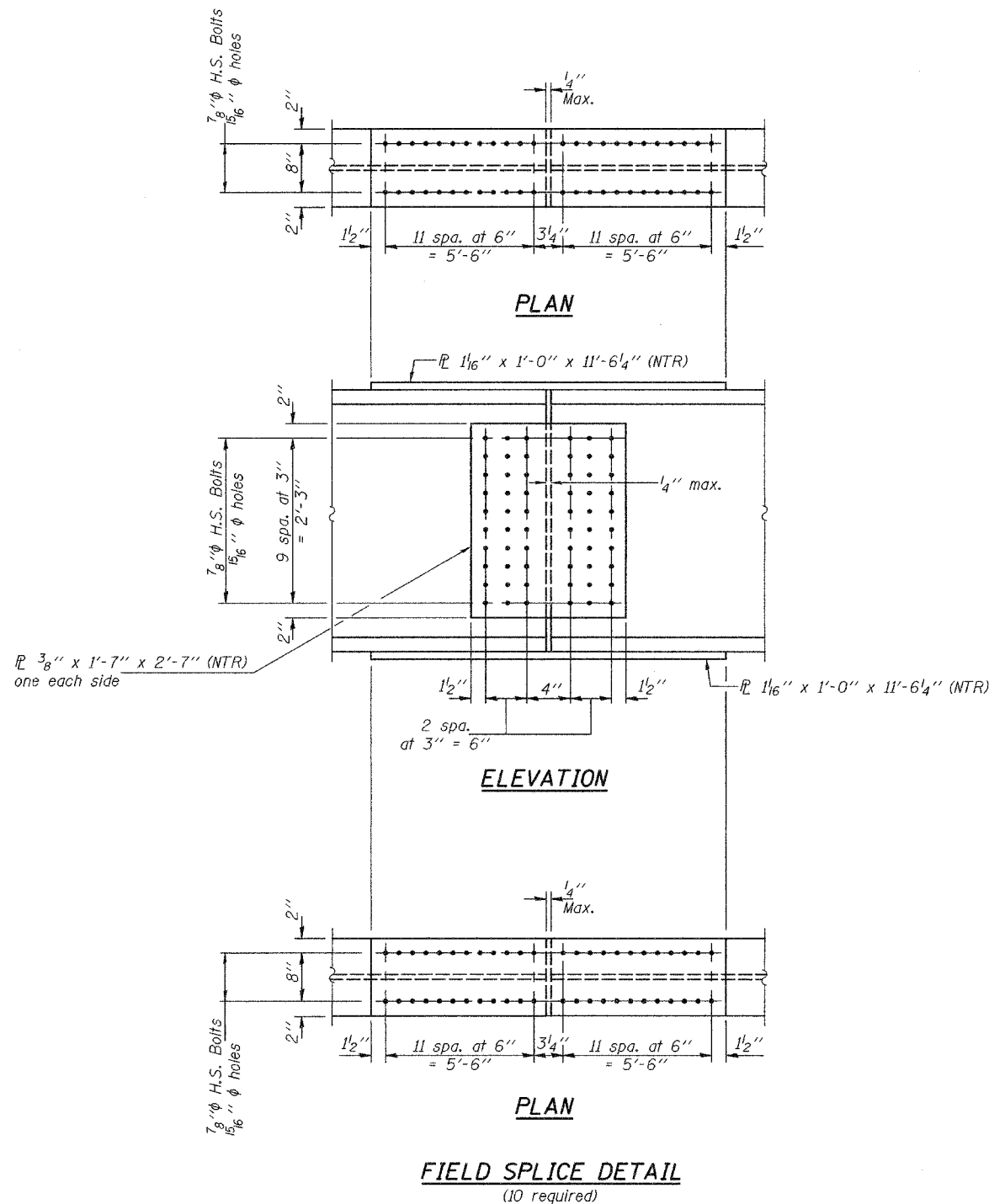


STATE OF ILLINOIS
DEPARTMENT OF TRANSPORTATION



INTERIOR GIRDER MOMENT TABLE

		0.4 Sp. 1	Pier 1	0.5 Sp. 2	Pier 2	0.6 Sp. 3
I_s	(in ⁴)	9750	9750	9750	9750	9750
I_c (n)	(in ⁴)	22651	-	22651	-	22651
I_c (3n)	(in ⁴)	16440	-	16440	-	16440
S_s	(in ³)	542	542	542	542	542
S_c (n)	(in ³)	753	-	753	-	753
S_c (3n)	(in ³)	676	-	676	-	676
S_f	(in ³)	24.5	24.5	24.5	24.5	24.5
ϕ	(k/ft.)	0.71	1.2	0.71	1.2	0.71
M_D	(k)	140.7	818.6	363.2	867.8	185
s_D	(k/ft.)	0.51	-	0.51	-	0.51
M_{sD}	(k)	96.4	-	223.4	-	117.3
M_L	(k)	351.8	369.2	460.4	390.6	388.7
M (Imp)	(k)	88	73.8	115.1	78.1	97.2
$S_3[M_L + M$ (Imp)]	(k)	733	738.3	959.2	781.2	809.8
M_a	(k)	1261	2024	2010	2144	1446
M_{be}	(k)	2.9	1.4	5.2	1.7	8.3
f_{sD} non-comp	(k.s.i.)	3.1	18.1	8	19.2	4.1
f_{sD} (comp)	(k.s.i.)	1.7	-	4	-	2.1
f_{s3} (k + Imp)	(k.s.i.)	11.7	16.3	15.3	17.3	12.9
f_2	(k.s.i.)	1.4	0.7	2.5	0.8	4.1
f_s (Overload)	(k.s.i.)	16.5	34.4	27.3	36.5	19.1
f_s (Total)	(k.s.i.)	21.5	44.7	35.5	47.5	24.8
F_{cr} (Overload)	(k.s.i.)	47.5	40	47.5	40	47.5
VR	(k)	23.7	-	20.1	-	27.4
F_{cr}	(k.s.i.)	49.5	48.3	49.2	48.2	48.6

INTERIOR GIRDER REACTION TABLE

		W. Abut.	Pier 1	Pier 2	E. Abut.
R_D	(k)	22.8	115.9	117	26.1
R_L	(k)	40.3	70.5	67.1	45.3
$Imp.$	(k)	12.1	17.6	16.8	13.6
R (Total)	(k)	75.2	204	200.9	85

I_s and S_s are the moment of inertia and section modulus of the steel section used in computing f_s (Total and Overload).

I_c (n) & S_c (n) are the moment of inertia and section modulus of the composite section used in computing stresses due to live load.

I_c (3n) and S_c (3n) are the moment of inertia and section modulus of the composite section used in computing stresses due to superimposed dead loads (See AASHTO 10.38).

S_f is the section modulus for one flange plate for lateral flange bending.

M_D - Moment due to dead loads on non-composite section.

M_{sD} - Moment due to dead loads on composite section.

M_L - Moment due to live load on non-composite or composite section.

M (Imp) - Moment due to live load impact on non-composite or composite section.

M_a (Applied Moment) = $1.3 [M_D + M_{sD} + \frac{5}{8} (M_L + M$ (Imp))].

M_{be} is the lateral bending moment for one flange plate (factored).

f_s (Overload) is the sum of the stresses due to $M_D + M_{sD} + \frac{5}{8} (M_L + M$ (Imp)).

f_2 is the calculated normal stress at the edge of the flange due to lateral bending (factored).

f_s (Total) is the sum of the stresses due to $1.3 [M_D + M_{sD} + \frac{5}{8} (M_L + M$ (Imp))].

F_{cr} (Overload) is the critical average flange stress at overload computed according to the 2003 AASHTO Guide Specifications for Horizontally Curved Steel Girder Highway Bridges Section 9.5.

VR is the maximum ϕ + impact shear range in span.

F_{cr} is the critical average flange stress computed according to the 2003 AASHTO Guide Specifications for Horizontally Curved Steel Girder Highway Bridges Sections 5.2, 5.3 and 5.4.

M_L and R_L includes the effects of centrifugal force and superelevation.

Note: "NTR" denotes elements to which notch toughness requirements are applicable.

DESIGNED	J. Mann
CHECKED	G. Ahanchi
DRAWN	BECKY M. LEACH
CHECKED	JWM/GRA

December 1, 2005

EXAMINED *Thomas J. Namagala*
ENGINEER OF BRIDGE DESIGN

PASSED *Ralph E. Anderson*
ENGINEER OF BRIDGES AND STRUCTURES

STRUCTURAL STEEL DETAILS
F.A.U. ROUTE 7968
SECTION 3R(BR, BR-1, BR-2)19RS-8
SANGAMON COUNTY
STATION 17+97.34
STRUCTURE NO. 084-0518