

INTERIOR GIRDER MOMENT TABLE					
	0.4 Sp. 1	Pier 1	0.5 Sp. 2	Pier 2	0.6 Sp. 3
$I_x$	(in <sup>4</sup> ) 17429	32995	22116	32995	17429
$I_x(n)$	(in <sup>4</sup> ) 40581	-	48002	-	40581
$I_x(3n)$	(in <sup>4</sup> ) 30457	-	36091	-	30457
$S_x$	(in <sup>3</sup> ) 677	1242	851	1242	677
$S_x(n)$	(in <sup>3</sup> ) 911	-	1097	-	911
$S_x(3n)$	(in <sup>3</sup> ) 837	-	1013	-	837
$\rho$	(K <sup>2</sup> ) 0.766	1.291	0.794	1.291	0.766
$M_D$	(K) 288	1288	458	1187	217
$s_D$	(K <sup>2</sup> ) 0.435	-	0.435	-	0.435
$M_{D1}$	(K) 189	-	294	-	143
$M_L$	(K) 552	505	670	481	499
$M_I$	(K) 132	113	141	109	124
$S_x(M_L + M_I)$	(K) 1140	1130	1352	983	1038
$M_s$	(K) 2102	3013	2735	2821	1818
$M_u$	(K) 3386	-	3877	-	3386
$f_s$ non-comp	(ksi) 5.1	12.4	6.5	11.5	3.8
$f_s$ comp	(ksi) 2.7	-	3.5	-	2.1
$f_s$ (M <sub>L</sub> + M <sub>I</sub> )	(ksi) 15.0	10.0	14.8	9.5	13.7
$f_s$ (Overload)	(ksi) 22.8	22.4	24.7	21.0	19.6
$f_s$ (Total)	(ksi) -	29.1	-	27.3	-
VR	(K) 47.1	-	42.7	-	48.4

INTERIOR GIRDER REACTION TABLE				
	S. Abut.	Pier 1	Pier 2	N. Abut.
R <sub>R</sub>	(K) 34.2	137.5	131.7	28.6
R <sub>L</sub>	(K) 34.8	54.2	53.0	34.5
R <sub>I</sub>	(K) 8.4	11.9	12.2	8.6
R <sub>Total</sub>	(K) 77.4	203.6	196.9	71.7

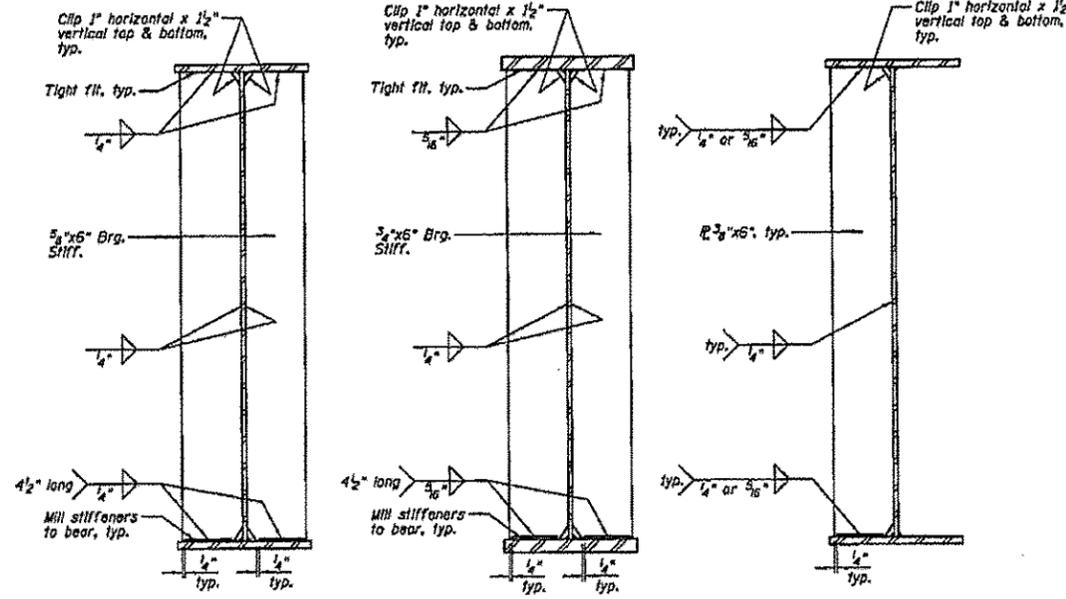
• Compact sections  
 •• Non-Compact and slender sections

$I_x, S_x$ : Non-composite moment of inertia and section modulus of the steel section used for computing  $f_s$  (Total and Overload) due to non-composite dead loads (in<sup>4</sup> and in<sup>3</sup>).  
 $I_x(n), S_x(n)$ : Composite moment of inertia and section modulus of the steel and deck based upon the modular ratio, "n", used for computing  $f_s$  (Total and Overload) due to short-term composite live loads (in<sup>4</sup> and in<sup>3</sup>).  
 $I_x(3n), S_x(3n)$ : Composite moment of inertia and section modulus of the steel and deck based upon 3 times the modular ratio, "3n", used for computing  $f_s$  (Total and Overload) due to long-term composite (superimposed) dead loads (in<sup>4</sup> and in<sup>3</sup>).  
 $\rho$ : Un-factored non-composite dead load (kips/ft.).  
 $M_D$ : Un-factored moment due to non-composite dead load (kip-ft.).  
 $s_D$ : Un-factored long-term composite (superimposed) dead load (kips/ft.).  
 $M_{D1}$ : Un-factored moment due to long-term composite (superimposed) dead load (kip-ft.).  
 $M_L$ : Un-factored live load moment (kip-ft.).  
 $M_I$ : Un-factored moment due to impact (kip-ft.).  
 $M_{D1}$ : Factored design moment (kip-ft.).  
 $1.3 [M_D + M_{D1} + \frac{1}{2} (M_L + M_I)]$   
 $M_u$ : Compact composite moment capacity according to AASHTO LFD 10.50.1.1 or compact non-composite moment capacity according to AASHTO LFD 10.48.1 (kip-ft.).  
 $f_s$  (Overload): Sum of stresses as computed from the moments below (ksi).  
 $M_R + M_{D1} + \frac{1}{2} (M_L + M_I)$   
 $f_s$  (Total): Sum of stresses as computed from the moments below on non-compact section (ksi).  
 $1.3 [M_R + M_{D1} + \frac{1}{2} (M_L + M_I)]$   
 VR: Maximum + impact horizontal shear range within the composite portion of the span for stud shear connector design (kips).

EXTERIOR GIRDER MOMENT TABLE					
	0.4 Sp. 1	Pier 1	0.5 Sp. 2	Pier 2	0.6 Sp. 3
$I_x$	(in <sup>4</sup> ) 18080	29968	22767	29968	18080
$I_x(n)$	(in <sup>4</sup> ) 42305	-	49613	-	42305
$I_x(3n)$	(in <sup>4</sup> ) 31445	-	37009	-	31445
$S_x$	(in <sup>3</sup> ) 702	1136	876	1136	702
$S_x(n)$	(in <sup>3</sup> ) 961	-	1146	-	961
$S_x(3n)$	(in <sup>3</sup> ) 875	-	1051	-	876
$\rho$	(K <sup>2</sup> ) 0.845	1.348	0.873	1.348	0.845
$M_D$	(K) 324	1348	520	1244	245
$s_D$	(K <sup>2</sup> ) 0.435	-	0.435	-	0.435
$M_{D1}$	(K) 190	-	302	-	146
$M_L$	(K) 521	464	642	441	471
$M_I$	(K) 125	104	134	100	117
$S_x(M_L + M_I)$	(K) 1077	947	1293	902	980
$M_s$	(K) 2068	2983	2750	2789	1782
$M_u$	(K) 4983	-	5705	-	4983
$f_s$ non-comp	(ksi) 5.5	14.2	7.1	13.1	4.2
$f_s$ comp	(ksi) 2.6	-	3.4	-	2.0
$f_s$ (M <sub>L</sub> + M <sub>I</sub> )	(ksi) 13.4	10.0	13.5	9.5	12.2
$f_s$ (Overload)	(ksi) 21.6	24.2	24.1	22.7	18.4
$f_s$ (Total)	(ksi) -	31.5	-	29.5	-
VR	(K) 44.2	-	40.1	-	45.4

EXTERIOR GIRDER REACTION TABLE				
	S. Abut.	Pier 1	Pier 2	N. Abut.
R <sub>R</sub>	(K) 36.7	145.6	139.5	30.8
R <sub>L</sub>	(K) 32.8	50.9	49.8	32.5
R <sub>I</sub>	(K) 7.9	11.2	11.5	8.1
R <sub>Total</sub>	(K) 77.4	207.7	200.8	71.4

• Compact sections  
 •• Non-Compact and slender sections

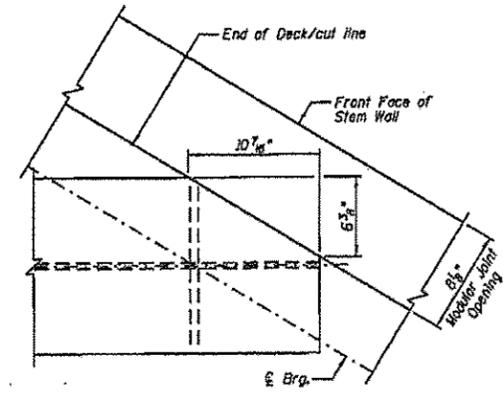


SECTION • ABUTMENTS

SECTION • PIERS

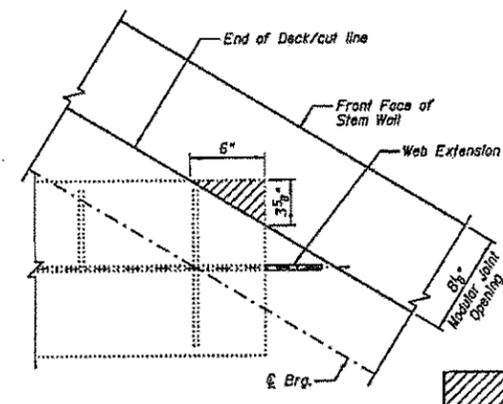
SECTION • CROSS FRAME CF2

Note: Connecting plate not required on outside face of plate girder.



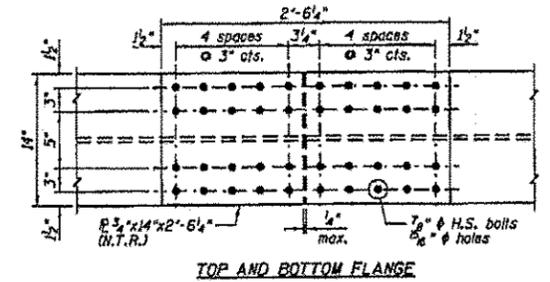
SECTION D-D

Note: Top Flange only.

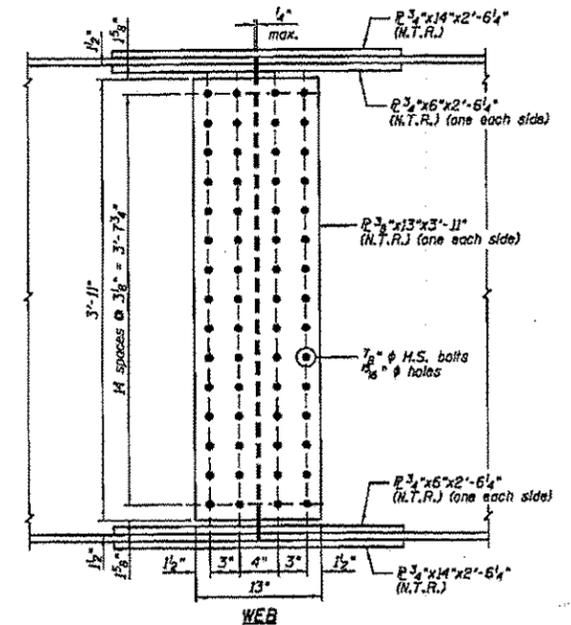


SECTION E-E

Note: Top Flange only.



TOP AND BOTTOM FLANGE



SPLICE DETAILS

(8 - Required)

NOTES:

- 1.) Load carrying components designated N.T.R. shall conform to the Supplemental Requirements for Notch Toughness, Zone 2.
- 2.) All girder flange plates, web plates, splice plates and bearing stiffener plates shall be AASHTO M270 Grade 50.
- 3.) See Sheet B23 for Sections D-D and E-E locations.

STRUCTURAL STEEL  
 STRUCTURE NO.084-0028

FOR INFORMATION ONLY

FILE NAME: c:\documents and settings\mcdonald-s\desktop\plansheet.dgn	USER NAME: mcdonald-s	DESIGNED: -	REVISED: -	STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION	STRUCTURAL STEEL	F.A.I. RTE. SS	SECTION DE PAINTING 2013	COUNTY SANGAMON	TOTAL SHEETS 26	SHEET NO. 9		
PLOT SCALE: = 1/8" = 1'-0"	PLOT DATE: Nov-28-2012 3:28:28PM	DRAWN: -	REVISED: -			SCALE: -	SHEET OF SHEETS STA. TO STA.	ILLINOIS FLD. AID PROJECT				
		CHECKED: -	REVISED: -									
		DATE: -	REVISED: -									