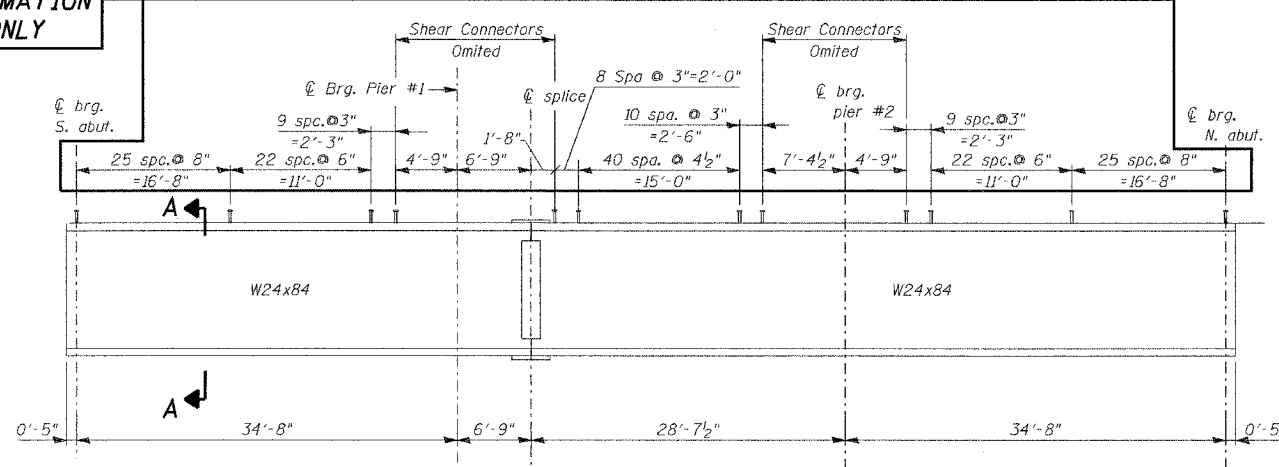


STATE OF ILLINOIS
DEPARTMENT OF TRANSPORTATION

ROUTE NO.	SECTION	COUNTY	SHEETS	POST	SHEET NO. 58
F. A. P. 846	4B-1-R	WILL	39	30	5 SHEETS 517
FED. ROAD DIST. NO. 7	ILL. PROJ. NO.	FED. AID PROJECT-			

CONTRACT NO. 60D26

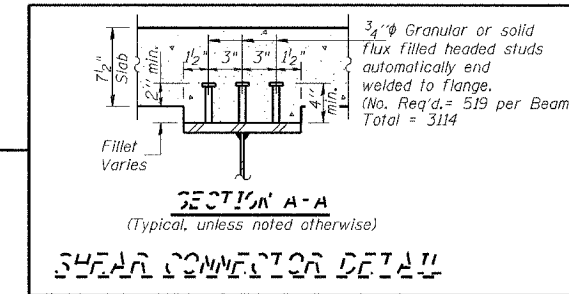
FOR
INFORMATION
ONLY



BEAM ELEVATION

NOTE:
All wide flange beams and splice plate material shall be AASHTO M270 Grade 50 and shall meet notch toughness requirements.

FOR
INFORMATION
ONLY



	INTERIOR BEAM MOMENT TABLE		
	0.4 Sp. 1 0.6 Sp. 3	Pier #1 Pier #2	0.5 Sp. 2
I_s	(in ⁴) 2370	2370	2370
$I_c (n)$	(in ⁴) 8522	-	8522
$I_c (3n)$	(in ⁴) 6354	-	6354
S_s	(in ³) 196	196	196
$S_c (n)$	(in ³) 335	-	335
$S_c (3n)$	(in ³) 302	-	302
Z	(in ³) 224	224	224
DC1	(K/')	0.92	0.92
MDC1	(K)	88	32
DC2	(K/')	0.15	0.15
MDC2	(K)	14	5
DW	(K/')	0.33	0.33
MDW	(K)	31	11
MLL+I	(K)	353	293
M_u (Strength I)	(K)	794.0	578.0
ϕM_n , ϕM_{nc}	(K)	1712.0	1712.0
f_s DC1	(ksi)	5.4	2.0
f_s DC2	(ksi)	0.5	0.2
f_s DW	(ksi)	1.1	0.4
f_s 1.3(LL+I)	(ksi)	16.4	13.6
f_s (Service II)	(ksi)	23.7	16.3
f_s (Total) (Strength I)	(ksi)	48.6	35.4
Vf	(k)	12	9.9

I_s and S_s are the moment of inertia and section modulus of the steel section used in computing f_s due to non-composite loads.

$I_c(n)$ and $S_c(n)$ are the moment of inertia and section modulus of the composite section based on modular ratio, n , used in computing f_s due to short-term composite live loads.

$I_c(3n)$ and $S_c(3n)$ are the moment of inertia and section modulus of the composite section based upon 3 times modular ratio, $3n$, used in computing f_s due to long-term composite (superimposed) dead loads.

Z is the plastic section modulus used to determine the fully plastic moments in the non-composite areas.

DC1 is the unfactored non-composite dead load acting on the non-composite section.

DC2 is the unfactored long term composite (superimposed excluding future wearing surface) dead load.

DW is the unfactored long term composite (superimposed future wearing surface only) dead load.

M_u (Strength I) Factored design moment
 $1.25(MDC1+MDC2)+1.5 M DW +1.75 MLL+Imp$

ϕM_n is the Compact composite positive moment capacity computed according to Article 6.10.7.1

ϕM_{nc} is the Compact non-composite negative moment capacity computed according to Article A6.1.1

f_s (Service II) is the sum of the stresses from the moments below:
 $MDC1+MDC2+MDW+1.3MLL+Imp$

f_s (Total) (Strength I) (Non-Compact Section) is the sum of the stresses due to $1.25MDC1+DC2+1.5MDW+1.75MLL+Imp$

Vf is the factored maximum shear range computed according to Article 6.10.10

TOP OF BEAM ELEVATIONS **					
Beam	¢ Brg. S Abut.	¢ Brg. Pier #1	¢ Splice	¢ Brg. Pier #2	¢ Brg. N Abut.
1	571.586	571.734	571.763	571.796	571.837
2	571.741	571.888	571.917	571.951	571.992
3	571.862	572.010	572.039	572.073	572.114
4	571.925	572.073	572.102	572.135	572.176
5	571.809	571.957	571.986	572.019	572.060
6	571.669	571.817	571.846	571.880	571.921

** For Fabrication Only.

INTERIOR GIRDER REACTION TABLE HS20 LOADING				
	S. Abut.	Pier #1	Pier #2	N. Abut.
R (DL) (K)	19.8	53.6	53.6	19.8
R (LL) (K)	36.0	44.2	44.0	36.0
R (Imp) (K)	11.2	13.8	13.7	11.2
R (Total) (K)	67.2	111.7	111.4	67.2

INTERIOR GIRDER REACTION TABLE HL93 Loading				
	S. Abut.	Pier #1	Pier #2	N. Abut.
R (DC1) (K)	12.7	35.5	35.5	12.7
R (DC2+DW) (K)	6.6	18.6	18.6	6.6
R (LL) (K)	42.2	83.7	83.7	42.2
R (Imp) (K)	13.9	27.6	27.6	13.9
R (Total) (K)	75.6	165.5	165.5	75.6

DESIGNED	NDS/GMK
CHECKED	MTP/SMK/GBC
DRAWN	NDS/GMK
CHECKED	SMK/GBC

ILLINOIS DEPARTMENT OF TRANSPORTATION

STRUCTURAL STEEL DETAILS

FAP 846
SB IL. ROUTE 53 OVER PRAIRIE CREEK
STATION 1305+00 SECTION 4B-1-R
WILL COUNTY

STRUCTURE NO. 099-0242

SCALE: NONE
DATE: JUNE 2007

DEI DELTA ENGINEERING INC.
CONSULTING ENGINEERS, CHICAGO, ILLINOIS