

All splices are symmetrical about ∉ splice. H.S. bolts shall be 7_8 " ϕ AASHTO M164/ASTM A325 Type 3. Load carrying components designated "NTR" shall conform to the Impact Testing Requirement, Zone 2.



	NTER	OR GIRDER MOMENT TA	BI F	
		0.4 Sp. 1 or 0.6 Sp. 3	Pier 1 & 2	0.5 Sp. 2
Is	(in ⁴)	6710	6710	6710
I _c (n)	(in4)	18650		18650
Ic(3n)	(in4)	13636		13636
Ic(cr)	(in4)		9404	
Ss	(in ³)	406	406	406
Sc(n)	(in ³)	610.3		610.3
Sc(3n)	(in ³)	550.1		550.1
Sc(cr)	(in ³)		474.7	
DC1	(k/′)	0.835	0.835	0.835
M DC1	(′k)	139	332	209
DC2	(k/′)	0.150	0.150	0.150
M DC2	(′k)	25	60	37
DW	(k/′)	0.300	0.300	0.300
Mow	(′k)	49	121	74
M4 + IM	(′k)	560	566	6 <i>1</i> 6
Mu (Strength I)	(′k)	1259	<i>1662</i>	1497
Øf Mn	(′k)	3176		3111
fs DC1	(ksi)	4.1	9.8	6.2
fs DC2	(ksi)	0.5	1.5	0.8
fs DW	(ksi)	1.1	3.1	1.6
fs (4+IM)	(ksi)	11.0	14.3	12.1
fs (Service II)	(ksi)	20.0	33.0	24.3
0.95RhFyf	(ksi)	47.5	47.5	47.5
fs (Total)(Strength I)	(ksi)		43.8	
Ø _f F _n	(ksi)		50.0	
Vf	(k)	24.9	24.9	24.9

INTERIOR DIAPHRAGM

Notes:

Α

L 6" x 4" x 1/2"

δoT

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Spa.

Two hardened washers required for each set of oversized or

* @ C 12 x 25

-∕4 sides

* @ Beam and

€ C 12 x 25 at end of channel

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Δ

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SECTION A-A

4''

To C

- * Alternate C 12 x 30 channels are permitted to facilitate material acquisition. Calculated weight of structural steel is based on the
- The alternate, if utilized, shall be provided at no additional cost
- ${}^3_{4''} \phi$ H.S. bolts, ${}^{l5}_{6} = \phi$ holes typ., except ${}^3_{4''} \phi$ H.S. bolts ${}^{l3}_{6} = x$ ${}^{l7}_{8} =$ slots provided on south side of Beam 3 to accommodate
- differential displacement between Beams 3 and 4 for Stage Construction. Bolts in slots shall be finger tight until Stage II Construction is complete. Position slots so bolts start at one end with no concrete load and finish near the opposite end under deck load, allowing maximum

INTERIOR GIRDER REACTION TABLE							
		W. Abut. & E. Abut.	Pier 1 & 2				
RDCI	(k)	16.2	58.2				
R DC2	(k)	2.8	10.5				
Row	(k)	5.5	21.0				
R4 + IN	1 (k)	72.6	100.1				
R Total	(k)	97.1	189.8				



FIXED BEARING AT PIER (12 Required)

des no.	engineers + planners + land surveyors	USER NAME = \$0PERATOR\$ FILE NAME = 0110514-72A61.dgn PLOT SCALE = 0:2.0000 ':' / 10.	DESIGNED - TJZ CHECKED - CWC DRAWN - DLH	REVISED REVISED REVISED	STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION	STRUCTURAL STEE STRUCTURE NO. (
	/	PLUI DATE = 972672013	CHECKED - IJZ	REVISED		SHEET NU. 15 UF 31

SHEETS		• 75	(IL 27)	& 714 (IL 48)		NO.	72A61
		RTE.		SECTION (4)I; 136B-1	COUNTY	SHEETS 97	NO. 55
		F.A.P.		SECTION	COLINEY	TOTAL	SHEET
© Beam 3 (W. A © Beam 4 (E. A	(but.) and () (but.)						
Provide ^I 4" x 9" x	11'2" Shim P						
AASHTO M270 Gro	ide 50W.	20					
orner plates or sh All plates, shape	ims and placed o es and pintles st	is sho nall co	wn on nform	bearing Defail to the requirer	s. ments of		
Two ^I 8" adjusting	g shims shall be imp and placed	provi	ded fo	r each bearing	in addition	to all	
of the Standard S,	pecifications.	ושעי	ាចាប់រាម	s accoranty 10	ALLIGE JZI		
he supported mem Drilled and set	nber is in place. anchor bolts sha	ll he i	Installa	t according to	Article 501	06	
Anchor bolts ma	y be either cast	in pl	ace or	installed in ho	les drilled a	fter	
corresponding spec of ASTM F1554.	ciried grade of i	a a SHi	'U M31	4 anchor bolts	may be use	ea in l	ieu
alternate material)	of the Grade(s)	and	Diamet	er(s) specified.	The	· .	1
Anchor bolts sh	all be ASTM F15.	54 AI	I-Three	nd (or an Engin	neer approve	ed	
atac							
v † :	to Article 6.10.1	0.	ar ruh	yə m əpun cu		, uny	
Vf:	Strength I loadi Maximum factore	ng ac ed she	cording ear ran	to Article 6.1 ge in span cou	U.7 or 6.10. mputed acco	8 (ksi, rdina	/.
$\phi_f F_n$:	Non-Compact co	mposi	te posi	tive or negativ	e stress cap	oacity	for
	section (Ksi). 1.25 (fspci + fsni	c2) +	1.5 fsi	ow + 1.75 fs (4	+ IM)		
Total)(Strength I):	Sum of stresses	s as c	compute	ed below on no	n-compact		
U.95R _h Fyf:	to Article 6.10.4	s cap 1.2 (k.	acity f si) .	or Service II I	vaaing accoi	raing	
	f _{sDC1} + f _s DC2 +	f _{s DW} +	1.3 fs	(4 + IM)			
fs (Service II):	M L + IM / S _c (n) Sum of stresses	or Mi s as c	ow / S. compute	c(cr) as applica d below (ksi).	ıble.		
	calculated below	(ksi).		(or)	ab/a		
is (4+1M):	flange due to ve	ess a ertical	eage compo	or riange for site live load p	controlling s vlus impact	loads	as
f (L±TIA)	MDW / Sc(3n) or	MDW	/ Sc	(cr) as application	ble.	staal	
	loads as calcula	ted be	elow (k	si).	unny sun uc		
fs DW:	Un-factored str	ess a	t edge	of flange for	controlling surface	steel	
	MDC2 / Sc(3n) or	- M DC2	2 / Sc	(cr) as applica	ble.		
	flange due to ve below (ksi)	ertical	compo	site dead load	s as calcula	ted	
fs DC2:	Un-factored str	ess a	t edge	of flange for	controlling s	steel	
	below (ksi). Moci / Sec						
,3 201.	flange due to ve	ertical	non-c	omposite dead	loads as ca	lculate	∂d
fs DC1:	according to Ar Un-factored str	ticle i ess a	46.1.1 (t edae	of flange for	rr). controllina s	steel	
	to Article 6.10.7	1 or	non-si	ender negative	moment cap	pacity	2
Øf Mn:	Compact compos	.z) + site po	ns mE sitive	w · 1.15 M Ł + moment capacii	'y computed	accor	ding
Mu (Strength I):	Factored design	mome	ent (kip	-ft.). w + 175 Ml	TM		
₩¥ + 1M:	(kip-ft.).	,000			.000 010000	.00 (//	
Mh . 11.	future wearing .	surfac Iond	ce only. momen) dead load (kij t plus dvoamie	o-ft.). load allowa	nce (ir	mpart)
M _{DW} :	Un-factored mol	ment a	due to	long-term com	posite (supe	rimpos	sed
DW:	Un-factored long	g-terr ad Ini	n comp 1d (kin	osite (superimp s/ft.).	osed future	wear	ing
WDC2:	excluding future	wear	ing su	face) dead loc	d (kip-ft.).		
Mores	wearing surface Un-factored mod) dea ment i	d load due to	(kips/ft.). Iona-term com	posite (sune	rimno«	sed
DC2:	Un-factored lon	g-terr	n comp	osite (superimp	osed exclud	ling fu	iture
DCI: MDCI:	Un-factored mon	n-com, ment a	due to	aeaa ioaa (kips non-composite	dead load (kip-ft	.).
	(superimposed) (dead l	oads (i posito	$n.^4$ and $in.^3$).	/ft)		
	both short-term	comp	osite l	ive loads and l	ong-term co	mposi	te
	and longitudinal (Total-Strength	deck I and	reinfor Servir	cement, used i e II) in crack	or computin ed sections	ng f _s due t	'n
Ic(cr), Sc(cr):	Composite mome	nt of	inertia	and section m	nodulus of ti	he ste	e/
	sections, due to (in.4 and in.3).	long	term d	composite (supe	erimposed) a	lead lo	iads
	computing f_s (To	tal-St	rength	I, and Service	II) in uncr	acked	
$I_{c}(3n), S_{c}(3n);$	composite mome and deck based	nt ot upon	3 time	and section m is the modular	nodulus of ti ratio, ".3n",	he ste used	el for
	to short-term c	ompos	ite live	loads (in.4 an	d in. ³).		
	ana deck based fs(Total-Strenat	upon h I. c	the mi Ind Sei	oaular ratio, "n vice II) in und	", used for cracked sect	compu ions c	uting Jue
Ic(n), Sc(n);	Composite mome	nt of	inertia	and section	modulus of	the st	eel utioc
	Service II) due	to no	n-com	osite dead loa	ds (in.4 and	in. ³).	
Is, Ss:	Non-composite r	nomen ed fo	t of in r comp	ertia and secti utina fa(Total-	on modulus Strepath I	of the	;
	N		1 C .	a sadd a sin a		. £ · ·	