



**STRUCTURE GEOTECHNICAL REPORT  
STRUCTURE NO. 056-0318, 056-0319, 056-0320  
056-0345 & 056-0346  
JOB D-91-476-16  
SECTION 2016-092B&R  
McHENRY COUNTY, ILLINOIS**

03/21/2018

INTERRA, INC.  
600 Territorial Drive, Suite G, Bolingbrook, IL 60440  
Phone: (630) 754-8700, Fax: (630) 754-8705  
[www.interraservices.com](http://www.interraservices.com)

***Prepared for:***

Baxter & Woodman Consulting Engineers  
8678 Ridgefield Road  
Crystal Lake, IL 60012

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## *Table of Contents*

<b>Section</b>	<b>Page No.</b>
<b>1.0 Introduction</b> .....	1
<b>2.0 Project Summary</b> .....	1
<b>3.0 Site Description and Geology</b> .....	2
<b>4.0 Field Investigation</b> .....	3
<b>5.0 Laboratory Testing</b> .....	3
<b>6.0 Subsurface Conditions</b> .....	4
<b>7.0 Analysis and Recommendations</b> .....	6
<b>8.0 Construction Considerations</b> .....	9
<b>9.0 Closure</b> .....	10
<b>10.0 References</b> .....	11

**Appendix A** – Site Location Map and Borehole Location Plan

**Appendix B** – Subsurface Data Profiles & Soil Boring Logs

**Appendix C** – Laboratory Test Reports

**Appendix D** – Retaining Wall Global Slope Stability Analysis Results

**Appendix E** – Roadway Plan & Profile



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**STRUCTURE GEOTECHNICAL REPORT  
STRUCTURE NO. 056-0319 & 056-0320  
JOB D-91-476-16  
SECTION 2016-092B&R  
MCHENRY COUNTY, ILLINOIS**

## **1.0 INTRODUCTION**

Baxter & Woodman Consulting Engineers (B & W) was tasked by Illinois Department of transportation (IDOT) to provide a Phase II Engineering services for various improvements to US20 (FAP 525, S. Grant Highway) in McHenry County which include three intersection improvements of US20 at West Union Road, Coral Road and Marengo/Beck/S Union Road; and the removal and replacement of an existing box culvert with multiple drainage culverts, widening the roadway for shoulder improvements and placing two feet of additional fill within this section to raise the roadway grade. The box culvert section is located between Coral Road and Marengo Road. In addition, the project involves the installation of a 200-foot long retaining wall on the west side of US 20 and a 160-foot long retaining wall on the east side to retain the additional fill materials for the shoulder improvements. Interra, Inc. was retained as the Geotechnical Engineering sub-consultant to perform subsurface soil exploration and prepare the Structural Geotechnical Report (SGR). The existing 8'X4' box culvert allows flow of an unnamed creek under US 20. The proposed improvements consist of replacement of the existing box culvert with a 10'X5' box culvert (SN 056-0318), and addition of two new 6'X5' box culverts, one on the north side (SN 056-0319) and the other on the south side (SN 056-0320) of the existing box culvert.

## **2.0 PROJECT SCOPE**

The scope of work included drilling a total of nine (9) structural soil borings to a depth of 30 feet each from the existing ground/pavement surface in accordance with approved Interra's Proposal number 3502 and dated, 12/14/16. The borings were located in areas of the proposed retaining walls and box culverts.



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### 3.0 SITE DESCRIPTION AND GEOLOGY

The project section is located in McHenry County, between Coral Road (north) and Marengo Road (south). The site is located within unincorporated Coral Township defined as Section 17, T43N, R6E Third Meridian, Marengo South Quadrangle.

The site is presently developed as a two lane road (US 20) with a small bridge which incorporates a box culvert that allows flow of an unnamed creek under US 20 with ponds on either side of US 20. The approximate elevation of the roadway surface on the bridge is 877 feet. Depth to water surface from road surface is noted to be approximately 8 feet, at the time of drilling on 5/9/2017.

The project area is located on the eastern flank of the southward plunging Wisconsin Arch. The area belongs to Valparaiso Morainic System. Majority of the area contains the quaternary deposits belonging to Henry and Glasford Formations, from the Wisconsin and Illinois Episodes. Thickness of the formations varies between 150 feet and 200 feet consisting of proglacial sands and gravels with interbedded diamictons underlain by loams, silty and sandy loams with interbedded sands and gravel. Bedrock surface is Ordovician dolomite with the upper surface fractured with crevices and solution cavities.

#### 3.1 *Mining Activity*

From the Illinois State Geological Survey (ISGS, 2000), McHenry County is not identified as coal producing area. Therefore, no past coal mining activities may have taken place at the project site. Sand and gravel mining from scattered locations across McHenry County is the only reported mining which occurred in the county.

#### 3.2 *Seismic Activity*

USGS National Seismic Hazard Maps (USGS, 2014) indicate a Peak Ground Acceleration (PGA) of 3% of gravity, with a 7% probability of exceedance in 75 years. The project area has no active, major faults (Kolata, 2005).



#### **4.0 FIELD INVESTIGATION**

A total of eight (8) out of the 9 proposed borings were performed during this investigation by Interra. Boring B-19 was attempted but could not be drilled beyond about 1 foot from surface due to auger refusal in an unknown old reinforced concrete structure. Borings B-14, B-16, B-18, B-20 and B-22 were drilled on the west side of US 20 and borings B-15, B-17 and B-21 were drilled on the east side of US 20. All of the eight borings were drilled to a depth of 30 feet from the existing pavement/ground surface. The boring locations were established in the field as shown in the boring location plan presented in Appendix A.

The borings were drilled and samples were tested in accordance with the guidelines in the IDOT Geotechnical Manual. Soil sampling was performed at 2.5 foot intervals to a depth of 30.0 feet. The soil samples were taken in conjunction with the Standard Penetration Test where a driving resistance to a standard 2" split-spoon samples indicates relative density of granular materials and consistency of cohesive soils. Also, pocket penetrometer tests were performed on the recovered samples. Shelby tube samples were obtained from selected depths of different boring locations. Water level readings were taken during drilling. Twenty-four hour water levels were not recorded as the boreholes were backfilled immediately due to safety concerns.

Soil specimens from the borings were visually identified in accordance with the AASHTO and IDOT textural classification systems. Pocket penetrometer estimates of unconfined compressive strength were obtained for all cohesive specimens from all the borings.

#### **5.0 LABORATORY TESTING**

All laboratory testing was performed in accordance with IDOT and/or AASHTO standard methods for testing. Moisture content tests were performed for all soil samples. Grainsize Analysis, Atterberg Limits and Unconfined Compressive Strength tests were performed on selected samples at depths where the proposed retaining walls and improvement of the culvert box are proposed.



Soil boring logs have been prepared for all the structure borings. The boring logs include the results of the laboratory testing. The boring logs are included in Appendix B of this report. Results of laboratory testing are presented in Appendix C.

## **6.0 SUBSURFACE CONDITIONS**

### West Side US 20

Borings on the west side of US 20 (B-14, B-16, B-18, B-20 and B-22) noted 6 to 8 inches of asphalt pavement and 6 to 12 inches of crushed rock aggregate (subbase). This is underlain by very loose to loose sandy or medium stiff to stiff clayey fill material to a depth of 3 feet below grade except at B-16 where black clay was encountered directly below the subbase. The fill material is underlain by a stiff to very soft clay loam/sandy clay or clay to a depth of 8 feet below grade. Buried topsoil or organic soils were observed in all borings from 1.5 feet at B-16 to a maximum depth of 8 feet below grade at B-20. The black soils were sometimes combined with greenish gray to gray or pale brown soils (B-16, B-18, B-22). Medium dense loam (B-14, B-20,) or silty loam (B-22) ranges in depth from 8.0 to a maximum depth of 10.5 feet. At boring B-18, a layer of medium dense sand with gravel extends from 8 to 10.5 feet, underlain by a loose loam to a depth of 13 feet. Medium dense to dense sands, sandy loams, and silty loams extend to depths ranging from 20.5 feet (B-18) and 30 feet (B-22). Hard to stiff clay or clay loam was observed in borings B-14, B-16, B-18 & B-20 underlying the sandy soils when present, to a final depth between 28 to 30 feet below grade.

### East side US 20

Borings on the east side of US 20 (B-15, B-17, B-21) noted 8 to 10 inches of asphalt pavement and 6-8 inches of crushed rock aggregate (sub-base). This is underlain by loose to medium dense sand or sandy loam fill to a depth of 2.5 to 3.0 feet below grade.

In boring B-15, medium stiff clay loam was observed to 5.5 feet below grade, underlain by very soft clay to 8.0 feet below grade. This is underlain by stiff to medium stiff sandy clay to 12.5 feet below grade. This is followed by loam to 14.4 feet and then by a medium dense sand layer



to 16.0 feet below grade. Medium dense to very dense silty loams extended to 23 feet below grade are followed by hard brown clay loam 25.5 feet. Medium dense silty loam ranges from 25.5 to the exploration depth of 30.0 feet.

In boring B-17, a stiff to very soft clay loam extends to 8.0 feet which is underlain by medium stiff sandy clay to 10.5 feet. Underlying the sandy clay is a medium dense loam to 13.0 feet, followed by a hard clay loam to a depth of 18.0 feet. Dense silt was noted between 18 and 20.5 feet, followed by dense silty loam to 23.0 feet below grade. Hard clay loam was noted from 23 feet to 25.5 feet and the boring is terminated in hard to very stiff clay at a depth of 30 feet.

In boring B-21, medium stiff black clay loam was noted from 3.0 to 5.5 feet and is underlain by a layer of very soft black clay to 8.0 feet below grade. Alternating sandy clays, loams, sandy loam, medium dense sands and silty loam complete the profile of this boring.

Please see the attached borehole logs in Appendix B for detailed soil stratification.

### Groundwater Information

Groundwater was encountered during drilling between the elevations of 865.5 (B-14) and 871.1 feet (B-21). This depth roughly corresponds with the first very permeable soils (sands/sandy loams) or below the water surface elevation of the unnamed creek.

Water levels were not measured after 24 hours upon completion of drilling. The boreholes were backfilled with auger cuttings after completion due to safety reasons and an asphalt patch was placed on top. Hence, the findings may not represent the long-term groundwater levels.

### Seismic Considerations

The following seismic data is recommended in accordance with IDOT Geotechnical Manual, AGMU 09.1 and the LRFD Bridge Design Specifications.



Soil Site Class: D

Seismic Performance Zone (SPZ): 1

Design Spectral Acceleration at a period of (T) of 1.0 sec,  $S_{D1}$  : 0.080g

Design Spectral Acceleration at a period of (T) of 0.2 sec,  $S_{DS}$  : 0.140g

### Liquefaction Potential

According to AGMU 10.1 "Liquefaction Analysis Procedure", the site does not require a liquefaction analysis as it is not located in Seismic Performance Zones 2, 3 or 4.

## **7.0 ANALYSIS AND RECOMMENDATIONS**

The following recommendations are developed based on the field investigation and laboratory testing, project information provided to INTERRA, IDOT standard specifications and the AASHTO LRFD Bridge Design Specifications, 8<sup>th</sup> Edition, 2017.

### BOX Culverts (Structure No. 056-0318, 056-0319 & 056-0320)

The bottom of the culverts is proposed at EL 871.5. Immediately below this elevation, the foundation soils consist of very soft clay and clay loam with organics and very high moisture content to a depth of 2 to 4 feet followed by medium stiff to very stiff sandy clay and medium dense to dense silt loam, loam and sand. The very soft soils do not have the required bearing and are unsuitable to support the box culvert. We recommend undercutting the unsuitable soils and replacing with coarse aggregate CA 1 or CA 2. A woven geotechnical fabric should be used below the aggregate subgrade improvement for ground stabilization. The aggregate subgrade shall be capped with a minimum 3 inches of CA 6 or CA 10.

### Bearing Capacity and Settlement

Foundation soils improved as recommended above can be designed for a bearing resistance of 3000 psf, which includes an LRFD Resistance Factor of 0.45. Settlement of the culverts is anticipated to be less than one inch.





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*East Retaining Wall (SN: 056-0346) and West Retaining Wall(SN: 056-0345)*

Two retaining walls totaling a length of approximately 350 feet are proposed in the area of the culverts on the east and west side of US 20 to retain the additional fill material for shoulder improvements and raising the roadway grade. Several possible wall types such as concrete cantilever wall, Mechanically Stabilized Earth (MSE) retaining wall, steel sheet pile wall and soldier pile wall. Of these, the steel sheet pile wall and the soldier pile walls are normally used in cut condition and deflections caused by compaction could be significant. Selection of a wall type depends on several factors such as soil conditions, feasibility, cost and control of top of wall deflections. In our opinion, a cast-in-place concrete retaining wall or MSE wall will be more appropriate.

*Concrete Retaining Wall*

The bottom of the footing for the proposed retaining walls is anticipated approximately at EL 869. At this elevation, the foundation soils consist of very soft clay and clay loam with organics and very high moisture content to a depth of 2 to 4 feet followed by medium stiff to very stiff sandy clay and medium dense to dense silt loam, loam and sand. The very soft soils do not have the required bearing and are unsuitable to support the retaining wall. We recommend undercutting the unsuitable soils and replacing with coarse aggregate CA 1 or CA 2. A woven geotechnical fabric should be used below the aggregate subgrade improvement for ground stabilization. The aggregate subgrade shall be capped with a minimum 3 inches of CA 6 or CA 10.

*Bearing Capacity*

A factored bearing resistance of 3000 psf, which includes an LRFD Resistance Factor of 0.55 is recommended. The bottom of the footings should be placed at minimum of four feet below final grade for frost protection.

*Settlement*

Based on the soil profile and the expected wall loads, settlement is estimated to be less than



0.5 inch.

### *Lateral Earth Pressures*

We recommend the retaining wall be designed for an active earth pressure of 43 psf per foot depth for a level backfill assuming drainable backfill material. Resistance to sliding may be calculated using a nominal sliding resistance of half of normal stress on the interface between the footing and the soil. The LRFD resistance factor for sliding should be taken as 1.0. Resistance offered by the passive pressures should be neglected. Lateral loads from traffic should be considered at a minimum surcharge pressure of 250 psf.

### *Drainage Considerations*

A geocomposite wall drain should be placed and connected to 6" diameter perforated drain pipe over the entire length of the back face of the retaining wall. Free draining porous granular embankment (special) material should be placed behind the retaining wall for a minimum width of 2.0 feet.

### MSE Wall

Based on the cross-sections provided by the client, the maximum wall height is approximately nine feet from top of leveling pad. The MSE wall should be analyzed and designed for external stability, internal stability and settlement. Interra performed analysis the external stability for bearing capacity, settlement, global slope stability. Contractor will provide design for the wall soil system and its internal stability.

### *Bearing Capacity*

The bottom of the reinforced soil system is anticipated at EL 869. Soft subgrade conditions exist at this elevation. Subgrade should be undercut and prepared as mentioned above for the concrete retaining wall. A factored bearing resistance of 3000 psf, which includes an LRFD Resistance Factor of 0.65, is recommended. The bottom of the concrete leveling pad should be placed at minimum of four feet below final grade for frost protection.



### *Settlement*

Based on the soil profile and the expected wall loads, settlement is estimated to be less than 0.5 inch.

### *Lateral Earth Pressures*

Resistance to sliding may be calculated using a nominal sliding resistance of half of normal stress on the interface between the reinforced mass and the soil. The LRFD resistance factor for sliding should be taken as 1.0. Resistance offered by the passive pressures should be neglected. Lateral loads from traffic should be considered at a minimum surcharge pressure of 250 psf. We recommend a base width of 0.75H or a minimum 8 feet, where H is the wall height measured from the leveling pad.

### *Stability Analyses*

Global slope stability analyses were conducted for the critical cross-section. The LRFD resistance factor considered is 0.65, which is equivalent to slope stability factor of safety of 1.54. Slope stability analyses were conducted using SLIDE V7.0. Analyses indicated that the global slope factor is above the required minimum value for both short and long-term loading conditions. Appendix D contains the results of the slope stability analyses. Preliminary analyses indicated that the wall be stable with regards to vertical pressure and overturning. Overturning should be checked for final dimensions of the MSE wall system.

## **8.0 CONSTRUCTION CONSIDERATIONS**

Construction of the box culverts and retaining walls will require sheeting, bracing and groundwater control due to the close proximity to the unnamed creek and ponds. Temporary sheet piling can be designed using IDOT's Temporary Sheet Piling Design Guide. Contractor should control seepage water accumulating in open excavations for the box culverts and the retaining walls. Seepage could be controlled using method such as drainage ditches, drainage blankets and sumps. If seepage cannot be controlled an open-graded backfill such as CA7 can be placed and compacted to come out of the standing water.



### Stage Construction Considerations

As per the TSL plan construction of the culverts will occur in two stages: stage one will involve the removal and construction of the culverts under the northbound portion of the roadway; stage two will involve the removal and construction of the culverts on the southbound portion of the roadway. A temporary soil retention system will be needed for a near vertical excavation along the centerline of the pavement. The exposed height will be on the order of 10 to 12 feet. Based on our evaluation, a temporary sheet piling may not be feasible at all locations. Therefore, we recommend a contractor-designed temporary soil retention system to accommodate stage construction. All Temporary Soil Retention Systems (TSRS) should consider surcharge loads from construction equipment, excavated material and trucks. The soil retention system should be designed by an Illinois Licensed Structural Engineer.

In accordance with the IDOT Culvert Manual for projects where the fill height is such that the Stage II traffic limitations cannot be met with a 1:1 slope, a geotextile retaining wall or a temporary soil retention system can be built to retain the soil on top of the box. Geotextile retaining walls require a minimum of 4 ft. 6 in. from the Stage I Construction line to the Stage II traffic line. The planner should consult with the District's construction staff to discuss the amount of room that will be necessary to properly build the pavement in Stage I.

The construction monitoring shall be according the IDOT Standard Specifications, Special Provisions and Contract Plans. Local, state and federal regulations and IDOT guidelines shall be followed for all excavations and construction.

## **9.0 CLOSURE**

The analysis and recommendations submitted in this report are based upon the data obtained from eight (8) soil boreholes performed at the locations indicated on the Borehole Location Plan, project information provided to INTERRA and from any other information discussed in this report. This report does not reflect any variations that may occur between these boreholes. In



performing subsurface explorations, specific information is obtained at specific locations at specific times. It is a well-known fact that variations in soil and rock conditions exist on most sites between borehole locations. Also, groundwater levels vary from time to time. The nature and extent of variations may not become evident until the course of construction. If project characteristics change or if variations in the subsurface conditions appear evident, it will be necessary for a re-evaluation of the recommendations of this report.

## **10.0 REFERENCES**

AASHTO 2017, LRFD Bridge Design Specifications, 8<sup>th</sup> Edition 2017, American Association of State Highway and Transportation Officials, Washington, DC.

IDOT 2015, Geotechnical Manual, Illinois Department of Transportation.

IDOT 2016, Standard Specifications for Road and Bridge Construction. Illinois Department of Transportation.

IDOT 2012, Bridge Manual, Bureau of Bridges and Structures, Illinois Department of Transportation.

IDOT 2015, Geotechnical Manual Illinois Department of Transportation.

Hannes E. Leetaru, Michael L.Sargent, and Dennis R.Kolata, 2004, Geologic Atlas of Cook County for Planning Purposes, Cook County, Illinois., 37pp.

Kolata, D. R., 2005, Bedrock Geology of Illinois, Illinois Map 14, Illinois State Geological Survey.

U.S.G.S. 2014, National Seismic Hazard Maps. <http://earthquake.usgs.gov/research/hazmaps/>

Coduto, Donald P., 1994, Foundation Design, Prentice Hall, Inc.



We appreciate the opportunity to be of service to you. Should you need additional information or clarifications, please call us at (630) 754-8700.

Yours truly,

**Interra, Inc.**



Ashok Guntaka, EI

Project Engineer



Eric Stusser, PG

Project Geologist



Sanjeev Bandi, Ph.D., PE

Principal Engineer



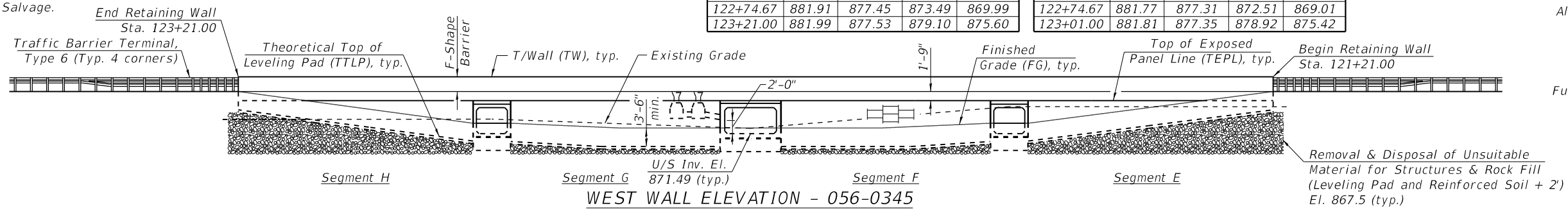
**Appendix A**  
Borehole Location Plan

Benchmark: Set iron rod with cap, 1' north of east guardrail end, 41' east of power pole. Elev. 876.894

Existing Structure: S.N. 056-0087, 8' x 4' cast in place concrete box culvert, approx. 32' in length with concrete headwalls and attached guardrail. Two 36" CMP culverts lie within the box culvert, approximate length of CMP 45' each.

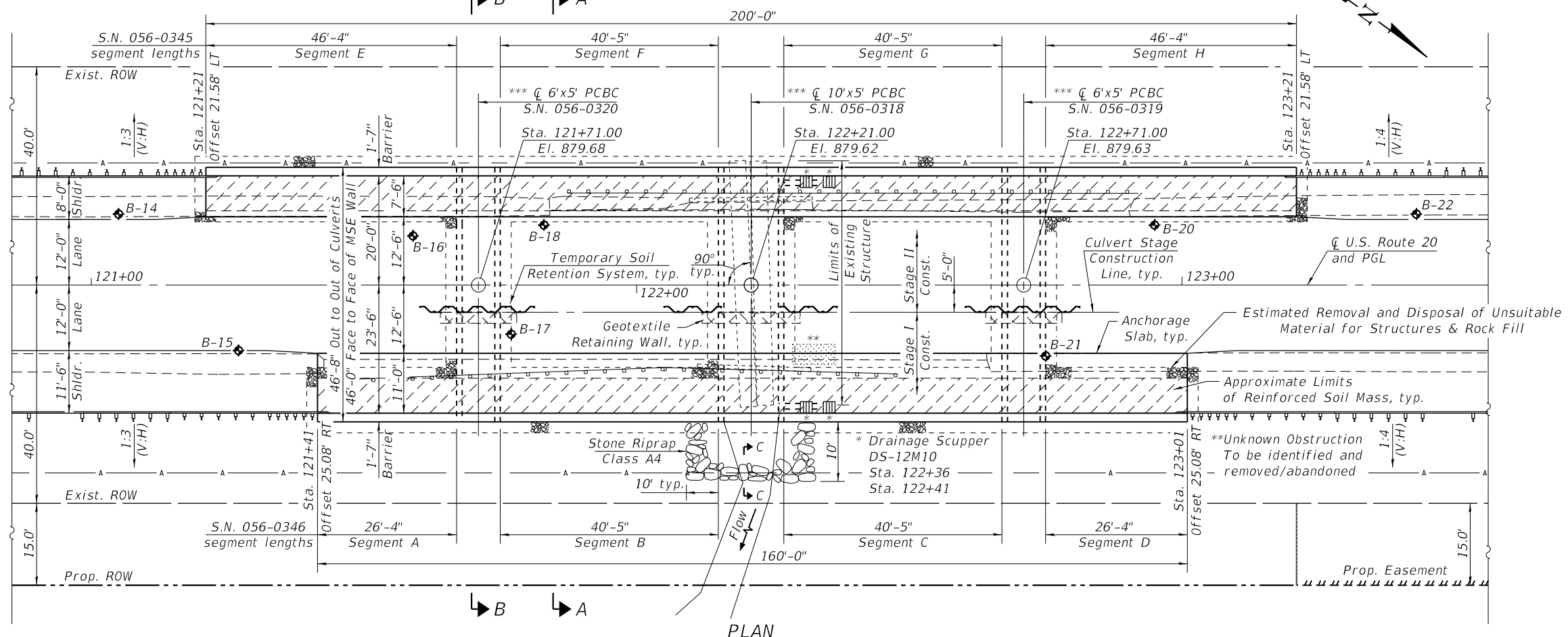
One lane of traffic to be maintained using staged construction.

No Salvage.



Note: Culverts shown for information only.

\*\*\* Design fill height for these boxes is 2 ft.



**DESIGN SPECIFICATIONS**  
2017 AASHTO LRFD Bridge Design  
Specifications Customary U.S. Units, 8th Edition

**LOADING HL-93**

Allow 50#/sq. ft. for future wearing surface.

**HIGHWAY CLASSIFICATION**

U.S. Rte. 20 - F.A.P. Rte. 525  
Functional Class: Strategic Regional Arterial  
ADT: 8,900 (2018)  
ADTT: 1,424 (2018)  
DHV: 890 (2018)  
Design Speed: 55 m.p.h.  
Posted Speed: 55 m.p.h.  
2-Way Traffic  
Directional Distribution: 50:50

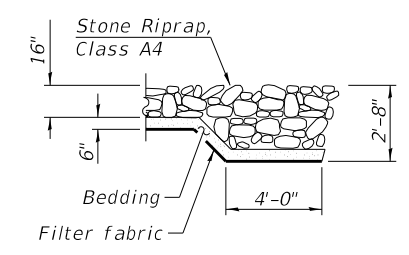
**DESIGN STRESSES**

**FIELD UNITS**

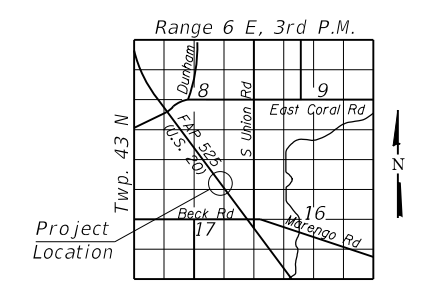
$f'_c = 3,500$  psi  
 $f_y = 60,000$  psi (Reinforcement)

**PRECAST UNITS**

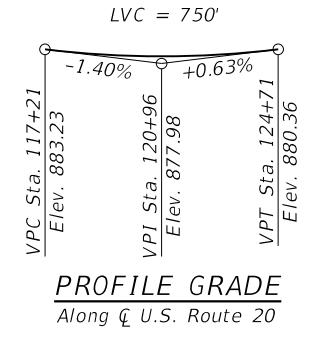
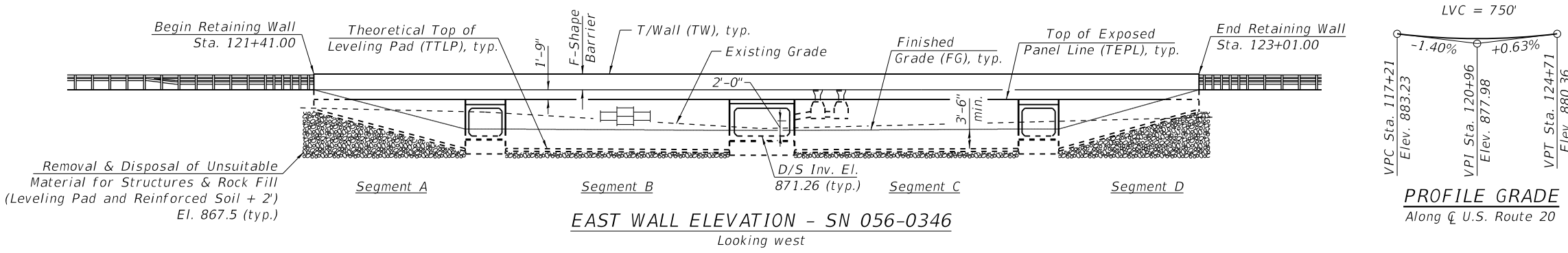
$f'_c = 4,500$  psi (Precast Panels)  
 $f'_c = 5,000$  psi (Precast Box Culverts)  
 $f_y = 65,000$  psi (Welded Wire Reinforcement)



**SECTION C-C**



**LOCATION SKETCH**



**PROFILE GRADE**  
Along  $\bar{c}$  U.S. Route 20

**BAXTER & WOODMAN**  
Consulting Engineers

USER NAME =	DESIGNED - BLB	REVISOR -
PLOT SCALE =	CHECKED - CDL	REVISIONS -
PLOT DATE =	DRAWN - BLB	REVISIONS -
	CHECKED - CDL	REVISIONS -

STATE OF ILLINOIS  
DEPARTMENT OF TRANSPORTATION

**BOREHOLE LOCATION PLAN**

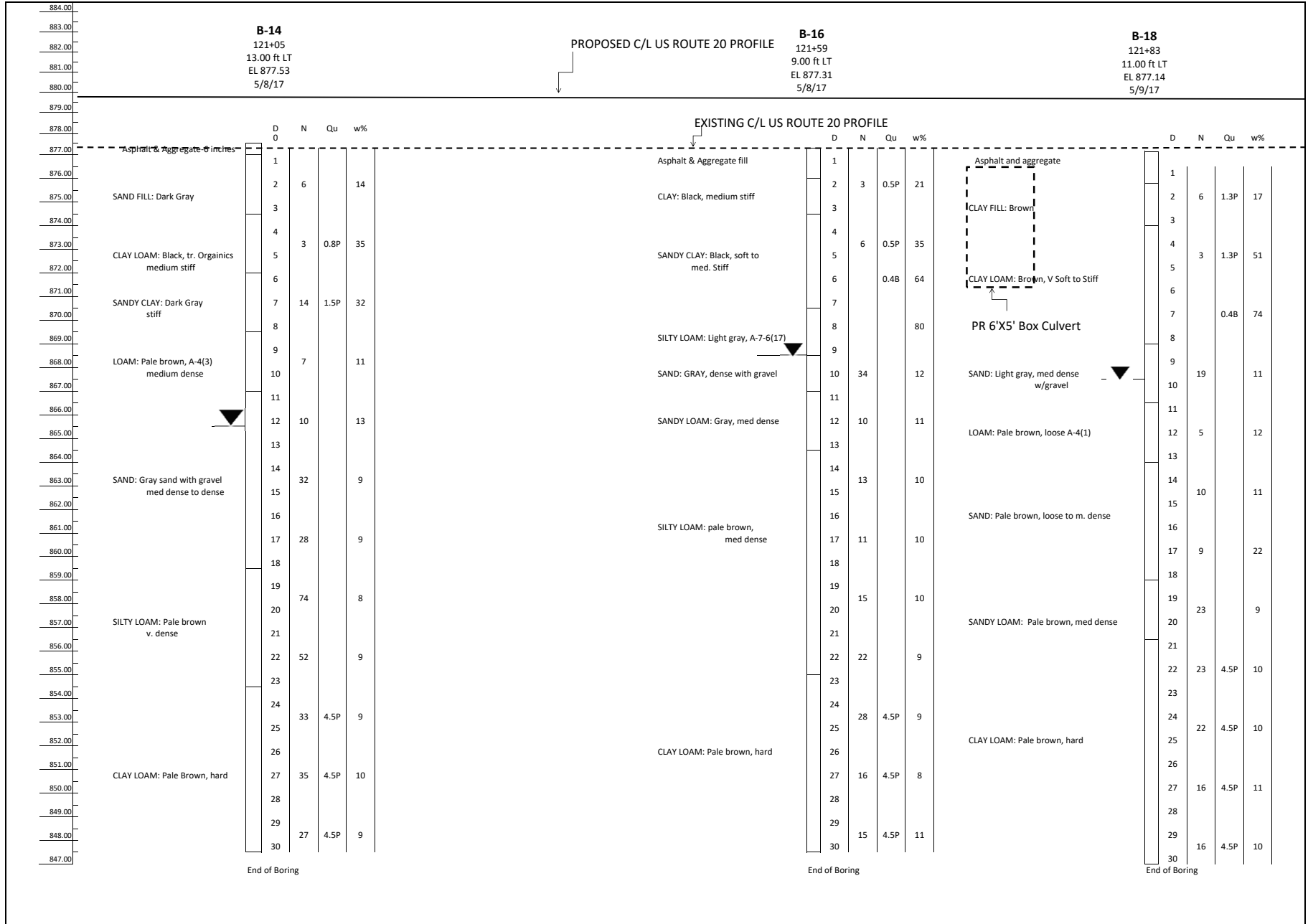
F.A.P. RTE. 525	SECTION 2016-092B&R	COUNTY McHENRY	TOTAL SHEETS	SHEET NO.
CONTRACT NO. 62D36				

ILLINOIS FED. AID PROJECT

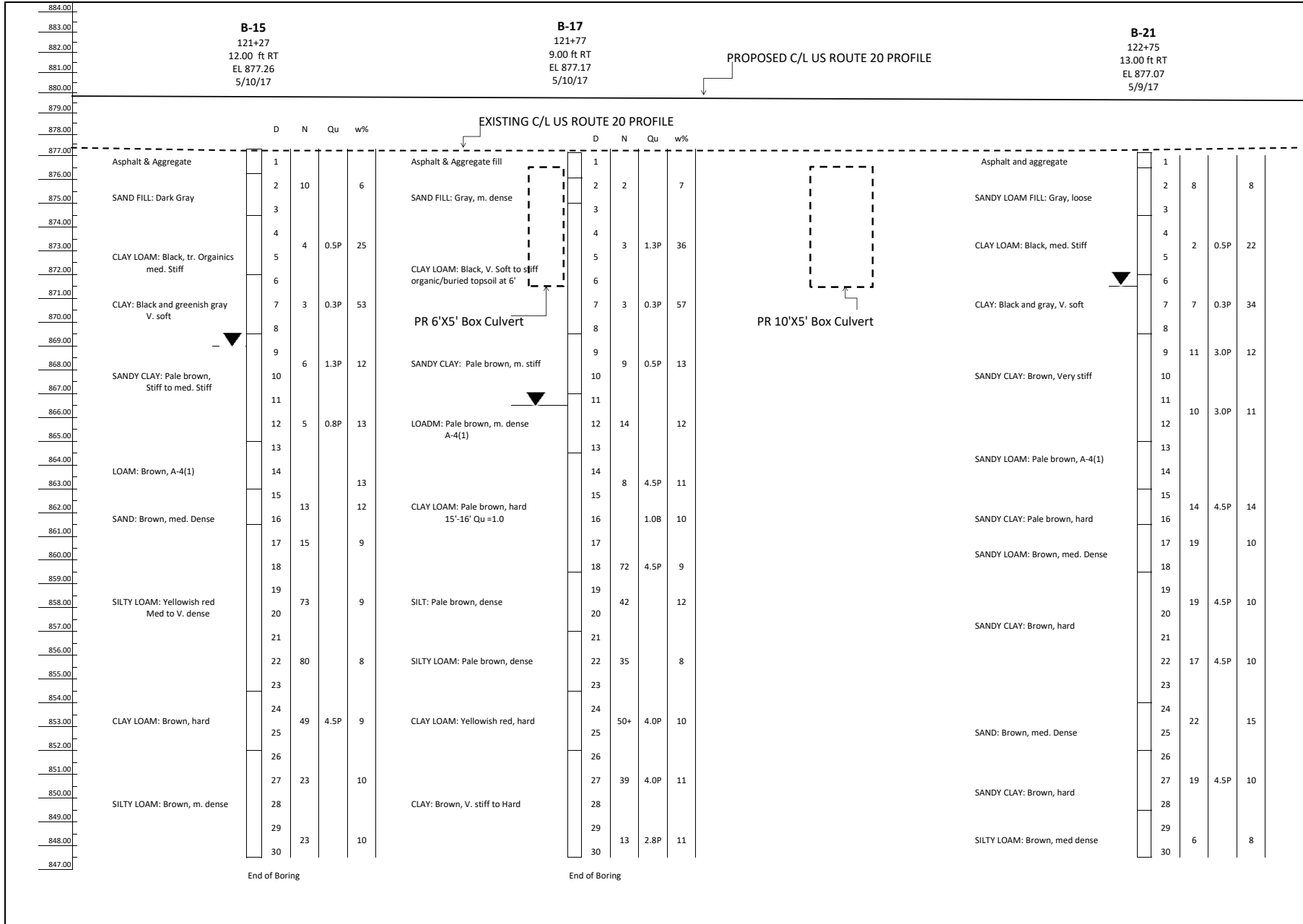


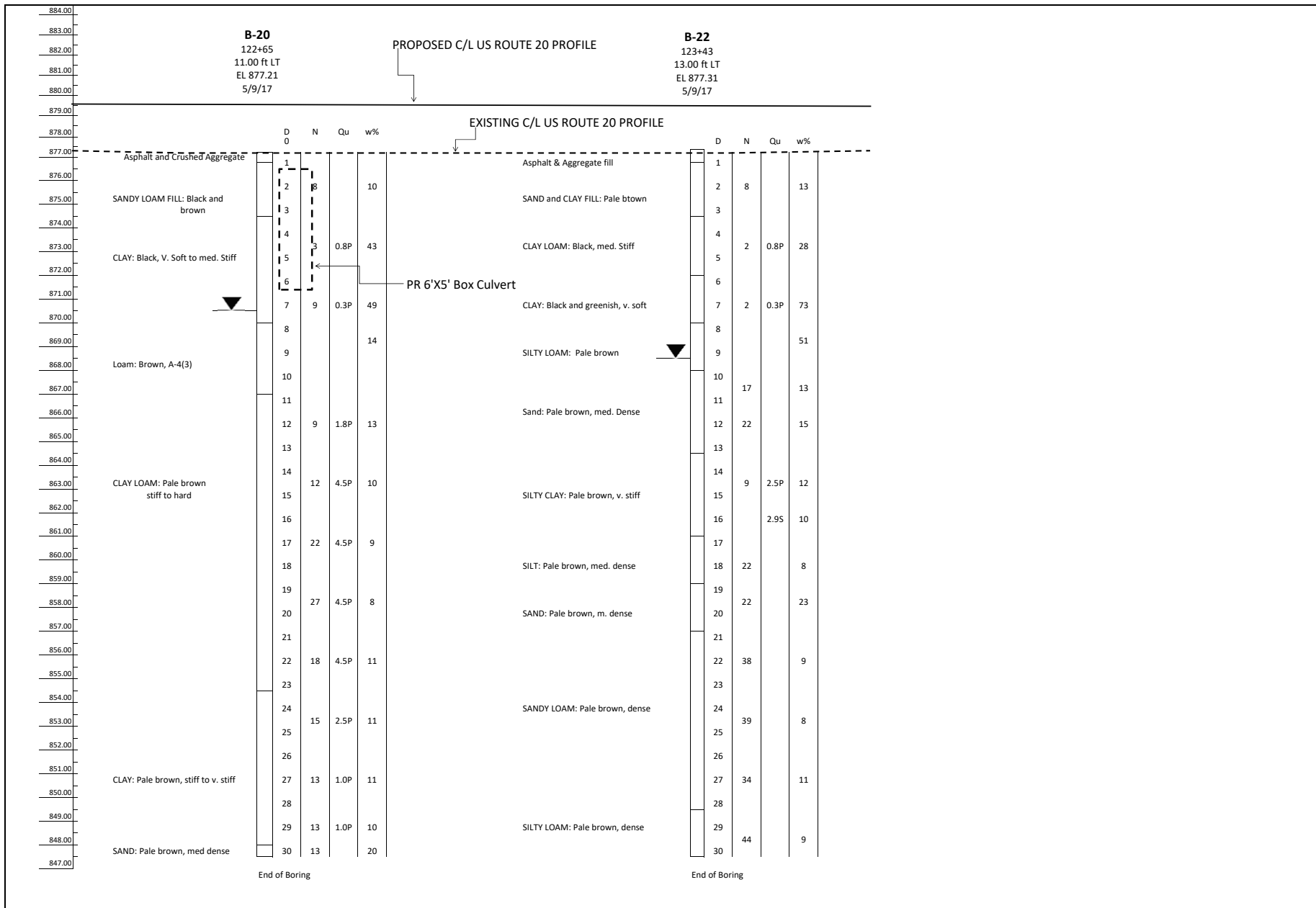
## **Appendix B**

Subsurface Data Profiles & Soil Boring Logs



<p>600 Territorial Drive, Suite G Bolingbrook, IL 60440 P: 630-754-8700, F: 630-754-8705 www.interraservices.com</p>	Drawn By <u>SB</u> Date <u>3/20/2018</u> Checked By <u>GAK</u> Date <u>3/20/2018</u>	<b>STATE OF ILLINOIS</b> <b>DEPARTMENT OF TRANSPORTATION</b>	<b>SUBSURFACE DATA PROFILE</b> <b>US ROUTE 20</b>	FAP RTE	SECTION	COUNTY	TOTAL SHEETS	SHEET NO
	525			2016-092B&R	MCHENRY	3	1	
	CONTRACT NO. 62D36							
		ILLINOIS		FED. AID PROJECT LGMW (759)				





<p>600 Territorial Drive, Suite G Bolingbrook, IL 60440 P: 630-754-8700, F: 630-754-8705 www.interraservices.com</p>	Drawn By <u>SB</u> Date <u>3/20/2018</u>	<b>STATE OF ILLINOIS DEPARTMENT OF TRANSPORTATION</b>	<b>SUBSURFACE DATA PROFILE US ROUTE 20</b>	FAP RTE	SECTION	COUNTY	TOTAL SHEETS	SHEET NO
	Checked By <u>GAK</u> Date <u>3/20/2018</u>			525	2016-092B&R	MCHENRY	3	3
				ILLINOIS		CONTRACT NO. 62D36		FED. AID PROJECT LGMW (759)



# SOIL BORING LOG

ROUTE FAP 525 (US Route 20) DESCRIPTION US 20 Culvert/proposed Retaining Wall LOGGED BY Eric Slusser

SECTION D-91-476-16 LOCATION West side US 20

COUNTY MCHENRY DRILLING METHOD Hollow Stem Auger HAMMER TYPE Automatic

STRUCT. NO. 056-0318, 056-0319  
& 056-0320  
Station \_\_\_\_\_

BORING NO. B-14  
Station 121+05  
Offset 13.00ft LT  
Ground Surface Elev. 877.53 ft

DEPTH H S	B L O W S	U C S Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

Surface Water Elev.	ft
Stream Bed Elev.	ft
Groundwater Elev.:	
First Encounter	<u>865.5</u> ft ▼
Upon Completion	<u>865.5</u> ft ▼
After _____ Hrs.	ft

DEPTH H S	B L O W S	U C S Qu	M O I S T
(ft)	(/6")	(tsf)	(%)

ASPHALT	877.03				Very Dense, pale brown (10YR 6/3) SILTY LOAM (SiL), trace to little gravel, trace to little sand, moist ( <i>continued</i> )				
CRUSHED AGGREGATE FILL (sub-base)	876.53	4				19			
Loose, dark gray (10YR 4/1) SAND FILL, medium to fine grained, moist		3		13.7		21			9.3
		3				31			
	874.53					854.53			
Medium Stiff, black (10YR 2/1) CLAY LOAM (CL), trace organics, moist. Remnant topsoil or organic soil		2			Hard, pale brown (10YR 6/3) CLAY LOAM (CL), trace to little gravel, trace to little sand, moist	9			
		1		34.6		14			8.5
		-5	0.8			-25	19	4.5	
	872.03							P	
Stiff, dark gray (10YR 4/1) SANDY CLAY (SaC), trace fine gravel, trace sand, moist		2				9			
		4		31.9		14			9.7
		10	1.5			21	4.5		
	869.53							P	
Medium Dense, pale brown (10YR 6/3) LOAM (L), little gravel, little sand, AASHTO Classification A-4(3), moist		3				8			
		3		11.4		13			9.4
		-10	4			14	4.5		
	867.03					847.53	-30		
Medium Dense to Dense, gray (10YR 5/1) SAND WITH GRAVEL (S), gravel large to fine, sand medium to fine, saturated at 12.0'		3							
		4		12.7					
		6							
		9							
		22		8.6					
		-15	10				-35		
		21							
		17		9.4					
		21							
	859.53								
Very Dense, pale brown (10YR 6/3) SILTY LOAM (SiL), trace to little gravel, trace to little sand, moist		16							
		31		8.1					
		-20	43				-40		

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)



# SOIL BORING LOG

ROUTE FAP 525 (US Route 20) DESCRIPTION US 20 Culvert/proposed Retaining Wall LOGGED BY Eric Slusser

SECTION D-91-476-16 LOCATION East side US 20

COUNTY MCHENRY DRILLING METHOD Hollow Stem Auger HAMMER TYPE Automatic

STRUCT. NO. 056-0318, 056-0319  
& 056-0320  
Station \_\_\_\_\_

BORING NO. B-15  
Station 121+27  
Offset 12.00ft RT  
Ground Surface Elev. 877.26 ft

DEPTH H S Qu T (ft)	B L O W S (/6")	U C S Qu T (tsf)	M O I S T (%)	Surface Water Elev. _____ ft	D E P T H (ft)	B L O W S (/6")	U C S Qu T (tsf)	M O I S T (%)
				Stream Bed Elev. _____ ft				
				Groundwater Elev.:				
				First Encounter <u>868.8</u> ft ▼				
				Upon Completion <u>868.8</u> ft ▼				
				After _____ Hrs. _____ ft				
ASPHALT				Medium Dense to Very Dense, brown (10YR 5/3) to 21.0', yellowish red (5YR 4/6) SILTY LOAM (SiL), trace to little medium to fine gravel, trace fine sand, saturated (continued)		19		8.2
876.59								
Medium Dense, black (10YR 2/1) CRUSHED AGGREGATE FILL (sub-base), moist	9		5.7			31		
875.93						49		
Medium Dense, brown (10YR 5/3) SAND FILL, medium to fine grained, pieces of concrete and rock, moist	5							
874.26				854.26				
Medium Stiff, black (10YR 2/1) CLAY LOAM (CL), trace fine gravel, organic soil or remnant topsoil, moist	3		25.3	Hard, brown (10YR 5/3) CLAY LOAM (CL), trace to little medium to fine gravel, trace fine sand, moist		13		9.1
	2					18		
	-5	0.5				31	4.5	
871.76		P		851.76			P	
Very Soft, black (10YR 2/1) and greenish gray (GLEYS 6/1) CLAY (C), pieces of wood, moist to wet,	1		53.4	Medium Dense, brown (10YR 5/3) SILTY LOAM (SiL), trace to little medium to fine gravel, trace fine sand, moist		8		10.1
	1					10		
	2	0.3				13		
869.26		P						
Stiff to Medium Stiff, pale brown (10YR 6/3) SANDY CLAY (SaC), trace to little gravel, moist	3		12.0			5		
	3					10		10.1
	-10	1.3		847.26	-30	13		
		P						
	2		12.7					
	2							
864.76		0.8						
brown (10YR 5/3) LOAM (L), trace fine gravel, some sand, moist AASHTO Classification A-4(1)			12.5					
862.76								
Medium Dense, brown (10YR 5/3) SAND (S), medium to fine grained, saturated	6		12.0					
	-15					-35		
	6							
861.26								
Medium Dense to Very Dense, brown (10YR 5/3) to 21.0', yellowish red (5YR 4/6) SILTY LOAM (SiL), trace to little medium to fine gravel, trace fine sand, saturated	5		8.9					
	8							
	7							
	10							
	39		8.6					
	-20	43				-40		

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)



# SOIL BORING LOG

ROUTE FAP 525 (US Route 20) DESCRIPTION US 20 Culvert/proposed Retaining Wall LOGGED BY Eric Slusser

SECTION D-91-476-16 LOCATION West side US 20

COUNTY MCHENRY DRILLING METHOD Hollow Stem Auger HAMMER TYPE Automatic

STRUCT. NO. 056-0318, 056-0319  
& 056-0320  
Station \_\_\_\_\_

BORING NO. B-16  
Station 121+59  
Offset 9.00ft LT  
Ground Surface Elev. 877.31 ft

DEPT H (ft)	BLOW S (/6")	UCS Qu (tsf)	MOIST (%)	Surface Water Elev.	ft	DEPT H (ft)	BLOW S (/6")	UCS Qu (tsf)	MOIST (%)
				Stream Bed Elev.	ft				
				Groundwater Elev.:					
				First Encounter	<u>868.3</u> ft				
				Upon Completion	<u>868.3</u> ft				
				After _____ Hrs.	_____ ft				
ASPHALT				Medium Dense, pale brown (10YR 6/3) SILTY LOAM (SiL), trace to little fine gravel, saturated					
876.81				(continued)					
Very Loose, black (10YR 2/1) CRUSHED AGGREGATE FILL (sub-base)	1					9			
875.81						11		9.3	
Medium Stiff, Black (10YR 2/1) CLAY (C), trace gravel, trace sand, moist	2	0.5	21.4			11			
874.31		P		Hard, pale brown (10YR 6/3) CLAY LOAM (CL), trace to little fine gravel, trace to little fine sand, moist					
						12			
Medium Stiff to Soft, black (10YR 2/1) and gray (10YR 6/1) SANDY CLAY (SaC), trace gravel, trace sand, shelly tubes ST-03 from 5'-7', UC=0.35 tsf, moist	1					13		9.1	
	4		35.1			15	4.5		
	-5	0.5				-25	P		
			64.3						
		0.4				5			
870.31		B				8		8.1	
light gray (10YR 7/1) SILTY LOAM (SiL), trace gravel, trace sand, little clay, AASHTO classification A-7-6(17), moist			80.3			8	4.5		
868.31						5			
Dense, gray (10YR 5/1) SAND WITH GRAVEL (S), gravel medium to fine grained, sand predominantly fine to very fine, saturated	7					6		10.9	
	13		12.0			9	4.5		
866.81					847.31	-30	P		
	21								
Medium Dense, gray (10YR 5/1) SANDY LOAM (SaL), little medium to fine gravel, sand medium to fine, saturated	4		11.1						
	5								
864.31									
Medium Dense, pale brown (10YR 6/3) SILTY LOAM (SiL), trace to little fine gravel, saturated	4								
	5		10.0						
	-15					-35			
	8								
	5								
	5		10.3						
	6								
	5								
	7		9.9						
	-20					-40			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)



# SOIL BORING LOG

ROUTE FAP 525 (US Route 20) DESCRIPTION US 20 Culvert/proposed Retaining Wall LOGGED BY Eric Slusser

SECTION D-91-476-16 LOCATION East side US 20

COUNTY MCHENRY DRILLING METHOD Hollow Stem Auger HAMMER TYPE Automatic

STRUCT. NO. 056-0318, 056-0319  
& 056-0320  
Station \_\_\_\_\_

BORING NO. B-17  
Station 121+77  
Offset 9.00ft RT  
Ground Surface Elev. 877.17 ft

DEPTH H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)	Surface Water Elev. _____ ft Stream Bed Elev. _____ ft	DEPTH H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
				Groundwater Elev.:				
				First Encounter <u>866.2</u> ft ▼				
				Upon Completion <u>866.2</u> ft ▼				
				After _____ Hrs. _____ ft				
ASPHALT				856.67				
876.34				Dense, pale brown (10YR 6/3)				
CRUSHED AGGREGATE FILL	8			SILTY LOAM (SiL), trace medium	13			
(sub-base)	8	7.3		to fine gravel, trace to little fine	17		8.4	
874.67	4			sand, moist	18			
Medium Dense, gray (10YR 5/1)				854.17				
SAND FILL, trace fine gravel, sand,				Hard, yellowish red (5YR 4/6)				
medium to fine, moist	3			CLAY LOAM (CL), trace fine	44			
Stiff to Very Soft, black (10YR 2/1)	2	35.9		gravel, trace fine sand, moist	50		10.0	
CLAY LOAM (CL), trace to little	-5	1	1.3				4.0	
fine gravel, trace to little fine sand,			P	851.67			P	
trace roots at 6.0', moist, organic	1			Hard to Very Stiff, brown (10YR				
soil or buried topsoil	1	57.4		5/3) CLAY (C), trace fine gravel,	13			
	2			trace fine sand, moist	18		11.3	
	2	0.3			21	4.0		
		P				P		
869.17								
Medium Stiff, pale brown (10YR	2				4			
6/3) SANDY CLAY (SaC), trace to	4	12.6			7		10.6	
little fine gravel, moist	-10	5	0.5		6	2.8		
			P	847.17	-30	P		
866.67								
Medium Dense, pale brown (10YR	5							
6/3) LOAM (L), trace fine gravel,	7	12.3						
some fine sand, little clay,	7							
AASHTO classification A-4(1),								
moist								
864.17								
Hard, pale brown (10YR 6/3)	2							
CLAY LOAM (CL), trace to little	2	10.5						
fine gravel, trace to little sand,	-15	6	4.5					
moist, Shelby tube 15-16' Qu=1.0			P					
tsf								
	18	9.9						
	31	1.0						
	41	B	8.7					
859.17								
Dense, pale brown (10YR 6/3)								
SILT (Si), moist to wet	15							
	18	11.8						
	-20	24						

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)





# SOIL BORING LOG

ROUTE FAP 525 (US Route 20) DESCRIPTION US 20 Culvert/proposed Retaining Wall LOGGED BY Eric Slusser

SECTION D-91-476-16 LOCATION West side US 20

COUNTY MCHENRY DRILLING METHOD Hollow Stem Auger HAMMER TYPE Automatic

STRUCT. NO. 056-0318, 056-0319  
& 056-0320  
Station \_\_\_\_\_

BORING NO. B-18  
Station 121+83  
Offset 11.00ft LT  
Ground Surface Elev. 877.14 ft

DEPTH (ft)	BLOW S (/6")	UCS Qu (tsf)	MOIST T (%)	Surface Water Elev. _____ ft	Stream Bed Elev. _____ ft	DEPTH (ft)	BLOW S (/6")	UCS Qu (tsf)	MOIST T (%)
ASPHALT						856.64			
876.47									
Loose, black (10YR 2/1) CRUSHED ROCK AGGREGATE FILL (sub-base)	9		17.1				8		
875.81	3						10		10.0
Stiff black (10YR 2/1) and brown (10YR 5/3) CLAY FILL, trace fine gravel, trace fine sand, moist	3	1.3 P					13	4.5 P	
874.14									
Stiff to Very Soft black (10YR 2/1) to 6.0', pale brown (10YR 6/3) to 8.0' CLAY LOAM (CL), trace organics to 5.0', shelly tube 5-7', moist	2						7		
	1		50.5				9		10.2
	-5	1.3 P				-25	13	4.5 P	
			73.5				6		
		0.4 B					7		10.5
869.14							9	4.5 P	
Medium Dense (light gray (10YR 7/1) SAND with GRAVEL (S), gravel large to fine, sand course to fine, saturated	5						5		
	8		10.5				7		9.9
	-10					847.14	9	4.5 P	
866.64									
Loose, pale brown (10YR 6/3) LOAM (L), trace fine gravel, some sand, little clay, moist, AASHTO Classification A-4(1)	3								
	2		12.3						
	3								
864.14									
Medium Dense to Loose, pale brown (10YR 6/3) SAND (S), some large to fine gravel from 15.5-15', sand medium to fine, saturated	3		11.1						
	4								
	-15					-35			
	3								
	3		21.8						
	6								
859.14									
Medium Dense, pale brown (10YR 6/3) SANDY LOAM (SaL), trace to little medium to fine gravel, sand medium to fine, saturated	5		8.6						
	10								
	-20	13				-40			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)



# SOIL BORING LOG

ROUTE FAP 525 (US Route 20) DESCRIPTION US 20 Culvert/proposed Retaining Wall LOGGED BY Eric Slusser

SECTION D-91-476-16 LOCATION West side US 20

COUNTY MCHENRY DRILLING METHOD Hollow Stem Auger HAMMER TYPE Automatic

STRUCT. NO. 056-0318, 056-0319  
& 056-0320  
Station \_\_\_\_\_

BORING NO. B-20  
Station 122+65  
Offset 11.00ft LT  
Ground Surface Elev. 877.21 ft

DEPTH (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)	Surface Water Elev. _____ ft Stream Bed Elev. _____ ft	DEPTH (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
876.63								
876.13	3					6		
	4		10.4			8		11.3
	4					10	4.5	
874.21					854.21		P	
	1					7		
	1		43.2			7		10.8
	-5	0.8			-25	8	2.5	
		P					P	
	0					5		
	3		49.1			6		11.2
869.71	6	0.3				7	1.0	
		P					P	
			13.5			5		
					847.71	7		10.2
	-10				847.21	-30	6	1.0
866.71							P	
	3							
	3		12.5					
	6	1.8						
		P						
	4							
	5		9.7					
	-15	4.5			-35			
		P						
	6							
	11		8.6					
	11	4.5						
		P						
	8							
	13		8.1					
	-20	4.5			-40			

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)



Interra, Inc.  
600 Territorial Drive, Suite G  
Bolingbrook, IL 60440  
www.interraservices.com

# SOIL BORING LOG

**ROUTE** FAP 525 (US Route 20) **DESCRIPTION** US 20 Culvert/proposed Retaining Wall **LOGGED BY** Eric Slusser

**SECTION** D-91-476-16 **LOCATION** East side US 20

**COUNTY** MCHENRY **DRILLING METHOD** Hollow Stem Auger **HAMMER TYPE** Automatic

056-0318, 056-0319

**STRUCT. NO.** & 056-0320  
**Station** \_\_\_\_\_

**BORING NO.** B-21  
**Station** 122+75  
**Offset** 13.00ft RT  
**Ground Surface Elev.** 877.07 ft

	DEPTH (ft)	B L O W S Qu	U C S Qu	M O I S T %			DEPTH (ft)	B L O W S Qu	U C S Qu	M O I S T %
					Surface Water Elev. _____ ft	Stream Bed Elev. _____ ft				
ASPHALT 876.40										
Loose, black (10YR 2/1) CRUSHED ROCK AGGREGATE FILL (sub-base) 875.97		6						6		
Loose, gray (10YR 5/1) SANDY LOAM FILL, trace large to fine gravel, sand medium to very fine, moist 874.07		3	8.4				8		10.0	
		5					9	4.5		
Medium Stiff black (10YR 2/1) CLAY LOAM (CL), trace fine gravel, trace fine sand, moist 871.57		1								
		1		21.8				6		
	-5	1	0.5					8		14.5
		1						14		
Very Soft black (10YR 2/1) and gray (10YR 5/1) CLAY (C), trace fine gravel, trace fine sand, wet, organic soil 869.07		1								
		1		34.2				7		
		6	0.3					8		9.9
								11	4.5	
Very Stiff to Hard brown (10YR 5/3) SANDY CLAY (SaC), trace medium to fine gravel, moist, 864.57		4								
		4		12.4				6		
	-10	7	3.0					11		8.3
								1		
		3						5		
		5		11.1						
		5	3.0							
Pale Brown (10YR 6/3) SANDY LOAM (SaL), trace gravel, little silt, little clay, AASHTO Classification A-4(1), saturated 862.57				11.8						
Hard Pale Brown (10YR 6/3) SANDY CLAY (SaC), trace gravel, moist 861.07		6								
	-15	7	4.5	14.4						
		7								
Medium Dense brown (10YR 5/30) SANDY LOAM (SaL), clay lense 16.1'-16.4', saturated 859.07		6		9.7						
		9								
		10								
Hard brown (10YR 5/3) SANDY CLAY (SaC), trace fine gravel, moist		5		10.3						
		8								
	-20	11	4.5							

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)



# SOIL BORING LOG

ROUTE FAP 525 (US Route 20) DESCRIPTION US 20 Culvert/proposed Retaining Wall LOGGED BY Eric Slusser

SECTION D-91-476-16 LOCATION West side US 20

COUNTY MCHENRY DRILLING METHOD Hollow Stem Auger HAMMER TYPE Automatic

056-0318, 056-0319  
STRUCT. NO. & 056-0320  
Station \_\_\_\_\_

BORING NO. B-22  
Station 123.43  
Offset 13.00ft LT  
Ground Surface Elev. 877.31 ft

DEPTH H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)	Surface Water Elev. _____ ft Stream Bed Elev. _____ ft Groundwater Elev.: First Encounter <u>868.3</u> ft ▼ Upon Completion <u>868.3</u> ft ▼ After _____ Hrs. _____ ft	DEPTH H (ft)	B L O W S (/6")	U C S Qu (tsf)	M O I S T (%)
ASPHALT				856.81				
876.64								
876.23	3			Dense pale brown (10 YR 6/3) SANDY LOAM (SaL), trace to little fine gravel, scattered silt lenses 0.01'-0.05', saturated	7			
	3		12.9		14			8.6
	5				24			
874.31								
	1				14			
	1		28.1		18			7.9
	1	0.8			21			
		P						
871.81								
	1				12			
	1		73.3		15			11.3
	1	0.3			19			
		P						
869.81								
			51.4					
				Dense pale brown (10YR 6/3) SILTY LOAM (SiL), trace fine gravel, trace to little fine sand, moist to wet	12			
					19			8.7
					25			
867.81								
	5							
	9		12.6					
	8							
	24							
	14		14.8					
	8							
864.31								
	5							
	4		11.7					
	5	2.5						
		P						
			9.6					
860.81		2.9						
		S						
	6							
	8		8.4					
	14							
858.81								
	9							
	10		22.5					
	12							

The Unconfined Compressive Strength (UCS) Failure Mode is indicated by (B-Bulge, S-Shear, P-Penetrometer)

## **Appendix C**

### Laboratory Test Reports

**STRUCTURE GEOTECHNICAL REPORT**  
**US 20 IMPROVEMENT, STRUCTURE NO. 056-0318, 056-0319 & 056-0320**  
**McHENRY COUNTY, ILLINOIS**  
**Interra Project # 7698**  
**Table 1 - Laboratory Test Summary**

BORING LOCATION:	B-14 SS-04	B-15 ST-06	B-16 ST-03	B-16 ST-04	B-17 ST-07	B-18 ST-03	B-18 SS-05	B-20 ST-04	B-21 ST-06	B-22 ST-04	B-22 ST-08
Station	121+05	121+27	121+59	121+59	121+77	121+83	121+83	122+65	122+75	123+43	123+43
Offset	13.00 ft LT	12.00 ft RT	9.00 ft LT	9.00 ft LT	9.00 ft RT	11.00 ft LT	11.00 ft LT	11.00 ft LT	13.00 ft RT	13.00 ft LT	13.00 ft LT
ELEVATION	877.53	887.26	877.31	877.31	877.17	877.14	877.14	877.21	877.07	877.31	877.31
SAMPLE DEPTH	8.5'-10.0'	12.5'-14.5'	5.0'-7.0'	7.0'-9.0'	15.0'-16.0'	6.0'-8.0'	11.0'-12.5'	7.5'-9.5'	12.5'-14.5'	7.5'-9.5'	15.0'-17.0'
IDH /AASHTO CLASSIFICATION	Loam A-4(3)	Loam A-4(1)	Sandy Clay	Silty Loam A-7-6(17)	Clay Loam	Clay Loam	Loam A-4(1)	Loam A-4(3)	Sandy Loam A-4(1)	Silty Loam A-6(6)	Silty Clay
GRADATION-PASSING 1" SIEVE %	100.0	100.0		100.0			100.0	100.0	100.0	100.0	
" 3/4" " %	93.6	100.0		100.0			100.0	100.0	100.0	98.3	
" 1/2" " %	93.6	98.3		100.0			96.7	98.2	98.1	97.1	
" 3/8" " %	89.5	97.5		100.0			96.7	97.7	97.7	96.7	
" NO. 4 " %	87.3	94.4		99.8			94.4	95.0	94.8	93.6	
" NO. 10 " %	85.0	91.7		99.6			91.1	92.0	91.6	90.6	
" NO. 40 " %	80.4	86.0		98.7			85.4	86.8	83.9	86.1	
" NO. 100 " %	68.7	71.6		97.3			70.5	73.2	65.8	74.6	
" NO. 200 " %	60.8	62.3		93.1			60.7	64.2	54.5	68.7	
GRAVEL % (IDH)	15.0	8.3		0.4			8.9	8.0	8.4	9.4	
SAND % (IDH)	28.5	32.0		6.5			33.4	30.2	37.1	24.2	
SILT % (IDH)	42.5	47.1		74.3			45.7	44.8	42.8	51.8	
CLAY % (IDH)	14.0	12.5		18.8			12.0	17.0	11.7	14.6	
D <sub>90</sub> (mm)											
D <sub>50</sub> (mm)											
LIQUID LIMIT											
PLASTICITY INDEX											
UNCONFINED COMPRESSIVE STRENGTH (PSF)			703		2054	710					5740
Moisture (%)	11.4	12.5	64.3	80.3	9.9	73.5	12.3	13.5	11.8	51.4	9.6
REMARKS:											



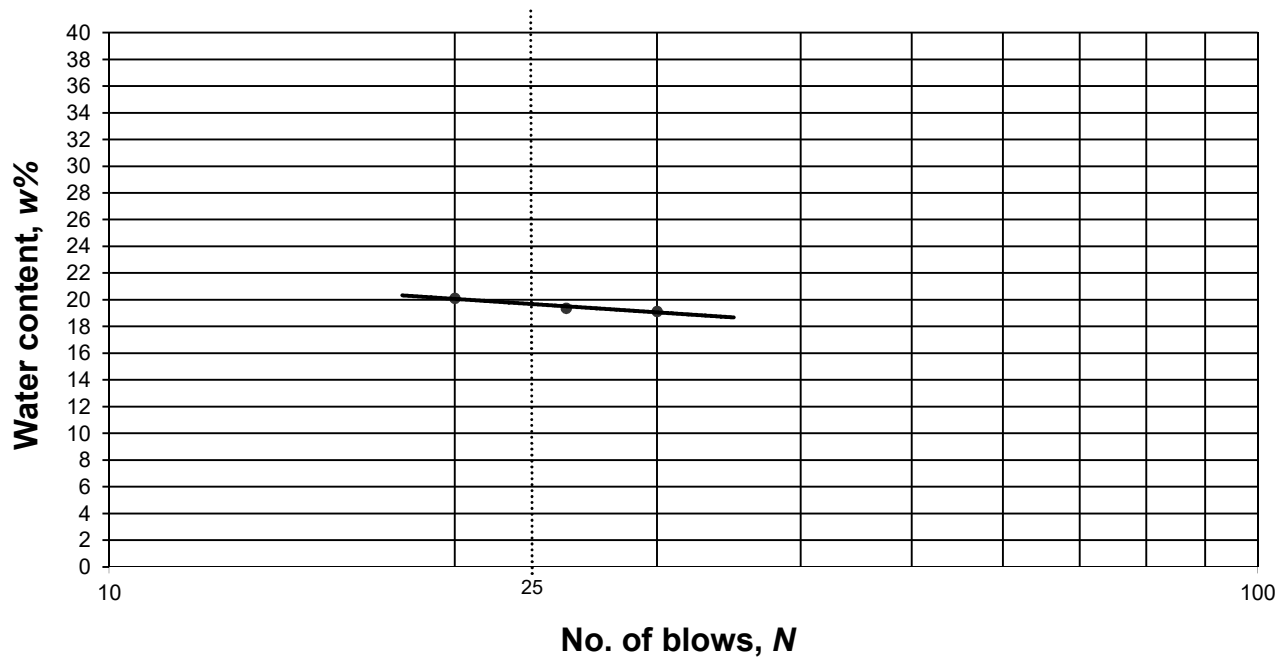
Atterberg Limits

AASHTO T89, 90

<b>Project</b>	US 20 Cont. No. 62D36 Geotech - Baxter Woodman						
<b>Client</b>	Baxter & Woodman, 8678 Ridgefield Road, Crystal Lake, IL 60012						
<b>File No.</b>	7698	<b>Sample #</b>	B-14 SS-04	<b>Date Tested</b>	6/21/2017	<b>Tested By</b>	PP
						<b>Qc By</b>	RC

<b>Date Sample Recd.</b>	5/8/2017
<b>Sample Location</b>	8.5-10'
<b>Sample Description</b>	Brown SANDY LEAN CLAY, little gravel

### LIQUID LIMIT DETERMINATION



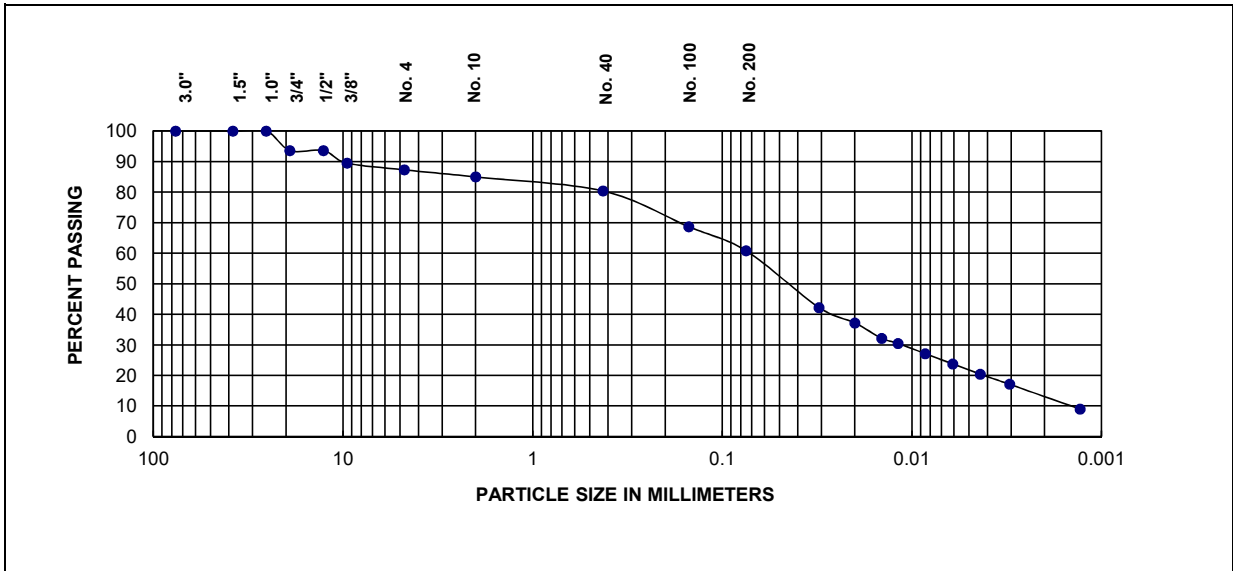
<b>Results</b>					
<b>Liquid Limit, LL</b>	20	<b>Plastic Limit, PL</b>	11	<b>Plasticity Index, PI</b>	9

<b>Remarks</b>	
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**GRAIN SIZE ANALYSIS  
AASHTO T88**

<b>Project</b>	US 20 Cont. No. 62D36 Geotech - Baxter Woodman						
<b>Client</b>	Baxter & Woodman, 8678 Ridgfield Road, Crystal Lake, IL 60012						
<b>File No.</b>	7698	<b>Sample #</b>	B-14 SS-04	<b>Date Tested</b>	6/2/2017	<b>Tested by</b>	PP
						<b>Qc by</b>	RC
<b>Date Sample Received:</b>	5/8/2017						
<b>Sample Location</b>	8.5-10'						
<b>Sample Description</b>	Brown SANDY LEAN CLAY, little gravel						



% + 3"	% Gravel	% Sand	Fines	
			% Silt	% Clay
0.0	12.7	26.5	38.9	21.9

For coarse-grained soils with <12% Fines	D60(mm)	D30(mm)	D10(mm)	Cu	Cc

Sieve Size	Percent Passing	Liquid Limit, L <sub>L</sub>	Plastic Limit, PL	Plasticity Index, PI
3.0"	100.0	20	11	9
1.5"	100.0			
1.0"	100.0			
3/4"	93.6	<b>Soil Classification:</b> CL		
1/2"	93.6	<b>Soil Description:</b> Sandy lean clay		
3/8"	89.5	<b>System:</b> USCS		
No. 4	87.3			
No. 10	85.0			
No. 40	80.4			
No. 100	68.7			
No. 200	60.8			

Remarks:

IDH Classification: Loam; AASHTO Classification: A-4(3)





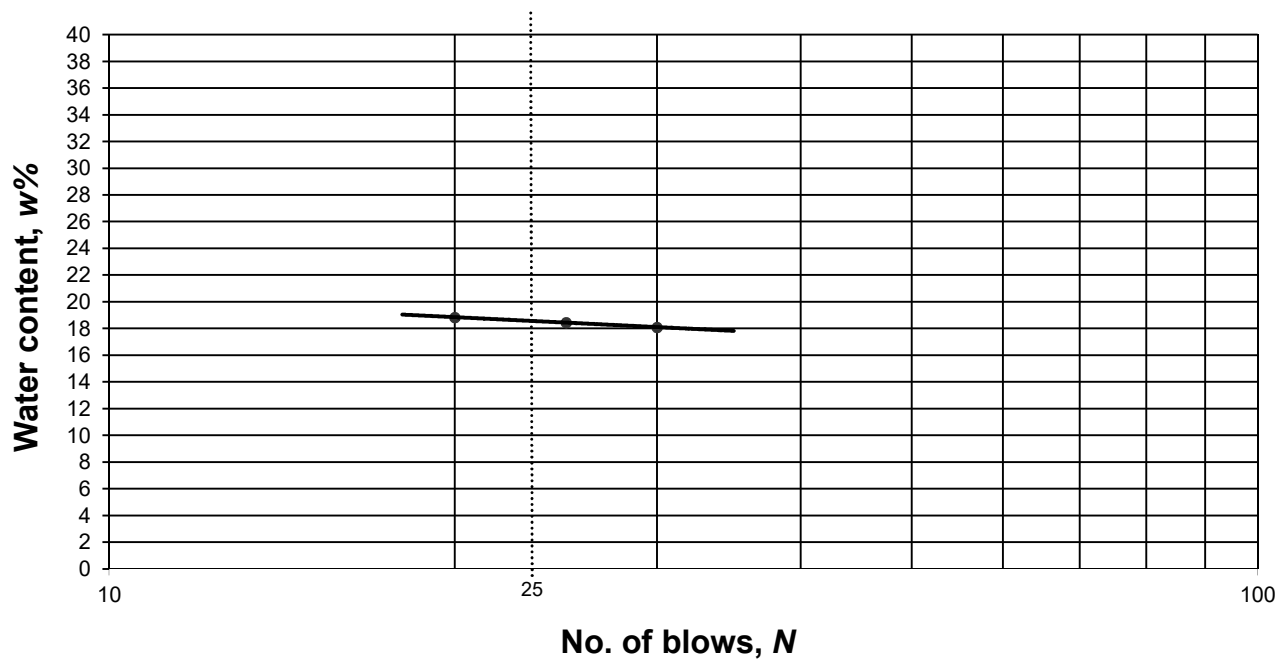
Atterberg Limits

AASHTO T89, 90

<b>Project</b>	US 20 Cont. No. 62D36 Geotech - Baxter Woodman						
<b>Client</b>	Baxter & Woodman, 8678 Ridgefield Road, Crystal Lake, IL 60012						
<b>File No.</b>	7698	<b>Sample #</b>	B-15 ST-06	<b>Date Tested</b>	6/1/2017	<b>Tested By</b>	PP
						<b>Qc By</b>	RC

<b>Date Sample Recd.</b>	5/10/2017
<b>Sample Location</b>	12.5-14.5
<b>Sample Description</b>	Pale brown (10YR 6/3)SANDY LEAN CLAY, trace gravel

### LIQUID LIMIT DETERMINATION



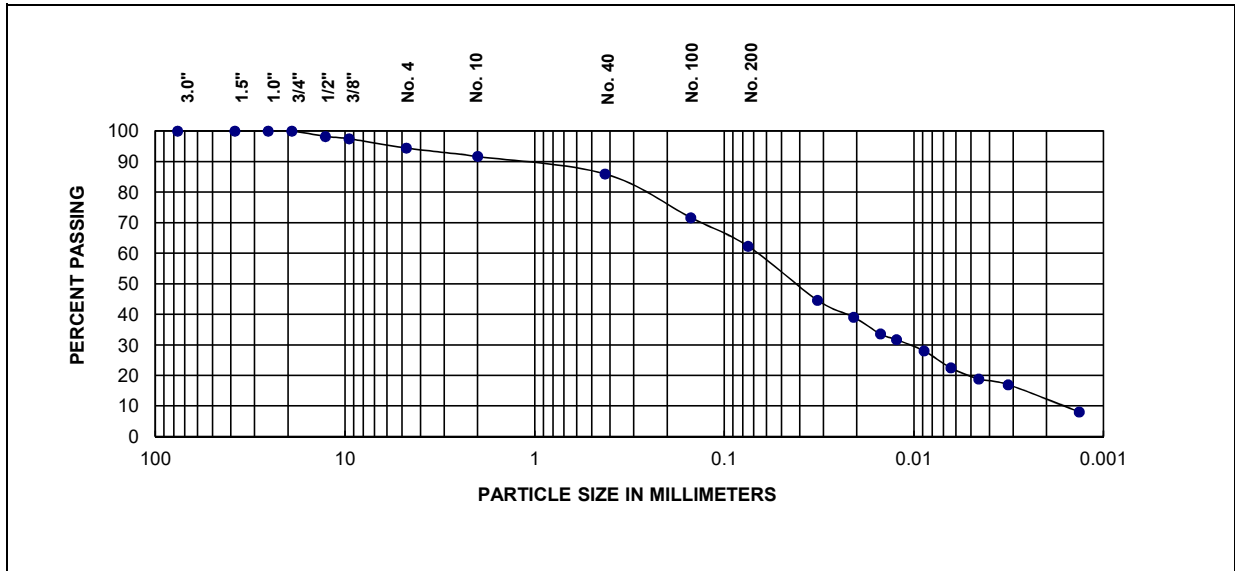
<b>Results</b>					
<b>Liquid Limit, LL</b>	18	<b>Plastic Limit, PL</b>	12	<b>Plasticity Index, PI</b>	6

<b>Remarks</b>	
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**GRAIN SIZE ANALYSIS  
AASHTO T88**

<b>Project</b>	US 20 Cont. No. 62D36 Geotech - Baxter Woodman						
<b>Client</b>	Baxter & Woodman, 8678 Ridgfield Road, Crystal Lake, IL 60012						
<b>File No.</b>	7698	<b>Sample #</b>	B-15 ST-06	<b>Date Tested</b>	6/2/2017	<b>Tested by</b>	PP
						<b>Qc by</b>	RC
<b>Date Sample Received:</b>	5/10/2017						
<b>Sample Location</b>	12.5-14.5						
<b>Sample Description</b>	Pale brown (10YR 6/3) SANDY LEAN CLAY, trace gravel						



% + 3"	% Gravel	% Sand	Fines	
			% Silt	% Clay
0.0	5.6	32.1	42.1	20.2

For coarse-grained soils with <12% Fines	D60(mm)	D30(mm)	D10(mm)	Cu	Cc

Sieve Size	Percent Passing	Liquid Limit, L <sub>L</sub>	Plastic Limit, PL	Plasticity Index, PI
3.0"	100.0	18	12	6
1.5"	100.0			
1.0"	100.0			
3/4"	100.0	<b>Soil Classification:</b> CL-ML		
1/2"	98.3	<b>Soil Description:</b> Sandy silty clay		
3/8"	97.5	<b>System:</b> USCS		
No. 4	94.4			
No. 10	91.7			
No. 40	86.0			
No. 100	71.6			
No. 200	62.3			

Remarks:

IDH Classification: Loam; AASHTO Classification: A-4(1)

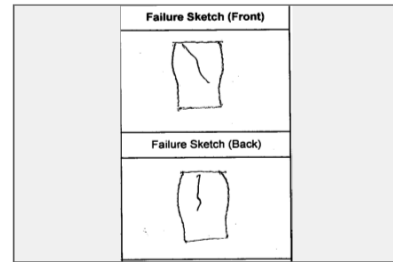


**UNCONFINED COMPRESSIVE STRENGTH (ASTM D 2166)**

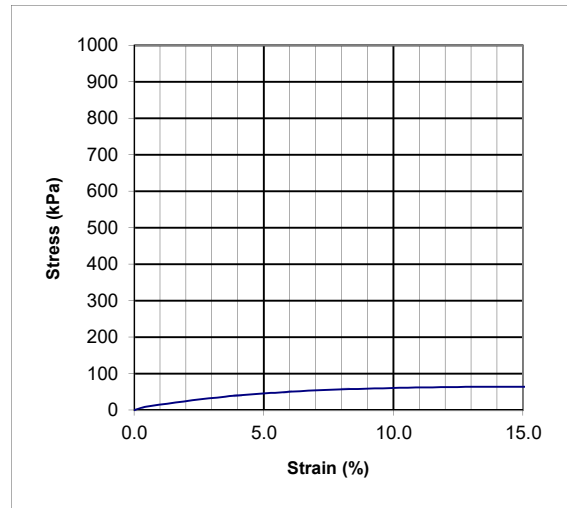
<b>Project</b>	US 20 Cont. No. 62D36 Geotech - Baxter Woodman						
<b>Client</b>	Baxter & Woodman, 8678 Ridgefield Road, Crystal Lake, IL 60012						
<b>File No.</b>	7698	<b>Sample No.</b>	B-15 ST-06	<b>Date Tested</b>	5/24/17	<b>Tested By</b>	PP
						<b>QC By</b>	RC

<b>Date Sample Received</b>	5/10/17
<b>Description of Soil</b>	pale brown (10YR 6/3) Sandy Clay , trace to little gravel
<b>Location</b>	12.5'-14.5'

Type of Sample	SS
Average Height =	15.89 cm
Average Diameter =	7.23 cm
Height/Diameter Ratio =	2.20
Wet Sample Weight=	1527.17 g
Wet Density =	2.34 g/cc
Moisture Content =	12.5 %
Dry Density =	2.08 g/cc
Strain Rate =	1.00 %/min



Failure Image



<b>Unconfined Compressive Strength =</b>	63.9 kPa 1335 psf
<b>Shear Strength =</b>	32 kPa 668 psf
<b>Strain at Failure =</b>	15.0 %

Remarks:

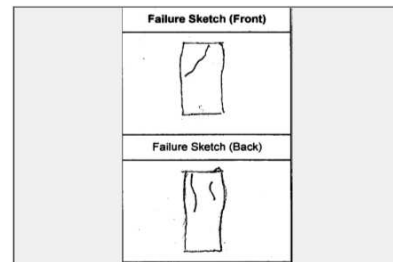


**UNCONFINED COMPRESSIVE STRENGTH (ASTM D 2166)**

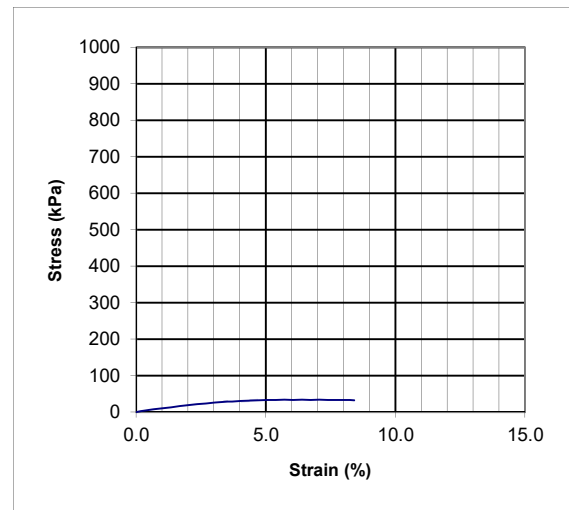
<b>Project</b>	US 20 Cont. No. 62D36 Geotech - Baxter Woodman						
<b>Client</b>	Baxter & Woodman, 8678 Ridgefield Road, Crystal Lake, IL 60012						
<b>File No.</b>	7698	<b>Sample No.</b>	B-16 ST-03	<b>Date Tested</b>	5/23/17	<b>Tested By</b>	PP
						<b>QC By</b>	RC

<b>Date Sample Received</b>	5/8/17
<b>Description of Soil</b>	
<b>Location</b>	5-7'

Type of Sample	SS	
Average Height =	15.10	cm
Average Diameter =	7.18	cm
Height/Diameter Ratio =	2.10	
Wet Sample Weight =	971.81	g
Wet Density =	1.59	g/cc
Moisture Content =	64.3	%
Dry Density =	0.97	g/cc
Strain Rate =	1.00	%/min



Failure Image



<b>Unconfined Compressive Strength =</b>	33.7 kPa
	<b>703 psf</b>
<b>Shear Strength =</b>	17 kPa
	352 psf
<b>Strain at Failure =</b>	7.1 %

**Remarks:**



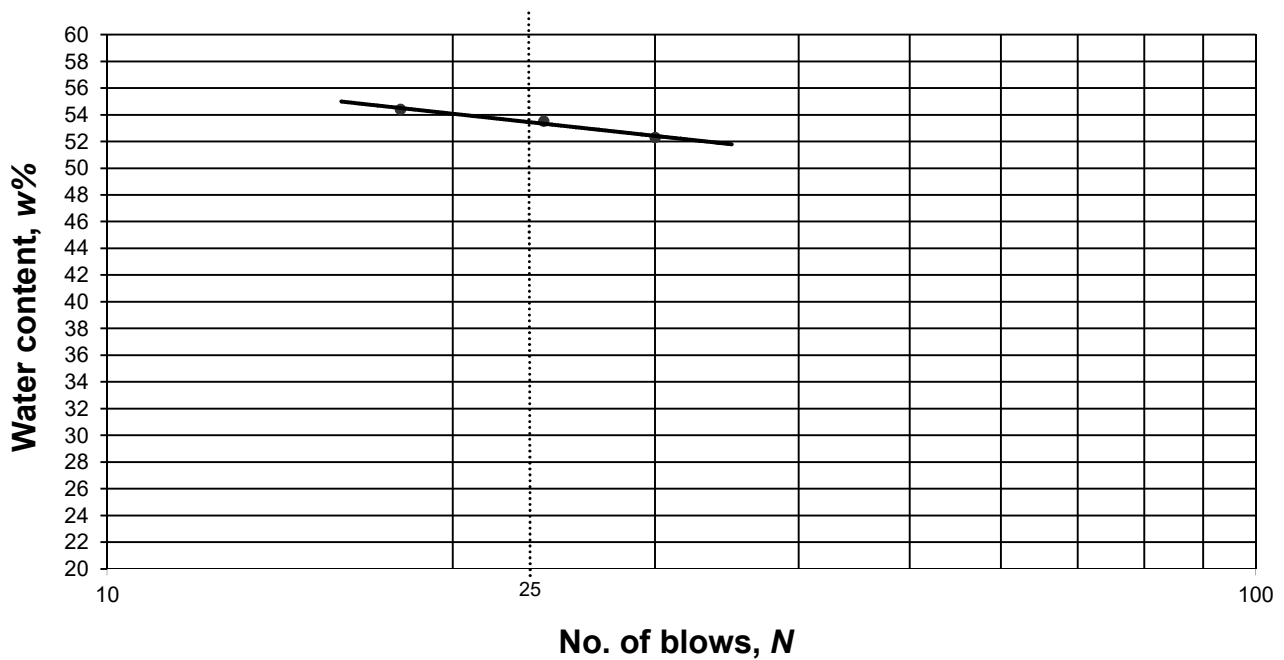
Atterberg Limits

AASHTO T89, 90

<b>Project</b>	US 20 Cont. No. 62D36 Geotech - Baxter Woodman						
<b>Client</b>	Baxter & Woodman, 8678 Ridgefield Road, Crystal Lake, IL 60012						
<b>File No.</b>	7698	<b>Sample #</b>	B-16 ST-04	<b>Date Tested</b>	7/10/2017	<b>Tested By</b>	PP
						<b>Qc By</b>	RC

<b>Date Sample Recd.</b>	5/8/2017
<b>Sample Location</b>	7-9'
<b>Sample Description</b>	light gray (10YR 7/1)

### LIQUID LIMIT DETERMINATION



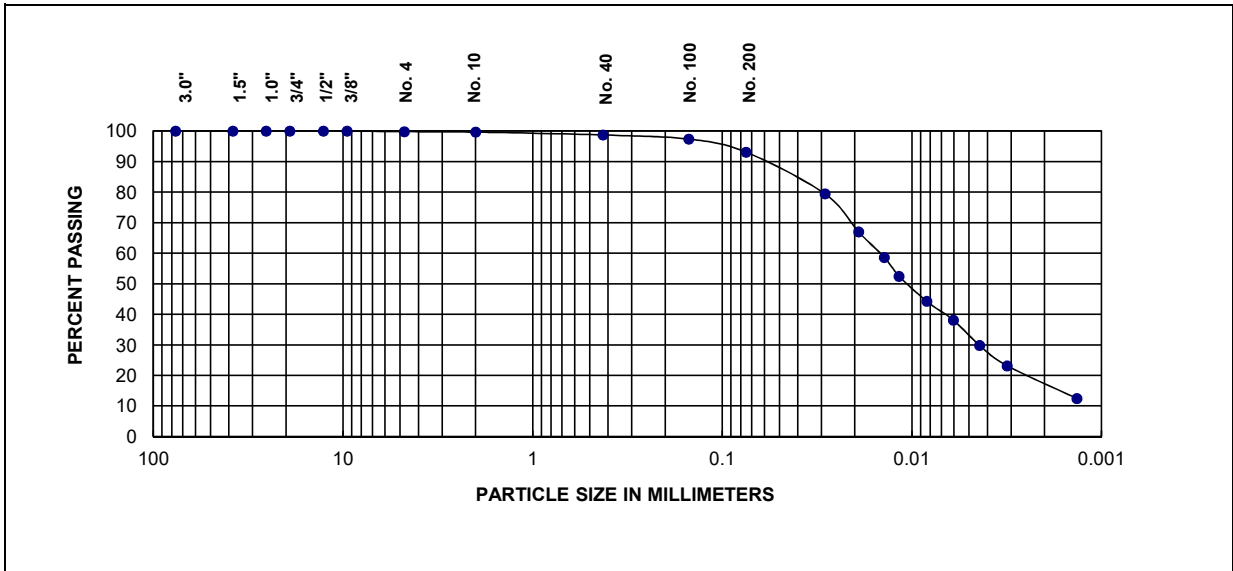
<b>Results</b>					
<b>Liquid Limit, LL</b>	53	<b>Plastic Limit, PL</b>	41	<b>Plasticity Index, PI</b>	12

<b>Remarks</b>	
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**GRAIN SIZE ANALYSIS  
AASHTO T88**

<b>Project</b>	US 20 Cont. No. 62D36 Geotech - Baxter Woodman						
<b>Client</b>	Baxter & Woodman, 8678 Ridgfield Road, Crystal Lake, IL 60012						
<b>File No.</b>	7698	<b>Sample #</b>	B-16 ST-04	<b>Date Tested</b>	7/10/2017	<b>Tested by</b>	PP
						<b>Qc by</b>	RC
<b>Date Sample Received:</b>	5/8/2017						
<b>Sample Location</b>	7-9'						
<b>Sample Description</b>	light gray (10YR 7/1)						



% + 3"	% Gravel	% Sand	Fines	
			% Silt	% Clay
0.0	0.2	6.7	59.8	33.3

For coarse-grained soils with <12% Fines	D60(mm)	D30(mm)	D10(mm)	Cu	Cc

Sieve Size	Percent Passing	Liquid Limit, L <sub>L</sub>	Plastic Limit, PL	Plasticity Index, PI
3.0"	100.0	53	41	12
1.5"	100.0			
1.0"	100.0			
3/4"	100.0	<b>Soil Classification:</b> MH		
1/2"	100.0	<b>Soil Description:</b> Elastic silt		
3/8"	100.0	<b>System:</b> USCS		
No. 4	99.8			
No. 10	99.6			
No. 40	98.7			
No. 100	97.3			
No. 200	93.1			

Remarks:

IDH Classification: Silty loam; AASHTO Classification: A-7-6(17)

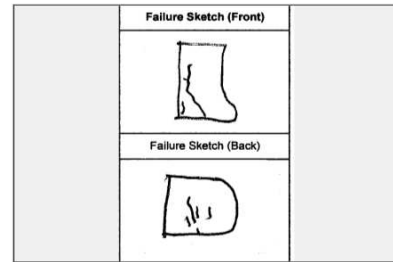


**UNCONFINED COMPRESSIVE STRENGTH (ASTM D 2166)**

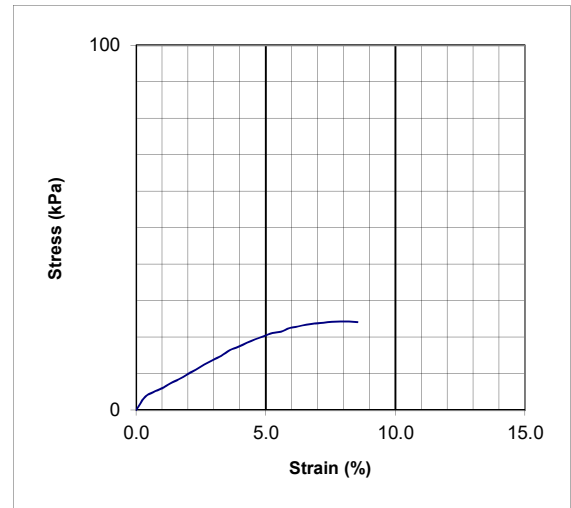
<b>Project</b>	US 20 Cont. No. 62D36 Geotech - Baxter Woodman						
<b>Client</b>	Baxter & Woodman, 8678 Ridgefield Road, Crystal Lake, IL 60012						
<b>File No.</b>	7698	<b>Sample No.</b>	B-16 ST-04	<b>Date Tested</b>	7/5/17	<b>Tested By</b>	PP
						<b>QC By</b>	RC

<b>Date Sample Received</b>	5/8/17
<b>Description of Soil</b>	light gray (10YR 7/1)
<b>Location</b>	7-9'

Type of Sample	SS
Average Height =	15.47 cm
Average Diameter =	7.16 cm
Height/Diameter Ratio =	2.16
Wet Sample Weight =	961.08 g
Wet Density =	1.54 g/cc
Moisture Content =	80.3 %
Dry Density =	0.86 g/cc
Strain Rate =	1.00 %/min



Failure Image



<b>Unconfined Compressive Strength =</b>	24.3 kPa
	<b>507 psf</b>
<b>Shear Strength =</b>	12 kPa
	254 psf
<b>Strain at Failure =</b>	7.9 %

**Remarks:**

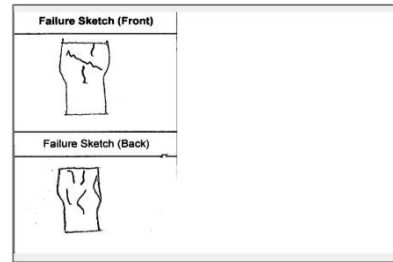


**UNCONFINED COMPRESSIVE STRENGTH (ASTM D 2166)**

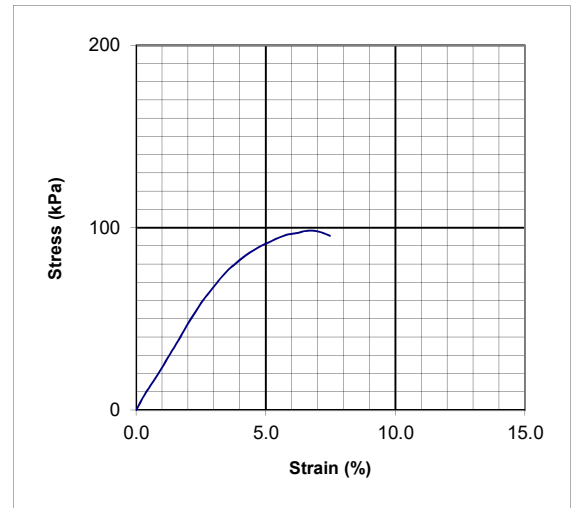
<b>Project</b>	US 20 Cont. No. 62D36 Geotech - Baxter Woodman						
<b>Client</b>	Baxter & Woodman, 8678 Ridgefield Road, Crystal Lake, IL 60012						
<b>File No.</b>	7698	<b>Sample No.</b>	B-17 ST-07	<b>Date Tested</b>	5/18/17	<b>Tested By</b>	PP
						<b>QC By</b>	RC

<b>Date Sample Received</b>	5/10/17
<b>Description of Soil</b>	Pale brown (10 YR 6/3) Clay loam, trace fine gravel
<b>Location</b>	15-17' (15-16')

Type of Sample	SS
Average Height =	15.64 cm
Average Diameter =	7.25 cm
Height/Diameter Ratio =	2.16
Wet Sample Weight =	1539.08 g
Wet Density =	2.38 g/cc
Moisture Content =	9.9 %
Dry Density =	2.17 g/cc
Strain Rate =	1.00 %/min



Failure Image



<b>Unconfined Compressive Strength =</b>	98.4 kPa <b>2054 psf</b>
<b>Shear Strength =</b>	49 kPa 1028 psf
<b>Strain at Failure =</b>	6.8 %

Remarks:





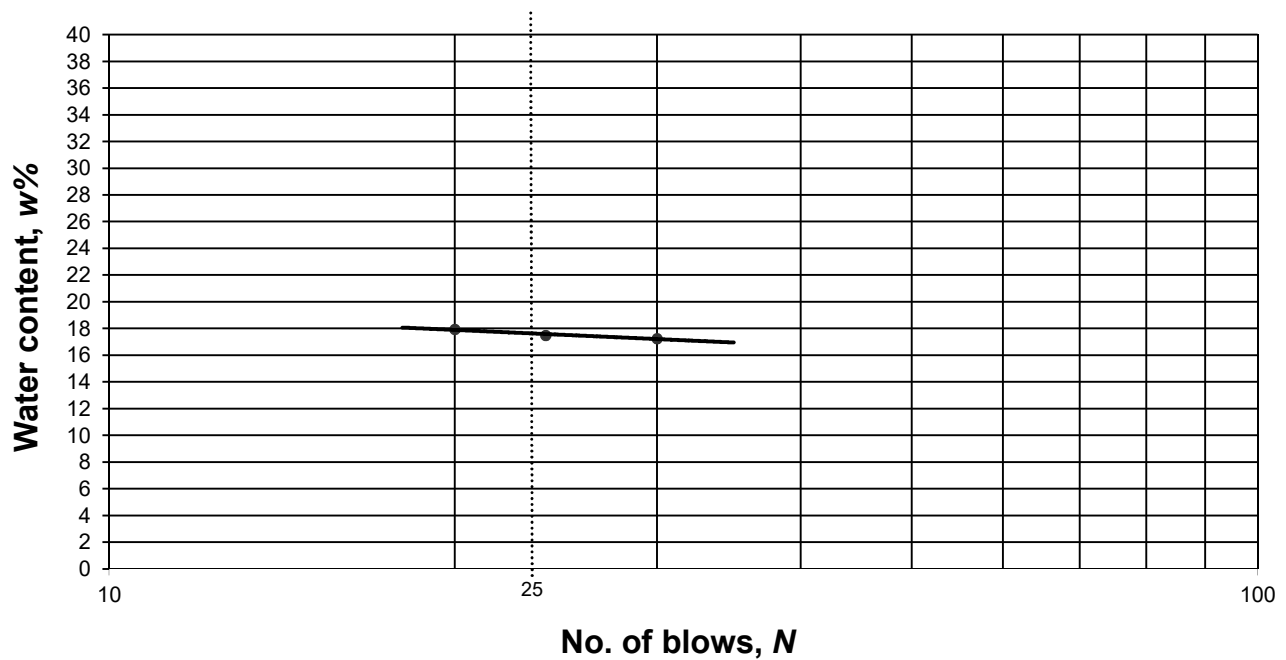
Atterberg Limits

AASHTO T89, 90

<b>Project</b>	US 20 Cont. No. 62D36 Geotech - Baxter Woodman						
<b>Client</b>	Baxter & Woodman, 8678 Ridgefield Road, Crystal Lake, IL 60012						
<b>File No.</b>	7698	<b>Sample #</b>	B-18 SS-05	<b>Date Tested</b>	6/1/2017	<b>Tested By</b>	PP
						<b>Qc By</b>	RC

<b>Date Sample Recd.</b>	5/9/2017
<b>Sample Location</b>	11-12.5'
<b>Sample Description</b>	Pale Brown (10YR 6/3) SANDY LEAN CLAY, trace gravel

### LIQUID LIMIT DETERMINATION



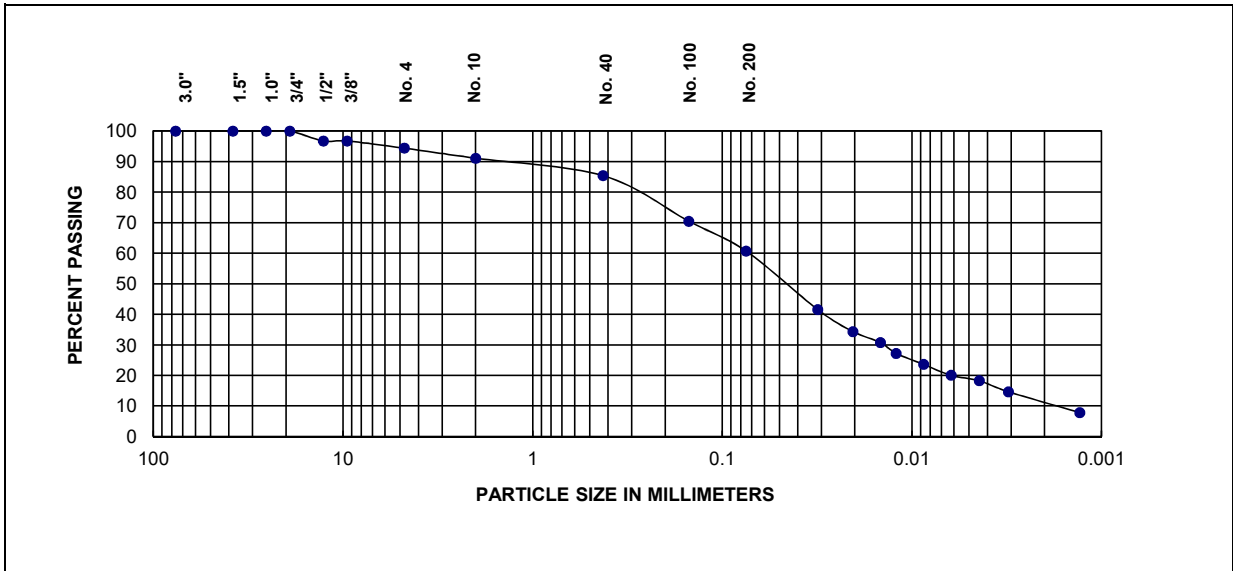
<b>Results</b>					
<b>Liquid Limit, LL</b>	18	<b>Plastic Limit, PL</b>	12	<b>Plasticity Index, PI</b>	6

<b>Remarks</b>	
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**GRAIN SIZE ANALYSIS  
AASHTO T88**

<b>Project</b>	US 20 Cont. No. 62D36 Geotech - Baxter Woodman						
<b>Client</b>	Baxter & Woodman, 8678 Ridgfield Road, Crystal Lake, IL 60012						
<b>File No.</b>	7698	<b>Sample #</b>	B-18 SS-05	<b>Date Tested</b>	6/2/2017	<b>Tested by</b>	PP
						<b>Qc by</b>	RC
<b>Date Sample Received:</b>	5/9/2017						
<b>Sample Location</b>	11-12.5'						
<b>Sample Description</b>	Pale Brown (10YR 6/3) SANDY LEAN CLAY, trace gravel						



% + 3"	% Gravel	% Sand	Fines	
			% Silt	% Clay
0.0	5.6	33.7	41.8	18.9

For coarse-grained soils with <12% Fines	D60(mm)	D30(mm)	D10(mm)	Cu	Cc

Sieve Size	Percent Passing	Liquid Limit, L <sub>L</sub>	Plastic Limit, PL	Plasticity Index, PI
3.0"	100.0	18	12	6
1.5"	100.0			
1.0"	100.0			
3/4"	100.0	<b>Soil Classification:</b> CL-ML		
1/2"	96.7	<b>Soil Description:</b> Sandy silty clay		
3/8"	96.7	<b>System:</b> USCS		
No. 4	94.4			
No. 10	91.1			
No. 40	85.4			
No. 100	70.5			
No. 200	60.7			

Remarks:

IDH Classification: Loam; AASHTO Classification: A-4(1)

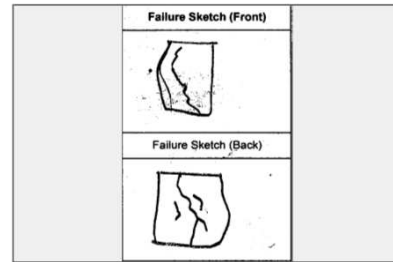


**UNCONFINED COMPRESSIVE STRENGTH (ASTM D 2166)**

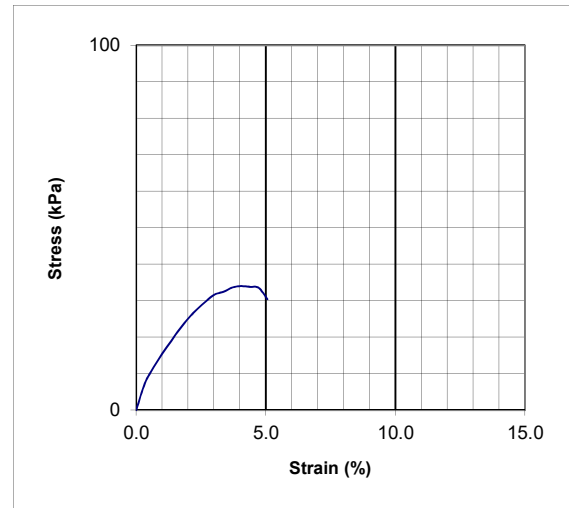
<b>Project</b>	US 20 Cont. No. 62D36 Geotech - Baxter Woodman						
<b>Client</b>	Baxter & Woodman, 8678 Ridgefield Road, Crystal Lake, IL 60012						
<b>File No.</b>	7698	<b>Sample No.</b>	B-18 ST-03	<b>Date Tested</b>	7/5/17	<b>Tested By</b>	ES
						<b>QC By</b>	RC

<b>Date Sample Received</b>	5/9/17
<b>Description of Soil</b>	Black (10YR 2/1)
<b>Location</b>	6-8'

Type of Sample	ST
Average Height =	15.05 cm
Average Diameter =	7.20 cm
Height/Diameter Ratio =	2.09
Wet Sample Weight =	881.25 g
Wet Density =	1.44 g/cc
Moisture Content =	73.5 %
Dry Density =	0.83 g/cc
Strain Rate =	1.00 %/min



Failure Image



<b>Unconfined Compressive Strength =</b>	34.0 kPa <b>710 psf</b>
<b>Shear Strength =</b>	17 kPa 355 psf
<b>Strain at Failure =</b>	4.4 %

Remarks:



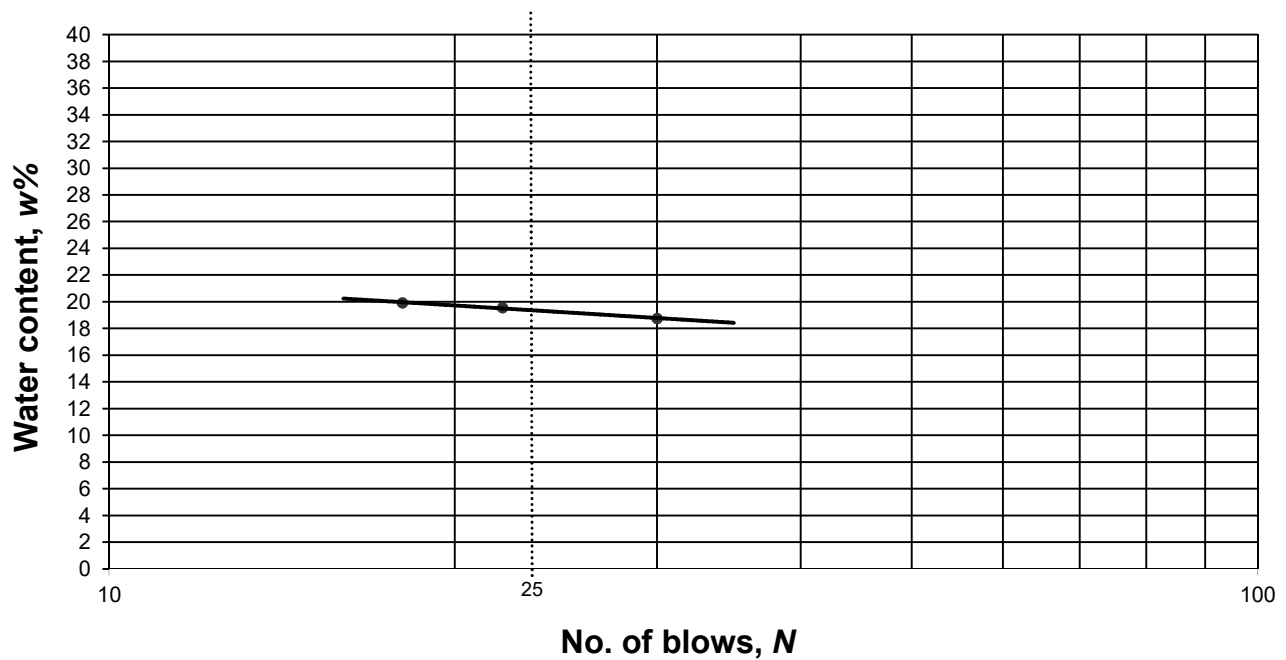
Atterberg Limits

AASHTO T89, 90

<b>Project</b>	US 20 Cont. No. 62D36 Geotech - Baxter Woodman						
<b>Client</b>	Baxter & Woodman, 8678 Ridgefield Road, Crystal Lake, IL 60012						
<b>File No.</b>	7698	<b>Sample #</b>	B-20 ST-04	<b>Date Tested</b>	7/10/2017	<b>Tested By</b>	PP
						<b>Qc By</b>	RC

<b>Date Sample Recd.</b>	5/9/2017
<b>Sample Location</b>	7.5-9.5'
<b>Sample Description</b>	Brown (10YR 5/3) SANDY LEAN CLAY, trace gravel

### LIQUID LIMIT DETERMINATION



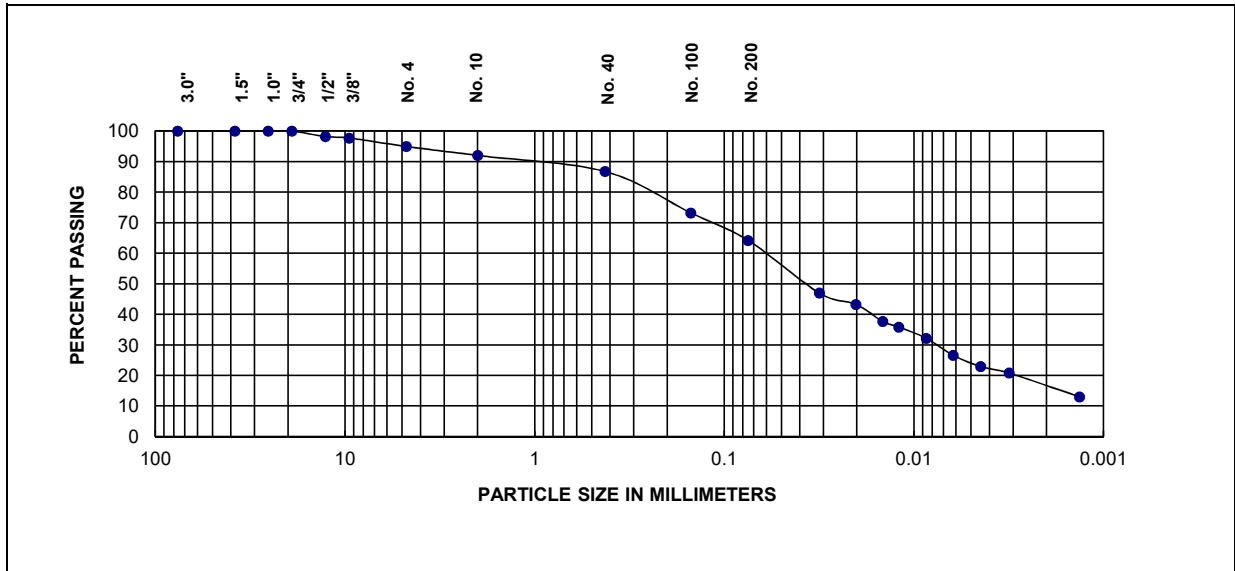
<b>Results</b>					
<b>Liquid Limit, LL</b>	19	<b>Plastic Limit, PL</b>	11	<b>Plasticity Index, PI</b>	8

<b>Remarks</b>	
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**GRAIN SIZE ANALYSIS  
AASHTO T88**

<b>Project</b>	US 20 Cont. No. 62D36 Geotech - Baxter Woodman						
<b>Client</b>	Baxter & Woodman, 8678 Ridgfield Road, Crystal Lake, IL 60012						
<b>File No.</b>	7698	<b>Sample #</b>	B-20 ST-04	<b>Date Tested</b>	7/10/2017	<b>Tested by</b>	PP
						<b>Qc by</b>	RC
<b>Date Sample Received:</b>	5/9/2017						
<b>Sample Location</b>	7.5-9.5'						
<b>Sample Description</b>	Brown (10YR 5/3) SANDY LEAN CLAY, trace gravel						



% + 3"	% Gravel	% Sand	Fines	
			% Silt	% Clay
0.0	5.0	30.8	39.7	24.5

For coarse-grained soils with <12% Fines	D60(mm)	D30(mm)	D10(mm)	Cu	Cc

Sieve Size	Percent Passing	Liquid Limit, L <sub>L</sub>	Plastic Limit, PL	Plasticity Index, PI
3.0"	100.0	19	11	8
1.5"	100.0			
1.0"	100.0			
3/4"	100.0	<b>Soil Classification:</b> CL		
1/2"	98.2	<b>Soil Description:</b> Sandy lean clay		
3/8"	97.7	<b>System:</b> USCS		
No. 4	95.0			
No. 10	92.0			
No. 40	86.8			
No. 100	73.2			
No. 200	64.2			

Remarks:

IDH Classification: Loam; AASHTO Classification: A-4(3)

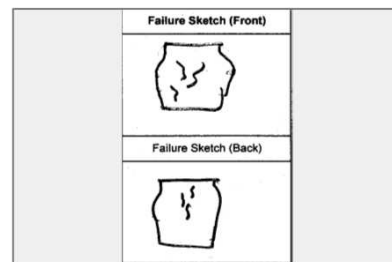


**UNCONFINED COMPRESSIVE STRENGTH (ASTM D 2166)**

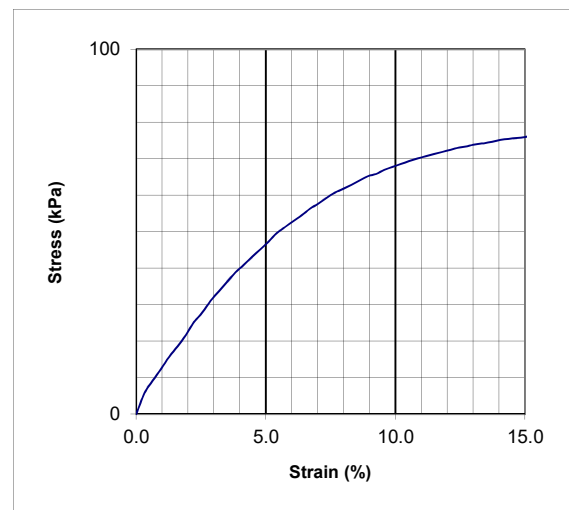
<b>Project</b>	US 20 Cont. No. 62D36 Geotech - Baxter Woodman						
<b>Client</b>	Baxter & Woodman, 8678 Ridgefield Road, Crystal Lake, IL 60012						
<b>File No.</b>	7698	<b>Sample No.</b>	B-20 ST-04	<b>Date Tested</b>	7/5/17	<b>Tested By</b>	ES
						<b>QC By</b>	RC

<b>Date Sample Received</b>	5/9/17
<b>Description of Soil</b>	Brown (10YR 5/3) SANDY LEAN CLAY, trace gravel
<b>Location</b>	7.5-9.5'

Type of Sample	ST
Average Height =	15.91 cm
Average Diameter =	7.23 cm
Height/Diameter Ratio =	2.20
Wet Sample Weight =	1494.34 g
Wet Density =	2.29 g/cc
Moisture Content =	13.5 %
Dry Density =	2.01 g/cc
Strain Rate =	1.00 %/min



Failure Image



<b>Unconfined Compressive Strength =</b>	75.9 kPa <b>1585 psf</b>
<b>Shear Strength =</b>	38 kPa 793 psf
<b>Strain at Failure =</b>	15.0 %

Remarks:

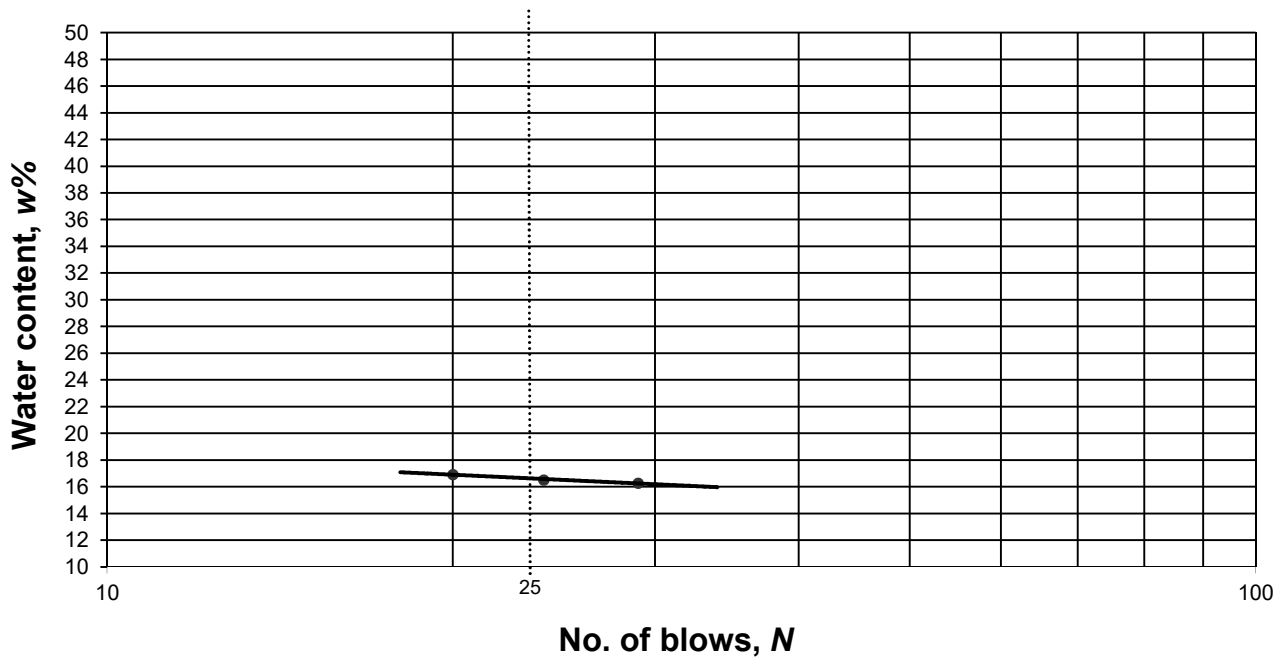


Atterberg Limits  
AASHTO T89, 90

<b>Project</b>	US 20 Cont. No. 62D36 Geotech - Baxter Woodman						
<b>Client</b>	Baxter & Woodman, 8678 Ridgefield Road, Crystal Lake, IL 60012						
<b>File No.</b>	7698	<b>Sample #</b>	B-21 ST-06	<b>Date Tested</b>	6/1/2017	<b>Tested By</b>	PP
						<b>Qc By</b>	RC

<b>Date Sample Recd.</b>	5/9/2017
<b>Sample Location</b>	12.5-14.5'
<b>Sample Description</b>	Pale brown (10 YR 6/3) SANDY SILTY CLAY, trace gravel

### LIQUID LIMIT DETERMINATION



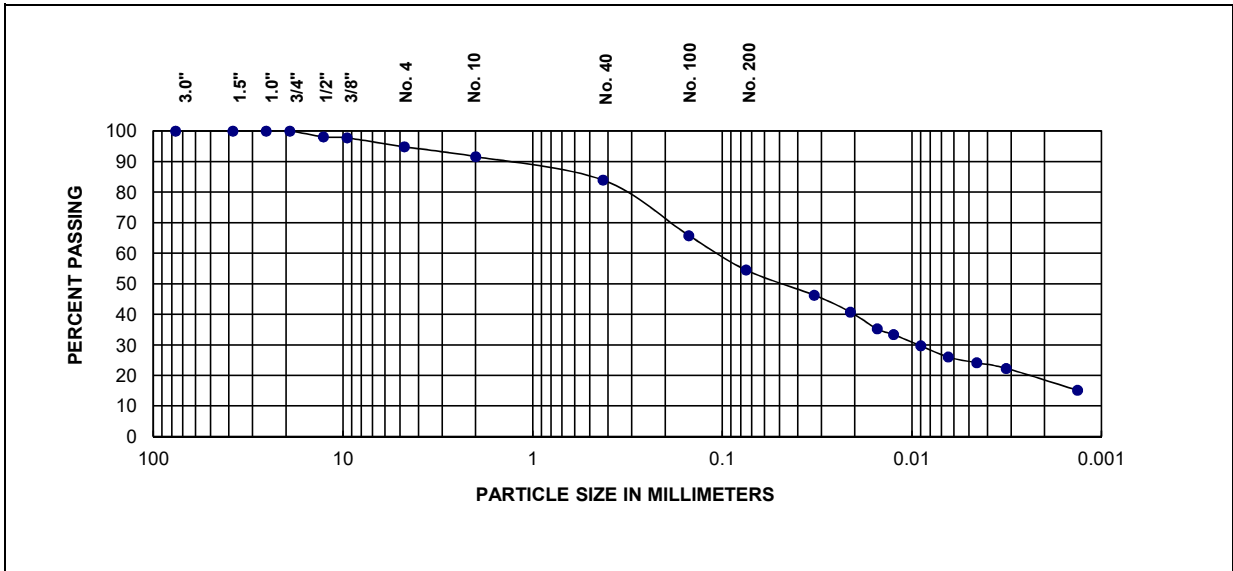
<b>Results</b>					
<b>Liquid Limit, LL</b>	17	<b>Plastic Limit, PL</b>	11	<b>Plasticity Index, PI</b>	6

<b>Remarks</b>	
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**GRAIN SIZE ANALYSIS  
AASHTO T88**

<b>Project</b>	US 20 Cont. No. 62D36 Geotech - Baxter Woodman						
<b>Client</b>	Baxter & Woodman, 8678 Ridgfield Road, Crystal Lake, IL 60012						
<b>File No.</b>	7698	<b>Sample #</b>	B-21 ST-06	<b>Date Tested</b>	6/2/2017	<b>Tested by</b>	PP
						<b>Qc by</b>	RC
<b>Date Sample Received:</b>	5/9/2017						
<b>Sample Location</b>	12.5-14.5'						
<b>Sample Description</b>	Pale brown (10 YR 6/3) SANDY SILTY CLAY, trace gravel						



% + 3"	% Gravel	% Sand	Fines	
			% Silt	% Clay
0.0	5.2	40.3	29.9	24.6

For coarse-grained soils with <12% Fines	D60(mm)	D30(mm)	D10(mm)	Cu	Cc

Sieve Size	Percent Passing	Liquid Limit, L <sub>L</sub>	Plastic Limit, PL	Plasticity Index, PI
3.0"	100.0	17	11	6
1.5"	100.0			
1.0"	100.0			
3/4"	100.0	<b>Soil Classification:</b> CL-ML		
1/2"	98.1	<b>Soil Description:</b> Sandy silty clay		
3/8"	97.7	<b>System:</b> USCS		
No. 4	94.8			
No. 10	91.6			
No. 40	83.9			
No. 100	65.8			
No. 200	54.5			

Remarks:

IDH Classification: Sandy loam; AASHTO Classification: A-4(1)



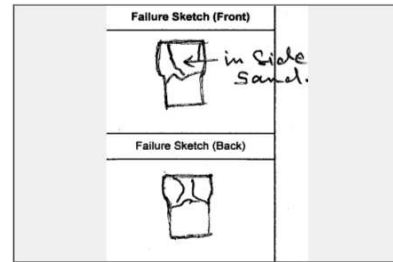


**UNCONFINED COMPRESSIVE STRENGTH (ASTM D 2166)**

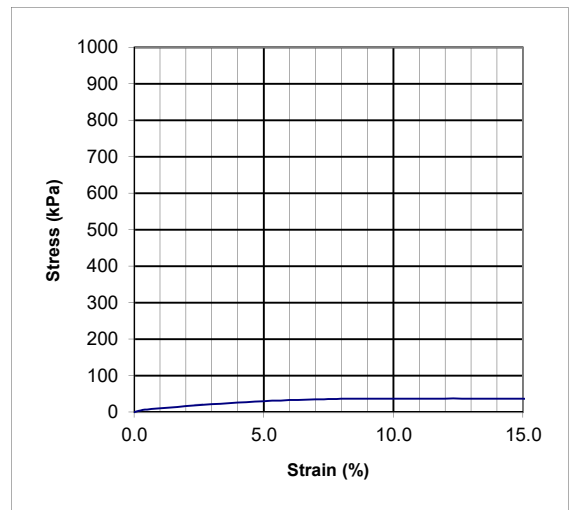
<b>Project</b>	US 20 Cont. No. 62D36 Geotech - Baxter Woodman						
<b>Client</b>	Baxter & Woodman, 8678 Ridgefield Road, Crystal Lake, IL 60012						
<b>File No.</b>	7698	<b>Sample No.</b>	B-21 ST-06	<b>Date Tested</b>	5/23/17	<b>Tested By</b>	PP
						<b>QC By</b>	RC

<b>Date Sample Received</b>	5/9/17
<b>Description of Soil</b>	Pale brown (10 YR 6/3) sandy clay
<b>Location</b>	12.5-14.5'

Type of Sample	ST
Average Height =	15.27 cm
Average Diameter =	7.32 cm
Height/Diameter Ratio =	2.09
Wet Sample Weight =	1481.81 g
Wet Density =	2.30 g/cc
Moisture Content =	11.8 %
Dry Density =	2.06 g/cc
Strain Rate =	1.00 %/min



Failure Image



<b>Unconfined Compressive Strength =</b>	37.2 kPa <b>776 psf</b>
<b>Shear Strength =</b>	19 kPa 388 psf
<b>Strain at Failure =</b>	12.3 %

**Remarks:**



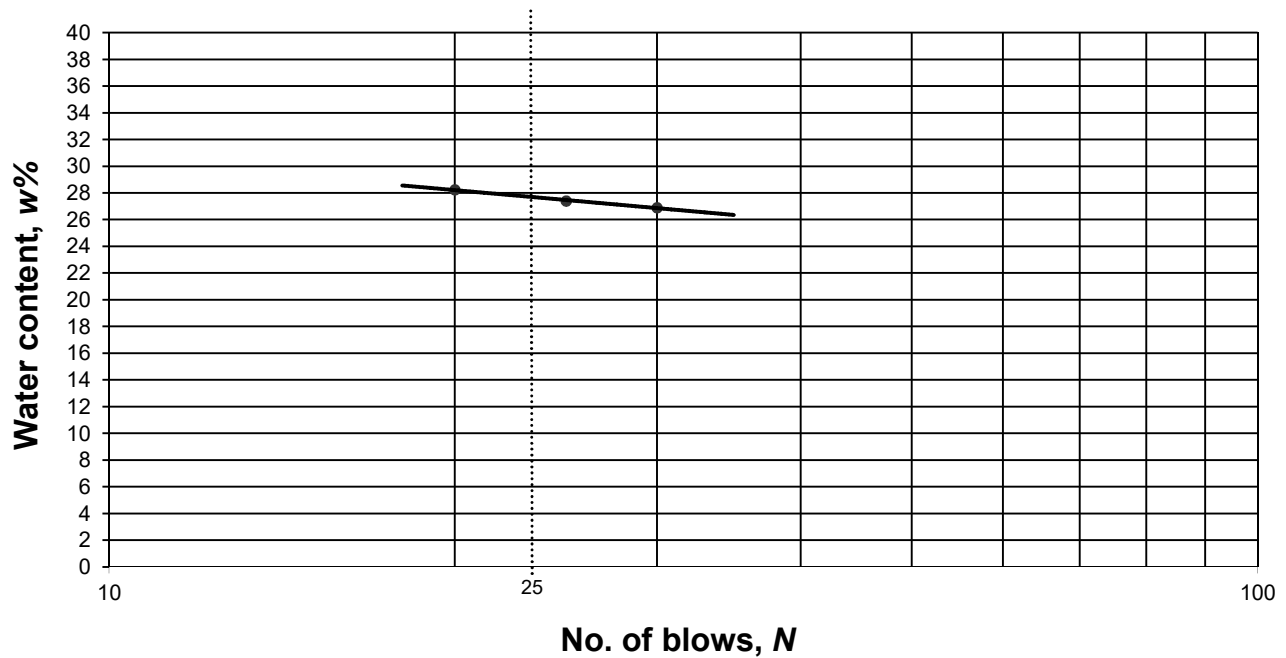
Atterberg Limits

AASHTO T89, 90

<b>Project</b>	US 20 Cont. No. 62D36 Geotech - Baxter Woodman						
<b>Client</b>	Baxter & Woodman, 8678 Ridgefield Road, Crystal Lake, IL 60012						
<b>File No.</b>	7698	<b>Sample #</b>	B-22 ST-04	<b>Date Tested</b>	6/1/2017	<b>Tested By</b>	PP
						<b>Qc By</b>	RC

<b>Date Sample Recd.</b>	5/9/2017
<b>Sample Location</b>	7.5-9.5'
<b>Sample Description</b>	Brown(10YR 5/3) SANDY LEAN CLAY, trace gravel

### LIQUID LIMIT DETERMINATION



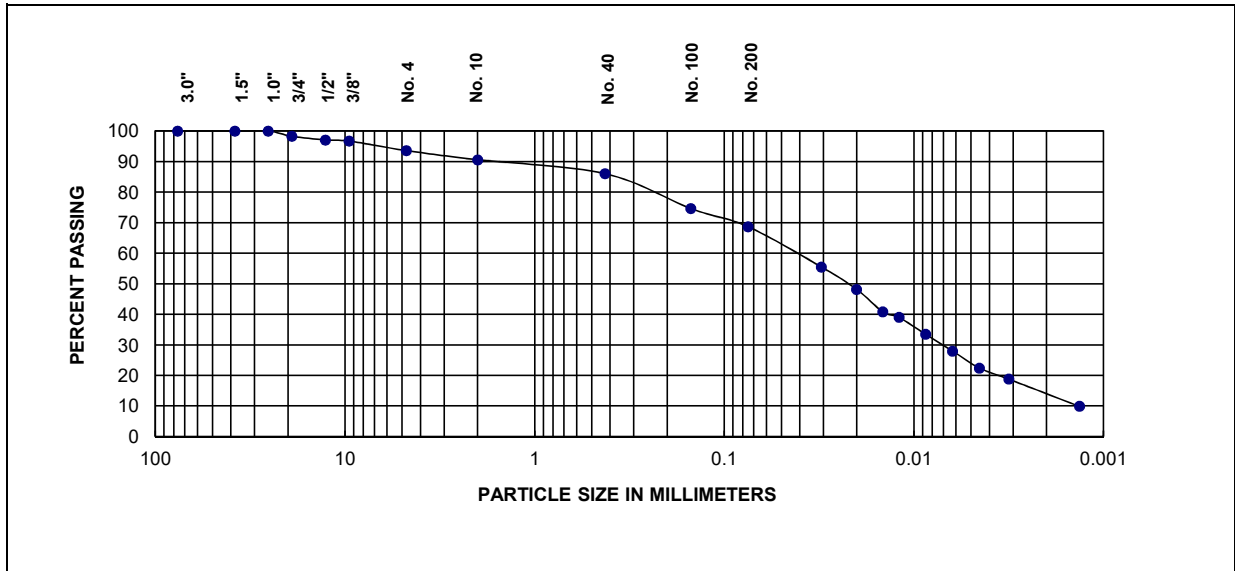
<b>Results</b>					
<b>Liquid Limit, LL</b>	27	<b>Plastic Limit, PL</b>	16	<b>Plasticity Index, PI</b>	11

<b>Remarks</b>	
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**GRAIN SIZE ANALYSIS  
AASHTO T88**

<b>Project</b>	US 20 Cont. No. 62D36 Geotech - Baxter Woodman						
<b>Client</b>	Baxter & Woodman, 8678 Ridgfield Road, Crystal Lake, IL 60012						
<b>File No.</b>	7698	<b>Sample #</b>	B-22 ST-04	<b>Date Tested</b>	6/2/2017	<b>Tested by</b>	PP
						<b>Qc by</b>	RC
<b>Date Sample Received:</b>	5/9/2017						
<b>Sample Location</b>	7.5-9.5'						
<b>Sample Description</b>	Brown(10YR 5/3) SANDY LEAN CLAY, trace gravel						



% + 3"	% Gravel	% Sand	Fines	
			% Silt	% Clay
0.0	6.4	24.9	44.2	24.5

For coarse-grained soils with <12% Fines	D60(mm)	D30(mm)	D10(mm)	Cu	Cc

Sieve Size	Percent Passing	Liquid Limit, L <sub>L</sub>	Plastic Limit, PL	Plasticity Index, PI
3.0"	100.0	27	16	11
1.5"	100.0			
1.0"	100.0			
3/4"	98.3	<b>Soil Classification:</b> CL		
1/2"	97.1	<b>Soil Description:</b> Sandy lean clay		
3/8"	96.7	<b>System:</b> USCS		
No. 4	93.6			
No. 10	90.6			
No. 40	86.1			
No. 100	74.6			
No. 200	68.7			

Remarks:

IDH Classification: Silty loam; AASHTO Classification: A-6(6)

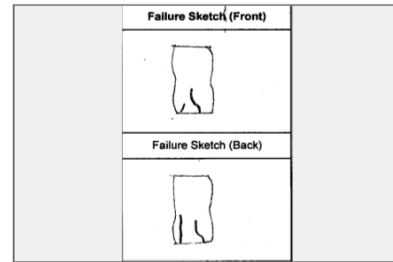


**UNCONFINED COMPRESSIVE STRENGTH (ASTM D 2166)**

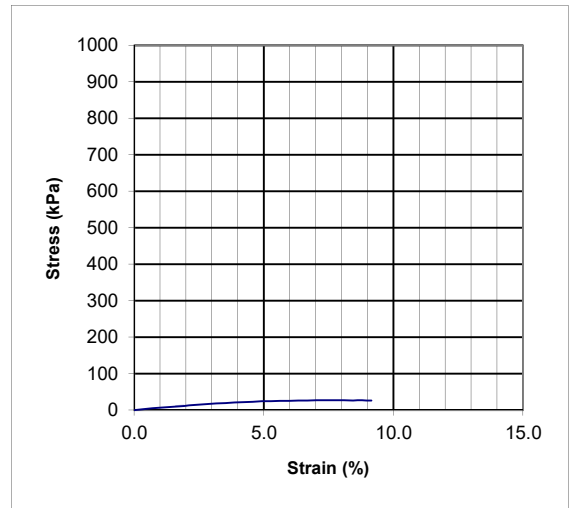
<b>Project</b>	US 20 Cont. No. 62D36 Geotech - Baxter Woodman						
<b>Client</b>	Baxter & Woodman, 8678 Ridgefield Road, Crystal Lake, IL 60012						
<b>File No.</b>	7698	<b>Sample No.</b>	B-22 ST-04	<b>Date Tested</b>	5/23/17	<b>Tested By</b>	PP
						<b>QC By</b>	RC

<b>Date Sample Received</b>	5/9/17
<b>Description of Soil</b>	
<b>Location</b>	7.5-9.5'

Type of Sample	ST
Average Height =	14.44 cm
Average Diameter =	7.15 cm
Height/Diameter Ratio =	2.02
Wet Sample Weight =	1042.89 g
Wet Density =	1.80 g/cc
Moisture Content =	51.4 %
Dry Density =	1.19 g/cc
Strain Rate =	1.00 %/min



Failure Image



<b>Unconfined Compressive Strength =</b>	26.8 kPa <b>560 psf</b>
<b>Shear Strength =</b>	13 kPa 280 psf
<b>Strain at Failure =</b>	7.7 %

**Remarks:**

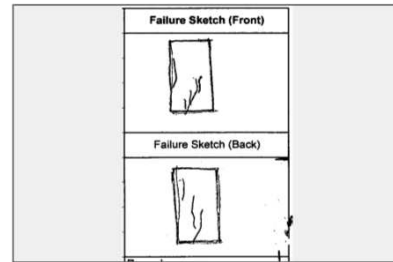


**UNCONFINED COMPRESSIVE STRENGTH (ASTM D 2166)**

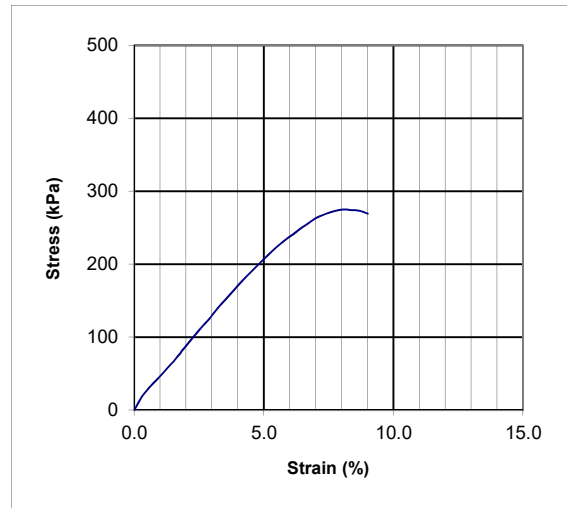
<b>Project</b>	US 20 Cont. No. 62D36 Geotech - Baxter Woodman						
<b>Client</b>	Baxter & Woodman, 8678 Ridgefield Road, Crystal Lake, IL 60012						
<b>File No.</b>	7698	<b>Sample No.</b>	B-22 ST-08	<b>Date Tested</b>	5/17/17	<b>Tested By</b>	PP
						<b>QC By</b>	RC

<b>Date Sample Received</b>	5/9/17
<b>Description of Soil</b>	Pale brown (10 YR 6/3) Silty clay, trace fine gravel, trace-little sand
<b>Location</b>	15-17'

Type of Sample	SS
Average Height =	15.78 cm
Average Diameter =	7.17 cm
Height/Diameter Ratio =	2.20
Wet Sample Weight =	1508.71 g
Wet Density =	2.37 g/cc
Moisture Content =	9.6 %
Dry Density =	2.16 g/cc
Strain Rate =	1.00 %/min



Failure Image



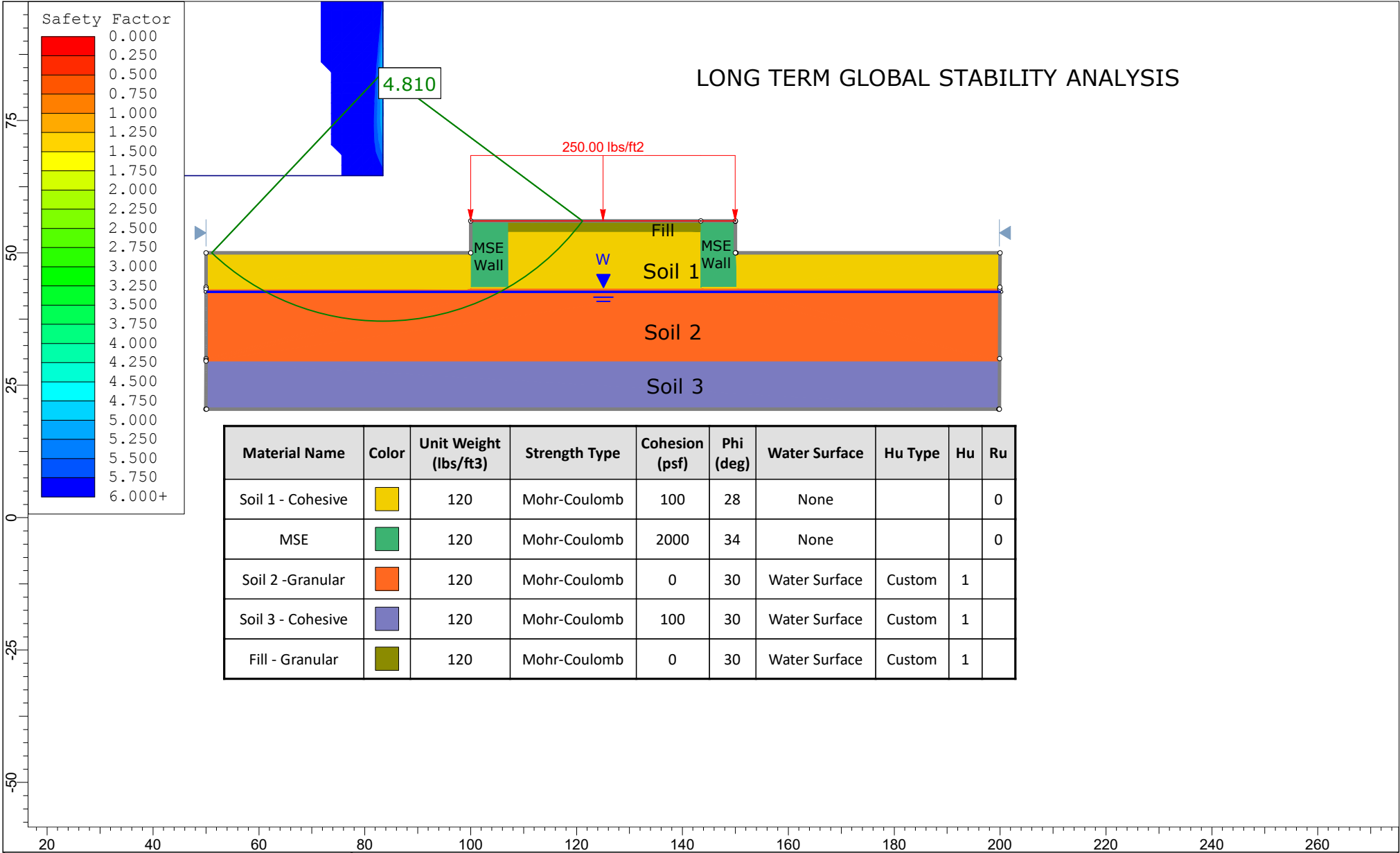
<b>Unconfined Compressive Strength =</b>	274.9 kPa <b>5740 psf</b>
<b>Shear Strength =</b>	137 kPa 2871 psf
<b>Strain at Failure =</b>	8.4 %

Remarks:


## **Appendix D**

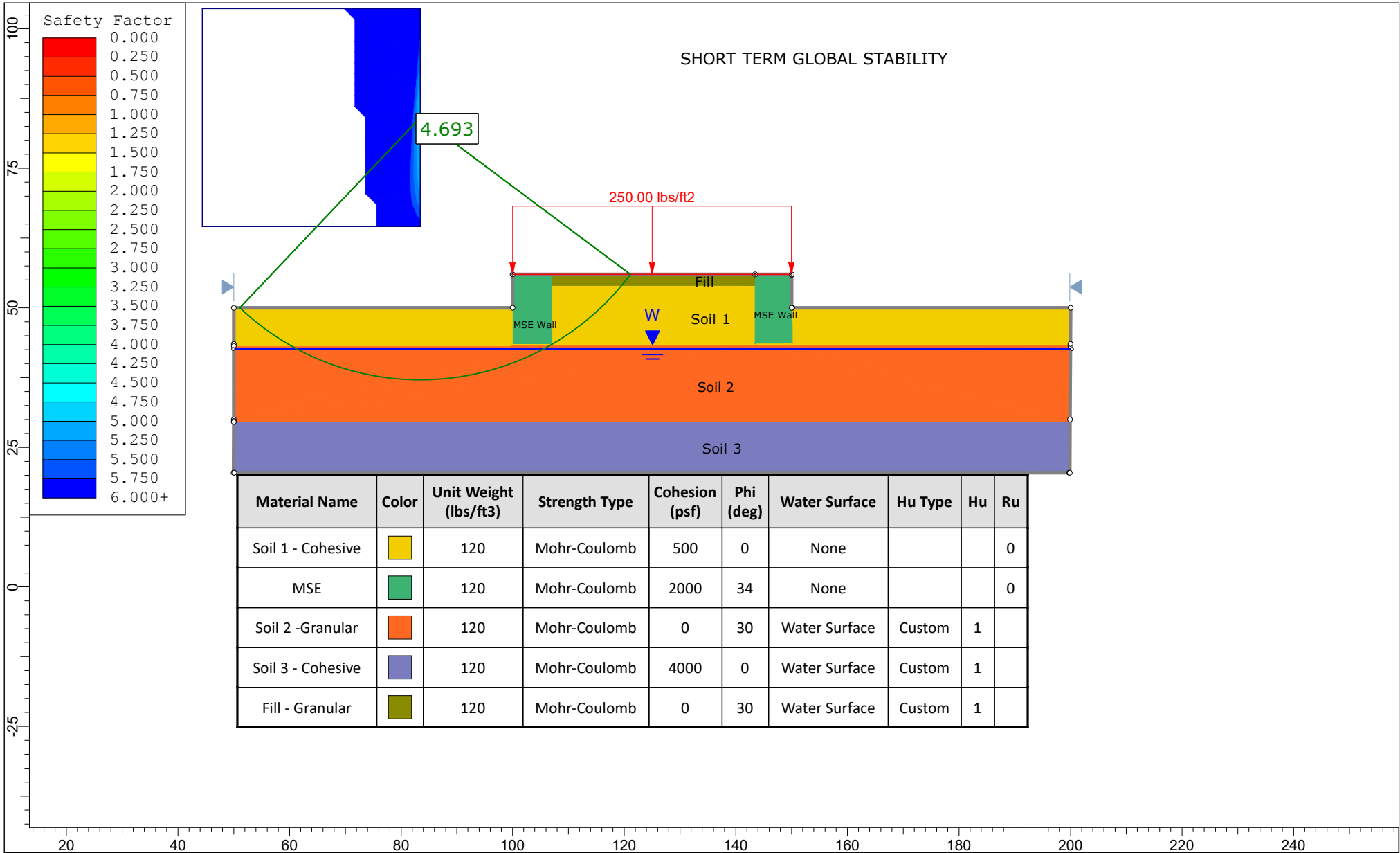
### Retaining Wall Global Slope Stability Analysis Results

# LONG TERM GLOBAL STABILITY ANALYSIS



Material Name	Color	Unit Weight (lbs/ft3)	Strength Type	Cohesion (psf)	Phi (deg)	Water Surface	Hu Type	Hu	Ru
Soil 1 - Cohesive	<span style="display:inline-block; width:15px; height:15px; background-color:yellow;"></span>	120	Mohr-Coulomb	100	28	None			0
MSE	<span style="display:inline-block; width:15px; height:15px; background-color:green;"></span>	120	Mohr-Coulomb	2000	34	None			0
Soil 2 - Granular	<span style="display:inline-block; width:15px; height:15px; background-color:orange;"></span>	120	Mohr-Coulomb	0	30	Water Surface	Custom	1	
Soil 3 - Cohesive	<span style="display:inline-block; width:15px; height:15px; background-color:purple;"></span>	120	Mohr-Coulomb	100	30	Water Surface	Custom	1	
Fill - Granular	<span style="display:inline-block; width:15px; height:15px; background-color:olive;"></span>	120	Mohr-Coulomb	0	30	Water Surface	Custom	1	

	<i>Project</i> US 20-MSE Retaining Walls, <b>JOB D-91-476-16</b>			
	<i>Analysis Description</i> GLOBAL STABILITY ANALYSIS			
	<i>Drawn By</i>	<i>Scale</i> 1:301	<i>Company</i> INTERRA, Inc.	
	<i>Date</i> 10/13/17	<i>File Name</i> Retaining Wall-Long Term.slim		



	Project			US 20-MSE Retaining Walls, JOB D-91-476-16		
	Analysis Description			GLOBAL STABILITY ANALYSIS		
	Drawn By	Scale	Company	INTERRA, Inc.		
	Date	10/13/17	File Name	Retaining Wall.slim		



## **Appendix E**

### Roadway Plan & Profile

