INTERIOR GIRDER MOMENT TARIE								
In English	01/12		THEE					
		0.4 Sp. 1	Pier	0.6 Sp. 2				
Is	(in 4)	19,731	37,959	19,731				
Ic(n)	(in4)	42,549	69,544	42,549				
Ic(3n)	(in4)	32,059	53,077	32,059				
Ic(cr)	(in4)		43,130					
Ss	(in <sup>3</sup> )	897	1650	897				
Sc(n)	(in <sup>3</sup> )	1147	1964	1147				
Sc(3n)	(in <sup>3</sup> )	1061	1833	1061				
Sc(cr)	(in <sup>3</sup> )		1721					
DC1	(k/′)	0.993	1.127	0.993				
M DC1	(′k)	966	1831	679				
DC2	(k/′)	0.220	0.220	0.220				
M DC2	(′k)	217	397	152				
DW	(k/′)	0,310	0.310	0.310				
Mow	(′k)	306	560	214				
M4 + IM	(′k)	1602	1782	1482				
Mu (Strength I)	(′k)	4741	6,744	3953				
$\phi_f M_n$	(′k)	5,688	7,688	5,688				
fs DC1	(ksi)	12.9	13.3	9.1				
fs DC2	(ksi)	2.5	2.8	1.7				
fs DW	(ksi)	3.5	3.9	2,4				
fs (4+IM)	(ksi)	16.8	12.4	15.5				
fs (Service II)	(ksi)	40.6	36.1	33.4				
$0.95R_hF_yf$	(ksi)	47.5	47.5	47.5				
fs (Total)(Strength I)	(ksi)							
$\phi_f F_n$	(ksi)							
Vf	(k)	60.9	60.9	65.1				

INTERIOR GIRDER REACTION TABLE							
		N. Abut.	Pier	S. Abut.			
RDCI	(k)	60.1	148.5	53.3			
R <sub>DC2</sub>	(k)	9.8	32.1	8.3			
Row	(k)	13.8	45.2	11.7			
R4 + IM	(k)	99.9	178.1	97.6			
RTotal	(k)	18.3.6	403.8	170.8			

All reactions are unfactored. Reactions at abutments include weight of diaphragm

- Is, Ss: Non-composite moment of inertia and section modulus of the steel section used for computing fs (Total-Strength I, and Service II) due to non-composite dead loads (in.<sup>4</sup> and in.<sup>3</sup>).  $I_c(n)$ ,  $S_c(n)$ : Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing
- $f_s$  (Total-Strength I, and Service II) in uncracked sections, due to short-term composite live loads (in.4 and in.3).  $I_c(3n)$ ,  $S_c(3n)$ : Composite moment of inertia and section modulus of the steel and
- deck based upon 3 times the modular ratio, "3n", used for computing fs(Total-Strength I, and Service II) in uncracked sections, due to long-term composite (superimposed) dead loads (in.<sup>4</sup> and in.<sup>3</sup>).
- Ic(cr), Sc(cr): Composite moment of inertia and section modulus of the steel and longitudinal deck reinforcement, used for computing  $f_s$  (Total-Strength I and Service II) in cracked sections, due to both short-term composite live loads and long-term composite dead loads (in.4 and in.3).
  - DC1: Un-factored non-composite dead load (kips/ft.).
  - M<sub>DCI</sub>: Un-factored moment due to non-composite dead load (kip-ft.). DC2: Un-factored long-term composite (superimposed excluding future wearing surface) dead load (kips/ft.).
  - MDC2: Un-factored moment due to long-term composite (superimposed excluding future wearing surface) dead load (kip-ft.).
  - DW: Un-factored long-term composite (superimposed future wearing surface only) dead load (kips/ft.).
  - M<sub>Dw</sub>: Un-factored moment due to long-term composite (superimposed future wearing surface only) dead load (kip-ft.).
  - M4 + IM: Un-factored live load moment plus dynamic load allowance (impact) ((kip-ft.).
- M<sub>u</sub> (Strength I): Factored design moment (kip-ft.).
  - 1.25 (MDC1 + MDC2) + 1.5 MDW + 1.75 M4 + IM  $\phi_f M_n$ : Compact composite positive moment capacity computed according to Article 6.10.7.1 or non-slender negative moment capacity according to Article A6.1.1 or A6.1.2 (kip-ft.).
  - fs DC1: Un-factored stress at edge of flange for controlling steel flange due to vertical non-composite dead loads as calculated below (ksi). MDCL / Snc
  - fs DC2: Un-factored stress at edge of flange for controlling steel flange due to vertical composite dead loads as calculated below (ksi).
  - MDc2 / Sc(3n) or MDc2 / Sc(cr) as applicable. fs DW: Un-factored stress at edge of flange for controlling steel
  - flange due to vertical composite future wearing surface loads as calculated below (ksi). Mow / Sc(3n) or Mow / Sc(cr) as applicable.
  - fs (4+IM): Un-factored stress at edge of flange for controlling steel flange due to vertical composite live plus impact loads as calculated below (ksi).
- M4+ IM / Sc(n) or M4+ IM / Sc(cr) as applicable. fs (Service II): Sum of stresses as computed below (ksi). fsDC1 + fsDC2 + fsDW + 1.3 fs(4 + IM)
- 0.95RhFyf: Composite stress capacity for Service II loading according to Article 6.10.4.2 (ksi).
- fs (Total)(Strength I): Sum of stresses as computed below on non-compact section (ksi). 1.25 (fsdc1 + fsdc2) + 1.5 fsdw + 1.75 fs & + IM
  - $\phi_f F_n$ : Non-Compact composite positive or negative stress capacity for Strength I loading according to Article 6.10.7.2 (ksi). Vf: Maximum factored shear range in composite portion of span
  - computed according to Article 6.10.10.



### ELEVATION AT PIER







### FILLER PLATE SCHEDULE

(In addition to adjustment shims, see General Notes) Cost Included with Structural Steel

Location	Girder	Plate Thickness t		
NB North Abut.	3	3_" 4		
SB North Abut.	7	4"		

Fill plates to be the same horizontal dimensions as the bottom bearing plates.



5. Steel members required for bearing assembly shall be included in the cost of structural steel.

1. Anchor bolts shall be ASTM F1554 all-thread (or an Engineer-approved alternate material) of the grade(s) and diameter(s) specified. The corresponding specified grade of AASHTO M314 Gr. 36

2. Anchor bolts at fixed bearings may be either cast in place or installed in holes drilled after the

anchor bolts may be used in lieu of ASTM F1554 Grade 36 (Fy = 36ksi) at the pier.

3. Drilled and set anchor bolts shall be installed according to Article 521.06 of the Standard



supported member is in place.

NOTES:

Specifications,

Job No. 10056

FILE NAME =	USER NAME = mbecker	DESIGNED -	MFB/DTS	REVISED -		GIRDER DETAILS 2 OF 3	F.A.I. BIF	SECTION	COUNTY	TOTAL SHEET
		CHECKED -	MRB/AAY	REVISED -	STATE OF ILLINOIS		74 90-[14	R:(14HB-4,14,14HVB)BR]	TAZEWELL	2433 1886
0900165_68620_22_stdt2.dgn PLOT SCAL PLOT DATE	PLOT SCALE =	DRAWN -	PRT	REVISED -	DEPARTMENT OF TRANSPORTATION	STRUCTURE NU. 090-0105 / 0100			CONTRACT NO. 68620	
	PLOT DATE = 7/16/2012	= 7/16/2012 CHECKED - MRB/AAY REVISED -	SHEET NO. SA22 OF SA47 SHEETS	ILLINOIS FED. AID PROJECT		ID PROJECT	,т			



# FIXED BEARING AT PIER

# FIXED BEARING AT ABUTMENT



## BILL OF MATERIAL

ITEM	UNIT	TOTAL
Anchor Bolts, 1"	Each	40
Anchor Bolts, 14"	Each	20

0:53:21