

STRUCTURE GEOTECHNICAL REPORT

ILLINOIS ROUTE 141 OVER
DRAINAGE DITCH
FAP ROUTE 877, SECTION 101B-3
EXISTING STRUCTURE 097-0064
PROPOSED STRUCTURE 097-2016
WHITE COUNTY, ILLINOIS
JOB NO. D-99-041-11
PTB 154-056

Prepared For:
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TSi Project Number 20111018.07



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STRUCTURE GEOTECHNICAL REPORT
(FAP 877) ILLINOIS ROUTE 141 OVER DRAINAGE DITCH
WHITE COUNTY, ILLINOIS

1.0 PROJECT DESCRIPTION AND PROPOSED STRUCTURE INFORMATION

1.1 INTRODUCTION

This report summarizes the results of a geotechnical investigation performed for the design of a replacement structure for an existing bridge on Illinois Route 141 over a drainage ditch 3 miles west of New Haven, White County, Illinois. The purpose of this study was to provide a geotechnical assessment of the planned replacement structure, based on subsurface conditions encountered at two borings performed by the Illinois Department of Transportation (IDOT) at the existing bridge. This report describes the exploration procedures used, presents the field and laboratory data, includes an assessment of the subsurface conditions in the area, and provides geotechnical recommendations for the construction.

1.2 PROJECT DESCRIPTION

The project consists of the removal and replacement of the existing bridge on Illinois Route 141 over a drainage ditch in White County, Illinois. The existing bridge is a 22-foot long, single-span concrete slab bridge supported by spread footings on timber piles. It is to be replaced with a new double box culvert with new guardrails and terminals along with minor earthwork and some resurfacing of existing pavements near the structure. The existing bridge will be removed in two stages, with one lane being open to traffic at all times. The bridge is located on Illinois Route 141 about 3 miles west of New Haven, at Station 352+76. The general site area is shown on the attached Vicinity Map, Figure 1 in Appendix A. A plan that shows the locations of the borings performed for this study is presented as the Site and Boring Location Plan, Figure 2 in Appendix A.

1.3 PROPOSED STRUCTURE INFORMATION

The proposed structure will be a double box culvert. The new culvert will be approximately 35 feet long, providing 12-foot driving lanes and 4-foot shoulders on each side. It will be approximately 26.5 feet wide. The proposed culvert centerline station will be 352+76. The culvert will have two barrels that each measure 12 feet in width and 7 feet in height, with 10-inch thick vertical walls, a 15-inch thick base slab and a 12-inch thick deck slab. Wing walls at 45 degrees to the bridge alignment will be approximately 13.25 feet in length, and will be cantilevered off the culvert. The dead loads imposed by the proposed structure are estimated to be approximately 950 kips. A copy of the current TS&L drawing is included in Appendix D. Present plans are to leave the existing pile-supported bridge abutment footings in place, where they will underlie the new box culvert. The footing segments supporting the wing walls will be removed.

2.0 SUBSURFACE EXPLORATION

The field exploration for this project was conducted by IDOT. The exploration consisted of completing two soil borings within the roadway pavement, with one boring on the east side and one on the west side of the existing bridge. The borings were designated as Borings 1-S and 2-S. The approximate locations of the borings are shown on the Site and Boring Location Plan, Figure 2 in Appendix A.

The two borings for this study were completed on August 23 and 24, 2011. Boring 1-S was located just east of the existing bridge at Station 352+97 and offset 10 feet right of the roadway centerline. Boring 2-S was located just west of the existing bridge at Station 352+51 and offset 10 feet left of the centerline. Each boring was augered through the pavement section and base rock, and then advanced into intact bedrock at depths ranging from 46.0 to 47.5 feet. Split-spoon (SPT) samples were obtained on 2.5-foot centers in the overburden soils. The sampling sequence for each boring is summarized on the Boring Logs in Appendix B of this report. A Subsurface Profile is provided as Figure 3 in Appendix A.

3.0 SUBSURFACE CONDITIONS

Details of the subsurface conditions encountered at the borings are shown on the Boring Logs. The general subsurface conditions encountered and their pertinent engineering characteristics are described in the following paragraphs. Conditions represented by the borings should be considered applicable only at the boring locations on the dates shown; the reported conditions may be different at other locations at other times.

3.1 GEOLOGY

The site lies in the Saline Watershed within the Mt. Vernon Hill Country portion of the Till Plains Section of the Central Lowland Physiographic Province. The watershed encompasses the Saline River which flows in a southeastern direction toward the Wabash River. The general geology at the project site appears to be Quaternary sand, silt, loam, and clay till and outwash deposits left by the glaciers of the Illinois Glacial Episode, underlain by Pennsylvanian and Permian sedimentary bedrock including shale, sandstone, and limestone. Thin coal deposits are also possible across Gallatin and White Counties. Geologic mapping by Illinois State Geologic Survey (ISGS) indicates the site is underlain by lakebed deposits of silt and clay laid down in glacial and early post-glacial time. These deposits would have formed an essentially level surface that has been subsequently crossed with erosion channels.

3.2 GENERALIZED SUBSURFACE PROFILE

The soils in the area are mainly lean and fat clays with occasional silt layers (A-6, A-7-6, and A-4 as defined by the AASHTO Classification System) that are typically soft to stiff throughout the soil profile. Standard penetration test values (N) in the soil range from 1 to 10 blows per foot (bpf). Unconfined compression tests were performed with a Rimac machine on the soils at each boring. The Rimac tests resulted in values ranging from 0.2 to 1.7 tons per square foot (tsf). Moisture contents in the soils vary from 20 to 35%.

Shale bedrock was encountered beneath the soils at a depth of approximately 44.5 feet in Boring 1-S and 46.5 feet in Boring 2-S. The shale is gray and highly to moderately weathered in the upper 1 to 3 feet of the formation. The moisture content of the highly weathered upper shale was 19% in Boring 1-S at a depth of 45.5 feet.

3.3 GROUNDWATER

Groundwater was encountered at 24.5 feet in Boring 1-S and 27 feet in Boring 2-S. The presence or absence of groundwater at a particular location does not necessarily mean that groundwater will be present or absent at that location at other times. Seasonal variations, the water level in the adjacent drainage ditch, and other unknown considerations could cause fluctuations in water levels and the presence of water in the soils. The elevation of the surface water in the ditch during the time of drilling was recorded at 382.8 on the boring logs.

4.0 GEOTECHNICAL EVALUATIONS

4.1 SETTLEMENT

The clay soils present at subgrade level appear to be relatively soft and potentially compressible. A settlement analysis made in general accordance with the IDOT January 1999 Geotechnical Manual, for the 950 kip loading imposed by the completed box culvert, the backfill over the culvert, and the pavement. Accounting for the original ground surface level in the site area, the calculated settlement is less than 2 inches. However, since the existing pile-supported abutment footings will be left in place beneath the culvert, any significant settlement of the foundation soils will result in the partial transfer of the load from the subgrade to the existing footings. The reduction in subgrade load will reduce and eventually halt further settlement, as any greater settlement will result in additional load transfer, further reducing the subgrade loading. A review of the loads imposed on the existing footings by the new structure, in comparison to the design capacity of the existing piles indicates an overload ratio of approximately 1.3. This degree of overload should result in some settlement of the existing footings, but not a failure. A settlement analysis was conducted assuming the existing soils would carry the difference in loading over the design capacity of the existing piles. The resultant settlement was less than ½ inch. On this basis, the overall settlement of the box culvert should be less than 1 inch. This settlement is anticipated to consist of recompression of the foundation soils rather than virgin consolidation, so it should occur rapidly. Consequently, no delay is required before the installation of final pavement.

The results of the borings indicate that the existing soil below the base of the box culvert should be suitable for support of the structure, so that a working mat of granular soil should not be required, provided that care is exercised by the contractor not to disrupt these soils. The existing footings are overlain by backfill, which may not be capable of safely supporting the new culvert. However, TSi understands that the existing bridge structure will be demolished down to the level of the footings. This demolition will likely result in the removal of most or all of the existing backfill, which would be replaced by new compacted fill suitable for structure support.

4.2 SLOPE STABILITY

A slope stability analysis was performed for the new wing walls and the 2 Horizontal to 1 Vertical (2H:1V) side slopes of the roadway utilizing the SLOPE/W 2007 program. In accordance with the IDOT Geotechnical Manual, Section 3.2.3.2, the minimum factor of safety (FOS) required is 1.5 for end-of-construction and long term stability. Analyses of these conditions indicate the slopes and wing walls as designed are within the required minimums, as shown in Table 4.1 below. The output sheets for these analyses are given in Appendix C.

**TABLE 4.1
CALCULATED CRITICAL FACTOR OF SAFETY**

	SLOPE/W Calculated Factor of Safety	
	End-of-Construction	Long Term
Wing Walls	3.4	1.5
Roadway Side Slopes	3.5	1.5

4.3 MINING ACTIVITY

A review of undermining was made using the Illinois State Geological Survey (ISGS) website for mapped coal mines in White and Gallatin Counties, Illinois. Based on this information, the project site is unlikely to be undermined. The nearest coal mines are more than 7 miles away near Norris City and Ridgeway, IL.

5.0 FOUNDATION EVALUATIONS AND DESIGN RECOMMENDATIONS

5.1 BOX CULVERT DESIGN

In accordance with the 2016 IDOT Culvert Manual, either a cast-in-place or a precast box culvert are viable options for the structure replacement. However, due to the stage construction of the culvert and the configuration of the culvert over a portion of the existing foundations, a precast alternate will not be allowed. TSi understands that the existing pile-supported bridge abutment footings will remain in place beneath the planned box culvert, but that the portions of the footings beneath the existing wing walls will be removed. As described in Section 4.1, the settlement of the foundation soils beneath the culvert could result in the structure being supported by the existing pile-supported footings. Consequently, it will be necessary to design the base slab to span between the two footings, and the completed culvert to be at least partially supported by the footings, spanning across the existing substructures. Because the portion of the footings beneath the existing bridge wing walls will be demolished, while the culvert itself will be supported at least partially on the footings, the new wing walls should be cantilevered from the culvert structure to avoid likely differential settlement.

Groundwater seepage and any surface flow into the footing excavation from the drainage ditch must be controlled so that the integrity of the footing bearing surface is maintained. The soils at the site appear to be moisture sensitive and will deteriorate rapidly when saturated. Groundwater control will very likely require the installation of a diversion system, such as a temporary dam at each end of the construction area, with adequate pumping capacity or other means to transfer any surface water flow across the area.

The results of the borings indicate that the existing soil below the base of the box culvert should be suitable for support of the structure, so that a working mat of granular soil should not be required, provided that care is exercised by the contractor not to disrupt these soils. The existing footings are overlain by backfill that may not be suitable for support of the box culvert. However, the existing abutment is to be demolished down to the level of the footings. This demolition should result in the removal of most or all of the existing backfill, which will be replaced with properly compacted new fill.

5.2 LATERAL EARTH PRESSURES

According to the current drawings, the wing walls are approximately 13.25 feet in length and up to 12.8 feet in height. As noted in Section 5.1 above, the wing walls will be horizontally cantilevered from the box culvert structure. The following design parameters are recommended for cohesive backfill materials:

TABLE 5.1

**LATERAL EARTH PRESSURE PARAMETERS
FOR WALLS WITH SURFACES INCLINED NO STEEPER THAN 2H:1V
(2.8H:1V AS MEASURED PERPENDICULAR TO THE WALL FACE)**

Parameter		Cohesive Soil
At-Rest Equivalent Fluid Pressure	Drained	90 pcf
	Undrained	105 pcf
Active Equivalent Fluid Pressure	Drained	65 pcf
	Undrained	95 pcf
Passive Equivalent Fluid Pressure	Drained	155 pcf
	Undrained	75 pcf
Soil Unit Weight		120 pcf
Angle of Internal Friction		25°
Assumed Surcharge Condition		None

No factor of safety has been applied to the values above.
pcf = pounds per cubic foot

Saturated values should be used for the calculation of lateral earth pressures for those portions of the walls that extend below the highest level of anticipated groundwater. The values for saturated fluid pressure for active and at-rest conditions include hydrostatic pressures. The effects of vertical surcharge or seismic loads are not included for the stated fluid pressures. Vertical surcharge effects can be accounted for by assuming an additional horizontal pressure equal to one-half the vertical surcharge pressure.

6.0 CONSTRUCTION CONSIDERATIONS

6.1 TEMPORARY SHEETING AND SOIL RETENTION

The construction activities should be performed in accordance with the current IDOT Standard Specifications for Road and Bridge Construction. Trenching, excavating, and bracing should be performed in accordance with OSHA (Occupational Safety and Health Administration) regulations, and other applicable regulatory agencies. In accordance with the OSHA excavation standards, the soil at the site is considered to be Type C, which requires a side slope for excavations no steeper than 1.5H:1.0V. However, worker safety and classification of the excavation soil is the responsibility of the contractor. Because one lane of the roadway is to remain in service during construction, sloping back the sides of the excavation will likely not be feasible. This will require a retention system such as a cantilever sheet pile wall. A cantilever sheet pile system appears feasible for the subsurface conditions encountered, and may be designed using IDOT Design Guide 3.13.1 – Temporary Sheet Piling Design.

6.2 SUBGRADE WATER PROTECTION

The need to provide a dry excavation for the box culvert is covered in Section 5.1 of this report. Additional shallow trenching and pumping from sumps may be needed to control local groundwater seepage within the construction area.

7.0 REPORT LIMITATIONS

This geotechnical report has been prepared for the exclusive use of **MODJESKI AND MASTERS, INC.** and **THE ILLINOIS DEPARTMENT OF TRANSPORTATION** for the specific application to the subject project. The information and recommendations contained in this report have been made in accordance with generally accepted geotechnical and foundation engineering practices; no other warranties are implied or expressed.

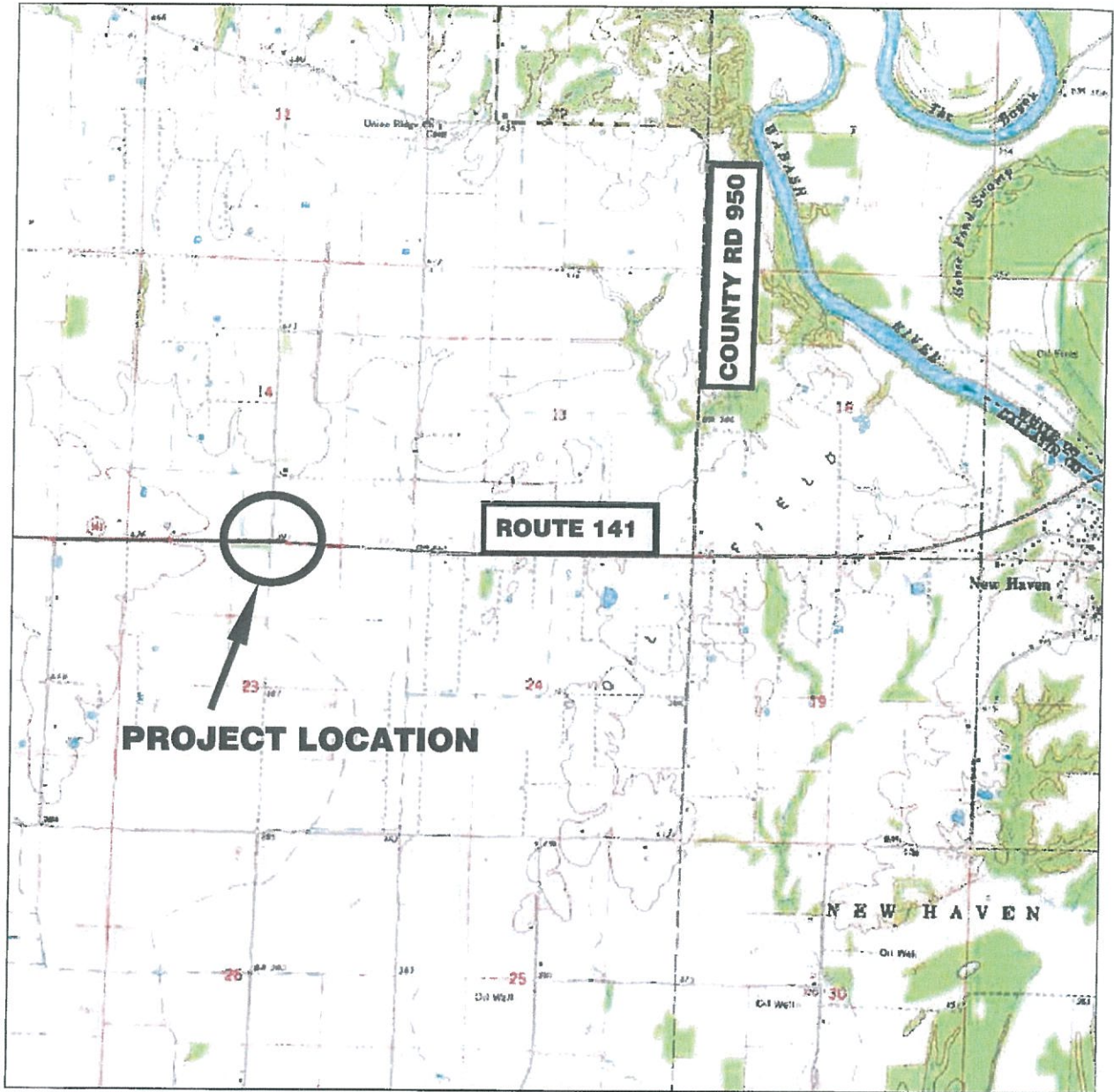
The assessments and recommendations submitted in this report are based in part upon the data obtained from the borings. The nature and extent of variations between the borings may not be evident at this time. If variations appear evident at a later date, it may be necessary to re-evaluate the recommendations of this report.

We emphasize that this report was prepared for design purposes only and may not be sufficient to prepare an accurate construction bid. Contractors reviewing this report should acknowledge that the information and recommendations contained herein are for design purposes.

If conditions at the site have changed due to natural causes or other operations, this report should be reviewed by TSi to determine the applicability of the analysis and recommendations considering the changed conditions. The report should also be reviewed by TSi if changes occur in the structure location, size, and type, in the planned loads, elevations, grading and site development plans or the project concepts.

TSi requests the opportunity to review the final plans and specifications for the project prior to construction to verify that the recommendations in this report are properly interpreted and incorporated in the design and construction documents. If TSi is not accorded the opportunity to make this recommended review, we can assume no responsibility for the misinterpretation of our recommendations.

Appendix A



NOT TO SCALE



NOTE:
DRAWING PREPARED FROM AN IMAGE
OBTAINED FROM TOPOQUEST.COM
ON 7/11/2012



5850 ARSENAL STREET
ST. LOUIS, MISSOURI 63139

VICINITY MAP
FAP (877) ILLINOIS ROUTE 141
OVER DRAINAGE DITCH
WHITE COUNTY, IL

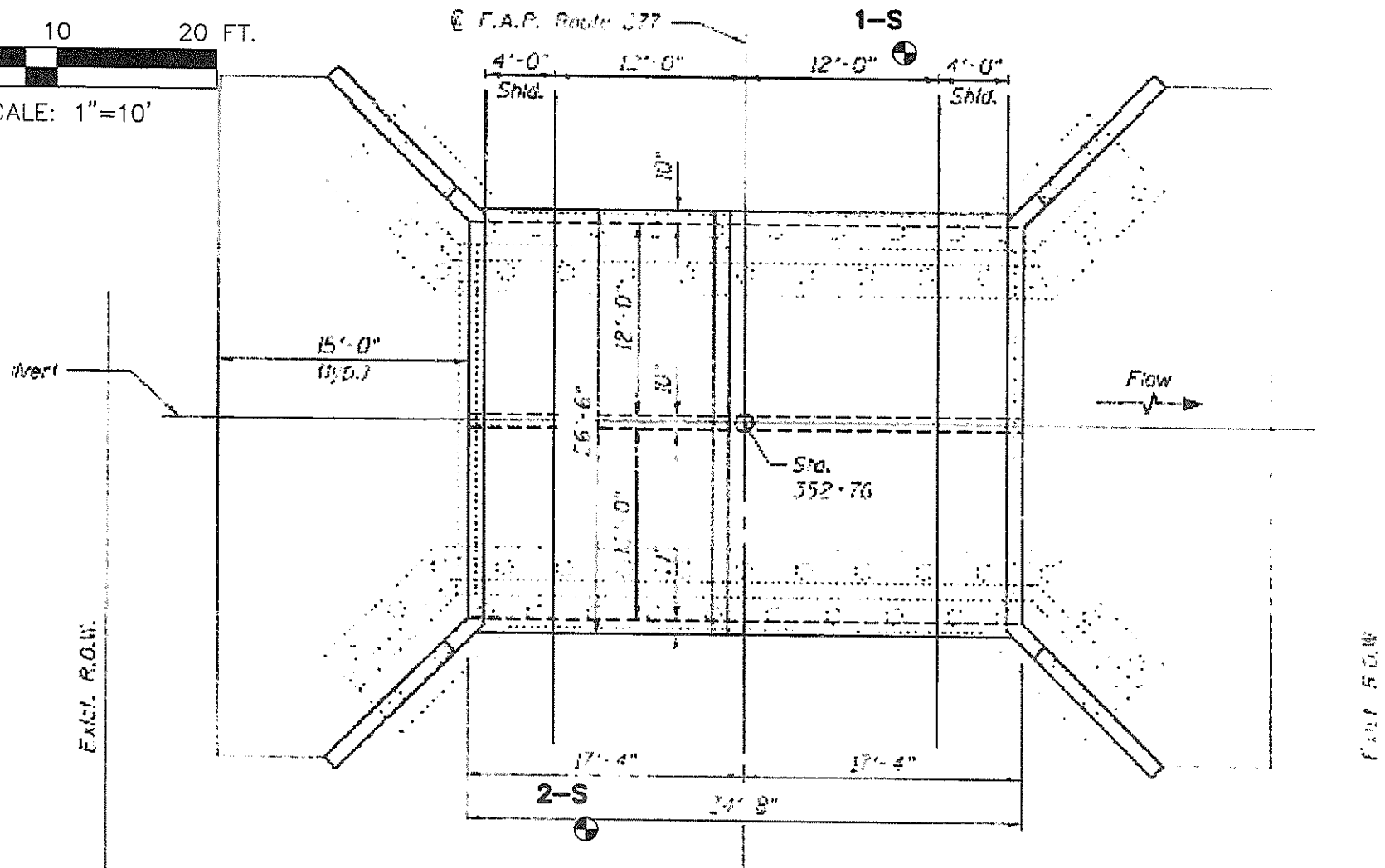
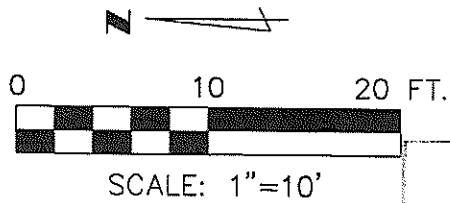
Drawn By: JAS

Checked By: WJG

Project No. 20111018.07

Date: 7/11/12


Figure 1

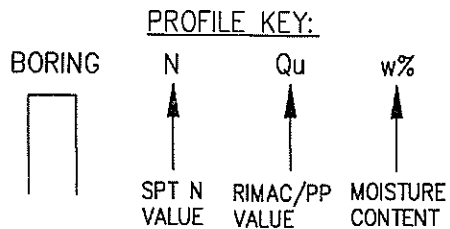
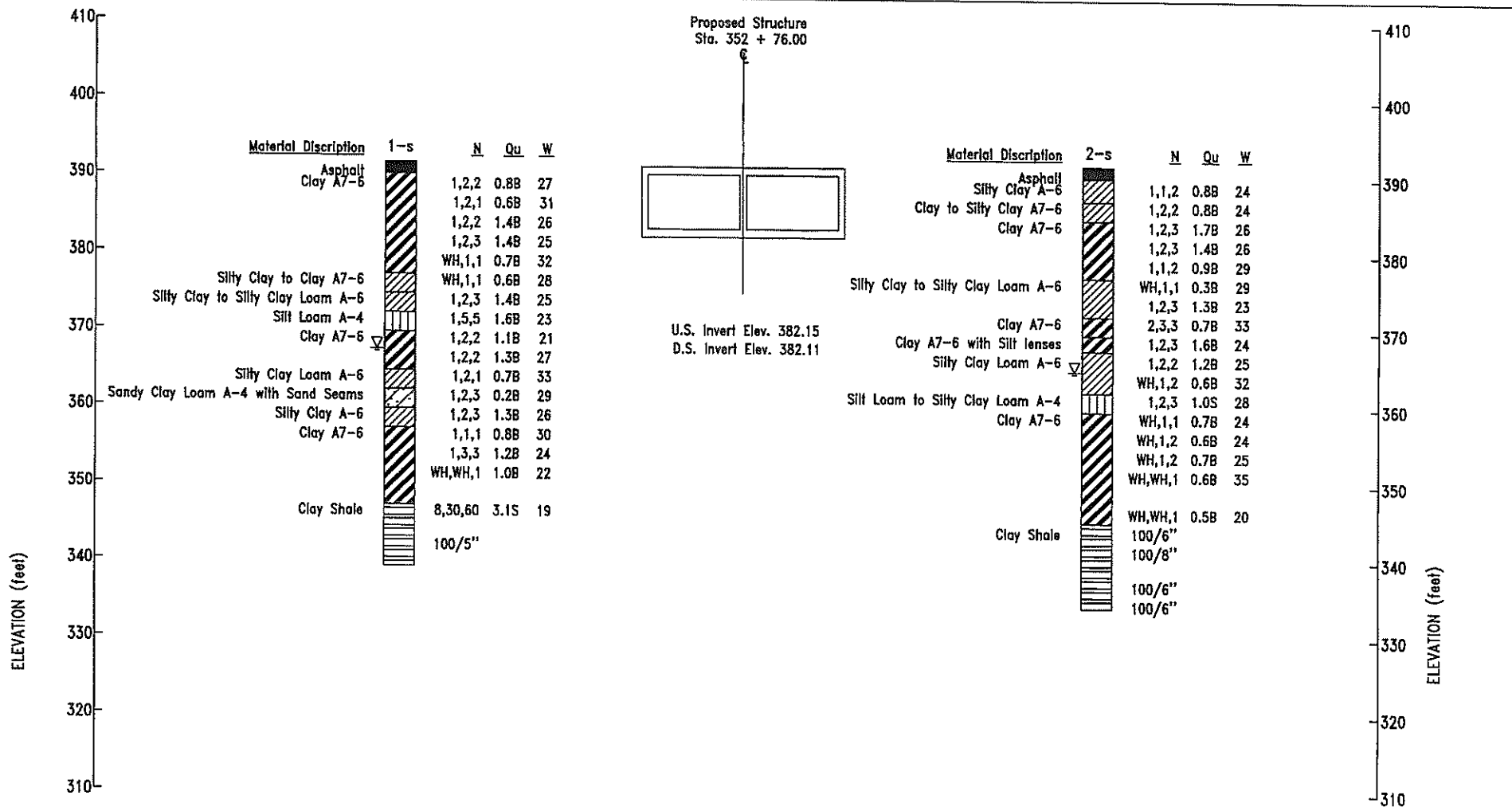


LEGEND

1-S APPROXIMATE BORING LOCATION AND NUMBER

NOTE: THIS PLAN WAS PREPARED FROM A PDF RECEIVED FROM MODJESKI AND MASTERS ON 3-26-12.

 engineering, inc. 5850 ARSENAL STREET ST. LOUIS, MISSOURI 63139	SITE AND BORING LOCATION PLAN ILLINOIS ROUTE 141 OVER DRAINAGE DITCH FAP ROUTE 877 SECTION 101B-3 WHITE COUNTY, ILLINOIS	
	Drawn By: JAS Project No. 20111018.07	Checked By: WJG Date: 7/20/12 Figure 2



VERTICAL SCALE: 1" = 20'

NOTE: THIS PLAN WAS PREPARED FROM DRAWINGS RECEIVED FROM MODJESKI AND MASTERS ON 3-22-13. BORING LOCATIONS SHOWN ON PROFILE ARE APPROXIMATE.

<p>TSI engineering, inc. 5850 ARSENAL STREET ST. LOUIS, MISSOURI 63139</p>	SOIL PROFILE	
	FAP (877) ILLINOIS ROUTE 141 OVER DRAINAGE DITCH WHITE COUNTY, IL	
Drawn By: JAS	Checked By: WJG	
Project No. 20111018.07	Date: 3/27/13	Figure 3

Appendix B

ILLINOIS DEPARTMENT OF TRANSPORTATION
District Nine Materials

Bridge Foundation
Boring Log

FAP 877 (IL 141) Over stream

Sheet 1 of 2

Route: FAP 877 (IL 141) Structure Number: 097-0064

Date: 8/23/2011

Section 101

Bored By: R Moberly

County: White

Location: 3 mi W of New Haven

Checked By: R Graeff

Boring No	DEPT H	BLOW S	Qu tsf	W%	Surf Wat Elev:	DEPT H	BLOW S	Qu tsf	W%
1-S					382.8				
Station 352+97					Ground Water Elevation when Drilling 367.1				
Offset 10' Rt CL					At Completion				
Ground Surface 391.6Ft					At: Hrs:				
Asphalt							2	0.3B	27
390.1							2		
Medium, moist to very moist, grey, Clay A7-6					364.6				
		1			Medium, very moist, grey, Silty Clay Loam A-6		1		
		2	0.8B	27			2	0.7B	33
		2					1		
					362.1				
	5.0	1			Very soft, wet, grey, Sandy Clay Loam A-4 with Sand seams	30.0	1		
		2	0.6B	31			2	0.2B	29
		1					3		
384.6					359.6				
Stiff, moist, grey, Clay A7-6					Stiff, moist, grey, Silty Clay A-6		1		
		1					2	1.3B	26
		2	1.4B	26			3		
		2							
382.1					357.1				
Stiff, moist, grey mottled brown, Clay A7-8	10.0	1			Medium, very moist, grey, Clay A7-6	35.0	1		
		2	1.4B	25			1	0.8B	30
		3					1		
379.6					354.6				
Medium, very moist, grey mottled brown, Clay A7-6		WH			Stiff, moist, grey, Clay A7-6		1		
		1	0.7B	32			3	1.2B	24
		1					3		
377.1					352.1				
Medium, very moist, brown mottled grey, Silty Clay to Clay A7-6	15.0	WH			Medium to stiff, moist to very moist, grey, Clay A7-6	40.0	WH		
		1	0.6B	28			WH	1.0B	22
		1					1		
374.6									
Stiff, moist, grey mottled brown, Silty Clay to Silty Clay Loam A-6									
		1							
		2	1.4B	25					
		3							
372.1					347.1				
Stiff, moist, grey, Silt Loam A-4	20.0	1			Very stiff, damp, grey, Weathered Clay Shale	45.0	8		
		5	1.6S	23			30	3.1S	19
		5					60		
369.6					Hard, damp, brown and grey, Clay Shale				
Stiff, moist, grey, Clay A7-5									
		1							
		2	1.1B	21					
		2							
367.1					Hard, dry, grey, Clay Shale				
Soft, very moist, grey, Clay A7-6	25.0	1					50.0	100/5"	

N-Std Penetr Test: 2" OD Sampler, 140# Hammer, 30" Fall (Type Fall. B-Bulge S-Shear E-Estimated P-Penetrometer)

Route: FAP 877 (IL 141)

Date: 8/23/2011

Section: 101

County: White

Boring No: 1-S

Station: 352+97

Offset: 10' Rt CL

Ground Surface: 391.6 Ft

	DEPTH	BLOWS	Qu tsf	W%		DEPTH	BLOWS	Qu tsf	W%
Hard, dry, grey, Clay Shale									
	339.1								
Boring abandoned due to mechanical breakdown.									
Bottom of hole = 52.5 feet	55.0					80.0			
Free water observed at 24.5 feet									
Elevation referenced to BM 108 at SW corner; Elev. = 391.3 feet									
Borehole advanced with hollow stem auger (8" O.D., 3.25" I.D.)									
To convert "N" values to "N60" multiply by 1.25	60.0					85.0			
	65.0					90.0			
	70.0					95.0			
	75.0					100.0			

N-Std Penetr Test: 2" OD Sampler, 140# Hammer, 30" Fall (Type Fail. B-Bulge S-Shear E-Estimated P-Penetrometer)

Route: EAP 877 (IL 141)

Date: 8/24/2011

Section: 101

County: White

Boring No: 2-S

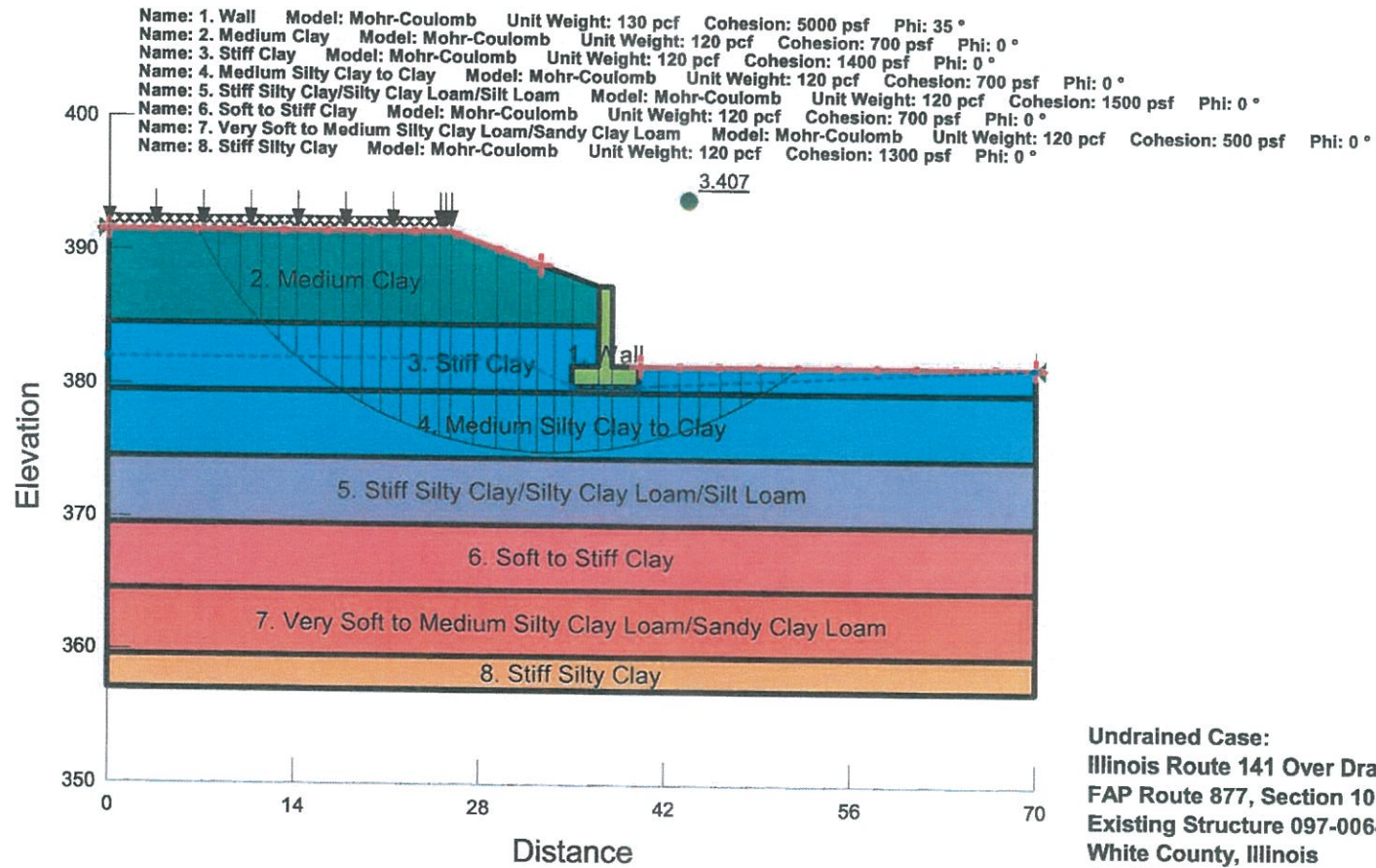
Station: 352+51

Offset: 10' Lt CL

Ground Surface: 391.6 Ft

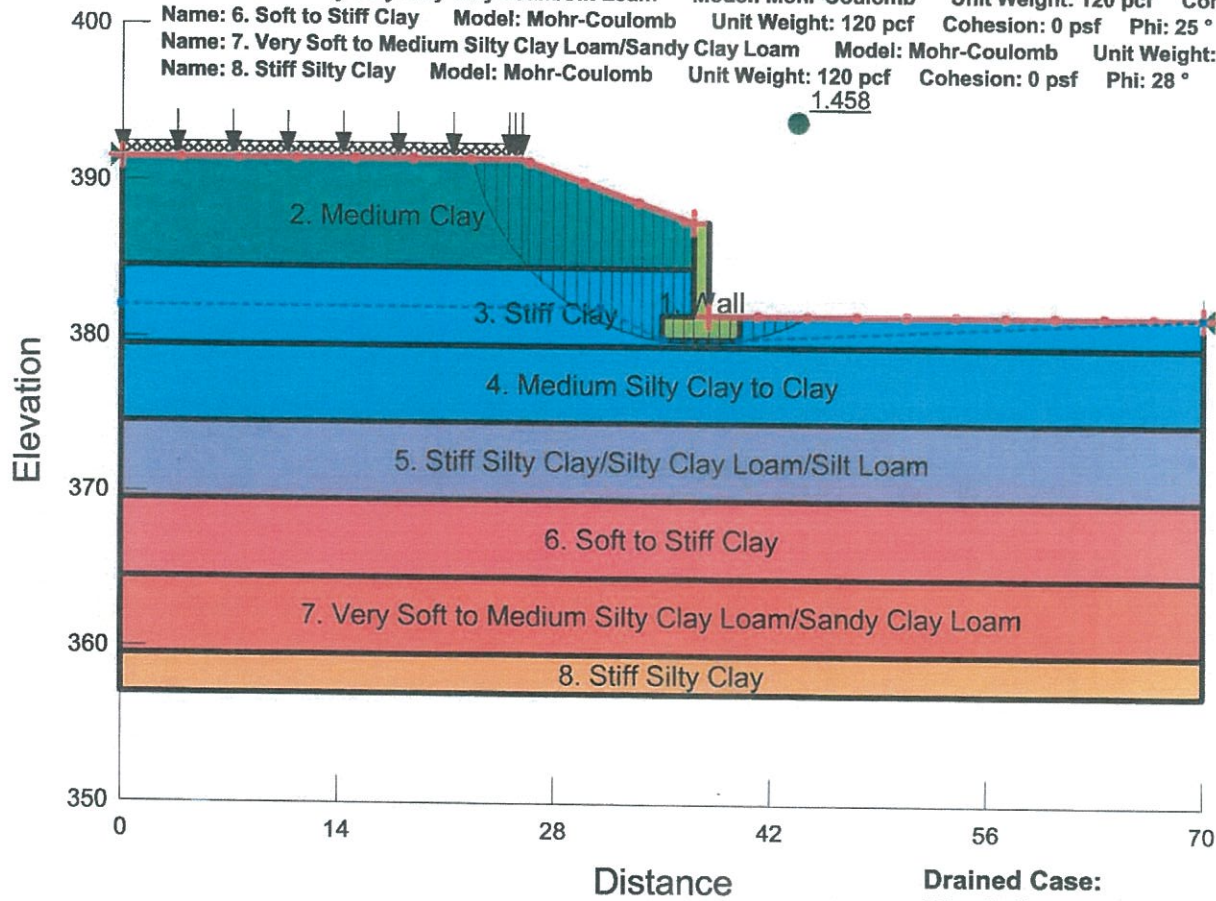
	DEPTH	BLOWS	Qu tsf	W%		DEPTH	BLOWS	Qu tsf	W%
Hard, damp to dry, grey, Clay Shale									
Note: Shale to soft to core									
	55.0	100/6"				80.0			
334.1		100/6"							
Bottom of hole = 57.5 feet									
Free water observed at 27.0 feet	60.0					85.0			
Elevation referenced to BM 108 at SW corner; Elev.= 391.3 feet									
Borehole advanced with hollow stem auger (8" O.D, 3.25" I.D.)									
To convert "N" values to "N60" multiply by 1.25	65.0					80.0			
	70.0					95.0			
	75.0					100.0			

Appendix C



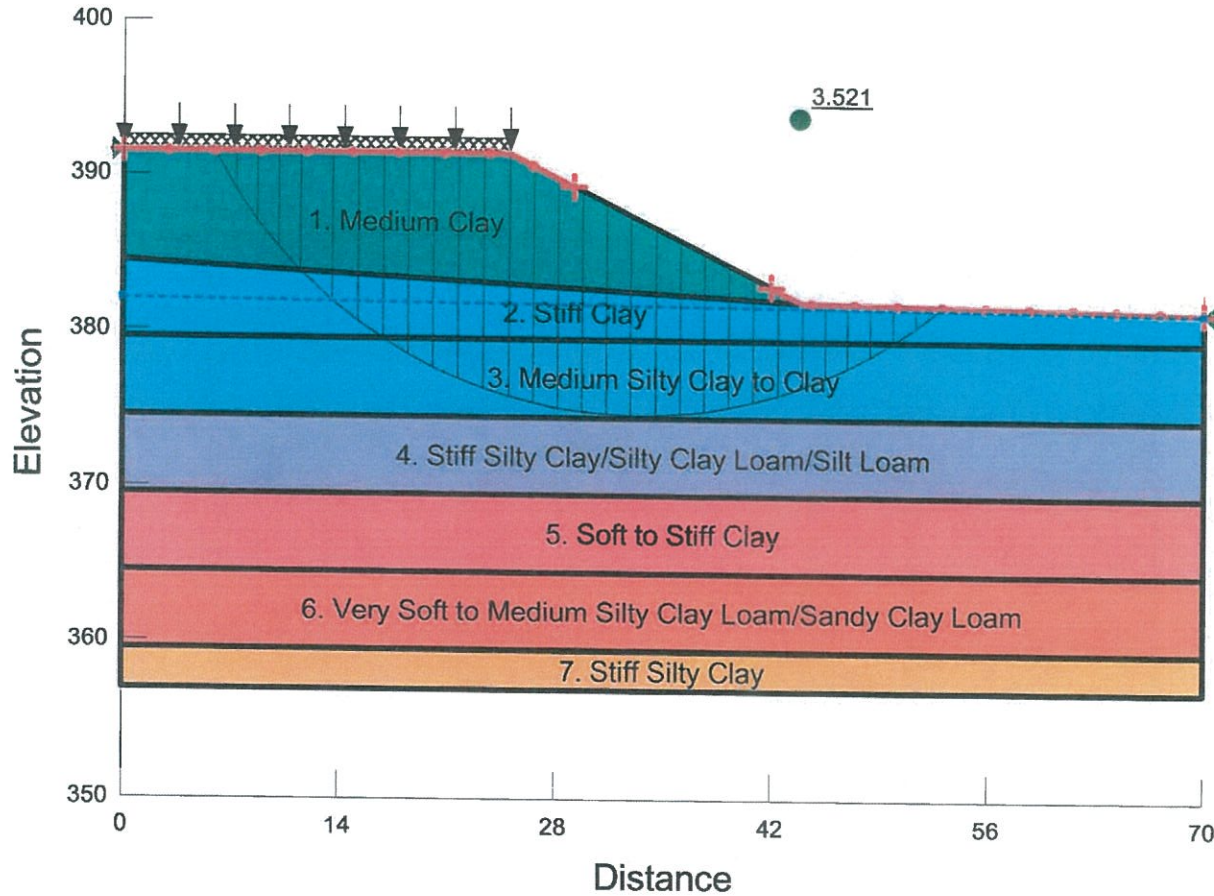
Undrained Case:
 Illinois Route 141 Over Drainage Ditch
 FAP Route 877, Section 101B-3
 Existing Structure 097-0064
 White County, Illinois
 Job No. D-99-041011
 PTB 154-056

- Name: 1. Wall Model: Mohr-Coulomb Unit Weight: 130 pcf Cohesion: 5000 psf Phi: 35 °
- Name: 2. Medium Clay Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion: 50 psf Phi: 26 °
- Name: 3. Stiff Clay Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion: 50 psf Phi: 26 °
- Name: 4. Medium Silty Clay to Clay Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion: 50 psf Phi: 26 °
- Name: 5. Stiff Silty Clay/Silty Clay Loam/Silt Loam Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion: 0 psf Phi: 28 °
- Name: 6. Soft to Stiff Clay Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion: 0 psf Phi: 25 °
- Name: 7. Very Soft to Medium Silty Clay Loam/Sandy Clay Loam Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion: 0 psf Phi: 28 °
- Name: 8. Stiff Silty Clay Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion: 0 psf Phi: 28 °



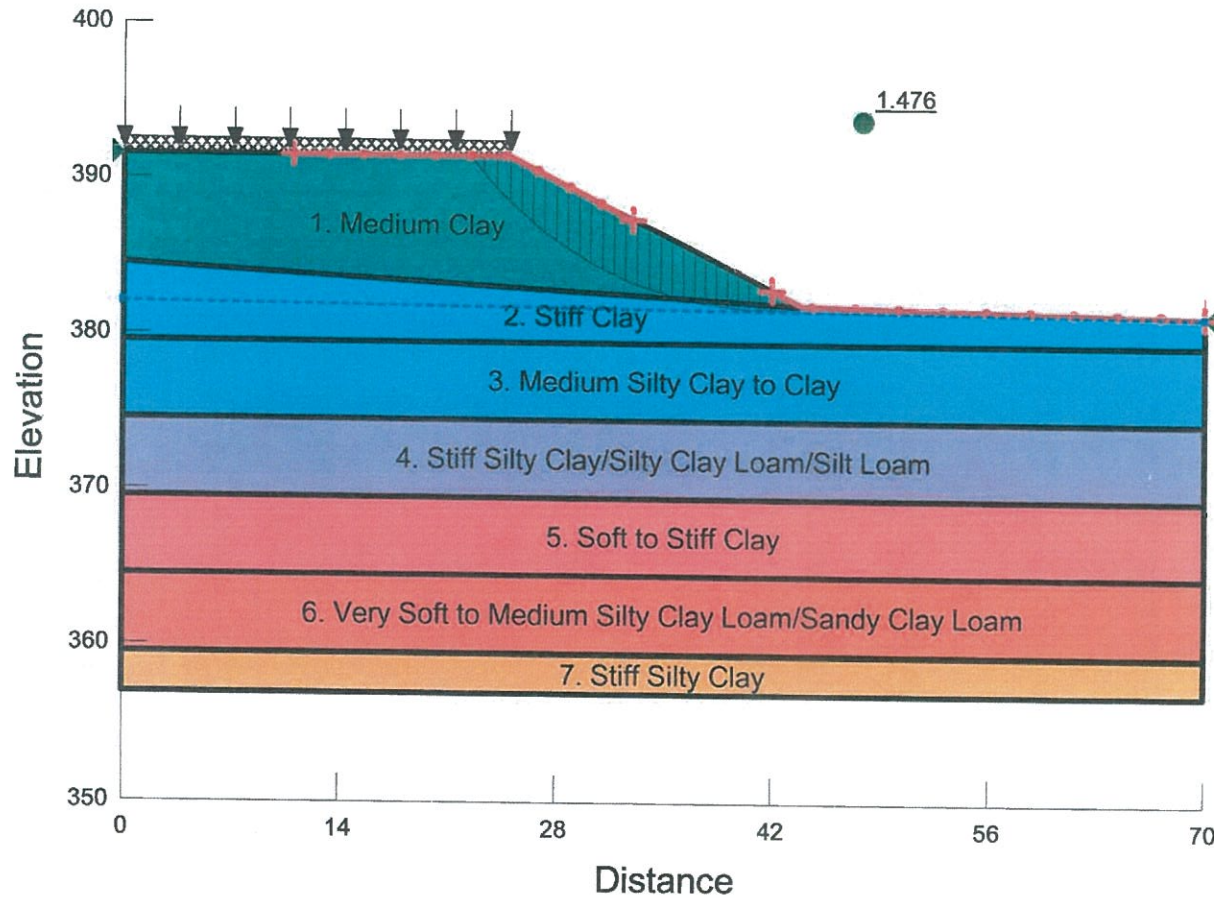
Drained Case:
Illinois Route 141 Over Drainage Ditch
FAP Route 877, Section 101B-3
Existing Structure 097-0064
White County, Illinois
Job No. D-99-041011
PTB 154-056

Name: 1. Medium Clay Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion: 700 psf Phi: 0°
 Name: 2. Stiff Clay Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion: 1400 psf Phi: 0°
 Name: 3. Medium Silty Clay to Clay Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion: 700 psf Phi: 0°
 Name: 4. Stiff Silty Clay/Silty Clay Loam/Silt Loam Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion: 1500 psf Phi: 0°
 Name: 5. Soft to Stiff Clay Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion: 700 psf Phi: 0°
 Name: 6. Very Soft to Medium Silty Clay Loam/Sandy Clay Loam Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion: 500 psf Phi: 0°
 Name: 7. Stiff Silty Clay Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion: 1300 psf Phi: 0°



Undrained Case:
 Illinois Route 141 Over Drainage Ditch
 FAP Route 877, Section 101B-3
 Existing Structure 097-0064
 White County, Illinois
 Job No. D-99-041011
 PTB 154-056

Name: 1. Medium Clay Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion: 50 psf Phi: 26 °
 Name: 2. Stiff Clay Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion: 50 psf Phi: 26 °
 Name: 3. Medium Silty Clay to Clay Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion: 50 psf Phi: 26 °
 Name: 4. Stiff Silty Clay/Silty Clay Loam/Silt Loam Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion: 0 psf Phi: 28 °
 Name: 5. Soft to Stiff Clay Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion: 0 psf Phi: 25 °
 Name: 6. Very Soft to Medium Silty Clay Loam/Sandy Clay Loam Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion: 0 psf Phi: 28 °
 Name: 7. Stiff Silty Clay Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion: 0 psf Phi: 28 °



Drained Case:
 Illinois Route 141 Over Drainage Ditch
 FAP Route 877, Section 101B-3
 Existing Structure 097-0064
 White County, Illinois
 Job No. D-99-041011
 PTB 154-056

Appendix D

Bench Mark: BM 108 - Chiseled square in southwest wingwall of SN 097-0064, Elev. 391.31.

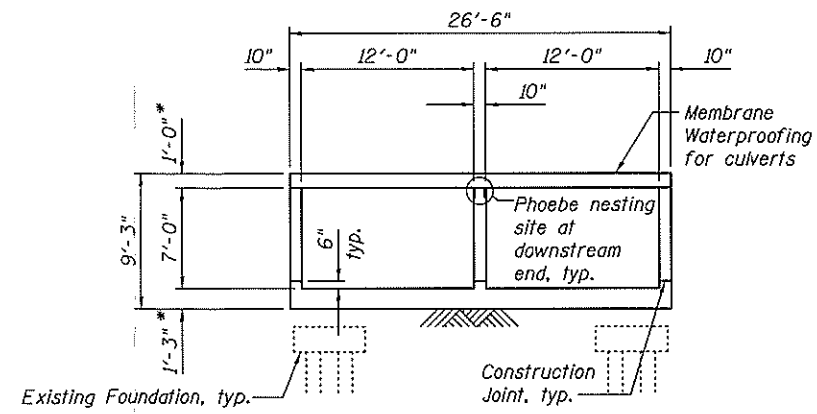
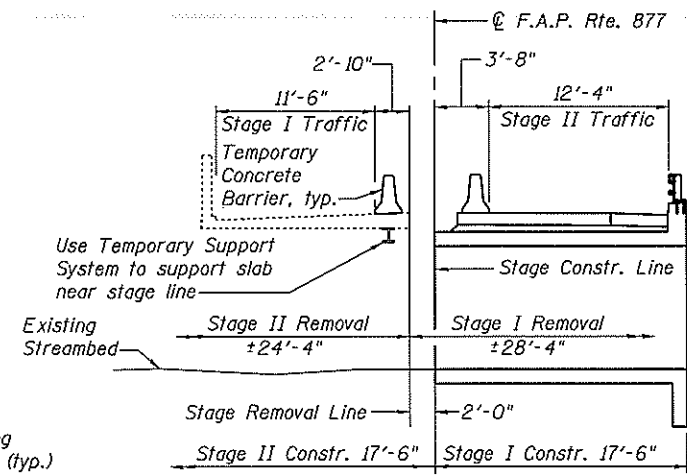
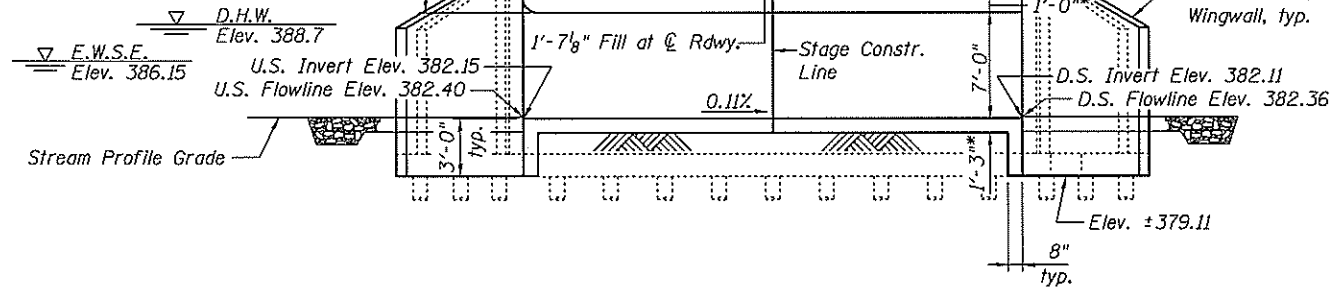
Existing Structure: SN 097-0064 was originally built in 1933 as SBI Route 141 (Section A-101) and resurfaced in 1970 as SBI Route 141 (Section 101W, RS). The existing structure is a 22 foot (back to back abutments) single span reinforced concrete slab bridge. The substructure consists of closed abutments founded on footings on timber piles. The deck measures 32'-8" between curbs and the overall out to out width of the bridge is 36'-2". The existing superstructure and abutment walls are to be removed and replaced. The existing foundation is to remain in place except as noted.

Traffic to be maintained utilizing stage construction.

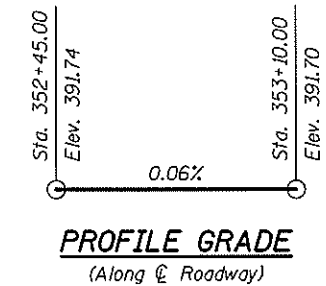
Excavation behind existing abutment walls shall be performed to balance front and back soil pressure before removing the existing superstructure. The Contractor shall sawcut the upper portion of the existing abutment at the stage removal line before Stage I removal to ensure the remaining portion will not be prematurely damaged.

No salvage.

Precast alternate is not allowed.



*Slab thickness is subject to refinement during Final Design.

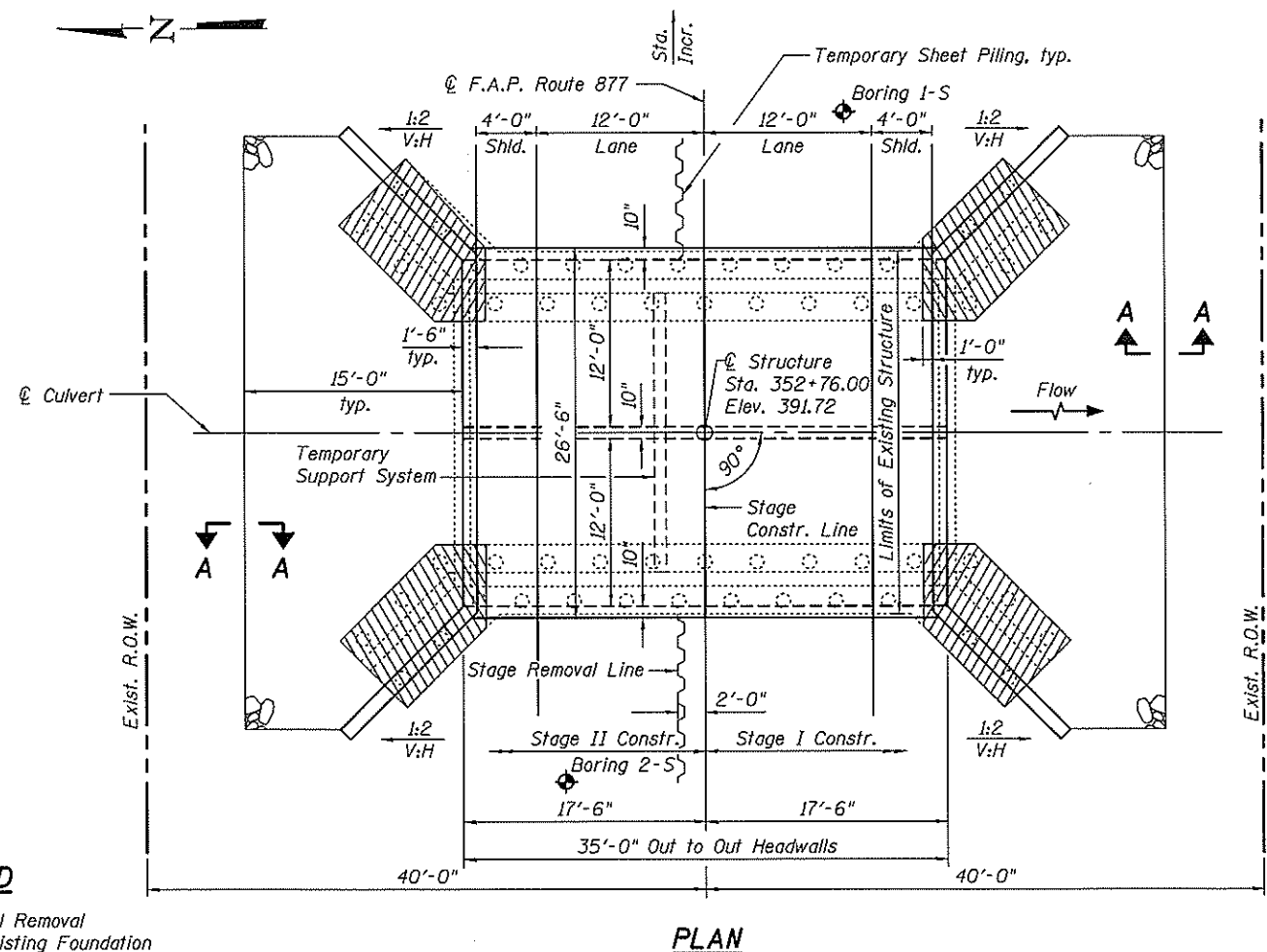


HIGHWAY CLASSIFICATION
 F.A.P. Rte. 877 (IL Rte. 141)
 Functional Class: Minor Arterial (Non-Urban)
 ADT: 2050 (2009); 2630 (2034)
 DHV: 265
 ADTT: SU = 3.4% MU = 9.8%
 Design Speed: 55 m.p.h.
 Posted Speed: 55 m.p.h.
 Two-Way Traffic
 Directional Distribution: 50/50

LOADING HL-93
 Allow 50#/sq. ft. for future wearing surface.

DESIGN SPECIFICATIONS
 2014 AASHTO LRFD Bridge Design Specifications, 7th Edition with 2015 and 2016 Interims

DESIGN STRESSES
 FIELD UNITS
 f'c = 3,500 psi
 fy = 60,000 psi (Reinforcement)

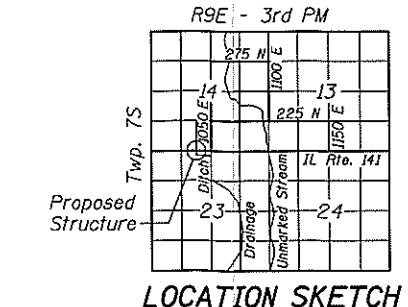
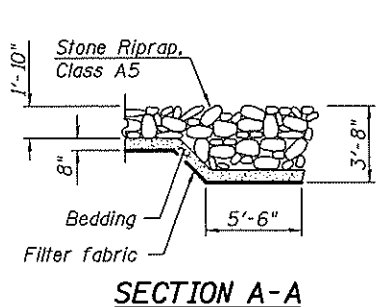


LEGEND
 Partial Removal of Existing Foundation

WATERWAY INFORMATION
 Drainage Area = 4.2 sq. mi. Low Grade Elev. 391.63 @ Sta. 380+98

Flood		Discharge (cfs)		Waterway Opening (sq. ft.)		Natural H.W.E.	Head (ft.)		Headwater Elevation	
		Existing	Proposed	Existing	Proposed		Existing	Proposed	Existing	Proposed
10	Main Channel	1119	1145	136	217	388.3	2.1	1.7	390.4	390.0
	Relief Structure	779	753	110	141					
	Total	1898	1898	246	358					
OVT (E)	Main Channel	1221	1480	142	217	388.5	2.8	2.8	391.3	391.3
	Relief Structure	862	1100	115	147					
	Total	2083	2580	257	364					
OVT (P)	Main Channel	1146	1480	143	217	388.6	2.8	2.7	391.4	391.2
	Relief Structure	808	1096	116	148					
	Total	1954	2576	259	365					
50	Main Channel	955	1260	146	217	388.7	2.8	2.7	391.4	391.4
	Relief Structure	674	950	118	151					
	Total	1629	2210	264	368					
100	Main Channel	631	918	150	217	388.8	2.8	2.7	391.6	391.5
	Relief Structure	434	672	121	154					
	Total	1065	1590	271	371					

Note: SN 097-2016 is the relief structure.



GENERAL PLAN AND ELEVATION
ILLINOIS ROUTE 141 OVER
DRAINAGE DITCH
F.A.P. ROUTE 877 - SEC. 101B-3
WHITE COUNTY
STATION 352+76.00
STRUCTURE NO. 097-2016

