



Original Report Date: <u>12-6-2018</u>	Proposed SN: <u>046-0159</u>	Route: <u>FAI 57 over Grinnell Rd</u>
Revised Date: <u>6-6-2019</u>	Existing SN: <u>046-0010, 11</u>	Section: <u>(139 VB)ES</u>
Geotechnical Engineer: <u>Terrence McCleary of McCleary Engineering</u>		County: <u>Kankakee</u>
Structural Engineer: <u>Michael Haley of Lin Engineering, Ltd.</u>		Contract <u>66F74</u>

Indicate the proposed structure type, substructure types, and foundation locations (attach plan and elevation drawing): Subject twin structures, carrying Interstate 57 over Grinnell Road, SN 046-0158 and -0159, will be 3 span, 159.25 ft. B-B abuts., 48 ft. wide F-F. The structures will have an 8 inch concrete deck on 36 inch PPC beams. The bridge will have integral abutments supported on steel piles driven to refusal and piers with drilled shaft column bents socketed into limestone. Existing skew equals 2.35°, no proposed skew. The total factored loading is 1538 kips at the abutments and 4832 kips at the piers. The width of each bridge is 50 ft. 11 inch O-O, future widening to allow 3 lanes in each direction could make that 62 ft. 11 inch O-O. The vertical profile of the roadway will be raised ±2 ft. See attached TSL for further information.

Discuss the existing boring data, existing plans foundation information, new subsurface exploration and need for any additional exploration to be provided with SGR Technical Memo (attach all data and subsurface profile plot): Four borings were taken in March 2018. Four other borings were taken in November 2017, however, the augered material was not documented. It did record the top of rock; 2 rock cores were taken. The 2018 borings were advanced about 25 ft. through the bridge and roadway fill, consisting of stiff to hard Silty Clay Loams and Silty Clay Loam Tills above a loose to medium, rust red/brown/black fine to coarse Sand. Groundwater was not reported. The fine to coarse sand overlaid bedrock, with a highly weathered limestone to a dense limestone/dolostone surface. Two rock cores were taken in 2017 at locations right (west side) and left (east side) of the existing structures on Grinnell Road. The elevation of the limestone surface was 631.47 on the right and 630.47 on the left. Below 1 to 5 ft. of highly fractured limestone the cores reported dense gray limestone with horizontal fractures with tight joints with strengths ranging from 630 to 1530 tsf. See attached 2017 & 2018 borings, rock cores, and the subsurface profile plot.

The existing structures were originally constructed in 1954 and widened in 1990. The 1954 bridge was supported by open counterfort abutments on spread footings bearing on rock, the pier columns were supported on spread footings bearing on rock. The 1990 bridge widening work is all supported by H piles bearing on rock. The 1954 General Plan and Elevation sheet is attached. The 1990 pile driving records for the widening improvement are attached to this SGR (note the 1990 elevation datum matches the 1954 datum, the one used for this improvement is different).

Provide the location and maximum height of any new soil fill or magnitude of footing bearing pressure. Estimate the amount and time of the expected settlement. Indicate if further testing, analysis, and/or ground improvement/treatment is necessary: The profile of the interstate will be raised ±2 ft.; any fill is expected to be granular material. Considering the length of time the existing structures have been in place and that no significant settlement problems have been reported, minimal, if any settlement is expected. No further testing, analysis, or ground improvement is necessary.

Identify any new cuts or fill slope angles and heights. Estimate the factor of safety against slope failure. Indicate if further testing, analysis or ground improvement/treatment is necessary: There are no cross sections this time, however with the slight raise in grade anticipated, fill slope angles will remain the same on the end slopes and will remain the same or become slightly steeper on the side slopes. Standard construction practices will result in stable side slopes. A temporary (undrained) condition was analyzed for a proposed worst case scenario end slope situation, the resulting factor of safety was 4.44 against slope failure. See attached slope stability analysis.

Indicate at each substructure, the 100-year and 200-year total scour depths in the Hydraulics report, the non-granular scour depth reduction, the proposed ground surface, and the recommended foundation design scour elevations: N/A

Determining the seismic soil site class, the seismic performance zone, the 0.2 and 1.0 second design spectral accelerations and indicate if that the soils are liquefiable: This site has a soil site class of "C", the seismic performance zone, SPZ = 1. The S_{DS} = 0.125 g and the S_{D1} = 0.072 g. Because the S_{D1} is less than 0.15 g, a liquefaction analysis is NOT required. See attached Seismic Report.

Confirm feasibility of the proposed foundation or wall type and provide design parameters. Attach a pile design table indicating feasible pile types, various nominal required bearings, factored resistances available and corresponding estimated lengths at locations where piles will be used. Provide factored bearing resistance and unit sliding resistance at various elevations and confirm no ground improvement/treatment is necessary where spread footings are proposed. Estimated top of rock elevations as well as preliminary factored unit side and tip resistance values shall be indicated when drilled shafts are proposed: Data from the 2018 borings were used to populate the fields in the pile length spreadsheets. Data from the 2017 cores were used to populate the drilled shaft spreadsheets.

Strength I loading was used at the substructures as follows: Abutments = 1538 kips, Piers = 4832 kips. H piles are recommended bear against the bedrock. The site is in a SPZ 1, therefore, liquefaction was not analyzed. We recommend one test pile per abutment. Metal Shell or concrete piling is not recommended. No reductions in the geotechnical analyses were used because all the substructure supports will be bearing on the limestone bedrock. See Pile Attachments, Table 1, PILE LENGTH TABLES.

Assumptions used for the pile length analysis include:

- The bottom elevation of both north abutments = 655.6.
- The bottom elevation of both the south abutments = 657.9
- The cutoff elevation for the piling allowed a 2 ft. embedment into the concrete.
- Pile shoes are recommended to drive into fractured bedrock.

See attached for pile length estimating spreadsheets, 2018 boring logs, and loading documentation.

Integral Abutments: The information from 2018 Boring 1 and 2 was to populate the fields in the integral abutment worksheet for the SB structure and Boring 3 and 4 was used for the NB structure. The stiffness of the soils at both structures dictate the need to precure the piles at all 4 abutments. Utilizing bentonite to backfill a 10 ft. precure at an 18 inch diameter would allow the required movement for integral abutments.

Drilled Shafts: Table 2 presents the factored side, tip and combined side and tip resistances for 48, 54, and 60 inch diameter rock sockets at the northbound and southbound piers. To complete this Table 2, the data from the last foot of the core was extended an additional 5 ft. below the bottom of the rock core.

Table 2, Drilled shaft resistance

Piers 1 and 2	Shaft Diameter, inches	Socket Depth, foot	Factored Side Resistance, kips	Factored Tip Resistance, kips	Combined Side and Tip Resistance, kips
NB	48	4	451	5331	1641
	48	6	903	5295	1967
	48	8	1355	31954	2417
	48	10	1806	32219	2593
	54	4	507	6748	2049
	54	6	1016	6735	2384
	54	8	1524	40516	2892
	54	10	2032	40814	3064
	60	4	564	8342	2501
	60	6	1128	8348	2836
	60	8	1693	50094	3401
	60	10	2258	50425	3565
	SB	48	4	225	2841
48		6	677	4013	3664
48		8	1129	36429	2655
48		10	1581	34165	2624
54		4	253	3590	2441
54		6	761	5035	4590
54		8	1270	45712	3230
54		10	1778	43165	3132
60		4	281	4435	3054
60		6	846	6173	5616
60		8	1411	56046	3857
60		10	1976	53216	3675

See the attached drilled shaft tables for further information. See the attached 2017 Rock Core Logs for further information on rock quality.

The recommended soil parameters for a lateral load analysis using the L-pile software are shown in the Table 3.

Table 3, Lateral Load Soil Parameters

Soil Type	Angle of Internal Friction (degrees)	Average Undrained Cohesion, (psf)	Static Soil Modulus k (pci)	Soil Strain Parameter E ₅₀	Total Unit Wt. (pcf)	Effective Unit Wt. (pcf)	UCS of Rock, (ksf)
V. Stiff Silty Clay Loam Fill	-	3000	1000	0.005	125	62.6	-
Loose Loamy Fine Sand	30	-	25	-	115	52.6	-
Fractured Limestone treated as Gravel	46	-	200	-	-	-	-
Dense Limestone	-	-	-	-	155	92.6	2000

Calculate the estimated water surface elevation and determine the need for cofferdams (type 1 or 2), and seal coat: N/A

Assess the need for sheeting or soil retention or temporary construction slope and provide recommendation for other construction concerns: Stage construction utilizing crossovers should minimize construction conflicts. The borings indicate sheet piling can be driven to a sufficient depth to permit abutment construction. The proposed foundations have been spaced to avoid conflict with the existing substructures. The substructures shall be removed as per Section 501 if the 2016 IDOT Standard Specifications for Road and Bridge Construction.

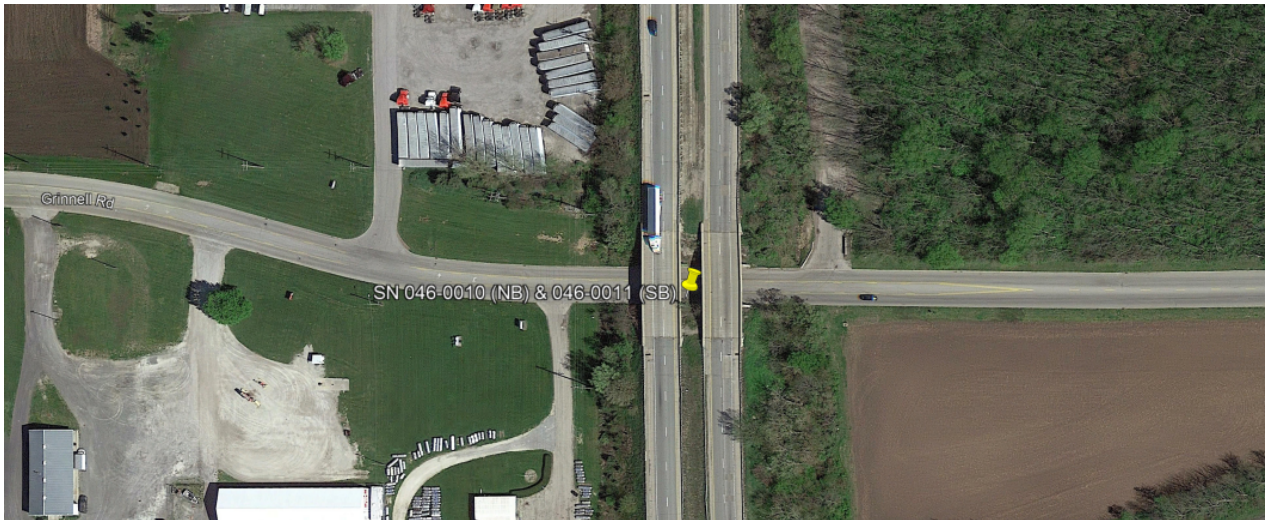
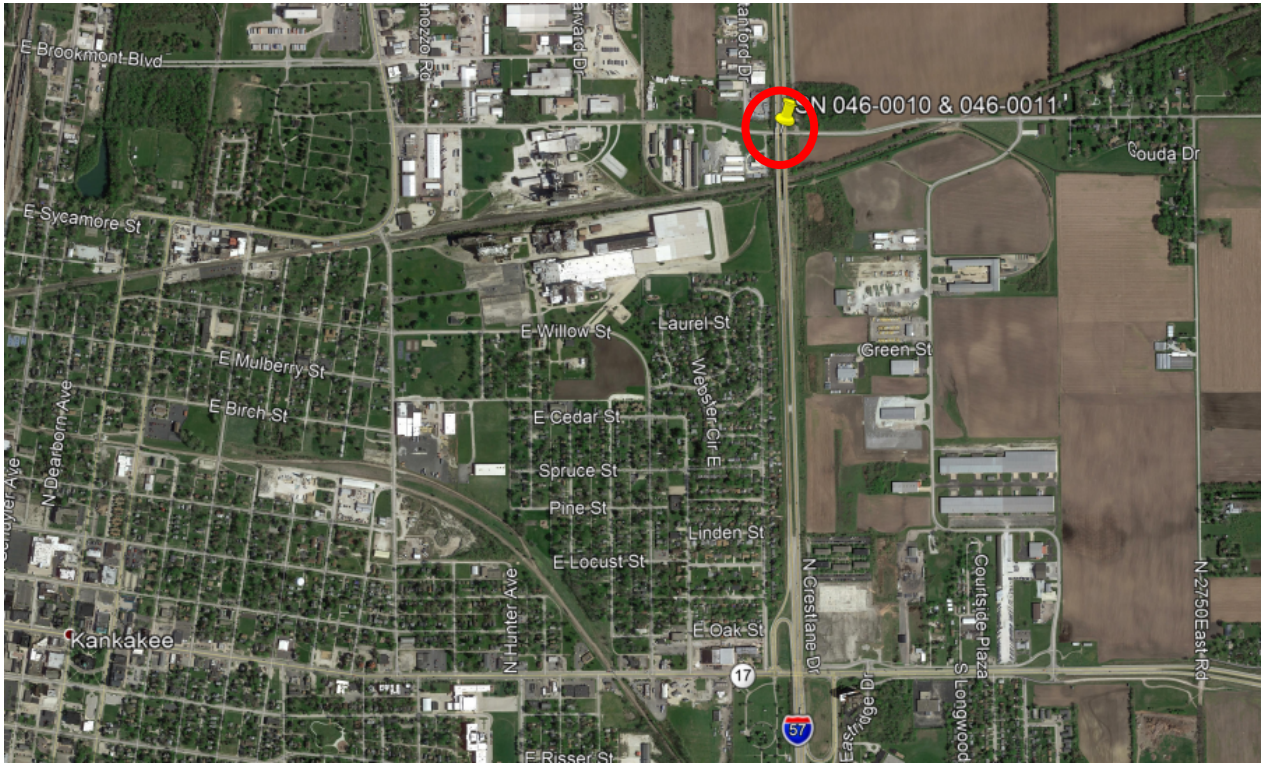
Prepared by McCleary Engineering
 Terrence McCleary, PE
 Office 815-780-8486
Terry@McClearyEngineering.com



Terrence L. McCleary
 Illinois Professional Engineer
 License No. 062.050019 Exp. 11/2019

LOCATION MAP

SNs 046-0010 & 046-0011



FAI-57(I-57)
Section (139VB)ES
Kankakee County
SNs 046-0010 (NB) & 046-0011 (SB) (Exist)
I-57 over Grinnell Rd.
1.0 Mi. N of IL-17

Bench Mark (BM 140): Chiseled "□" top of curb at southeast end of east parapet wall SN 046-0010, Sta. 139+61, 54' Left, Elev. 663.37.
 Existing Structures: S.N. 046-0010 (N.B.) and S.N. 046-0011 (S.B.), built in 1954 as F.A. Rte 26, Section 139-HB3-HF3, at station 138+90.96. The bridge decks were replaced and structures widened in 1990 under F.A.I. Rte 57, Section 139HBR-3. The existing dual structures are 3-span bridges with rolled steel beams supported on spill-thru counterfort abutments and multi-column concrete piers on spread footings. 120'-2" back to back abutments, 43'-2" out to out deck with a 2'-21'-00" left ahead skew. Structures to be removed and replaced. Traffic shall be maintained utilizing crossovers during construction. No Salvage.

LOADING HL-93

Allow 50#/sq. ft. for future wearing surface.

DESIGN SPECIFICATIONS

2017 AASHTO LRFD Bridge Design Specifications, 8th Edition

DESIGN STRESSES

FIELD UNITS

$f'_c = 3,500$ psi
 $f'_c = 4,000$ psi (Superstructure Concrete)
 $f_y = 60,000$ psi (Reinforcement)

PRECAST PRESTRESSED UNITS

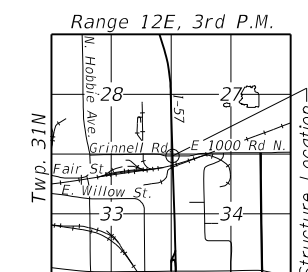
$f'_c = 8,500$ psi
 $f'_{ci} = 7,000$ psi
 $f_{pu} = 270,000$ psi (0.6" \circ low lax. strands)
 $f_{pbt} = 202,300$ psi (0.6" \circ low lax. strands)

SEISMIC DATA

Seismic Performance Zone (SPZ) = 1
 Design Spectral Acceleration at 1.0 sec. (SD1) = 0.072 g
 Design Spectral Acceleration at 0.2 sec. (SDS) = 0.125 g
 Soil Site Class = C

HIGHWAY CLASSIFICATION

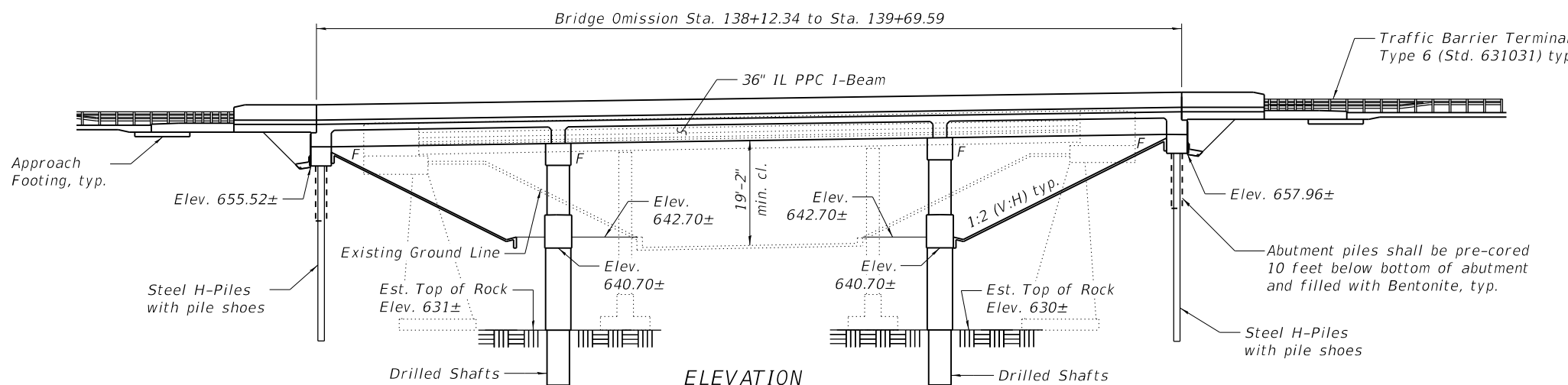
F.A.U. Rte. 6221 (Grinnell Rd.)	F.A.I. Rte. 57
Functional Class: Minor Arterial	Functional Class: Interstate
ADT: 3,120 (2021); 3,720 (2041)	ADT: 31,392 (2021); 37,152 (2041)
ADTT: 250 (2021); 298 (2041)	ADTT: 7,409 (2021); 8,768 (2041)
DHV: 312 (2021); 372 (2041)	DHV: 3,139 (2021); 3,715 (2041)
Design Speed: 30 m.p.h.	Design Speed: 75 m.p.h.
Posted Speed: 30 m.p.h.	Posted Speed: 70 m.p.h.
Two-Way Traffic	Two-Way Traffic
Directional Distribution: 50:50	Directional Distribution: 50:50



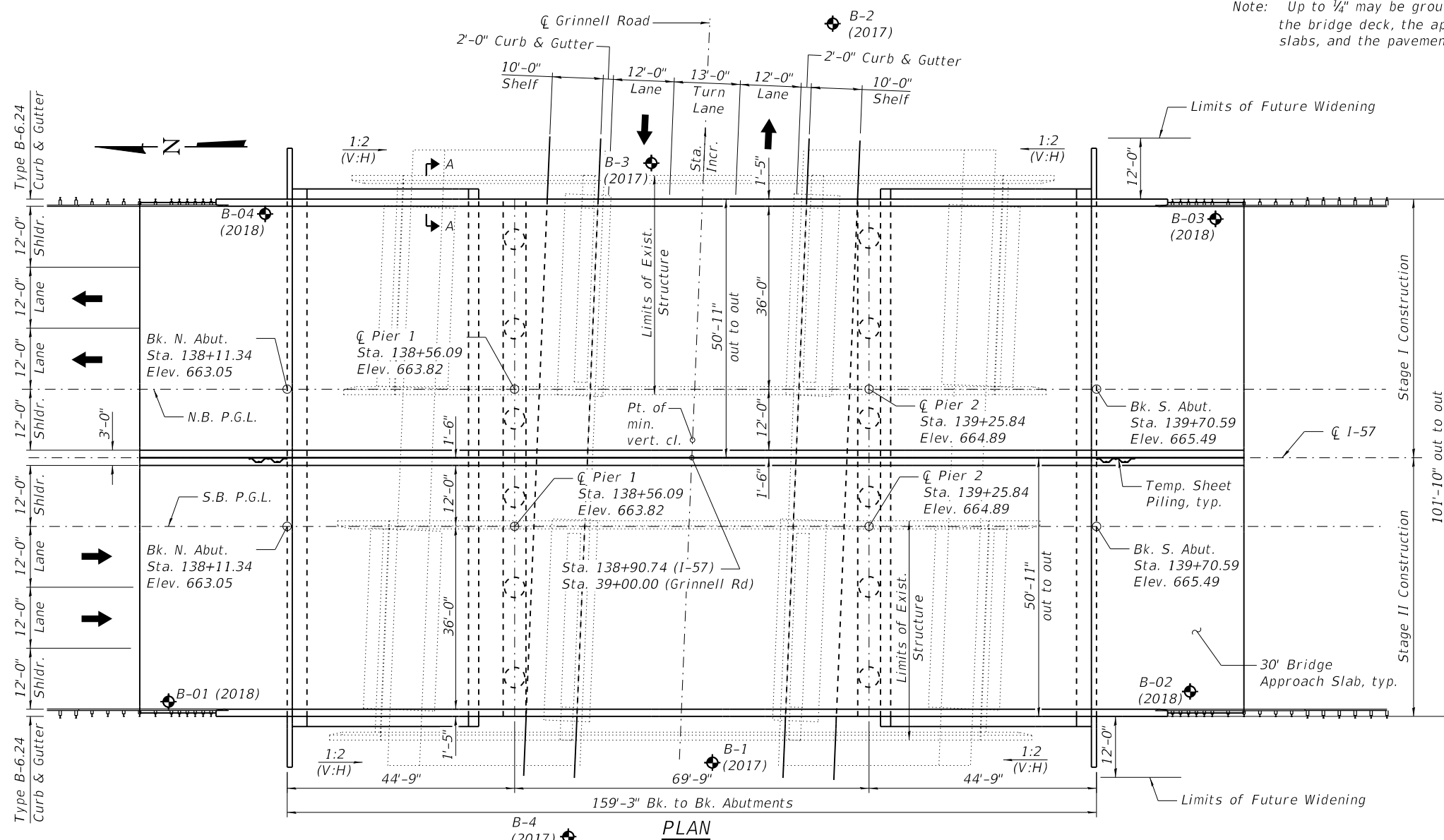
LOCATION SKETCH

GENERAL PLAN & ELEVATION

I-57 OVER GRINNELL ROAD
F.A.I. RTE 57 - SEC. [(139)HB-3]ES
KANKAKEE COUNTY
STATION 138+90.74
STRUCTURE NO. 046-0158 (N.B.)
STRUCTURE NO. 046-0159 (S.B.)



Note: Up to 1/4" may be ground off the bridge deck, the approach slabs, and the pavement connectors.



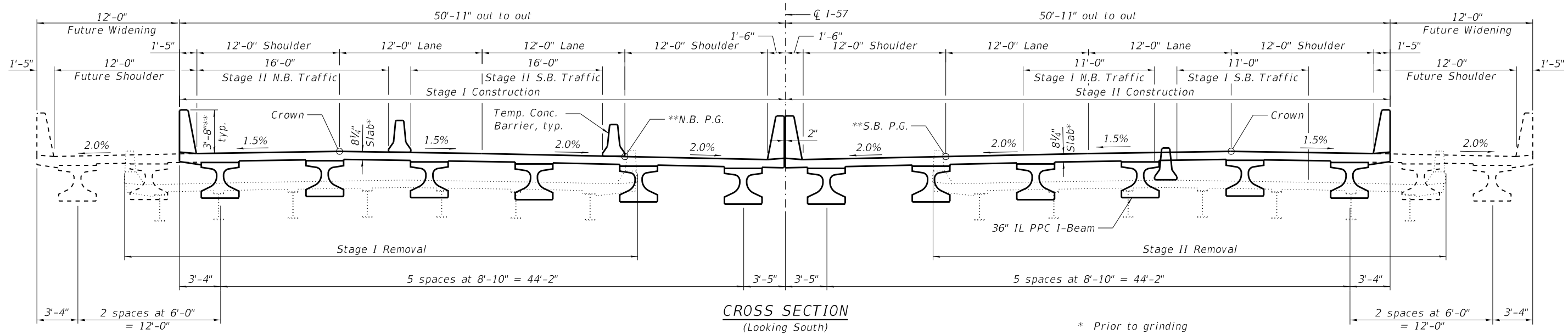
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LE LIN ENGINEERING, LTD.
 Consulting Engineers
 Springfield, Illinois

USER NAME =	DESIGNED - MTH	REVISED -
PLOT SCALE =	CHECKED - VPT	REVISED -
PLOT DATE = 2/19/2019	DRAWN - DAS	REVISED -
	CHECKED - MTH	REVISED -

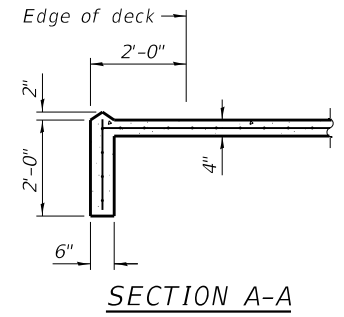
STATE OF ILLINOIS
DEPARTMENT OF TRANSPORTATION

F.A.I. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
57	[(139)HB-3]ES	KANKAKEE		
CONTRACT NO. 66F74				
ILLINOIS FED. AID PROJECT				

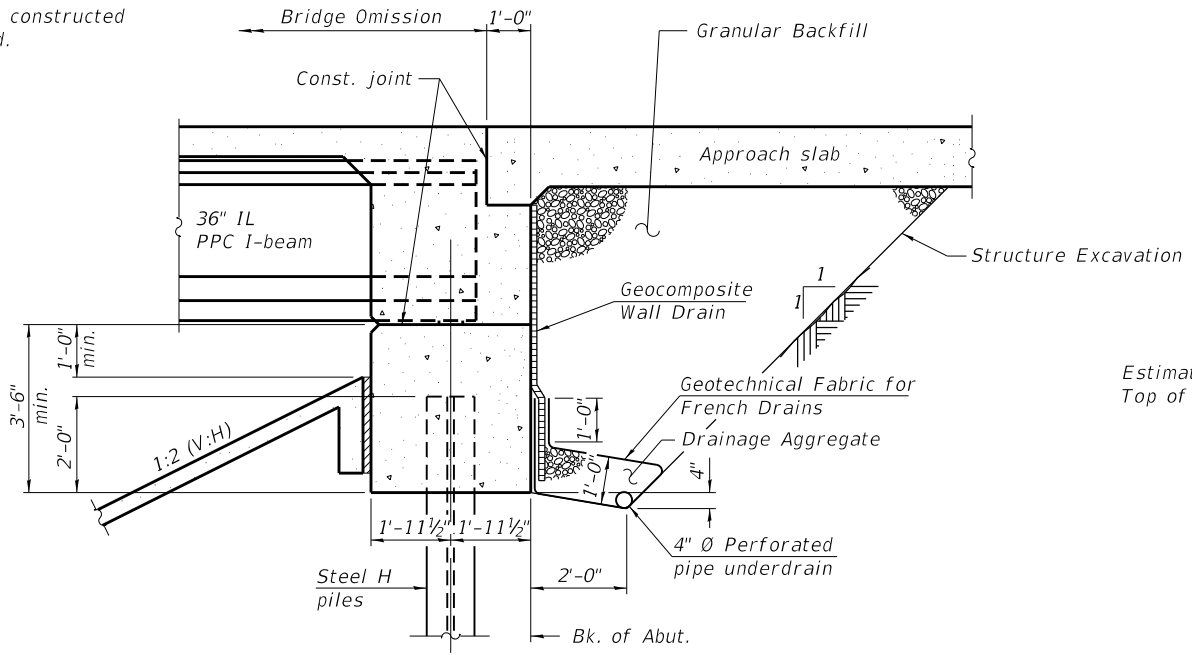


Note:
Both median parapets shall be constructed after Stage II deck is completed.

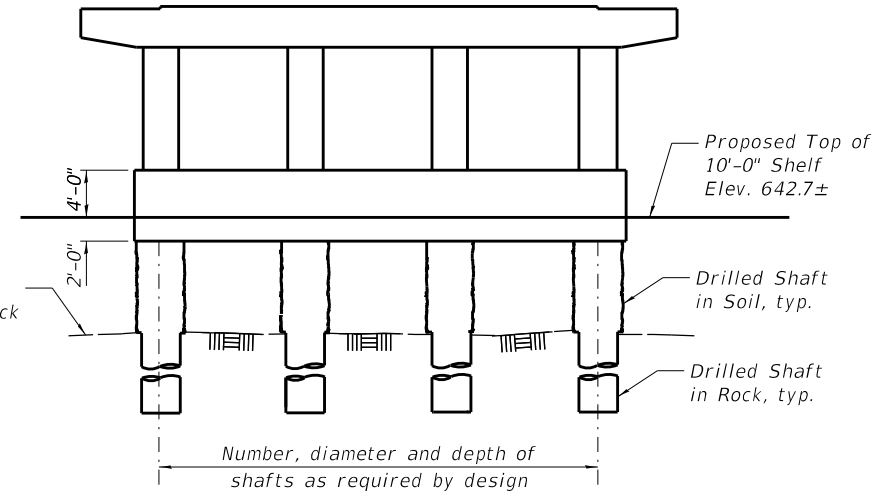
* Prior to grinding
** After grinding



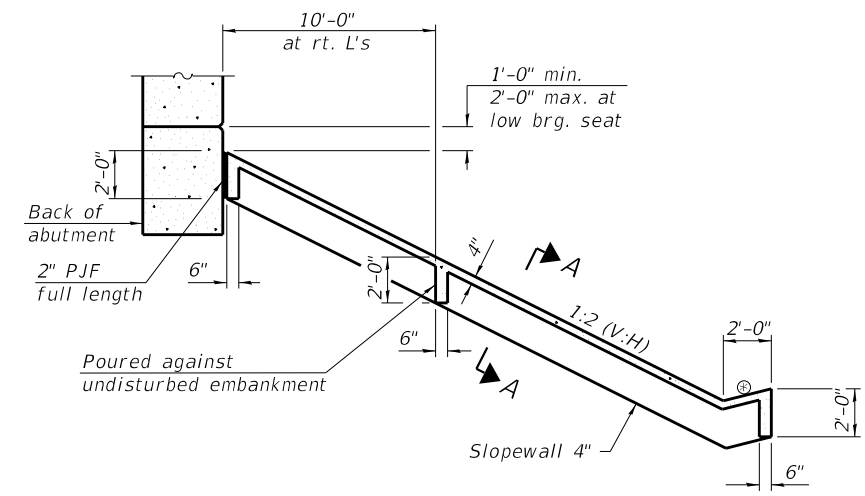
SECTION A-A



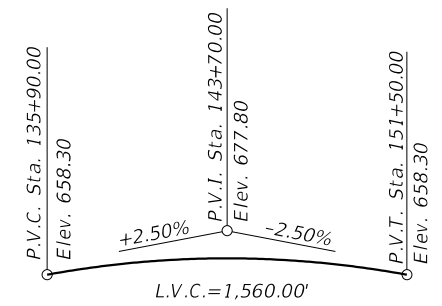
SECTION THRU INTEGRAL ABUTMENT



PIER SKETCH
(Separate piers for N.B. and S.B. bridges)



SECTION THRU CONCRETE SLOPEWALL



I-57 PROFILE GRADE
(Along inside edge of pavement)
(PG shows final elevations after grinding)



GRINNELL ROAD PROFILE GRADE
(Along centerline roadway)

GENERAL DATA
I-57 OVER GRINNELL ROAD
F.A.I. RTE 57 - SEC. [(139)HB-3]ES
KANKAKEE COUNTY
STATION 138+90.74
STRUCTURE NO. 046-0158 (N.B.)
STRUCTURE NO. 046-0159 (S.B.)

MODEL: Default
FILE NAME: EX11609-1\Struct\TSL\CADD\CADD_Sheets\I57\046-0010&0011-002-GeneralData.dgn



USER NAME =	DESIGNED - MTH	REVISED -
PLOT SCALE =	CHECKED - VPT	REVISED -
PLOT DATE = 2/19/2019	DRAWN - DAS	REVISED -
	CHECKED - MTH	REVISED -

STATE OF ILLINOIS
DEPARTMENT OF TRANSPORTATION

F.A.I. RTE.	SECTION	COUNTY	TOTAL SHEETS	SHEET NO.
57	[(139)HB-3]ES	KANKAKEE		
CONTRACT NO. 66F74				
ILLINOIS FED. AID PROJECT				



SOIL BORING LOG

ROUTE FAI 57 (I-57) DESCRIPTION I-57 over Grinnell Road, 0.95 Miles North of IL 17 LOGGED BY Larry Myers

SECTION 139HBR-3 LOCATION NW 1/4, SEC. 34, TWP. 31N, RNG. 12E, 3rd PM,
Latitude 41.133472, Longitude -87.836087

COUNTY Kankakee DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME Automatic

STRUCT. NO. 046-0010/0011
 Station 138+90.96

BORING NO. 04
 Station 138+07
 Offset 48.0 ft Lt.
 Ground Surface Elev. 660.59 ft

D E P T H H	B L O W S	U C S Qu	M O I S T	Surface Water Elev. _____ ft	D E P T H H	B L O W S	U C S Qu	M O I S T
(ft)	(/6")	(tsf)	(%)	Stream Bed Elev. _____ ft	(ft)	(/6")	(tsf)	(%)

Augered Bituminous Shoulder. Black Silty Clay Loam Fill				Very Stiff Black, Gray, Brown Silty Clay Loam Fill with Asphalt Pieces at 21.5 ft. (continued)	658.09	6		
						8	3.7	10
						16	B	
Stiff to Very Stiff Black Silty Clay Loam and Brown & Gray Silty Clay Loam Fill	2			Medium Rust Red / Brown Fine to Coarse Sand	637.59	4		
	3	1.8	29			5		18
	3	P				6		
	-5					-25		
	2					4		
	3	2.0	29			5		10
	2	P				5		
	2					4		
	1	1.5	28			5		7
	2	P			631.59	6		
				Dense Gray Limestone / Dolostone - Weathered at Surface				
	-10				630.34	-30		
	1			End of Boring		100/3"		6
	1	1.5	26					
	2	P						
Very Stiff Black, Gray, Brown Silty Clay Loam Fill with Asphalt Pieces at 21.5 ft.								
	3							
	4	2.9	19					
	5	B						
	-15					-35		
	2							
	5	3.2	17					
	6	B						
	3							
	6	3.5	15					
	7	B						
	-20					-40		

SOIL BORING 046-0010,0011.GPJ IL_DOT.GDT 3/29/18

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
 The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



SOIL BORING LOG

ROUTE FAI 57 (I-57) DESCRIPTION I-57 over Grinnell Road, 0.95 Miles North of IL 17 LOGGED BY Larry Myers

SECTION 139HBR-3 LOCATION NE 1/4, SEC. 33, TWP. 31N, RNG. 12E, 3rd PM,
Latitude 41.133231, Longitude -87.836477

COUNTY Kankakee DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME Automatic

STRUCT. NO. 046-0010/0011
Station 138+90.96

BORING NO. 1
Station 138+95
Offset 60.0 ft Rt.
Ground Surface Elev. 641.47 ft

**D
E
P
T
H** (ft)
**B
L
O
W
S** (/6")
**U
C
S** (tsf)
**M
O
I
S
T** (%)

Surface Water Elev. _____ ft
Stream Bed Elev. _____ ft
Groundwater Elev.:
First Encounter None ft
Upon Completion _____ ft
After _____ Hrs. _____ ft

Augered Material - Not Documented

631.47 -10

Borehole continued with rock coring.

-15

-20

SOIL BORING 046-0010,0011.GPJ IL_DOT.GDT 9/25/18

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



SOIL BORING LOG

ROUTE FAI 57 (I-57) DESCRIPTION I-57 over Grinnell Road, 0.95 Miles North of IL 17 LOGGED BY Larry Myers

SECTION 139HBR-3 LOCATION NW 1/4, SEC. 34, TWP. 31N, RNG. 12E, 3rd PM,
Latitude 41.133181, Longitude -87.835945

COUNTY Kankakee DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME Automatic

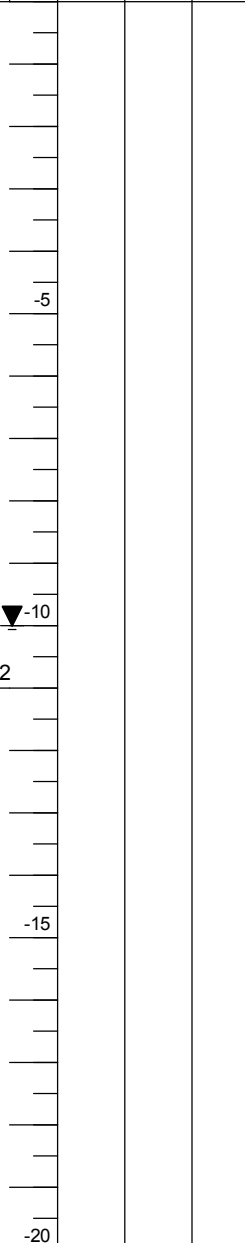
STRUCT. NO. 046-0010/0011
 Station 138+90.96

BORING NO. 2
 Station 139+12
 Offset 84.0 ft Lt.
 Ground Surface Elev. 641.42 ft

D E P T H (ft)
B L O W S (/6")
U C S (tsf)
M O I S T (%)

Surface Water Elev. _____ ft
 Stream Bed Elev. _____ ft
 Groundwater Elev.:
 First Encounter 631.4 ft ▼
 Upon Completion _____ ft
 After _____ Hrs. _____ ft

Augered Material - Not Documented



Rock Surface
 End of Boring

SOIL BORING 046-0010,0011.GPJ IL_DOT.GDT 9/25/18

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
 The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



SOIL BORING LOG

ROUTE FAI 57 (I-57) DESCRIPTION I-57 over Grinnell Road, 0.95 Miles North of IL 17 LOGGED BY Larry Myers

SECTION 139HBR-3 LOCATION NW 1/4, SEC. 34, TWP. 31N, RNG. 12E, 3rd PM,
Latitude 41.133265, Longitude -87.836022

COUNTY Kankakee DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME Automatic

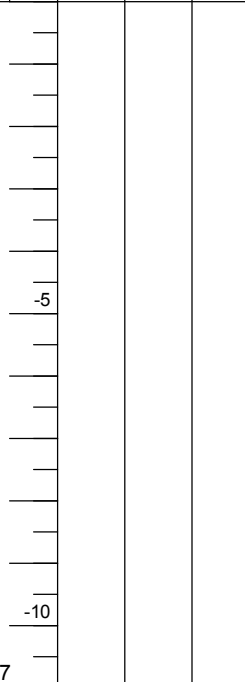
STRUCT. NO. 046-0010/0011
Station 138+90.96

BORING NO. 3
Station 138+83
Offset 58.0 ft Lt.
Ground Surface Elev. 641.47 ft

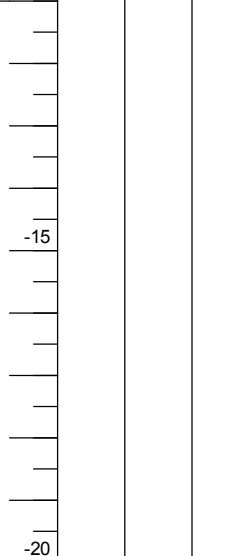
D E P T H	B L O W S	U C S Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

Surface Water Elev. _____	ft
Stream Bed Elev. _____	ft
Groundwater Elev.:	
First Encounter _____	None ft
Upon Completion _____	ft
After _____ Hrs.	ft

Augered Material - Not Documented



Borehole continued with rock coring.



SOIL BORING 046-0010,0011.GPJ IL_DOT.GDT 9/25/18

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



SOIL BORING LOG

ROUTE FAI 57 (I-57) DESCRIPTION I-57 over Grinnell Road, 0.95 Miles North of IL 17 LOGGED BY Larry Myers

SECTION 139HBR-3 LOCATION NE 1/4, SEC. 33, TWP. 31N, RNG. 12E, 3rd PM,
Latitude 41.13331, Longitude -87.836545

COUNTY Kankakee DRILLING METHOD Hollow Stem Auger HAMMER TYPE CME Automatic

STRUCT. NO. 046-0010/0011
Station 138+90.96

BORING NO. 4
Station 138+73
Offset 82.0 ft Rt.
Ground Surface Elev. 641.35 ft

**D
E
P
T
H** (ft)
**B
L
O
W
S** (/6")
**U
C
S** (tsf)
**M
O
I
S
T** (%)

Surface Water Elev. _____ ft
Stream Bed Elev. _____ ft
Groundwater Elev.:
First Encounter Dry ft
Upon Completion Dry ft
After _____ Hrs. _____ ft

Augered Material - Not Documented

632.35

Rock Surface
End of Boring

-10

-15

-20

SOIL BORING 046-0010,0011.GPJ IL_DOT.GDT 9/25/18

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)
The SPT (N value) is the sum of the last two blow values in each sampling zone (AASHTO T206)



McCleary Engineering
 3705 Progress Blvd, Ste 2
 Peru, Illinois 61354
 Telephone: 815-780-8486

ROUTE FAI 57
 SECTION 139HBR-3
 COUNTY Kankakee
 PROJECT LOCATION Grinnell Rd

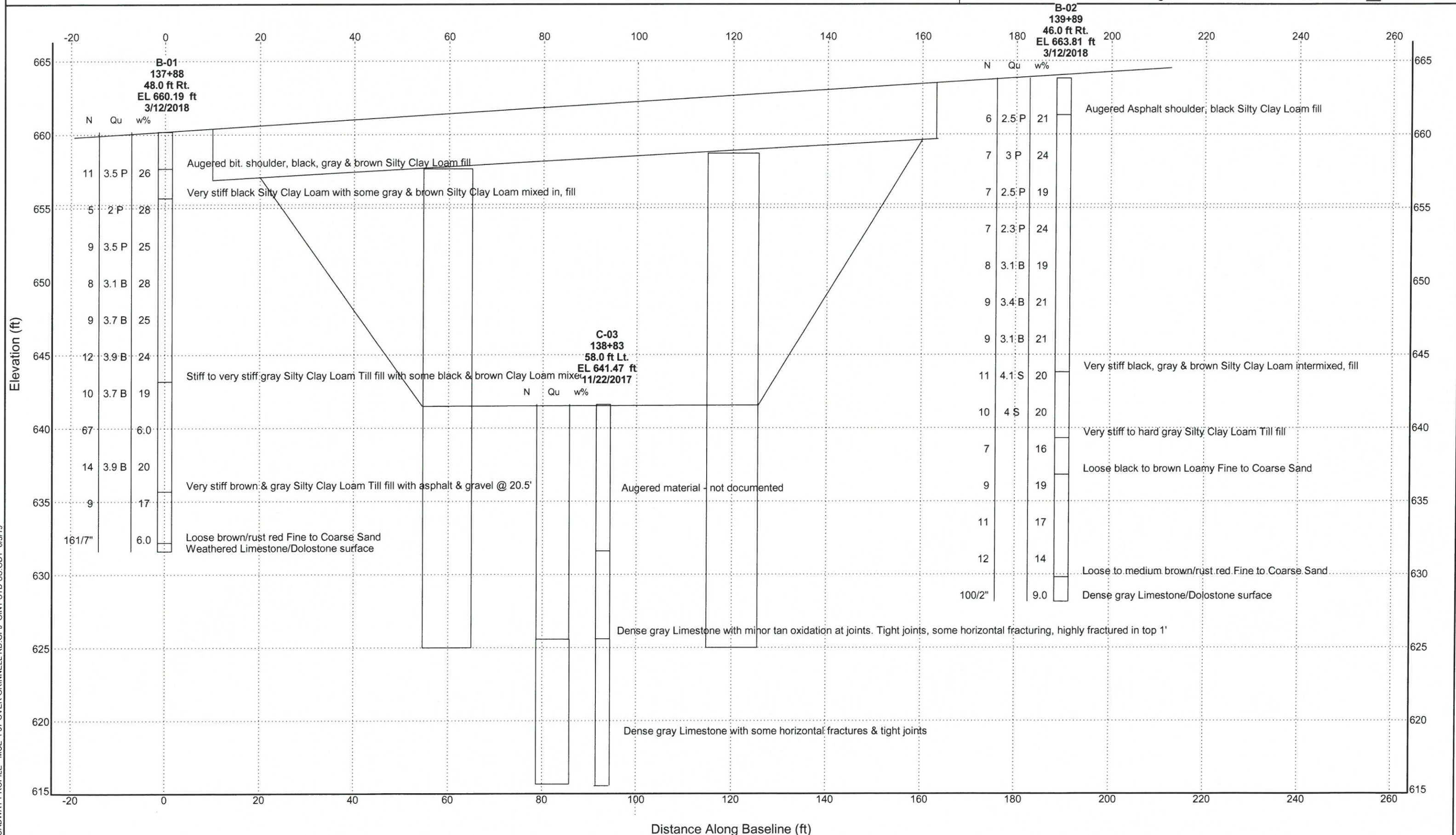
SUBSURFACE PROFILE I-57 over Grinnell Road in Kankakee

LEGEND

EL = Elevation (ft)
 D = Depth Below Existing Ground Surface (ft)
 N = SPT N-Value (AASHTO T206)
 Qu = Unconfined compressive Strength (tsf)
 Failure Mode (B= Bulge, S= shear, P= penetrometer)
 w% = Moisture Content Percentage

WATER TABLE LEGEND

▼ = First Encountered
 ▽ = Upon Completion
 ▾ = After ___ hours



ROADWAY PROFILE - MCE I-57 OVER GRINNELL RD.GPJ GINT STD US.GDT 6/3/19



McCleary Engineering
 3705 Progress Blvd, Ste 2
 Peru, Illinois 61354
 Telephone: 815-780-8486

ROUTE FAI 57
 SECTION 139HBR-3
 COUNTY Kankakee
 PROJECT LOCATION Grinnell Rd

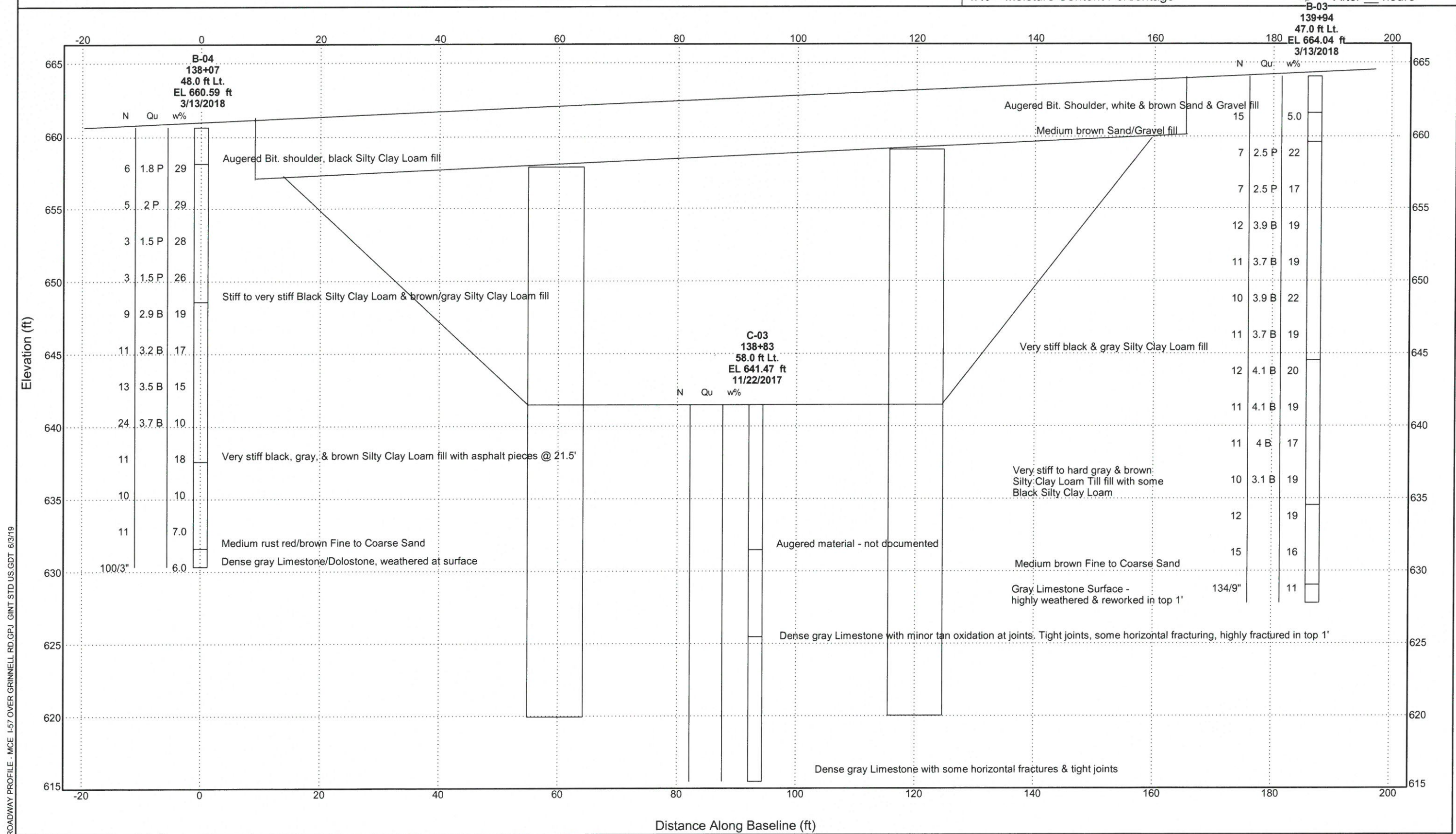
SUBSURFACE PROFILE I-57 over Grinnell Road in Kankakee

LEGEND

EL = Elevation (ft)
 D = Depth Below Existing Ground Surface (ft)
 N = SPT N-Value (AASHTO T206)
 Qu = Unconfined compressive Strength (tsf)
 Failure Mode (B= Bulge, S= shear, P= penetrometer)
 w% = Moisture Content Percentage

WATER TABLE LEGEND

▼ = First Encountered
 ▽ = Upon Completion
 ▾ = After ___ hours



ROADWAY PROFILE - MCE I-57 OVER GRINNELL RD.GPJ_GINT STD US.GDT 6/3/19

I-57 over Grinnell Road

SN 046-0010 / 0011

Hole # 1 11-21-2017

Depth 10 FT to 19.5 FT

Box 1 of 2

Core from 1
Start 10'



SAMPLE 17.05

SAMPLE 17.45

SAMPLE 17.85

SAMPLE 18.3

SAMPLE 18.65

12/11/2017

17.85

18.3

18.65

19.25

I-57 over Grinnell Road

SN 046-0010 / 0011

Hole #1 11-21-2017

Depth 19.5 FT to 25.0 FT

Box 2 of 2

Sample 2
19.5

Sample 2
Sample 3
20.0



12/11/2017

Grinnell Road under 1-57

SN 046-0010 / 0011

Hole # 3 11-22-2017

Depth 11 Ft to 21 Ft

Box 1 of 2

Bottom
Core Run #
11



12/11/2017

Grinnell Road under I-57

SN 046-0010 / 0011

Hole #3 11-22-2017

Depth 21 FT to 26 FT

Box 2 of 2



12/11/2017

Final Inspection Report of State Road Work



**Illinois Department
of Transportation**

Director of Highways
Department of Transportation
Springfield, Illinois

Contract No. 42818
FAI Route 57
Section 139VBR, 139HBR-3, 139BR-2
County Kankakee
F. A. Project IR-57-6(150)313

Contractor Azzarelli Const. Co.
P. O. Box 767
Address Kankakee, IL 60901
(City) (State)

C-93-004-88

Dear Sir:

On February 4, 1991 final inspection was made of work designated and same was found to be completed substantially in accordance with all of the requirements of the plans, specifications and contract. The improvement begins at Station 91+67.80 CL and ends at Station 145+01.86 CL Gross length 5534.00 ft. The work is located between (nearest town) Bradley and (nearest town) Kankakee on (marked route) FAI 57.

SUMMARY OF LENGTH BUILT

Nature of Improvement	Surface or Bridge		Net Length	Shoulders		Within corporate limits of	Station to Station
	Type	Width		Width	Type		
Section 139BR-2			76'-7"			91+67.80 CL to 92+45.24 CL	
Widened Bridge to 43'-2" & Replaced Deck (Both directions)						(STR # 046-0012, 046-0013)	
Section 139HBR-3			120'-2"			138+30.88 CL to 139+51.04 CL	
Widened Bridge to 43'-2" & Replaced Deck (Both Directions)						(STR # 046-0011, 046-0010)	
Section 139VBR			259'-8"			142+42.19 CL to 145+01.86 CL	
Widened Bridge to 43'-2" & Replaced Deck						(Both Directions)	
						(STR # 046-0009, 046-0008)	
Resurfaced approaches to all structures with bituminous overlay.							
Total							

* Describe nature of improvements as (1) PCC Pavement, (2) W&RS, (3) Resurfacing, (4) Bridge Widening, (5) Bridge Repairs, (6) Bridge Inew, (7) Pregrade. Omission and equations should be noted. Use above space for remarks or comments. If additional space is necessary use additional BC-71 Forms.

GENERAL INFORMATION

Date contract awarded 2-24-89 Construction began 4-3-89 Construction completed 2-1-91
Date pavement opened to traffic N/A Was work completed under traffic? Yes
Contract time limit 200 Working days used 200 Extension(s) N/A Liquidated damages (days) _____
Sub-contractors Ald-Cass Electric, Maintenance Coating, Interstate Landscaping, SSACC Inc., Certified Painting Co., Midwest Const. Services, Gateway Erectors
Resident Engineer and Inspectors J. Gromer, G. Sargent, R. Fortelka, T. Magolan, N. Love, C. Purcell, A. Sargent, W. Bott, E. Collins, Contractor's Superintendent Johnny Azzarelli
Contractor's performance: Excavating & Grading S; PCC Paving _____; Bituminous Paving S; Structures S; Drainage _____; Electrical S; Seal Coat _____; Miscellaneous S; EEO S
(Use E = Excellent; S = Satisfactory; P = Poor; U = Unacceptable)
Bonding company Firemen's Insurance Company of Newark, New Jersey
Final Inspection made by Ken Lang 2-4-91 Sal Deocampo 2-4-91
(State personnel) Date (FHWA Personnel) Date

Yours truly,

R. H. Blawie
District Engineer

JUL 19 1991

Date

Contract Price 2,418,095.76
Additions 242,385.16
Deductions 92,649.29
Total Cost 2,567,831.63

Passed _____

Final Inspection Date

Date



Piling Diagram Report

Structure No. 046-0010 NBL

Pier/Abutment No. NE ABUT. NBL
Plan Length 30 FT.

Pile Type Steel HP 10 x 42
Ordered Length 30 FT.

Required Bearing REFUSAL (84 TON)

Cutoff Elevation 305.39

Letter to Contractor 6-12-89

Hammer Data: Type VULCAN
Height of Fall 3'

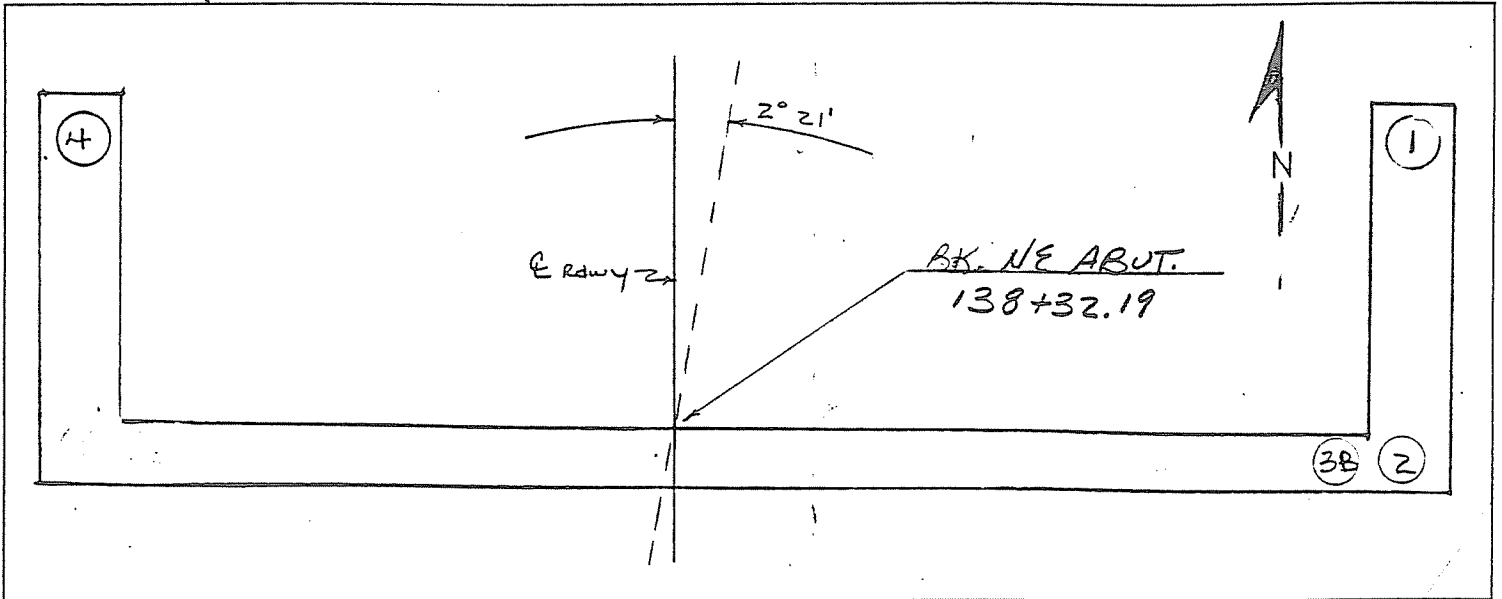
Ram Weight 5000#
Blows/min. 60

Cushion Material _____

Thickness _____

Formula: $P = \frac{2WH}{(S+1)}$

Batter Coefficient .97



Pile No.	Length Furn. Ft.	Length Del. Ft.	Length Cutoff Ft.	Length Driven Ft.	Final Bearing Tons	Pile No.	Length Furn. Ft.	Length Del. Ft.	Length Cutoff Ft.	Length Driven Ft.	Final Bearing Tons
1	30	30	5.1	24.9	98						
2	30	30.2	4.9	25.3	94						
3B	30	30	3.6	26.4	91						
4	30	30.2	5.0	25.2	88						
						TOTAL	120	120.4	18.6	101.8	







B indicates batter.

Pay Quantities

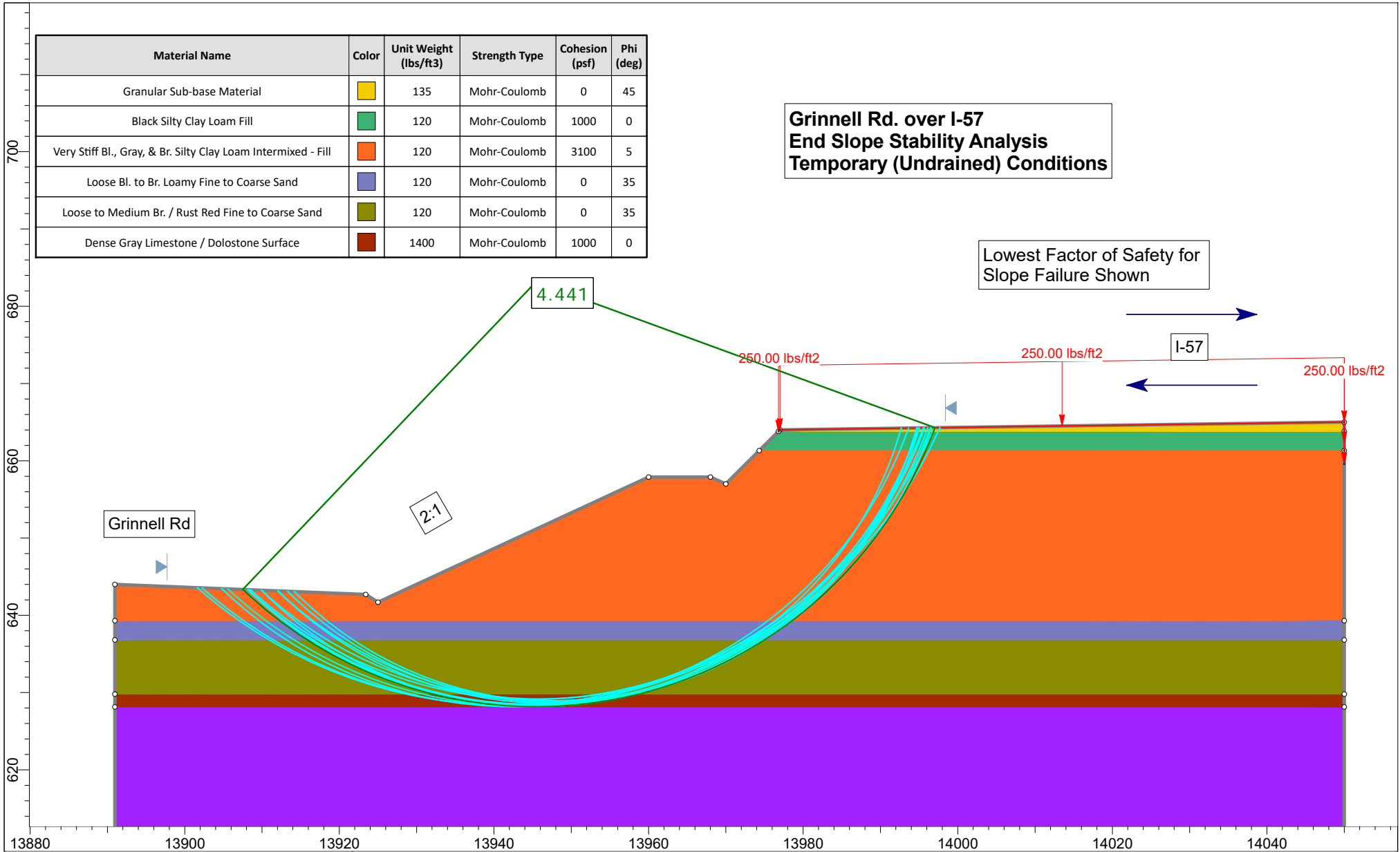
Remarks: _____

Initial(s) _____
Calculated By: GS
Checked By: JLG

Date 5-8-90
" _____
" _____

Material Name	Color	Unit Weight (lbs/ft3)	Strength Type	Cohesion (psf)	Phi (deg)
Granular Sub-base Material		135	Mohr-Coulomb	0	45
Black Silty Clay Loam Fill		120	Mohr-Coulomb	1000	0
Very Stiff Bl., Gray, & Br. Silty Clay Loam Intermixed - Fill		120	Mohr-Coulomb	3100	5
Loose Bl. to Br. Loamy Fine to Coarse Sand		120	Mohr-Coulomb	0	35
Loose to Medium Br. / Rust Red Fine to Coarse Sand		120	Mohr-Coulomb	0	35
Dense Gray Limestone / Dolostone Surface		1400	Mohr-Coulomb	1000	0

**Grinnell Rd. over I-57
End Slope Stability Analysis
Temporary (Undrained) Conditions**



<i>Project</i>			
Grinnell Rd. over I-57 Endslope Stability Analysis Temporary (Undrained) Conditions			
<i>Analysis Method</i>			
SLIDEINTERPRET 8.018 Bishop simplified			
<i>Drawn By</i>		<i>Scale</i>	
MEJ		1:206	
<i>Date</i>		<i>Company</i>	
11/15/2018		McCleary Engineering	
<i>File Name</i>			
Temporary Endslope Stability Analysis - I-57 over Grinnell Road.sldm			

USGS Design Maps Summary Report

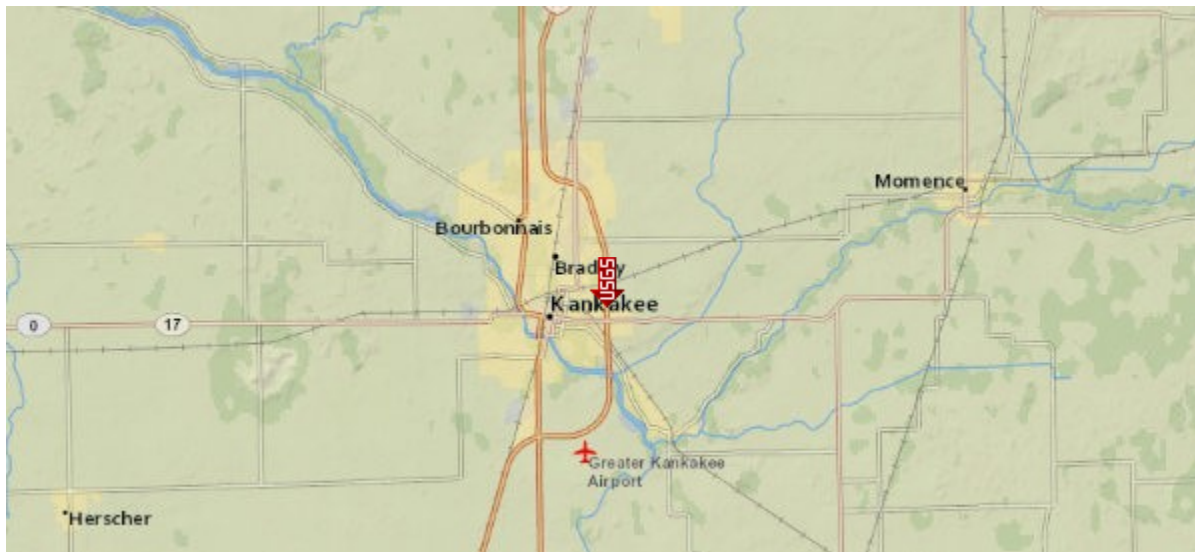
User-Specified Input

Report Title Seismic Report I-57 over Grinnell Rd. Kankakee
Sun November 18, 2018 02:04:46 UTC

Building Code Reference Document 2009 AASHTO Guide Specifications for LRFD Seismic Bridge Design
(which utilizes USGS hazard data available in 2002)

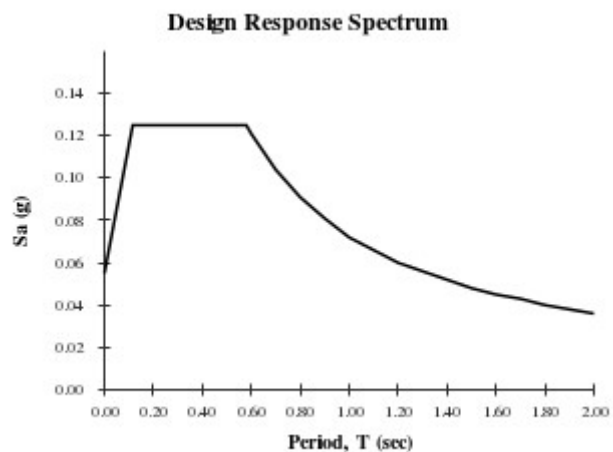
Site Coordinates 41.13322°N, 87.83636°W

Site Soil Classification Site Class C – “Very Dense Soil and Soft Rock”



USGS-Provided Output

PGA = 0.046 g	A_s = 0.055 g
S_s = 0.104 g	S_{DS} = 0.125 g
S₁ = 0.043 g	S_{D1} = 0.072 g



Although this information is a product of the U.S. Geological Survey, we provide no warranty, expressed or implied, as to the accuracy of the data contained therein. This tool is not a substitute for technical subject-matter knowledge.

PROJECT TITLE=====Grinnell Rd - This page is SB, west side. B-01 (Substructure 1) is SB North Abut / (Substructure 2 is SB Pier 1) / (Substructure 3 is SB Pier 2) / B-02 (Substructure 4) is SB South Abut-----

Substructure 1

Base of Substruct. Elev. (or ground surf for bents)	655.6	ft.
Pile or Shaft Dia.	12	inches
Boring Number	B-01 2018	
Top of Boring Elev.	660.19	ft.
Approximate Fixity Elev.	649.6	ft.

Individual Site Class Definition:

N (bar): 51 (Blows/ft.) Soil Site Class C
 N₆₀ (bar): 81 (Blows/ft.) Soil Site Class C <----Controls
 s_u (bar): 4.76 (ksf) Soil Site Class C

Seismic Soil Column	Bot. Of Sample	Sample	Layer		
			Thick.	N	Qu
Depth	Elevation	Thick.	N	Qu	Boundary
(ft)	(ft.)	(ft.)	(tsf)		
	657.7	2.50			B
	655.7	2.00	11	3.50	B
	653.2	2.50	5	2.00	
	650.7	2.50	9	3.50	
1.4	648.2	2.50	8	3.10	
3.9	645.7	2.50	9	3.70	
6.4	643.2	2.50	12	3.90	B
8.9	640.7	2.50	10	3.70	
11.4	638.2	2.50	67		
13.9	635.7	2.50	14	3.90	B
16.4	633.2	2.50	9		
17.4	632.2	1.00	21		B
18.0	631.6	0.58	660		
100.0	549.6	82.02	120	5.00	R

Substructure 2

Base of Substruct. Elev. (or ground surf for bents)	642.7	ft.
Pile or Shaft Dia.	18	inches
Boring Number	B-01, C-1	
Top of Boring Elev.	641.47	ft.
Approximate Fixity Elev.	633.7	ft.

Individual Site Class Definition:

N (bar): 92 (Blows/ft.) Soil Site Class C <----Controls
 N₆₀ (bar): 92 (Blows/ft.) Soil Site Class C
 s_u (bar): 5 (ksf) Soil Site Class C

Seismic Soil Column	Bot. Of Sample	Sample	Layer		
			Thick.	N	Qu
Depth	Elevation	Thick.	N	Qu	Boundary
(ft)	(ft.)	(ft.)	(tsf)		
	640.7	0.78	10	3.70	
	638.2	2.50	67		
	635.7	2.50	14	3.90	B
0.5	633.2	2.50	9		
1.5	632.2	1.00	21		B
2.1	631.6	0.58	660		
100.0	533.7	97.92	120	5.00	R

Substructure 3

Base of Substruct. Elev. (or ground surf for bents)	642.7	ft.
Pile or Shaft Dia.	18	inches
Boring Number	B-02, C-1	
Top of Boring Elev.	641.47	ft.
Approximate Fixity Elev.	633.7	ft.

Individual Site Class Definition:

N (bar): 64 (Blows/ft.) Soil Site Class C <----Controls
 N₆₀ (bar): 64 (Blows/ft.) Soil Site Class C
 s_u (bar): 5 (ksf) Soil Site Class C

Seismic Soil Column	Bot. Of Sample	Sample	Layer		
			Thick.	N	Qu
Depth	Elevation	Thick.	N	Qu	Boundary
(ft)	(ft.)	(ft.)	(tsf)		
	641.3	0.16	11	4.10	
	639.3	2.00	10	4.00	B
	636.8	2.50	7		
	634.3	2.50	9		
1.9	631.8	2.50	11		B
4.4	629.3	2.50	12		
6.1	627.8	1.67	600		
100.0	533.7	93.90	120	5.00	R

Substructure 4

Base of Substruct. Elev. (or ground surf for bents)	657.9	ft.
Pile or Shaft Dia.	12	inches
Boring Number	B-02 2018	
Top of Boring Elev.	663.81	ft.
Approximate Fixity Elev.	651.9	ft.

Individual Site Class Definition:

N (bar): 31 (Blows/ft.) Soil Site Class D
 N₆₀ (bar): 49 (Blows/ft.) Soil Site Class D <----Controls
 s_u (bar): 4.09 (ksf) Soil Site Class C

Seismic Soil Column	Bot. Of Sample	Sample	Layer		
			Thick.	N	Qu
Depth	Elevation	Thick.	N	Qu	Boundary
(ft)	(ft.)	(ft.)	(tsf)		
	661.3	2.50			
	658.8	2.50	6	2.50	
	656.3	2.50	7	3.00	
	653.8	2.50	7	2.50	
0.6	651.3	2.50	7	2.30	
3.1	648.8	2.50	8	3.10	
5.6	646.3	2.50	9	3.40	
8.1	643.8	2.50	9	3.10	B
10.6	641.3	2.50	11	4.10	
12.6	639.3	2.00	10	4.00	B
15.1	636.8	2.50	7		B
17.6	634.3	2.50	9		
20.1	631.8	2.50	11		
22.1	629.8	2.00	12		B
23.8	628.1	1.67	600		
100.0	551.9	76.23	120	5.00	R

Global Site Class Definition: Substructures 1 through 8

N (bar): 60 (Blows/ft.) Soil Site Class C
 N₆₀ (bar): 73 (Blows/ft.) Soil Site Class C <----Controls
 s_u (bar): 4.67 (ksf) Soil Site Class C

PROJECT TITLE===== **Grinnell Rd - This page is NB, east side. B-03 (Substructure 5) is NB South abut / (Substructure 6 is NB Pier 2) / (Substructure 7 is NB Pier 1) / B-04(Substructure 8) is NB N Abut**

Substructure 5

Base of Substruct. Elev. (or ground surf for bents)	657.9 ft.
Pile or Shaft Dia.	12 inches
Boring Number	B-03 2018
Top of Boring Elev.	664.04 ft.
Approximate Fixity Elev.	651.9 ft.

Individual Site Class Definition:

N (bar): 36 (Blows/ft.) Soil Site Class D
 N_{ch} (bar): 71 (Blows/ft.) Soil Site Class C <----Controls
 s_u (bar): 4.31 (ksf) Soil Site Class C

Seismic Soil Column Depth (ft)	Bot. Of Sample Elevation (ft)	Sample Thickness (ft)	Sample (tsf)		Layer Description Boundary
			N	Qu	
	661.5	2.50			
	659.5	2.00	15		B
	657.0	2.50	7	2.50	
	654.5	2.50	7	2.50	
	652.0	2.50	12	3.90	
2.4	649.5	2.50	11	3.70	
4.9	647.0	2.50	10	3.90	
7.4	644.5	2.50	11	3.70	B
9.9	642.0	2.50	12	4.10	
12.4	639.5	2.50	11	4.10	
14.9	637.0	2.50	11	4.00	
17.4	634.5	2.50	10	3.10	B
19.9	632.0	2.50	12		
21.9	630.0	2.00	15		
22.9	629.0	1.00	15		B
24.1	627.8	1.25	434		
100.0	551.9	75.90	120	5.00	R

Substructure 6

Base of Substruct. Elev. (or ground surf for bents)	642.7 ft.
Pile or Shaft Dia.	18 inches
Boring Number	B-03, C-3
Top of Boring Elev.	641.47 ft.
Approximate Fixity Elev.	633.7 ft.

Individual Site Class Definition:

N (bar): 78 (Blows/ft.) Soil Site Class C <----Controls
 N_{ch} (bar): 78 (Blows/ft.) Soil Site Class C
 s_u (bar): 5 (ksf) Soil Site Class C

Seismic Soil Column Depth (ft)	Bot. Of Sample Elevation (ft)	Sample Thickness (ft)	Sample (tsf)		Layer Description Boundary
			N	Qu	
	639.5	1.93	11	4.10	
	637.0	2.50	11	4.00	
	634.5	2.50	10	3.10	B
1.7	632.0	2.50	12		
3.7	630.0	2.00	15		
4.7	629.0	1.00	15		B
5.9	627.8	1.25	434		
100.0	533.7	94.10	120	5.00	R

Substructure 7

Base of Substruct. Elev. (or ground surf for bents)	642.7 ft.
Pile or Shaft Dia.	18 inches
Boring Number	B-04, C-3
Top of Boring Elev.	641.47 ft.
Approximate Fixity Elev.	633.7 ft.

Individual Site Class Definition:

N (bar): 85 (Blows/ft.) Soil Site Class C <----Controls
 N_{ch} (bar): 85 (Blows/ft.) Soil Site Class C
 s_u (bar): 5 (ksf) Soil Site Class C

Seismic Soil Column Depth (ft)	Bot. Of Sample Elevation (ft)	Sample Thickness (ft)	Sample (tsf)		Layer Description Boundary
			N	Qu	
	641.1	0.38	13	3.90	
	638.6	2.50	24	3.70	
	637.6	1.00	24	3.70	B
	635.6	2.00	11		
0.1	633.6	2.00	10		
2.1	631.6	2.00	11		B
3.4	630.3	1.25	400		
100.0	533.7	96.60	120	5.00	R

Substructure 8

Base of Substruct. Elev. (or ground surf for bents)	655.6 ft.
Pile or Shaft Dia.	12 inches
Boring Number	B-04 2018
Top of Boring Elev.	660.59 ft.
Approximate Fixity Elev.	649.6 ft.

Individual Site Class Definition:

N (bar): 42 (Blows/ft.) Soil Site Class D
 N_{ch} (bar): 64 (Blows/ft.) Soil Site Class C <----Controls
 s_u (bar): 4.09 (ksf) Soil Site Class C

Seismic Soil Column Depth (ft)	Bot. Of Sample Elevation (ft)	Sample Thickness (ft)	Sample (tsf)		Layer Description Boundary
			N	Qu	
	658.1	2.50			
	655.6	2.50	6	1.80	
	653.1	2.50	5	2.00	
	650.6	2.50	3	1.50	
1.0	648.6	2.00	3	1.50	B
3.5	646.1	2.50	9	2.90	
6.0	643.6	2.50	11	3.20	
8.5	641.1	2.50	13	3.50	
11.0	638.6	2.50	24	3.70	
12.0	637.6	1.00	24	3.70	B
14.0	635.6	2.00	11		
16.0	633.6	2.00	10		
18.0	631.6	2.00	11		B
19.3	630.3	1.25	400		
100.0	549.6	80.70	120	5.00	R

From: Michael Haley <mhaley@lineng.com>

Sent: Monday, July 30, 2018 2:35:09 PM

To: Ferguson, Steven P

Cc: Fred Lin

Subject: [External] RE: New work order

Steve,

Below are the preliminary loads for developing the Grinnell Road SGR.

- Strength I
 - Abutments – 1538 kips
 - Piers – 4832 kips
- Service I
 - Abutments – 1126 kips
 - Piers – 3680 kips

Our preliminary bridge layout is in line with the attached Structure Sketch from the BCR. Let me know if you need any more information at this time.

Thanks.

Mike Haley
Lin Engineering, Ltd.

From: Ferguson, Steven P [<mailto:Steven.Ferguson@illinois.gov>]

Sent: Tuesday, May 01, 2018 9:04 AM

To: Michael Haley

GENERAL DATA

STRUCTURE NUMBER===== NB structure
 STRUCTURE TYPE ===== MULTI-SPAN
 STRUCTURE SKEW===== 0 DEGREES
 SUPER. DATA IN REFERENCE TO SUB. DATA ===== ABUT 2

TOTAL STRUCTURE LENGTH===== 159.25 FT
 NUMBER OF SPANS ===== 3
 END SPAN LENGTH ===== 44.75 FT
 ADJACENT INTERIOR SPAN LENGTH ===== 69.75 FT

SUPERSTRUCTURE DATA (END OR MAIN SPAN)	
BEAM TYPE	CONCRETE BEAM
CONCRETE BEAM	36" PPC I-BEAM
BEAM F'C	7 KSI
BEAM SPACING PERP. TO CL	7.00 FT
SLAB THICKNESS	8.00 IN
SLAB F'C	4.00 KSI

SUPERSTRUCTURE DATA (ADJACENT SPAN)	
CONCRETE BEAM	36" PPC I-BEAM
BEAM F'C	7 KSI
BEAM SPACING PERP. TO CL	7.00 FT
SLAB THICKNESS	8.00 IN
SLAB F'C	4.00 KSI

ABUTMENT #1 DATA	
ABUTMENT NAME	NB south abut
ABUTMENT REFERENCE BORING	B-3
BOTTOM OF ABUTMENT ELEVATION	657.96 FT
ESTIMATED NUMBER OF PILES AT ABUT.	7
PILE SPACING PERP. TO CL	7.33 FT

ABUTMENT #2 DATA	
ABUTMENT NAME	NB north abut
ABUTMENT REFERENCE BORING	B-4
BOTTOM OF ABUTMENT ELEVATION	655.52 FT
ESTIMATED NUMBER OF PILES AT ABUT.	7
PILE SPACING PERP. TO CL	7.33 FT

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #1				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
657.56	0.40	2.5		
655.06	2.50	2.5		
652.56	2.50	3.9		
650.06	2.50	3.7		
647.96	2.10	3.9		

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #2				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
655.02	0.50	1.8		
652.52	2.50	2.0		
650.02	2.50	1.5		
647.52	2.50	1.50		
645.52	2.00	2.90		

10.00 FT = TOTAL DEPTH ENTERED

10.00 FT = TOTAL DEPTH ENTERED

WEIGHTED AVERAGE Qu FOR ABUTMENT #1===== 3.44 TSF

WEIGHTED AVERAGE Qu FOR ABUTMENT #2===== 1.92 TSF

PILE STIFFNESS MODIFIER FOR ABUTMENT #1
 = 1/(1.45-[0.3*3.44])===== 2.40

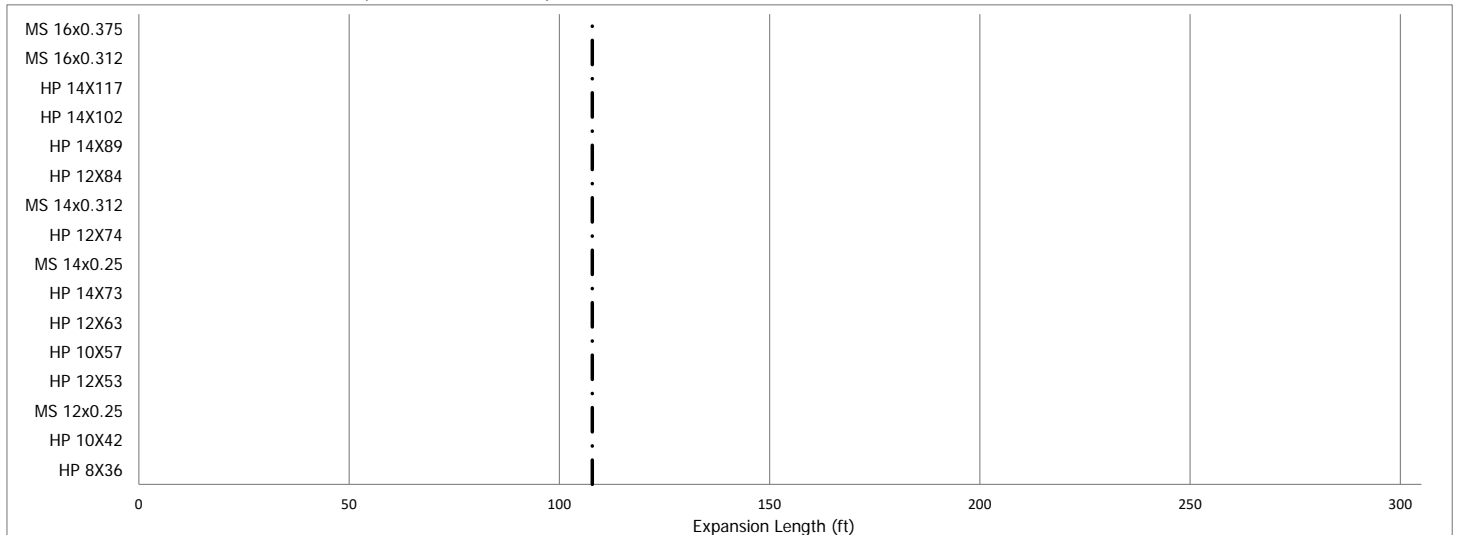
PILE STIFFNESS MODIFIER FOR ABUTMENT #2
 = 1/(1.45-[0.3*1.92])===== 1.14

WEIGHTED AVG. Qu > 3.0 TSF WITH TRIB. LENGTH > 20%, INTEGRAL ABUTMENT STRUCTURE NOT ALLOWED

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #1 = [2.4*7*0+1.14*7*159.25]/[2.4*7+1.14*7]===== 51.42 FT

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #2 = [1.14*7*0+2.4*7*159.25]/[1.14*7+2.4*7]===== 107.83 FT

ABUT 2 (NB north abut) - EXPANSION LENGTH LIMIT CHART - 0 DEG. SKEW



--- = Estimated expansion length for the indicated abutment. Piles with an expansion length greater than this are suitable for consideration. (Note: The same size pile should be used at both abutments.)

GENERAL DATA

STRUCTURE NUMBER===== SB structure
 STRUCTURE TYPE ===== MULTI-SPAN
 STRUCTURE SKEW===== 0 DEGREES
 SUPER. DATA IN REFERENCE TO SUB. DATA ===== ABUT 1

TOTAL STRUCTURE LENGTH===== 159.25 FT
 NUMBER OF SPANS ===== 3
 END SPAN LENGTH ===== 44.75 FT
 ADJACENT INTERIOR SPAN LENGTH ===== 69.75 FT

SUPERSTRUCTURE DATA (END OR MAIN SPAN)	
BEAM TYPE	CONCRETE BEAM
CONCRETE BEAM	36" PPC I-BEAM
BEAM F'C	7 KSI
BEAM SPACING PERP. TO CL	7.00 FT
SLAB THICKNESS	8.00 IN
SLAB F'C	4.00 KSI

SUPERSTRUCTURE DATA (ADJACENT SPAN)	
CONCRETE BEAM	36" PPC I-BEAM
BEAM F'C	7 KSI
BEAM SPACING PERP. TO CL	7.00 FT
SLAB THICKNESS	8.00 IN
SLAB F'C	4.00 KSI

ABUTMENT #1 DATA	
ABUTMENT NAME	SB north abut
ABUTMENT REFERENCE BORING	B-1
BOTTOM OF ABUTMENT ELEVATION	655.52 FT
ESTIMATED NUMBER OF PILES AT ABUT.	6
PILE SPACING PERP. TO CL	7.33 FT

ABUTMENT #2 DATA	
ABUTMENT NAME	SB south abut
ABUTMENT REFERENCE BORING	B-2
BOTTOM OF ABUTMENT ELEVATION	657.96 FT
ESTIMATED NUMBER OF PILES AT ABUT.	6
PILE SPACING PERP. TO CL	7.33 FT

ENTER ONLY Qu VALUE IF AVAILABLE, OTHERWISE ENTER N VALUE

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #1				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
653.12	2.40	3.5		
650.62	2.50	2.0		
648.12	2.50	3.5		
645.62	2.50	3.1		
645.52	0.10	3.7	9	2.3

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #2				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
657.36	0.60	3.0		
654.86	2.50	2.5		
652.36	2.50	2.3		
649.86	2.50	3.10		
647.96	1.90	3.40		

10.00 FT = TOTAL DEPTH ENTERED

10.00 FT = TOTAL DEPTH ENTERED

WEIGHTED AVERAGE Qu FOR ABUTMENT #1===== 3.03 TSF

WEIGHTED AVERAGE Qu FOR ABUTMENT #2===== 2.80 TSF

PILE STIFFNESS MODIFIER FOR ABUTMENT #1 = 1/(1.45-[0.3*3.03])===== 1.85

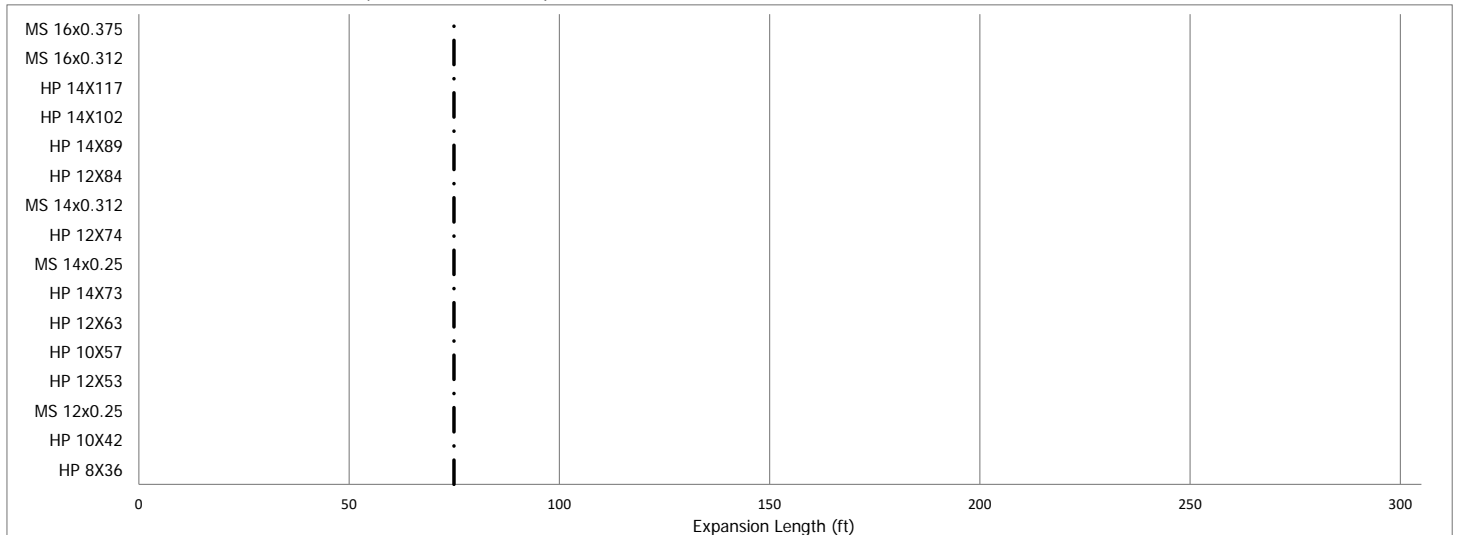
PILE STIFFNESS MODIFIER FOR ABUTMENT #2 = 1/(1.45-[0.3*2.8])===== 1.64

WEIGHTED AVG. Qu > 3.0 TSF WITH TRIB. LENGTH > 20%, INTEGRAL ABUTMENT STRUCTURE NOT ALLOWED

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #1 = [1.85*6*0+1.64*6*159.25]/[1.85*6+1.64*6]===== 74.94 FT

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #2 = [1.64*6*0+1.85*6*159.25]/[1.64*6+1.85*6]===== 84.31 FT

ABUT 1 (SB north abut) - EXPANSION LENGTH LIMIT CHART - 0 DEG. SKEW



--- = Estimated expansion length for the indicated abutment. Piles with an expansion length greater than this are suitable for consideration. (Note: The same size pile should be used at both abutments.)

GENERAL DATA

STRUCTURE NUMBER===== NB structure w/ 10' precure, bentonite
 STRUCTURE TYPE ===== MULTI-SPAN
 STRUCTURE SKEW===== 0 DEGREES
 SUPER. DATA IN REFERENCE TO SUB. DATA ===== ABUT 2

TOTAL STRUCTURE LENGTH===== 159.25 FT
 NUMBER OF SPANS ===== 3
 END SPAN LENGTH ===== 44.75 FT
 ADJACENT INTERIOR SPAN LENGTH ===== 69.75 FT

SUPERSTRUCTURE DATA (END OR MAIN SPAN)	
BEAM TYPE	CONCRETE BEAM
CONCRETE BEAM	36" PPC I-BEAM
BEAM F'C	7 KSI
BEAM SPACING PERP. TO CL	7.00 FT
SLAB THICKNESS	8.00 IN
SLAB F'C	4.00 KSI

SUPERSTRUCTURE DATA (ADJACENT SPAN)	
CONCRETE BEAM	36" PPC I-BEAM
BEAM F'C	7 KSI
BEAM SPACING PERP. TO CL	7.00 FT
SLAB THICKNESS	8.00 IN
SLAB F'C	4.00 KSI

ABUTMENT #1 DATA	
ABUTMENT NAME	NB south abut
ABUTMENT REFERENCE BORING	B-3
BOTTOM OF ABUTMENT ELEVATION	657.96 FT
ESTIMATED NUMBER OF PILES AT ABUT.	7
PILE SPACING PERP. TO CL	7.33 FT

ABUTMENT #2 DATA	
ABUTMENT NAME	NB north abut
ABUTMENT REFERENCE BORING	B-4
BOTTOM OF ABUTMENT ELEVATION	655.52 FT
ESTIMATED NUMBER OF PILES AT ABUT.	7
PILE SPACING PERP. TO CL	7.33 FT

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #1				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
657.56	0.40	0.1		
655.06	2.50	0.1		
652.56	2.50	0.1		
650.06	2.50	0.1		
647.96	2.10	0.1		

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #2				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
655.02	0.50	0.1		
652.52	2.50	0.1		
650.02	2.50	0.1		
647.52	2.50	0.10		
645.52	2.00	0.10		

10.00 FT = TOTAL DEPTH ENTERED

10.00 FT = TOTAL DEPTH ENTERED

WEIGHTED AVERAGE Qu FOR ABUTMENT #1===== 0.10 TSF

WEIGHTED AVERAGE Qu FOR ABUTMENT #2===== 0.10 TSF

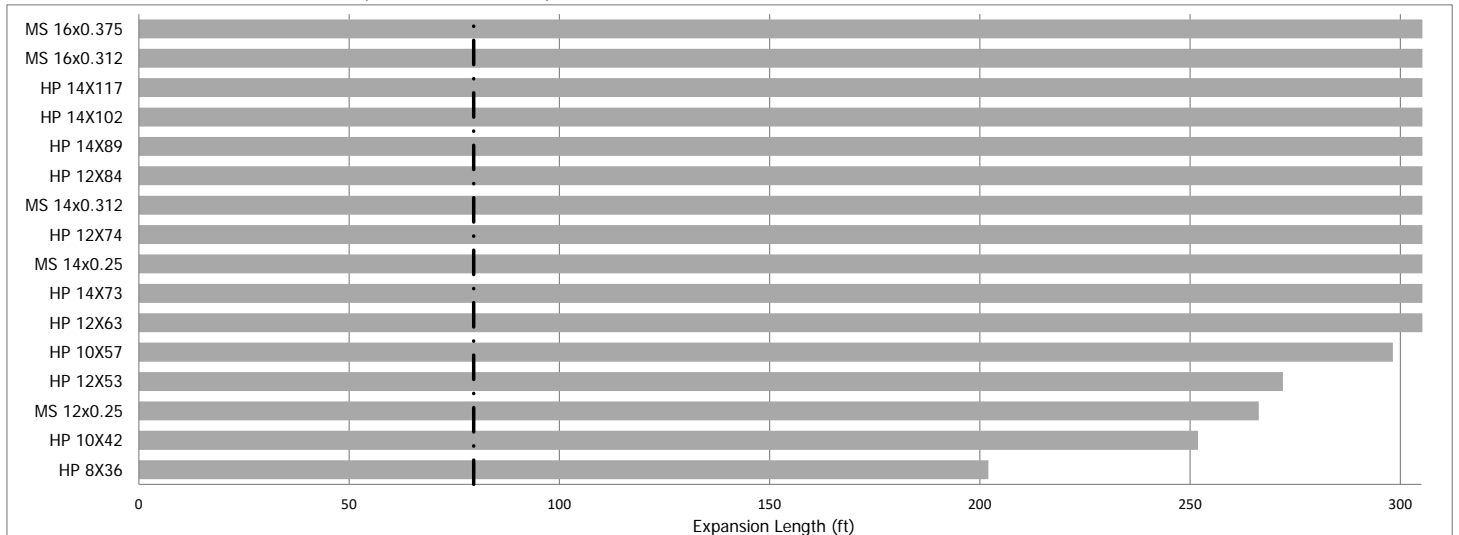
PILE STIFFNESS MODIFIER FOR ABUTMENT #1
 = 1/(1.45-[0.3*0.1])===== 0.70

PILE STIFFNESS MODIFIER FOR ABUTMENT #2
 = 1/(1.45-[0.3*0.1])===== 0.70

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #1 = $[0.7*7*0+0.7*7*159.25]/[0.7*7+0.7*7]$ ===== 79.63 FT

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #2 = $[0.7*7*0+0.7*7*159.25]/[0.7*7+0.7*7]$ ===== 79.63 FT

ABUT 2 (NB north abut) - EXPANSION LENGTH LIMIT CHART - 0 DEG. SKEW



----- = Estimated expansion length for the indicated abutment. Piles with an expansion length greater than this are suitable for consideration.
 (Note: The same size pile should be used at both abutments.)

GENERAL DATA

STRUCTURE NUMBER===== SB structure w/ 10' precure, bentonite
 STRUCTURE TYPE ===== MULTI-SPAN
 STRUCTURE SKEW===== 0 DEGREES
 SUPER. DATA IN REFERENCE TO SUB. DATA ===== ABUT 1

TOTAL STRUCTURE LENGTH===== 159.25 FT
 NUMBER OF SPANS ===== 3
 END SPAN LENGTH ===== 44.75 FT
 ADJACENT INTERIOR SPAN LENGTH ===== 69.75 FT

SUPERSTRUCTURE DATA (END OR MAIN SPAN)	
BEAM TYPE	CONCRETE BEAM
CONCRETE BEAM	36" PPC I-BEAM
BEAM F'C	7 KSI
BEAM SPACING PERP. TO CL	7.00 FT
SLAB THICKNESS	8.00 IN
SLAB F'C	4.00 KSI

SUPERSTRUCTURE DATA (ADJACENT SPAN)	
CONCRETE BEAM	36" PPC I-BEAM
BEAM F'C	7 KSI
BEAM SPACING PERP. TO CL	7.00 FT
SLAB THICKNESS	8.00 IN
SLAB F'C	4.00 KSI

ABUTMENT #1 DATA	
ABUTMENT NAME	SB north abut
ABUTMENT REFERENCE BORING	B-1
BOTTOM OF ABUTMENT ELEVATION	655.52 FT
ESTIMATED NUMBER OF PILES AT ABUT.	6
PILE SPACING PERP. TO CL	7.33 FT

ABUTMENT #2 DATA	
ABUTMENT NAME	SB south abut
ABUTMENT REFERENCE BORING	B-2
BOTTOM OF ABUTMENT ELEVATION	657.96 FT
ESTIMATED NUMBER OF PILES AT ABUT.	6
PILE SPACING PERP. TO CL	7.33 FT

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #1				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
653.12	2.40	0.1		
650.62	2.50	0.1		
648.12	2.50	0.1		
645.62	2.50	0.1		
645.52	0.10	0.1		

SOIL DATA FOR 10 FT BENEATH BOTTOM OF ABUTMENT #2				
BOT. OF LAYER ELEV. (FT)	LAYER THICKNESS (FT)	UNCONFINED COMPRESSIVE STRENGTH (TSF)	N S.P.T. VALUE (BLOWS/12 IN.)	Qu EQUIV. FOR N VALUE (TSF)
657.36	0.60	0.1		
654.86	2.50	0.1		
652.36	2.50	0.1		
649.86	2.50	0.10		
647.96	1.90	0.10		

10.00 FT = TOTAL DEPTH ENTERED

10.00 FT = TOTAL DEPTH ENTERED

WEIGHTED AVERAGE Qu FOR ABUTMENT #1===== 0.10 TSF

WEIGHTED AVERAGE Qu FOR ABUTMENT #2===== 0.10 TSF

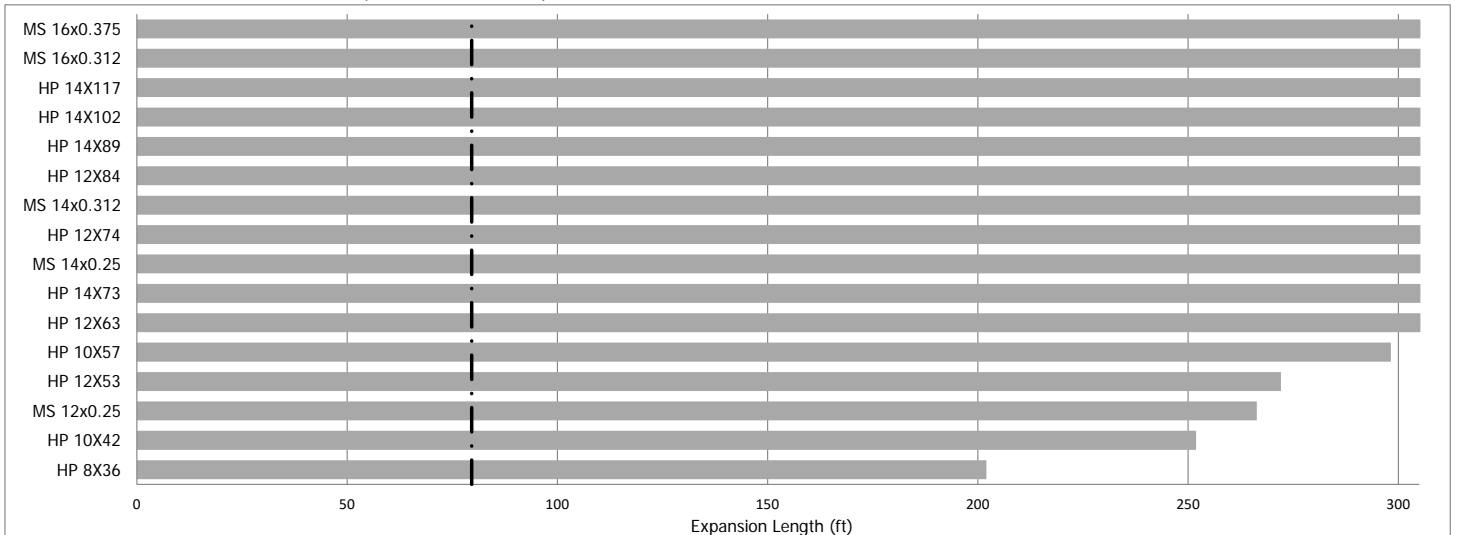
PILE STIFFNESS MODIFIER FOR ABUTMENT #1
 = 1/(1.45-[0.3*0.1])===== 0.70

PILE STIFFNESS MODIFIER FOR ABUTMENT #2
 = 1/(1.45-[0.3*0.1])===== 0.70

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #1 = $[0.7*6*0+0.7*6*159.25]/[0.7*6+0.7*6]$ ===== 79.63 FT

DISTANCE TO CENTROID OF STIFFNESS FROM ABUTMENT #2 = $[0.7*6*0+0.7*6*159.25]/[0.7*6+0.7*6]$ ===== 79.63 FT

ABUT 1 (SB north abut) - EXPANSION LENGTH LIMIT CHART - 0 DEG. SKEW



----- = Estimated expansion length for the indicated abutment. Piles with an expansion length greater than this are suitable for consideration.
 (Note: The same size pile should be used at both abutments.)

Table 1: PILE LENGTH TABLES USING SOIL DATA for NB SN046-0158 N & S Abutments

North Abutment, Using Boring B-04			South Abutment, Using Boring B-03		
Nominal Required Bearing (KIPS)	Factored Resistance Available (KIPS)	Estimated Pile Length (Ft.)	Nominal Required Bearing (KIPS)	Factored Resistance Available (KIPS)	Estimated Pile Length (Ft.)
HP 10x42			HP 10x42		
193	106	27	175	96	31
314	173	28	265	146	32
*335	184	29	*335	184	33
HP 12x53			HP 12x53		
232	127	27	212	117	31
376	207	28	318	175	32
*418	230	29	*418	230	33
HP 12x63			HP 12x63		
240	132	27	327	180	32
386	212	28	474	260	33
*497	273	29	*497	273	34
HP 14x73			HP 14x73		
284	156	27	387	213	32
457	252	28	561	308	33
*578	318	29	*578	318	34
HP 14x89			HP 14x89		
469	258	28	398	219	32
644	354	29	573	315	33
*705	388	30	*705	388	34

* Maximum nominal required bearing at refusal

Table 1: PILE LENGTH TABLES USING SOIL DATA for SB SN046-0159 N & S Abutments

North Abutment, Using Boring B-01			South Abutment, Using Boring B-02		
Nominal Required Bearing (KIPS)	Factored Resistance Available (KIPS)	Estimated Pile Length (Ft.)	Nominal Required Bearing (KIPS)	Factored Resistance Available (KIPS)	Estimated Pile Length (Ft.)
HP 10x42			HP 10x42		
86	47	25	70	39	26
225	124	26	73	40	28
*335	184	27	*335	87	30
HP 12x53			HP 12x53		
103	57	25	93	51	28
276	152	26	192	106	30
*418	230	27	*418	230	32
HP 12x63			HP 12x63		
335	184	26	212	117	30
482	265	27	437	241	32
*497	273	28	*497	273	33
HP 14x73			HP 14x73		
397	218	26	249	137	30
570	314	27	518	285	32
*578	318	28	*578	318	33
HP 14x89			HP 14x89		
408	224	26	279	154	30
583	321	27	530	291	32
*705	388	28	*705	338	33

* Maximum nominal required bearing at refusal

SUBSTRUCTURE===== north abut NB SN046-0158
 REFERENCE BORING ===== 4
 LRFD or ASD or SEISMIC ===== LRFD
 PILE CUTOFF ELEV. ===== 657.60 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 655.60 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== None
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== 424.00 ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== 434.00 ft

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
335 KIPS	335 KIPS	184 KIPS	29 FT.

TOTAL FACTORED SUBSTRUCTURE LOAD ===== 1538 kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 51.20 ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 1
 Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 240.31 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 90.12 KIPS

PILE TYPE AND SIZE ===== Steel HP 10 X 42

Plugged Pile Perimeter===== 3.300 FT. Unplugged Pile Perimeter===== 4.858 FT.
 Plugged Pile End Bearing Area===== 0.680 SQFT. Unplugged Pile End Bearing Area===== 0.086 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL PLUGGED			NOMINAL UNPLUG'D			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)	SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
653.10	2.50	0.00	0		0.0	0.0	0.0	0.0	0.0	0.0	0	0	0	0	5
650.60	2.50	0.00	0		0.0	0.0	0.0	0.0	0.0	0.0	0	0	0	0	7
648.60	2.00	0.00	0		0.0	0.0	0.0	0.0	0.0	0.0	0	0	0	0	9
646.10	2.50	0.00	0		0.0	0.0	0.0	0.0	0.0	0.0	0	0	0	0	12
645.60	0.50	0.00	0		0.0	0.0	30.5	0.0	0.0	3.9	4	0	0	2	12
643.60	2.00	3.20	11		10.6	30.5	44.0	15.6	3.9	19.8	20	0	0	11	14
641.10	2.50	3.50	13		14.1	33.4	60.0	20.8	4.2	40.8	41	0	0	22	17
638.60	2.50	3.70	24		14.7	35.3	74.7	21.7	4.5	62.5	63	0	0	34	19
637.60	1.00	3.70	24		5.9	35.3	64.0	8.7	4.5	69.1	64	0	0	35	20
635.60	2.00		11	Medium Sand	1.3	18.6	63.6	1.9	2.4	70.8	64	0	0	35	22
633.60	2.00		10	Medium Sand	1.2	17.0	66.5	1.8	2.1	72.8	67	0	0	37	24
631.60	2.00		11	Medium Sand	1.3	18.6	388.2	1.9	2.4	115.3	115	0	0	63	26
630.35	1.25		200	Sandy Gravel	67.4	339.0	286.1	99.3	42.9	193.2	193	0	0	106	27
629.35	1.00			Limestone	82.2	169.5	368.4	121.0	21.5	314.2	314	0	0	173	28.3
628.35	1.00			Limestone	82.2	169.5	450.6	121.0	21.5	435.2	435	0	0	299	29.3
627.35	1.00			Limestone	82.2	169.5	532.8	121.0	21.5	556.3	533	0	0	293	30.3
626.35	1.00			Limestone		169.5			21.5						

Pile Design Table for north abut NB SN046-0158 utilizing Boring #4

Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)
			Steel HP 10 X 42			Steel HP 12 X 84		
			115	63	26	88	49	24
			193	106	27	174	96	26
			335	184	29	253	139	27
			Steel HP 10 X 57			664	365	30
			131	72	26	Steel HP 14 X 73		
			202	111	27	105	58	24
			454	250	30	178	98	26
			Steel HP 12 X 53			284	156	27
			140	77	26	578	318	29
			232	127	27	Steel HP 14 X 89		
			418	230	29	107	59	24
			Steel HP 12 X 63			195	107	26
			151	83	26	294	162	27
			240	132	27	705	388	30
			497	273	29	Steel HP 14 X 102		
			Steel HP 12 X 74			108	59	24
			164	90	26	209	115	26
			247	136	27	301	166	27
			589	324	30	810	445	30
						Steel HP 14 X 117		
						110	60	24
						225	124	26
						311	171	27
						Precast 14"x 14"		
						143	78	19
						195	107	20
						195	108	22
						213	117	24
Steel HP 8 X 36								
253	139	28						

SUBSTRUCTURE===== south abut. NB SN 046-0158
 REFERENCE BORING ===== 3
 LRFD or ASD or SEISMIC ===== LRFD
 PILE CUTOFF ELEV. ===== 659.90 ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = 657.90 ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== None
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== 424.00 ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== 434.00 ft

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of Pile	Maximum Nominal Req'd Bearing of Boring	Maximum Factored Resistance Available in Boring	Maximum Pile Driveable Length in Boring
705 KIPS	705 KIPS	388 KIPS	34 FT.

TOTAL FACTORED SUBSTRUCTURE LOAD ===== 1538 kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== 51.20 ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== 1
 Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 240.31 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 90.12 KIPS

PILE TYPE AND SIZE ===== **Steel HP 14 X 89**

Plugged Pile Perimeter===== 4.750 FT. Unplugged Pile Perimeter===== 7.033 FT.
 Plugged Pile End Bearing Area===== 1.409 SQFT. Unplugged Pile End Bearing Area===== 0.181 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF.)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL PLUGGED			NOMINAL UNPLUG'D			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)	SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
657.04	0.86	0.00	0		0.0	0.0	0.0	0.0	0.0	0.0	0	0	0	0	3
654.54	2.50	0.00	0		0.0	0.0	0.0	0.0	0.0	0.0	0	0	0	0	5
652.04	2.50	0.00	0		0.0	0.0	0.0	0.0	0.0	0.0	0	0	0	0	8
649.54	2.50	0.00	0		0.0	0.0	0.0	0.0	0.0	0.0	0	0	0	0	10
647.90	1.64	0.00	0		0.0	0.0	77.0	0.0	0.0	9.9	10	0	0	5	12
647.04	0.86	3.90	10		7.6	77.0	80.6	11.2	9.9	20.6	21	0	0	11	13
644.54	2.50	3.70	11		21.2	73.0	109.7	31.4	9.4	53.1	53	0	0	29	15
642.04	2.50	4.10	12		22.9	80.9	132.7	34.0	10.4	87.0	87	0	0	48	18
639.54	2.50	4.10	11		22.9	80.9	153.7	34.0	10.4	120.8	121	0	0	66	20
637.04	2.50	4.00	11		22.5	79.0	158.4	33.3	10.2	151.8	152	0	0	84	23
634.54	2.50	3.10	10		18.6	61.2	157.9	27.5	7.9	176.9	158	0	0	87	25
632.04	2.50		12	Medium Sand	2.6	42.1	171.1	3.8	5.4	182.1	171	0	0	94	28
630.04	2.00		15	Medium Sand	2.6	52.6	173.7	3.8	6.8	185.9	174	0	0	96	30
629.04	1.00		15	Medium Sand	1.3	52.6	943.6	1.9	6.8	286.8	287	0	0	158	31
627.79	1.25		234	Sandy Gravel	115.9	821.3	589.2	171.7	105.7	397.9	398	0	0	219	32
626.79	1.00			Limestone	118.3	351.0	707.6	175.2	45.2	573.2	573	0	0	315	33.1
625.79	1.00			Limestone	118.3	351.0	825.9	175.2	45.2	748.4	748	0	0	442	34.4
624.79	1.00			Limestone	118.3	351.0	944.3	175.2	45.2	923.6	924	0	0	508	35.4
623.79	1.00			Limestone	118.3	351.0	1062.6	175.2	45.2	1098.9	1063	0	0	584	36.4
622.79	1.00			Limestone	118.3	351.0	1180.9	175.2	45.2	1274.1	1184	0	0	660	37.4
621.79	1.00			Limestone		351.0			45.2						

Pile Design Table for south abut. NB SN 046-0158 utilizing Boring #3

Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)
			Steel HP 10 X 42			Steel HP 12 X 84		
			109	60	30	144	79	30
			175	96	31	253	139	31
			265	146	32	341	187	32
			335	184	33	664	365	35
			Steel HP 10 X 57			Steel HP 14 X 73		
			112	62	30	156	86	25
			194	107	31	169	93	28
			274	151	32	171	94	30
			454	250	34	266	146	31
			Steel HP 12 X 53			Steel HP 14 X 89		
			138	76	30	387	213	32
			212	117	31	578	318	34
			318	175	32			
			418	230	33			
			Steel HP 12 X 63			Steel HP 14 X 102		
			139	77	30	160	88	25
			226	124	31	173	95	28
			327	180	32	176	97	30
			497	273	34	303	167	31
			Steel HP 12 X 74			Steel HP 14 X 117		
			141	78	30	406	223	32
			240	132	31	810	445	35
			334	184	32			
			589	324	34			
			Steel HP 8 X 36			Precast 14"x 14"		
			143	79	31	141	77	18
			214	117	32	175	96	20
			286	157	33	196	108	23

SUBSTRUCTURE===== **North Abut SB SN 046-0159**
 REFERENCE BORING ===== **1**
 LRFD or ASD or SEISMIC ===== **LRFD**
 PILE CUTOFF ELEV. ===== **657.60** ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = **655.60** ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== **None**
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== **424.00** ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== **434.00** ft

TOTAL FACTORED SUBSTRUCTURE LOAD ===== **1538** kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== **51.20** ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== **1**
 Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 240.31 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 90.12 KIPS

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of <u>Pile</u>	Maximum Nominal Req'd Bearing of <u>Boring</u>	Maximum Factored Resistance Available in <u>Boring</u>	Maximum Pile Driveable Length in <u>Boring</u>
705 KIPS	705 KIPS	388 KIPS	28 FT.

PILE TYPE AND SIZE ===== **Steel HP 14 X 89**
 Plugged Pile Perimeter===== 4.750 FT. Unplugged Pile Perimeter===== 7.033 FT.
 Plugged Pile End Bearing Area===== 1.409 SQFT. Unplugged Pile End Bearing Area===== 0.181 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL PLUGGED			NOMINAL UNPLUG'D			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)	SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
653.10	2.50	0.00	0		0.0	0.0	0.0	0.0	0.0	0.0	0	0	0	5	
650.60	2.50	0.00	0		0.0	0.0	0.0	0.0	0.0	0.0	0	0	0	7	
648.10	2.50	0.00	0		0.0	0.0	0.0	0.0	0.0	0.0	0	0	0	10	
645.60	2.50	0.00	0		0.0	0.0	77.0	0.0	0.0	9.9	10	0	0	5	
643.10	2.50	3.90	12		22.1	77.0	95.1	32.7	9.9	42.1	42	0	0	23	
640.60	2.50	3.70	10		21.2	73.0	219.7	31.4	9.4	86.8	87	0	0	48	
638.10	2.50		67	Hard Till	12.3	176.4	132.6	18.2	22.7	92.2	92	0	0	51	
635.60	2.50	3.90	14		22.1	77.0	109.2	32.7	9.9	119.0	109	0	0	60	
633.10	2.50		9	Medium Sand	1.9	31.6	153.3	2.9	4.1	127.3	127	0	0	70	
632.10	1.00		21	Medium Sand	1.8	73.7	2397.9	2.7	9.5	418.7	419	0	0	230	
631.52	0.58		660	Sandy Gravel	163.4	2316.5	595.8	242.0	298.1	407.7	408	0	0	224	
630.52	1.00			Limestone	118.3	351.0	714.2	175.2	45.2	583.0	583	0	0	321	
629.52	1.00			Limestone	118.3	351.0	832.5	175.2	45.2	758.2	758	0	0	447	
628.52	1.00			Limestone	118.3	351.0	950.9	175.2	45.2	933.4	933	0	0	543	
627.52	1.00			Limestone	118.3	351.0	1069.2	175.2	45.2	1108.6	1069	0	0	588	
626.52	1.00			Limestone		351.0			45.2					30.4	

Pile Design Table for North Abut SB SN 046-0159 utilizing Boring #1

Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)
			Steel HP 10 X 42			Steel HP 12 X 84		
			86	47	25	108	60	25
			225	124	26	349	192	26
			272	150	26	664	365	29
			335	184	27	Steel HP 14 X 73		
			Steel HP 10 X 57			125	69	25
			88	48	25	364	200	26
			276	152	26	397	218	26
			281	154	26	578	318	28
			454	250	28	Steel HP 14 X 89		
			Steel HP 12 X 53			127	70	25
			103	57	25	408	224	26
			276	152	26	705	388	28
			326	179	26	Steel HP 14 X 102		
			418	230	27	129	71	25
Steel HP 12 X 63			416	229	26			
105	58	25	810	445	29			
311	171	26	Steel HP 14 X 117					
335	184	26	132	72	25			
497	273	28	426	235	26			
Steel HP 12 X 74			Precast 14"x 14"					
107	59	25	89	49	15			
342	188	26						
589	324	28						
Steel HP 8 X 36								
69	38	25						
188	103	26						
219	120	26						
286	157	27						

SUBSTRUCTURE===== **South abut SB SN 046-0159**
 REFERENCE BORING ===== **2**
 LRFD or ASD or SEISMIC ===== **LRFD**
 PILE CUTOFF ELEV. ===== **659.90** ft
 GROUND SURFACE ELEV. AGAINST PILE DURING DRIVING = **657.90** ft
 GEOTECHNICAL LOSS TYPE (None, Scour, Liquef., DD) ===== **None**
 BOTTOM ELEV. OF SCOUR, LIQUEF., or DD ===== **424.00** ft
 TOP ELEV. OF LIQUEF. (so layers above apply DD) ===== **434.00** ft

MAX. REQUIRED BEARING & RESISTANCE for Selected Pile, Soil Profile, & Losses

Maximum Nominal Req'd Bearing of <u>Pile</u>	Maximum Nominal Req'd Bearing of <u>Boring</u>	Maximum Factored Resistance Available in <u>Boring</u>	Maximum Pile Driveable Length in <u>Boring</u>
705 KIPS	705 KIPS	388 KIPS	33 FT.

TOTAL FACTORED SUBSTRUCTURE LOAD ===== **1538** kips
 TOTAL LENGTH OF SUBSTRUCTURE (along skew)===== **51.20** ft
 NUMBER OF ROWS OF PILES PER SUBSTRUCTURE ===== **1**
 Approx. Factored Loading Applied per pile at 8 ft. Cts ===== 240.31 KIPS
 Approx. Factored Loading Applied per pile at 3 ft. Cts ===== 90.12 KIPS

PILE TYPE AND SIZE ===== **Steel HP 14 X 89**

Plugged Pile Perimeter===== 4.750 FT. Unplugged Pile Perimeter===== 7.033 FT.
 Plugged Pile End Bearing Area===== 1.409 SQFT. Unplugged Pile End Bearing Area===== 0.181 SQFT.

BOT. OF LAYER ELEV. (FT.)	LAYER THICK. (FT.)	UNCONF. COMPR. STRENGTH (TSF)	S.P.T. N VALUE (BLOWS)	GRANULAR OR ROCK LAYER DESCRIPTION	NOMINAL PLUGGED			NOMINAL UNPLUG'D			NOMINAL REQ'D BEARING (KIPS)	FACTORED GEOTECH. LOSS FROM SCOUR or DD (KIPS)	FACTORED GEOTECH. LOSS LOAD FROM DD (KIPS)	FACTORED RESISTANCE AVAILABLE (KIPS)	ESTIMATED PILE LENGTH (FT.)
					SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)	SIDE RESIST. (KIPS)	END BRG. RESIST. (KIPS)	TOTAL RESIST. (KIPS)					
655.40	2.50	0.00	0		0.0	0.0	0.0	0.0	0.0	0.0	0	0	0	0	5
652.90	2.50	0.00	0		0.0	0.0	0.0	0.0	0.0	0.0	0	0	0	0	7
650.40	2.50	0.00	0		0.0	0.0	0.0	0.0	0.0	0.0	0	0	0	0	10
647.90	2.50	0.00	0		0.0	0.0	67.1	0.0	0.0	8.6	9	0	0	5	12
645.40	2.50	3.40	9		19.9	67.1	81.1	29.5	8.6	37.4	37	0	0	21	15
642.90	2.50	3.10	9		18.6	61.2	119.5	27.5	7.9	67.4	67	0	0	37	17
640.40	2.50	4.10	11		22.9	80.9	140.4	34.0	10.4	101.2	101	0	0	56	20
639.40	1.00	4.00	10		9.0	79.0	95.0	13.3	10.2	107.5	95	0	0	52	21
636.90	2.50		7	Medium Sand	1.5	24.6	103.6	2.2	3.2	110.6	104	0	0	57	23
634.40	2.50		9	Medium Sand	1.9	31.6	112.5	2.9	4.1	114.4	113	0	0	62	26
631.90	2.50		11	Medium Sand	2.4	38.6	118.4	3.5	5.0	118.4	118	0	0	65	28
629.90	2.00		12	Medium Sand	2.1	42.1	1345.4	3.1	5.4	279.1	279	0	0	154	30
628.23	1.67		361	Sandy Gravel	249.0	1267.0	678.4	368.7	163.1	529.9	530	0	0	291	32
627.23	1.00			Limestone	118.3	351.0	796.7	175.2	45.2	705.2	705	0	0	388	32.7
626.23	1.00			Limestone	118.3	351.0	915.1	175.2	45.2	880.4	880	0	0	484	33.7
625.23	1.00			Limestone	118.3	351.0	1033.4	175.2	45.2	1055.6	1033	0	0	568	34.7
624.23	1.00			Limestone	118.3	351.0	1151.7	175.2	45.2	1230.9	1152	0	0	633	35.7
623.23	1.00			Limestone		351.0			45.2						

Pile Design Table for South abut SB SN 046-0159 utilizing Boring #2

Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)	Nominal Required Bearing (Kips)	Factored Resistance Available (Kips)	Estimated Pile Length (Ft.)
			Steel HP 10 X 42			Steel HP 12 X 84		
			158	87	30	97	53	28
			Steel HP 10 X 57			252	138	30
			75	41	28	452	249	32
			186	102	30	664	365	34
			366	201	32	Steel HP 14 X 73		
			454	250	33	116	64	28
			Steel HP 12 X 53			249	137	30
			93	51	28	518	285	32
			192	106	30	578	318	33
			418	230	32	Steel HP 14 X 89		
			Steel HP 12 X 63			118	65	28
			94	52	28	279	154	30
			212	117	30	530	291	32
			437	241	32	705	388	33
			497	273	33	Steel HP 14 X 102		
			Steel HP 12 X 74			120	66	28
			96	53	28	304	167	30
			234	129	30	538	296	32
			445	245	32	810	445	34
			589	324	33	Steel HP 14 X 117		
Steel HP 8 X 36						121	67	28
130	72	30				332	183	30
						550	303	32
						Precast 14"x 14"		
						154	85	20
						168	93	21
						193	106	23
						220	121	26
						240	132	28



**DRILLED SHAFT AXIAL CAPACITY IN ROCK -
DOLOMITE, LIMESTONE, SANDSTONE, AND HARD SHALE**

Drilled Shaft Dia.'s for Design Table

STRUCTURE ===== SN 046-0010/0011
 SUBSTRUCTURE & REFERENCE BORING ===== NB Pier 1 & Pier 2 using Core 3
 GROUND SURFACE ELEVATION ===== 642.70 FT
 GROUND WATER ELEVATION ===== FT
 ESTIMATED TOP OF ROCK ELEVATION ===== 630.47 FT
 DRILLED SHAFT DIAMETER IN ROCK ===== 48 IN.
 FACTORED AXIAL LOAD ===== 4832 KIPS
 DRILLED SHAFT CONCRETE STRENGTH, f_c ===== 3.5 KSI

FOUNDATION REDUNDANCY === REDUNDANT

30 IN.
 36 IN.
 42 IN.
 48 IN.
 54 IN.
 60 IN.

SOCKET DEPTH (FT)	TIP ELEV. (FT)	LAYER THICK. (FT)	UNCONFINED COMPRESSIVE STRENGTH (q _u) (KSF)	ROCK TYPE	GSI	ROCK CONDITION	RQD (%)	JOINT TYPE	ROCK INTACT OR TIGHTLY JOINTED?	SIDE RESISTANCE						AVG. q _u W/IN 2 - SHAFT DIA. (KSF)	TIP RESISTANCE			COMBINED SIDE & TIP RESISTANCE					
										NOM. RESIST. (KIPS)	Σ NOM. RESIST. (KIPS)	Σ FACT. RESIST. (KIPS)	SETTLEMENT				NOM. RESIST. (KIPS)	FACT. RESIST. (KIPS)	SETTL. w _{Rn} (IN.)	R _p /R _n	NOM. RESIST. (KIPS)	FACT. RESIST. (KIPS)	SETTLEMENT		
													Q _{C1} (KIPS)	w _{C1} (IN.)	w _{Rn} (IN.)								Q _{C1} (KIPS)	w _{C1} (IN.)	w _{Rn} (IN.)
1.00	629.47	1.00	100.0	Limestone	35	Fractured	0	Open	No	0	0	0	35	0.000	-0.426	1586.4	4358	2179	0.447	0.00	0	0	35	0.000	-0.426
2.00	628.47	1.00	200.0	Limestone	40	Fractured	0	Open	No	0	0	0	90	0.009	-0.378	1805.5	6142	3071	0.548	0.00	0	0	90	0.009	-0.378
3.00	627.47	1.00	500.0	Limestone	50	Normal	23	Closed	Yes	409	409	225	194	0.017	0.370	2001.8	10522	5261	0.878	0.88	3386	1713	406	0.018	0.250
4.00	626.47	1.00	1904.0	Limestone	50	Normal	23	Closed	Yes	411	820	451	456	0.034	0.281	2014.5	10662	5331	0.829	0.74	3201	1642	955	0.038	0.188
5.00	625.47	1.00	2217.0	Limestone	50	Normal	23	Closed	Yes	411	1231	677	760	0.050	0.244	1989.6	10619	5309	0.764	0.64	3389	1756	1643	0.060	0.161
6.00	624.47	1.00	2217.0	Limestone	50	Normal	50	Closed	Yes	411	1641	903	1080	0.065	0.230	1967.9	10589	5295	0.701	0.56	3770	1967	2466	0.084	0.150
7.00	623.47	1.00	2336.0	Limestone	50	Normal	50	Closed	Yes	411	2052	1129	1432	0.079	0.221	1934.4	60770	30385	3.670	0.51	4198	2202	3552	0.114	0.142
8.00	622.47	1.00	1269.0	Limestone	60	Normal	50	Closed	Yes	411	2463	1355	1697	0.082	0.220	2034.3	63908	31954	3.816	0.46	4591	2419	4099	0.124	0.144
9.00	621.47	1.00	2048.0	Limestone	60	Normal	50	Closed	Yes	411	2874	1581	2082	0.090	0.205	2036.8	63986	31993	3.721	0.40	4823	2555	5102	0.147	0.137
10.00	620.47	1.00	1953.0	Limestone	70	Normal	50	Closed	Yes	411	3285	1807	2537	0.095	0.177	2051.1	64438	32219	3.884	0.32	4858	2593	5899	0.161	0.124
11.00	619.47	1.00	2070.0	Limestone	70	Normal	80	Closed	Yes	411	3695	2032	3068	0.103	0.158	2050.9	64430	32215	3.997	0.26	4986	2678	6964	0.182	0.116
12.00	618.47	1.00	2006.0	Limestone	70	Normal	80	Closed	Yes	411	4106	2258	3660	0.113	0.146	2058.6	64674	32337	4.139	0.21	5184	2797	8226	0.208	0.111
13.00	617.47	1.00	2018.0	Limestone	70	Normal	80	Closed	Yes	411	4517	2484	4336	0.126	0.137										
14.00	616.47	1.00	2043.0	Limestone	70	Normal	80	Closed	Yes	411	4928	2710	5114	0.141	0.131										
15.00	615.47	1.00	2068.0	Limestone	70	Normal	80	Closed	Yes	411	5338	2936	6014	0.159	0.126										
16.00	614.47	1.00	2068.0	Limestone	70	Normal	80	Closed	Yes	411	5749	3162	7054	0.181	0.123										
17.00	613.47	1.00	2068.0	Limestone	70	Normal	80	Closed	Yes	411	6160	3388	8261	0.207	0.122										
18.00	612.47	1.00	2068.0	Limestone	70	Normal	80	Closed	Yes	411	6571	3614	9671	0.238	0.121										
19.00	611.47	1.00	2068.0	Limestone	70	Normal	80	Closed	Yes	411	6981	3840	11333	0.274	0.121										
20.00	610.47	1.00	2068.0	Limestone	70	Normal	80	Closed	Yes	411	7392	4066	13307	0.317	0.122										

This data is below the bottom of the rock core. This information was extended from the last foot of the core.



**DRILLED SHAFT AXIAL CAPACITY IN ROCK -
DOLOMITE, LIMESTONE, SANDSTONE, AND HARD SHALE**

Drilled Shaft Dia.'s for Design Table

STRUCTURE ===== SN 046-0010/0011
 SUBSTRUCTURE & REFERENCE BORING ===== NB Pier 1 & Pier 2 using Core 3
 GROUND SURFACE ELEVATION ===== 642.70 FT
 GROUND WATER ELEVATION ===== FT
 ESTIMATED TOP OF ROCK ELEVATION ===== 630.47 FT
 DRILLED SHAFT DIAMETER IN ROCK ===== 54 IN.
 FACTORED AXIAL LOAD ===== 4832 KIPS
 DRILLED SHAFT CONCRETE STRENGTH, f_c ===== 3.5 KSI

FOUNDATION REDUNDANCY === REDUNDANT

30 IN.
 36 IN.
 42 IN.
 48 IN.
 54 IN.
 60 IN.

SOCKET DEPTH (FT)	TIP ELEV. (FT)	LAYER THICK. (FT)	UNCONFINED COMPRESSIVE STRENGTH (q _u) (KSF)	ROCK TYPE	GSI	ROCK CONDITION	RQD (%)	JOINT TYPE	ROCK INTACT OR TIGHTLY JOINTED?	SIDE RESISTANCE						AVG. q _u W/IN 2 - SHAFT DIA. (KSF)	TIP RESISTANCE			COMBINED SIDE & TIP RESISTANCE					
										NOM. RESIST. (KIPS)	Σ NOM. RESIST. (KIPS)	Σ FACT. RESIST. (KIPS)	SETTLEMENT				RESIST. (KIPS)	FACT. RESIST. (KIPS)	SETTL. (IN.)	R _p /R _n	NOM. RESIST. (KIPS)	FACT. RESIST. (KIPS)	SETTLEMENT		
													Q _{C1} (KIPS)	w _{C1} (IN.)	w _{Rn} (IN.)								Q _{C1} (KIPS)	w _{C1} (IN.)	w _{Rn} (IN.)
1.00	629.47	1.00	100.0	Limestone	35	Fractured	0	Open	No	0	0	0	0	0.000	-0.479	1627.1	5633	2817	0.466	1.00	5633	2817	0	0.000	-0.003
2.00	628.47	1.00	200.0	Limestone	40	Fractured	0	Open	No	0	0	0	102	0.009	-0.426	1834.9	7883	3941	0.588	0.00	0	0	102	0.009	-0.426
3.00	627.47	1.00	500.0	Limestone	50	Normal	23	Closed	Yes	460	460	253	218	0.017	0.413	2002.2	13320	6660	0.932	0.89	4341	2194	471	0.018	0.272
4.00	626.47	1.00	1904.0	Limestone	50	Normal	23	Closed	Yes	462	922	507	511	0.035	0.313	2014.9	13496	6748	0.908	0.77	4006	2049	1114	0.039	0.204
5.00	625.47	1.00	2217.0	Limestone	50	Normal	23	Closed	Yes	462	1385	762	849	0.052	0.270	1995.6	13475	6738	0.820	0.67	4168	2153	1912	0.062	0.174
6.00	624.47	1.00	2217.0	Limestone	50	Normal	50	Closed	Yes	462	1847	1016	1203	0.067	0.255	1979.0	13470	6735	0.784	0.60	4584	2384	2855	0.086	0.162
7.00	623.47	1.00	2336.0	Limestone	50	Normal	50	Closed	Yes	462	2309	1270	1589	0.082	0.245	1949.2	77503	38751	4.036	0.54	5062	2646	4075	0.116	0.154
8.00	622.47	1.00	1269.0	Limestone	60	Normal	50	Closed	Yes	462	2771	1524	1877	0.084	0.245	2038.0	81032	40516	4.114	0.50	5512	2895	4669	0.125	0.155
9.00	621.47	1.00	2048.0	Limestone	60	Normal	50	Closed	Yes	462	3233	1778	2292	0.092	0.228	2040.2	81121	40560	4.065	0.44	5757	3040	5754	0.147	0.147
10.00	620.47	1.00	1953.0	Limestone	70	Normal	50	Closed	Yes	462	3695	2032	2772	0.096	0.197	2053.0	81629	40814	4.242	0.36	5760	3065	6583	0.159	0.133
11.00	619.47	1.00	2070.0	Limestone	70	Normal	80	Closed	Yes	462	4157	2286	3325	0.103	0.176	2052.8	81620	40810	4.341	0.29	5878	3147	7682	0.177	0.123
12.00	618.47	1.00	2006.0	Limestone	70	Normal	80	Closed	Yes	462	4619	2541	3934	0.111	0.162										
13.00	617.47	1.00	2018.0	Limestone	70	Normal	80	Closed	Yes	462	5081	2795	4617	0.122	0.151										
14.00	616.47	1.00	2043.0	Limestone	70	Normal	80	Closed	Yes	462	5544	3049	5392	0.135	0.144										
15.00	615.47	1.00	2068.0	Limestone	70	Normal	80	Closed	Yes	462	6006	3303	6273	0.151	0.138										
16.00	614.47	1.00	2068.0	Limestone	70	Normal	80	Closed	Yes	462	6468	3557	7272	0.169	0.134										
17.00	613.47	1.00	2068.0	Limestone	70	Normal	80	Closed	Yes	462	6930	3811	8408	0.190	0.131										
18.00	612.47	1.00	2068.0	Limestone	70	Normal	80	Closed	Yes	462	7392	4066	9708	0.214	0.129										
19.00	611.47	1.00	2068.0	Limestone	70	Normal	80	Closed	Yes	462	7854	4320	11201	0.242	0.128										
20.00	610.47	1.00	2068.0	Limestone	70	Normal	80	Closed	Yes	462	8316	4574	12927	0.275	0.128										

This data is below the bottom of the rock core. This information was extended from the last foot of the core.



**DRILLED SHAFT AXIAL CAPACITY IN ROCK -
DOLOMITE, LIMESTONE, SANDSTONE, AND HARD SHALE**

Drilled Shaft Dia.'s for Design Table

STRUCTURE ===== SN 046-0010/0011
 SUBSTRUCTURE & REFERENCE BORING ===== NB Pier 1 & Pier 2 using Core 3
 GROUND SURFACE ELEVATION ===== 642.70 FT
 GROUND WATER ELEVATION ===== FT
 ESTIMATED TOP OF ROCK ELEVATION ===== 630.47 FT
 DRILLED SHAFT DIAMETER IN ROCK ===== 60 IN.
 FACTORED AXIAL LOAD ===== 4832 KIPS
 DRILLED SHAFT CONCRETE STRENGTH, f_c ===== 3.5 KSI

FOUNDATION REDUNDANCY === REDUNDANT

30 IN.
 36 IN.
 42 IN.
 48 IN.
 54 IN.
 60 IN.

SOCKET DEPTH (FT)	TIP ELEV. (FT)	LAYER THICK. (FT)	UNCONFINED COMPRESSIVE STRENGTH (q _u) (KSF)	ROCK TYPE	GSI	ROCK CONDITION	RQD (%)	JOINT TYPE	ROCK INTACT OR TIGHTLY JOINTED?	SIDE RESISTANCE						AVG. q _u W/IN 2 - SHAFT DIA. (KSF)	TIP RESISTANCE			COMBINED SIDE & TIP RESISTANCE					
										NOM. RESIST. (KIPS)	Σ NOM. RESIST. (KIPS)	Σ FACT. RESIST. (KIPS)	SETTLEMENT				NOM. RESIST. (KIPS)	FACT. RESIST. (KIPS)	SETTL. w _{Rn} (IN.)	R _p /R _n	NOM. RESIST. (KIPS)	FACT. RESIST. (KIPS)	SETTLEMENT		
													Q _{C1} (KIPS)	w _{C1} (IN.)	w _{Rn} (IN.)								Q _{C1} (KIPS)	w _{C1} (IN.)	w _{Rn} (IN.)
1.00	629.47	1.00	100.0	Limestone	35	Fractured	0	Open	No	0	0	0	0	0.000	-0.533	1671.4	7111	3556	0.541	1.00	7111	3556	0	0.000	-0.003
2.00	628.47	1.00	200.0	Limestone	40	Fractured	0	Open	No	0	0	0	113	0.008	-0.473	1852.0	9810	4905	0.610	0.00	0	0	113	0.008	-0.473
3.00	627.47	1.00	500.0	Limestone	50	Normal	23	Closed	Yes	511	511	281	242	0.017	0.456	2003.8	16456	8228	0.987	0.91	5418	2735	534	0.018	0.295
4.00	626.47	1.00	1904.0	Limestone	50	Normal	23	Closed	Yes	513	1025	564	566	0.035	0.344	2017.7	16683	8342	0.910	0.79	4899	2501	1273	0.039	0.220
5.00	625.47	1.00	2217.0	Limestone	50	Normal	23	Closed	Yes	513	1538	846	938	0.053	0.296	2002.8	16691	8346	0.906	0.69	5021	2587	2184	0.063	0.187
6.00	624.47	1.00	2217.0	Limestone	50	Normal	50	Closed	Yes	513	2052	1129	1326	0.069	0.279	1987.9	16697	8348	0.802	0.62	5467	2836	3248	0.088	0.174
7.00	623.47	1.00	2336.0	Limestone	50	Normal	50	Closed	Yes	513	2565	1411	1747	0.084	0.268	1961.1	16611	8305	0.751	0.57	5976	3116	4601	0.117	0.164
8.00	622.47	1.00	1269.0	Limestone	60	Normal	50	Closed	Yes	513	3079	1693	2058	0.086	0.269	2041.0	100187	50094	4.488	0.53	6502	3405	5243	0.126	0.167
9.00	621.47	1.00	2048.0	Limestone	60	Normal	50	Closed	Yes	513	3592	1976	2503	0.094	0.250	2043.0	100286	50143	4.370	0.47	6756	3558	6409	0.147	0.157
10.00	620.47	1.00	1953.0	Limestone	70	Normal	50	Closed	Yes	513	4106	2258	3010	0.097	0.217	2054.5	100850	50425	4.548	0.39	6721	3566	7270	0.157	0.141
11.00	619.47	1.00	2070.0	Limestone	70	Normal	80	Closed	Yes	513	4619	2541	3588	0.103	0.193										
12.00	618.47	1.00	2006.0	Limestone	70	Normal	80	Closed	Yes	513	5133	2823	4216	0.111	0.177										
13.00	617.47	1.00	2018.0	Limestone	70	Normal	80	Closed	Yes	513	5646	3105	4914	0.120	0.166										
14.00	616.47	1.00	2043.0	Limestone	70	Normal	80	Closed	Yes	513	6160	3388	5694	0.132	0.157										
15.00	615.47	1.00	2068.0	Limestone	70	Normal	80	Closed	Yes	513	6673	3670	6570	0.145	0.150										
16.00	614.47	1.00	2068.0	Limestone	70	Normal	80	Closed	Yes	513	7186	3953	7549	0.160	0.145										
17.00	613.47	1.00	2068.0	Limestone	70	Normal	80	Closed	Yes	513	7700	4235	8646	0.178	0.141										
18.00	612.47	1.00	2068.0	Limestone	70	Normal	80	Closed	Yes	513	8213	4517	9881	0.198	0.138										
19.00	611.47	1.00	2068.0	Limestone	70	Normal	80	Closed	Yes	513	8727	4800	11274	0.222	0.137										
20.00	610.47	1.00	2068.0	Limestone	70	Normal	80	Closed	Yes	513	9240	5082	12853	0.248	0.136										

This data is below the bottom of the rock core. This information was extended from the last foot of the core.



Drilled Shaft Design Table for NB Pier 1 & Pier 2 using Core 3

Estimated Top of Rock Elevation: 630.47

(Page 1 of 3)

SOCKET DEPTH (FT)	TIP ELEV. (FT)	NOMINAL SHAFT RESIST. (KIPS)	FACTORED SHAFT RESIST. (KIPS)	RESIST. METHOD	SETTLEMENT DATA		
					Q _{C1} (KIPS)	W _{C1} (IN.)	W _{Rn} (IN.)
30 in. Diameter Drilled Shaft							
1	629.47	1543	772	TIP	--	--	0.283
2	628.47	2433	1216	TIP	--	--	0.409
3	627.47	4085	2043	TIP	--	--	0.675
4	626.47	24757	12379	TIP	--	--	3.970
5	625.47	24109	12055	TIP	--	--	3.496
6	624.47	23748	11874	TIP	--	--	3.093
7	623.47	22939	11469	TIP	--	--	2.663
8	622.47	24777	12388	TIP	--	--	2.788
9	621.47	24765	12382	TIP	--	--	2.721
10	620.47	25047	12523	TIP	--	--	2.884
11	619.47	25042	12521	TIP	--	--	3.008
12	618.47	25194	12597	TIP	--	--	3.152
13	617.47	25317	12658	TIP	--	--	3.293
14	616.47	25378	12689	TIP	--	--	3.428
15	615.47	25378	12689	TIP	--	--	3.547
16	614.47	3593	1976	SIDE	7422	0.300	0.103
17	613.47	3850	2117	SIDE	9533	0.381	0.105
18	612.47	4107	2259	SIDE	12474	0.493	0.109
19	611.47	4363	2400	SIDE	16803	0.659	0.114
20	610.47	4620	2541	SIDE	23726	0.925	0.119
36 in. Diameter Drilled Shaft							
1	629.47	2421	1210	TIP	--	--	0.363
2	628.47	3348	1674	TIP	--	--	0.436
3	627.47	5910	2955	TIP	--	--	0.770
4	626.47	5976	2988	TIP	--	--	0.709
5	625.47	35028	17514	TIP	--	--	3.862
6	624.47	34406	17203	TIP	--	--	3.423
7	623.47	33470	16735	TIP	--	--	3.004
8	622.47	35749	17875	TIP	--	--	3.124
9	621.47	35808	17904	TIP	--	--	3.081
10	620.47	36147	18073	TIP	--	--	3.218
11	619.47	36141	18071	TIP	--	--	3.359
12	618.47	36324	18162	TIP	--	--	3.485
13	617.47	36471	18235	TIP	--	--	3.625
14	616.47	36545	18272	TIP	--	--	3.776
15	615.47	4004	2202	SIDE	5727	0.197	0.107
16	614.47	4312	2372	SIDE	6991	0.235	0.107
17	613.47	4620	2541	SIDE	8566	0.283	0.108
18	612.47	4928	2710	SIDE	10563	0.345	0.110
19	611.47	5236	2880	SIDE	13156	0.425	0.113
20	610.47	5544	3049	SIDE	16623	0.533	0.117
42 in. Diameter Drilled Shaft							
1	629.47	3222	1611	TIP	--	--	0.397
2	628.47	4655	2328	TIP	--	--	0.512
3	627.47	8020	4010	TIP	--	--	0.821
4	626.47	8167	4084	TIP	--	--	0.775
5	625.47	8115	4057	TIP	--	--	0.728
6	624.47	47075	23537	TIP	--	--	3.755
7	623.47	46068	23034	TIP	--	--	3.317
8	622.47	48813	24407	TIP	--	--	3.460
9	621.47	48882	24441	TIP	--	--	3.418
10	620.47	49277	24639	TIP	--	--	3.551
11	619.47	49270	24635	TIP	--	--	3.666
12	618.47	49484	24742	TIP	--	--	3.818
13	617.47	49655	24828	TIP	--	--	3.977
14	616.47	4312	2371	SIDE	4874	0.151	0.119



Drilled Shaft Design Table for NB Pier 1 & Pier 2 using Core 3

Estimated Top of Rock Elevation: 630.47

(Page 2 of 3)

SOCKET DEPTH (FT)	TIP ELEV. (FT)	NOMINAL SHAFT RESIST. (KIPS)	FACTORED SHAFT RESIST. (KIPS)	RESIST. METHOD	SETTLEMENT DATA		
					Q _{C1} (KIPS)	W _{C1} (IN.)	W _{Rn} (IN.)
15	615.47	4671	2569	SIDE	5817	0.174	0.116
16	614.47	5030	2767	SIDE	6934	0.201	0.114
17	613.47	5390	2964	SIDE	8267	0.235	0.114
18	612.47	5749	3162	SIDE	9876	0.276	0.114
19	611.47	6109	3360	SIDE	11840	0.326	0.116
20	610.47	6468	3557	SIDE	14276	0.389	0.118
48 in. Diameter Drilled Shaft							
1	629.47	4358	2179	TIP	--	--	0.447
2	628.47	6142	3071	TIP	--	--	0.548
3	627.47	10522	5261	TIP	--	--	0.878
4	626.47	10662	5331	TIP	--	--	0.829
5	625.47	10619	5309	TIP	--	--	0.764
6	624.47	10589	5295	TIP	--	--	0.701
7	623.47	60770	30385	TIP	--	--	3.670
8	622.47	63908	31954	TIP	--	--	3.816
9	621.47	63986	31993	TIP	--	--	3.721
10	620.47	64438	32219	TIP	--	--	3.884
11	619.47	64430	32215	TIP	--	--	3.997
12	618.47	64674	32337	TIP	--	--	4.139
13	617.47	4517	2484	SIDE	4336	0.126	0.137
14	616.47	4928	2710	SIDE	5114	0.141	0.131
15	615.47	5338	2936	SIDE	6014	0.159	0.126
16	614.47	5749	3162	SIDE	7054	0.181	0.123
17	613.47	6160	3388	SIDE	8261	0.207	0.122
18	612.47	6571	3614	SIDE	9671	0.238	0.121
19	611.47	6981	3840	SIDE	11333	0.274	0.121
20	610.47	7392	4066	SIDE	13307	0.317	0.122
54 in. Diameter Drilled Shaft							
1	629.47	5633	2817	TIP	--	--	0.466
2	628.47	7883	3941	TIP	--	--	0.588
3	627.47	13320	6660	TIP	--	--	0.932
4	626.47	13496	6748	TIP	--	--	0.908
5	625.47	13475	6738	TIP	--	--	0.820
6	624.47	13470	6735	TIP	--	--	0.784
7	623.47	77503	38751	TIP	--	--	4.036
8	622.47	81032	40516	TIP	--	--	4.114
9	621.47	81121	40560	TIP	--	--	4.065
10	620.47	81629	40814	TIP	--	--	4.242
11	619.47	81620	40810	TIP	--	--	4.341
12	618.47	4619	2541	SIDE	3934	0.111	0.162
13	617.47	5081	2795	SIDE	4617	0.122	0.151
14	616.47	5544	3049	SIDE	5392	0.135	0.144
15	615.47	6006	3303	SIDE	6273	0.151	0.138
16	614.47	6468	3557	SIDE	7272	0.169	0.134
17	613.47	6930	3811	SIDE	8408	0.190	0.131
18	612.47	7392	4066	SIDE	9708	0.214	0.129
19	611.47	7854	4320	SIDE	11201	0.242	0.128
20	610.47	8316	4574	SIDE	12927	0.275	0.128
60 in. Diameter Drilled Shaft							
1	629.47	7111	3556	TIP	--	--	0.541
2	628.47	9810	4905	TIP	--	--	0.610
3	627.47	16456	8228	TIP	--	--	0.987
4	626.47	16683	8342	TIP	--	--	0.910
5	625.47	16691	8346	TIP	--	--	0.906
6	624.47	16697	8348	TIP	--	--	0.802
7	623.47	16611	8305	TIP	--	--	0.751
8	622.47	100187	50094	TIP	--	--	4.488



Drilled Shaft Design Table for NB Pier 1 & Pier 2 using Core 3

Estimated Top of Rock Elevation: 630.47

(Page 3 of 3)

SOCKET DEPTH (FT)	TIP ELEV. (FT)	NOMINAL SHAFT RESIST. (KIPS)	FACTORED SHAFT RESIST. (KIPS)	RESIST. METHOD	SETTLEMENT DATA		
					Q _{C1} (KIPS)	w _{C1} (IN.)	w _{Rn} (IN.)
9	621.47	100286	50143	TIP	--	--	4.370
10	620.47	100850	50425	TIP	--	--	4.548
11	619.47	4619	2541	SIDE	3588	0.103	0.193
12	618.47	5133	2823	SIDE	4216	0.111	0.177
13	617.47	5646	3105	SIDE	4914	0.120	0.166
14	616.47	6160	3388	SIDE	5694	0.132	0.157
15	615.47	6673	3670	SIDE	6570	0.145	0.150
16	614.47	7186	3953	SIDE	7549	0.160	0.145
17	613.47	7700	4235	SIDE	8646	0.178	0.141
18	612.47	8213	4517	SIDE	9881	0.198	0.138
19	611.47	8727	4800	SIDE	11274	0.222	0.137
20	610.47	9240	5082	SIDE	12853	0.248	0.136



**DRILLED SHAFT AXIAL CAPACITY IN ROCK -
DOLOMITE, LIMESTONE, SANDSTONE, AND HARD SHALE**

Drilled Shaft Dia.'s for Design Table

STRUCTURE ===== SN 046-0010/0011
 SUBSTRUCTURE & REFERENCE BORING ===== SB Pier 1 & Pier 2 Rock Core 1
 GROUND SURFACE ELEVATION ===== 642.70 FT
 GROUND WATER ELEVATION ===== FT
 ESTIMATED TOP OF ROCK ELEVATION ===== 631.47 FT
 DRILLED SHAFT DIAMETER IN ROCK ===== 48 IN.
 FACTORED AXIAL LOAD ===== 4832 KIPS
 DRILLED SHAFT CONCRETE STRENGTH, f_c ===== 3.5 KSI

FOUNDATION REDUNDANCY === REDUNDANT

30 IN.
 36 IN.
 42 IN.
 48 IN.
 54 IN.
 60 IN.

SOCKET DEPTH (FT)	TIP ELEV. (FT)	LAYER THICK. (FT)	UNCONFINED COMPRESSIVE STRENGTH (q _u) (KSF)	ROCK TYPE	GSI	ROCK CONDITION	RQD (%)	JOINT TYPE	ROCK INTACT OR TIGHTLY JOINTED?	SIDE RESISTANCE						AVG. q _u W/IN 2 - SHAFT DIA. (KSF)	TIP RESISTANCE			COMBINED SIDE & TIP RESISTANCE					
										NOM. RESIST. (KIPS)	Σ NOM. RESIST. (KIPS)	Σ FACT. RESIST. (KIPS)	SETTLEMENT				NOM. RESIST. (KIPS)	FACT. RESIST. (KIPS)	SETTL. w _{Rn} (IN.)	R _p /R _n	NOM. RESIST. (KIPS)	FACT. RESIST. (KIPS)	SETTLEMENT		
													Q _{C1} (KIPS)	w _{C1} (IN.)	w _{Rn} (IN.)								Q _{C1} (KIPS)	w _{C1} (IN.)	w _{Rn} (IN.)
1.00	630.47	1.00	100.0	Limestone	20	Fractured	0	Open	No	0	0	0	35	0.001	-0.843	1252.3	1743	871	0.250	0.00	0	0	35	0.001	-0.843
2.00	629.47	1.00	100.0	Limestone	35	Fractured	0	Open	No	0	0	0	70	0.011	-0.565	1585.8	4384	2192	0.561	0.00	0	0	70	0.011	-0.565
3.00	628.47	1.00	200.0	Limestone	35	Fractured	0	Open	No	0	0	0	125	0.018	-0.510	1857.8	5085	2542	0.557	0.00	0	0	125	0.018	-0.510
4.00	627.47	1.00	500.0	Limestone	35	Normal	0	Closed	Yes	409	409	225	229	0.030	0.437	2084.5	5682	2841	0.517	0.89	3757	1899	578	0.032	0.306
5.00	626.47	1.00	1000.0	Limestone	40	Normal	0	Closed	Yes	411	820	451	395	0.044	0.572	2215.6	7540	3770	0.586	0.86	5678	2880	1035	0.050	0.381
6.00	625.47	1.00	1000.0	Limestone	40	Normal	44	Closed	Yes	411	1231	677	565	0.056	0.622	2352.8	8025	4013	0.517	0.83	7206	3665	1616	0.067	0.392
7.00	624.47	1.00	2000.0	Limestone	60	Normal	44	Closed	Yes	411	1642	903	852	0.062	0.422	2370.4	74468	37234	4.720	0.71	5742	2953	2114	0.078	0.270
8.00	623.47	1.00	2551.0	Limestone	60	Normal	44	Closed	Yes	411	2052	1129	1211	0.071	0.315	2319.1	72857	36429	4.565	0.60	5104	2655	2853	0.097	0.205
9.00	622.47	1.00	2667.0	Limestone	60	Normal	44	Closed	Yes	411	2463	1355	1613	0.082	0.258	2253.4	70792	35396	4.329	0.50	4933	2590	3756	0.120	0.171
10.00	621.47	1.00	2768.0	Limestone	60	Normal	44	Closed	Yes	411	2874	1581	2063	0.094	0.222	2175.0	68330	34165	4.118	0.42	4961	2624	4881	0.148	0.152
11.00	620.47	1.00	2376.0	Limestone	70	Normal	81	Closed	Yes	411	3285	1807	2556	0.100	0.186	2145.6	67407	33703	4.183	0.33	4904	2616	5744	0.164	0.133
12.00	619.47	1.00	2314.0	Limestone	70	Normal	81	Closed	Yes	411	3695	2032	3109	0.109	0.164	2124.0	66727	33364	4.270	0.26	4996	2683	6799	0.186	0.122
13.00	618.47	1.00	2049.0	Limestone	70	Normal	81	Closed	Yes	411	4106	2258	3694	0.119	0.151										
14.00	617.47	1.00	2097.0	Limestone	70	Normal	81	Closed	Yes	411	4517	2484	4367	0.131	0.141										
15.00	616.47	1.00	2141.0	Limestone	70	Normal	81	Closed	Yes	411	4928	2710	5144	0.147	0.134										
16.00	615.47	1.00	2141.0	Limestone	70	Normal	81	Closed	Yes	411	5338	2936	6036	0.166	0.130										
17.00	614.47	1.00	2141.0	Limestone	70	Normal	81	Closed	Yes	411	5749	3162	7064	0.188	0.127										
18.00	613.47	1.00	2141.0	Limestone	70	Normal	81	Closed	Yes	411	6160	3388	8254	0.214	0.125										
19.00	612.47	1.00	2141.0	Limestone	70	Normal	81	Closed	Yes	411	6571	3614	9641	0.244	0.124										
20.00	611.47	1.00	2141.0	Limestone	70	Normal	81	Closed	Yes	411	6981	3840	11269	0.280	0.124										

This data is below the bottom of the rock core. This information was extended from the last foot of the core.



**DRILLED SHAFT AXIAL CAPACITY IN ROCK -
DOLOMITE, LIMESTONE, SANDSTONE, AND HARD SHALE**

Drilled Shaft Dia.'s for Design Table

STRUCTURE ===== SN 046-0010/0011
 SUBSTRUCTURE & REFERENCE BORING ===== SB Pier 1 & Pier 2 Rock Core 1
 GROUND SURFACE ELEVATION ===== 642.70 FT
 GROUND WATER ELEVATION ===== FT
 ESTIMATED TOP OF ROCK ELEVATION ===== 631.47 FT
 DRILLED SHAFT DIAMETER IN ROCK ===== 54 IN.
 FACTORED AXIAL LOAD ===== 4832 KIPS
 DRILLED SHAFT CONCRETE STRENGTH, f_c ===== 3.5 KSI

FOUNDATION REDUNDANCY === REDUNDANT

30 IN.
 36 IN.
 42 IN.
 48 IN.
 54 IN.
 60 IN.

SOCKET DEPTH (FT)	TIP ELEV. (FT)	LAYER THICK. (FT)	UNCONFINED COMPRESSIVE STRENGTH (q _u) (KSF)	ROCK TYPE	GSI	ROCK CONDITION	RQD (%)	JOINT TYPE	ROCK INTACT OR TIGHTLY JOINTED?	SIDE RESISTANCE						AVG. q _u W/IN 2 - SHAFT DIA. (KSF)	TIP RESISTANCE			COMBINED SIDE & TIP RESISTANCE					
										NOM. RESIST. (KIPS)	Σ NOM. RESIST. (KIPS)	Σ FACT. RESIST. (KIPS)	SETTLEMENT				NOM. RESIST. (KIPS)	FACT. RESIST. (KIPS)	SETTL. w _{Rn} (IN.)	R _p /R _n	NOM. RESIST. (KIPS)	FACT. RESIST. (KIPS)	SETTLEMENT		
													Q _{C1} (KIPS)	w _{C1} (IN.)	w _{Rn} (IN.)								Q _{C1} (KIPS)	w _{C1} (IN.)	w _{Rn} (IN.)
1.00	630.47	1.00	100.0	Limestone	20	Fractured	0	Open	No	0	0	0	0	0.000	-0.948	1420.7	2413	1207	0.277	1.00	2413	1207	0	0.000	-0.005
2.00	629.47	1.00	100.0	Limestone	35	Fractured	0	Open	No	0	0	0	78	0.010	-0.636	1673.6	5801	2901	0.610	0.00	0	0	78	0.010	-0.636
3.00	628.47	1.00	200.0	Limestone	35	Fractured	0	Open	No	0	0	0	141	0.018	-0.573	1908.4	6581	3290	0.596	0.00	0	0	141	0.018	-0.573
4.00	627.47	1.00	500.0	Limestone	35	Normal	0	Closed	Yes	460	460	253	257	0.031	0.487	2080.6	7180	3590	0.570	0.90	4837	2442	687	0.033	0.333
5.00	626.47	1.00	1000.0	Limestone	40	Normal	0	Closed	Yes	462	922	507	444	0.046	0.638	2202.4	9494	4747	0.621	0.87	7218	3655	1230	0.051	0.415
6.00	625.47	1.00	1000.0	Limestone	40	Normal	44	Closed	Yes	462	1385	762	634	0.059	0.694	2329.2	10070	5035	0.579	0.85	9043	4591	1910	0.070	0.427
7.00	624.47	1.00	2000.0	Limestone	60	Normal	44	Closed	Yes	462	1847	1016	952	0.064	0.470	2344.9	93235	46617	5.070	0.74	7105	3645	2479	0.081	0.294
8.00	623.47	1.00	2551.0	Limestone	60	Normal	44	Closed	Yes	462	2309	1270	1349	0.074	0.350	2299.3	91423	45712	4.859	0.63	6231	3231	3315	0.099	0.222
9.00	622.47	1.00	2667.0	Limestone	60	Normal	44	Closed	Yes	462	2771	1524	1788	0.085	0.286	2240.9	89099	44550	4.675	0.53	5956	3117	4325	0.122	0.185
10.00	621.47	1.00	2768.0	Limestone	60	Normal	44	Closed	Yes	462	3233	1778	2275	0.096	0.247	2171.2	86329	43165	4.484	0.46	5940	3132	5564	0.149	0.163
11.00	620.47	1.00	2376.0	Limestone	70	Normal	81	Closed	Yes	462	3695	2032	2799	0.101	0.206	2145.1	85291	42646	4.537	0.37	5824	3097	6476	0.164	0.142
12.00	619.47	1.00	2314.0	Limestone	70	Normal	81	Closed	Yes	462	4157	2286	3377	0.109	0.181										
13.00	618.47	1.00	2049.0	Limestone	70	Normal	81	Closed	Yes	462	4619	2541	3981	0.117	0.167										
14.00	617.47	1.00	2097.0	Limestone	70	Normal	81	Closed	Yes	462	5081	2795	4665	0.128	0.156										
15.00	616.47	1.00	2141.0	Limestone	70	Normal	81	Closed	Yes	462	5544	3049	5444	0.141	0.147										
16.00	615.47	1.00	2141.0	Limestone	70	Normal	81	Closed	Yes	462	6006	3303	6322	0.157	0.141										
17.00	614.47	1.00	2141.0	Limestone	70	Normal	81	Closed	Yes	462	6468	3557	7317	0.175	0.137										
18.00	613.47	1.00	2141.0	Limestone	70	Normal	81	Closed	Yes	462	6930	3811	8447	0.197	0.134										
19.00	612.47	1.00	2141.0	Limestone	70	Normal	81	Closed	Yes	462	7392	4066	9738	0.221	0.132										
20.00	611.47	1.00	2141.0	Limestone	70	Normal	81	Closed	Yes	462	7854	4320	11219	0.250	0.131										

This data is below the bottom of the rock core. This information was extended from the last foot of the core.



DRILLED SHAFT AXIAL CAPACITY IN ROCK -
DOLOMITE, LIMESTONE, SANDSTONE, AND HARD SHALE

Drilled Shaft Dia.'s for Design Table

STRUCTURE ===== SN 046-0010/0011
 SUBSTRUCTURE & REFERENCE BORING ===== SB Pier 1 & Pier 2 Rock Core 1
 GROUND SURFACE ELEVATION ===== 642.70 FT
 GROUND WATER ELEVATION ===== FT
 ESTIMATED TOP OF ROCK ELEVATION ===== 631.47 FT
 DRILLED SHAFT DIAMETER IN ROCK ===== 60 IN.
 FACTORED AXIAL LOAD ===== 4832 KIPS
 DRILLED SHAFT CONCRETE STRENGTH, f_c ===== 3.5 KSI

FOUNDATION REDUNDANCY === REDUNDANT

30 IN.
 36 IN.
 42 IN.
 48 IN.
 54 IN.
 60 IN.

SOCKET DEPTH (FT)	TIP ELEV. (FT)	LAYER THICK. (FT)	UNCONFINED COMPRESSIVE STRENGTH (q _u) (KSF)	ROCK TYPE	GSI	ROCK CONDITION	RQD (%)	JOINT TYPE	ROCK INTACT OR TIGHTLY JOINTED?	SIDE RESISTANCE						AVG. q _u W/IN 2 - SHAFT DIA. (KSF)	TIP RESISTANCE			COMBINED SIDE & TIP RESISTANCE					
										NOM. RESIST. (KIPS)	Σ NOM. RESIST. (KIPS)	Σ FACT. RESIST. (KIPS)	SETTLEMENT				NOM. RESIST. (KIPS)	FACT. RESIST. (KIPS)	SETTL. w _{Rn} (IN.)	R _p /R _n	NOM. RESIST. (KIPS)	FACT. RESIST. (KIPS)	SETTLEMENT		
													Q _{C1} (KIPS)	w _{C1} (IN.)	w _{Rn} (IN.)								Q _{C1} (KIPS)	w _{C1} (IN.)	w _{Rn} (IN.)
1.00	630.47	1.00	100.0	Limestone	20	Fractured	0	Open	No	0	0	0	0	0.000	-1.053	1516.2	3122	1561	0.342	1.00	3122	1561	0	0.000	-0.004
2.00	629.47	1.00	100.0	Limestone	35	Fractured	0	Open	No	0	0	0	87	0.009	-0.706	1737.6	7389	3694	0.640	0.00	0	0	87	0.009	-0.706
3.00	628.47	1.00	200.0	Limestone	35	Fractured	0	Open	No	0	0	0	157	0.018	-0.637	1922.5	8174	4087	0.626	0.00	0	0	157	0.018	-0.637
4.00	627.47	1.00	500.0	Limestone	35	Normal	0	Closed	Yes	511	512	281	285	0.031	0.537	2082.2	8870	4435	0.546	0.92	6058	3055	798	0.033	0.360
5.00	626.47	1.00	1000.0	Limestone	40	Normal	0	Closed	Yes	513	1025	564	492	0.047	0.703	2196.3	11692	5846	0.686	0.89	8941	4522	1430	0.053	0.448
6.00	625.47	1.00	1000.0	Limestone	40	Normal	44	Closed	Yes	513	1538	846	703	0.061	0.765	2310.4	12346	6173	0.575	0.86	11080	5617	2211	0.072	0.461
7.00	624.47	1.00	2000.0	Limestone	60	Normal	44	Closed	Yes	513	2052	1129	1053	0.066	0.517	2324.5	30035	15018	1.414	0.76	8592	4399	2851	0.083	0.316
8.00	623.47	1.00	2551.0	Limestone	60	Normal	44	Closed	Yes	513	2565	1411	1487	0.076	0.385	2283.5	112091	56046	5.232	0.66	7458	3857	3787	0.101	0.239
9.00	622.47	1.00	2667.0	Limestone	60	Normal	44	Closed	Yes	513	3079	1693	1964	0.087	0.315	2230.9	109509	54755	4.983	0.56	7063	3685	4903	0.124	0.198
10.00	621.47	1.00	2768.0	Limestone	60	Normal	44	Closed	Yes	513	3592	1976	2489	0.099	0.271	2168.2	106431	53216	4.800	0.49	6990	3675	6252	0.150	0.174
11.00	620.47	1.00	2376.0	Limestone	70	Normal	81	Closed	Yes	513	4106	2258	3044	0.103	0.227										
12.00	619.47	1.00	2314.0	Limestone	70	Normal	81	Closed	Yes	513	4619	2541	3650	0.109	0.199										
13.00	618.47	1.00	2049.0	Limestone	70	Normal	81	Closed	Yes	513	5133	2823	4275	0.117	0.183										
14.00	617.47	1.00	2097.0	Limestone	70	Normal	81	Closed	Yes	513	5646	3105	4976	0.126	0.170										
15.00	616.47	1.00	2141.0	Limestone	70	Normal	81	Closed	Yes	513	6160	3388	5764	0.138	0.160										
16.00	615.47	1.00	2141.0	Limestone	70	Normal	81	Closed	Yes	513	6673	3670	6641	0.152	0.153										
17.00	614.47	1.00	2141.0	Limestone	70	Normal	81	Closed	Yes	513	7186	3953	7621	0.167	0.148										
18.00	613.47	1.00	2141.0	Limestone	70	Normal	81	Closed	Yes	513	7700	4235	8719	0.185	0.144										
19.00	612.47	1.00	2141.0	Limestone	70	Normal	81	Closed	Yes	513	8213	4517	9953	0.206	0.141										
20.00	611.47	1.00	2141.0	Limestone	70	Normal	81	Closed	Yes	513	8727	4800	11345	0.229	0.139										

This data is below the bottom of the rock core. This information was extended from the last foot of the core.

Drilled Shaft Design Table for SB Pier 1 & Pier 2 Rock Core 1
Estimated Top of Rock Elevation: 631.47

(Page 1 of 3)

SOCKET DEPTH (FT)	TIP ELEV. (FT)	NOMINAL SHAFT RESIST. (KIPS)	FACTORED SHAFT RESIST. (KIPS)	RESIST. METHOD	SETTLEMENT DATA		
					Q _{C1} (KIPS)	W _{C1} (IN.)	W _{Rn} (IN.)
30 in. Diameter Drilled Shaft							
1	630.47	393	196	TIP	--	--	0.113
2	629.47	1126	563	TIP	--	--	0.285
3	628.47	1586	793	TIP	--	--	0.351
4	627.47	22624	11312	TIP	--	--	4.224
5	626.47	26964	13482	TIP	--	--	4.307
6	625.47	30341	15170	TIP	--	--	3.816
7	624.47	31112	15556	TIP	--	--	3.844
8	623.47	29879	14940	TIP	--	--	3.592
9	622.47	28481	14240	TIP	--	--	3.348
10	621.47	26942	13471	TIP	--	--	3.102
11	620.47	26365	13182	TIP	--	--	3.167
12	619.47	25940	12970	TIP	--	--	3.245
13	618.47	26166	13083	TIP	--	--	3.404
14	617.47	26274	13137	TIP	--	--	3.549
15	616.47	26274	13137	TIP	--	--	3.673
16	615.47	3336	1835	SIDE	5658	0.242	0.105
17	614.47	3593	1976	SIDE	7102	0.298	0.107
18	613.47	3850	2117	SIDE	8997	0.372	0.110
19	612.47	4107	2259	SIDE	11564	0.472	0.114
20	611.47	4363	2400	SIDE	15198	0.615	0.119
36 in. Diameter Drilled Shaft							
1	630.47	718	359	TIP	--	--	0.154
2	629.47	1978	989	TIP	--	--	0.376
3	628.47	2555	1277	TIP	--	--	0.438
4	627.47	3085	1543	TIP	--	--	0.435
5	626.47	39354	19677	TIP	--	--	4.739
6	625.47	43224	21612	TIP	--	--	4.167
7	624.47	43369	21684	TIP	--	--	4.117
8	623.47	42032	21016	TIP	--	--	3.897
9	622.47	40482	20241	TIP	--	--	3.695
10	621.47	38636	19318	TIP	--	--	3.439
11	620.47	37944	18972	TIP	--	--	3.526
12	619.47	37434	18717	TIP	--	--	3.592
13	618.47	37705	18853	TIP	--	--	3.748
14	617.47	37835	18917	TIP	--	--	3.909
15	616.47	3696	2033	SIDE	4660	0.172	0.113
16	615.47	4004	2202	SIDE	5652	0.202	0.111
17	614.47	4312	2372	SIDE	6861	0.239	0.111
18	613.47	4620	2541	SIDE	8353	0.286	0.112
19	612.47	4928	2710	SIDE	10224	0.344	0.114
20	611.47	5236	2880	SIDE	12618	0.420	0.117
42 in. Diameter Drilled Shaft							
1	630.47	1179	590	TIP	--	--	0.209
2	629.47	3061	1531	TIP	--	--	0.480
3	628.47	3764	1882	TIP	--	--	0.513
4	627.47	4293	2147	TIP	--	--	0.482
5	626.47	5826	2913	TIP	--	--	0.572
6	625.47	57469	28735	TIP	--	--	4.453
7	624.47	57802	28901	TIP	--	--	4.390
8	623.47	56394	28197	TIP	--	--	4.217
9	622.47	54586	27293	TIP	--	--	4.027
10	621.47	52432	26216	TIP	--	--	3.778
11	620.47	51624	25812	TIP	--	--	3.842
12	619.47	51030	25515	TIP	--	--	3.937
13	618.47	51346	25673	TIP	--	--	4.112
14	617.47	3952	2174	SIDE	4088	0.137	0.128



**DRILLED SHAFT AXIAL CAPACITY IN ROCK -
DOLOMITE, LIMESTONE, SANDSTONE,
AND HARD SHALE**

Drilled Shaft Design Table for SB Pier 1 & Pier 2 Rock Core 1

Estimated Top of Rock Elevation: 631.47

(Page 2 of 3)

SOCKET DEPTH (FT)	TIP ELEV. (FT)	NOMINAL SHAFT RESIST. (KIPS)	FACTORED SHAFT RESIST. (KIPS)	RESIST. METHOD	SETTLEMENT DATA		
					Q _{C1} (KIPS)	w _{C1} (IN.)	w _{Rn} (IN.)
15	616.47	4312	2371	SIDE	4877	0.156	0.123
16	615.47	4671	2569	SIDE	5801	0.179	0.120
17	614.47	5031	2767	SIDE	6892	0.207	0.118
18	613.47	5390	2964	SIDE	8188	0.240	0.117
19	612.47	5749	3162	SIDE	9743	0.281	0.118
20	611.47	6109	3360	SIDE	11630	0.330	0.120
48 in. Diameter Drilled Shaft							
1	630.47	1743	871	TIP	--	--	0.250
2	629.47	4384	2192	TIP	--	--	0.561
3	628.47	5085	2542	TIP	--	--	0.557
4	627.47	5682	2841	TIP	--	--	0.517
5	626.47	7540	3770	TIP	--	--	0.586
6	625.47	8025	4013	TIP	--	--	0.517
7	624.47	74468	37234	TIP	--	--	4.720
8	623.47	72857	36429	TIP	--	--	4.565
9	622.47	70792	35396	TIP	--	--	4.329
10	621.47	68330	34165	TIP	--	--	4.118
11	620.47	67407	33703	TIP	--	--	4.183
12	619.47	66727	33364	TIP	--	--	4.270
13	618.47	4106	2258	SIDE	3694	0.119	0.151
14	617.47	4517	2484	SIDE	4367	0.131	0.141
15	616.47	4928	2710	SIDE	5144	0.147	0.134
16	615.47	5338	2936	SIDE	6036	0.166	0.130
17	614.47	5749	3162	SIDE	7064	0.188	0.127
18	613.47	6160	3388	SIDE	8254	0.214	0.125
19	612.47	6571	3614	SIDE	9641	0.244	0.124
20	611.47	6981	3840	SIDE	11269	0.280	0.124
54 in. Diameter Drilled Shaft							
1	630.47	2413	1207	TIP	--	--	0.277
2	629.47	5801	2901	TIP	--	--	0.610
3	628.47	6581	3290	TIP	--	--	0.596
4	627.47	7180	3590	TIP	--	--	0.570
5	626.47	9494	4747	TIP	--	--	0.621
6	625.47	10070	5035	TIP	--	--	0.579
7	624.47	93235	46617	TIP	--	--	5.070
8	623.47	91423	45712	TIP	--	--	4.859
9	622.47	89099	44550	TIP	--	--	4.675
10	621.47	86329	43165	TIP	--	--	4.484
11	620.47	85291	42646	TIP	--	--	4.537
12	619.47	4157	2286	SIDE	3377	0.109	0.181
13	618.47	4619	2541	SIDE	3981	0.117	0.167
14	617.47	5081	2795	SIDE	4665	0.128	0.156
15	616.47	5544	3049	SIDE	5444	0.141	0.147
16	615.47	6006	3303	SIDE	6322	0.157	0.141
17	614.47	6468	3557	SIDE	7317	0.175	0.137
18	613.47	6930	3811	SIDE	8447	0.197	0.134
19	612.47	7392	4066	SIDE	9738	0.221	0.132
20	611.47	7854	4320	SIDE	11219	0.250	0.131
60 in. Diameter Drilled Shaft							
1	630.47	3122	1561	TIP	--	--	0.342
2	629.47	7389	3694	TIP	--	--	0.640
3	628.47	8174	4087	TIP	--	--	0.626
4	627.47	8870	4435	TIP	--	--	0.546
5	626.47	11692	5846	TIP	--	--	0.686
6	625.47	12346	6173	TIP	--	--	0.575
7	624.47	30035	15018	TIP	--	--	1.414
8	623.47	112091	56046	TIP	--	--	5.232



**DRILLED SHAFT AXIAL CAPACITY IN ROCK -
DOLOMITE, LIMESTONE, SANDSTONE,
AND HARD SHALE**

Drilled Shaft Design Table for SB Pier 1 & Pier 2 Rock Core 1

Estimated Top of Rock Elevation: 631.47

(Page 3 of 3)

SOCKET DEPTH (FT)	TIP ELEV. (FT)	NOMINAL SHAFT RESIST. (KIPS)	FACTORED SHAFT RESIST. (KIPS)	RESIST. METHOD	SETTLEMENT DATA		
					Q _{C1} (KIPS)	w _{C1} (IN.)	w _{Rn} (IN.)
9	622.47	109509	54755	TIP	--	--	4.983
10	621.47	106431	53216	TIP	--	--	4.800
11	620.47	4106	2258	SIDE	3044	0.103	0.227
12	619.47	4619	2541	SIDE	3650	0.109	0.199
13	618.47	5133	2823	SIDE	4275	0.117	0.183
14	617.47	5646	3105	SIDE	4976	0.126	0.170
15	616.47	6160	3388	SIDE	5764	0.138	0.160
16	615.47	6673	3670	SIDE	6641	0.152	0.153
17	614.47	7186	3953	SIDE	7621	0.167	0.148
18	613.47	7700	4235	SIDE	8719	0.185	0.144
19	612.47	8213	4517	SIDE	9953	0.206	0.141
20	611.47	8727	4800	SIDE	11345	0.229	0.139