k (pci)	20					
<b>500 50</b> (2) + <b>500</b> 00		(psf)	(Degree)	(Degree)	-						
593.60 <sup>(2)</sup> to 582.90	115	0	30	30	5						
Silty Loam to Sand											
582.90 to 578.00	115	1500	0	30	500	0.007					
Clay to Silty Clay											
578.00 to 562.60	110	650	0	30	100	0.010					
Clay to Silty Clay					100						
562.60 to 557.60	110	600	0	30		0.010					
Clay to Silty Clay											
557.60 to 540.60	115	1050	0	31	500	0.007					
Clay to Silty Clay											
540.60 to 528.90	100	5200	0	22	••••	0.004					
Silty Clay to Silty	120	5300	0	32	2000	0.004					
Clay Loam											
528.90 to 514.40	120	0	33	33	50						
Silty Loam to Sand											
514.40 to 506.30	125	8000	0	32	2000	0.004					
Silty Clay Loam											
506.30 to 492.40 <sup>(3)</sup>	105	0	22	22	<b>C</b> 0						
Silty Loam to	125	0	33	33	60						
Gravelly Sand	1. 1. 20	1.2									

Table 4: Costachnical Daramatara for Design of Walls

<sup>(1)</sup>Based on L-Pile Technical Manual 2012

<sup>(2)</sup> Top of boring elevation

<sup>(3)</sup> Top of bedrock elevation

As per AECOM's cross sections, there will be a temporary retention system adjacent to the UIC building as well as a permanent soil retention system providing full lateral support for the excavation and MSE wall section. These walls will be designed by others. The soil parameters in Tables 1 through 4 may be used for the design of the soil retention systems.

#### 6.2.1 Settlement Analyses

Long-term settlement is not an issue since no new fill is planned to be added back of the drilled shaft with lagging wall.



#### 6.2.2 Global Stability Analyses

Global stability analysis was performed for the maximum wall height with up to 25.5 feet at Station 7309+74 for both short-term (undrained) and long-term (drained) soil conditions as presented in Appendix B. The soil parameters previously established in Section 6.2 were used for the stability analysis.

We estimate the maximum cut wall section has a short-term factor of safety (FOS) of 1.5 and a long-term FOS of 1.8 (Appendices B-2 and B-3), therefore satisfying the minimum IDOT FOS requirements (IDOT, 2015). The analysis basically shows the wall configuration needed to achieve a minimum 1.5 FOS against global instability for the most critical case. We estimate that the bottom of the wall should be at or below elevation of 547 feet to achieve a minimum FOS of 1.5 against global stability failure based on the short-term conditions. Additional embedment and lateral analyses will also be performed to establish final wall design. The minimum FOS calculated was less than the minimum required of 1.5 without considering wall embedment (Appendix B-1).

#### 6.3 MSE Wall

IDOT/AECOM are considering the MSE wall with proposed soil retention system between Station 7315+46.05 and Station 7316+31.15 due to the UIC Recreation Facility, and the existing and proposed combined sewers in the wall foot print. There will be a temporary retention system adjacent to the UIC building as well as a permanent soil retention system providing full lateral support for the excavation and MSE wall section.

Based on the information provided by AECOM, we understand the proposed MSE wall will be about 84.75 feet long with a maximum total height of 14.75 feet and exposed/retained height of 12.25 feet. During the MSE wall option development, we discussed with AECOM various fill alternatives for the MSE wall taking into consideration of the soil conditions at founding level and available MSE reinforcement zone width. We have analyzed several alternatives for the fill material to be used in the reinforcement zone and fill area between the reinforcement zone and the proposed soil retention system as follows:

- 1. Using the regular fill material for the MSE reinforcement zone and fill area, and
- 2. Using Class III Lightweight Cellular Concrete Fill (LCCF) for the MSE reinforcement zone and fill area.



Based on our analyses, alternative 2 satisfies the bearing capacity requirements which govern and is the recommend as backfill for the MSE wall. The LCCF filled MSE wall will have full lateral support by the proposed permanent shoring system, external stability is not a concern.

## 6.3.1 Bearing Resistance

The factored bearing resistance to be considered for the design of the MSE wall was calculated assuming the top of the levelling pad will be established at 3.5 feet below the finished grade on the front face of the wall. As per 2014 AASHTO LRFD Bridge Design Specifications, a bearing resistance factor of 0.65 was used. The nominal bearing resistance of the foundation soils is calculated to be 3,200 psf and the factored bearing resistance is 2,100 psf. The estimated applied factored maximum uniform bearing pressure for the LCCF is 2,000 psf.

## 6.3.2 Sliding and Overturning

The estimated friction angles between the base of the MSE wall and the existing cohesive foundation soil or granular backfill are 28° and 30°, respectively, and the corresponding friction coefficients are 0.53 and 0.58, respectively. MSE retaining walls are designed based on a geotechnical sliding resistance factor ( $\phi_{\tau}$ ) of 1.0 for soil-on-soil contact (AASHTO 2014). Sliding and eccentricity of the LCCF filled MSE wall is stable due to the retention of lateral forces by the proposed permanent shoring system. It should be noted that for very narrow MSE wall sections located between Sta. 7315+46.05 to Sta. 7315+66.46, the soil reinforcement may need to be tied to the shoring system to avoid overturning of the hardened slender LCCF MSE block.

## 6.3.3 Settlement Analyses

Considering the unloading and reloading effect and the placement of LCCF, the long-term primary settlement of MSE wall with LCCF will be 1 inch or less.

## 6.3.4 Global Stability Analyses

Global stability is not a concern due to the proposed permanent deep soil retention system.

## 6.4 Impact of Wall Installation on Existing Buildings and Utilities

Based on the TSL, the nearest existing building to the proposed drilled shaft with lagging wall is the UIC Recreation Facility located about 26 feet away at Station 7314+00 where a maximum wall height of 17 feet was considered. AECOM has selected a maximum lateral top of wall deflection of 0.5% of the



exposed wall height which corresponds to 1 inch for the 17 feet height. The acceptable surface movement of 0.25 inches was provided by CDOT.

Using empirical data compiled in various research papers, Wang estimated the ground movement of about 0.4 inches adjacent to the building that is 26 feet away from the wall using 0.5 % maximum lateral deflection limit criteria. The facility is supported on a deep foundation system. The ground movement estimates are provided in Appendix D.

The potential impact of the wall deflection inducing ground movements on other structures that are closer such as the relocated 60-inch diameter sewer, proposed 48-inch diameter watermain, and buried utilities (sewer, water, electric, ITS cable, etc.) must be considered in final design to ensure specific deformation limits are not exceeded, leading to settlement or structural cracks.

## 7.0 CONSTRUCTION CONSIDERATIONS

#### 7.1 Excavation and Dewatering

Foundation excavations should be performed in accordance with local, state, and federal regulations including current OSHA regulations. The potential effect of ground movements upon nearby structures and utilities should be considered during construction.

Based on the results of our investigation and proposed excavation in front of the wall, perched water is likely to be encountered during construction within the fill. The water accumulated in excavation should be removed through conventional sump and pump methods. Intermittent water-bearing layers may also be present at deeper levels within the proposed drilled shafts. These layers may locally impact drilled shaft installations. Casing will be required to seal these interbeds off in the event that they are exposed. Casing will also be necessary to prevent shaft squeeze within the soft and deformable clays encountered (**Layer 3**). Moreover, during drilling we encountered hard drilling which indicates the possibility of cobbles or boulders.

#### 7.2 Filling and Backfilling

All fill and backfill materials will be as per IDOT Standard Specification.

## 7.3 Drilled Shaft with Lagging Wall

The wall should be constructed as per IDOT Standard Specifications and the current special provision



developed by IDOT for construction of secant pile wall. The impact of the presence of existing buildings, parking lots, and utilities on the construction of the proposed Wall 10 should be evaluated.

## 7.4 MSE Wall

The MSE wall should be constructed as per Section 522 Retaining Walls of the IDOT Standard Specifications. Select fill material should be Class III LCCF material if used, as per IDOT District One Special Provisions. The impact of the presence of existing buildings, parking lots, and utilities on the construction of the proposed Wall 10 should be evaluated.

## 7.5 Drilled Shafts

Walls will be formed with drilled shafts. After a drilled shaft is completed to the required elevation, the base should be cleaned and inspected, the flange placed, and the concrete discharged at the base using a tremie pipe or concrete pump. The drilled shafts should be constructed in accordance with Section 516 Drilled Shafts of IDOT Standard Specifications for Road and Bridge Construction (IDOT, 2016). As mentioned in section 7.1 casing will be required to seal-off water and/or prevent squeezing of soft clays. Casings will be required to maintain an open borehole at these locations. Failure to anticipate the challenges posed by the groundwater may result in caving or heaving sand and weakening of the foundation soils, as well as the potential for shaft squeeze in the soft clay. Shaft squeeze and heavy dewatering can result in ground loss around the perimeter of the shaft, affecting adjacent roadways and facilities.

## 7.6 Construction Monitoring

Due to the wall's proximity to utilities, buildings and other structures, Wang recommends instrumentation of the wall and ground surfaces with the use of ground survey monuments, survey pins on wall, and inclinometers to monitor actual deflections and movements during construction.

## 8.0 QUALIFICATIONS

The analysis and recommendations submitted in this report are based upon the data obtained from the borings drilled at the locations shown on the boring logs and in Exhibit 3. This report does not reflect any variations that may occur between the borings or elsewhere on the site, variations whose nature and extent may not become evident until the course of construction. In the event that any changes in the design and/or location of Retaining Wall 10 (SN016-1729) are planned, we should be timely informed so that our recommendations can be adjusted accordingly.



It has been a pleasure to assist AECOM and the Illinois Department of Transportation on this project. Please call if there are any questions, or if we can be of further service.

Respectfully Submitted,

Exp. 11 30 2017 WANG ENGINEERING, INC. Corina T. Farez, P.E., P.G. Metin W. Seyhun, P.E. Senior Geotechnical Engineer Vice President P K, FNGIMEEA Jerry W.H. Wang, PhD., P QA/QC Reviewer

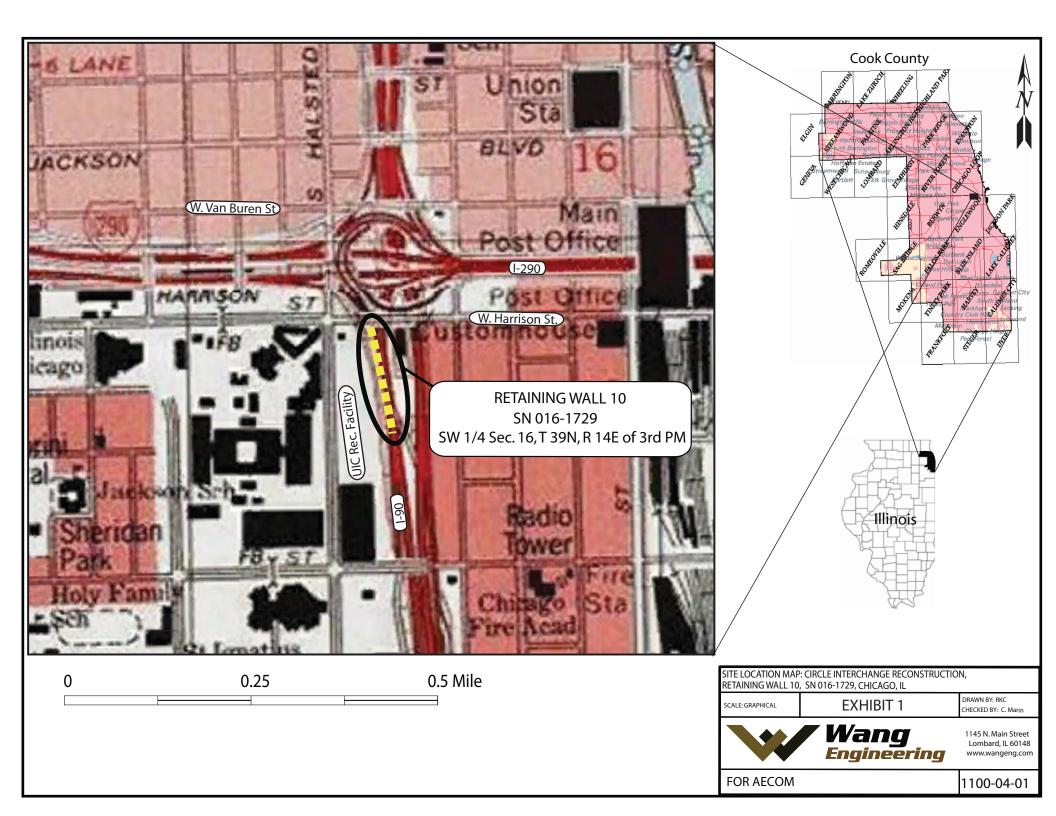


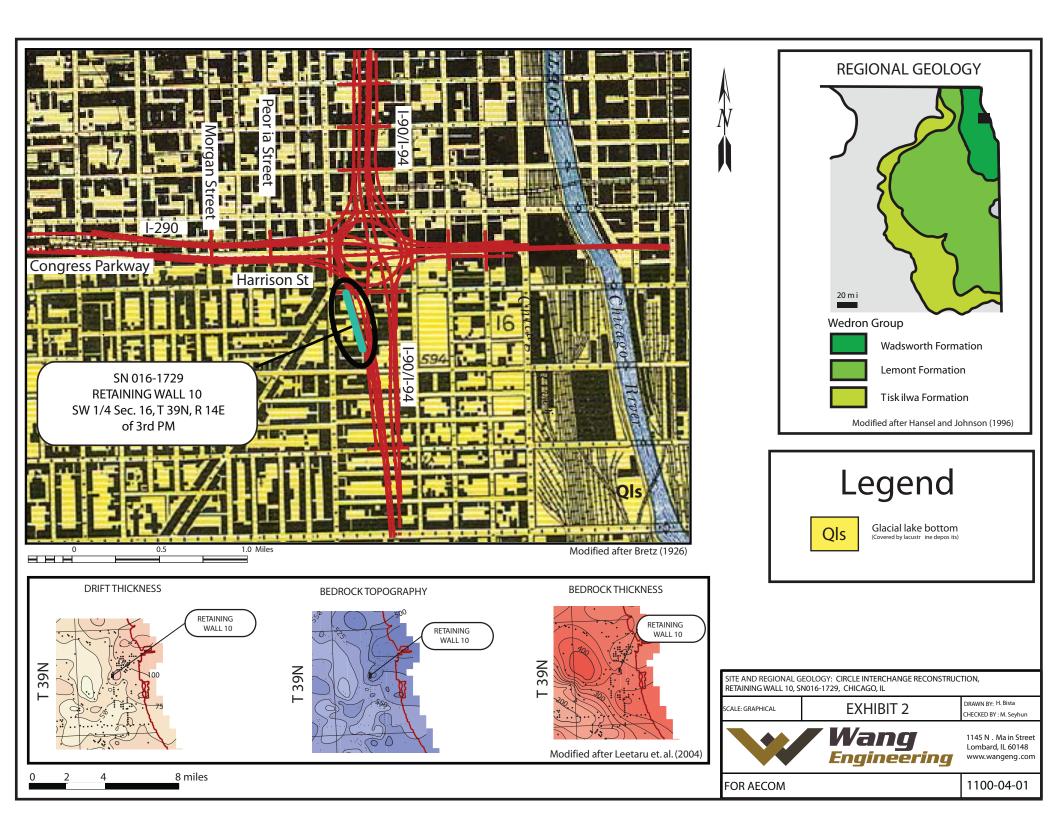
#### REFERENCES

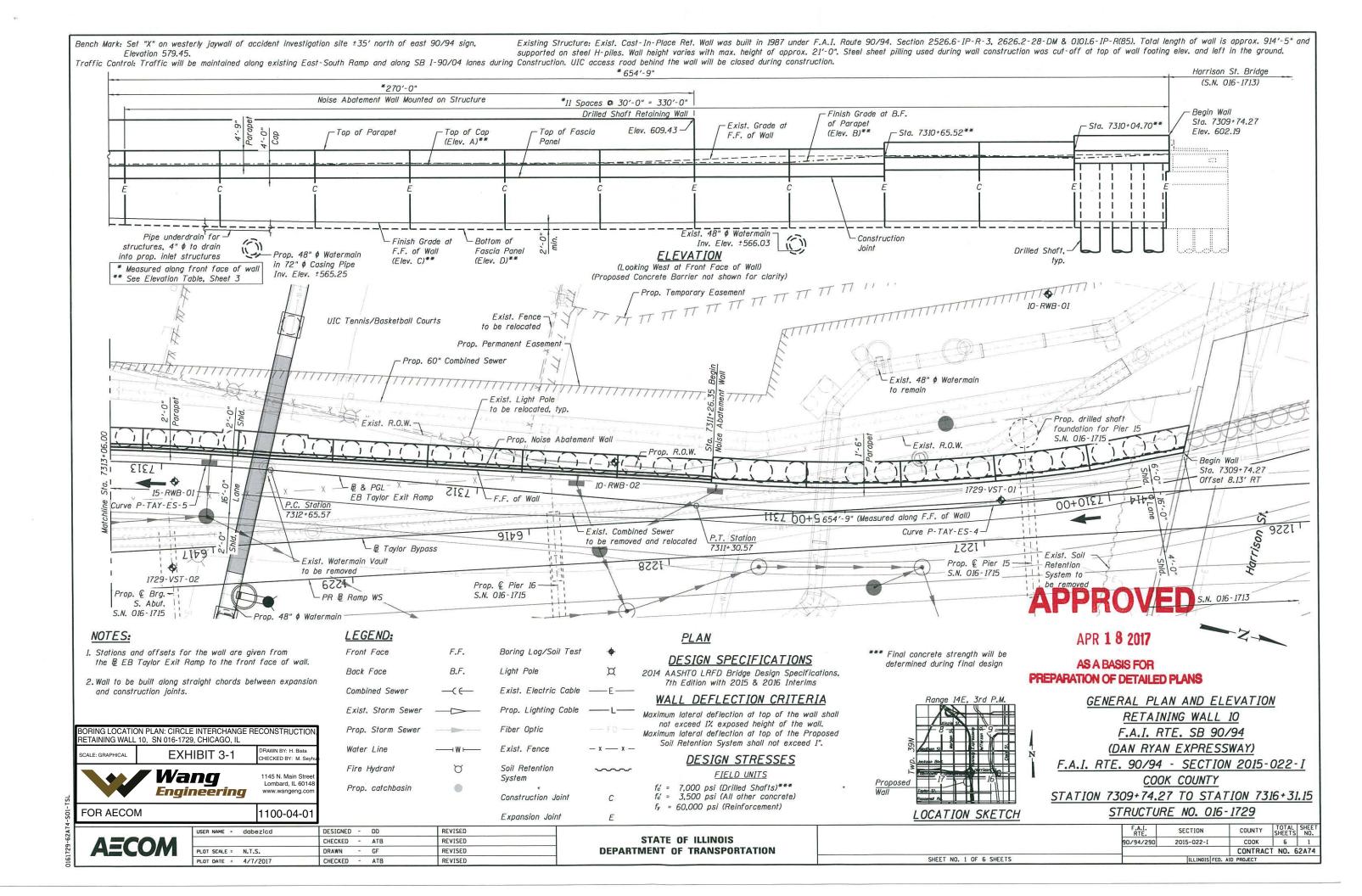
- AMERICAN ASSOCIATION OF STATE HIGHWAY TRANSPORTATION OFFICIALS (2014) *LRFD Bridge Design Specifications*. United States Department of Transportation, Washington, D.C.
- BAUER, R.A., CURRY, B.B., GRAESE, A.M., VAIDEN, R.C., SU, W.J., and HASEK, M.J., 1991, Geotechnical Properties of Selected Pleistocene, Silurian, and Ordovician Deposits of Northeastern Illinois: Environmental Geology 139, Illinois State Geological Survey, 69 p.
- CHRZATOWSKY, M.J., and THOMPSON, T.A., 1992, Late Wisconsinan and Holocene coastal evolution of the southern shore of Lake Michigan, *in* Fletcher, C.H., III, and Wehmiller, J.F., eds., Quaternary Coasts of the United States: Marine and Lacustrine Systems: SEPM Special Publication No.48: Tulsa, Oklahoma, Society for Sedimentary Geology, p. 397-413.
- HANSEL, A.K., and JOHNSON, W.H. (1996) Wedron and Mason Groups: Lithostratigraphic Reclassification of the Wisconsin Episode, Lake Michigan Lobe Area: ISGS Bulletin 104.
   Illinois State Geological Survey, Champaign, IL. 116 p.
- LEETARU, H.E., SARGENT, M.L., AND KOLATA, D.R, 2004, *Geologic Atlas of Cook County for Planning Purposes*, Open File Series 2004-12, Illinois State Geological Survey, p. 30.
- ILLINOIS DEPARTMENT OF TRANSPORTATION (2015) *Geotechnical Manual*. IDOT Bureau of Materials and Physical Research, Springfield, IL.
- ILLINOIS DEPARTMENT OF TRANSPORTATION (2016) Standard Specifications for Road and Bridge Construction. IDOT Division of Highways, Springfield, IL.
- ILLINOIS DEPARTMENT OF TRANSPORTATION (2012) *Bridge Manual*. IDOT Bureau of Bridges and Structures, Springfield, IL.
- WILLMAN, H.B., 1971, *Summary of the Geology of the Chicago Area*, ISGS Circular C460: Urbana, Illinois State Geological Survey, p. 77.

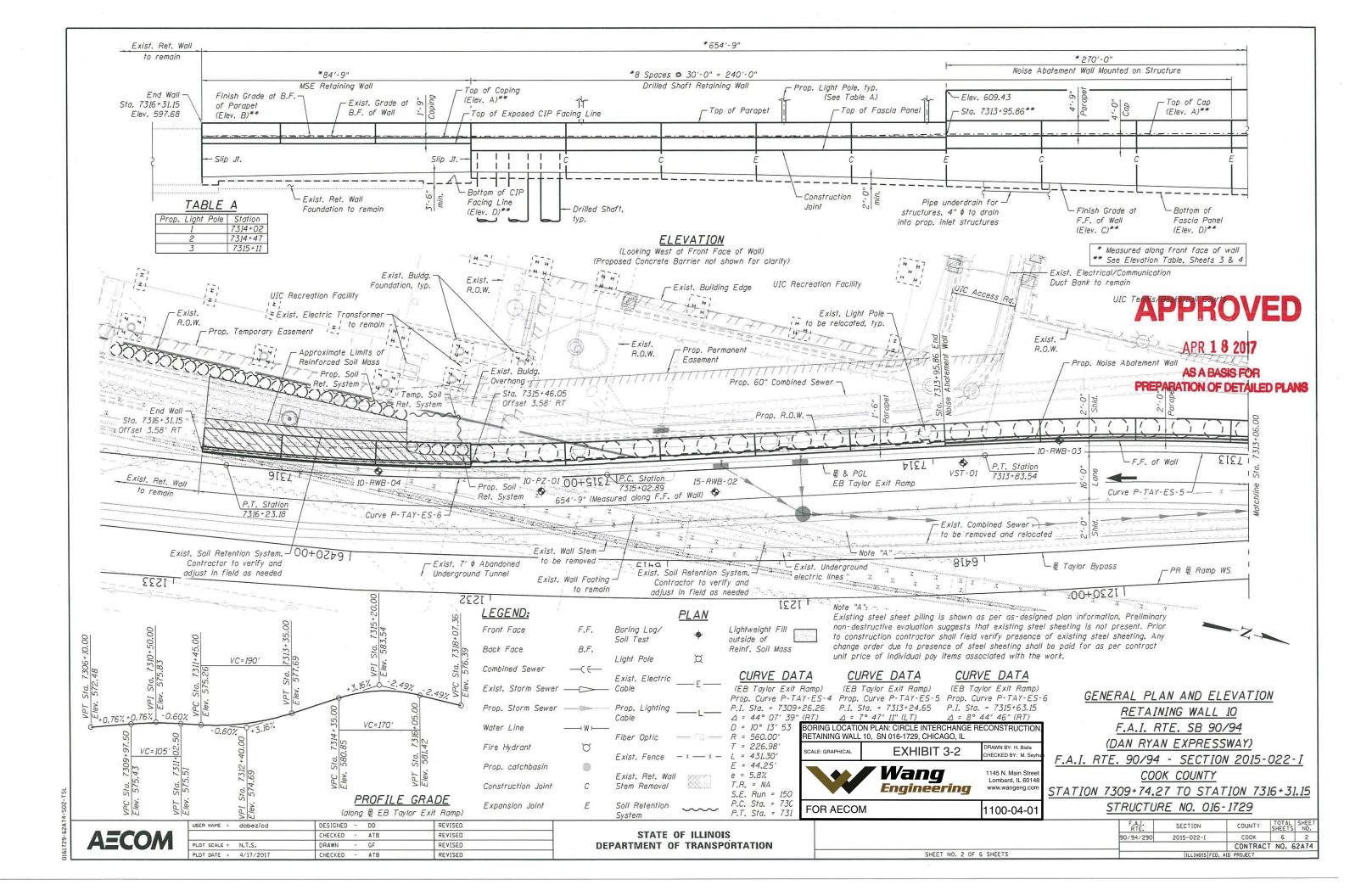


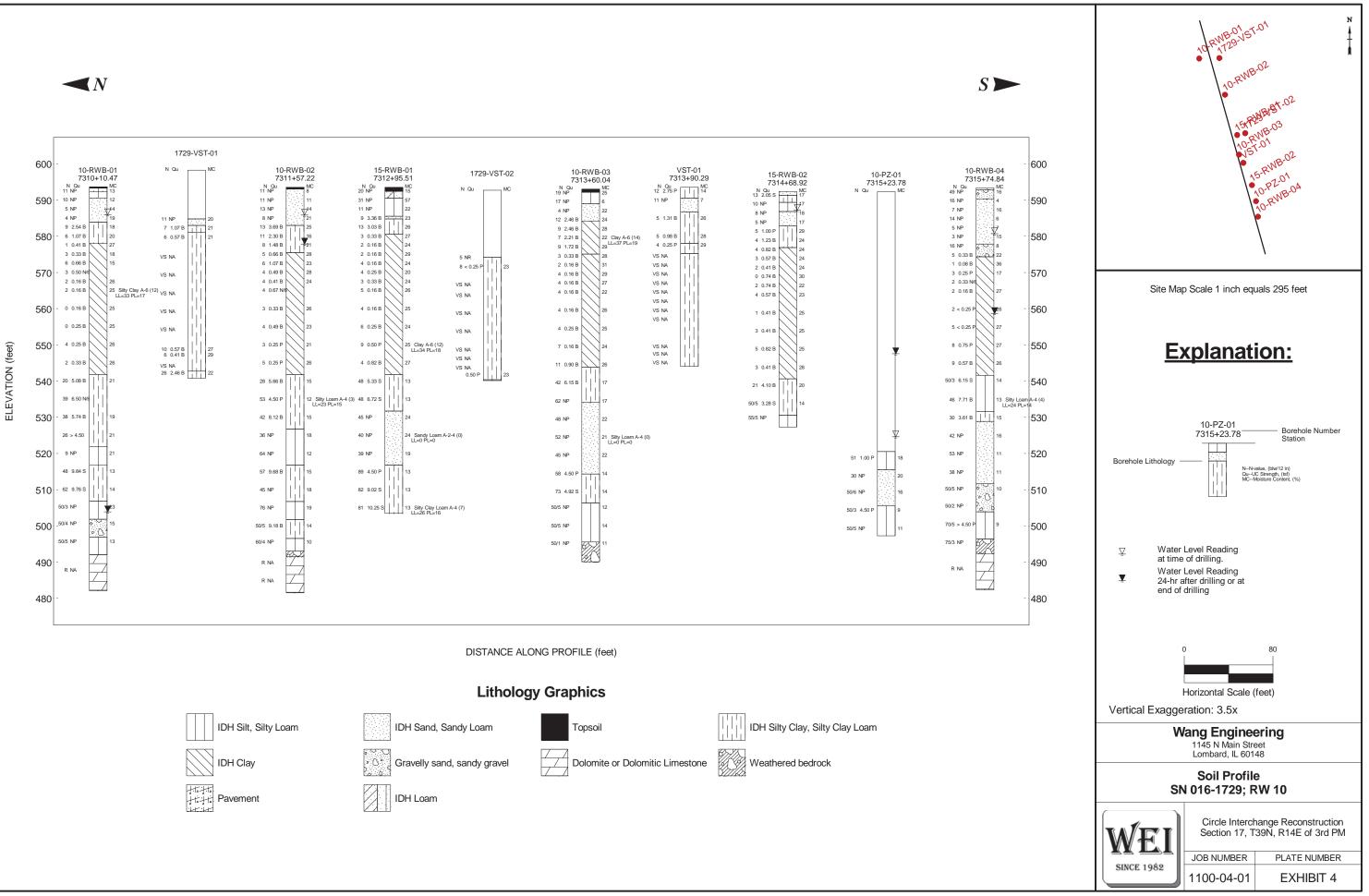
# **EXHIBITS**













# **APPENDIX** A



Client

Project

Location

## BORING LOG 10-PZ-01

WEI Job No.: 1100-04-01

Page 1 of 3

wangeng@wangeng.com 1145 N Main Street Lombard, IL 60148 Telephone: 630 953-9928 Fax: 630 953-9928

AECOM Circle Interchange Reconstruction Section 17, T39N, R14E of 3rd PM Datum: NAVD 88 Elevation: 592.32 ft North: 1896981.56 ft East: 1171477.47 ft Station: 7315+23.78 Offset: 8.25157 RT

Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft) Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ff)	Sample Type	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
		Drilled without sampling	-								-					
			- - - 5_ -						In B	zometer Data: istalled in Dec. 11, 2014 entonite Seal 66 to 71 feet						
			- - - - - 10						To S	op of Sand Pack at 71 feet op of Screen at 73 feet creen Length 20 feet ottom of Screen at 93 feet	-					
			 15 								 35  -					
			_ _ _ _ 20_								- - - 40					
5	_	GENER	AL NOTI	ES		_	_			WATER	LEVE	LD	AT.	A	-	
Be	egin Drilli		Complete			1	2-11	-201	4	While Drilling	<u> </u>			)0 ft		
E Dr	illing Co						B-57			At Completion of Drilling	<b>T</b>		74.0	)0 ft		
Dr	iller	P&P Logger	A. Happe		. Che						4 hour					
Dr	illing Me		oring wate	er v	vell;	pizor	nete	r		Depth to Water The stratification lines represe	5.04 ft		ate br	Jundan		
installed on 12/11/2014							between soil types; the actual	transition r	nay be	e grad	dual.	Y				



Client

Project

Location

## BORING LOG 10-PZ-01

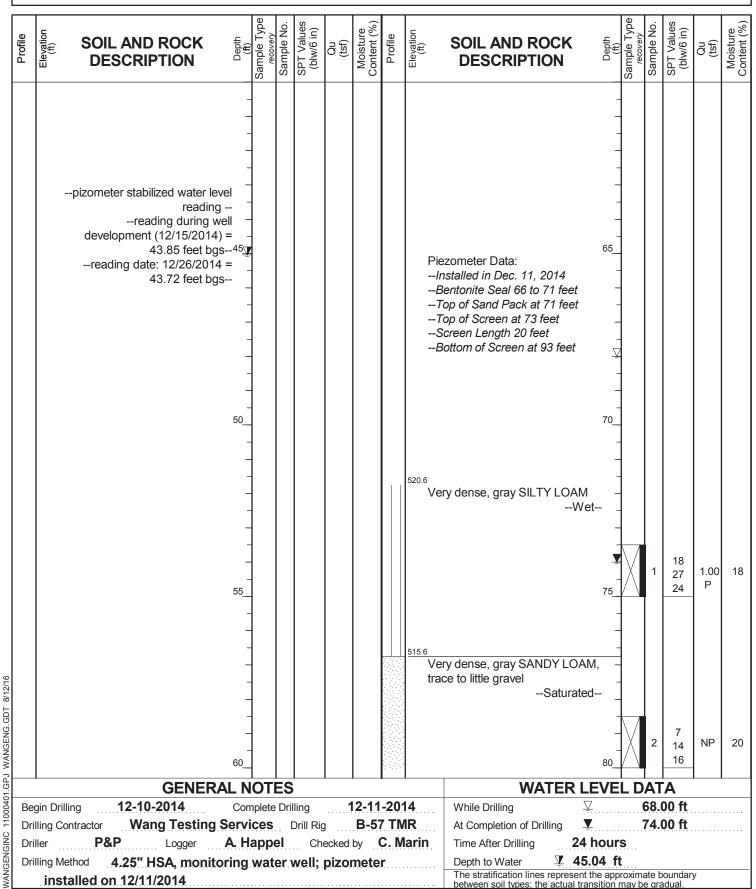
WEI Job No.: 1100-04-01

Page 2 of 3

wangeng@wangeng.com 1145 N Main Street Lombard, IL 60148 Telephone: 630 953-9928 Fax: 630 953-9928

#### AECOM Circle Interchange Reconstruction Section 17, T39N, R14E of 3rd PM

Datum: NAVD 88 Elevation: 592.32 ft North: 1896981.56 ft East: 1171477.47 ft Station: 7315+23.78 Offset: 8.25157 RT





Client

Project

# **BORING LOG 10-PZ-01**

WEI Job No.: 1100-04-01

Page 3 of 3

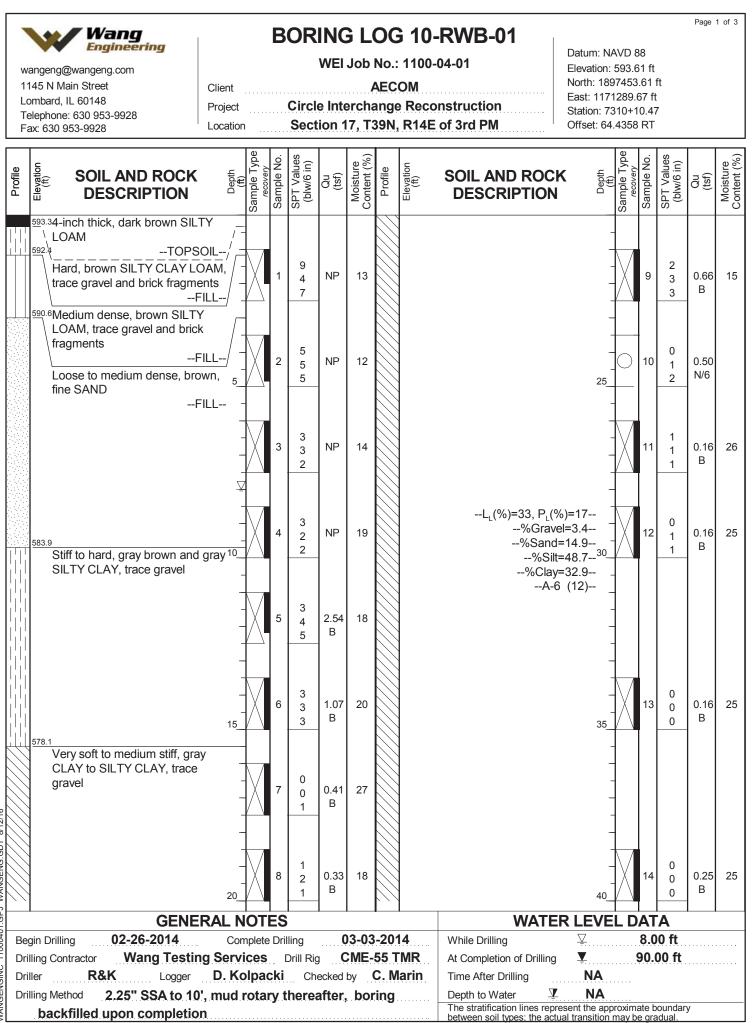
wangeng@wangeng.com 1145 N Main Street Lombard, IL 60148 Telephone: 630 953-9928

#### AECOM **Circle Interchange Reconstruction**

Datum: NAVD 88 Elevation: 592.32 ft North: 1896981.56 ft East: 1171477.47 ft Station: 7315+23.78 Offset: 8.25157 RT

between soil types; the actual transition may be gradual

Section 17, T39N, R14E of 3rd PM Location Fax: 630 953-9928 SPT Values (blw/6 in) SPT Values (blw/6 in) Moisture Content (%) Moisture Content (%) Sample Type Sample No Sample No Elevation (ft) Elevation (ft) Profile Profile SOIL AND ROCK Depth (ff) SOIL AND ROCK Depth (ft) Qu (tsf) Qu (tsf) Sample DESCRIPTION DESCRIPTION 3 NP 16 50/6 85 505.6 Very dense, gray SILTY LOAM, trace gravel 4 4.50 9 50/3 Ρ --Moist--90 --Wet--5 NP 11 50/5 --HARD DRILLING--95 497.3 Boring terminated at 95.00 ft 100 WATER LEVEL DATA **GENERAL NOTES** 68.00 ft 12-11-2014 **Begin Drilling** 12-10-2014 **Complete Drilling** While Drilling  $\nabla$ 74.00 ft Wang Testing Services Drill Rig **B-57 TMR** Ţ **Drilling Contractor** At Completion of Drilling Driller P&P Logger A. Happel Checked by **C. Marin** Time After Drilling 24 hours ¥ 45.04 ft **Drilling Method** 4.25" HSA, monitoring water well; pizometer Depth to Water The stratification lines represent the approximate boundary installed on 12/11/2014



WANGENGINC 11000401.GPJ WANGENG.GDT 8/12/16



## **BORING LOG 10-RWB-01**

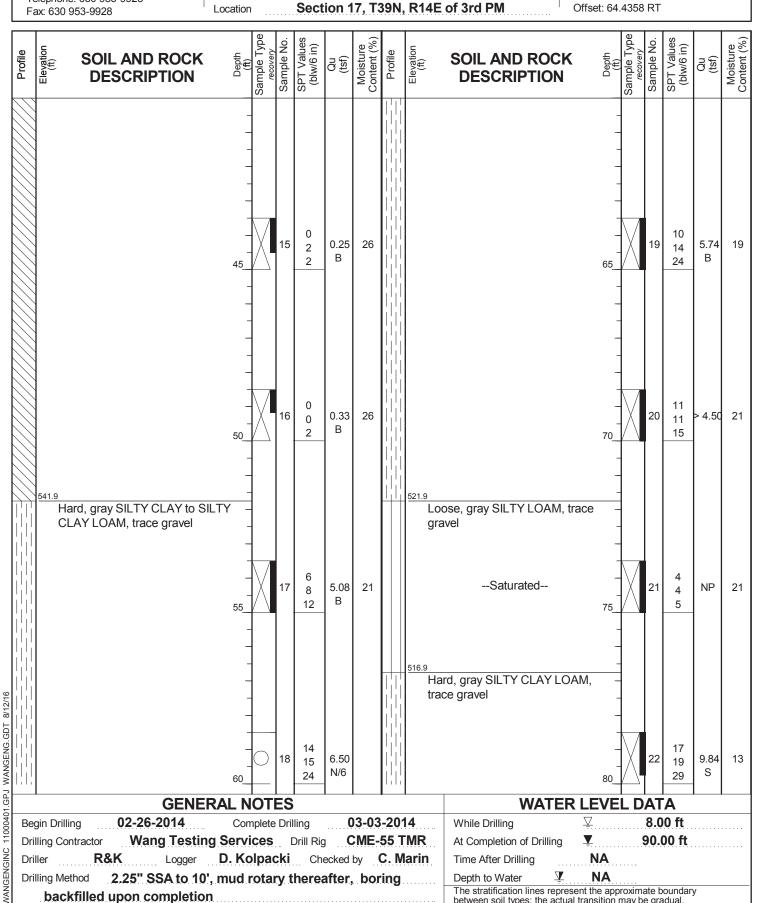
WEI Job No.: 1100-04-01

Page 2 of 3

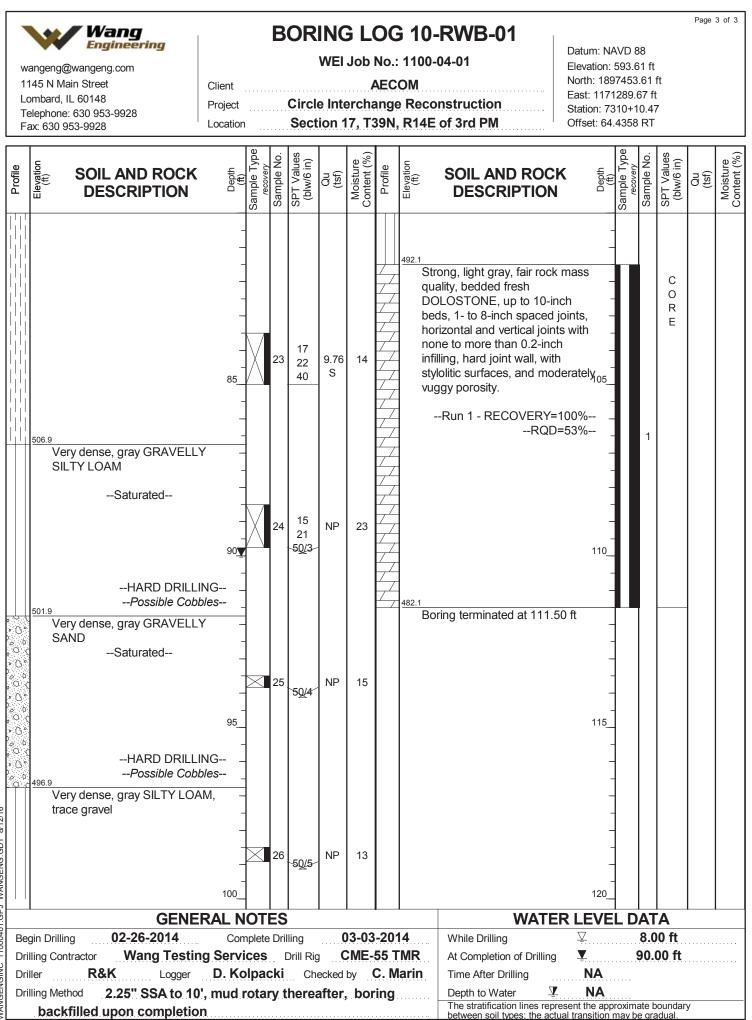
wangeng@wangeng.com 1145 N Main Street Lombard, IL 60148 Telephone: 630 953-9928

#### AECOM Client Project **Circle Interchange Reconstruction**

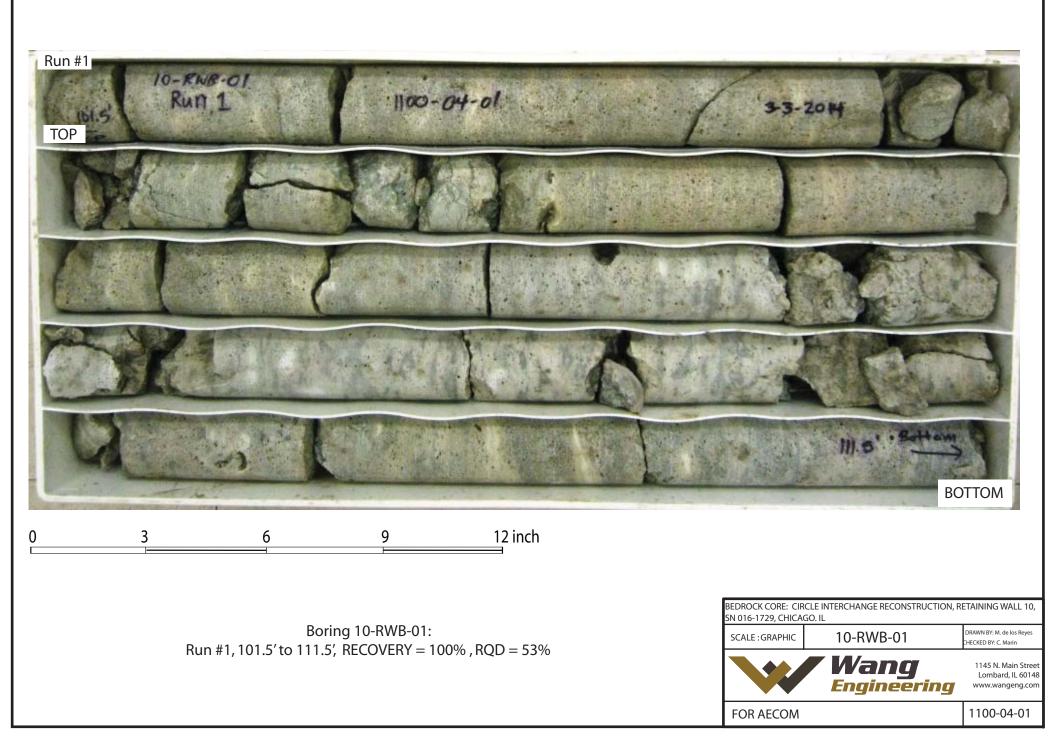
Datum: NAVD 88 Elevation: 593.61 ft North: 1897453.61 ft East: 1171289.67 ft Station: 7310+10.47 Offset: 64.4358 RT

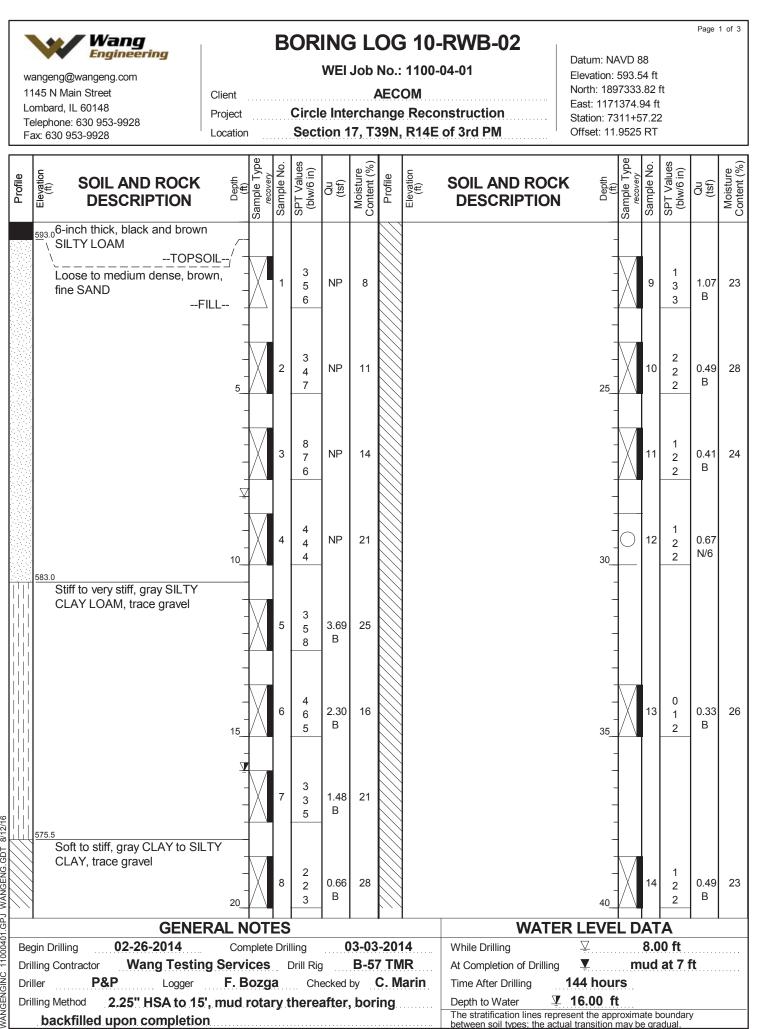


between soil types; the actual transition may be gradual



NANGENGINC 11000401.GPJ WANGENG.GDT 8/12/16





8/12/16 WANGENGINC 11000401.GPJ WANGENG.GDT



## BORING LOG 10-RWB-02

WEI Job No.: 1100-04-01

Page 2 of 3

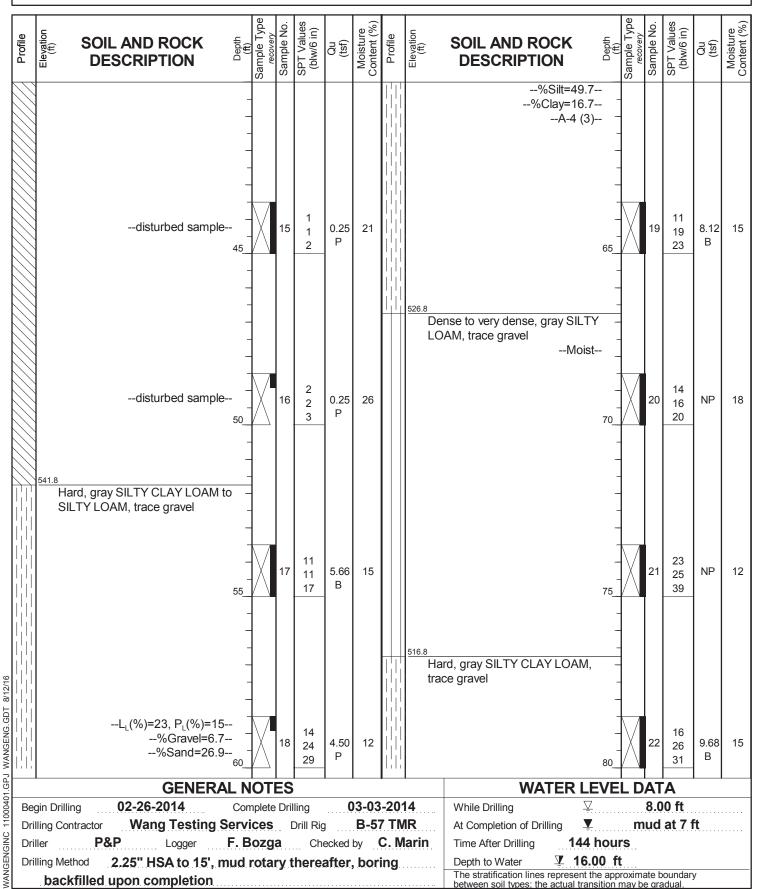
wangeng@wangeng.com 1145 N Main Street Lombard, IL 60148 Telephone: 630 953-9928 Fax: 630 953-9928

 Client
 AECOM

 Project
 Circle Interchange Reconstruction

 Location
 Section 17, T39N, R14E of 3rd PM

Datum: NAVD 88 Elevation: 593.54 ft North: 1897333.82 ft East: 1171374.94 ft Station: 7311+57.22 Offset: 11.9525 RT





## **BORING LOG 10-RWB-02**

WEI Job No.: 1100-04-01

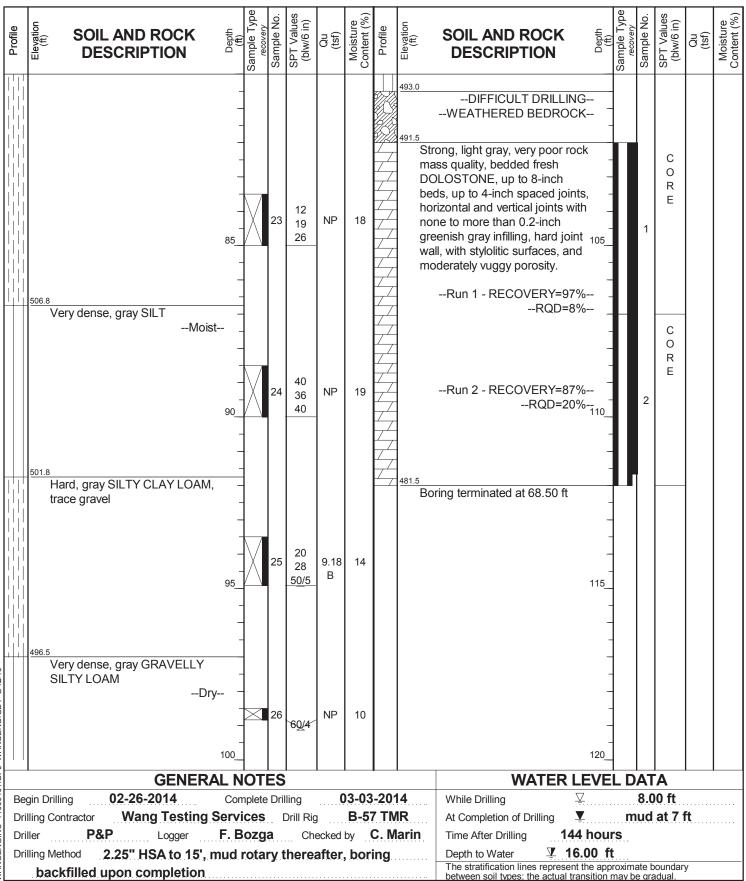
wangeng@wangeng.com 1145 N Main Street Lombard, IL 60148 Telephone: 630 953-9928 Fax: 630 953-9928

 Client
 AECOM

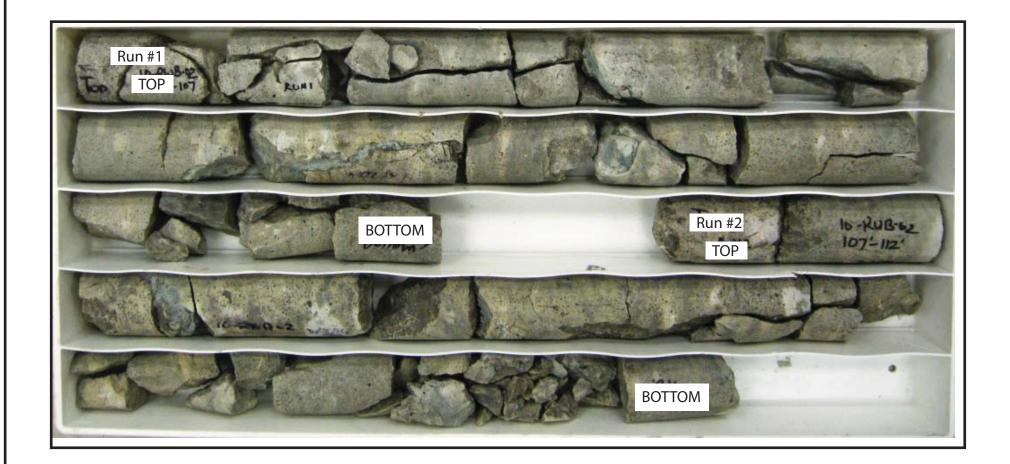
 Project
 Circle Interchange Reconstruction

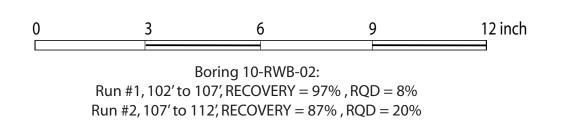
 Location
 Section 17, T39N, R14E of 3rd PM

Datum: NAVD 88 Elevation: 593.54 ft North: 1897333.82 ft East: 1171374.94 ft Station: 7311+57.22 Offset: 11.9525 RT

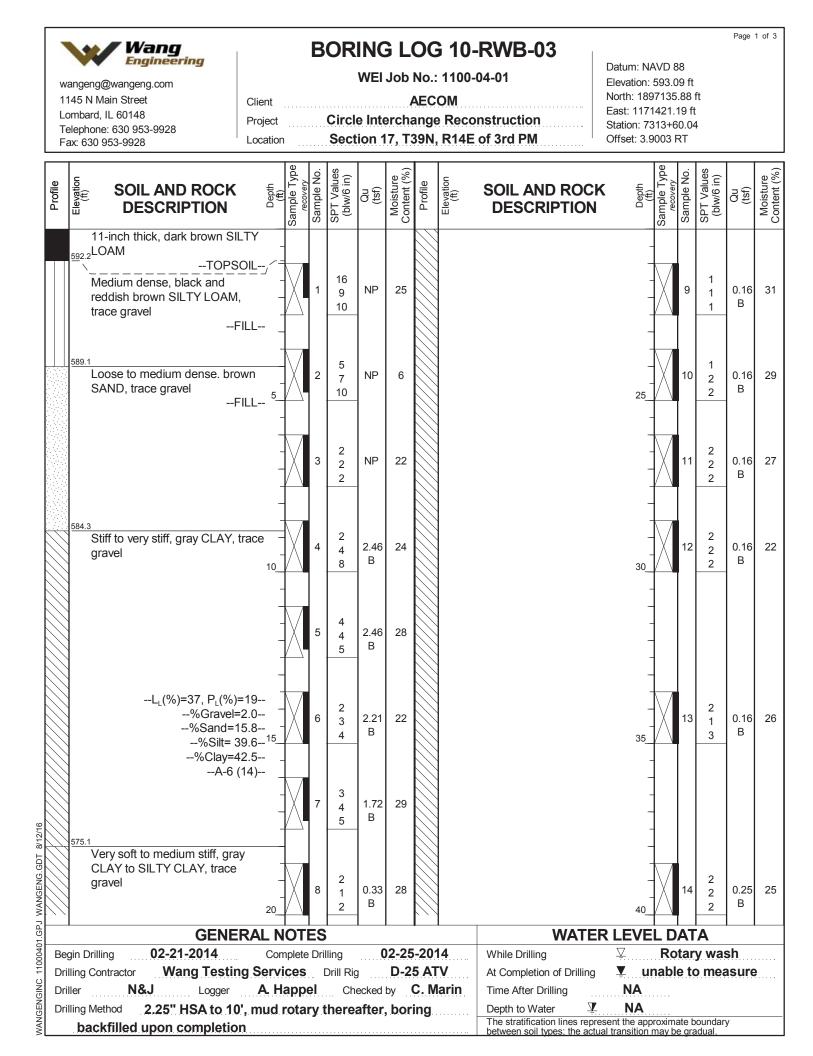


Page 3 of 3











Client

Project

## **BORING LOG 10-RWB-03**

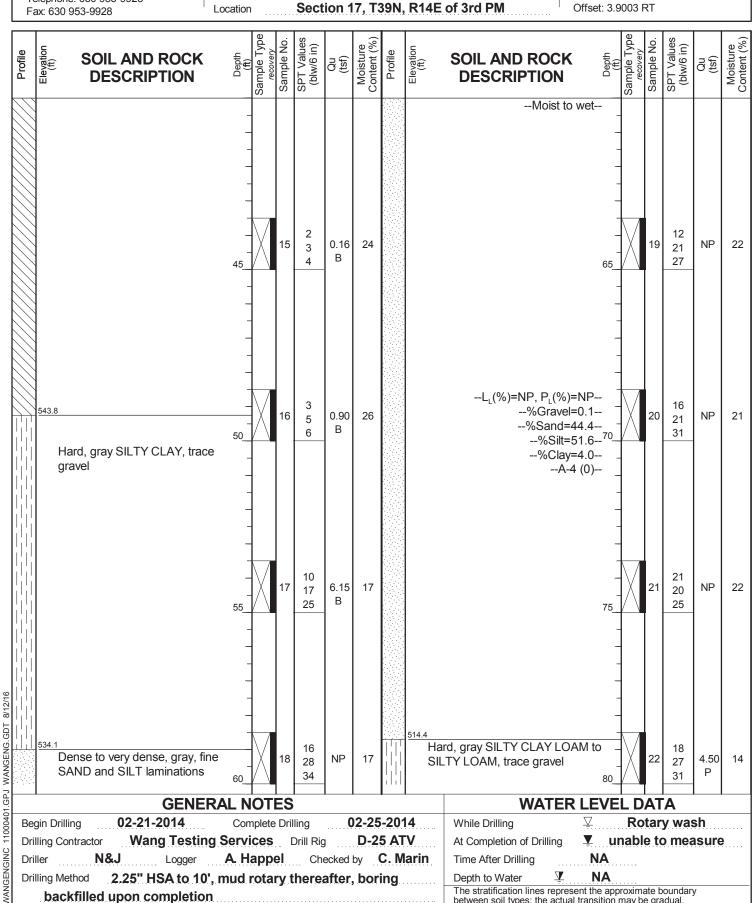
WEI Job No.: 1100-04-01

Page 2 of 3

wangeng@wangeng.com 1145 N Main Street Lombard, IL 60148 Telephone: 630 953-9928

AECOM **Circle Interchange Reconstruction**  Datum: NAVD 88 Elevation: 593.09 ft North: 1897135.88 ft East: 1171421.19 ft Station: 7313+60.04 Offset: 3.9003 RT

between soil types; the actual transition may be gradual





## **BORING LOG 10-RWB-03**

WEI Job No.: 1100-04-01

Page 3 of 3

wangeng@wangeng.com 1145 N Main Street Lombard, IL 60148 Telephone: 630 953-9928 Fax: 630 953-9928

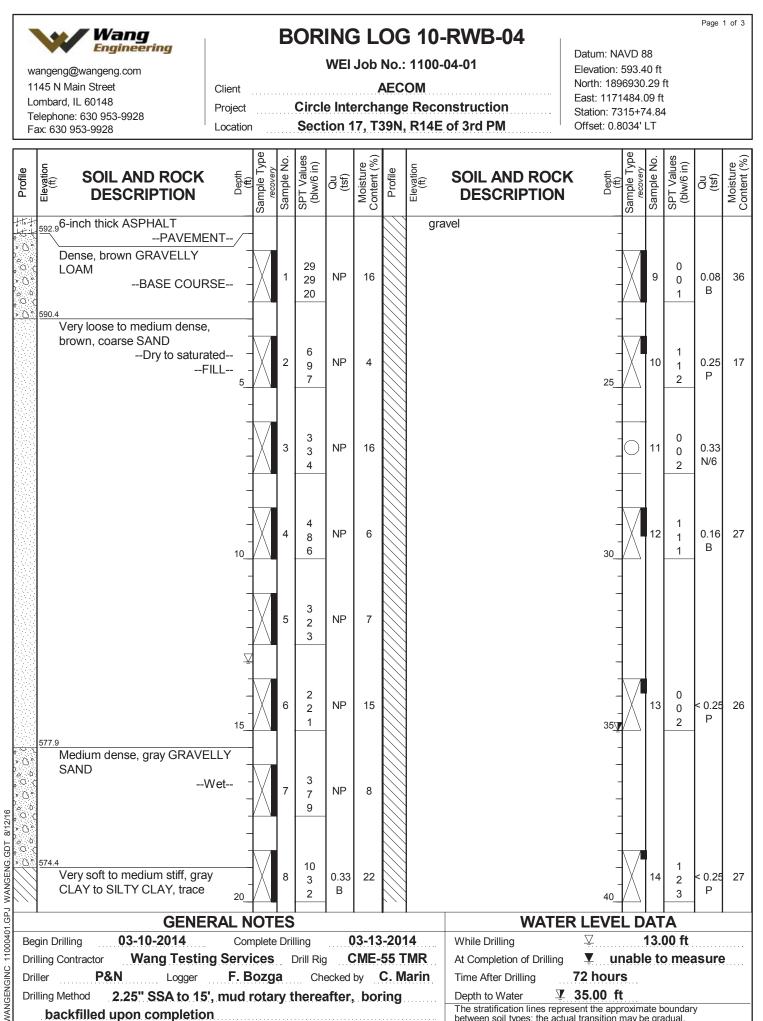
 Client
 AECOM

 Project
 Circle Interchange Reconstruction

 Location
 Section 17, T39N, R14E of 3rd PM

Datum: NAVD 88 Elevation: 593.09 ft North: 1897135.88 ft East: 1171421.19 ft Station: 7313+60.04 Offset: 3.9003 RT

Profile	Generation Soil AND ROCK	Sample Type recovery Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)) Sample Type recovery (ft)) Sample Type recovery (ft)) Sample No.
		23	20 27 46	4.92 S	14		DIFFICULT DRILLING AUGER REFUSAL 490.1 Boring terminated at 103.00 ft
	 Very dense, gray SILTY LOAM, trace to little gravel Damp to dry  90 -	<b>≥</b> 124	-50/5-	NP	12		
		25	-50/5-	NP	14		
3PJ WANGENG.GDT 8/12/16	HARD DRILLING 495.6 Very dense, gray DOLOSTONE fragments WEATHERED BEDROCK 100_	26 OTES	50/1	NP	11		
MANGENGINC 11000401.GPJ ag ag ag by and an age and an age ag age age age age age age age age age age	GENERAL N gin Drilling 02-21-2014 Con	DIES		ſ	)2-25	-201	
Dr	Illing Contractor Wang Testing Servi	•	-				
		appel					
Dr	Illing Method 2.25" HSA to 10', mud I						Depth to Water 🖳 🛛 🗛
MAN						-	The stratification lines represent the approximate boundary



between soil types; the actual transition may be gradual



Client

Project

Location

## **BORING LOG 10-RWB-04**

WEI Job No.: 1100-04-01

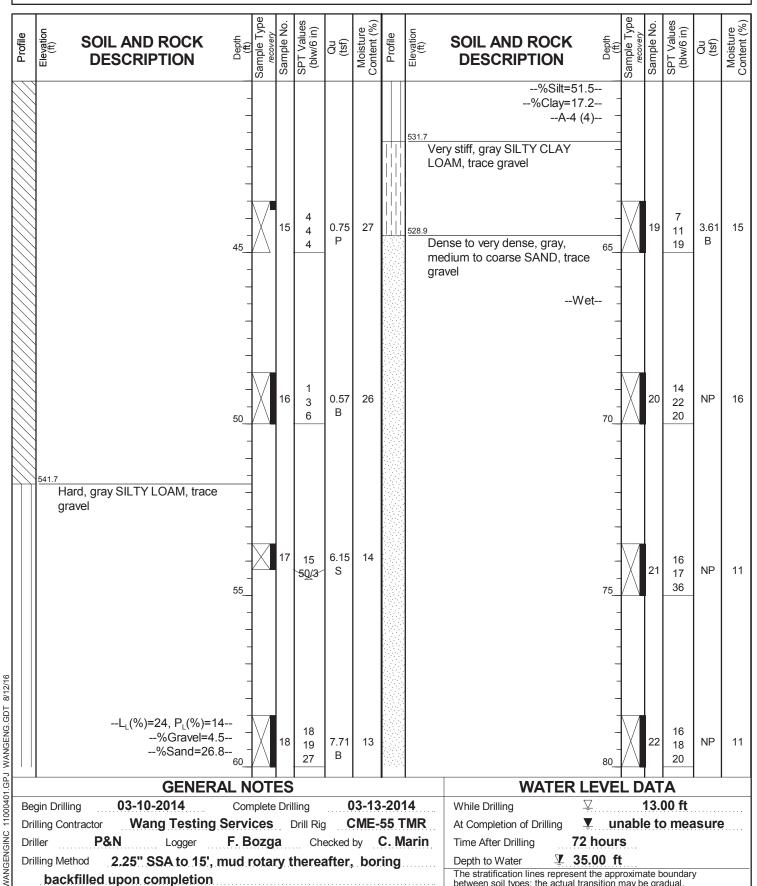
Page 2 of 3

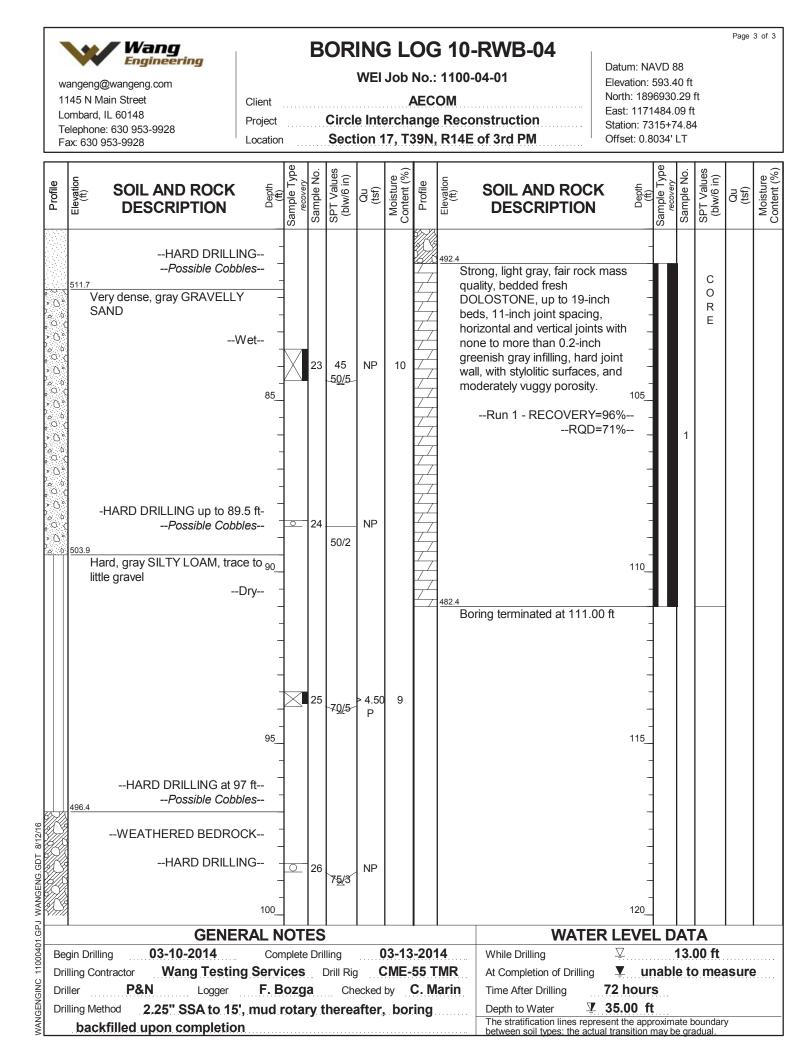
wangeng@wangeng.com 1145 N Main Street Lombard, IL 60148 Telephone: 630 953-9928 Fax: 630 953-9928

### AECOM **Circle Interchange Reconstruction** Section 17, T39N, R14E of 3rd PM

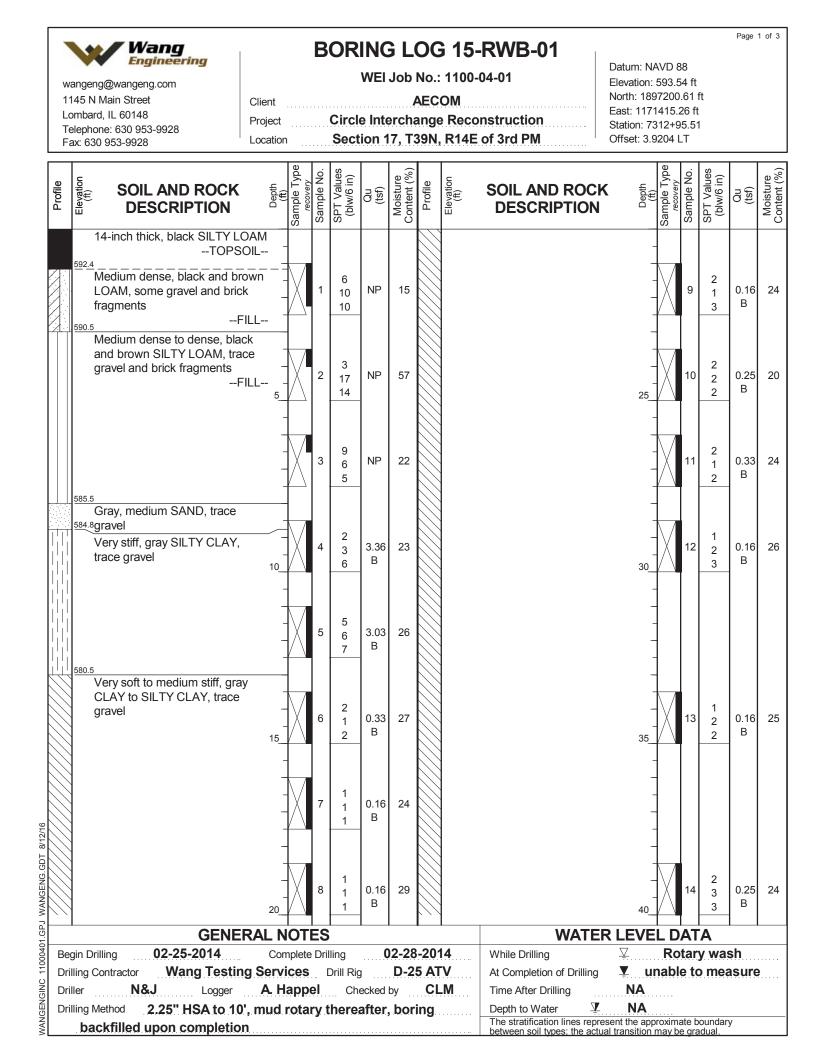
Datum: NAVD 88 Elevation: 593.40 ft North: 1896930.29 ft East: 1171484.09 ft Station: 7315+74.84 Offset: 0.8034' LT

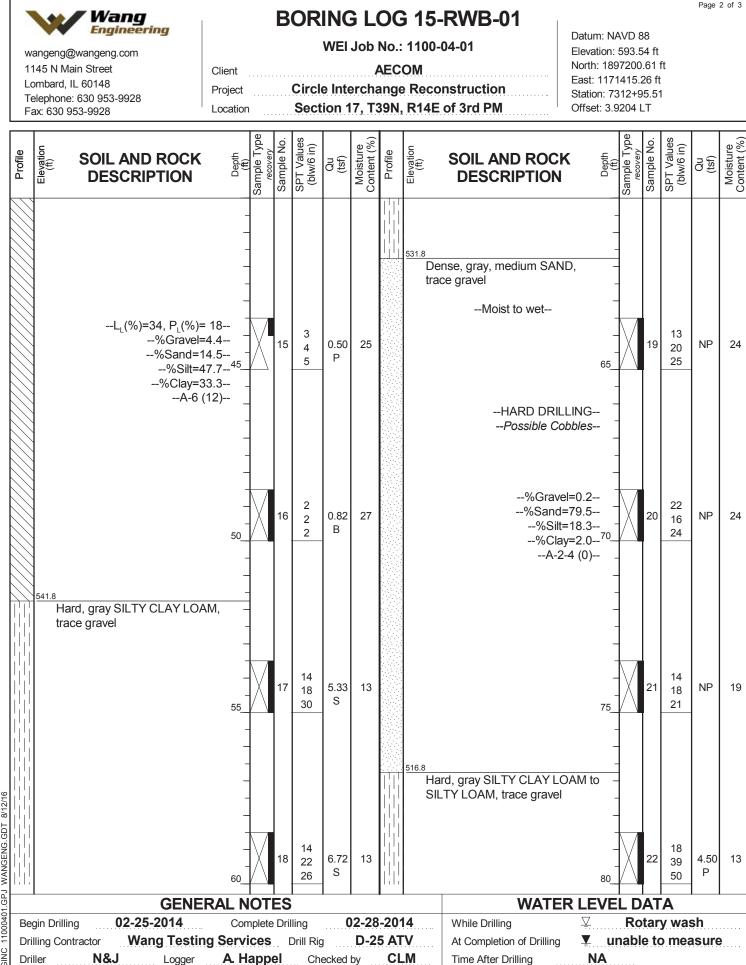
between soil types; the actual transition may be gradual











Depth to Water

V

The stratification lines represent the approximate boundary

between soil types; the actual transition may be gradual

NA

VANGENGINC 11000401.GPJ WANGENG.GDT 8/12/16

**Drilling Method** 

backfilled upon completion

2.25" HSA to 10', mud rotary thereafter, boring

Page 2 of 3



Client

Project

## **BORING LOG 15-RWB-01**

WEI Job No.: 1100-04-01

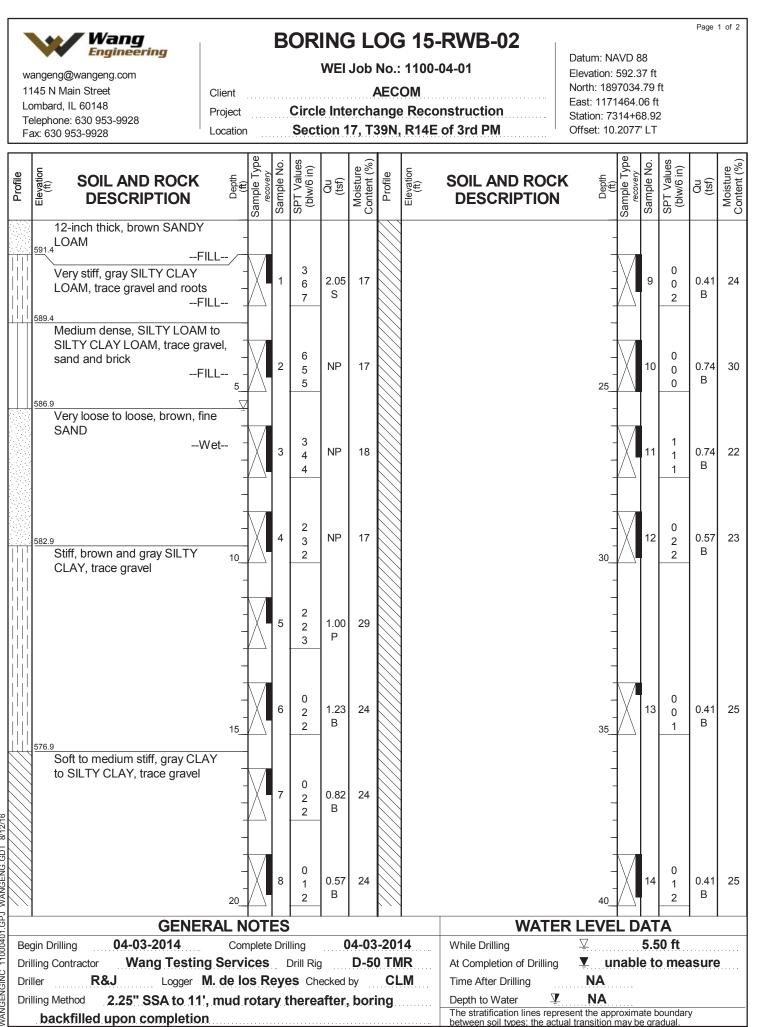
Page 3 of 3

wangeng@wangeng.com 1145 N Main Street Lombard, IL 60148 Telephone: 630 953-9928 Fax: 630 953-9928

## AECOM Circle Interchange Reconstruction

Datum: NAVD 88 Elevation: 593.54 ft North: 1897200.61 ft East: 1171415.26 ft Station: 7312+95.51 Offset: 3.9204 LT

F	ax: 630 9	953-9928	Location	۱ 		Sect		<u>/,  </u> ;	91N,	R14E	of 3rd Pivi	U	TSET: 3.9	204 L	. 1			
Profile	Elevation (ft)	SOIL AND F		Sample Type	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND DESCRIP		Depth (ft)	Sample Type	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
			- - - - - - 85_ - - - -		23	22 32 50	9.02 S	13										
	503.5 Bo	%	6, P <sub>L</sub> (%)=16 %Gravel=0.1 %Sand=11.7 %Silt=62.6 %Clay=25.6 A-4 (7) 90 t 90.00 ft          -		24	25 33 48	10.25 S	13										
WANGENGING 11000401.GPJ WANGENG.GDT &12/16			- 95_ - - - - - - - - - - - - - - - - - - -															
1.GF			GENERAL N	ют	ËS					L	V	VATER I	EVE	LD	AT	Α		
Be	egin Drillii			nplete			C	2-28	-201	4	While Drilling		<u> </u>			y was	sh	
	illing Cor		g Testing Servi			-		D-2			At Completion of	-	<b>⊈</b> ur	nabl	e to	mea	isure	
	iller		Logger A.H							M	Time After Drillin		NA					
ז Dr אופי	illing Met	nod 2.25" HS filled upon cor	A to 10', mud		-				-		Depth to Water The stratification I between soil types	ines represen	NA it the app	roxima	ate bo	oundary	/	
2	Dack	med abou col	uhieriou								between soil types	s: the actual tr	ansition r	nav be	e ara	dual. Í		



WANGENGINC 11000401.GPJ WANGENG.GDT 8/12/16



## **BORING LOG 15-RWB-02**

WEI Job No.: 1100-04-01

Page 2 of 2

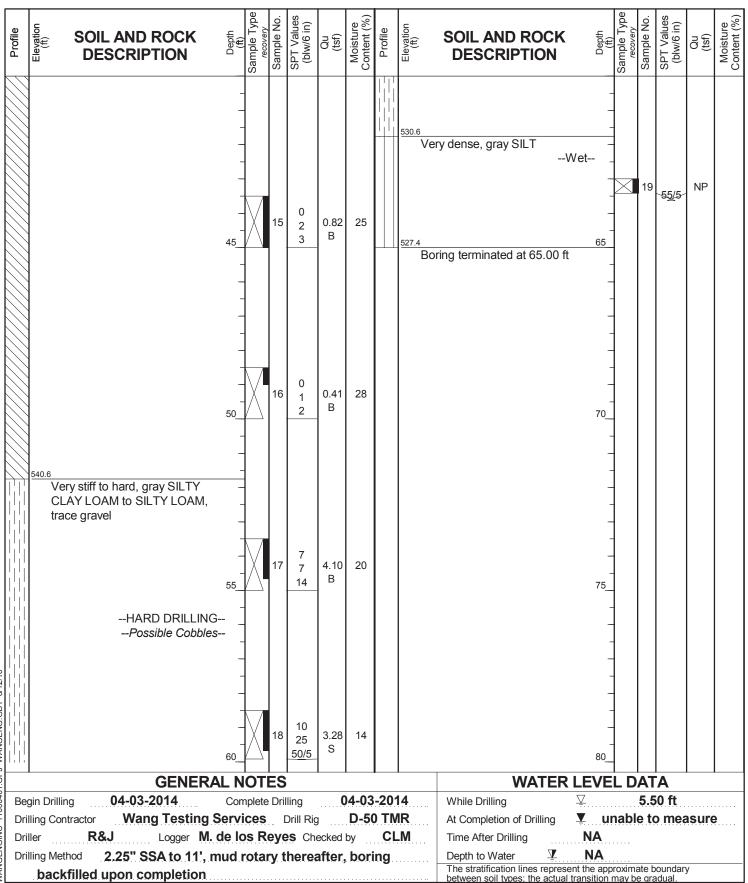
wangeng@wangeng.com 1145 N Main Street Lombard, IL 60148 Telephone: 630 953-9928 Fax: 630 953-9928

 Client
 AECOM

 Project
 Circle Interchange Reconstruction

 Location
 Section 17, T39N, R14E of 3rd PM

Datum: NAVD 88 Elevation: 592.37 ft North: 1897034.79 ft East: 1171464.06 ft Station: 7314+68.92 Offset: 10.2077' LT



WANGENGINC 11000401.GPJ WANGENG.GDT 8/12/16



WEI Job No.: 1100-04-01

Page 1 of 2

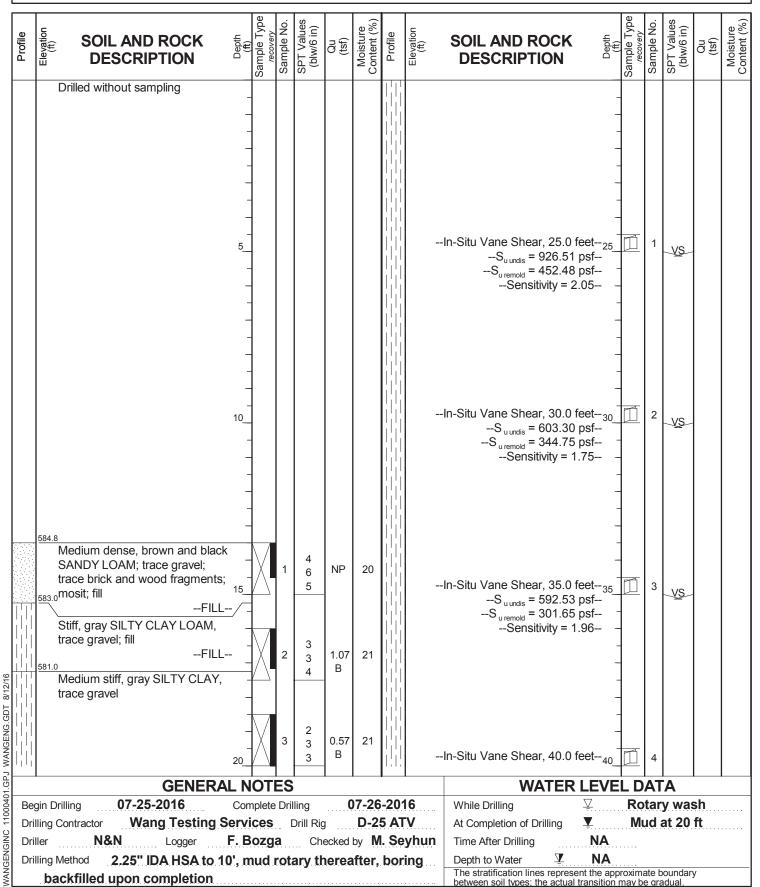
wangeng@wangeng.com 1145 N Main Street Lombard, IL 60148 Telephone: 630 953-9928 Fax: 630 953-9928

 Client
 AECOM

 Project
 Circle Interchange Reconstruction

 Location
 Section 17, T39N, R14E of 3rd PM

Datum: NAVD 88 Elevation: 598.29 ft North: 1897455.09 ft East: 1171356.40 ft Station: Offset:



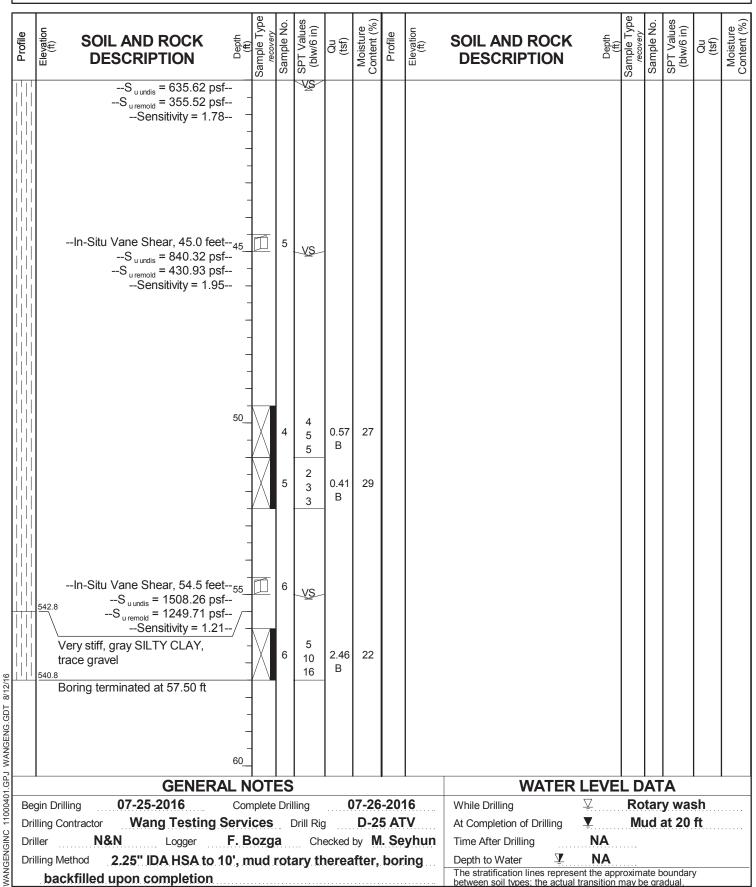


WEI Job No.: 1100-04-01

wangeng@wangeng.com 1145 N Main Street Lombard, IL 60148 Telephone: 630 953-9928 Fax: 630 953-9928

# Client AECOM Project Circle Interchange Reconstruction Location Section 17, T39N, R14E of 3rd PM

Datum: NAVD 88 Elevation: 598.29 ft North: 1897455.09 ft East: 1171356.40 ft Station: Offset:





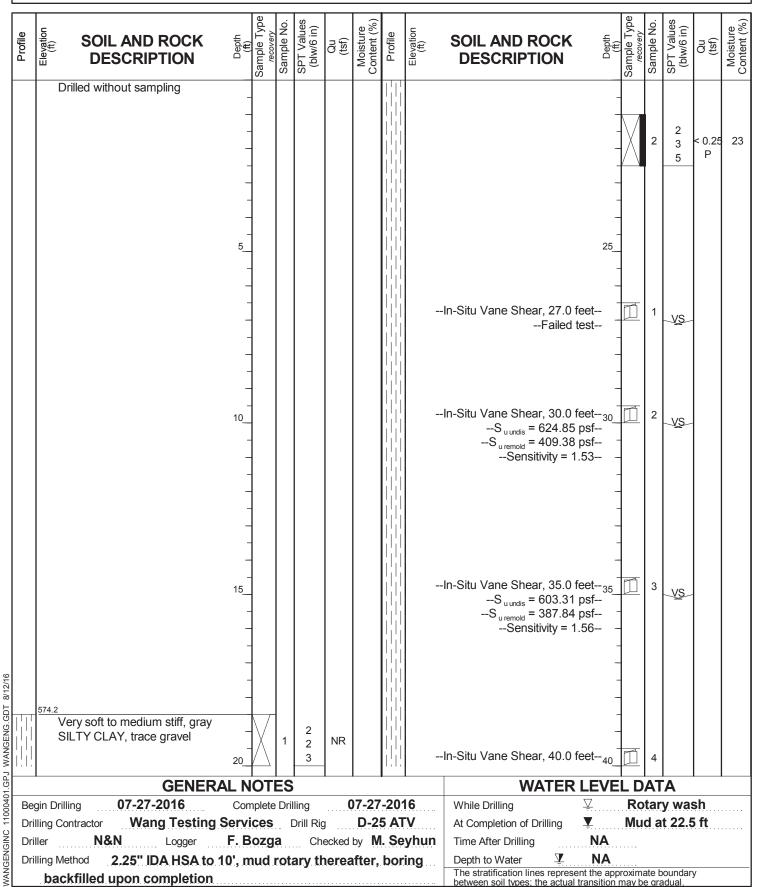
WEI Job No.: 1100-04-01

Page 1 of 2

wangeng@wangeng.com 1145 N Main Street Lombard, IL 60148 Telephone: 630 953-9928 Fax: 630 953-9928

# Client AECOM Project Circle Interchange Reconstruction Location Section 17, T39N, R14E of 3rd PM

Datum: NAVD 88 Elevation: 592.70 ft North: 1897206.55 ft East: 1171441.79 ft Station: Offset:





WEI Job No.: 1100-04-01

wangeng@wangeng.com 1145 N Main Street Lombard, IL 60148 Telephone: 630 953-9928 Fax: 630 953-9928

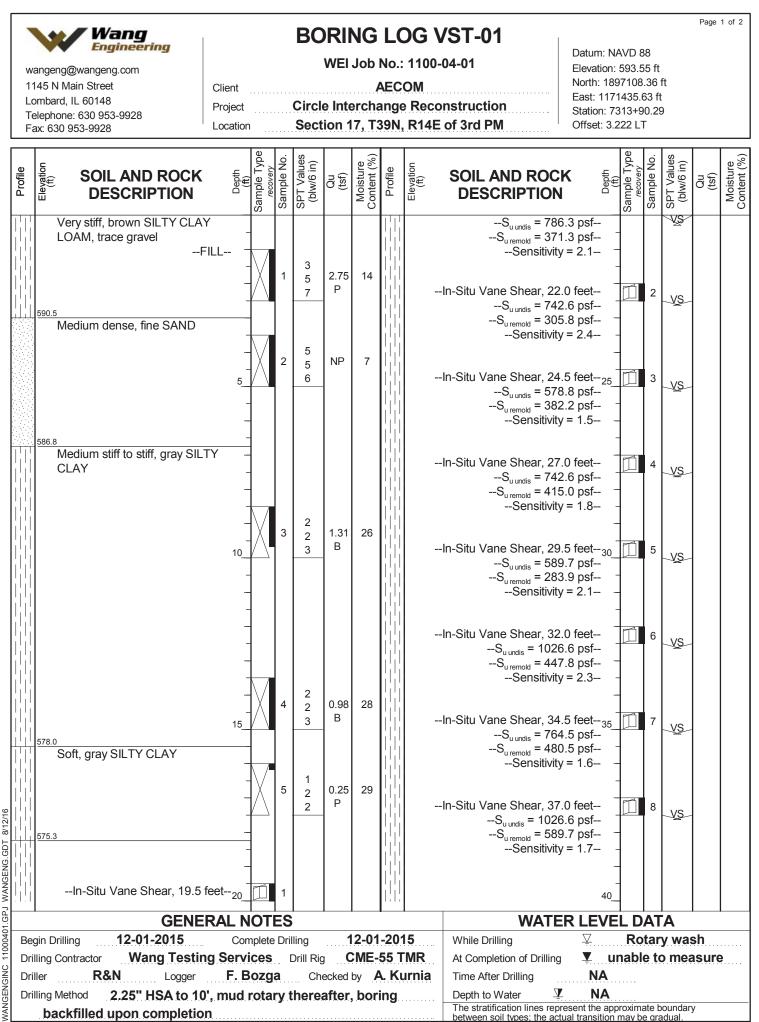
 Client
 AECOM

 Project
 Circle Interchange Reconstruction

 Location
 Section 17, T39N, R14E of 3rd PM

Datum: NAVD 88 Elevation: 592.70 ft North: 1897206.55 ft East: 1171441.79 ft Station: Offset:

Bigure         SOIL AND ROCK DESCRIPTION         Use of the second of the second
In-Situ Vane Shear, 45.0 feet- Sundia = 1422.08 psf- Sensitivity = 1.64- In-Situ Vane Shear, 47.5 feet- Sundia = 1422.08 psf- Sundia = 1422.08 psf- Sundia = 1422.07 psf- Sun
In-Situ Vane Shear, 47.5 feet- S $_{undis} = 1422.08 \text{ psf}-$ S $_{urenoid} = 775.68 \text{ psf}-$ Sensitivity = 1.83 Surenoid = 775.68 psf- S $_{urenoid} = 775.68 \text{ psf}-$ S $_{urenoid} = 775.68 \text{ psf}-$ Sensitivity = 1.83 Sensitivity = 1.
$\begin{array}{c}S_{u \text{ undis}} = 1422.08 \text{ psf-} \\S_{u \text{ remold}} = 775.68 \text{ psf-} \\Sensitivity = 1.83 \\S_{u \text{ undis}} = 1422.07 \text{ psf-} \\S_{u \text{ undis}} = 1422.07 \text{ psf-} \\S_{u \text{ remold}} = 775.68 \text{ psf-} \\S_{\text{ undis}} = 775.68 \text{ psf-} \\S_{\text{ ermold}} = 1.83 \\S_{\text{ ermold}} = 775.68 \text{ psf-} \\S_{\text{ ermold}} = 75.68  p$
$\begin{array}{c c}S_{u \text{ undis}} = 1422.07 \text{ psf} \\S_{u \text{ remold}} = 775.68 \text{ psf} \\Sensitivity = 1.83 \\Sensi$
540 <sup>2</sup> Hard, gray SILTY CLAY Boring terminated at 52.50 ft
Begin Drilling       07-27-2016       Complete Drilling       07-27-2016         Begin Drilling       07-27-2016       Complete Drilling       07-27-2016         Drilling Contractor       Wang Testing Services       Drill Rig       D-25 ATV         Drilling Method       2.25" IDA HSA to 10', mud rotary thereafter, boring       Depth to Water       NA         Depth to Water       NA         The stratification lines represent the approximate boundary between solit bytes; the actual transition may be gradual.
GENERAL NOTES WATER LEVEL DATA
Begin Drilling 07-27-2016 Complete Drilling 07-27-2016 While Drilling ♀ Rotary wash
Drilling Contractor Wang Testing Services Drill Rig D-25 ATV At Completion of Drilling V Mud at 22.5 ft
Zoriller       N&N       Logger       F. Bozga       Checked by       M. Seyhun       Time After Drilling       NA         Unilling Method       2.25" IDA HSA to 10', mud rotary thereafter, boring       Depth to Water       V       NA





Client

Project

## **BORING LOG VST-01**

WEI Job No.: 1100-04-01

**Circle Interchange Reconstruction** 

Page 2 of 2

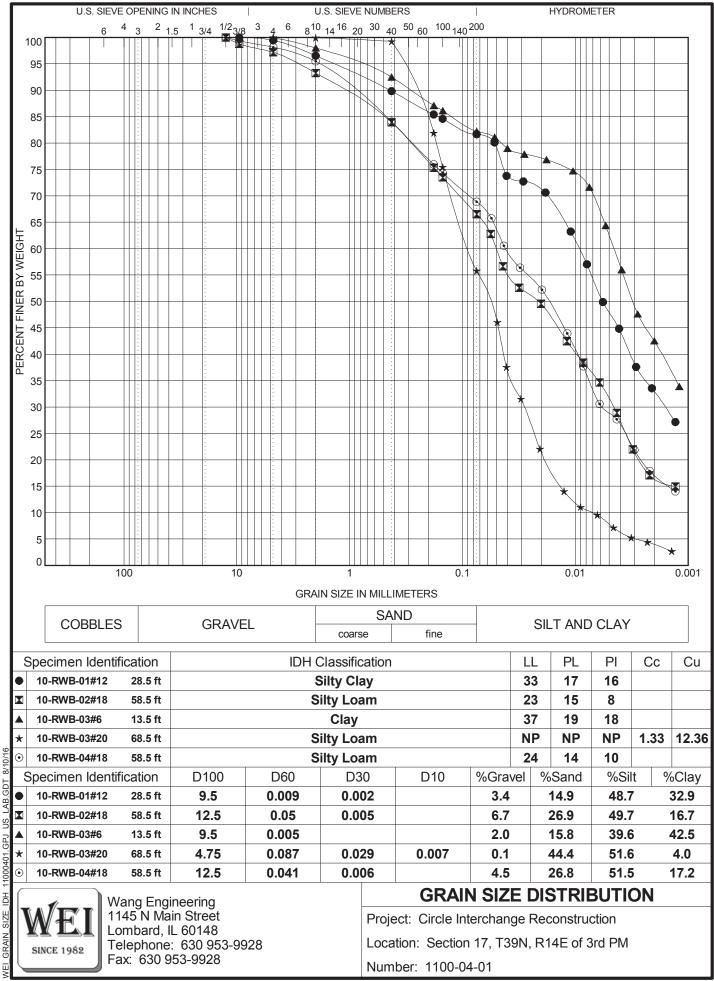
wangeng@wangeng.com 1145 N Main Street Lombard, IL 60148 Telephone: 630 953-9928

## AECOM

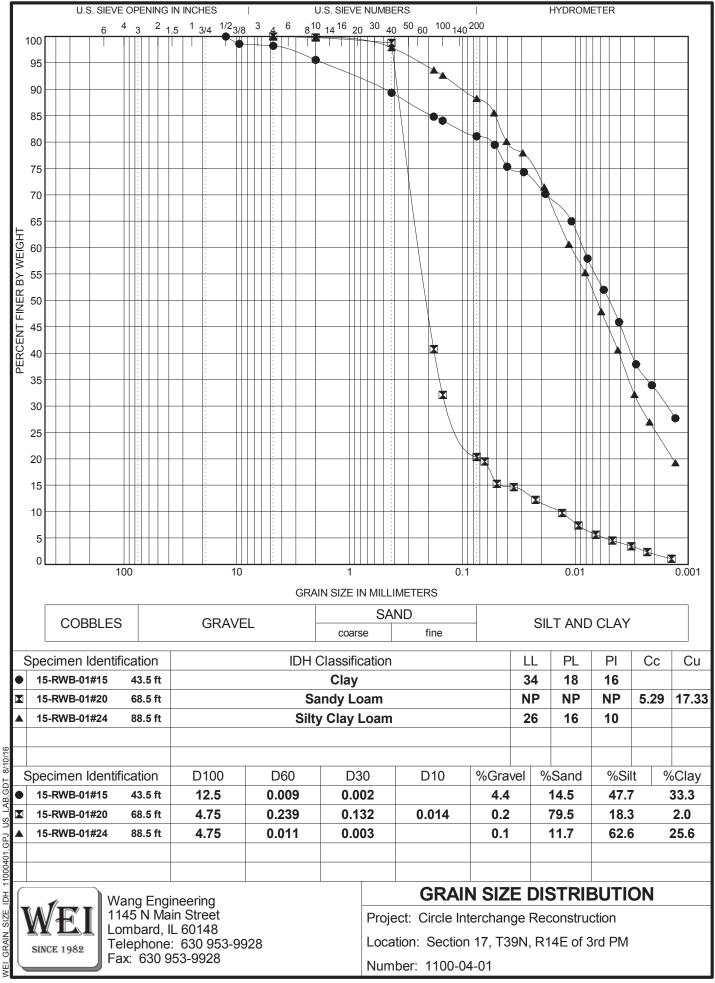
Datum: NAVD 88 Elevation: 593.55 ft North: 1897108.36 ft East: 1171435.63 ft Station: 7313+90.29 Offset: 3.222 LT

between soil types; the actual transition may be gradual.

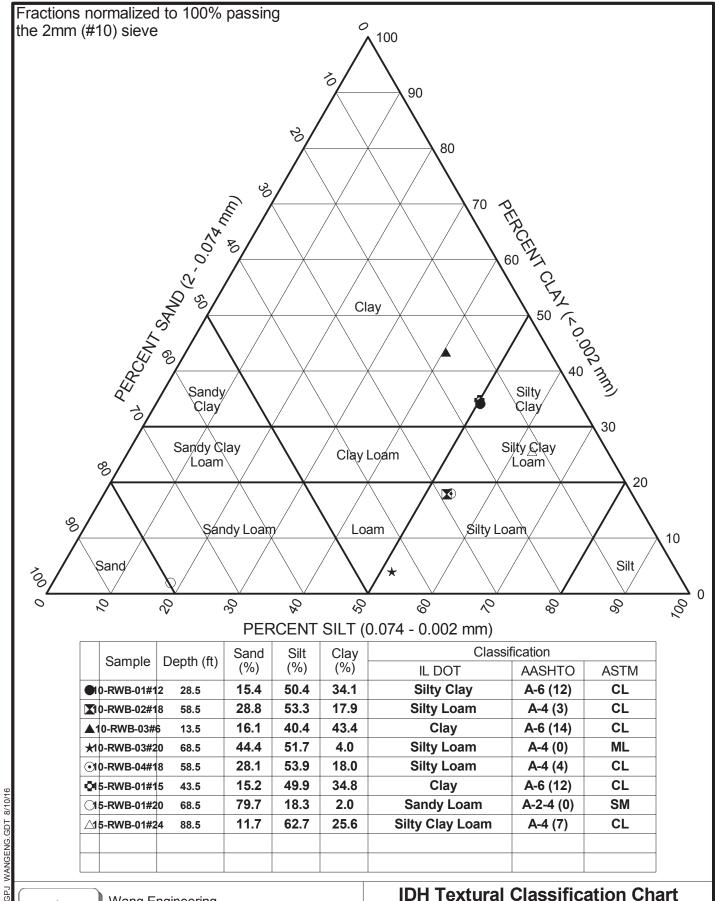
		0 953-9928	Location		Sect	ion 1	7, T3	39N	R14E	of 3rd PM	Offset: 3.2	222 L	Г			
Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ft) Sample Type recovery	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)	Profile	Elevation (ft)	SOIL AND ROCK DESCRIPTION	Depth (ff)	Sample Type	Sample No.	SPT Values (blw/6 in)	Qu (tsf)	Moisture Content (%)
MANGENGINC 11000401.GPJ WANGENG.GDT 8/12/16	544.0	Equipment Slip In-Situ Vane Shear, 46.5 S <sub>u undis</sub> = 1070.2 S <sub>u remold</sub> = 633.4 Sensitivity = In-Situ Vane Shear, 49.0 S <sub>u undis</sub> = 1157.6 S <sub>u remold</sub> = 611.6 Sensitivity = Boring terminated at 49.50 ft	ped45	9	VS VS											
CPJ.		GENE		ES						WATE	R LEVE		AT	А		
00000 Be	egin Dr		Complete			1	2-01	-20′	15	While Drilling	Į			y was	sh	
F Dr	rilling C	Contractor Wang Testir	-		Drill Rig	, <b>C</b>	ME-	55 T	MR	At Completion of Drilling				o mea		
N Dr	riller	R&N Logger	F. Bozga	a	Ch	ecked	by 📕	. Kı	urnia	Time After Drilling	NA					
Dr	-	Alethod 2.25" HSA to 10		-				-		Depth to Water	NA		ote !			
WAN	ba	ckfilled upon completio	<b>n</b>							The stratification lines repre- between soil types; the actu	sent the app al transition	roxima mav b	ate b e ara	oundar adual.	y	



<u>v</u> d C C 1000401 НО SIZE GRAIN



<u>v</u> 11000401.GPJ Ы SIZE GRAIN



**SINCE 1982** 

HO

ų

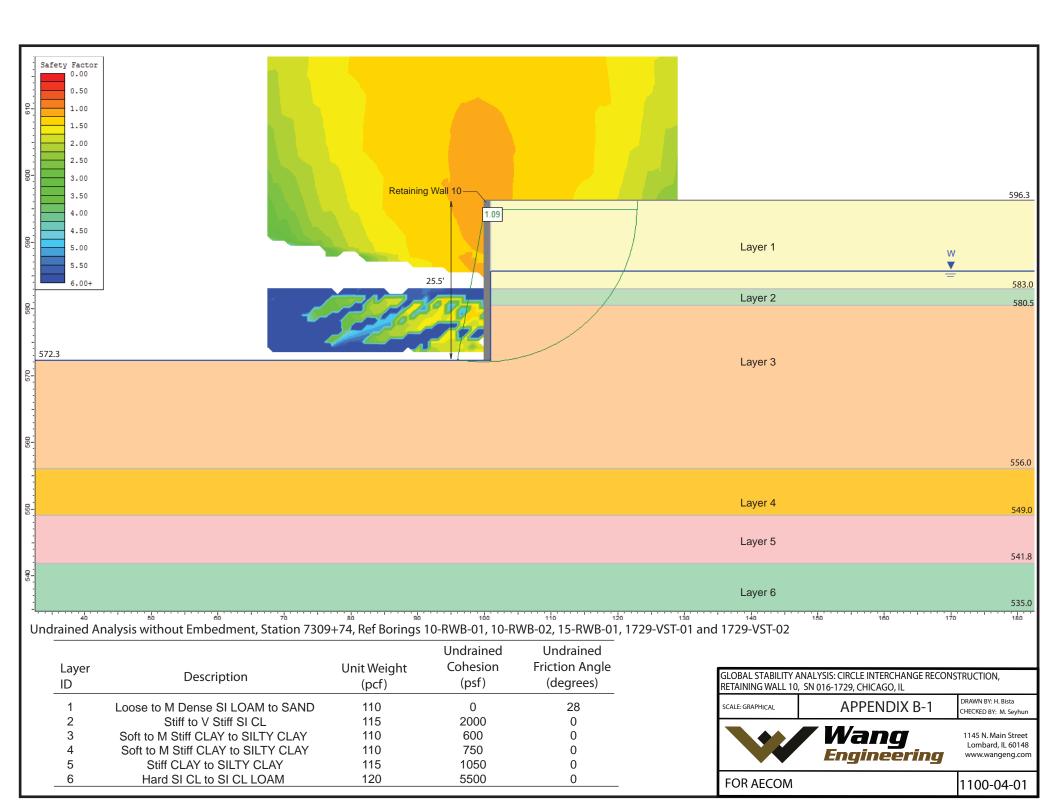
Wang Engineering 1145 N Main Street Lombard, IL 60148 Telephone: 630 953-9928 Fax: 630 953-9928

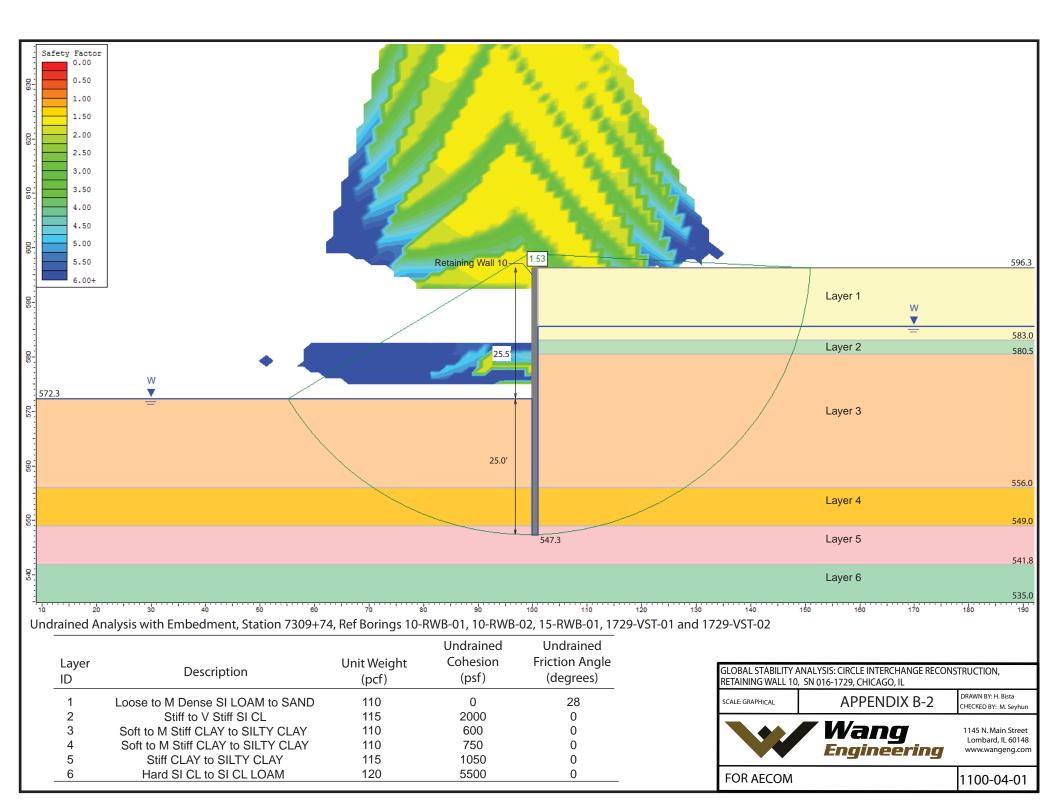
## **IDH Textural Classification Chart**

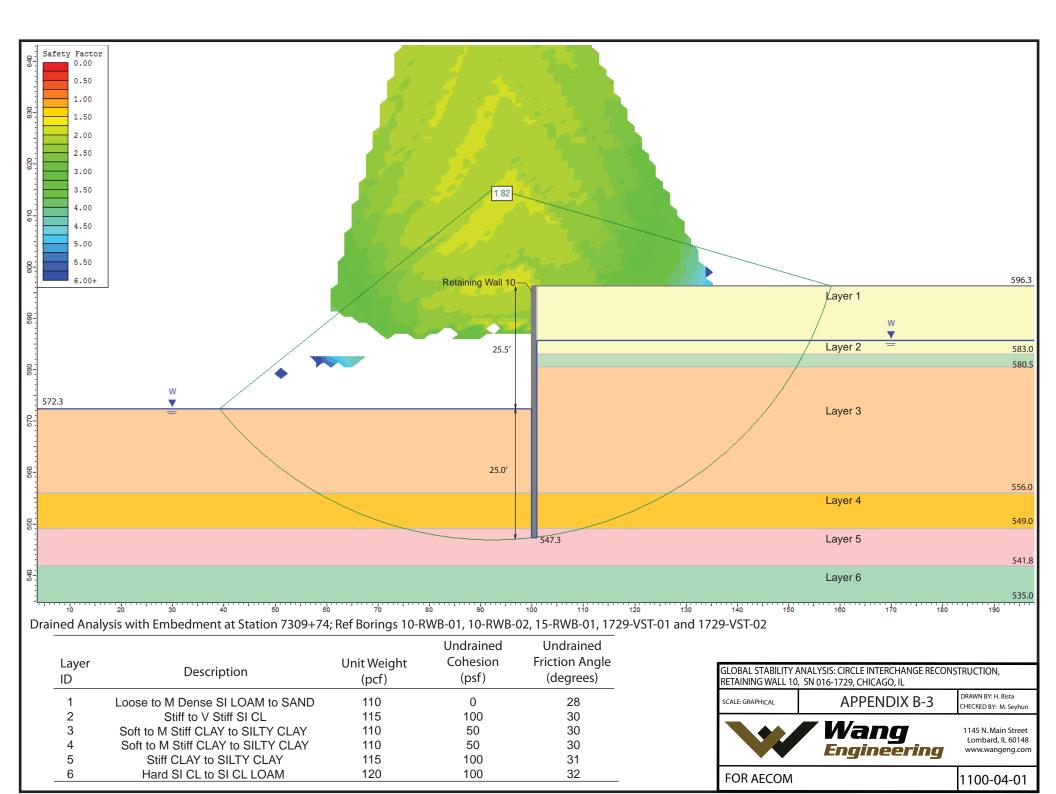
Project: Circle Interchange Reconstruction Location: Section 17, T39N, R14E of 3rd PM Number: 1100-04-01



# **APPENDIX B**

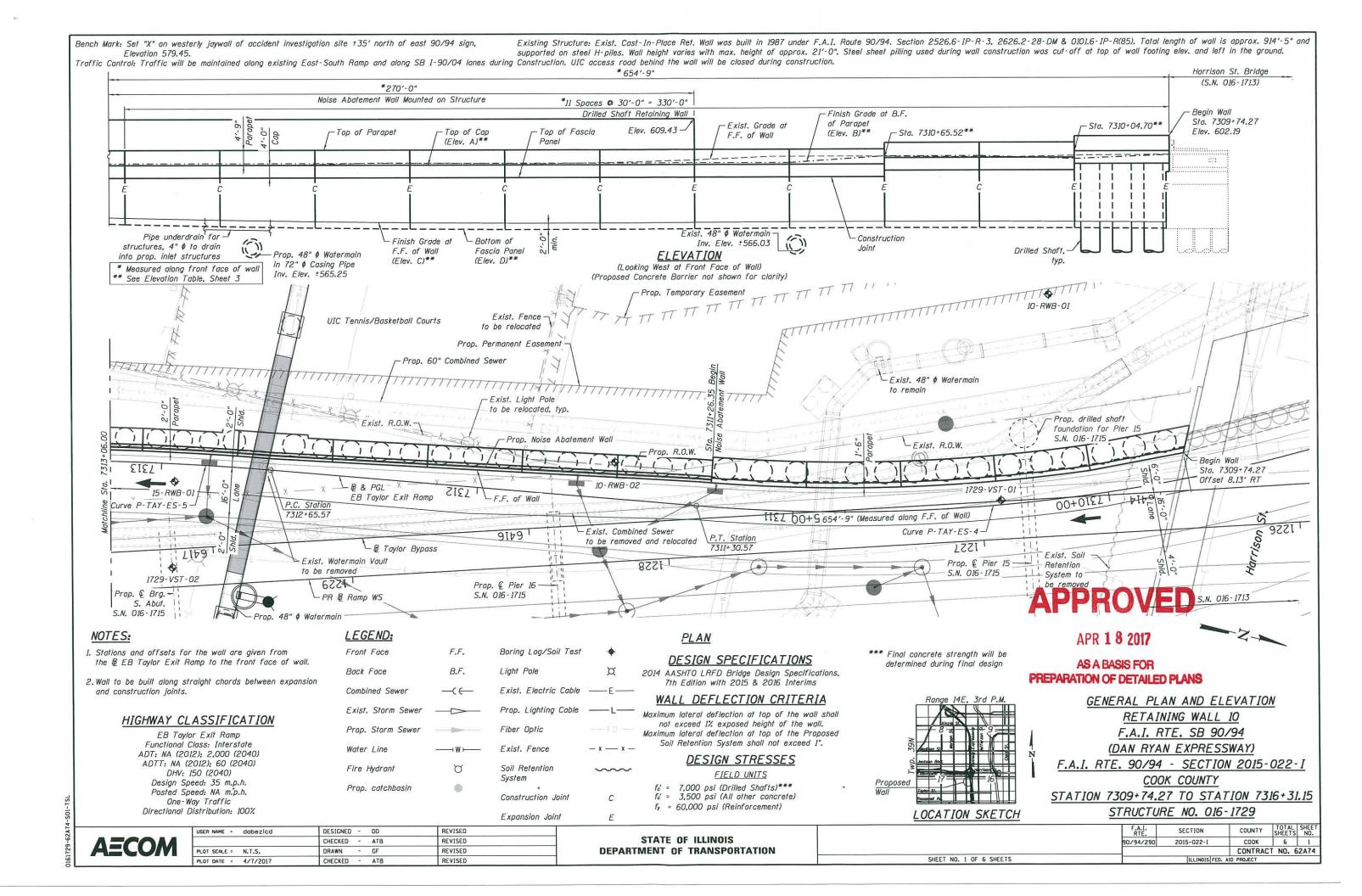


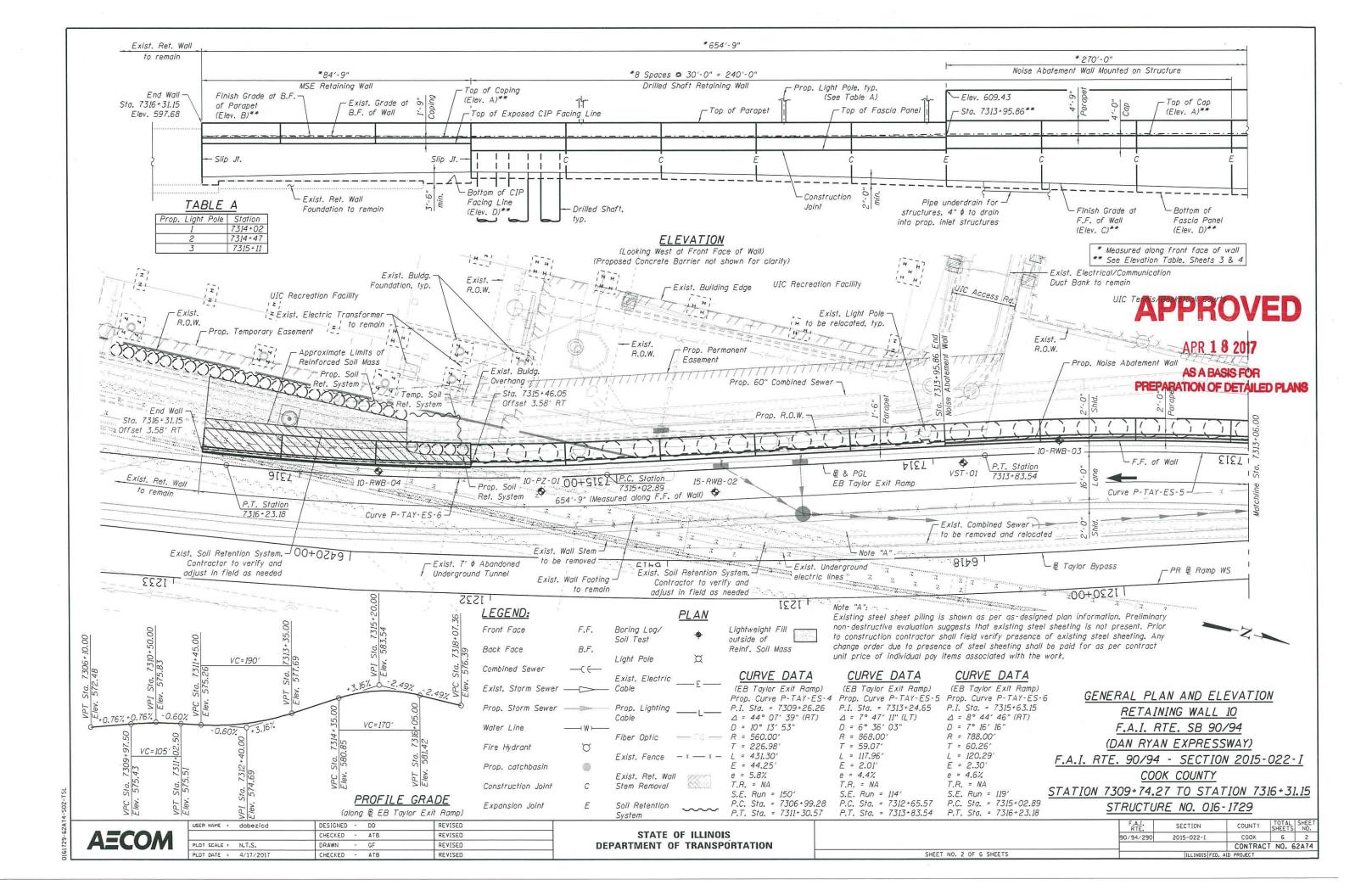


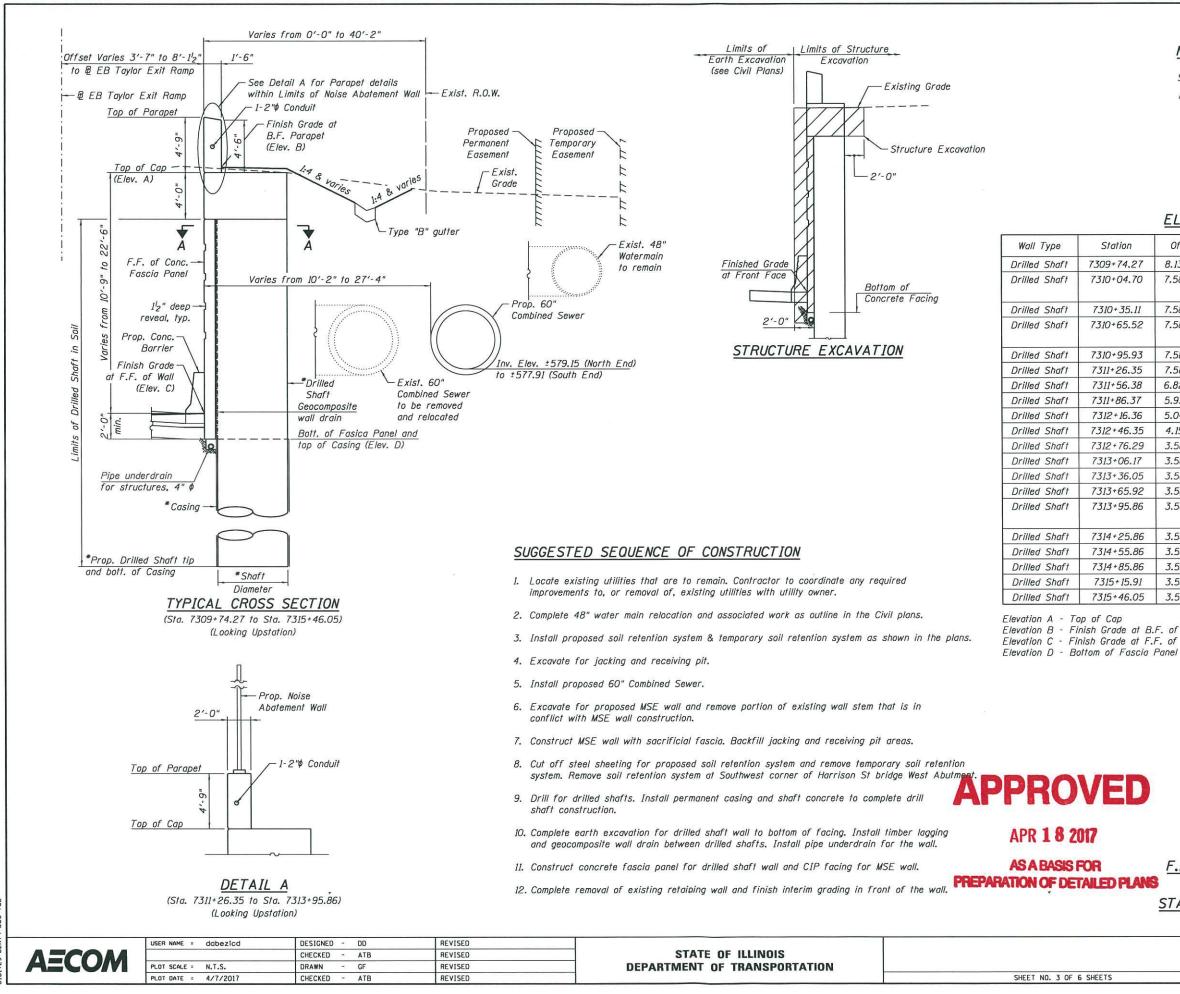




# **APPENDIX C**







## NOTES:

See Sheet 5 for Section A-A.

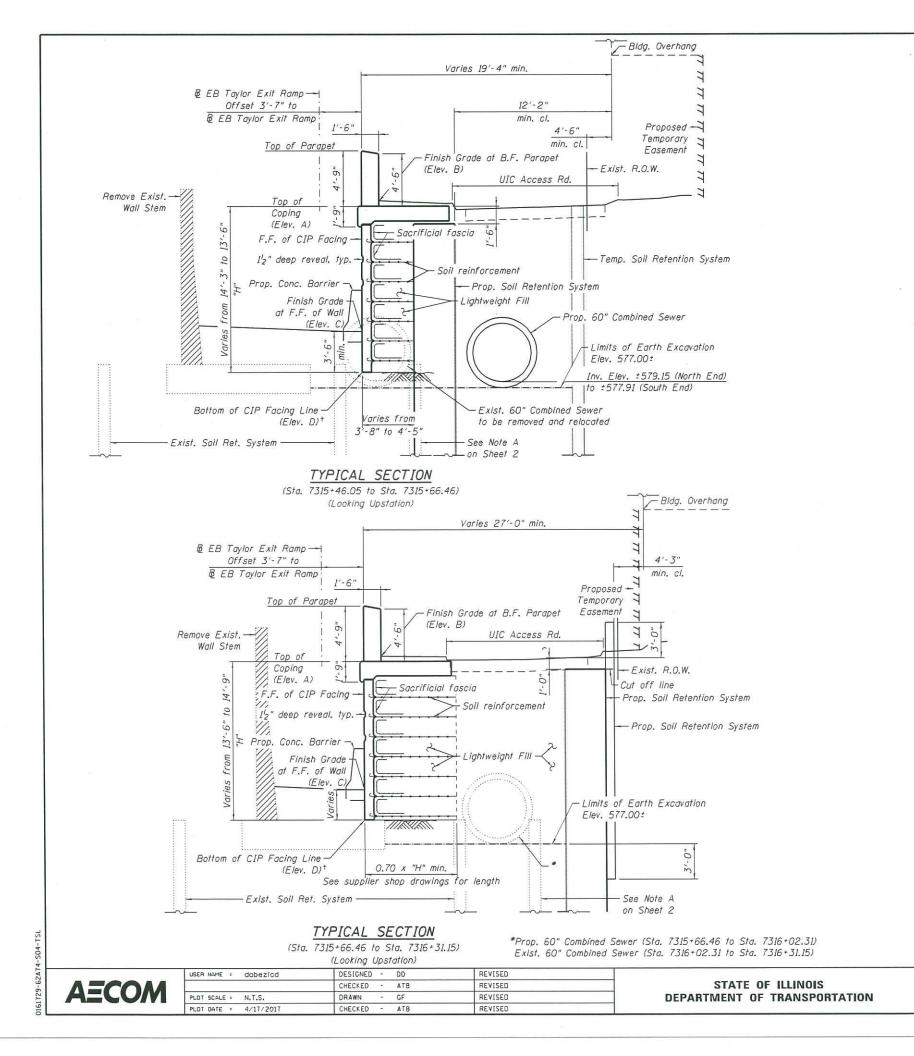
\* Drilled shaft diameter, spacing, tip elevation & casing to be determined during final design.

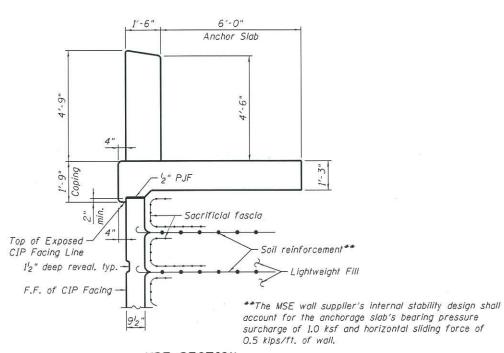
	No. 199				
Station	Offset	Elevation A	Elevation B	Elevation C	Elevation D
309+74.27	8.13' RT	597.44	596.21	574.91	572.91
7310+04.70	7.58' RT	597.44 (N)	595.02	575.13	573.13
		595.44 (S)			
7310+35.11	7.58' RT	595.44	596.00	575.26	573.26
7310+65.52	7.58' RT	595.44 (N)	596.00	575.31	573.31
3		593.43 (S)			
7310+95.93	7.58' RT	593.43	593.99	575.29	573.29
7311+26.35	7.58' RT	593.43	593.99	575.13	573.13
7311+56.38	6.82' RT	593.43	593.99	575.01	573.01
7311+86.37	5.93' RT	593.43	593.99	575.02	573.02
7312+16.36	5.04' RT	593.43	593.99	575.21	573.21
7312+46.35	4.15' RT	593.43	593.99	575.57	573.57
7312+76.29	3.58' RT	593.43	593.99	576.10	574.10
7313+06.17	3.58' RT	593.43	593.99	576.80	574.80
7313+36.05	3.58' RT	593.43	593.99	577.65	575.65
7313+65.92	3.58' RT	593.43	593.99	578.59	576.59
7313+95.86	3.58' RT	593.43 (N)	593.99	579.54	577.54
		592.93 (S)			
7314+25.86	3.58' RT	592.93	593.49	580.48	578.48
7314+55.86	3.58' RT	592.93	593.49	581.34	579.34
7314+85.86	3.58' RT	592.93	593.49	581.92	579.92
7315+15.91	3.58' RT	592.93	593.49	582.04	580.04
7315+46.05	3.58' RT	592.93	593.49	582.22	580.22

#### ELEVATION TABLE

Elevation B - Finish Grade at B.F. of Parapet Elevation C - Finish Grade at F.F. of Wall

	E	LEVATI	ON TABLE	AND								
<b>ED</b>	DRILL	ED SHA	AFT WALL	SECTIO	V							
		RETAIN	ING WALL	10	-							
	1	F.A.I. R	TE. SB 90	/94								
	(D	AN RYA	N EXPRESS	SWAY)								
R	F.A.I. RTE.	90/94	- SECTIO	N 2015-	022-	Ι						
LED PLANS												
	STATION 73	09+74.2	7 TO STAT	TION 73.	16+31	.15						
	<u>57</u>	RUCTUF	RE NO. 016	1729								
		F.A.I. RTE.	SECTION	COUNTY	TOTAL	SHEET NO.						
		90/94/290	2015-022-I	СООК	6	3						
				CONTRAC	T NO. 6	2A74						
IEETS		1.	ILLINOIS FED.	AID PROJECT								





Wall Type	Station	Offset	Elevation A	Elevation B	Elevation C	Elevation D
MSE	7315+46.05	3.58' RT	592.93	593.49	582.22	578.72
MSE	7315+76.18	3.58' RT	592.93	593.49	581.91	579.44
MSE	7316+06.32	3.58' RT	592.93	593.49	581.31	579.44
MSE	7316+31.15	3.58' RT	592.93	593.49	580.69	578.19

Elevation A - Top of Coping Elevation B - Finish Grade at B.F. of Parapet Elevation C - Finish Grade at F.F. of Wall Elevation D - Bottom of CIP Facing Line

APPROVED

APR 1 8 2017

AS A BASIS FOR PREPARATION OF DETAILED PLANS

SHEET NO. 4 OF 6 SHE

MSE SECTION

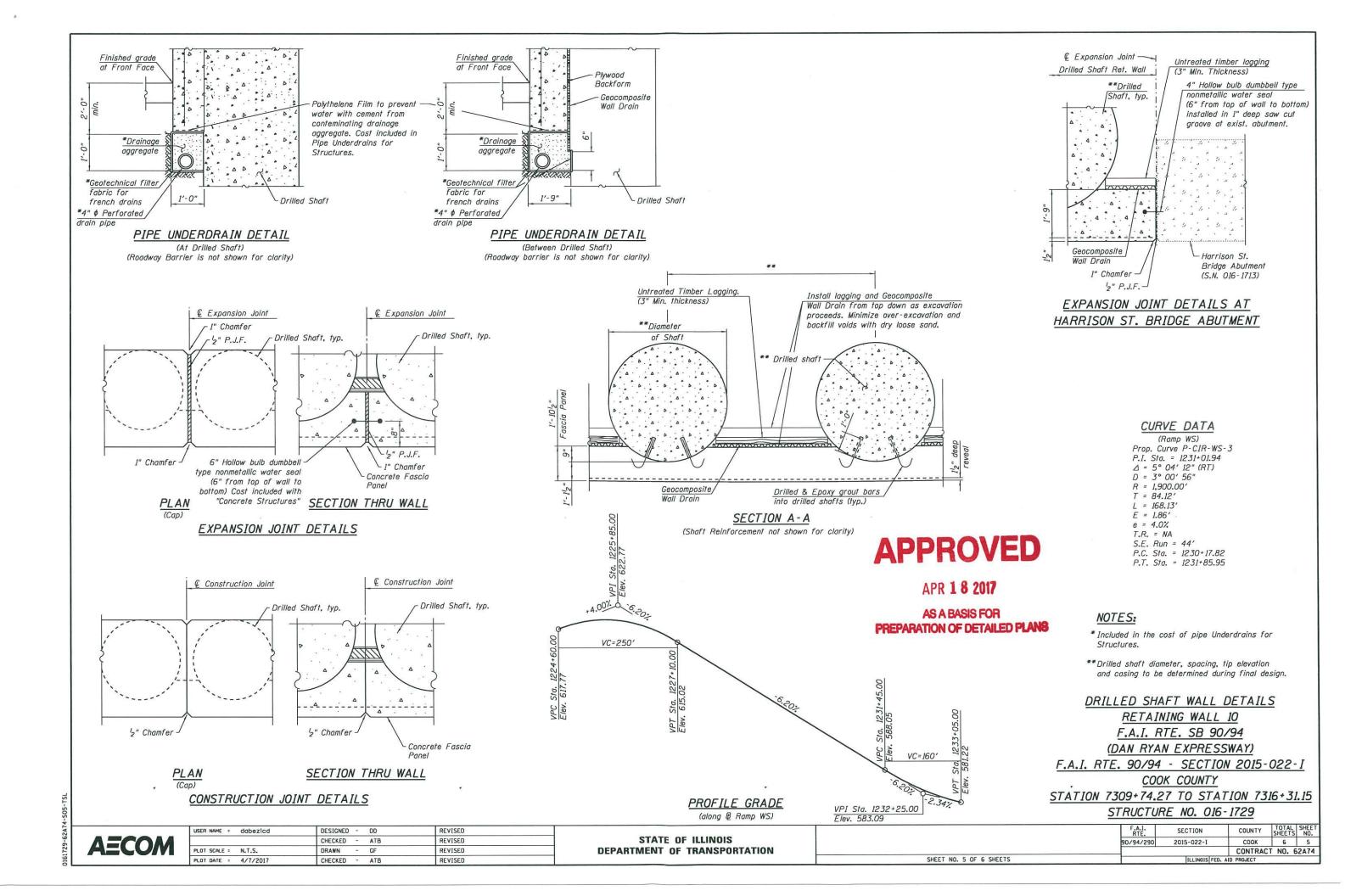
(Looking Upstation)

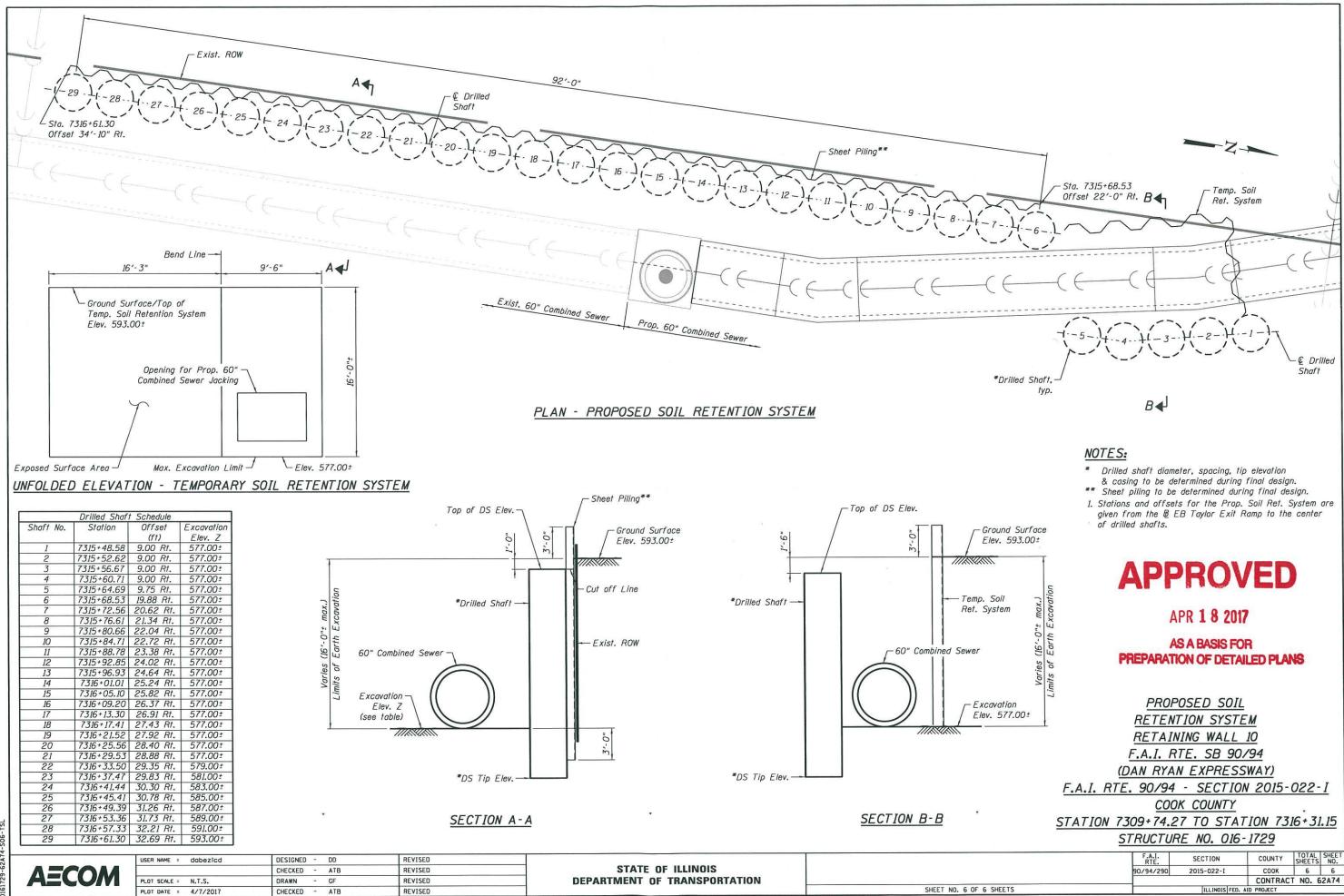
### ELEVATION TABLE

### NOTES:

- + From Sta. 7315+61.16 to Sta. 7316+31.15 MSE Panels are supported on the existing Ret. Wall footing.
- 1. For Proposed & Temporary Soil Retention System see Sheet 6.

	ELEVATI	ON TABLE	AND										
	MSE WA	ALL SECTI	ON										
	RETAIN	IING WALL	10										
	F.A.I. RTE. SB 90/94												
	(DAN RYAN EXPRESSWAY)												
	F.A.I. RTE. 90/94 - SECTION 2015-022-1												
	COOK COUNTY												
	STATION 7309+74.27 TO STATION 7316+31.15												
	STRUCTUR	RE NO. 016	- 1729										
	F.A.I. RTE.	SECTION	COUNTY	TOTAL	SHEET NO.								
	90/94/290	2015-022-1	COOK	6	4								
			CONTRACT	NO. 6	2A74								
HEETS		ILLINOIS FED.	AID PROJECT										





SHEET NO. 6 OF 6 SHEETS



# **APPENDIX D**



2/9/2017 of 5 Date: Sheet: Calculation By: N. Balakumavan Approved By: M. Seyhan Engineering Project Number: 1100-04-01 Client Name: AECOM 1145 North Main Street Project Name: Circle Interchange Lombard, Illinois 60148 Phone: (630)-953-9928 Wal 5N 016-1729 Estimates Ground Movement the surface ground movement To estimate Purpose. Recreation Facility located at LITC Wall 10 induced by the OF West tot the proposed wall los Novemer type wall shall and lagging Drilled Reference (DClough, W and O'Rourke (1990) movement of " Construction induced n-sity Walls Ou, C.y, H.sieh, PE, and Chev. D (1993) (2)" Charactertics of ground surface settlements during excavation " Canadian Geotechnical Journel", V.30, P 758-767 3 J.H., X.U.Z.H, and Wang W.D (2010) Nang Walp Ground Movements Odue to and eep foundations in Shanahae Soft Soils" Journal of Geolecha Geornary Engineering, P985-994 Assumptions. LITE Recreation Facility 1) 15 26 feet away from Wall 10's drined shaft and Lagging Walta 7314100 Height of Wall Maximum = 17 feet no existing upall There is 3) behind Wall 10 Max. lateral displacement Notat 2005 Of Wal Ground Surface settlement Max. Ground surface Settlement



Date: \_2/9/2017 \_\_\_\_\_ Sheet: <u>2</u> of \_\_\_\_\_ Calculation By: N. Bala Kumara Mpproved By: M. Seyha Engineering Project Number: 1100-04-01 Client Name: AECON Project Name: \_\_\_\_\_ Circle Interchange 1145 North Main Street Lombard, Illinois 60148 Phone: (630)-953-9928 Walt ()3N 016-1729 Max Design Criteria: Shm 0.5% of Wall is height in ches. 02 Evaluations 00 a ratio Sum = 1.6 , Usiz From Tigure 6.14 Spm Sym= 1.02 inches obtain Then Ur 26 = 0 1.529 for -17 Method Clough and O'Rourke 1990, - 0.4 Ob Jaim SV Svm 0.4×1.02= 0.41 inches 0.4 inches Say Method SV Obtain 0.4 1.62 Inches S.4 inches

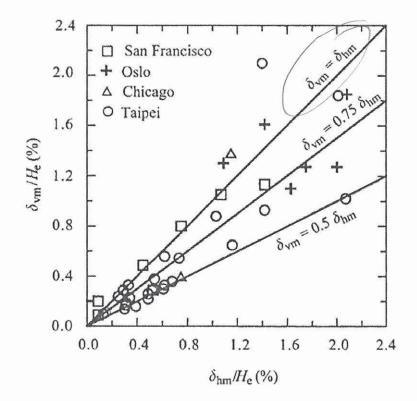


Figure 6.14 Maximum ground surface settlement and lateral wall deflection (Ou et al., 1993).

OU, C.-Y., HSIEH, P.-G., AND CHIOU, D.-C., 1993, Characteristics of ground surface settlement during excavation: Canadian Geotechnical Journal, v. 30, p. 758-767.

N

3/5

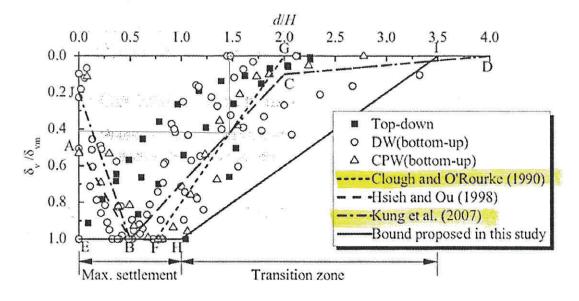


Fig. 11. Relationship between ground settlement normalized by maximum settlement and normalized distance from wall

WANG, J., XU, Z., AND WANG, W., 2009, Wall and ground movements due to deep excavations in Shanghai soft soils Journal of Geotechnical and Geoenvironmental Engineering, v. 136, p. 985-994.

4/5

