

Abbreviated Structure Geotechnical Report

Original Report Date: 3-2-2015	Proposed SN: 027-2020	Route:	FAP 71 (IL 54)
Revised Date: N/A	Existing SN: 027-0021	Section:	(115BR-1)-1
Geotechnical Engineer: Michael S	County:	Ford	
Structural Engineer: Toni McDone	ough, McDonough-Whitlow, P.C.	Contract:	66C94

Indicate the proposed structure type, substructure types, and foundation locations (attach plan and elevation drawing): The proposed structure is a double 9-feet by 6-feet precast box culvert with a 45° right forward skew.

Discuss the existing boring data, existing plans foundation information, new subsurface exploration and need for any additional exploration to be provided with SGR Technical Memo (attach all data and subsurface profile plot): *The existing structure a is a 25 ft single span bridge on a 45° right forward skew supported by untreated timber piles. Two soil borings were performed by IDOT District 3 in 2014. The soil boring logs are attached.*

Provide the location and maximum height of any new soil fill or magnitude of footing bearing pressure. Estimate the amount and time of the expected settlement. Indicate if further testing, analysis, and/or ground improvement/treatment is necessary: The profile of the proposed roadway is not expected to change significantly, therefore there will not be any additional loads applied to the soils. A site visit indicated no signs of settlement problems near the existing structure. No further settlement analysis is required.

Identify any new cuts or fill slope angles and heights. Estimate the factor of safety against slope failure. Indicate if further testing, analysis or ground improvement/treatment is necessary. The proposed side slopes are expected to be flatter than existing. Proposed slopes are 1:3 and a maximum of 9 ft at culvert ends. A site visit indicated no slope stability problems near the existing structure. No further slope stability analysis is warranted.

Indicate at each substructure, the 100-year and 200-year total scour depths in the Hydraulics report, the non-granular scour depth reduction, the proposed ground surface, and the recommended foundation design scour elevations. *The design scour elevation table is not required for closed bottom box culverts per ABD Memo 14.2.*

Determining the seismic soil site class, the seismic performance zone, the 0.2 and 1.0 second design spectral accelerations and indicate if that the soils are liquefiable. *Not applicable to box culverts.*

Confirm feasibility of the proposed foundation or wall type and provide design parameters. Attach a pile design table indicating feasible pile types, various nominal required bearings, factored resistances available and corresponding estimated lengths at locations where piles will be used. Provide factored bearing resistance and unit sliding resistance at various elevations and confirm no ground improvement/treatment is necessary where spread footings are proposed. Estimated top of rock elevations as well as preliminary factored unit side and tip resistance values shall be indicated when drilled shafts are proposed. Since the length of the long wingwalls exceed the maximum allowable length for horizontal cantilever wingwalls, L-type wingwalls or a horizontal cantilever wingwall with gabion extensions are feasible. For L-type and gabion wingwalls, the allowable bearing capacity exceeds 5 ksf. The only aggregate needed under the precast concrete box culvert is the 6 inches required by Article 540.06 of the Standard Specifications.

Calculate the estimated water surface elevation and determine the need for cofferdams (type 1 or 2), and seal coat: The structure can be constructed using conventional methods for water diversion.

Assess the need for sheeting or soil retention or temporary construction slope and provide recommendation for other construction concerns. The new structure will be constructed using a detour. However, if it becomes necessary to use staged construction, the pay item "Temporary Soil Retention System" should be used because soil strengths exceed 4.5 tsf.



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		Division of Highways Illinois Department of Transp	ortation, Di	strict 3	3						Date	6/1	8/14
	ROUTE	IL 54 (SBI-48)	DES	SCR	IPTION	IL 5	54 over	Drainage Ditch, 7.06 mi 9	les North of IL	LOGG	ED BY	Larry	Myers
	SECTION	115-B		_ I			SW 1/	4, SEC. 15, TWP. 24N, F	NG. 8E, 3 rd PM ,				
	COUNTY	Ford DI	RILLING	ME	THOD		Hol	low Stem Auger	HAMMER TYPE	(CME A	utoma	tic
	STRUCT. NO. Station BORING NO. Station Offset	. 027-0021 (Exist. 425+87 01 (E. Quad.) 425+40 15.0 ft Lt.)	D E P T H	B L O W S	U C S Qu	M O I S T	Surface Water Elev Stream Bed Elev Groundwater Elev.: First Encounter Upon Completion	<u>746.23</u> ft 745.99 ft <u>Dry</u> ft 724.0 ft √	D E P T H	B L O W S	U C S Qu	M O I S T
	Ground Sur	face Elev754.04	ft	(ft)	(/6")	(tsf)	(%)	After Hrs	ft	(ft)	(/6")	(tsf)	(%)
	Gray Silty Cla	ulder Gravel, Black & ay Loam Fill		_	-			Hard Gray and Olive G Clay Loam Till (continu	ireen Silty ied)		5 6	4.5 S	14
	Stiff to Very S Silty Clay Loa	Stiff Black & Gray	751.54		2	2.0	18				2	4.5	14
					3	Р					7	S	
	Soft Gray & E with Sand/Gra	Brown Sandy Loam avel layers	749.54	-5	1	0.5 P	21			-25	5 8 10	5.3 S	15
	Very Stiff to F Gray Silty Cla	lard Olive Green and ay Loam Till	747.04		2 3 4	3.8 S	16				6 9 10	5.1 S	19
	Hard Gray Sil and Silt seam	lty Clay Till with Sand is	744.54 I	-10	3 4 6	4.2 S	14	0	1	<u>∑</u> -30 	6 10 10	5.6 S	18
15					5 8 9	4.6 S	16		Í C	4			
U IL_DOT.GDT 3/2/				-15	4 5 7	4.2 S	18		717.5	-35	5 8 10	4.8 S	19
021.GP			736.54					End of Boring			4		
RING 027-00	Very Stiff Gra	y Silt with Minor Clay	/	_	3 5 7	3.5 P	22						
SOIL BC			734.54	-20						-40			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer) The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)

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		Division of Highways Illinois Department of Tran	of Lation	1						Date	6/1	8/14
	ROUTE	IL 54 (SBI-48)	DESC	RIPTION	؛ ∟ا 	54 over	Drainage Ditch, 7.06 m 9	hiles North of IL	OGG	ED BY	Larry	Myers
		115-B		LOCAT		SW 1/	4, SEC. 15, TWP. 24N,	RNG. 8E, 3 rd PM,				
	COUNTY	Ford	DRILLING M	ETHOD		Hol	lde 40.53631, Longitud llow Stem Auger	HAMMER TYPE	(CME A	utoma	tic
	STRUCT. NO. Station BORING NO. Station Offset Cround Suff	027-0021 (Exis 425+87 02 (W. Quad.) 426+39 16.0 ft Rt.	<u>st.)</u> <u> </u>) B L O W I S	U C S Qu (tsf)	M O I S T	Surface Water Elev. Stream Bed Elev. Groundwater Elev.: First Encounter Upon Completion	746.23 ft 746.50 ft Dry ft Dry ft	D E P T H	B L O W S	U C S Qu (tsf)	M O I S T
	Augered Shou Silty Clay Loar	ulder Gravel, Black m Fill					Very Stiff Olive Silty C Till (continued)	Clay Loam		2 4 5	3.5 B	14
	Stiff Black Silt	y Clay Loam Fill	751.44	2 2 3	1.5 P	26				5 6 8	4.3 S	13
	Loam & Sand	/ Gravel Fill	746.94	-5 1 1 1	0.5 P	24	Hard Gray Silty Clay L with some Sand & Silt	728.94 .oam Till : seams	4 -25	4 5 9	4.9 S	13
	Hard Olive Silf	ty Clay Loam Till	744.44	3 5 7	4.1 S	15				4 5 8	4.8 S	16
	Hard Gray Silt	y Clay Till	 	10 3 5 6	4.0 S	13	Ċ	$\boldsymbol{\mathcal{V}}$	30 	4 5 5	4.1 S	22
15			 	5 6 8	5.4 S	17		Í O	4			
FU IL_DOI.GDI 3/2/	Hard Gray Silt	with Minor Clay	738.94 -	5 5 8 10	4.5 P	19	End of Boring	717.4	-35	4 6 7	4.3 S	15
L BORING 027-0021.G			734.44	3 5 6	4.0 P	20						
SO			-2	20					-40			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer) The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)