

**CROSS FRAME DIMENSIONS (a)**

BAY	D1	D2	D3	D4	D5	D6	D7	D8	D9	D10	D11	D12	D13	D14	D15	D16	D17	D18	D19	D20	D21
Girder 1-2	6"	6"	6"	6"	6"	6"	6"	6 1/8"	6 1/8"	6"	6"	6 1/8"	6 1/8"	6"	6"	6 1/8"	6 1/8"	6 1/8"	6 1/8"		
Girder 2-3	6 3/16"	6 3/16"	6 3/16"	6 3/8"	6 3/16"	6 3/16"	6 3/16"	6 1/4"	6 1/4"	6 3/16"	6 3/16"	6 1/4"	6 1/4"	6 3/16"	6 3/16"	6 3/16"	6 1/4"	6 1/4"	6 1/4"		
Girder 3-4																				6"	
Girder 4-5																				6"	
Girder 5-6																					6"
Girder 6-7																					6"
Girder 7-8																					6"
Girder 8-9																					6"

BAY	D22	D23	D24	D25	D26	D27	D28	D29	D30	D31	D32	D33	D34	D35	D36	D37	D38	D39	D40	D41	D42
Girder 10-11	6"																				
Girder 11-12	6"																				
Girder 12-13	6"																				
Girder 13-14	6"																				
Girder 14-15		6"																			
Girder 15-16			6"	6"	6"	6"	6"	6"	6"	6 1/8"	6 1/8"	6"	6"	6 1/8"	6 1/8"	6"	6"	6 1/8"	6"	6"	6 1/8"
Girder 16-17			6 1/4"	6 1/4"	6 1/4"	6 1/4"	6 1/4"	6 1/4"	6 1/4"	6 5/16"	6 5/16"	6 3/8"	6 1/4"	6 5/16"	6 5/16"	6 3/8"	6 1/4"	6 5/16"	6 1/4"	6 3/8"	6 1/8"
Girder 17-18			6 7/16"	6 7/16"	6 7/16"	6 7/16"	6 7/16"	6 7/16"	6 7/16"	6 9/16"	6 9/16"	6 7/8"	6 1/2"	6 9/16"	6 9/16"	6 7/8"	6 1/2"	6 9/16"	6 1/2"	6 7/8"	6 3/4"
Girder 18-19			6 5/8"	6 5/8"	6 5/8"	6 5/8"	6 5/8"	6 5/8"	6 5/8"	6 13/16"	6 13/16"	6 7/8"	6 1/2"	6 13/16"	6 13/16"	6 7/8"	6 1/2"	6 13/16"	6 7/8"	6 13/16"	7 1/16"

**CROSS FRAME DIMENSIONS (b)**

D1	D2	D3	D4	D5	D6	D7	D8	D9	D10	D11	D12	D13	D14	D15	D16	D17	D18	D19	D20	D21
6'-6"	6'-7 1/2"	6'-9"	6'-10 5/8"	7'-0 3/8"	7'-1 1/4"	7'-2 1/2"	7'-3"	7'-4 1/4"	7'-5 1/2"	7'-6 3/4"	7'-7 3/4"	7'-9"	7'-10 3/4"	8'-0"	8'-1 1/2"	8'-3"	8'-4 1/2"	8'-6"	8'-2"	8'-0"
D22	D23	D24	D25	D26	D27	D28	D29	D30	D31	D32	D33	D34	D35	D36	D37	D38	D39	D40	D41	D42
8'-0"	8'-3"	5'-1 1/2"	5'-4 3/8"	5'-6 3/4"	5'-9 3/8"	6'-0"	6'-2"	6'-4"	6'-5"	6'-7"	6'-9 1/4"	6'-11 1/4"	7'-1 1/4"	7'-3 1/4"	7'-6"	7'-8 1/4"	7'-10 3/4"	8'-1 1/2"	8'-4"	8'-6 1/2"

**INTERIOR GIRDER MOMENT TABLE (For Girder Line 4 WB)**

	0.4 Sp. 1	Pier	0.6 Sp. 2
$I_s$	(in <sup>4</sup> ) 80956	150013	99291
$I_c(n)$	(in <sup>4</sup> ) 177266	-	224293
$I_c(3n)$	(in <sup>4</sup> ) 129197	-	159632
$I_c(cr)$	(in <sup>4</sup> ) -	168588	-
$S_s$	(in <sup>3</sup> ) 2284	4017	3133
$S_c(n)$	(in <sup>3</sup> ) 3065	-	4122
$S_c(3n)$	(in <sup>3</sup> ) 2768	-	3740
$S_c(cr)$	(in <sup>3</sup> ) -	4191	-
DC1	(k/ft) 1.32	1.45	1.34
MDC1	(k) 2506	6766	3672
DC2	(k/ft) 0.17	0.17	0.17
MDC2	(k) 342	824	471
DW	(k/ft) 0.45	0.45	0.45
M <sub>DW</sub>	(k) 891	2143	1224
$M_k \cdot I_M$	(k) 3175	3714	3595
$M_u$ (Strength I)	(k) 10453	19202	13306
$\phi_r M_n$	(k) 14966	-	19220
$f_s$ DC1	(ksi) 13.17	20.21	14.06
$f_s$ DC2	(ksi) 1.48	2.37	1.51
$f_s$ DW	(ksi) 3.86	6.14	3.93
$f_s$ ( $\phi \cdot I_M$ )	(ksi) 12.43	10.63	10.47
$f_s$ (Service II)	(ksi) 34.67	42.54	33.11
$0.95R_n F_y$	(ksi) 47.50	65.84	47.50
$f_s$ (Total Strength I)	(ksi) -	56.04	-
$\phi_r F_n$	(ksi) -	62.39	-
$V_r$	(k) 81.6	70.4	81.4

**INTERIOR GIRDER REACTION TABLE (For Girder Line 4 WB)**

	W. Abut.	Pier	E. Abut.
RDC1	(k) 78.71	339.63	101.81
RDC2	(k) 11.12	41.07	12.93
R <sub>DW</sub>	(k) 28.91	106.83	35.18
$R_k \cdot I_M$	(k) 138.83	292.93	143.66
R <sub>Total</sub>	(k) 257.57	780.46	293.58

$I_s, S_s$ : Non-composite moment of inertia and section modulus of the steel section used for computing  $f_s$  (Total-Strength I, and Service II) due to non-composite dead loads (in<sup>4</sup> and in<sup>3</sup>).

$I_c(n), S_c(n)$ : Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing  $f_s$  (Total-Strength I, and Service II) in uncracked sections due to short-term composite live loads (in<sup>4</sup> and in<sup>3</sup>).

$I_c(3n), S_c(3n)$ : Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing  $f_s$  (Total-Strength I, and Service II) in uncracked sections, due to long-term composite (superimposed) dead loads (in<sup>4</sup> and in<sup>3</sup>).

$I_c(cr), S_c(cr)$ : Composite moment of inertia and section modulus of the steel and longitudinal deck reinforcement, used for computing  $f_s$  (Total-Strength I and Service II) in cracked sections, due to both short-term composite live loads and long-term composite (superimposed) dead loads (in<sup>4</sup> and in<sup>3</sup>).

DC1: Un-factored non-composite dead load (kips/ft.).

MDC1: Un-factored moment due to non-composite dead load (kip-ft.).

DC2: Un-factored long-term composite (superimposed excluding future wearing surface) dead load (kips/ft.).

MDC2: Un-factored moment due to long-term composite (superimposed excluding future wearing surface) dead load (kip-ft.).

DW: Un-factored long-term composite (superimposed future wearing surface only) dead load (kips/ft.).

M<sub>DW</sub>: Un-factored moment due to long-term composite (superimposed future wearing surface only) dead load (kip-ft.).

$M_k \cdot I_M$ : Un-factored live load moment plus dynamic load allowance (impact) (kip-ft.).

$M_u$  (Strength I): Factored design moment (kip-ft.).

$1.25 (M_{DC1} + M_{DC2}) + 1.5 M_{DW} + 1.75 M_k \cdot I_M$

$\phi_r M_n$ : Compact composite positive moment capacity computed according to Article 6.10.7.1 or non-slender negative moment capacity according to Article A6.1.1 or A6.1.2 (kip-ft.).

$f_s$  DC1: Un-factored stress at edge of flange for controlling steel flange due to vertical non-composite dead loads as calculated below (ksi).

$M_{DC1} / S_c$

$f_s$  DC2: Un-factored stress at edge of flange for controlling steel flange due to vertical composite dead loads as calculated below (ksi).

$M_{DC2} / S_c(3n)$  or  $M_{DC2} / S_c(cr)$  as applicable.

$f_s$  DW: Un-factored stress at edge of flange for controlling steel flange due to vertical composite future wearing surface loads as calculated below (ksi).

$M_{DW} / S_c(3n)$  or  $M_{DW} / S_c(cr)$  as applicable.

$f_s$  ( $\phi \cdot I_M$ ): Un-factored stress at edge of flange for controlling steel flange due to vertical composite live load plus impact loads as calculated below (ksi).

$M_k \cdot I_M / S_c(n)$  or  $M_k \cdot I_M / S_c(cr)$  as applicable.

$f_s$  (Service II): Sum of stresses as computed below (ksi).

$f_{SDC1} + f_{SDC2} + f_{SDW} + 1.3 f_s (\phi \cdot I_M)$

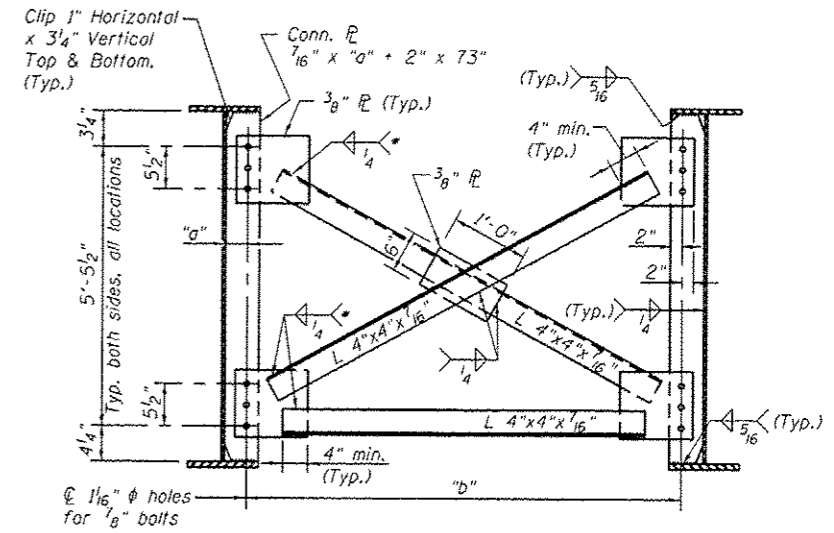
$0.95R_n F_y$ : Composite stress capacity for Service II loading according to Article 6.10.4.2 (ksi).

$f_s$  (Total Strength I): Sum of stresses as computed below on non-compact section (ksi).

$1.25 (f_{SDC1} + f_{SDC2}) + 1.5 f_{SDW} + 1.75 f_s (\phi \cdot I_M)$

$\phi_r F_n$ : Non-compact composite positive or negative stress capacity for Strength I loading according to Article 6.10.7 or 6.10.8 (ksi).

$V_r$ : Maximum factored shear range in span computed according to Article 6.10.10.

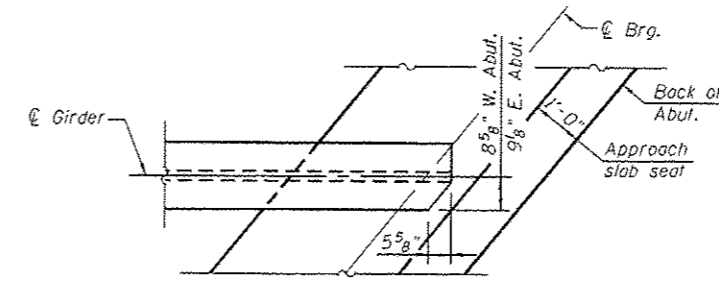


**TYPICAL INTERIOR CROSS FRAME**

(2 ea. D1-D19, 38-D20, 76-D21 for SN 025-0111 (WB))  
(76-D22, 19-D23, 4 ea. D24-D42 for SN 025-0112 (EB))

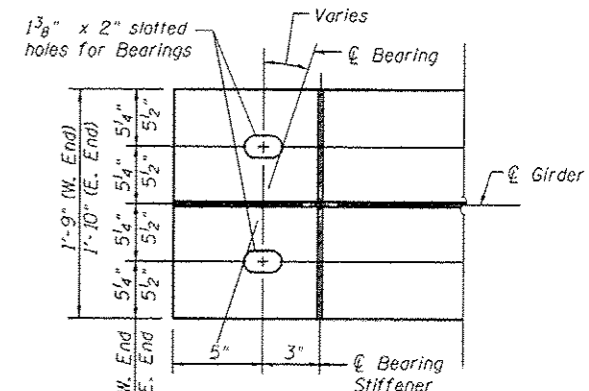
\* Fillet weld angles along 3 sides of one face of gusset plate

Notes:  
Two hardened washers required for each set of oversized holes.  
All cross frames between girders shall be installed with erection pins and bolts according to the erection plan approved by the Engineer. Individual cross frames of supports may be temporarily disconnected to install bearing anchor rods.  
All cross frames shall be Grade 50!



**END GIRDER TOP FLANGE CLIP DETAIL**

(Showing top flange of steel beam at integral abutment)



**END GIRDER DETAIL**