

INTERIOR BEAM MOMENT TABLE				
		0.4 Sp. 1 or 0.6 Sp. 3	Pier 1 or 2	0.5 Sp. 2
$I_s$	(in <sup>4</sup> )	2,850	2,850	2,850
$I_c(n)$	(in <sup>4</sup> )	9,235	---	9,235
$I_c(3n)$	(in <sup>4</sup> )	7,054	---	7,054
$S_s$	(in <sup>3</sup> )	213	213	213
$S_c(n)$	(in <sup>3</sup> )	340	---	340
$S_c(3n)$	(in <sup>3</sup> )	309	---	309
$Z$	(in <sup>3</sup> )	---	244	---
DC1	(k/ft)	0.836	0.836	0.836
MDC1	(k)	38	123	83
DC2	(k/ft)	0.155	0.155	0.155
MDC2	(k)	9	19	21
DW	(k/ft)	0.333	0.333	0.333
MDW	(k)	20	39	44
$M_L + IM$	(k)	312	217	453
$M_u$ (Strength I)	(k)	635	616	989
$\phi_r M_n, \phi_r M_{nc}$	(k)	1,749	---	1,749
$f_s$ DC1	(ksi)	2.2	7.0	4.7
$f_s$ DC2	(ksi)	0.4	1.1	0.9
$f_s$ DW	(ksi)	0.8	2.2	1.8
$f_s$ 1.3(L+IM)	(ksi)	14.4	15.9	20.8
$f_s$ (Service II)	(ksi)	17.8	26.2	28.2
$f_s$ (Total)(Strength I)	(ksi)	---	34.9	---
$V_f$	(k)	36.2	---	35.4

\* Compact sections  
 \*\* Non-Compact and slender sections

INTERIOR BEAM REACTION TABLE			
	Abuts.	Pier 1 & 2	
R <sub>DC1</sub>	(k)	8.1	34.9
R <sub>DC2</sub>	(k)	1.7	6.4
R <sub>DW</sub>	(k)	3.6	13.7
R <sub>L + IM</sub>	(k)	53.4	84.9
R <sub>Total</sub>	(k)	66.8	139.9

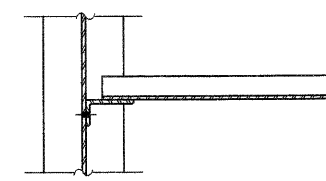
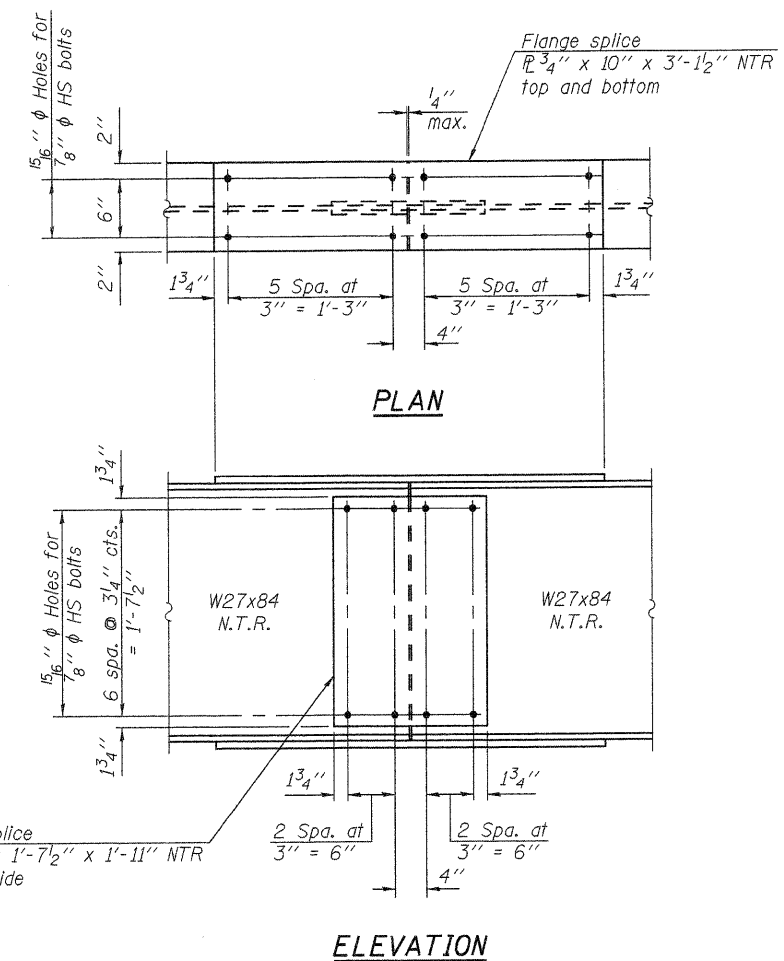
$I_s, S_s$ : Non-composite moment of inertia and section modulus of the steel section used for computing  $f_s$  (Total-Strength I, and Service II) due to non-composite dead loads (in<sup>4</sup> and in<sup>3</sup>).

$I_c(n), S_c(n)$ : Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing  $f_s$  (Total-Strength I, and Service II) due to short-term composite live loads (in<sup>4</sup> and in<sup>3</sup>).

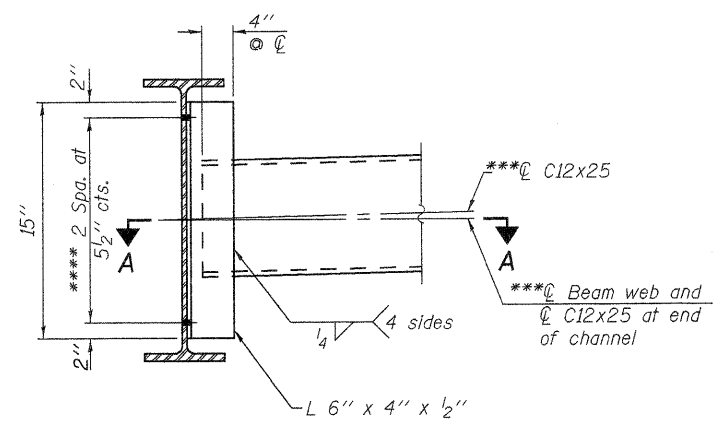
$I_c(3n), S_c(3n)$ : Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing  $f_s$  (Total-Strength I, and Service II) due to long-term composite (superimposed) dead loads (in<sup>4</sup> and in<sup>3</sup>).

Z: Plastic Section Modulus of the steel section in non-composite areas.

DC1: Un-factored non-composite dead load (kips/ft.).  
 MDC1: Un-factored moment due to non-composite dead load (kip-ft.).  
 DC2: Un-factored long-term composite (superimposed excluding future wearing surface) dead load (kips/ft.).  
 MDC2: Un-factored moment due to long-term composite (superimposed excluding future wearing surface) dead load (kip-ft.).  
 DW: Un-factored long-term composite (superimposed future wearing surface only) dead load (kips/ft.).  
 MDW: Un-factored moment due to long-term composite (superimposed future wearing surface only) dead load (kip-ft.).  
 $M_L + IM$ : Un-factored live load moment plus dynamic load allowance (impact) (kip-ft.).  
 $M_u$  (Strength I): Factored design moment (kip-ft.).  
 $1.25 (M_{DC1} + M_{DC2}) + 1.5 M_{DW} + 1.75 M_L + IM$   
 $\phi_r M_n$ : Compact composite positive moment capacity computed according to Article 6.10.7.1 (kip-ft.).  
 $\phi_r M_{nc}$ : Compact non-composite negative moment capacity computed according to Article A6.1.1 (kip-ft.).  
 $f_s$  (Service II): Sum of stresses as computed from the moments below (ksi).  
 $M_{DC1} + M_{DC2} + M_{DW} + 1.3 M_L + IM$   
 $f_s$  (Total)(Strength I): Sum of stresses as computed from the moments below on non-compact section (ksi).  
 $1.25 (M_{DC1} + M_{DC2}) + 1.5 M_{DW} + 1.75 M_L + IM$   
 $V_f$ : Maximum factored shear range in composite portion of span computed according to Article 6.10.10.

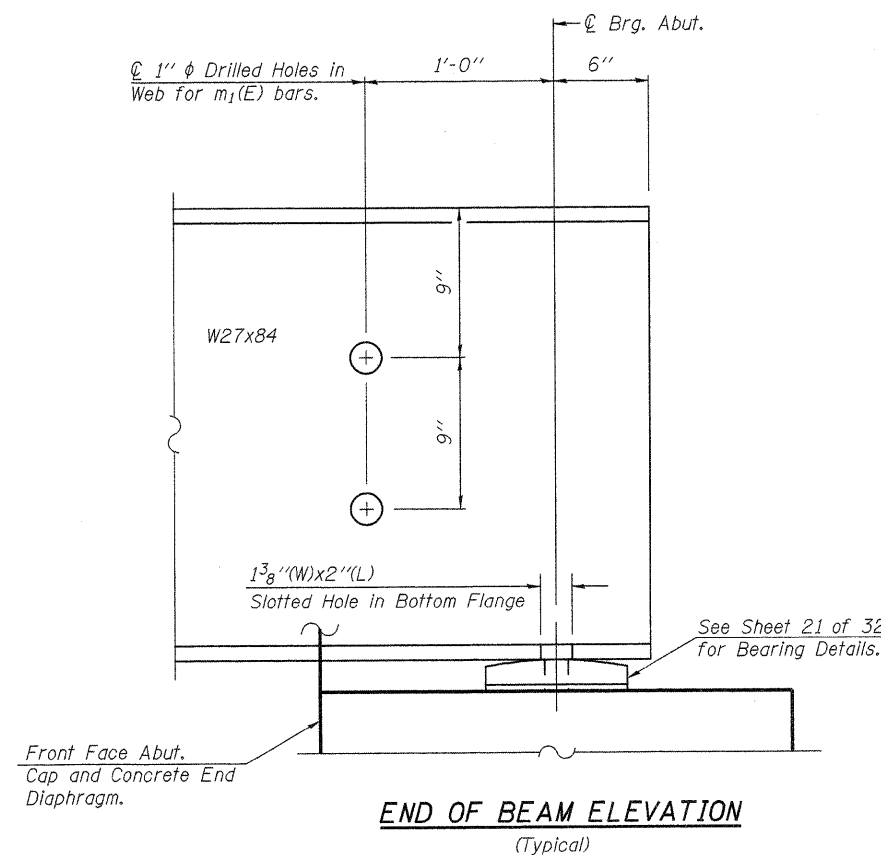


SECTION A-A



INTERIOR DIAPHRAGM - D  
(25 Req'd.)

Note:  
 Two hardened washers required for each set of oversized holes.  
 \*\*\*Alternate channels C12x30 are permitted to facilitate material acquisition. Calculated weight of structural steel is based on the lighter section. The alternate, if utilized, shall be provided at no additional cost to the Department.  
 \*\*\*\*3/4"  $\phi$  HS bolts, 15/16"  $\phi$  holes



END OF BEAM ELEVATION  
(Typical)

Work this Sheet with Sheets 19 & 21 of 32.