STRUCTURE GEOTECHNICAL REPORT

085-0504

Existing SN 085-0002

US 67 over Bluff Ditch **Section FAP 310 Schuyler County**

D-96-072-17

Contract 72K08

Prepared By: Brian Laningham

IDOT Region 4 District 6

Geotechnical Unit

217-782-6709

Date: May 9, 2019

Prepared For: Poepping, Stone,

Bach & Assoc.

217-223-4605

Checked By: 3KL

Approved By: _B____

Brian Laningham, PE

D-6 Geotechnical Engr.

Lic. #062-053757

Date: May 9, 2019

Attachments: Preliminary TSL

Subsurface Profile

Boring Logs **Existing Plans**

This Report has been prepared based on a preliminary TSL from February 2019. Contact the author if there are any questions regarding this Report or if there are modifications to structure location, size, geometry, or vertical alignment.

Electronic copies of boring logs are available upon request for inclusion in the plans. Calculations are also available upon request.

This Report has been prepared according to the 2012 IDOT Bureau of Bridges and Structures Bridge Manual and AASHTO LRFD Bridge Design Specifications 8th Edition - 2017

Project Description and Proposed Structure Information

The project includes replacing an existing 113-8" long and 36'-4" wide three-span slab bridge structure (SN 085-0002) with a new 93'-2 $\frac{1}{2}$ " long and 38'-10" wide, single span structure (SN 085-0504). The proposed structure will utilize integral abutments founded on piling. Work will be completed under stage construction.

Site Investigation

The project is located approximately 3.5 miles Northeast of Beardstown over Bluff Creek on US 67. The land surrounding this site is varied. To the north are bluffs of the IL River basin, at the south is the flood plain of the IL river. The structure sets on a levee of the Coal Creek Drainage & Levee District. The Illinois river is located approximately 3.0 miles to the Southeast.

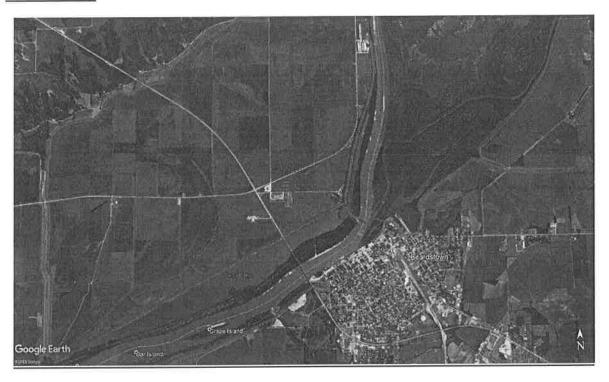
The original structure was built in 1958, as a 113-8" long and 36'-4" wide three-span slab bridge structure founded on piling. Its superstructure has a 3"-6" HMA wearing surface overlay.

Water flows from the northeast to southwest. There is no evidence of scour at the abutments or pier. There are concrete slope walls which a badly cracked.

The existing roadway crosses the top of the levee. No embankment slope stability problems have been observed, and there is no evidence of approach settlement problems. Both borings indicate \pm /- 20 of Silty Clay, and Silty Clay Loam with strengths ranging from .05 – 4.0 tsf. From \pm /- 20' to \pm /- 60', weak Silts, with strengths of 0.0 - 0.5 tsf were identified. Bedrock was encountered at elevation \pm /-399.00' (Boring #1) and \pm /-402.00' (Boring #2). Borings from the 1958 plans indicate very similar subsurface material.

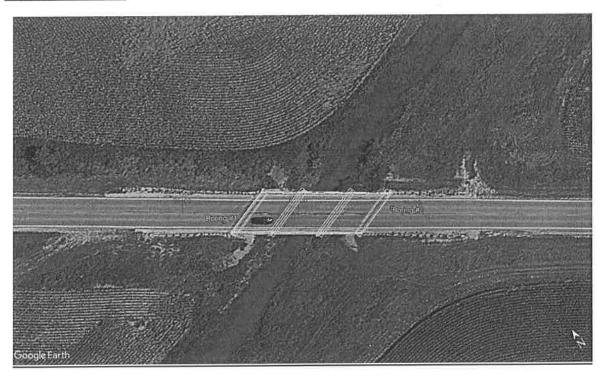
Borings were advanced by the District 6 drill crew using hollow stem auger methods according to AASHTO T 206 and the IDOT Geotechnical Manual. Borings were filled with cuttings immediately after drilling to allow traffic on the roadway.

Location Map

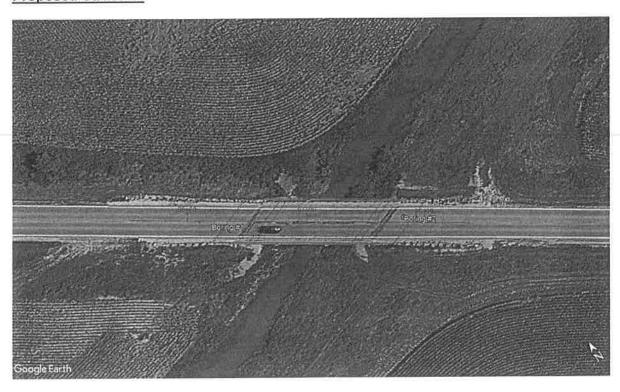




Existing Structure



Proposed Structure



Geotechnical Evaluation

Settlement: No change in grade is proposed. No settlement problems are anticipated

<u>Slope Stability</u>: There is no evidence of any slope stability problems with the existing cross slopes. Slope stability analysis indicated a Factor-of-Safety greater than the 1.5 required.

<u>Seismic Considerations:</u> The following table shows recommended seismic design data based on a 1000-year return period event.

Seismic Performance Zone (SPZ)	2
Spectral Acceleration at 1 second (S _{D1})	0.186g
Design Spectral Acceleration at 0.2 Seconds	0.328g
(S _{DS})	
Soil Site Class	Е

Seismic Performance Zone 2 requires liquefaction and seismic slope stability analysis to be performed.

<u>Liquefaction</u>. In general, the liquefiable layers are below the non-liquefiable layers beginning at elevation +/- 439.00' and terminating at +/- 400.00 at the North abutment. At the South abutment liquefiable layers begin at +/- 438.00' and terminate at +/- 402.00.

<u>Seismic Slope Stability</u>. The stability of a 2:1 end slope using a Peak Ground Acceleration (PGA) of 0.034g with a return period of 5% in 50 years has been analyzed at the North and South abutments. The Factor-of-Safety is greater than the required 1.5 for both abutments. Slope stability problems are not anticipated following a seismic event.

<u>Scour:</u> Scour elevations for a 100 and 200-year event was determined by the District 6 Hydraulics unit. The following table shows recommended design scour elevations at each substructure unit. The design scour elevation at abutments is equal to the proposed bottom of abutment elevation. Some adjustment to bottom of abutment elevation may be made during final design.

Design Scour Elevation Table										
Design Scour Elevation (ft.)	South Abut.	North Abut.	Item 113							
Q ₁₀₀	451.27	453.06	0							
Q ₂₀₀	451.27	453.06	0							

Mining Activity: ISGS records indicate no mines in the proposed project area.

Foundation Evaluation

Vertical Loading

Preliminary maximum factored loads, provided by the structure designer, are approximately 1673 kips vertical at the abutments. Spread footings will not be evaluated because of inadequate bearing capacity. Drilled shafts will not be evaluated because the required shaft depth would make them uneconomical when compared to driven piles. A driven pile foundation is recommended at each substructure.

Because Shale bedrock is shallow at ±51ft. to ±55ft., Metal Shell and H-Piles were analyzed. After analyzing Metal Shell pile, it was determined that not enough skin friction was developed before encountering Shale bedrock. The pile supported foundation would need to utilize end bearing. Metal Shell piles <u>are not recommended</u> because of potential damage that could occur during driving. **H-piles** <u>are</u> recommended. No piles shoes are required.

The following table shows Max. Nominal Required Bearing (NRB), Max. Factored Resistance Available (FRA) and Max. Seismic Resistance Available (SRA) for each pile size.

North Abutment

Pile Section	NRB, (kips)	FRA, (kips)	Seismic Downdrag, (kips)	SRA, (kips)	Driving Elev. (Ft.)	Cutoff Elev. (Ft).	Est. Tip Elev. (Ft.)	Est. Cutoff Elev. (Ft.)
HP 8x36	286	187	74	212	453.40	455.40	399.00	56.4
HP 10x42	335	184	91	244	453.40	455.40	399.00	56.4
HP 12x53	419	230	110	309	453.40	455.40	399.00	56.4
HP 12x63	497	273	110	387	453.40	455.40	399.00	56.4

South Abutment

Pile Section	NRB, kips	FRA, kips	Seismic Downdrag, kips	SRA, kips	Driving Elev. (Ft.)	Cutoff Elev. (Ft).	Est. Tip Elev. (Ft.)	Est. Cutoff Elev. (Ft.)
HP 8x36	286	187	67	219	451.60	453.60	402.00	51.6
HP 10x42	335	184	83	252	451.60	453.60	402.00	51.6
HP 12x53	419	230	100	319	451.60	453.60	402.00	51.6
HP 12x63	497	273	100	397	451.60	453.60	402.00	51.6

Lateral Loading

Soil inputs have been provided to facilitate a more detailed analysis as requested by the structural designer.

				Soil	Param	eters					
Substructure		Elev	ation	Unit \	Veight	Cohesion	ф	k		Description	
Unit	Layer	Тор	Bottom	(pcf)	(pci)	(psi)	(deg)	(pci)	e 50	Description	
	1	453.40	449.60	115	0.066	7.64	38	268.7	0.0086	Silty Loam	
	2	449.60	447.10	110	0.064	3.47		53.4	0.0167	Silty Loam	
	3	447.10	444.60	120	0.069	18.1	127	866.0	0.0055	Silty Clay Loam	
	4	444.60	441.60	120	0.069	9.72	727	446.5	0.0074	Silt	
	5	441.60	439.6	115	0.066	4.17	190	72.0	0.0140	Silt	
North Abutment Boring #1	6	439.6	437.1	110	0.064	0.69	Tall	8.0	0.010	Silty Clay Loam	
butr ng #	7	437.1	432.1	105	0.061	0.0	90	0.1	0.010	Silty Clay Loam	
th Abutm Boring #1	8	432.1	429.6	115	0.066	2.1	125	24	0.0238	Silty Clay Loam	
For H	9	429.6	423.6	105	0.061	0.0	1200	0.1	0.015	Silty Clay Loam	
_	10	423.6	417.6	115	0.066	-	30	20	*	Sand	
	11	417.6	412.1	110	0.064	0.0		0.1	0.02	Loam	
	12	412,1	407.1	105	0.061	3.5		53.4	0.0167	Loam	
	13	407.1	402.1	105	0.061	0.0		0.1	0.10	Loam	
	14	402.1	399.6	105	0.061	3.5		53.4	0.0167	Silt	
	1	451.6	448.6	125	0.072	27.8		1332.3	0,0047	Silt	
ent	2	448.6	446,1	115	0.066	9		393	0.0078	Silt	
tm #2	3	446.1	443.6	115	0.066	1.4		16	0.029	Silt	
South Abutment Boring #2	4	443.6	440.6	115	0.066	4.9		90.8	0.011	Silt Loam	
h A ori	5	440.6	438.6	115	0.066	4.2		72	0.014	Silt Ioam	
D'utl B	6	438.6	420,6	105	0.061	0.0		0.1	0.010	Silt Loam	
Š	7	420.6	402.0	105	0.061	2.1		24	0.024	Silty Clay Loam	

 $[\]phi$ = phi angle

Losses

Liquefaction was analyzed for Seismic Performance Zone (SPZ) 2, there is potential Downdrag losses if a significant earthquake event occurs.

Because there is no change in the roadway profile grade, there are no Downdrag (DD) losses.

There are no scour losses at the abutments.

k = subgrade modulus

 E_{50} = strain at 50% deflection in p-y curve

Approach Pavement

Foundation conditions beneath proposed approach pavement footings have been reviewed, based on available boring data, the available bearing capacity is greater than required. For structure replacement projects, experience indicates approach pavement footings do not experience excessive settlement when there is no new fill beneath the footing, and it is constructed on undisturbed soil. No remedial action is required.

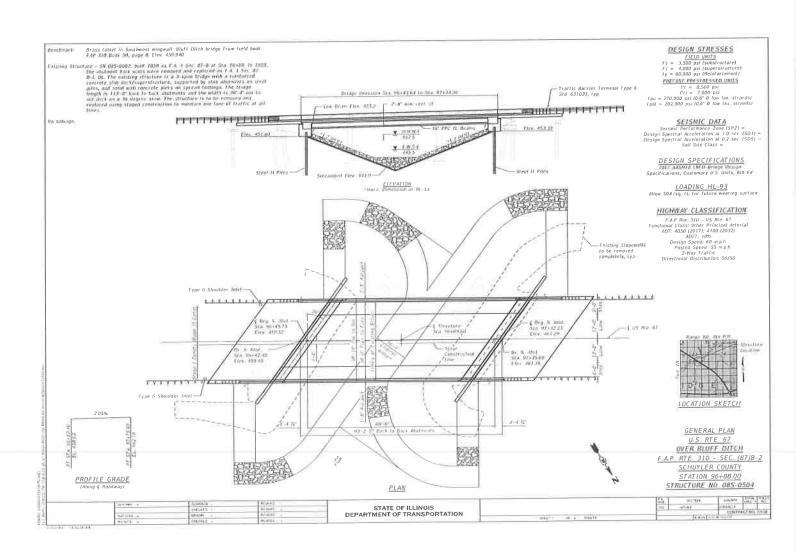
Construction Considerations

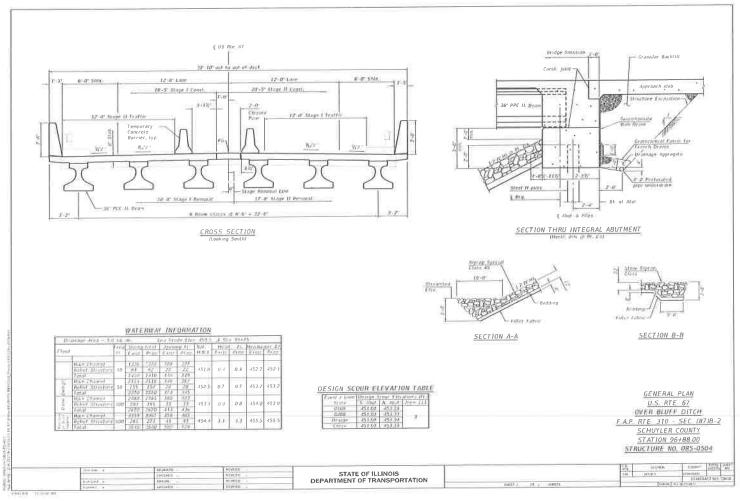
<u>Stage Construction:</u> This project will be constructed under Detour; No Stage Construction will be required in that case.

Ground Improvement: No ground improvement is required.

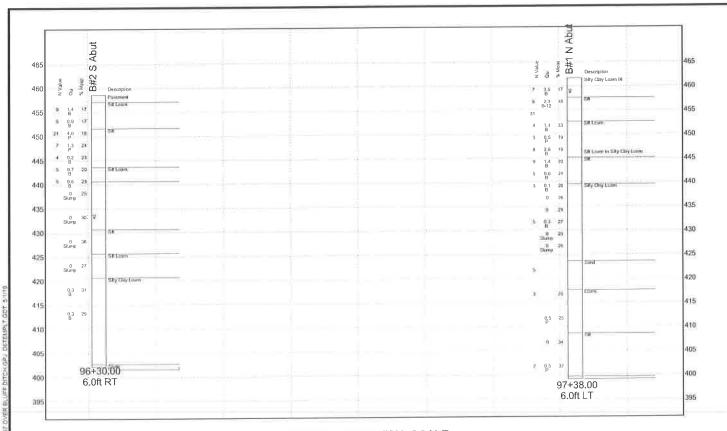
The following is a list of spreadsheets and software programs that were used in the geotechnical analysis:

- AASHTO Guide Specifications for LRFD Seismic Bridge Design 2018
- BBS 145 "Integral Abutment Feasibility Analysis" spreadsheet
- BBS 146 "Liquefaction Analysis" spreadsheet
- BBS 147 "IDOT Static Method of Estimating Pile Length" spreadsheet
- BBS 149 "Seismic Site Class Determination" spreadsheet
- "Slide" by Rocscience





Structure Number EX SN 085-0002 $\,\,$ PR SN 085-0504 US 67 over Bluff Ditch N of Beardstown Located in the NE 1/4, SE 1/4 of Section 23, Township 1N, Range 1W of the 4 P.M.



NOT TO HORIZONTAL SCALE



VARIATIONS IN SUBSURFACE CONDITIONS MAY EXIST BETWEEN BORINGS

g First Encounter
g Completion
w after trefer to loo

Abbreviations
WOH - Sampler Advanced by Weight
of Hanstrer, WOP - Weight of Pipe
B. S. - Before Seating

SUBSURFACE DATA PROFILE

Route: 67

Section: FAP Rte. 310 -- SEC. (87)B-2

County: Schuyler

BSURFACE DATA PROFILE IL67 OVER BLUFF DITCH GP., D6TEM

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Date 4/9/19

ROUTE 67	DESCRIPTION			US 67	over Bl	uff Ditch N of Beardstown	LOGGE	D BY		S. Jone	es
SECTION FAP Rte. 3 (87)	10 – SEC. B-2 LO	CATIO	Ν _	NE 1/4	, SE 1	4, SEC. 23, TWP. 1N, RNG. 1W, 4	PM				
COUNTY Schuyle	r DRILLING	METH	IOD			HSA HAMMER	TYPE		140#	Auto	
EX SN PR S	+89.00 N Abut	D E P T H	B L O W S	U C S Qu	M O I S T	Surface Water Elev. 443.57 Stream Bed Elev. 442.57 Groundwater Elev.: ▽ First Encounter 458.6 ▼ Upon Completion Plugged	ft S ft	D E P T H	B L O W S	U C S Qu	M O I S T
Offset <u>6.</u> Ground Surface Elev.	0ft L I 461.63 ft	(ft)		(tsf)	(%)	▼ After Hrs. Plugged	ft	(ft)		(tsf)	(%)
Dk Gray SILTY CLAY LO Fill						Gray Moist SILT (continued) Dk Gray		=	3 2	0.6 B	24
	Ā		0 3 4	3.6 B	17	Gray and Brown Moist SILTY CLAY LOAM	439.63	-	WOH 1 2	0.1 B	20
Gray SILT	457.63							-	0		
		5 	3 3	2.3 S-12	18	Brown		-25	WOH 1	0	26
Poor Recovery			12			Brown V. Moist Silty Clay Loam)— —	W	0	29
Hit boulder Fill			15 16			w/ Iron Oxide staining		T	Н		20
Brown Moist SILT LOAN	452.63 1	-10	1	1.1	33	Gray and Brown		-30	0 2	0.3	27
			3	В					3	В	
Poor Recovery			1	0.5	19			_	0 H	0 Slump	25
			2	Р				=		Siump	
Brown and Gray Moist S to Dk Gray SILTY CLAY	ILT LOAM LOAM	-15	0 4 4	2.6 B	19			35	0	0 Slump	26
Gray Moist SILT	445.13							_			
			1 4 5	1.4 B	20	Med Grained Tan SAND w/ 1/4" aggregate Poor Recovery	423.63	-			
		-	2						0		

File Name S.;SOILS\GINT FILES\085 SCHUYLER\BRIDGE BORINGS\IL67 OVER BLUFF DITCH.GPJ Data Template D6TEMPLT.GDT Date Printed 4/19/19 Latitude 40D 2.8177N Longitude 90D 28.8442W Datum NADB3 Job Number

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer, E-Estimated) Abbreviations W.O.H - Sampler Advanced By Weight of Hammer, W.O.P - Advanced by Weight of Pipe, B.S. - Before Seating The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206) BBS, from 137 (Rev. 8-99)

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Date 4/9/19

ROUTE	67 DESC	RIPTION			US 67	over B	luff Ditch N of Beardstown	LOGGE	D BY		S. Jone	es
SECTION _	FAP Rte. 310 – SEC (87)B-2		CATIC	DN	NE 1/4	, SE 1	/4, SEC. 23, TWP. 1N, RNG. 1W, 4	PM				
COUNTYSchuyler DRILLING METHOD				HOD	-		HSA HAMMER	R TYPE 140# Auto				
Station BORING NO. Station Offset	EX SN 085-000 PR SN 085-050 96+89.00 1 N Abut 97+38.00 6.0ft LT face Elev. 461.63	4	D E P T H (ft)	B L O W S	U C S Qu (tsf)	M O I S T	Surface Water Elev. 443.57 Stream Bed Elev. 442.57 Groundwater Elev.: ▼ First Encounter 458.6 ▼ Upon Completion Plugged ▼ After Hrs. Plugged	f ft S ft I ft	D E P T H	B L O W S	U C S Qu (tsf)	M O I S T (%)
Med Grained w/ 1/4" aggre	Tan SAND		7=	1 4			Wet Gray SILT w/ thin seams of V. Weathered		-	0 2	0.5 P	32
Poor Recove	ery (continued)		_	4			Shale (continued) Sand Seams @61ft		_			
			_				Auger Refusal	399.63 399.13				
							No Recovery	_		100/4		
Gray Wet LC	2004	417.63	-						_			
Glay Well LC)/4IVI		-45	0		00			-65			
				1 2		26			-			
									-			
			_	6 0								
			_						7			
V. Wet Gray	Loam to Loam w/		-50	W	0.5	25			-70			
Sand Seams			_	Н	Р							
									_			
		408.63							_			
Wet Gray SII w/ thin seam	LT s of V. Weathered		-									
Shale				w					-75			
			<u>55</u>	0	0	34						
				Н								
									_			
									_			
			-60	0					-80			

Page $\underline{1}$ of $\underline{2}$

Date 4/15/19

	IPTION	_		US 67	over B	luff Ditch N of Beardstown		LOGGE	D BY	>9	S. Jone	es
FAP Rte. 310 – SEC. (87)B-2	LO	CATIC	ж _	NE 1/4	I, SE 1	/4, SEC. 23, TWP. 1N, RNC	G. 1W, 4 I	PM				
COUNTY SEX SN 085-0002	HOD	_		HSA I	HAMMER	TYPE		1407	# Auto			
STRUCT. NO. Station EX SN 085-0002 PR SN 085-0504 96+89.00 BORING NO. 2 S Abut		D E P T	B L O W	U C S	M 0 1 s	Surface Water Elev. Stream Bed Elev. Groundwater Elev.:	443.57 442.57		D E P T	B L O W	U C S	M O I S
Station 96+30.00		н	S	Qu	Т	☑ First Encounter	433.2		Н	S	Qu	Т
Offset 6.0ft RT Ground Surface Elev. 458.67	— _{ft}	(ft)		(tsf)	(%)	▼ Upon Completion ▼ After Hrs	Plugged Plugged		(ft)		(tsf)	(%)
Pavement						Brown Moist SILT LOAM	(Till)		-	WOH		
and the second s						natural ground (continued	1)			WOH 2	0 Slump	25
Brown Moist SILT LOAM (Levy Fill)	457.17								-		Siump	
Diewii Mola ele Lee y Lay		-										
			1 5	1.4	17							
		-	4	B	''							
		5	2						-25	w		
Silt Loam to Silty Clay Loam		_	3	0.9	17		Δ		-	0	0	30
			3	В		10 10			_	Н	Slump	
Gray and Brown SILT	451.67					w/ Sand Seam FREE WATER			_			
sample broken		-	2					430.67				
			11	4.0	18	Brown Wet SILT w/ Iron Oxide Nodules			7			
		-	10	Р		W ITOH Oxide Noddles			-	-		
		-10							-30			
			1		0.4					W	0	38
Gray Moist Silt sample broken			3	1.3 P	24						Slump	
		7										
		-						gazes are	_			
			2	0.2	23	Gray and Brown Wet SIL	T LOAM	425.67				
		_	2	В		w/ 6" Med Grained Sand @36ft	Seam					
	TAULANNESCE	9				(((((((((((((((((((-			
Gray Moist SILT LOAM	443.67	-15	0						35	W		
Committee and Co			2	0.7	20					0	0	27
		_	3	В					_	Н	Slump	
	440.67		1			0 10 70 70 70 70 70 70 70 70 70 70 70 70 70	0.484	420.67				
Brown Moist SILT LOAM (Till) natural ground		_	2	0.6 B	23	Gray Wet SILTY CLAY L	UAM					
, attacking out the			3									
		1		1	1	II .				1	1	

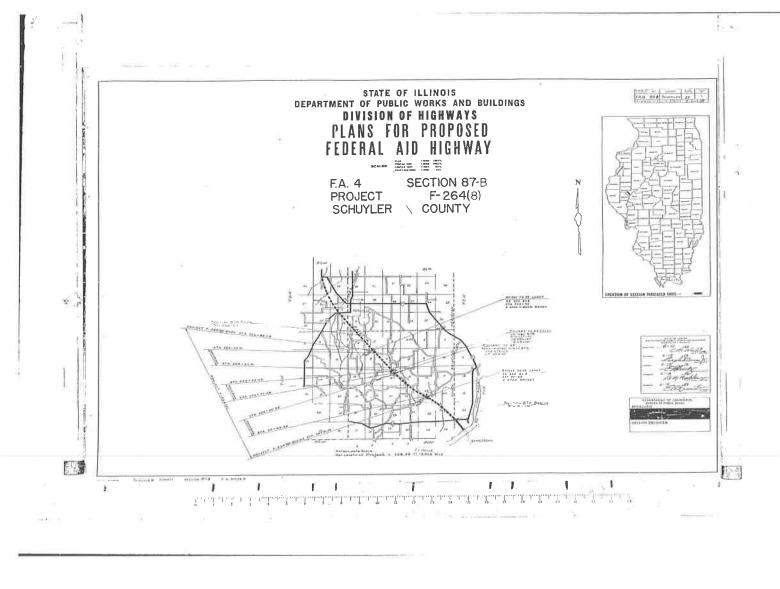
File Name S.\SOILS\GNT FILES\\QBS SCHUYLE\\BRIDGE BORNOS\\IL67 OVER BLUFF DITCH\\GPJ Data Template D6TEMPLT\GDT Date Printed 4/19/19 Latitude 40D 2.8062'W Longitude 90D 28.8163'W Datum NAD83 Job Number

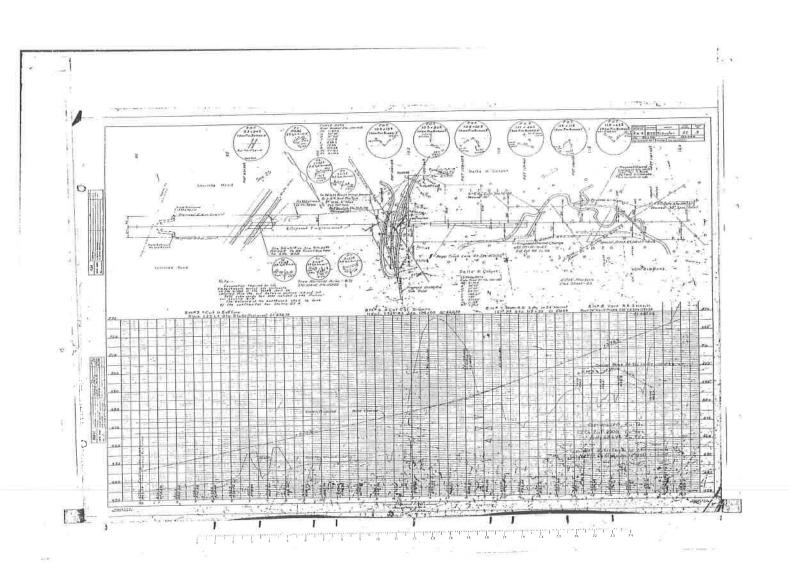


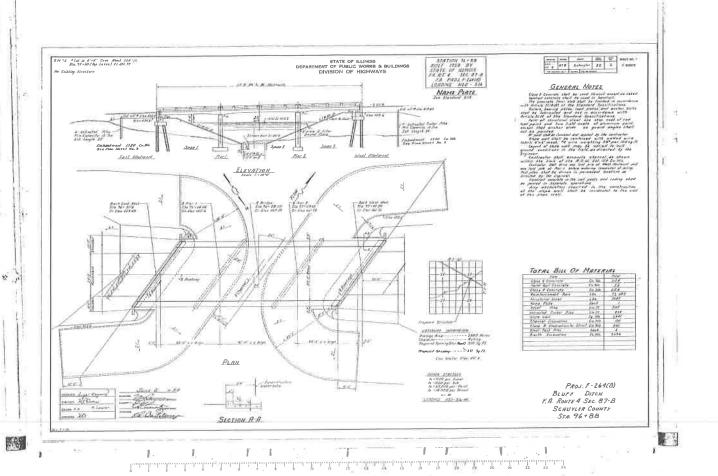
Page $\underline{2}$ of $\underline{2}$

Date 4/15/19

	67 DESCRIP P Rte. 310 – SEC.	PTION			JS 67	over B	luff Ditch N of Beardstow	vn	LOGGED BY	S. Jones
SECTION	(87)B-2	LOC	ATIO	ON	NE 1/4	, SE 1	/4, SEC. 23, TWP. 1N, R	RNG. 1W, 4 P	PM	
COUNTY	SEX SN 085-0002	LUNG	MET	HOD	-		HSA	HAMMER	TYPE	140# Auto
STRUCT. NO	EX SN 085-0002 PR SN 085-0504 eation 96+89.00	_ 1 _ 1	D E P	B L O	U C S	M 0 1	Surface Water Elev. Stream Bed Elev.			
Station Offset Ground Surface	6.0ft RT	- ft	H (ft)	W S	Qu (tsf)	S T (%)	Groundwater Elev.:	433.2 Plugged Plugged	ft	
Gray Wet SILTY (continued)				W	0.3	31				
(oonanaoa)		3		Н	B	J1				
		-								
		3								
		-	-45	WOH						
		a	_	WOH	0.3	29				
			-	1	В					
			-							
		9	-							
		8								
		17	-50							
		3								
		9								
			_							
			-55							
	4	02.67	_							
Gray Weathered Auger Refusal @	SHALE	02.17		55 \ /4" /						
			_							
										-
			-60							







. S. | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 STATE OF ILLINOIS
DEPARTMENT OF PUBLIC WORKS & BUILDINGS
DIVISION OF HIGHWAYS The Country Loan

See Some Sep Cay I can

Country Loan

Loan See Cay I can

Loan See C Address from the stage of the s Signature Bell # State S 18 Mole: II - These see first of proceedings of beautiful seems to the part 1250 Est. Drug 125 house of the beautiful seems to the part of the seems to BORING DATA
BLUFF DITCH
F.A.RT. 4 SLC 87-8
SCHUYLER COUNTY
STA. 96+88 man hap tan 1866 . 1866 **1** M.) I 222 $r = t_c = t_c$ harak dadan da malan mal

