

STRUCTURE GEOTECHNICAL REPORT

FAI RTE 57- I-57 Over Eastern Illinois Railroad

Proposed S.N. 018-0069 (SB)

Proposed S.N. 018-0070 (NB)



08/09/2024

Exp. 11/30/2025

FAI 57
SECTION 18-1V8
CUMBERLAND COUNTY, ILLINOIS
JOB NO. P-97-047-12
PTB 197/034
CONTRACT NO. 74597
KEG NO. 20-1152.00

Authored By:

Matt D. Masterson, P.E. &
Christoph Opperman, E.I.

mmasterson@kaskaskiaeng.com

(618) 233-5877

Prepared For:

BLA, Inc.
333 Pierce Road, Suite 200
Itasca, Illinois 60143

November 5, 2021
REVISED August 9, 2024



TABLE OF CONTENTS

1.0	Project Description and Scope	3
1.1	Introduction.....	3
1.2	Project Description	3
1.3	Proposed Structure Information	3
2.0	Field Exploration.....	3
2.1	Subsurface Exploration and Testing	3
2.2	Subsurface Conditions.....	3
3.0	Geotechnical Evaluations	4
3.1	Settlement	4
3.2	Slope Stability.....	4
	Table 3.2 – Slope Stability Critical FOS	5
3.4	Seismic Considerations	5
	Table 3.3 - Summary of Seismic Parameters	6
4.0	Foundation Evaluations and Design Recommendations	6
4.1	Bearing Resistance	6
4.2	Driven Piles	6
	Table 4.2 - Preliminary Design Loads	7
	Table 4.2.1 - Estimated Pile Lengths for Metal Shell 12"Φ w/.25" walls	7
	Table 4.2.2 - Estimated Pile Lengths for Metal Shell 14"Φ w/.25" walls	8
	Table 4.2.3 - Estimated Pile Lengths for Metal Shell 14"Φ w/.312" walls	8
	Table 4.2.4 - Estimated Pile Lengths for HP 10x42 Steel H-Piles.....	9
	Table 4.2.5 - Estimated Pile Lengths for HP 12x53 Steel H-Piles.....	9
	Table 4.2.6 - Estimated Pile Lengths for HP 12x63 Steel H-Piles.....	10
	Table 4.2.7 - Estimated Pile Lengths for HP 14x73 Steel H-Piles.....	10
	Table 4.2.8 - Estimated Pile Lengths for HP 14x89 Steel H-Piles.....	11
	Table 4.2.9 - Estimated Pile Lengths for HP 14x117 Steel H-Piles.....	11
	Table 4.2.10 - Estimated Pile Lengths for Metal Shell 12"Φ w/.25" walls	12
	Table 4.2.11 - Estimated Pile Lengths for Metal Shell 14"Φ w/.25" walls	12
	Table 4.2.12 - Estimated Pile Lengths for Metal Shell 14"Φ w/.312" walls	13
	Table 4.2.13 - Estimated Pile Lengths for HP 10x42 Steel H-Piles.....	14
	Table 4.2.14 - Estimated Pile Lengths for HP 12x53 Steel H-Piles.....	14
	Table 4.2.15 - Estimated Pile Lengths for HP 12x63 Steel H-Piles.....	14

Table 4.2.16 - Estimated Pile Lengths for HP 14x73 Steel H-Piles.....	15
Table 4.2.17 - Estimated Pile Lengths for HP 14x89 Steel H-Piles.....	15
4.3 Lateral Pile Response.....	16
Table 4.3.1 - Soil Parameters for Lateral Pile Load Analysis	16
5.0 Construction Considerations.....	16
5.1 Construction Activities	16
5.2 Temporary Sheet piling and Soil Retention	16
5.3 Site and Soil Conditions.....	16
6.0 Computations	17
7.0 Geotechnical Data.....	17
8.0 Limitations	17

EXHIBITS

- Exhibit A – Location Map
- Exhibit B – Type, Size, and Location Plan (TS&L)
- Exhibit C – Boring Logs
- Exhibit D – Subsurface Profile
- Exhibit E – Slope/W Slope Stability Analysis
- Exhibit F – Bearing Resistance Calculations
- Exhibit G – Pile Length/Pile Type

1.0 Project Description and Scope

1.1 Introduction

The geotechnical study summarized in this report was performed by Kaskaskia Engineering Group, LLC (KEG) for a proposed bridge carrying I-57 over the Eastern Illinois Railroad (EIRR) in Cumberland County, Illinois. The purpose of this report is to document subsurface geotechnical conditions, provide analyses of anticipated site conditions as they pertain to the project described herein, and to present design and construction recommendations for the proposed structure.

1.2 Project Description

The project consists of the replacement of two three-span continuous wide flange beam bridges with a reinforced concrete deck, existing SNs 018-0001 (SB) and 018-0002 (NB), carrying I-57 over the EIRR in Cumberland County, Illinois.

The general location of the proposed structures is shown on a Location Map, Exhibit A. The project is located approximately 1 mile northeast of Neoga, Illinois. The site lies within the limits of the Third Principal Meridian (Twp. 10N, R. 7E) within the Springfield Plain of the Till Plains Section of the Central Lowland Province.

1.3 Proposed Structure Information

The proposed structures will consist of two three-span continuous welded plate girder bridges with a reinforced concrete deck, which will be built on a 45-degree skew from the centerline of the EIRR and will provide 12 ft.-wide driving lanes and 8.0 to 12.0 ft.-wide shoulders with a total width of 46 ft- 10-inches out-to-out. The southbound proposed bridge centerline station will be at 6052+69.15 on I-57 and at 49+05.34 on the EIRR. The northbound proposed bridge centerline station will be at 6054+03.02 on I-57 and at 50+94.67 on the EIRR. Both bridges will consist of two, 95 ft. end spans, and one, 150 ft span, and will measure 345 ft.-2 3/16-inches back-to-back of abutments. Abutments for both bridges will be integral. A Type, Size, and Location Plan (TS&L) is included in Exhibit B.

Further substructure details will be based on the findings of this SGR.

2.0 Field Exploration

2.1 Subsurface Exploration and Testing

The site exploration plan was developed and completed by IDOT. Two standard penetration test (SPT) borings (designated B-1 and B-2) were drilled from October 7 through October 8, 2020. Boring Locations are shown on Exhibit B – TS&L. Detailed information regarding the nature and thickness of the soils encountered and the results of the field sampling and laboratory testing are shown on the Boring Logs, Exhibit C. The soil profile for the above-mentioned borings can be found in Subsurface Profile, Exhibit D.

2.2 Subsurface Conditions

The profiles at the two boring locations exhibited layers of clays, silts, sands, loam, and till. Borings B-1 and B-2 were terminated at 100 ft. and 75 ft. below ground surface elevation (GSE)

respectively. Boring B-1 has an estimated GSE of 690.19 ft., and B-2 has an estimated GSE of 690.51 ft. In general, the lithologic succession is as follows:

Clay - Borings B-1 and B-2 encountered approximately 29.5 ft. of clay below the ground surface elevations (BSE). Boring B-2 also encountered clay between 34.5 and 40.0 ft BSE. The driving resistance values (N-values) ranged from 5 to 11 blows per foot (bpf), with unconfined compressive strength (Q_u) values between 1.1 to 4.5 tons per square foot (tsf). The moisture contents varied from 10 to 23 percent.

Silty Clay/Silty Loam/Silty Clay Loam - Below the clay layer in Borings B-1 and B-2, silty clay, silty loam, and silty clay loam was encountered between 29.5 and 45 ft. below GSE. The N-values ranged from 3 bpf to 5 bpf, with (Q_u) values between 0.8 and 1.7 tsf, and moisture contents of 20 percent to 23 percent.

Sand/Sandy Loam/Sandy Clay – A sand, sandy loam, and sandy clay was encountered below the silty clays at depths between 45.0 and 64.5 feet below GSE of Boring B-1 and between 40.0 and 54.5 feet below GSE of Boring B-2. The N-values ranged from 3 to 45 bpf, with unconfined compressive strength (Q_u) values between 0.4 to 2.8 tsf. The moisture contents varied from 7 to 19 percent.

Clay Till – Below the sand/sandy loam/sandy clay in both borings, a layer of clay till was encountered in boring B-1 between 64.5 ft. to termination of the boring at 100 ft. below GSE, and in boring B-2 between 54.5 ft to termination of the boring at 81 ft. below GSE. The N-value for this layer ranged from 20 to 100 bpf, with unconfined compressive strength (Q_u) values between 3.7 and 9.2 tsf. The moisture content varied from 7 to 19 percent.

Groundwater was first encountered during drilling in Boring B-1 at 49.0 ft. below GSE, and in Boring B-2 at 44.5 ft. below GSE. Groundwater was also measured upon completion of the borings at 32.0 ft below GSE for Boring B-1, and at 30.0 ft below GSE for Boring B-2. Measurements 24-hours later showed a groundwater elevation of 34.0 ft below GSE for Boring B-1, and 14.0 ft below GSE for Boring B-2. It should be noted that the groundwater level is subject to seasonal and climatic variations. In addition, without extended periods of observation, measurement of true groundwater levels may not be possible. Bedrock was not encountered in the borings.

3.0 Geotechnical Evaluations

3.1 Settlement

Since no significant grading or changes to the existing embankments are expected at the proposed structure, it is estimated that the existing embankments will experience no settlement. Therefore, no settlement calculations were performed for the proposed structure.

3.2 Slope Stability

A stability analysis using SLOPE/W was performed using the proposed roadway and bridge geometry on the TS&L and soil characteristics from Boring B-1 and B-2. Two conditions were modeled for each scenario: end-of-construction and long-term stability. A critical factor of safety (FOS) was calculated for each condition. According to current standard of practice, the target FOS is 1.5 for end-of-construction and long-term slope stability. The slope stability analyses indicated that the required minimum FOS for all conditions were met.

In order to model the end-of-construction condition, full cohesion and a friction angle of 0 degrees were assumed. Nominal values for cohesion were used with full friction angle to model the long-term condition to analyze the theoretical condition where pore water pressure has dissipated. Nominal values were between 50 and 150 psf for the cohesive soils, with friction angles between 26 and 30 degrees.

The Bishop Circular Method, which generates circular-shaped failure surfaces, was used to calculate the critical failure surfaces and FOS for the proposed conditions. The FOS obtained in the analysis is shown in Table 3.2. SLOPE/W program output from this analysis can be found in SLOPE/W Slope Stability Analysis, Exhibit E.

Table 3.2 – Slope Stability Critical FOS

Location (2H:1V Slope)	Critical FOS	
	End-of Construction	Long Term
South Abutment	2.6	2.1
North Abutment	3.8	2.1

The results indicate that an acceptable F.O.S. will exist under undrained and drained conditions. No additional ground improvement/treatments are necessary for long term support of the proposed slopes.

3.3 Scour

The proposed structure will not cross a river or other tributary; therefore, scour is not an issue.

3.4 Seismic Considerations

The determination of Seismic Site Class was based on the method described by IDOT AGMU Memo 09.1 - Seismic Site Class Definition and the IDOT provided spreadsheet titled: '*Seismic Site Class Determination*.' Using these resources, the controlling global site class for this project is Soil Site Class D.

Additional seismic parameters were calculated for use in design of the structure and evaluation of liquefaction potential. Published information and mapping from the USGS, including software directly applicable to the AASHTO Guide Specifications for LRFD Seismic Bridge Design, was used to develop the parameters for the bridge location. The values, based on Soil Site Class D, are summarized below.

Table 3.3 - Summary of Seismic Parameters

Parameter	Value
Soil Site Class	D
Spectral Response Acceleration, 0.2 Sec, S_{DS}	0.408g (Site Class D)
Spectral Response Acceleration, 1.0 Sec, S_{D1}	0.19g (Site Class D)
Seismic Performance Zone	2

As indicated in the table above, the Seismic Performance Zone is 2, based on S_{D1} and Table 3.15.2 in the IDOT Bridge Manual, the Soil Site Class D, and Figure 2.3.10-3 in the IDOT Bridge Manual.

4.0 Foundation Evaluations and Design Recommendations

4.1 Bearing Resistance

The soil encountered at the anticipated bearing elevation of the piers will consist of a silty clay material based on the borings. The assumed bearing elevation at the bottom of the piers is El. 657 +/- . Using a cohesion of 1,300 psf for the bearing soil, the calculated allowable bearing resistance, using a Bearing Resistance Factor of 0.5, at the approximate bottom elevation of the piers is estimated to be about 4,100 psf. Sliding resistance is calculated as 400 psf. See Exhibit F for calculations performed.

Table 4.1 – Factored Bearing and Sliding Resistances

Substructure Unit	Factored Bearing Resistance (psf)	Factored Sliding Resistance (psf)
Pier 1	4,100	400

4.2 Driven Piles

The foundations supporting the proposed bridge must provide sufficient support to resist dead and live loads. The IDOT Static Method uses the LRFD Pile Design Guide Procedure to estimate the pile lengths (Pile Length/Pile Type, Exhibit G).

The factored reactions and the preliminary design loads, as provided by BLA Inc. are provided in Table 4.2. The Nominal Required Bearing (RN) represents the resistance the pile will experience during driving, as well as assist the contractor in selecting a proper hammer size. The Factored Resistance Available (RF) documents the net long term axial factored pile capacity available at the top of the pile to support factored substructure loadings.

Table 4.2 - Preliminary Design Loads

Substructure Unit	Factored Reactions (kips)
South Abutment (B-1)	1,650
Pier 1 (B-1)	3,780
Pier 2 (B-2)	3,780
North Abutment (B-2)	1,650

The estimated pile lengths for applicable Metal-shell pile and H-pile types are shown in Tables 4.2.1 thru 4.2. below. The Nominal Required Bearing (R_N) represents the resistance the pile will experience during driving, and will assist the contractor in selecting a proper hammer size. The Factored Resistance Available (R_F) documents the net long-term axial factored pile capacity available at the top of the pile to support factored substructure loadings.

Southbound (SN 018-0069)**Table 4.2.1 - Estimated Pile Lengths for Metal Shell 12" Φ w/.25" walls**

Substructure Unit	R_N Nominal Required Bearing (kips)	R_F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
South Abutment B-1	253	139	46	686.77
	231	127	51	686.77
	265	146	56	686.77
	392	216	59	686.77
Pier 1 B-1	305	168	44	659.84
	348	191	49	659.84
	386	212	54	659.84
	392	216	55	659.84
Pier 2 B-2	296	163	32	657.85
	305	168	37	657.85
	371	204	42	657.85
	392	216	43	657.85
North Abutment B-2	175	97	35	685.97
	198	109	40	685.97
	391	215	45	685.97
	392	216	50	685.97

Table 4.2.2 - Estimated Pile Lengths for Metal Shell 14"Φ w/.25" walls

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
South Abutment B-1	307	169	46	686.77
	275	151	51	686.77
	313	172	56	686.77
	459	252	59	686.77
Pier 1 B-1	439	241	39	659.84
	370	203	44	659.84
	425	234	49	659.84
	459	252	53	659.84
Pier 2 B-2	365	201	32	657.85
	373	205	37	657.85
	458	252	42	657.85
	459	252	42	657.85
North Abutment B-2	187	103	30	685.97
	206	113	35	685.97
	234	129	40	685.97
	459	252	44	685.97

Table 4.2.3 - Estimated Pile Lengths for Metal Shell 14"Φ w/.312" walls

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
South Abutment B-1	307	169	46	686.77
	275	151	51	686.77
	313	172	56	686.77
	570	314	61	686.77
Pier 1 B-1	473	260	54	659.84
	504	277	59	659.84
	530	292	64	659.84
	570	314	65	659.84

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
Pier 2 B-2	365	201	32	657.85
	373	205	37	657.85
	458	252	42	657.85
	570	314	45	657.85
North Abutment B-2	479	263	50	685.97
	535	294	60	685.97
	543	298	65	685.97
	570	314	67	685.97

Table 4.2.4 - Estimated Pile Lengths for HP 10x42 Steel H-Piles

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
South Abutment B-1	335	184	97	686.77
Pier 1 B-1	335	184	72	659.84
Pier 2 B-2	335	184	70	657.85
North Abutment B-2	335	184	96	685.97

Table 4.2.5 - Estimated Pile Lengths for HP 12x53 Steel H-Piles

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
South Abutment B-1	418	230	97	686.77
Pier 1 B-1	418	230	72	659.84

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
Pier 2 B-2	418	230	70	657.85
North Abutment B-2	418	230	96	685.97

Table 4.2.6 - Estimated Pile Lengths for HP 12x63 Steel H-Piles

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
South Abutment B-1	497	273	98	686.77
Pier 1 B-1	497	273	74	659.84
Pier 2 B-2	497	273	71	657.85
North Abutment B-2	497	273	97	685.97

Table 4.2.7 - Estimated Pile Lengths for HP 14x73 Steel H-Piles

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
South Abutment B-1	578	318	98	686.77
Pier 1 B-1	578	318	73	659.84
Pier 2 B-2	578	318	71	657.85
North Abutment B-2	578	318	97	685.97

Table 4.2.8 - Estimated Pile Lengths for HP 14x89 Steel H-Piles

Substructure Unit	R_n Nominal Required Bearing (kips)	R_F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
South Abutment B-1	705	388	100	686.77
Pier 1 B-1	705	388	75	659.84
Pier 2 B-2	705	388	73	657.85
North Abutment B-2	705	388	99	685.97

Table 4.2.9 - Estimated Pile Lengths for HP 14x117 Steel H-Piles

Substructure Unit	R_n Nominal Required Bearing (kips)	R_F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
South Abutment B-1	929	511	103	686.77
Pier 1 B-1	929	511	78	659.84
Pier 2 B-2	929	511	76	657.85
North Abutment B-2	929	511	102	685.97

Northbound (SN 018-0070)

Table 4.2.10 - Estimated Pile Lengths for Metal Shell 12"Φ w/.25" walls

Substructure Unit	R_n Nominal Required Bearing (kips)	R_F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
South Abutment B-1	264	145	47	687.91
	243	134	52	687.91
	276	152	57	687.91
	392	216	60	687.91
Pier 1 B-1	325	179	43	658.58
	363	200	48	658.58
	390	214	53	658.58
	392	216	54	658.58
Pier 2 B-2	300	165	32	658.33
	309	170	37	658.33
	375	206	42	658.33
	392	216	43	658.33
North Abutment B-2	160	88	30	686.32
	177	97	35	686.32
	199	110	40	686.32
	392	216	50	686.32

Table 4.2.11 - Estimated Pile Lengths for Metal Shell 14"Φ w/.25" walls

Substructure Unit	R_n Nominal Required Bearing (kips)	R_F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
South Abutment B-1	321	177	47	687.91
	288	159	52	687.91
	327	180	57	687.91
	459	252	59	687.91
Pier 1 B-1	343	189	38	658.58
	399	219	43	658.58
	446	245	48	658.58
	459	252	50	658.58

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
Pier 2 B-2	435	239	27	658.33
	970	204	32	658.33
	378	208	37	658.33
	459	252	42	658.33
North Abutment B-2	189	104	30	686.32
	208	114	35	686.32
	235	129	40	686.32
	459	252	44	686.32

Table 4.2.12 - Estimated Pile Lengths for Metal Shell 14"Φ w/.312" walls

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
South Abutment B-1	321	177	47	687.91
	288	159	52	687.91
	327	180	57	687.91
	570	314	62	687.91
Pier 1 B-1	446	245	48	658.58
	477	262	53	658.58
	503	277	58	658.58
	570	314	60	658.58
Pier 2 B-2	370	204	32	658.33
	378	208	37	658.33
	463	255	42	658.33
	570	314	45	658.33
North Abutment B-2	480	264	45	686.32
	536	295	50	686.32
	544	299	60	686.32
	570	314	67	686.32

Table 4.2.13 - Estimated Pile Lengths for HP 10x42 Steel H-Piles

Substructure Unit	R_n Nominal Required Bearing (kips)	R_F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
South Abutment B-1	335	184	98	687.91
Pier 1 B-1	335	184	66	658.58
Pier 2 B-2	335	184	70	658.33
North Abutment B-2	335	184	96	686.32

Table 4.2.14 - Estimated Pile Lengths for HP 12x53 Steel H-Piles

Substructure Unit	R_n Nominal Required Bearing (kips)	R_F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
South Abutment B-1	418	230	98	687.91
Pier 1 B-1	418	230	66	658.58
Pier 2 B-2	418	230	70	658.33
North Abutment B-2	418	230	96	686.32

Table 4.2.15 - Estimated Pile Lengths for HP 12x63 Steel H-Piles

Substructure Unit	R_n Nominal Required Bearing (kips)	R_F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
South Abutment B-1	497	273	99	687.91
Pier 1 B-1	497	273	68	658.58

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
Pier 2 B-2	497	273	72	658.33
North Abutment B-2	497	273	97	686.32

Table 4.2.16 - Estimated Pile Lengths for HP 14x73 Steel H-Piles

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
South Abutment B-1	578	318	99	687.91
Pier 1 B-1	578	318	67	658.58
Pier 2 B-2	578	318	71	658.33
North Abutment B-2	578	318	97	686.32

Table 4.2.17 - Estimated Pile Lengths for HP 14x89 Steel H-Piles

Substructure Unit	R _n Nominal Required Bearing (kips)	R _F Factored Resistance Available (LRFD) (kips)	Estimated Pile Length (ft.)	Assumed Pile Cut-off Elevation (ft.)
South Abutment B-1	705	388	101	687.91
Pier 1 B-1	705	388	69	658.58
Pier 2 B-2	705	388	73	658.33
North Abutment B-2	705	388	99	686.32

4.3 Lateral Pile Response

Generally, the geotechnical engineer provides soil parameters to the structural engineer so that an L-Pile program or other approved software can be used for the lateral or displacement analysis of the foundations. Table 4.3.1 is included for the structural engineer's use in determining lateral pile response.

Table 4.3.1 - Soil Parameters for Lateral Pile Load Analysis

Boring	Depth at Bottom of Layer (Feet)	γ (pcf)	Short Term		Long Term		N Value (Est. Range)	Assumed % Fines < #200	K (pci)	ϵ_{50}
			ϕ (deg.)	c (psf)	ϕ (deg.)	c (psf)				
B-1	29.5	120	0	2000	28	100	5-11	85	1000	0.005
	45.0	120	0	950	26	100	3-5	80	100	0.01
	64.5	120	0	1900	30	100	13-45	25	60	--
	100	130	0	4600	28	100	20-43	85	2000	0.005
B-2	29.5	120	0	2000	26	100	6-10	85	1000	0.005
	34.5	120	0	1700	26	100	5	60	500	0.007
	40.0	120	0	1200	26	100	5	85	500	0.007
	54.5	120	0	1000	28	100	3-55	25	20	--
	81.0	130	0	6000	28	150	28-61	85	2000	0.005

5.0 Construction Considerations

5.1 Construction Activities

Construction activities should be performed in accordance with the current IDOT Standard Specifications for Road and Bridge Construction and any pertinent Special Provisions or Policies.

Should any design considerations assumed by KEG change, KEG should be contacted to determine if the recommendations stated in this report still apply.

5.2 Temporary Sheet piling and Soil Retention

Temporary shoring is not anticipated as the bridge will be reconstructed with a crossover.

5.3 Site and Soil Conditions

Provisions of the Standard Specifications should adequately address site and soil conditions.

6.0 Computations

Computations and analyses for specific circumstances, if any, are included as exhibits. Please refer to each section of the report for reference to the exhibit containing any such calculations or analysis used.

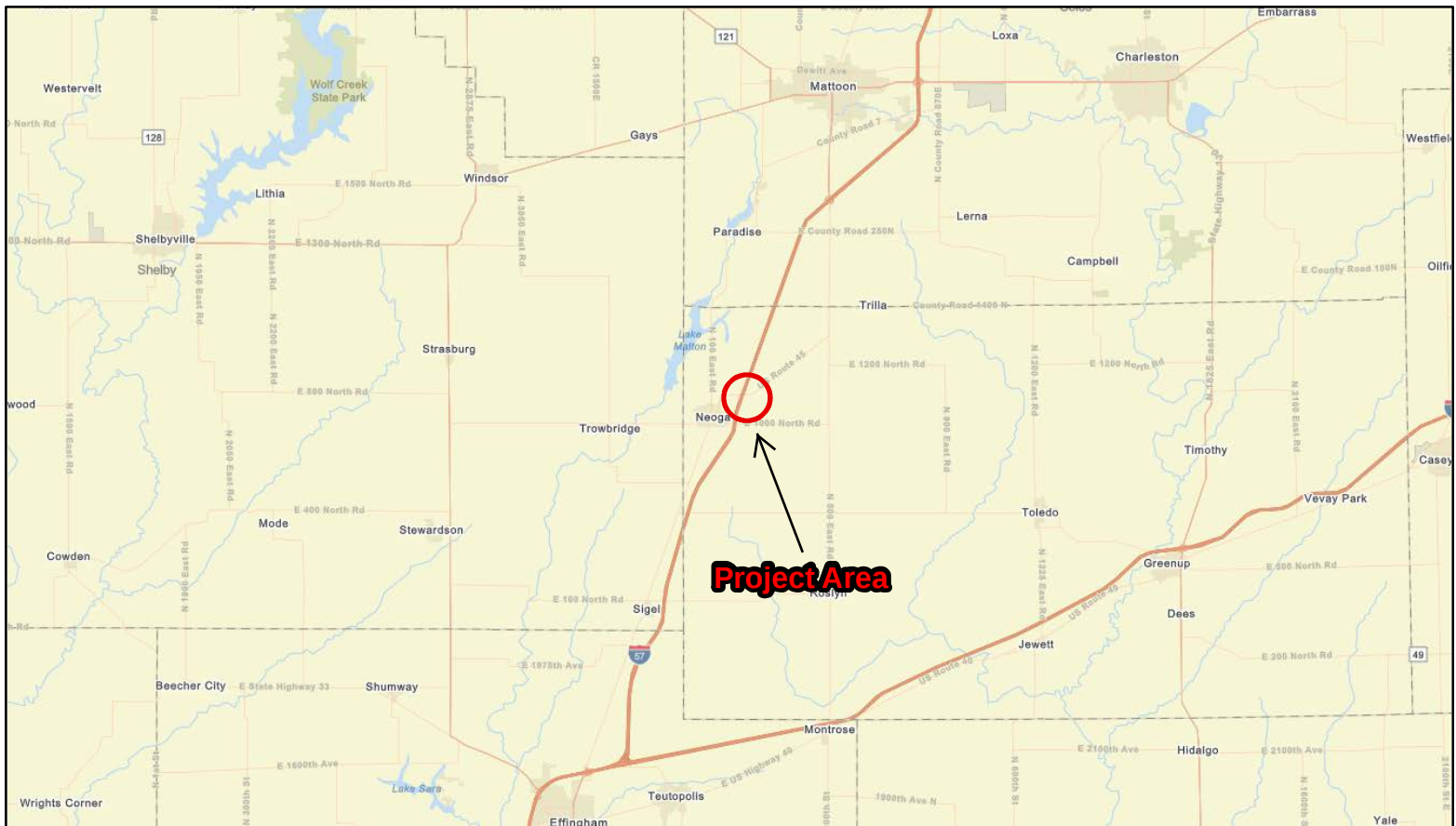
7.0 Geotechnical Data

Soil boring logs can be found in Exhibit C. The Subsurface Profile can be found in Exhibit D.

8.0 Limitations

The recommendations provided herein are for the exclusive use of BLA Inc. and the Illinois Department of Transportation (IDOT) District 7. They are specific only to the project described and are based on the subsurface information obtained by KEG at two boring locations within the structure area, KEG's understanding of the project as described herein, and geotechnical engineering practice consistent with the standard of care. No other warranty is expressed or implied. KEG should be contacted if conditions encountered during construction are not consistent with those described.

EXHIBIT A
LOCATION MAP



LOCATION MAP

I-57 over Eastern Illinois Railroad
Cumberland County, Illinois

Exhibit No.

A

KEG JOB #20-1152.00

EXHIBIT B

TYPE, SIZE, AND LOCATION PLAN (TS&L)

Benchmark: BM 701 - Chiseled square on the N.W. corner of north bound I57 over railroad bridge.
Sta. 6055+20, RT 24', Elev. 692.845

Existing Structures: SN 018-0001 (SB) and SN 018-0002 (NB) were originally constructed in 1963. The structures consist of three-span continuous wide flange beams with a 7" concrete deck. The structure is skewed 56°44'52" right forward relative to I-57 with an out to out width of 36'-4" northbound and varies from 36'-4" to 39'-7¼" for southbound. Back to back abutments is 294'-6"

Traffic Control: This bridge will be built with a crossover.

No Salvage.

Note:
No freefall deck drains will be permitted in the span over the tracks or within 10 ft. of cross arms of a railroad pole line.

HIGHWAY CLASSIFICATION

F.A.I. 57 (I-57)
Functional Class: Interstate
NBL ADT: 9,300 (2019); 13,500 (2044)
NBL DHV: 1,377 (2044)
NBL ADTT: 3,553 (2019); 4,779 (2044)
SBL ADT: 9,800 (2019); 13,900 (2044)
SBL DHV: 1,418 (2044)
SBL ADTT: 3,852 (2019); 5,102 (2044)
Design Speed: 75 m.p.h.
Posted Speed: 70 m.p.h.

SEISMIC DATA

Seismic Performance Zone (SPZ) = 1
Design Spectral Acceleration at 1.0 sec. (SD1) = 0.095
Design Spectral Acceleration at 0.2 sec. (SDS) = 0.121
Soil Site Class = D

DESIGN SPECIFICATIONS

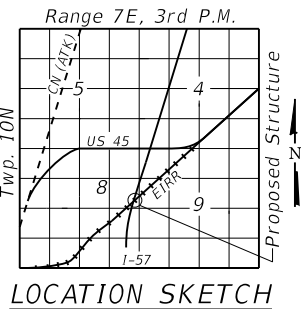
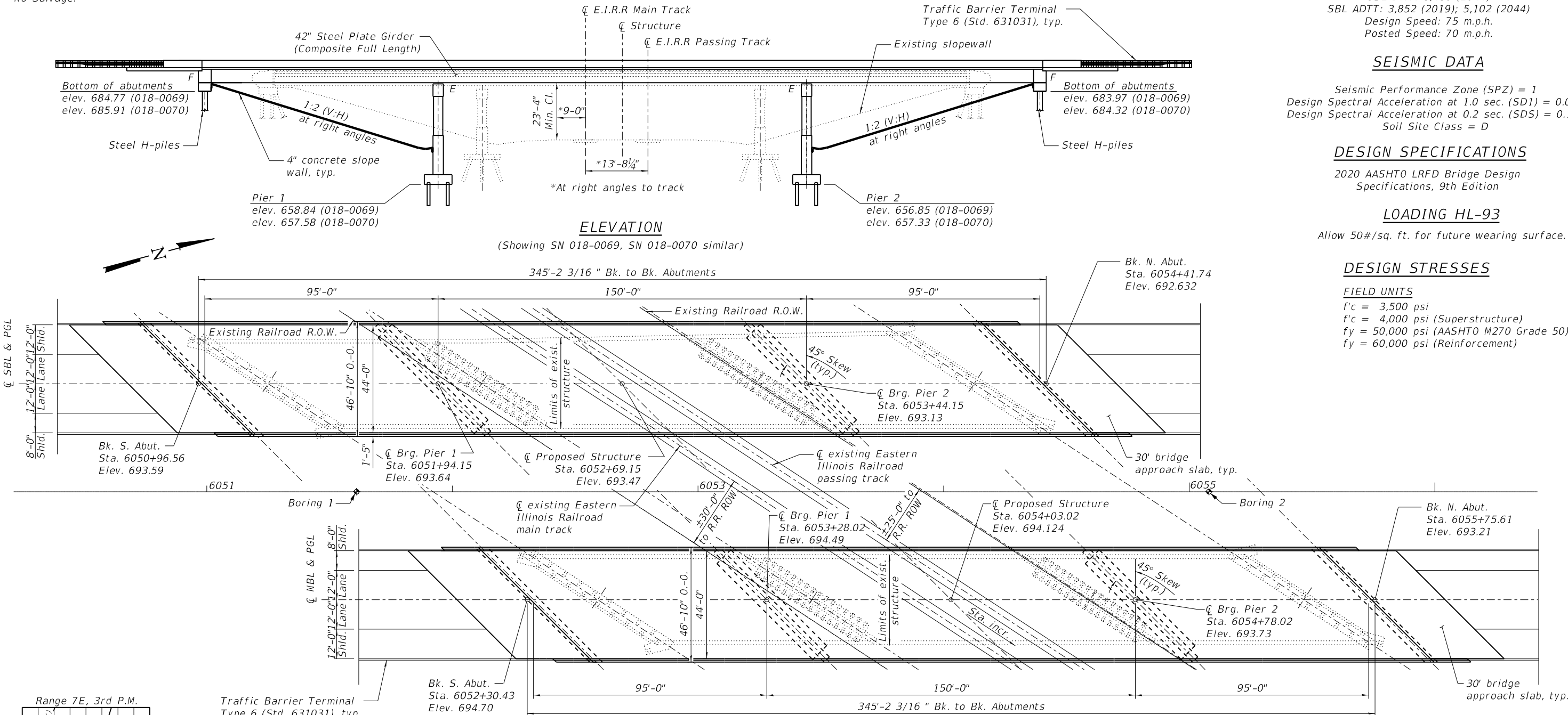
2020 AASHTO LRFD Bridge Design Specifications, 9th Edition

LOADING HL-93

Allow 50#/sq. ft. for future wearing surface.

DESIGN STRESSES

FIELD UNITS
f'c = 3,500 psi
f'c = 4,000 psi (Superstructure)
fy = 50,000 psi (AASHTO M270 Grade 50)
fy = 60,000 psi (Reinforcement)



PLAN

GENERAL PLAN & ELEVATION
I-57 OVER EASTERN ILLINOIS RAILROAD
FAI RTE 57 - SECTION 18-1VB
CUMBERLAND COUNTY
STATION 6053+34.087
STRUCTURE NO. 018-0069 (SB)
STRUCTURE NO. 018-0070 (NB)



USER NAME = kpatel	DESIGNED -	REVISED -
PLOT SCALE =	CHECKED -	REVISED -
PLOT DATE = 10/8/2021	DRAWN -	REVISED -
	CHECKED -	REVISED -

STATE OF ILLINOIS
DEPARTMENT OF TRANSPORTATION

SHEET NO. 1 OF 2 SHEETS

F.A.I. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
57	18-1VB	CUMBERLAND	2	1
CONTRACT NO. 74597				
ILLINOIS FED. AID PROJECT				

EXHBIT C
BORING LOGS

Page 1 of 3

Date 10/8/20

BBS, form 137 (Rev. 8-99)

ROUTE	FAI 57 (I-57)	DESCRIPTION	I-57 over Eastern Illinois Railroad	LOGGED BY	Sandschafer

SECTION (18-1VB, 18-20HB)B **LOCATION** NW 1/4, SEC. 8, TWP. 10N, RNG. 7E, 3rd PM, Lat N 39.3256, Long W 88.4358

COUNTY Cumberland **DRILLING METHOD** Hollow Steam Auger & Split Spoon **HAMMER TYPE** AUTO 140#

STRUCT. NO.	018-0001, -0002 (E)
	018-0069, -0070 (P)
Station	6053+21.53

BORING NO.	<u>B-1 (South Abutment)</u>
Station	<u>6051+61</u>
Offset	<u>0.0 ft</u>
Ground Surface Elev.	690.19

018-0001, -0002 (E) 018-0069, -0070 (P)		DEPTH (ft)	BLOWS (/6")	UCS Qu (tsf)	MOIST (%)	Surface Water Elev. NA ft			DEPTH (ft)	BLOWS (/6")	UCS Qu (tsf)	MOIST (%)
Station 6053+21.53						Stream Bed Elev. NA ft						
BORING NO. B-1 (South Abutment)						Groundwater Elev.:						
Station 6051+61						First Encounter 641.2 ft						
Offset 0.0 ft						Upon Completion 658.2 ft						
Ground Surface Elev. 690.19 ft						After 24 Hrs. 656.2 ft						
Medium, moist, brown and grey, SILTY CLAY LOAM			23	0.8B	23	Very stiff, moist, grey, SANDY CLAY (Till)			2322	2.5S	12	
645.2			5			625.7						
Soft, moist, grey, SANDY LOAM			713	0.4S	16	Hard, moist, brown, CLAY (Till)			112031	4.5B	10	
640.7												
Medium, wet, grey, fine, SAND 14% passing #200 Sieve			467		18	Grey			71330	5.6B	9	
635.7												
Very stiff, moist, grey, SANDY CLAY (Till)			41521	2.8S	12				5812	4.1B	16	
630.2			11									

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, form 137 (Rev. 8-99)

Page 3 of 3

Date 10/8/20

BBS, form 137 (Rev. 8-99)

ROUTE	<u>FAI 57 (I-57)</u>	DESCRIPTION	<u>I-57 over Eastern Illinois Railroad</u>	LOGGED BY	<u>E. Sandschafer</u>
--------------	----------------------	--------------------	--	------------------	-----------------------

SECTION (18-1VB, 18-20HB)B **LOCATION** NW 1/4, SEC. 8, TWP. 10N, RNG. 7E, 3rd PM, Lat N 39.3265, Long W 88.4354

COUNTY Cumberland **DRILLING METHOD** Hollow Steam Auger & Split Spoon **HAMMER TYPE** AUTO 140#

STRUCT. NO.	018-0001, -0002 (E)
	018-0069, -0070 (P)
Station	6053+21.53

BORING NO.	<u>B-2 (North Abutment)</u>
Station	<u>6055+08</u>
Offset	<u>0.0 ft</u>
Ground Surface Elev.	<u>690.51</u>

STRUCT. NO. 018-0001, -0002 (E) 018-0069, -0070 (P) Station 6053+21.53		DEPTH (ft)	BLOWS (/6")	UCS Qu (tsf)	MOIST (%)	Surface Water Elev. NA ft Stream Bed Elev. NA ft			DEPTH (ft)	BLOWS (/6")	UCS Qu (tsf)	MOIST (%)
BORING NO. B-2 (North Abutment) Station 6055+08 Offset 0.0 ft Ground Surface Elev. 690.51 ft						Groundwater Elev.: First Encounter 646.0 ft Upon Completion 660.5 ft After 24 Hrs. 677.0 ft						
Brown, CLAY						Stiff, moist, brown and grey, CLAY (Embankment)				3 4	1.2 B	18
Hard, moist (Embankment)			5	4.5 P	10	Very stiff, grey (Embankment)				3 4 5	2.9 B	16
			4 5	1.1 E	12	Stiff (Embankment)				1 3 4	1.7 B	17
Stiff, brown and grey marbled, with silt (Embankment)			3 3 4	1.1 B	21	Very stiff, brown and grey marbled (Embankment)				1 3 5	2.1 B	16
Very stiff (Embankment)			3 3 5	2.1 B	23	Stiff, moist, grey, SILTY LOAM				2 2 3	1.7 BS	21
Stiff (Embankment)			2 3 4	1.4 B	21							
Very Stiff (Embankment)			1 3 4	2.5 B	23	Stiff, moist, grey and brown marbled, CLAY				1 2 3	1.2 B	23
Stiff (Embankment)			2 2 4	1.7 B	22							
			1							1		

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

BBS, form 137 (Rev. 8-99)

Page 2 of 3

Date 10/7/20

[illegible]

BBS, form 137 (Rev. 8-99)

ROUTE	<u>FAI 57 (I-57)</u>	DESCRIPTION	<u>I-57 over Eastern Illinois Railroad</u>	LOGGED BY	<u>E. Sandschafer</u>
--------------	----------------------	--------------------	--	------------------	-----------------------

SECTION (18-1VB, 18-20HB)B **LOCATION** NW 1/4, SEC. 8, TWP. 10N, RNG. 7E, 3rd PM, Lat N 39.3265, Long W 88.4354

COUNTY Cumberland **DRILLING METHOD** Hollow Steam Auger & Split Spoon **HAMMER TYPE** AUTO 140#

STRUCT. NO.	018-0001, -0002 (E)
	018-0069, -0070 (P)
Station	6053+21.53

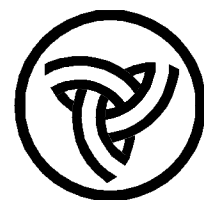
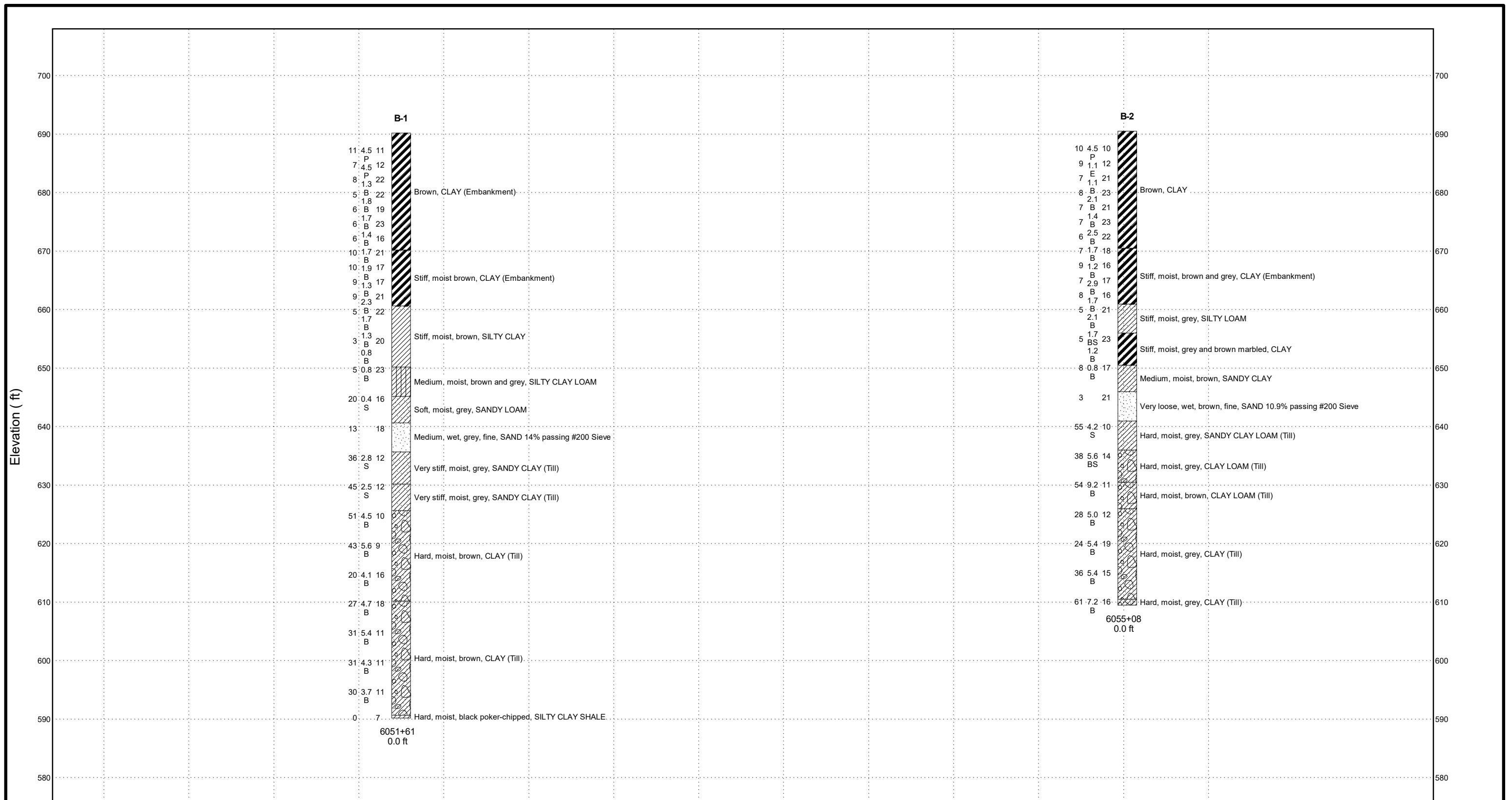
BORING NO.	<u>B-2 (North Abutment)</u>
Station	<u>6055+08</u>
Offset	<u>0.0 ft</u>
Ground Surface Elev.	<u>690.51</u>

DEPTH	BLOWS	UCS	MOIST
(ft)	(/6")	(tsf)	(%)

Surface Water Elev.	NA	ft
Stream Bed Elev.	NA	ft
Groundwater Elev.:		
First Encounter	646.0	ft ▼
Upon Completion	660.5	ft ▼
After 24 Hrs.	677.0	ft ▼

Hard, moist, grey, CLAY (Till)	609.5	27 34	7.2 B	16	
Benchmark: BM 702 - Chiseled square on Southeast corner of FAI 57 bridge over Railroad End of Boring					

EXHIBIT D
SUBSURFACE PROFILE



**Illinois Department
of Transportation**
Division of Highways

NOT TO HORIZONTAL SCALE

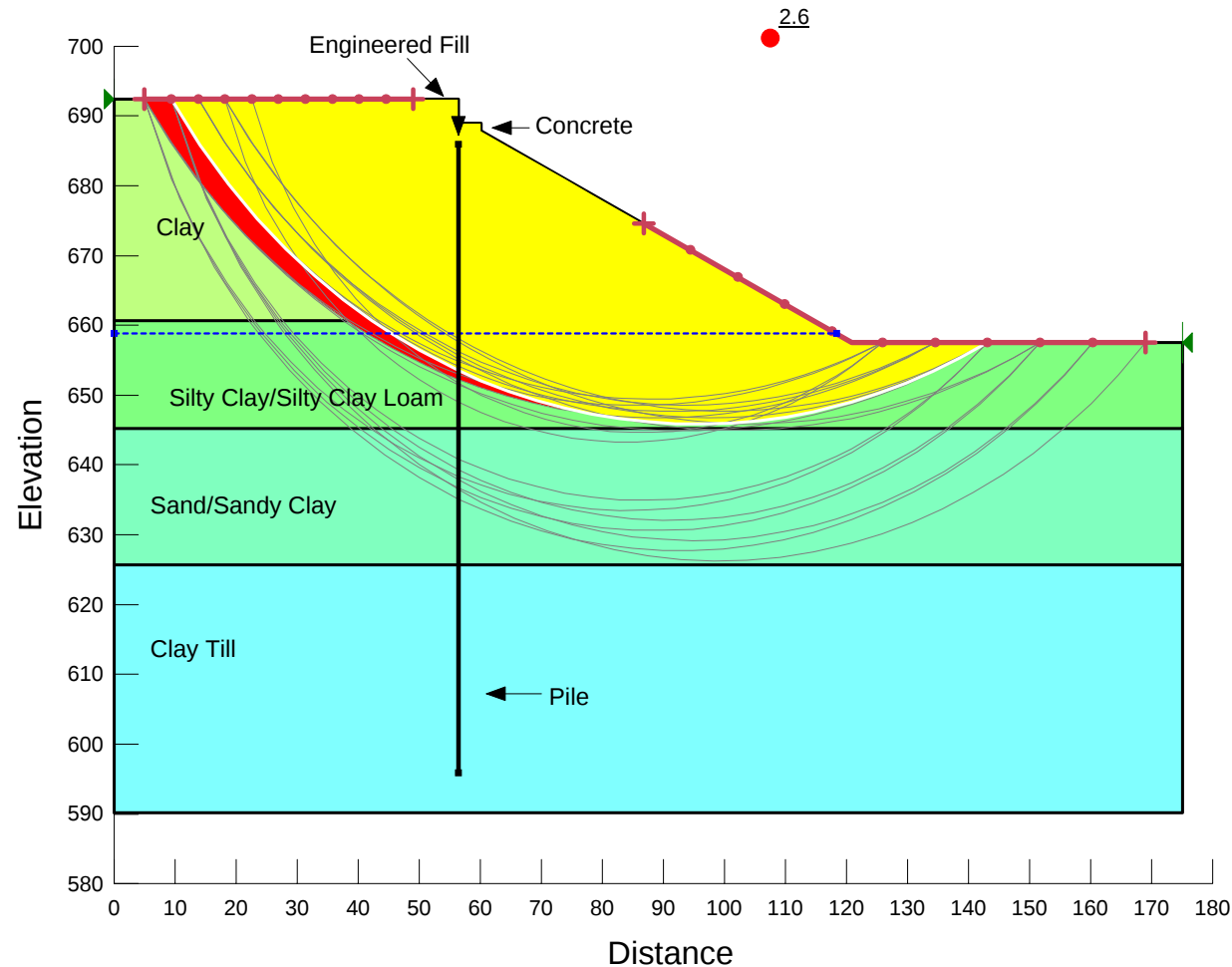
SUBSURFACE DATA PROFILE

Route: FAI 57 (I-57)
Section: (18-1VB, 18-20HB)B
County: Cumberland

EXHIBIT E

SLOPE W SLOPE STABILITY ANALYSIS

IL 57 Over Eastern Illinois Railroad
South Abutment (B-1)
End-of-Construction (Undrained Analysis)



Name: Engineered Fill
Model: Mohr-Coulomb
Unit Weight: 125 pcf
Cohesion': 1,500 psf
Phi': 0 °

Name: Clay
Model: Mohr-Coulomb
Unit Weight: 120 pcf
Cohesion': 2,000 psf
Phi': 0 °

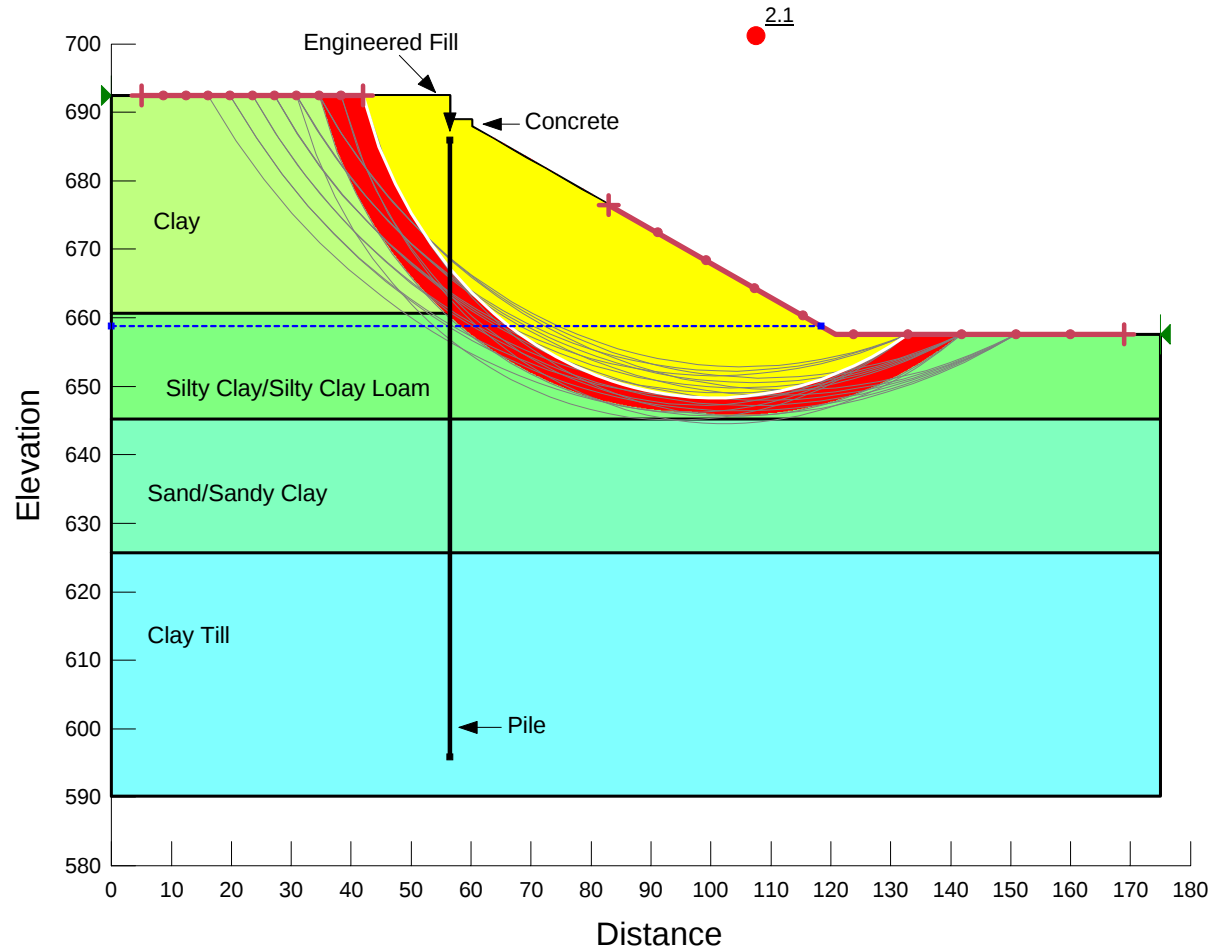
Name: Silty Clay/Silty Clay Loam
Model: Mohr-Coulomb
Unit Weight: 120 pcf
Cohesion': 950 psf
Phi': 0 °

Name: Sand/Sandy Clay
Model: Mohr-Coulomb
Unit Weight: 120 pcf
Cohesion': 1,900 psf
Phi': 0 °

Name: Clay Till
Model: Mohr-Coulomb
Unit Weight: 130 pcf
Cohesion': 4,600 psf
Phi': 0 °

Name: Concrete
Model: Mohr-Coulomb
Unit Weight: 150 pcf
Cohesion': 20,000 psf
Phi': 0 °

IL 57 Over Eastern Illinois Railroad
South Abutment (B-1)
Long Term (Drained Analysis)



Name: Engineered Fill
Model: Mohr-Coulomb
Unit Weight: 125 pcf
Cohesion': 100 psf
Phi': 26 °

Name: Clay
Model: Mohr-Coulomb
Unit Weight: 120 pcf
Cohesion': 100 psf
Phi': 28 °

Name: Silty Clay/Silty Clay Loam
Model: Mohr-Coulomb
Unit Weight: 120 pcf
Cohesion': 100 psf
Phi': 26 °

Name: Sand/Sandy Clay
Model: Mohr-Coulomb
Unit Weight: 120 pcf
Cohesion': 100 psf
Phi': 30 °

Name: Clay Till
Model: Mohr-Coulomb
Unit Weight: 130 pcf
Cohesion': 150 psf
Phi': 28 °

Name: Concrete
Model: Mohr-Coulomb
Unit Weight: 150 pcf
Cohesion': 250 psf
Phi': 45 °

**IL 57 Over Eastern Illinois Railroad
North Abutment (B-2)
End-of Construction (Undrained Analysis)**

Name: Engineered Fill
Model: Mohr-Coulomb
Unit Weight: 125 pcf
Cohesion': 1,500 psf
Phi': 0 °

Name: Clay I
Model: Mohr-Coulomb
Unit Weight: 120 pcf
Cohesion': 2,000 psf
Phi': 0 °

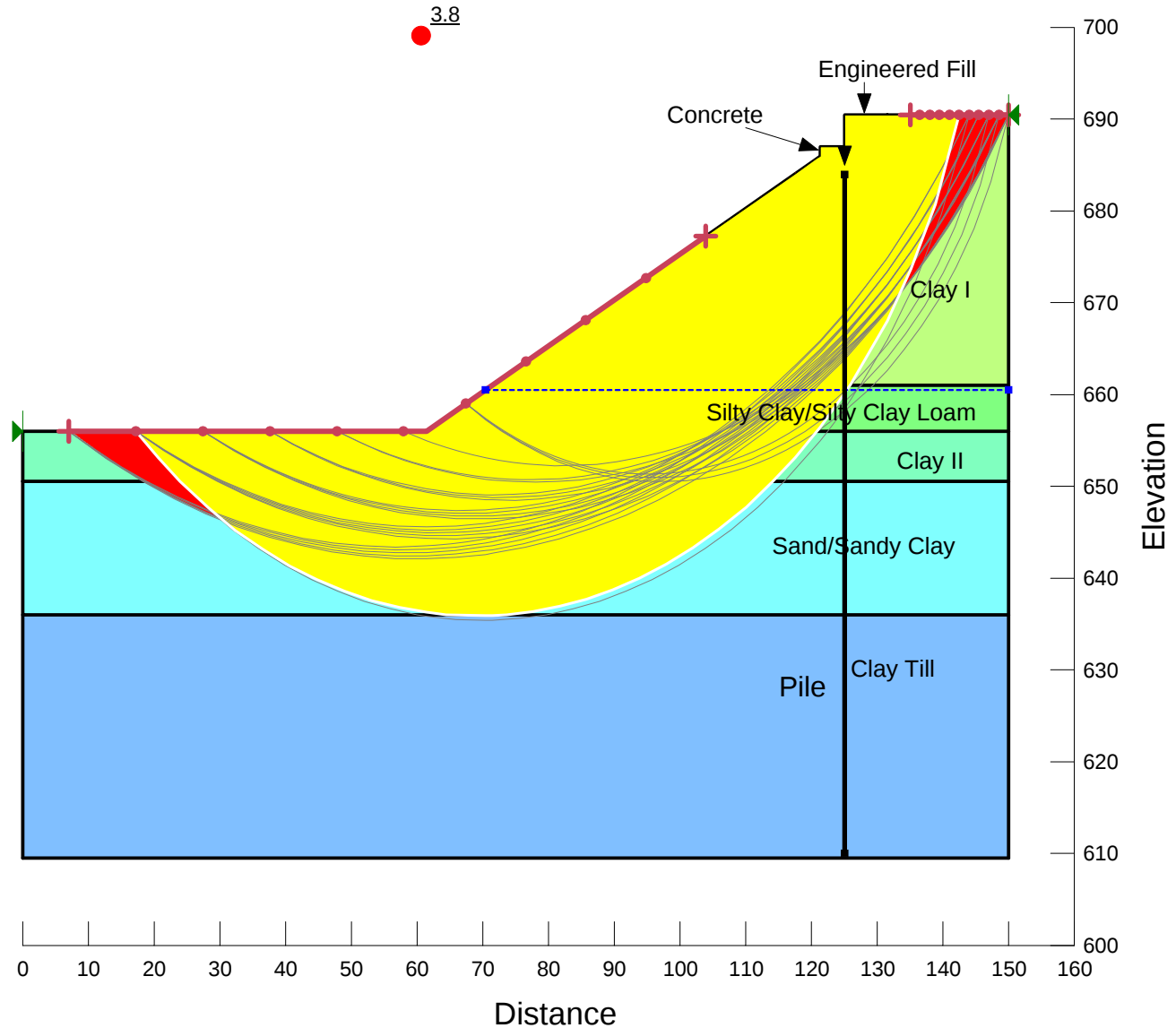
Name: Silty Clay/Silty Clay Loam
Model: Mohr-Coulomb
Unit Weight: 120 pcf
Cohesion': 1,700 psf
Phi': 0 °

Name: Clay II
Model: Mohr-Coulomb
Unit Weight: 120 pcf
Cohesion': 1,200 psf
Phi': 0 °

Name: Sandy/Sandy Clay
Model: Mohr-Coulomb
Unit Weight: 120 pcf
Cohesion': 1,000 psf
Phi': 0 °

Name: Clay Till
Model: Mohr-Coulomb
Unit Weight: 130 pcf
Cohesion': 6,000 psf
Phi': 0 °

Name: Concrete
Model: Mohr-Coulomb
Unit Weight: 150 pcf
Cohesion': 20,000 psf
Phi': 0 °



IL 57 Over Eastern Illinois Railroad North Abutment (B-2) Long Term (Drained Analysis)

Name: Engineered Fill
Model: Mohr-Coulomb
Unit Weight: 125 pcf
Cohesion': 100 psf
Phi': 26 °

Name: Clay I
Model: Mohr-Coulomb
Unit Weight: 120 pcf
Cohesion': 100 psf
Phi': 26 °

Name: Silty Clay/Silty Clay Loam
Model: Mohr-Coulomb
Unit Weight: 120 pcf
Cohesion': 100 psf
Phi': 26 °

Name: Clay II
Model: Mohr-Coulomb
Unit Weight: 120 pcf
Cohesion': 100 psf
Phi': 26 °

Name: Sandy/Sandy Clay
Model: Mohr-Coulomb
Unit Weight: 120 pcf
Cohesion': 100 psf
Phi': 28 °

Name: Clay Till
Model: Mohr-Coulomb
Unit Weight: 130 pcf
Cohesion': 150 psf
Phi': 28 °

Name: Concrete
Model: Mohr-Coulomb
Unit Weight: 150 pcf
Cohesion': 250 psf
Phi': 45 °

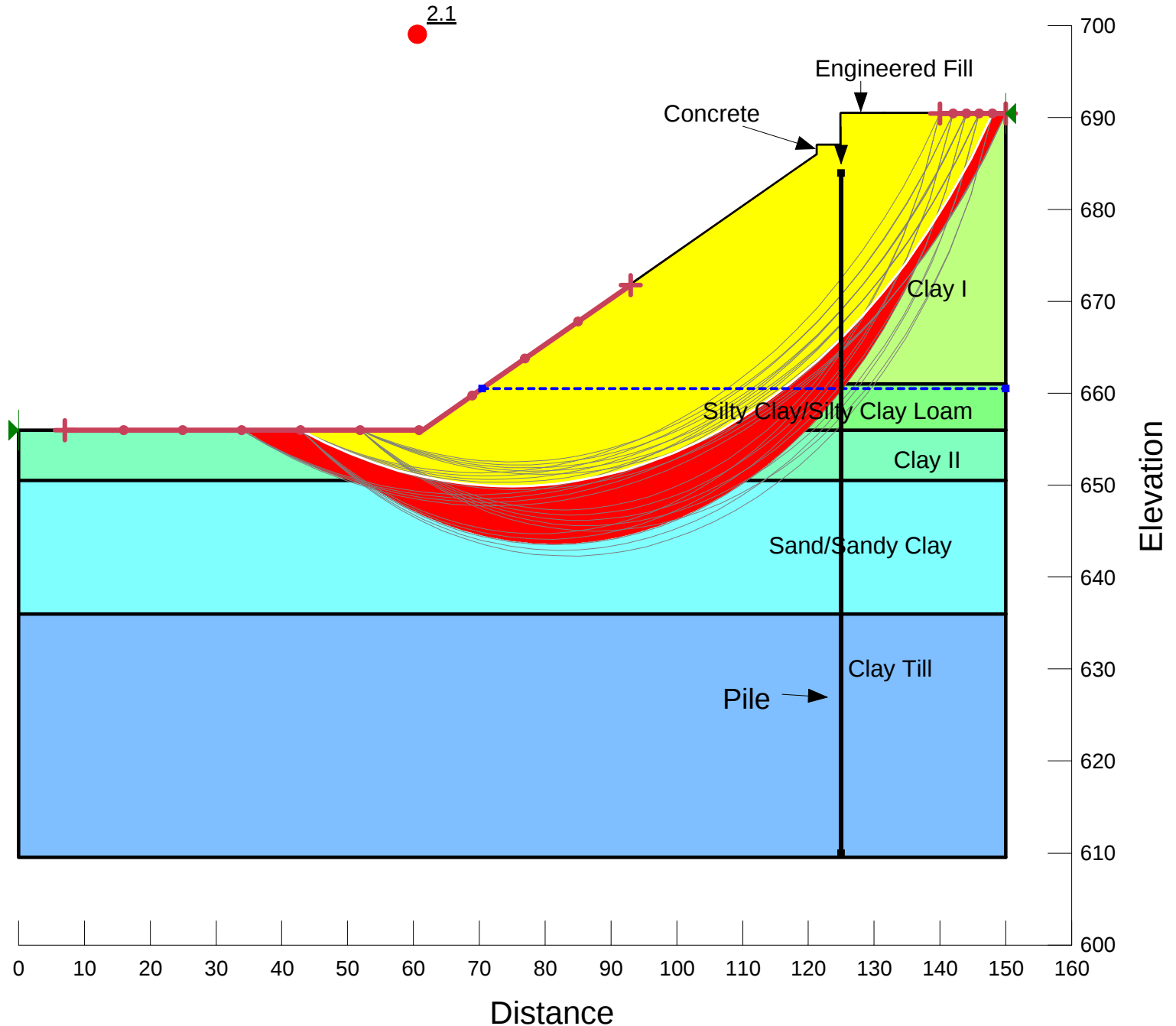


EXHIBIT F

BEARING RESISTANCE CALCULATIONS

Bearing Capacity for Continuous Foundations (Terzaghi)

Top of Rail Elevation = 665.48 ft

GSE = 658.84 ft

Ref 1 (B-01)

$$q_{ultimate} = c' N_c + \sigma'_{20} N_q + 0.5 \gamma' B N_\gamma$$

$$\sigma'_{20} = \gamma' D_f \quad (\gamma' = \gamma)$$

Bearings in Clay to Silty Clay (Based on B-01)

Parameters: q_{ult} = Ultimate Bearing Capacity

$$c' = 1300 \text{ psf}$$

$$\phi' = 0$$

$$\gamma = 120 \text{ psf}$$

$$D_f = 6.64 \text{ ft}$$

$$B = 8 \text{ ft}$$

Table 6.1

$$\begin{cases} N_c = 5.7 \\ N_q = 1.0 \\ N_\gamma = 0.0 \end{cases}$$

$$q_u = (1300 \text{ psf})(5.7) + (120 \text{ psf})(6.64 \text{ ft})(1.0) + 0.5(120 \text{ psf})(8 \text{ ft})(0.0)$$

$$q_u = (7410 \text{ psf}) + 796.8 \text{ psf} = 8206.8 \text{ psf}$$

$$q_{allowable} = \frac{q_{ultimate}}{\text{Factor of Safety}} = \frac{8206.8 \text{ psf}}{2.0} = 4103.4 \text{ psf}$$

$$q_{allowable} = 4100 \text{ psf}$$

Sliding Bearing Resistance

Part 1

Sliding Bearing Resistance = $\frac{1}{2} \gamma$ or Cohesion
* use lesser of the two values

Parameters: Cohesion = ~~800~~ psf

1,300psf

$\gamma = 120$ psf

$R_{ph} = 6.64$ ft

$$\frac{1}{2} \gamma = \frac{1}{2} (120 \text{ psf} \times 6.64 \text{ ft}) = 398.4 \text{ psf}$$

$$398.4 \text{ psf} < 1300 \text{ psf}$$

$$\boxed{\text{Sliding Bearing Resistance} = 398.4 \text{ psf}}$$

EXHIBIT G

PILE LENGTH/PILE TYPE

SUBSTRUCTURE===== **South Abutment (SN 18-0069)**
 REFERENCE BORING ===== **B-1**
 LRFD or ASD or SEISMIC ===== **LRFD**
 PILE CUTOFF ELEV. ===== **686.77** ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = **684.77** ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== **None**
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of <u>Pile</u>	Maximum Nominal Req'd Bearing of <u>Boring</u>	Maximum Factored Resistance Available in <u>Boring</u>	Maximum Pile Driveable Length in <u>Boring</u>
459 KIPS	313 KIPS	172 KIPS	56 FT.

TOTAL FACTORED SUBSTRUCTURE LOAD ===== **1650** kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== **46.83** ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== **1**
 Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 281.87 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 105.70 KIPS

PILE TYPE AND SIZE ===== **Metal Shell 14"Φ w/.25" walls**
 Pile Perimeter===== 3.665 FT.
 Pile End Bearing Area===== 1.069 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL						NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)								
683.19	1.58	4.50	7		18.8		34.1				34	0	0	19	4
680.69	2.50	1.30			12.5	15.2	52.4				52	0	0	29	6
678.19	2.50	1.80			15.6	21.1	66.8				67	0	0	37	9
675.69	2.50	1.70			15.0	19.9	78.4				78	0	0	43	11
673.19	2.50	1.40			13.2	16.4	95.0				95	0	0	52	14
670.69	2.50	1.70			15.0	19.9	112.4				112	0	0	62	16
668.19	2.50	1.90			16.2	22.3	121.5				122	0	0	67	19
665.69	2.50	1.30			12.5	15.2	145.7				146	0	0	80	21
663.19	2.50	2.30			18.3	27.0	156.9				157	0	0	86	24
660.69	2.50	1.70			15.0	19.9	167.3				167	0	0	92	26
655.69	5.00	1.30			24.9	15.2	186.4				186	0	0	102	31
650.69	5.00	0.80			16.9	9.4	203.3				203	0	0	112	36
645.69	5.00	0.80			16.9	9.4	215.6				216	0	0	119	41
640.69	5.00	0.40			9.1	4.7	307.4				307	0	0	169	46
635.69	5.00		13	Medium Sand	21.9	87.5	274.7				275	0	0	151	51
630.69	5.00	2.80			41.8	32.8	313.0				313	0	0	172	56
625.69	5.00	2.50			38.6	29.3	579.7				580	0	0	319	61
620.69	5.00		51	Hard Till	60.8	257.4	600.1				600	0	0	330	66
615.69	5.00		43	Hard Till	47.1	217.0	531.1				531	0	0	292	71
610.69	5.00		20	Hard Till	20.2	100.9	586.6				587	0	0	323	76
605.69	5.00		27	Hard Till	27.3	136.3	634.0				634	0	0	349	81
600.69	5.00		31	Hard Till	31.2	156.5	665.2				665	0	0	366	86
595.69	5.00		31	Hard Till	31.2	156.5	691.3				691	0	0	380	91
590.69	5.00		30	Hard Till	30.1	151.4	906.5				907	0	0	499	96
589.69	1.00			Shale	230.7	336.5	1137.2				1137	0	0	625	97.1
588.69	1.00			Shale	230.7	336.5	1368.0				1368	0	0	752	98.1
588.19	0.50			Shale	115.4	336.5	1483.3				1483	0	0	816	98.6
587.69	0.50			Shale	115.4	336.5	1598.7				1599	0	0	879	99.1
587.19	0.50			Shale	115.4	336.5	1714.0				1714	0	0	943	99.6
586.69	0.50			Shale	115.4	336.5	1829.4				1829	0	0	1006	100.1
586.19	0.50			Shale	115.4	336.5	1944.8				1945	0	0	1070	100.6
585.69	0.50			Shale	115.4	336.5	2060.1				2060	0	0	1133	101.1
585.19	0.50			Shale	115.4	336.5	2175.5				2175	0	0	1197	101.6
584.69	0.50			Shale	115.4	336.5	2290.9				2291	0	0	1260	102.1
584.19	0.50			Shale	115.4	336.5	2406.2				2406	0	0	1323	102.6
583.69	0.50			Shale	115.4	336.5	2521.6				2522	0	0	1387	103.1
583.19	0.50			Shale	115.4	336.5	2636.9				2637	0	0	1450	103.6
582.69	0.50			Shale		336.5									

SUBSTRUCTURE===== Pier 1 (SN 18-0069)
REFERENCE BORING ===== B-1
LRFD or ASD or SEISMIC ===== LRFD
PILE CUTOFF ELEV. ===== 659.84 ft
GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 658.84 ft
GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== None
BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft
TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

TOTAL FACTORED SUBSTRUCTURE LOAD ===== 3780 kips
TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 46.83 ft
NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 1

Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 645.74 KIPS
Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 242.15 KIPS

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
459 KIPS	425 KIPS	234 KIPS	49 FT.

PILE TYPE AND SIZE ===== Metal Shell 14"Φ w/.25" walls
Pile Perimeter===== 3.665 FT.
Pile End Bearing Area===== 1.069 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL						NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)								
655.69	3.15	1.30			15.7		25.1				25	0	0	14	4
645.69	10.00	0.80			33.9	9.4	54.3				54	0	0	30	14
640.69	5.00	0.40			9.1	4.7	146.2				146	0	0	80	19
635.69	5.00		13	Medium Sand	21.9	87.5	113.5				113	0	0	62	24
630.69	5.00	2.80			41.8	32.8	151.7				152	0	0	83	29
625.69	5.00	2.50			38.6	29.3	418.5				418	0	0	230	34
620.69	5.00		51	Hard Till	60.8	257.4	438.9				439	0	0	241	39
615.69	5.00		43	Hard Till	47.1	217.0	369.8				370	0	0	203	44
610.69	5.00		20	Hard Till	20.2	100.9	425.3				425	0	0	234	49
605.69	5.00		27	Hard Till	27.3	136.3	472.8				473	0	0	260	54
600.69	5.00		31	Hard Till	31.2	156.5	504.0				504	0	0	277	59
595.69	5.00		31	Hard Till	31.2	156.5	530.1				530	0	0	292	64
590.69	5.00		30	Hard Till	30.1	151.4	745.2				745	0	0	410	69
589.69	1.00			Shale	230.7	336.5	976.0				976	0	0	537	70.2
588.69	1.00			Shale	230.7	336.5	1206.7				1207	0	0	664	71.2
588.19	0.50			Shale	115.4	336.5	1322.1				1322	0	0	727	71.7
587.69	0.50			Shale	115.4	336.5	1437.4				1437	0	0	791	72.2
587.19	0.50			Shale	115.4	336.5	1552.8				1553	0	0	854	72.7
586.69	0.50			Shale	115.4	336.5	1668.1				1668	0	0	917	73.2
586.19	0.50			Shale	115.4	336.5	1783.5				1784	0	0	981	73.7
585.69	0.50			Shale	115.4	336.5	1898.9				1899	0	0	1044	74.2
585.19	0.50			Shale	115.4	336.5	2014.2				2014	0	0	1108	74.7
584.69	0.50			Shale	115.4	336.5	2129.6				2130	0	0	1171	75.2
584.19	0.50			Shale	115.4	336.5	2245.0				2245	0	0	1235	75.7
583.69	0.50			Shale	115.4	336.5	2360.3				2360	0	0	1298	76.2
583.19	0.50			Shale	115.4	336.5	2475.7				2476	0	0	1362	76.7
582.69	0.50			Shale	115.4	336.5	2591.0				2591	0	0	1425	77.2
582.19	0.50			Shale	115.4	336.5	2706.4				2706	0	0	1489	77.7
581.69	0.50			Shale	115.4	336.5	2821.8				2822	0	0	1552	78.2
581.19	0.50			Shale	115.4	336.5	2937.1				2937	0	0	1615	78.7
580.69	0.50			Shale	115.4	336.5	3052.5				3052	0	0	1679	79.2
580.19	0.50			Shale	115.4	336.5	3167.8				3168	0	0	1742	79.7
579.69	0.50			Shale	115.4	336.5	3283.2				3283	0	0	1806	80.2
579.19	0.50			Shale											

SUBSTRUCTURE===== Pier 2 (SN 18-0069)
 REFERENCE BORING ===== B-2
 LRFD or ASD or SEISMIC ===== LRFD
 PILE CUTOFF ELEV. ===== 657.85 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 656.85 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== None
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

TOTAL FACTORED SUBSTRUCTURE LOAD ===== 3780 kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 46.83 ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 1

Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 645.74 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 242.15 KIPS

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
459 KIPS	458 KIPS	252 KIPS	42 FT.

PILE TYPE AND SIZE ===== Metal Shell 14"Φ w/.25" walls
 Pile Perimeter===== 3.665 FT.
 Pile End Bearing Area===== 1.069 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL						NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)								
651.01	5.84	1.20			27.5		36.8				37	0	0	20	7
646.01	5.00	0.80			16.9	9.4	64.6				65	0	0	36	12
641.01	5.00		3	Fine Sand	4.8	20.2	326.7				327	0	0	180	17
636.01	5.00		55	Hard Till	68.6	277.6	309.5				310	0	0	170	22
631.01	5.00		38	Hard Till	39.7	191.8	430.0				430	0	0	237	27
626.01	5.00		54	Hard Till	66.6	272.5	365.4				365	0	0	201	32
621.01	5.00		28	Hard Till	28.3	141.3	373.4				373	0	0	205	37
616.01	5.00		24	Hard Till	24.2	121.1	458.2				458	0	0	252	42
611.01	5.00		36	Hard Till	37.1	181.7	621.5				622	0	0	342	47
609.51	1.50		61	Hard Till	24.4	307.9	645.9				646	0	0	355	48
604.51	5.00		61	Hard Till	81.5	307.9	727.4				727	0	0	409	53
599.51	5.00		61	Hard Till	81.5	307.9	808.9				809	0	0	445	58
594.51	5.00		61	Hard Till	81.5	307.9	890.3				890	0	0	490	63
590.69	3.82		61	Hard Till	62.2	307.9	981.2				981	0	0	540	67
589.69	1.00			Shale	230.7	336.5	1211.9				1212	0	0	667	68.2
588.69	1.00			Shale	230.7	336.5	1442.6				1443	0	0	793	69.2
587.69	1.00			Shale	230.7	336.5	1673.3				1673	0	0	920	70.2
586.69	1.00			Shale	230.7	336.5	1904.0				1904	0	0	1047	71.2
585.69	1.00			Shale	230.7	336.5	2134.8				2135	0	0	1174	72.2
584.69	1.00			Shale	230.7	336.5	2365.5				2365	0	0	1301	73.2
583.69	1.00			Shale	230.7	336.5	2596.2				2596	0	0	1428	74.2
582.69	1.00			Shale	230.7	336.5	2826.9				2827	0	0	1555	75.2
581.69	1.00			Shale	230.7	336.5	3057.7				3058	0	0	1682	76.2
580.69	1.00			Shale	230.7	336.5	3288.4				3288	0	0	1809	77.2
579.69	1.00			Shale	230.7	336.5	3519.1				3519	0	0	1936	78.2
578.69	1.00			Shale		336.5									

SUBSTRUCTURE=====North Abutment (SN 18-0069)
REFERENCE BORING =====B-2
LRFD or ASD or SEISMIC =====LRFD
PILE CUTOFF ELEV. =====685.97 ft
GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 683.97 ft
GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) =====None
BOTTOM ELEV. OF SCOUR, LIQUEF., or DD =====ft
TOP ELEV. OF LIQUEF. (so layers above apply DD) =====ft

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
459 KIPS	234 KIPS	129 KIPS	40 FT.

TOTAL FACTORED SUBSTRUCTURE LOAD =====1650 kips
TOTAL LENGTH OF SUBSTRUCTURE (along skew)=====46.83 ft
NUMBER OF ROWS OF PILES PER SUBSTRUCTURE =====1
Approx. Factored Loading Applied per pile at 8 ft. Cts =====281.87 KIPS
Approx. Factored Loading Applied per pile at 3 ft. Cts =====105.70 KIPS

PILE TYPE AND SIZE =====Metal Shell 14"Φ w/.25" walls
Pile Perimeter=====3.665 FT.
Pile End Bearing Area=====1.069 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL						NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)								
681.01	2.96	1.10			13.0		37.6				38	0	0	21	5
678.51	2.50	2.10			17.2	24.6	46.6				47	0	0	26	7
676.01	2.50	1.40			13.2	16.4	72.7				73	0	0	40	10
673.51	2.50	2.50			19.3	29.3	82.6				83	0	0	45	12
671.01	2.50	1.70			15.0	19.9	91.8				92	0	0	50	15
668.51	2.50	1.20			11.8	14.1	123.5				123	0	0	68	17
666.01	2.50	2.90			21.4	34.0	130.8				131	0	0	72	20
663.51	2.50	1.70			15.0	19.9	150.5				151	0	0	83	22
661.01	2.50	2.10			17.2	24.6	163.1				163	0	0	90	25
656.01	5.00	1.70			30.0	19.9	187.2				187	0	0	103	30
651.01	5.00	1.20			23.5	14.1	206.1				206	0	0	113	35
646.01	5.00	0.80			16.9	9.4	233.8				234	0	0	129	40
641.01	5.00		3	Fine Sand	4.8	20.2	496.0				496	0	0	273	45
636.01	5.00		55	Hard Till	68.6	277.6	478.7				479	0	0	263	60
631.01	5.00		38	Hard Till	39.7	191.8	599.2				599	0	0	330	65
626.01	5.00		54	Hard Till	66.6	272.5	534.6				535	0	0	294	60
621.01	5.00		28	Hard Till	28.3	141.3	542.7				543	0	0	298	65
616.01	5.00		24	Hard Till	24.2	121.1	627.5				627	0	0	345	70
611.01	5.00		36	Hard Till	37.1	181.7	790.7				791	0	0	435	75
609.51	1.50		61	Hard Till	24.4	307.9	815.2				815	0	0	448	76
604.51	5.00		61	Hard Till	81.5	307.9	896.6				897	0	0	493	81
599.51	5.00		61	Hard Till	81.5	307.9	978.1				978	0	0	538	86
594.51	5.00		61	Hard Till	81.5	307.9	1059.5				1060	0	0	583	91
590.69	3.82		61	Hard Till	62.2	307.9	1150.4				1150	0	0	633	95
589.69	1.00			Shale	230.7	336.5	1381.1				1381	0	0	760	96.3
588.69	1.00			Shale	230.7	336.5	1611.8				1612	0	0	887	97.3
587.69	1.00			Shale	230.7	336.5	1842.6				1843	0	0	1013	98.3
586.69	1.00			Shale	230.7	336.5	2073.3				2073	0	0	1140	99.3
585.69	1.00			Shale	230.7	336.5	2304.0				2304	0	0	1267	100.3
584.69	1.00			Shale	230.7	336.5	2534.7				2535	0	0	1394	101.3
583.69	1.00			Shale	230.7	336.5	2765.4				2765	0	0	1521	102.3
582.69	1.00			Shale	230.7	336.5	2996.2				2996	0	0	1648	103.3
581.69	1.00			Shale	230.7	336.5	3226.9				3227	0	0	1775	104.3
580.69	1.00			Shale	230.7	336.5	3457.6				3458	0	0	1902	105.3
579.69	1.00			Shale	230.7	336.5	3688.3				3688	0	0	2029	106.3
578.69	1.00			Shale	230.7	336.5	3919.1				3919	0	0	2155	107.3
577.69	1.00			Shale	230.7	336.5	4149.8				4150	0	0	2282	108.3
576.69	1.00			Shale	115.4	336.5	3928.7				3929	0	0	2161	109.3
	1.00			Shale											
	1.00			Shale											

SUBSTRUCTURE=====South Abutment (18-0070)
 REFERENCE BORING =====B-1
 LRFD or ASD or SEISMIC =====LRFD
 PILE CUTOFF ELEV. =====687.91 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 685.91 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) =====None
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD =====ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) =====ft

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
459 KIPS	327 KIPS	180 KIPS	57 FT.

TOTAL FACTORED SUBSTRUCTURE LOAD =====1650 kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)=====46.83 ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE =====1
 Approx. Factored Loading Applied per pile at 8 ft. Cts =====281.87 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts =====105.70 KIPS

PILE TYPE AND SIZE =====Metal Shell 14"Φ w/.25" walls
 Pile Perimeter=====3.665 FT.
 Pile End Bearing Area=====1.069 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
683.19	2.72	4.50	7		32.4		47.7	48	0	0	26	5
680.69	2.50	1.30			12.5	15.2	66.0	66	0	0	36	7
678.19	2.50	1.80			15.6	21.1	80.4	80	0	0	44	10
675.69	2.50	1.70			15.0	19.9	91.9	92	0	0	51	12
673.19	2.50	1.40			13.2	16.4	108.6	109	0	0	60	15
670.69	2.50	1.70			15.0	19.9	126.0	126	0	0	69	17
668.19	2.50	1.90			16.2	22.3	135.1	135	0	0	74	20
665.69	2.50	1.30			12.5	15.2	159.3	159	0	0	88	22
663.19	2.50	2.30			18.3	27.0	170.5	171	0	0	94	25
660.69	2.50	1.70			15.0	19.9	180.9	181	0	0	99	27
655.69	5.00	1.30			24.9	15.2	200.0	200	0	0	110	32
650.69	5.00	0.80			16.9	9.4	216.9	217	0	0	119	37
645.69	5.00	0.80			16.9	9.4	229.1	229	0	0	126	42
640.69	5.00	0.40			9.1	4.7	321.0	321	0	0	177	47
635.69	5.00		13	Medium Sand	21.9	87.5	288.3	288	0	0	159	52
630.69	5.00	2.80			41.8	32.8	326.6	327	0	0	180	57
625.69	5.00	2.50			38.6	29.3	593.3	593	0	0	326	62
620.69	5.00		51	Hard Till	60.8	257.4	613.7	614	0	0	338	67
615.69	5.00		43	Hard Till	47.1	217.0	544.7	545	0	0	309	72
610.69	5.00		20	Hard Till	20.2	100.9	600.2	600	0	0	330	77
605.69	5.00		27	Hard Till	27.3	136.3	647.6	648	0	0	356	82
600.69	5.00		31	Hard Till	31.2	156.5	678.8	679	0	0	373	87
595.69	5.00		31	Hard Till	31.2	156.5	704.9	705	0	0	388	92
590.69	5.00		30	Hard Till	30.1	151.4	920.1	920	0	0	506	97
590.19	0.50			Shale	115.4	336.5	1035.5	1035	0	0	670	97.7
589.69	0.50			Shale	115.4	336.5	1150.8	1151	0	0	633	98.2
589.19	0.50			Shale	115.4	336.5	1266.2	1266	0	0	696	98.7
588.69	0.50			Shale	115.4	336.5	1381.6	1382	0	0	760	99.2
588.19	0.50			Shale	115.4	336.5	1496.9	1497	0	0	823	99.7
587.69	0.50			Shale	115.4	336.5	1612.3	1612	0	0	887	100.2
587.19	0.50			Shale	115.4	336.5	1727.6	1728	0	0	950	100.7
586.69	0.50			Shale	115.4	336.5	1843.0	1843	0	0	1014	101.2
586.19	0.50			Shale	115.4	336.5	1958.4	1958	0	0	1077	101.7
585.69	0.50			Shale	115.4	336.5	2073.7	2074	0	0	1141	102.2
585.19	0.50			Shale	115.4	336.5	2189.1	2189	0	0	1204	102.7
584.69	0.50			Shale	115.4	336.5	2304.4	2304	0	0	1267	103.2
584.19	0.50			Shale	115.4	336.5	2419.8	2420	0	0	1331	103.7
583.69	0.50			Shale		336.5						

SUBSTRUCTURE===== **Pier 1**
REFERENCE BORING ===== **B-1**
LRFD or ASD or SEISMIC ===== **LRFD**
PILE CUTOFF ELEV. ===== **658.58** ft
GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = **657.58** ft
GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== **None**
BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft
TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of <u>Pile</u>	Maximum Nominal Req'd Bearing of <u>Boring</u>	Maximum Factored Resistance Available in <u>Boring</u>	Maximum Pile Driveable Length in <u>Boring</u>
459 KIPS	446 KIPS	245 KIPS	48 FT.

TOTAL FACTORED SUBSTRUCTURE LOAD ===== **3780** kips
TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== **46.83** ft
NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== **1**
Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 645.74 KIPS
Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 242.15 KIPS

PILE TYPE AND SIZE ===== **Metal Shell 14"Φ w/.25" walls**
Pile Perimeter===== 3.665 FT.
Pile End Bearing Area===== 1.069 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL						NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)								
655.20	2.38	0.80			8.1		17.4				17	0	0	10	3
650.20	5.00	0.80			16.9	9.4	29.7				30	0	0	16	8
645.20	5.00	0.40			9.1	4.7	121.6				122	0	0	67	13
640.70	4.50		13	Medium Sand	19.7	87.5	86.7				87	0	0	48	18
635.70	5.00	2.80			41.8	32.8	125.0				125	0	0	69	23
630.70	5.00	2.50			38.6	29.3	391.7				392	0	0	215	28
625.70	5.00		51	Hard Till	60.8	257.4	412.1				412	0	0	227	33
620.70	5.00		43	Hard Till	47.1	217.0	343.0				343	0	0	189	38
615.70	5.00		20	Hard Till	20.2	100.9	398.6				399	0	0	219	43
610.70	5.00		27	Hard Till	27.3	136.3	446.0				446	0	0	245	48
605.70	5.00		31	Hard Till	31.2	156.5	477.2				477	0	0	262	53
600.70	5.00		31	Hard Till	31.2	156.5	503.3				503	0	0	277	58
595.70	5.00		30	Hard Till	30.1	151.4	718.5				718	0	0	395	63
595.20	0.50			Shale	115.4	336.5	833.8				834	0	0	459	63.4
594.70	0.50			Shale	115.4	336.5	949.2				949	0	0	522	63.9
594.20	0.50			Shale	115.4	336.5	1064.5				1065	0	0	585	64.4
593.70	0.50			Shale	115.4	336.5	1179.9				1180	0	0	649	64.9
593.20	0.50			Shale	115.4	336.5	1295.3				1295	0	0	712	65.4
592.70	0.50			Shale	115.4	336.5	1410.6				1411	0	0	776	65.9
592.20	0.50			Shale	115.4	336.5	1526.0				1526	0	0	839	66.4
591.70	0.50			Shale	115.4	336.5	1641.4				1641	0	0	903	66.9
591.20	0.50			Shale	115.4	336.5	1756.7				1757	0	0	966	67.4
590.70	0.50			Shale	115.4	336.5	1872.1				1872	0	0	1030	67.9
590.20	0.50			Shale	115.4	336.5	1987.4				1987	0	0	1093	68.4
589.70	0.50			Shale	115.4	336.5	2102.8				2103	0	0	1157	68.9
589.20	0.50			Shale	115.4	336.5	2218.2				2218	0	0	1220	69.4
588.70	0.50			Shale	115.4	336.5	2333.5				2334	0	0	1283	69.9
588.20	0.50			Shale		336.5									

SUBSTRUCTURE===== Pier 2 (SN 18-0070)
REFERENCE BORING ===== B-2
LRFD or ASD or SEISMIC ===== LRFD
PILE CUTOFF ELEV. ===== 658.33 ft
GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 657.33 ft
GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== None
BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== ft
TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== ft

TOTAL FACTORED SUBSTRUCTURE LOAD ===== 3780 kips
TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 46.83 ft
NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 1
Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 645.74 KIPS
Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 242.15 KIPS

PILE TYPE AND SIZE ===== Metal Shell 14"Φ w/.25" walls
Pile Perimeter===== 3.665 FT.
Pile End Bearing Area===== 1.069 SQFT.

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
459 KIPS	378 KIPS	208 KIPS	37 FT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL						NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)								
656.00	1.33	1.70			8.0		22.1				22	0	0	12	2
650.50	5.50	1.20			25.9	14.1	43.2				43	0	0	24	8
646.00	4.50	0.80			15.2	9.4	69.3				69	0	0	38	12
641.00	5.00		3	Fine Sand	4.8	20.2	331.4				331	0	0	182	17
636.00	5.00		55	Hard Till	68.6	277.6	314.2				314	0	0	173	22
631.00	5.00		38	Hard Till	39.7	191.8	434.7				435	0	0	239	27
626.00	5.00		54	Hard Till	66.6	272.5	370.1				370	0	0	204	32
621.00	5.00		28	Hard Till	28.3	141.3	378.1				378	0	0	208	37
616.00	5.00		24	Hard Till	24.2	121.1	462.9				463	0	0	255	42
611.00	5.00		36	Hard Till	37.1	181.7	626.2				626	0	0	344	47
609.00	2.00		61	Hard Till	32.6	307.9	658.8				659	0	0	362	49
604.00	5.00		61	Hard Till	81.5	307.9	740.2				740	0	0	407	54
599.00	5.00		61	Hard Till	81.5	307.9	821.7				822	0	0	452	59
594.00	5.00		61	Hard Till	81.5	307.9	903.2				903	0	0	497	64
590.68	3.32		61	Hard Till	54.1	307.9	985.9				986	0	0	542	68
589.68	1.00			Shale	230.7	336.5	1216.6				1217	0	0	669	68.7
588.68	1.00			Shale	230.7	336.5	1447.3				1447	0	0	796	69.7
587.68	1.00			Shale	230.7	336.5	1678.0				1678	0	0	923	70.7
586.68	1.00			Shale	230.7	336.5	1908.7				1909	0	0	1050	71.7
585.68	1.00			Shale	230.7	336.5	2139.5				2139	0	0	1177	72.7
584.68	1.00			Shale	230.7	336.5	2370.2				2370	0	0	1304	73.7
583.68	1.00			Shale	230.7	336.5	2600.9				2601	0	0	1431	74.7
582.68	1.00			Shale	230.7	336.5	2831.6				2832	0	0	1557	75.7
581.68	1.00			Shale	230.7	336.5	3062.4				3062	0	0	1684	76.7
580.68	1.00			Shale	230.7	336.5	3293.1				3293	0	0	1811	77.7
579.68	1.00			Shale	230.7	336.5	3523.8				3524	0	0	1938	78.7
578.68	1.00			Shale		336.5									

SUBSTRUCTURE=====North Abutment (18-0070)
 REFERENCE BORING =====B-2
 LRFD or ASD or SEISMIC =====LRFD
 PILE CUTOFF ELEV. =====686.32 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 684.32 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) =====None
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD =====ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) =====ft

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
459 KIPS	235 KIPS	129 KIPS	40 FT.

TOTAL FACTORED SUBSTRUCTURE LOAD =====1650 kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)=====46.86 ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE =====1
 Approx. Factored Loading Applied per pile at 8 ft. Cts =====281.69 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts =====105.63 KIPS

PILE TYPE AND SIZE =====Metal Shell 14"Φ w/.25" walls
 Pile Perimeter=====3.665 FT.
 Pile End Bearing Area=====1.069 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
681.01	3.31	1.10			14.6		39.2	39	0	0	22	5
678.51	2.50	2.10			17.2	24.6	48.2	48	0	0	27	8
676.01	2.50	1.40			13.2	16.4	74.2	74	0	0	41	10
673.51	2.50	2.50			19.3	29.3	84.2	84	0	0	46	13
671.01	2.50	1.70			15.0	19.9	93.3	93	0	0	51	15
668.51	2.50	1.20			11.8	14.1	125.0	125	0	0	69	18
666.01	2.50	2.90			21.4	34.0	132.4	132	0	0	73	20
663.51	2.50	1.70			15.0	19.9	152.1	152	0	0	84	23
661.01	2.50	2.10			17.2	24.6	164.6	165	0	0	91	25
656.01	5.00	1.70			30.0	19.9	188.8	189	0	0	104	30
651.01	5.00	1.20			23.5	14.1	207.6	208	0	0	114	35
646.01	5.00	0.80			16.9	9.4	235.3	235	0	0	129	40
641.01	5.00		3	Fine Sand	4.8	20.2	497.5	498	0	0	274	45
636.01	5.00		55	Hard Till	68.6	277.6	480.3	480	0	0	264	50
631.01	5.00		38	Hard Till	39.7	191.8	600.8	601	0	0	330	55
626.01	5.00		54	Hard Till	66.6	272.5	536.1	536	0	0	295	60
621.01	5.00		28	Hard Till	28.3	141.3	544.2	544	0	0	299	65
616.01	5.00		24	Hard Till	24.2	121.1	629.0	629	0	0	346	70
611.01	5.00		36	Hard Till	37.1	181.7	792.3	792	0	0	436	75
609.51	1.50		61	Hard Till	24.4	307.9	816.7	817	0	0	449	77
604.51	5.00		61	Hard Till	81.5	307.9	898.2	898	0	0	494	82
599.51	5.00		61	Hard Till	81.5	307.9	979.6	980	0	0	539	87
594.51	5.00		61	Hard Till	81.5	307.9	1061.1	1061	0	0	584	92
590.69	3.82		61	Hard Till	62.2	307.9	1151.9	1152	0	0	634	96
589.69	1.00			Shale	230.7	336.5	1382.6	1383	0	0	760	96.6
588.69	1.00			Shale	230.7	336.5	1613.4	1613	0	0	887	97.6
587.69	1.00			Shale	230.7	336.5	1844.1	1844	0	0	1014	98.6
586.69	1.00			Shale	230.7	336.5	2074.8	2075	0	0	1141	99.6
585.69	1.00			Shale	230.7	336.5	2305.5	2306	0	0	1268	100.6
584.69	1.00			Shale	230.7	336.5	2536.3	2536	0	0	1395	101.6
583.69	1.00			Shale	230.7	336.5	2767.0	2767	0	0	1522	102.6
582.69	1.00			Shale	230.7	336.5	2997.7	2998	0	0	1649	103.6
581.69	1.00			Shale	230.7	336.5	3228.4	3228	0	0	1776	104.6
580.69	1.00			Shale	230.7	336.5	3459.2	3459	0	0	1903	105.6
579.69	1.00			Shale	230.7	336.5	3689.9	3690	0	0	2029	106.6
578.69	1.00			Shale	230.7	336.5	3920.6	3921	0	0	2156	107.6
577.69	1.00			Shale	230.7	336.5	4151.3	4151	0	0	2283	108.6
576.69	1.00			Shale		336.5						